FILE NOTATIONS

Entered in NID File ...✓...
Location Map Pinned ...✓...
Card Indexed ...✓...

Checked by Chief PWB
Approval Letter 6-20-74
Disapproval Letter .....

COMPLETION DATA:

Date Well Completed 9-3-74

Location Inspected .....

W..... WW..... TA.....
OW..... OS..... PA...✓...

Bond released
State or Fee Land .....

LOGS FILED

Driller's Log.....✓.....
Electric Logs (No.) ...✓...
E..... I..... Dual I Lat..... GR-N..... Micro.....
BHC Sonic GR..... Lat..... ML-L..... Sonic.....
CBLog..... CCLog..... Others.....

Form 9-331 C
(May 1963)

SUBMIT IN TRIPLICATE*
(Other instructions on reverse side)

Form approved.
Budget Bureau No. 42-R1425.

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

APPLICATION FOR PERMIT TO DRILL, DEEPEN, OR PLUG BACK

5. LEASE DESIGNATION AND SERIAL NO.: Tully-Federal U-8350

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

7. UNIT AGREEMENT NAME:

8. FARM OR LEASE NAME:

9. WELL NO.: 1

10. FIELD AND POOL, OR WILDCAT: Wildcat

11. SEC., T., R., M., OR BLK. AND SURVEY OR AREA: 27-4S-22E

12. COUNTY OR PARISH: Uintah

13. STATE: Utah

1a. TYPE OF WORK: DRILL [X] DEEPEN [ ] PLUG BACK [ ]

b. TYPE OF WELL: OIL WELL [X] GAS WELL [X] OTHER SINGLE ZONE [X] MULTIPLE ZONE [ ]

2. NAME OF OPERATOR: Westates Petroleum Company

3. ADDRESS OF OPERATOR: 1600 Broadway, Suite 2360; Denver, Colorado 80202

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements.*)
At surface: 390' fr. S.L., 2100 fr. EL (State variance is being requested)
At proposed prod. zone: Same SW SW SE

14. DISTANCE IN MILES AND DIRECTION FROM NEAREST TOWN OR POST OFFICE*:

15. DISTANCE FROM PROPOSED* LOCATION TO NEAREST PROPERTY OR LEASE LINE, FT. (Also to nearest drlg. unit line, if any): 390

16. NO. OF ACRES IN LEASE: 760.00

17. NO. OF ACRES ASSIGNED TO THIS WELL: 40

18. DISTANCE FROM PROPOSED LOCATION* TO NEAREST WELL, DRILLING, COMPLETED, OR APPLIED FOR, ON THIS LEASE, FT.:

19. PROPOSED DEPTH: 4270

20. ROTARY OR CABLE TOOLS: Rotary

21. ELEVATIONS (Show whether DF, RT, GR, etc.): 5085 Gr. (Topo)

22. APPROX. DATE WORK WILL START*: July 5, 1974

23. PROPOSED CASING AND CEMENTING PROGRAM

SIZE OF HOLE	SIZE OF CASING	WEIGHT PER FOOT	SETTING DEPTH	QUANTITY OF CEMENT
13"	9 5/8" new	36#	300'	Sufficient to circulate
8 3/4"	7" new	23#	4270'	500 sacks minimum

Well is to test Weber Sand. If productive, will be completed through casing perforations. A 10" Series 900 S.S. Cameron Hydraulic double gate BOP will be flanged to a 10" Series 900 casing head. The BOP is equipped with an 80 gallon Koomey accumulator remote control closing unit. Kill and choke lines will be installed on the BOP. Maximum anticipated BHP @ 300 is 100#, and at T.D. is 1500#. Water base mud will be used and weight will be adequate for control of well at all times.

Sub C-3

IN ABOVE SPACE DESCRIBE PROPOSED PROGRAM: If proposal is to deepen or plug back, give data on present productive zone and proposed new productive zone. If proposal is to drill or deepen directionally, give pertinent data on subsurface locations and measured and true vertical depths. Give blowout preventer program, if any.

24. SIGNED: Gustav E. Swan TITLE: Area Manager, Rocky Mtn.-Mid Cont. Area DATE: June 11, 1974

(This space for Federal or State office use)

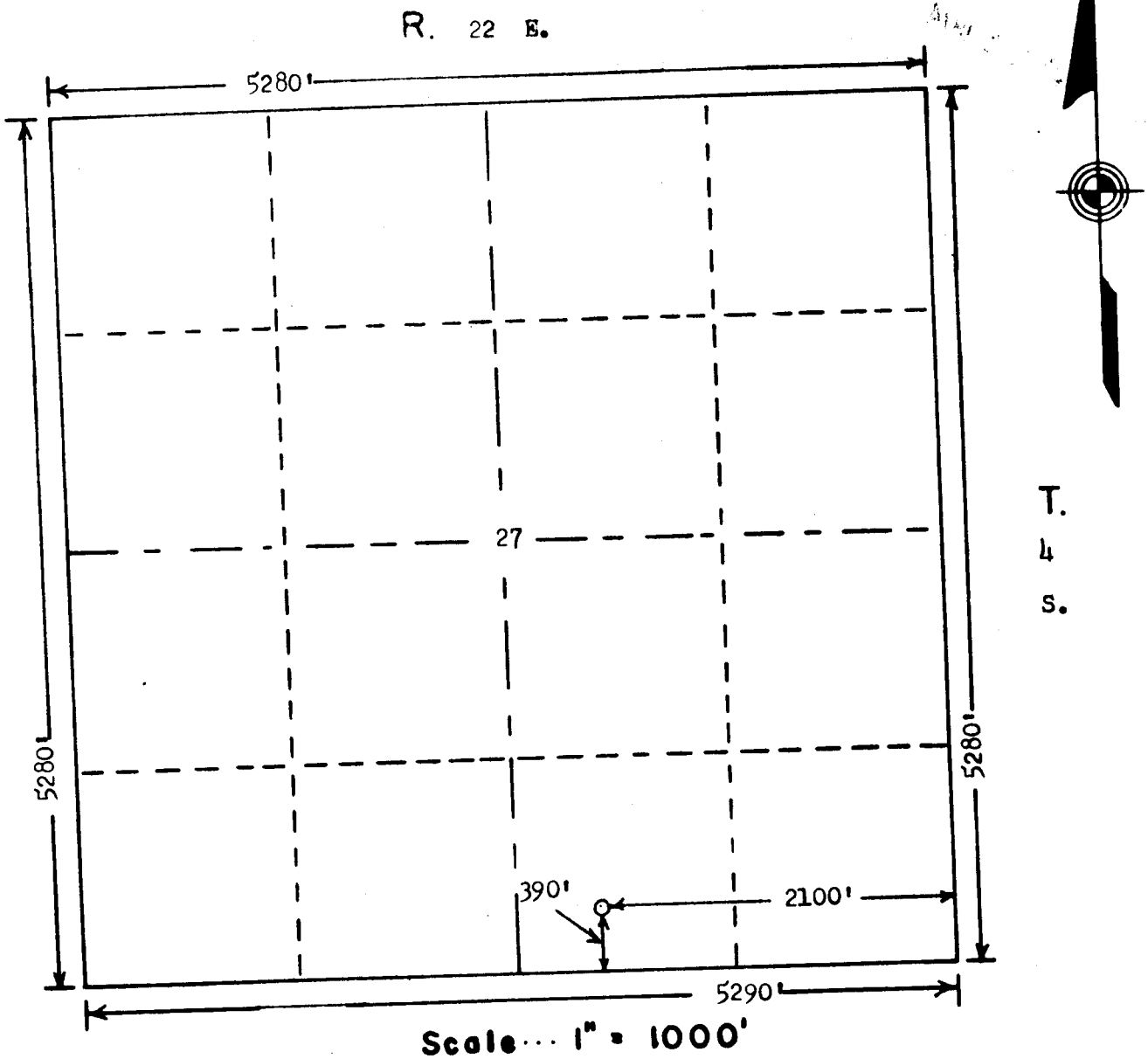
PERMIT NO. 43-047-30177 APPROVAL DATE

APPROVED BY TITLE DATE

CONDITIONS OF APPROVAL, IF ANY:

*See Instructions On Reverse Side

FORM F-106



Scale··· 1" = 1000'

Powers Elevation Company, Inc. of Denver, Colorado has in accordance with a request from Burt Dunn for Westates Petroleum Company determined the location of #1 Tully-Federal to be 390'FS & 2100'FE Section 27 Township 4 S. Range 22 E. of the Salt Lake Principal Meridian Uintah County, Utah

I hereby certify that this plat is an accurate representation of a correct survey showing the location of #1 Tully-Federal

Date: 6-11-74

Darrell T White
Licensed Land Surveyor No. 2658PE
State of Utah

DEVELOPMENT PLAN

1. Map attached (Naples, Utah Quadrangle) shows existing roads.

2. Planned access roads are shown on map in 1. above. Blading will be done only if necessary.

3. Locations of existing wells are shown on map in 1. above.

4. Lateral road to location of well to be drilled is shown on map referred to in 1. above.

5. A plat attached shows probable location of tank battery and flow lines. There are no existing flow lines or batteries within a half-mile radius of the proposed location.

6. Rivers, creeks, lakes, etc. are shown on the map in 1. above. Which reservoir or stream to be used in drilling operations is not now known.

7. All waste material will be buried.

8. There will not be any camps.

9. No airstrips will be used.

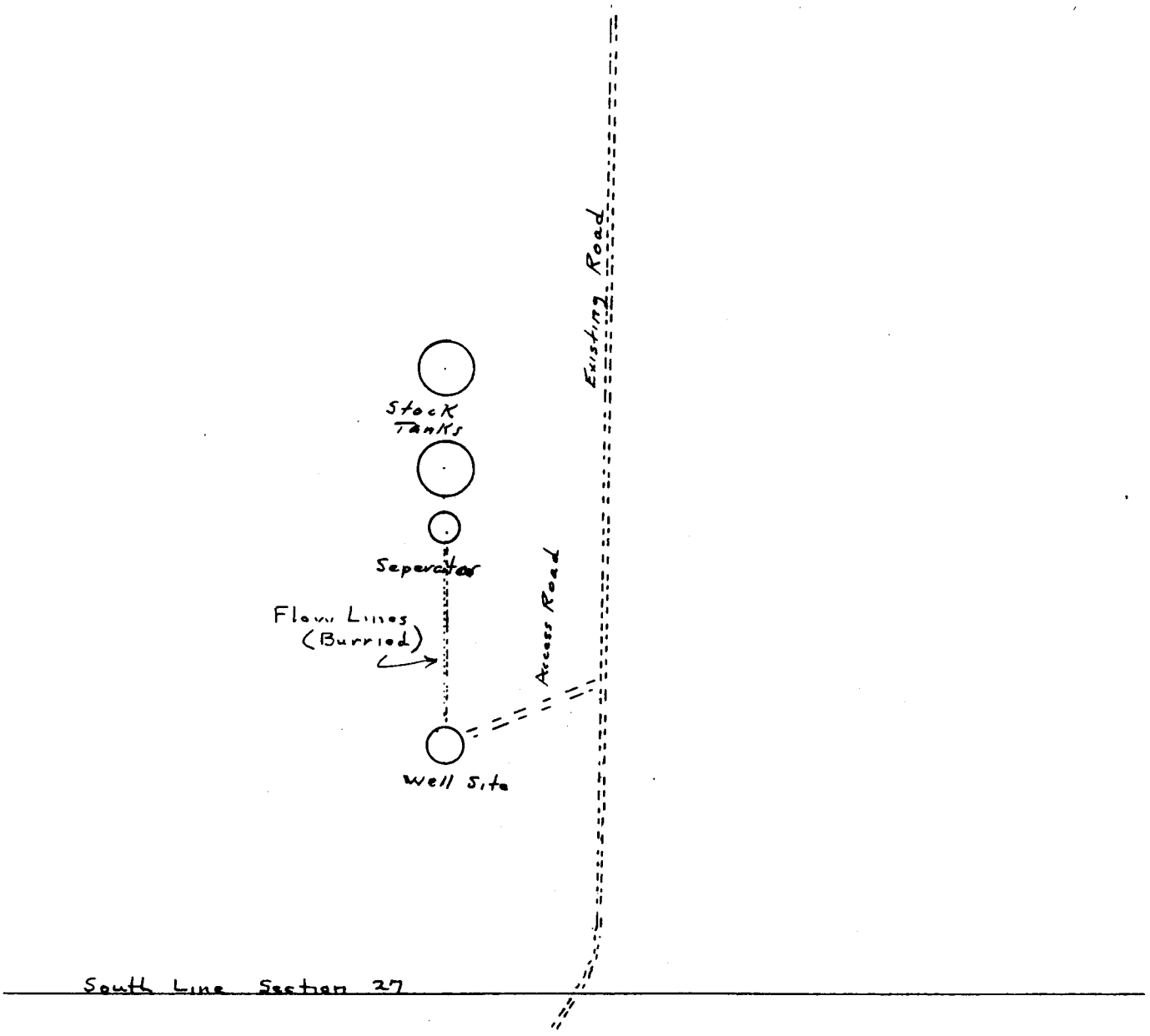
10. Plat is attached showing rig layout.

11. After drilling is completed, the surface of the ground will be restored to as near as practicable its present condition.

12. The location dips gently eastward, vegitation is sparse.

WESTATES PETROLEUM COMPANY #1 WEST

5. Location of tank battery and flow lines.

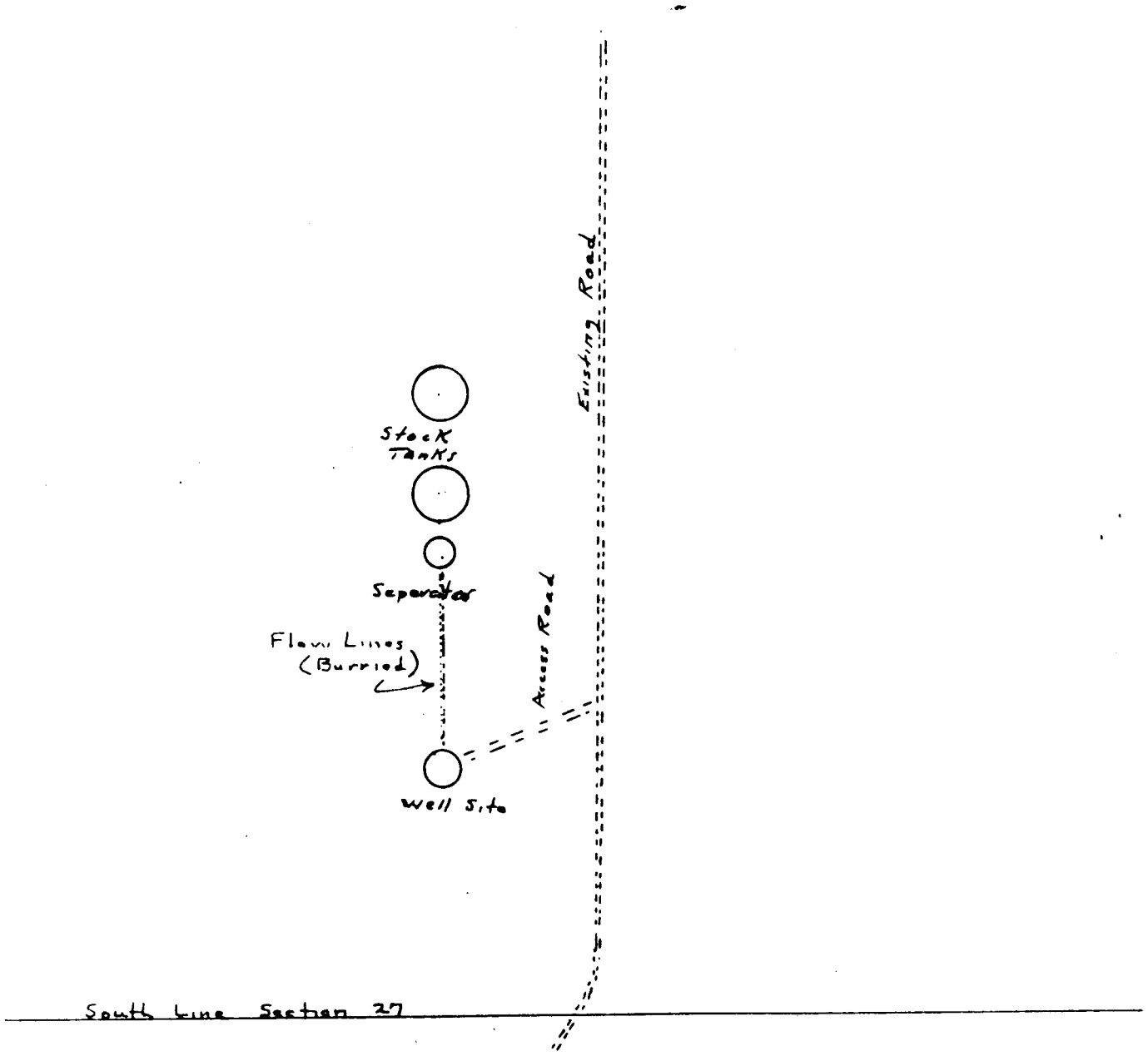


Please note
attached Corrected
Sheet to be filed
with our Application
for Permit To Drill!
Thank you

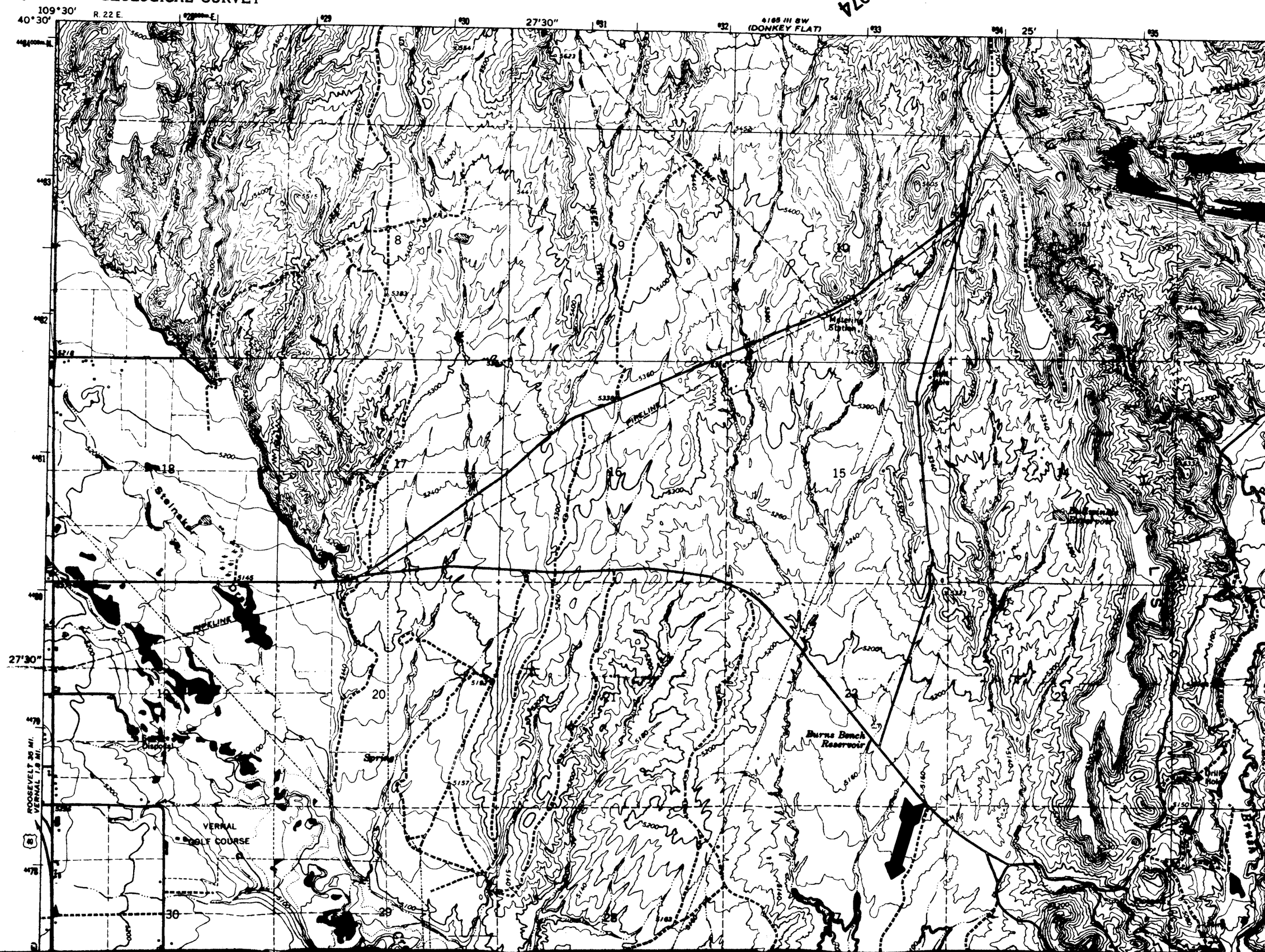
WESTATES #1 TULLY- FEDERAL

Correction: 6/14/74

5. Location of tank battery and flow lines.



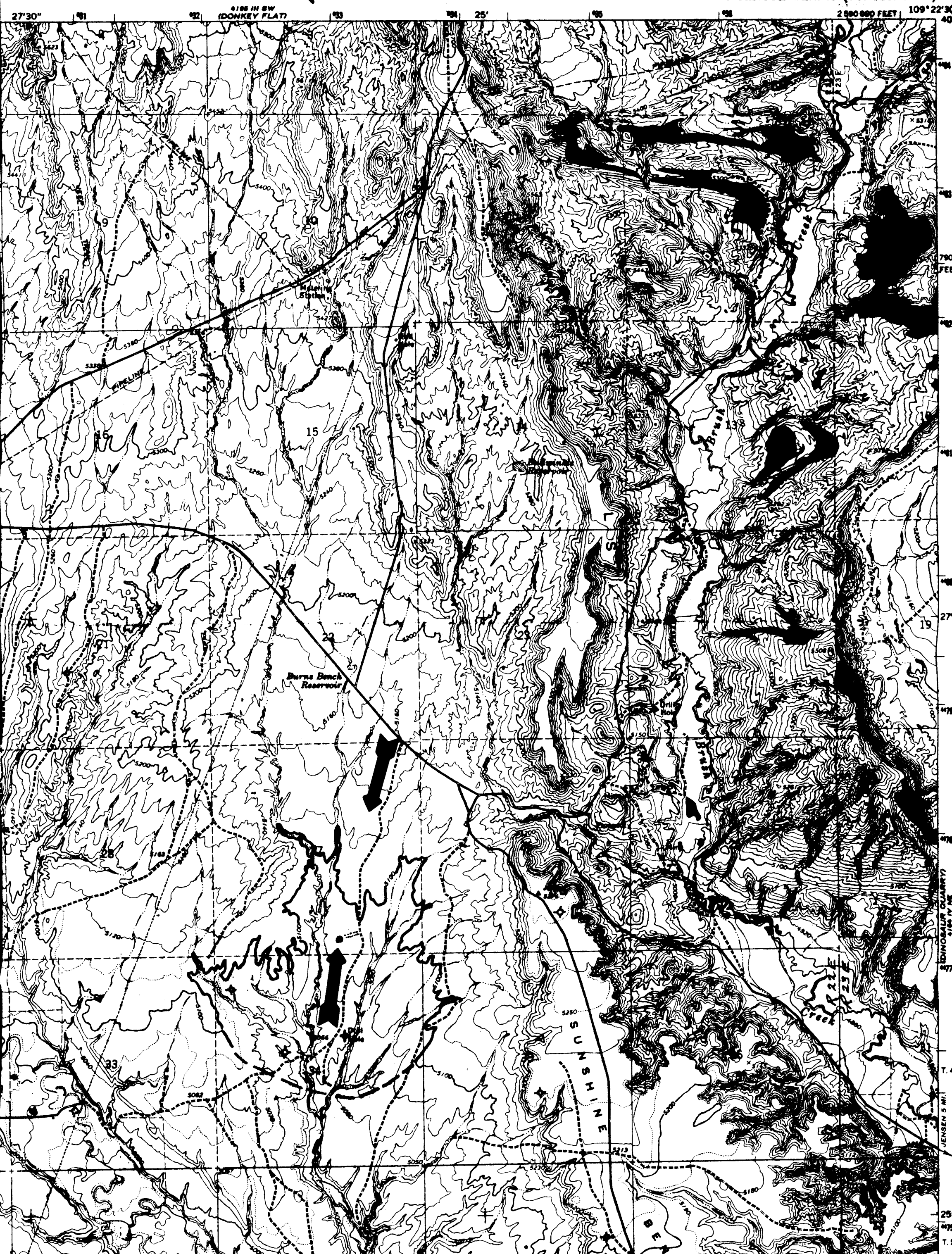
UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

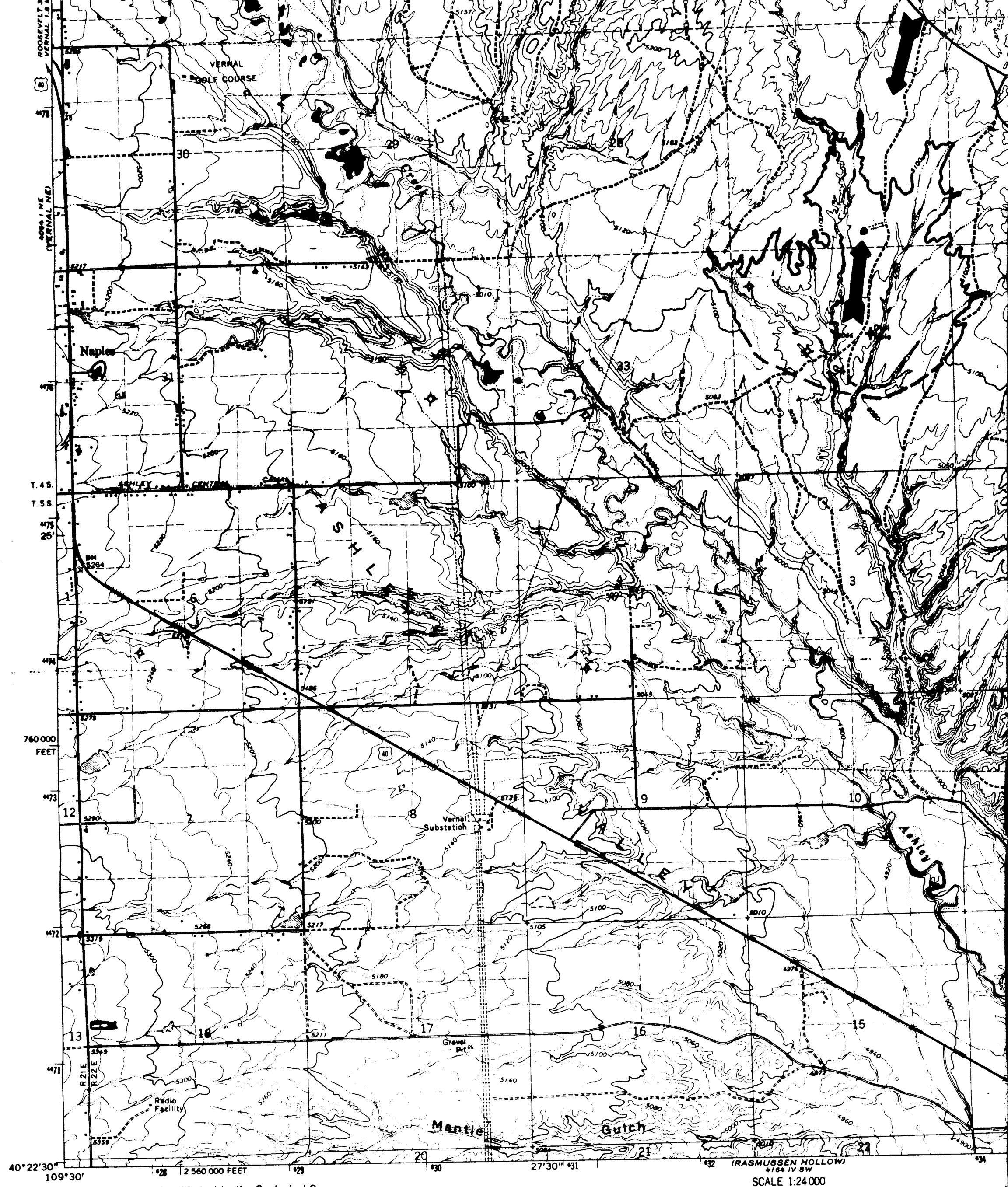


JUN 17 1974

JUN 17 1974

NAPLES QUADRANGLE
UTAH–UINTAH CO.
7.5 MINUTE SERIES (TOPOGRAPHIC)





Mapped, edited, and published by the Geological Survey in cooperation with the Bureau of Reclamation

Control by USGS USC&GS. and USBR

Topography by photogrammetric methods from aerial photographs taken 1964 and planetable surveys by USBR 1955
Field checked 1965

Polyconic projection. 1927 North American datum
10,000-foot grid based on Utah coordinate system, central zone
1000-meter Universal Transverse Mercator grid ticks, zone 12, shown in blue

Fine red dashed lines indicate selected fence lines

GN MN
1°01′ 18 MILS
15½° 276 MILS

UTM GRID AND 1965 MAGNETIC NORTH DECLINATION AT CENTER OF SHEET

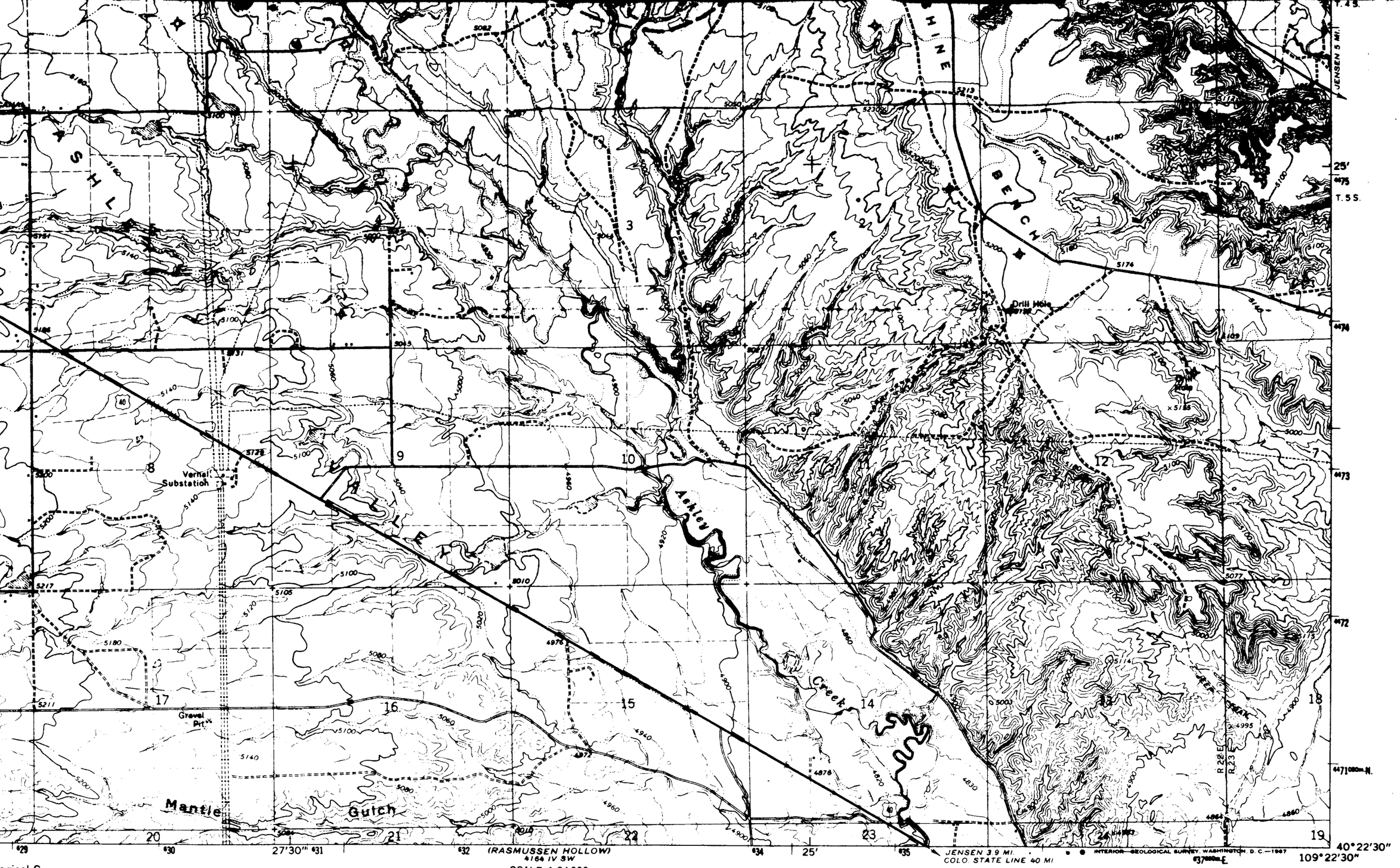
SCALE 1:24 000

1000 0 1000 2000 3000 4000 5000 6000 7000 FEET

1 .5 0 1 KILOMETER

CONTOUR INTERVAL 20 FEET
DOTTED LINES REPRESENT 10-FOOT CONTOURS
DATUM IS MEAN SEA LEVEL

THIS MAP COMPLIES WITH NATIONAL MAP ACCURACY STANDARDS
FOR SALE BY U. S. GEOLOGICAL SURVEY, DENVER, COLORADO 80225, OR WASHINGTON, D. C.
A FOLDER DESCRIBING TOPOGRAPHIC MAPS AND SYMBOLS IS AVAILABLE ON REQUEST

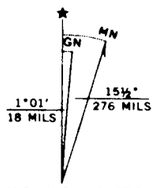


ogical Survey
tion

erial
by USBR 1955

um
m, central zone
icks.

s



UTM GRID AND 1965 MAGNETIC NORTH DECLINATION AT CENTER OF SHEET

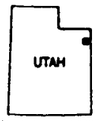
SCALE 1:24 000

1 ½ 0 1 MILE

1000 0 1000 2000 3000 4000 5000 6000 7000 FEET

1 .5 0 1 KILOMETER

CONTOUR INTERVAL 20 FEET
DOTTED LINES REPRESENT 10-FOOT CONTOURS
DATUM IS MEAN SEA LEVEL



QUADRANGLE LOCATION

ROAD CLASSIFICATION

Heavy-duty
Light-duty
Medium-duty
Unimproved dirt
U. S. Route

THIS MAP COMPLIES WITH NATIONAL MAP ACCURACY STANDARDS
FOR SALE BY U. S. GEOLOGICAL SURVEY, DENVER, COLORADO 80225, OR WASHINGTON, D. C. 20242
A FOLDER DESCRIBING TOPOGRAPHIC MAPS AND SYMBOLS IS AVAILABLE ON REQUEST

NAPLES, UTAH

N4022.5—W10922.5/7.5

1965

AMS 4164 IV NW—SERIES V897

WESTATES PETROLEUM COMPANY

SUITE 2360, 1600 BROADWAY | DENVER, COLORADO 80202 | (303) 825-2854

June 13, 1974

Mr. Cleon B. Feight, Director
Utah Division
Oil and Gas Conservation Commission
1588 West, North Temple
Salt Lake City, UT 84116

Dear Mr. Feight:

Pursuant to our telephone conversation this date, enclosed in triplicate are copies of the Application For Permit To Drill, Deepen, Or Plug Back (Form 9-331C) relative to Westates #1 Tully-Federal in Section 27-4S-22E. Also enclosed are copies of a letter addressed to you from Westates Area Exploration Manager stating the reasons for requesting a drill site less than 500' from the nearest property line. The location is being staked and survey plats will be forwarded to you when they become available.

Thank you very much.

Very truly yours,

Burton C. Dunn

Burton C. Dunn - Area Manager
Rocky Mtn. - Mid Continent Area

BCD/khw

Enclosures

WESTATES PETROLEUM COMPANY

SUITE 2360, 1600 BROADWAY | DENVER, COLORADO 80202 | (303) 825-2854

June 13, 1974

Mr. Cleon B. Feight, Director
Utah Division
Oil and Gas Conservation Commission
1588 West, North Temple
Salt Lake City, UT 84116

Dear Mr. Feight:

We are requesting a variance from the spacing requirements for our Westates #1 Tully-Federal Well for the following reasons:

1. Our control indicates the well is being drilled on a rather tightly folded nose extending off the Split Mountain Anticline. Dips on both flanks are quite steep, and we would like to locate the well so as to penetrate the objective sands as nearly as possible on the crest of the fold. Wells drilled down plunge to the west indicated water was present in our objective zones, so we feel it is imperative to get as high a structural location as possible on this feature.

2. Westates controls the lease to the south of the requested location, so we should not have ownership problems.

Thank you very much.

Very truly yours,

Stanley D. Conrad

Stanley D. Conrad
Area Exploration Manager

SDC/khw

WESTATES PETROLEUM COMPANY

SUITE 2360, 1600 BROADWAY | DENVER, COLORADO 80202 | (303) 825-2854

June 14, 1974

State of Utah
Department of Natural Resources
Division of Oil and Gas Conservation
1588 West, North Temple
Salt Lake City, UT 84116
ATTN: CLEON B. FEIGHT, DIRECTOR

Re: Westates #1 Tully-Federal
Section 27-4S-22E
Uintah County, Utah

Gentlemen:

Enclosed are three (3) copies of the Surveyor's Plat which should be attached to the Application For Permit to Drill (Form 9-331C) previously filed with you.

Thank you.

Very truly yours,

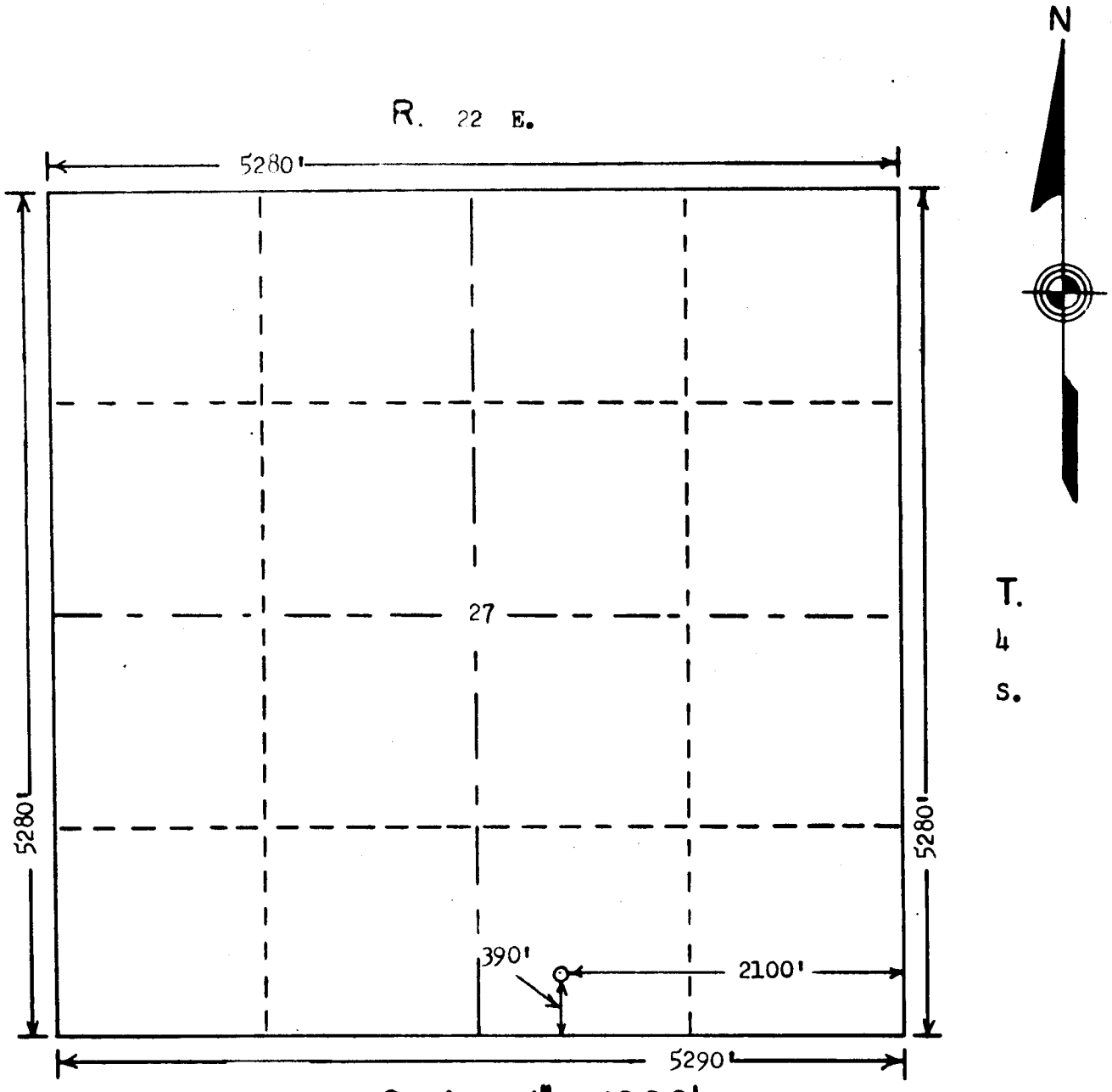
Burton C. Dunn

Burton C. Dunn - Area Manager
Rocky Mtn. - Mid Continent Area

BCD/khw

Enclosures

FORM



Scale··· 1" = 1000'

Powers Elevation Company, Inc. of Denver, Colorado
has in accordance with a request from Burt Dunn
for Westates Petroleum Company
determined the location of #1 Tully-Federal
to be 390'FS & 2100'FE **Section** 27 **Township** 4 S.
Range 22 E. of the Salt Lake Principal **Meridian**
Uintah **County,** Utah

I hereby certify that this plat is an accurate representation of a correct survey showing the location of
#1 Tully-Federal

Date: 6-11-74

Darrell T White
Licensed Land Surveyor No. 2658PE
State of Utah

June 20, 1974

Westates Petroleum Company
1600 Broadway
Denver, Colorado 80202

Re: Well No. Tully-Federal #1
Sec. 27, T. 4 S, R. 22 E,
Uintah County, Utah

Gentlemen:

Insofar as this office is concerned, approval to drill the above referred to well is hereby granted in accordance with Rule C-3(c) of the General Rules and Regulations and Rules of Practice and Procedure.

Should you determine that it will be necessary to plug and abandon this well, you are hereby requested to immediately notify the following:

PAUL W. BURCHELL - Chief Petroleum Engineer
HOME: 277-2890
OFFICE: 328-5771

Enclosed please find Form OGC-8-X, which is to be completed whether or not water sands (aquifers) are encountered during drilling. Your cooperation relative to the above will be greatly appreciated.

The API number assigned to this well is 43-047-30177.

Very truly yours,

DIVISION OF OIL & GAS CONSERVATION

CLEON B. FEIGHT
DIRECTOR

CBF:sw
cc: U.S. Geological Survey

P 2 pl

File in Duplicate

DIVISION OF OIL AND GAS CONSERVATION

OF THE STATE OF UTAH

DESIGNATION OF AGENT

* * * * * * * * * * *

The undersigned producer, operator, transporter, refiner, gasoline or initial purchaser who is conducting oil and/or gas operations in the State of Utah, does, pursuant to the Rules and Regulations and Rules of Practice and Procedure of the Division of Oil and Gas Conservation of the State of Utah, hereby appoint C. T. Corporation System, whose address is 176 South Main; Salt Lake City, UT 84111, ~~xxxxxxxxxx~~ its) designated agent to accept and to be served with notices from said Board, or from other persons authorized under the Oil and Gas Conservation Act of the State of Utah.

The undersigned further agrees to immediately report in writing, all changes of address of the agent, and any termination of the agent's authority, and in the latter case, the designation of a new agent or agents shall be immediately made. This designation of agent, however, shall remain in full force and effect until and unless a new designation agent is filed in accordance with said statute and said regulations.

Effective date of designation June 24, 1974

Company Westates Petroleum Company Address 1600 Broadway, Suite 2360 Denver, CO 80004

By Burton C. Dunn (signature) Burton C. Dunn Title Area Manager Rocky Mtn. - Mid Continent Area

NOTE: Agent must be a resident of the State of Utah

FORM OGC-8-X
File in Quadruplicate

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL AND GAS CONSERVATION
1588 West North Temple
Salt Lake City, Utah 84116

REPORT OF WATER ENCOUNTERED DURING DRILLING

Well Name and Number Tully-Federal #1

Operator Westates Petroleum Company

Address 1600 Broadway, Suite 2360 - Denver, Colorado 80202

Contractor Signal Drilling Company

Address 1200 Security Life Building - Denver, Colorado 80202

Location SW 1/4, SE 1/4; Sec. 27 ; T. 4 ~~N~~ S; R. 22 E ~~W~~:, Uintah County.

Water Sands:

	Depth: From - To -	Volume: Flow Rate or Head -	Quality: Fresh or Salty -
1.	D.S.T. 4745-4835 in Weber Sand	Rec. total fluid of 3370' of watery mud and water in 90' flow time, probably would have flowed to surface	Fresh, tested 215 ppm chlorides at 92°F
2.			
3.	NOTE: The Frontier, Dakota, Entrada and Shinarump Sands all indicated porosity from cuttings and e logs but were not tested. Resistivity and S.P. logs		
4.	indicated reasonably fresh water was probably present in all these sands.		
5.			

(Continue on Reverse Side of Necessary)

Formation Tops:

NOTE: (a) Upon diminishing supply of forms, please inform this office.
(b) Report on this form as provided for in Rule C-20, General Rules and Regulations and Rules of Practice and Procedure.
(c) If a water quality analysis has been made of the above reported zone, please forward a copy along with this form.

Rcy to O. S. Leafhauer
1 cy to Frank Tully
1 cy to Robert Ferguson
9-6-74

JOHNSTON

Schlumberger

technical report

COMPANY WESTATES PETROLEUM CO. WELL TULLY FEDERAL #1 TEST NO. 1 COUNTY UINTAH STATE UTAH

F.R. #04245 C

JOHNSTON
...found a better way

SURFACE INFORMATION

Description (Rate of Flow)	Time	Pressure (P.S.I.G.)	Surface Choke
Opened Tool	1630	-	-
PACKER SEAT FAILED			

Cushion Type	Amount	Pressure	Bottom Choke
	-		Size 3/4"

MUD DATA

Mud Type GEL Wt. 9
Viscosity 55 Water Loss - C.C.
Resist: of Mud - @ - °F; of Filtrate - @ - °F
Chloride Content - PPM

EQUIPMENT & HOLE DATA

Type Test M. F. E. OPEN HOLE
Formation Tested MORRISON
Elevation - Ft.
Net Productive Interval - Ft.
Estimated Porosity 15 %
All Depths Measured From KELLY BUSHING
Total Depth ~~1785~~ 1735 Ft.
Main Hole/Casing Size -
Rat Hole/Liner Size -
Drill Collar Length 323' I.D. -
Drill Pipe Length 1355' I.D. -
Packer Depth(s) 1708' & 1719 Ft.

MULTI-FLOW EVALUATOR FLUID SAMPLE DATA

Sampler Pressure _____ P.S.I.G. at Surface
Recovery: Cu. Ft. Gas _____
cc. Oil _____
cc. Water _____
cc. Mud _____
Tot. Liquid cc. _____
Gravity _____ °API @ _____ °F.
Gas/Oil Ratio _____ cu. ft./bbl.

	RESISTIVITY	CHLORIDE CONTENT
Recovery Water	@ °F.	ppm
Recovery Mud	@ °F.	
Recovery Mud Filtrate	@ °F.	ppm
Mud Pit Sample	@ °F.	
Mud Pit Sample Filtrate	@ °F.	ppm

RECOVERY DESCRIPTION	FEET	BARRELS	% OIL	% WATER	% OTHERS	API GRAVITY	RESISTIVITY	CHL. PPM
NORMAL HOLE FLUID	120	-				@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	

Remarks: UNSUCCESSFUL TEST; PACKER SEAT FAILURE. HAD ABOUT 4' OF FILL-UP ON BOTTOM.

Address 1600 BROADWAY; ROOM 2360; DENVER, COLORADO 80202

Company WESTATES PETROLEUM COMPANY Field WILD CAT
Well TULLY FEDERAL #1 Location -
Test Interval 1719' TO 1785' (UNSUCCESSFUL) Test # 1 Date 8-8-74

County UINTAH State UTAH
Technician MC LAUGHLIN (VERNAL) Test Approved By MR. BURTON DUNN

Field Report No. 04245 C
No. Reports Requested 5

JOHNSTON
...found a better way

PRESSURE DATA

Instrument No.		J-405			Field Report No. 04245 C
Capacity (P.S.I.G.)		2800			
Instrument Depth		1731'			
Instrument Opening		OUTSIDE			TIME DATA
Pressure Gradient P.S.I./Ft.					
Well Temperature °F.		108			Time Given / Time Computed
Initial Hydrostatic Mud	A	863			
Initial Shut-in	B	-			- Mins. / Mins.
Initial Flow	C	-			- Mins. / Mins.
					- Mins. / Mins.
					- Mins. / Mins.
Final Flow	D	-			- Mins. / Mins.
Final Shut-in	E	-			- Mins. / Mins.
Final Hydrostatic Mud	F	-			

Remarks:

UNSUCCESSFUL TEST.

*Shut in pressure did not reach static reservoir pressure.

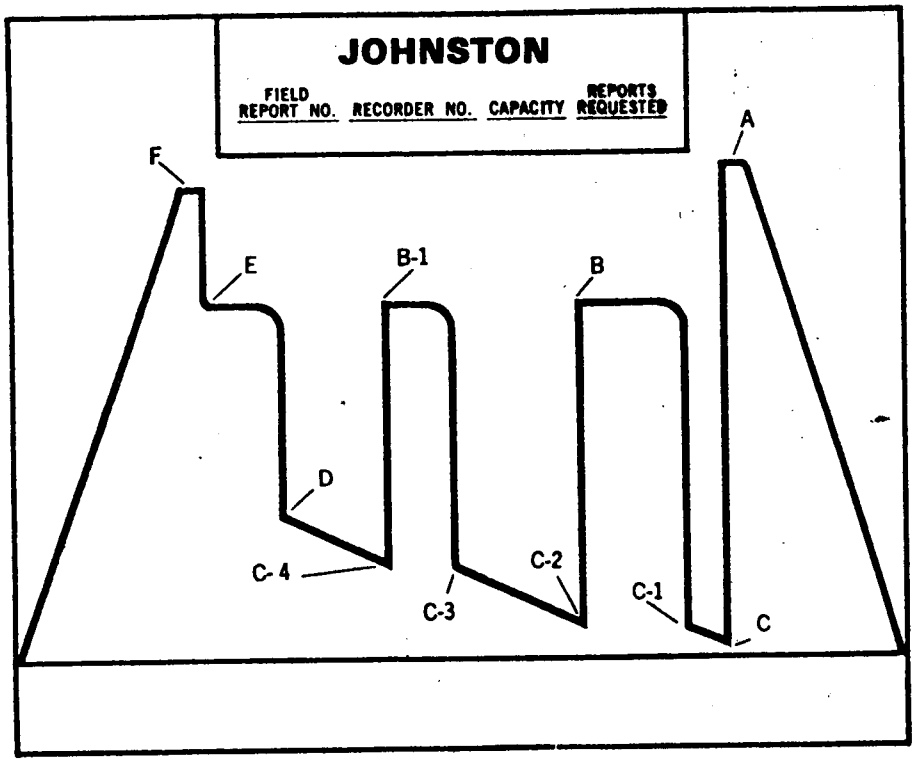
Clock Travel _____ inches per min.

PRESSURE INCREMENTS

Point Minutes	Pressure	$\frac{T+\Delta t}{\Delta t}$	Point Minutes	Pressure	$\frac{T+\Delta t}{\Delta t}$	Point Minutes	Pressure	$\frac{T+\Delta t}{\Delta t}$

JOHNSTON
...found a better way

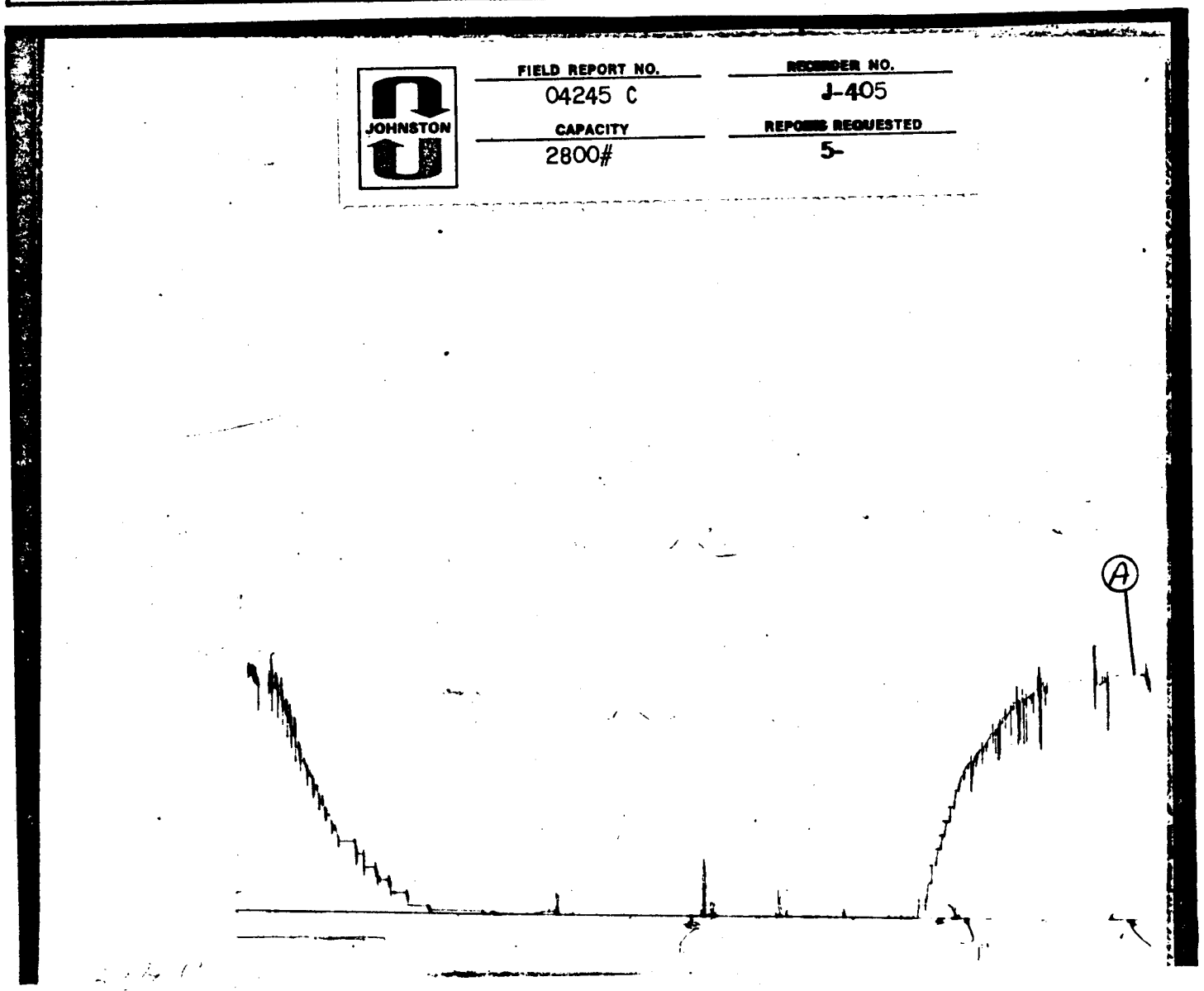
GUIDE TO IDENTIFICATION OF DRILL STEM TEST PRESSURE CHARTS



A. Initial Hyd. Mud
B. Initial Shut-in
C. Initial Flow
D. Final Flow
E. Final Shut-in
F. Final Hyd. Mud

The following points are either fluctuating pressures or points indicating other packer settings, (testing different zones).

A-1, A-2, A-3, etc. Initial Hyd. Pressures
B-1, B-2, B-3, etc. Subsequent Shut-in Pressures
C-1, C-2, C-3, etc. Flowing Pressures
D-1, D-2, D-3, etc. Subsequent Final Flow Pressures
E-1, E-2, E-3, etc. Subsequent Final Shut-in Pressures
F-1, F-2, F-3, etc. Final Hyd. Mud Pressures
Z—Special pressure points such as pumping pressure recorded for formation breakdown.



```
****************
*              *
****************
* SCHLUMBERGER *
****************
```

DIRECTIONAL

SURVEY

******

D-1473 DIRECTIONAL SURVEY INTEGRATION PROGRAM FOR 6050

WESTATES WILDCAT

TULLY FEDERAL NO. 1 UINTAH COUNTY, UTAH

RUN NO. ONE 289 - 4830 SEPTEMBER 2, 1974 D-1473

START DEPTH OF SURVEY IS 289 FEET

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
289	.2	70	.00	289.00	.00	.00	.00	.00
336	.2	70	.16	336.00	.15	.06	.15	.06
340	.2	69	.01	340.00	.01	.01	.17	.06
344	.3	69	.02	344.00	.02	.01	.19	.07
348	.4	70	.03	348.00	.03	.01	.21	.08
352	.4	70	.03	352.00	.03	.01	.24	.09
356	.3	73	.02	356.00	.02	.01	.26	.09
360	.4	76	.03	360.00	.03	.01	.29	.10
364	.3	75	.02	364.00	.02	.01	.31	.11
368	.3	73	.02	368.00	.02	.01	.33	.11
372	.3	72	.02	372.00	.02	.01	.35	.12
376	.6	73	.04	376.00	.04	.01	.39	.13
380	.6	76	.04	380.00	.04	.01	.43	.14
384	.4	78	.03	384.00	.03	.01	.45	.15
388	.4	82	.03	388.00	.03	.00	.48	.15
392	.4	85	.03	392.00	.03	.00	.51	.15
396	.6	85	.04	396.00	.04	.00	.55	.16
400	.6	85	.04	400.00	.04	.00	.59	.16
404	.4	86	.03	404.00	.03	.00	.62	.16
408	.4	81	.03	408.00	.03	.00	.65	.17
412	.6	74	.04	412.00	.04	.01	.69	.18
416	.6	73	.04	416.00	.04	.01	.73	.19
420	.6	74	.04	420.00	.04	.01	.77	.20
424	.6	75	.04	424.00	.04	.01	.81	.21
428	.7	74	.05	428.00	.05	.01	.86	.23
432	.5	72	.03	432.00	.03	.01	.89	.24
436	.5	71	.03	436.00	.03	.01	.92	.25
440	.7	68	.05	440.00	.05	.02	.97	.27
444	.5	66	.03	444.00	.03	.01	1.00	.28
448	.5	66	.03	448.00	.03	.01	1.03	.30
452	.4	69	.03	452.00	.03	.01	1.06	.31
456	.6	69	.04	456.00	.04	.02	1.10	.32
460	.9	66	.06	459.99	.06	.03	1.15	.35
464	.9	64	.06	463.99	.06	.03	1.21	.37
468	.7	63	.05	467.99	.04	.02	1.25	.40
472	.6	63	.04	471.99	.04	.02	1.29	.41
476	.5	61	.03	475.99	.03	.02	1.32	.43
480	.6	59	.04	479.99	.04	.02	1.36	.45
484	.9	61	.06	483.99	.05	.03	1.41	.48
488	.8	62	.06	487.99	.05	.03	1.46	.51
492	.7	61	.05	491.99	.04	.02	1.51	.53
496	.6	60	.04	495.99	.04	.02	1.54	.55
500	.7	60	.05	499.99	.04	.02	1.58	.58
504	.5	58	.03	503.99	.03	.02	1.61	.60
508	.4	55	.03	507.99	.02	.02	1.64	.61

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
512	.7	55	.05	511.99	.04	.03	1.68	.64
516	.8	56	.06	515.99	.05	.03	1.72	.67
520	.6	55	.04	519.99	.03	.02	1.76	.70
524	.7	54	.05	523.99	.04	.03	1.80	.73
528	.8	54	.06	527.99	.05	.03	1.84	.76
532	.6	54	.04	531.99	.03	.02	1.88	.78
536	.6	53	.04	535.99	.03	.03	1.91	.81
540	.5	50	.03	539.99	.03	.02	1.94	.83
544	.5	49	.03	543.99	.03	.02	1.96	.85
548	.8	48	.06	547.99	.04	.04	2.00	.89
552	.7	48	.05	551.99	.04	.03	2.04	.92
556	.7	49	.05	555.99	.04	.03	2.08	.96
560	.9	49	.06	559.99	.05	.04	2.12	1.00
564	.6	48	.04	563.99	.03	.03	2.16	1.02
568	.4	49	.03	567.99	.02	.02	2.18	1.04
572	.5	45	.03	571.99	.02	.02	2.20	1.07
576	.6	43	.04	575.99	.03	.03	2.23	1.10
580	.8	43	.06	579.99	.04	.04	2.27	1.14
584	.8	41	.06	583.99	.04	.04	2.30	1.18
588	.8	39	.06	587.99	.04	.04	2.34	1.22
592	.9	39	.06	591.99	.04	.05	2.38	1.27
596	1.0	40	.07	595.98	.04	.05	2.42	1.33
600	.9	43	.06	599.98	.04	.05	2.47	1.37
604	.7	44	.05	603.98	.03	.04	2.50	1.41
608	.8	43	.06	607.98	.04	.04	2.54	1.45
612	1.0	44	.07	611.98	.05	.05	2.59	1.50
616	1.1	45	.08	615.98	.05	.05	2.64	1.55
620	1.2	43	.08	619.98	.06	.06	2.70	1.61
624	1.2	44	.08	623.98	.06	.06	2.76	1.68
628	1.2	46	.08	627.98	.06	.06	2.82	1.73
632	1.0	47	.07	631.98	.05	.05	2.87	1.78
636	.9	48	.06	635.98	.05	.04	2.92	1.82
640	1.0	48	.07	639.98	.05	.05	2.97	1.87
644	.9	50	.06	643.98	.05	.04	3.02	1.91
648	.8	51	.06	647.98	.04	.04	3.06	1.95
652	.8	49	.06	651.98	.04	.04	3.10	1.98
656	.8	48	.06	655.98	.04	.04	3.14	2.02
660	.9	49	.06	659.98	.05	.04	3.19	2.06
664	.9	50	.06	663.98	.05	.04	3.24	2.10
668	.8	49	.06	667.97	.04	.04	3.28	2.14
672	.8	51	.06	671.97	.04	.04	3.32	2.17
676	1.0	52	.07	675.97	.06	.04	3.38	2.22
680	.9	48	.06	679.97	.05	.04	3.43	2.26
684	.9	46	.06	683.97	.05	.04	3.47	2.30
688	1.0	46	.07	687.97	.05	.05	3.52	2.35

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
692	1.1	47	.08	691.97	.06	.05	3.58	2.40
696	1.1	48	.08	695.97	.06	.05	3.63	2.45
700	1.0	46	.07	699.97	.05	.05	3.68	2.50
704	1.1	46	.08	703.97	.06	.05	3.74	2.56
708	1.4	46	.10	707.97	.07	.07	3.81	2.62
712	1.4	44	.10	711.97	.07	.07	3.88	2.69
716	1.2	42	.08	715.97	.06	.06	3.93	2.76
720	1.2	42	.08	719.97	.06	.06	3.99	2.82
724	1.3	43	.09	723.96	.06	.07	4.05	2.88
728	1.1	44	.08	727.96	.05	.06	4.10	2.94
732	1.0	43	.07	731.96	.05	.05	4.15	2.99
736	1.4	44	.10	735.96	.07	.07	4.22	3.06
740	1.5	45	.10	739.96	.07	.07	4.29	3.13
744	1.6	42	.11	743.96	.07	.08	4.37	3.22
748	1.6	41	.11	747.96	.07	.08	4.44	3.30
752	1.6	41	.11	751.96	.07	.08	4.52	3.39
756	1.4	42	.10	755.95	.07	.07	4.58	3.46
760	1.4	41	.10	759.95	.06	.07	4.65	3.53
764	1.6	39	.11	763.95	.07	.09	4.72	3.62
768	1.6	39	.11	767.95	.07	.09	4.79	3.71
772	1.6	39	.11	771.95	.07	.09	4.86	3.79
776	1.7	38	.12	775.95	.07	.09	4.93	3.89
780	1.7	37	.12	779.95	.07	.09	5.00	3.98
784	1.6	36	.11	783.94	.07	.09	5.07	4.07
788	1.4	34	.10	787.94	.05	.08	5.12	4.15
792	1.5	33	.10	791.94	.06	.09	5.18	4.24
796	1.9	32	.13	795.94	.07	.11	5.25	4.35
800	1.8	32	.13	799.94	.07	.11	5.31	4.46
804	1.8	32	.13	803.93	.07	.11	5.38	4.57
808	1.8	32	.13	807.93	.07	.11	5.45	4.67
812	1.5	31	.10	811.93	.05	.09	5.50	4.76
816	1.7	32	.12	815.93	.06	.10	5.56	4.86
820	2.0	32	.14	819.93	.07	.12	5.64	4.98
824	2.0	31	.14	823.92	.07	.12	5.71	5.10
828	1.8	31	.13	827.92	.06	.11	5.78	5.21
832	1.5	31	.10	831.92	.05	.09	5.83	5.30
836	1.6	31	.11	835.92	.06	.10	5.89	5.39
840	1.7	30	.12	839.92	.06	.10	5.95	5.50
844	1.7	28	.12	843.92	.06	.10	6.00	5.60
848	1.8	26	.13	847.91	.06	.11	6.06	5.71
852	2.0	26	.14	851.91	.06	.13	6.12	5.84
856	1.8	26	.13	855.91	.06	.11	6.17	5.95
860	1.8	26	.13	859.91	.06	.11	6.23	6.07
864	1.9	25	.13	863.91	.06	.12	6.28	6.19
868	1.7	23	.12	867.90	.05	.11	6.33	6.30

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
872	1.9	21	.13	871.90	.05	.12	6.38	6.42
876	2.2	20	.15	875.90	.05	.14	6.43	6.56
880	2.2	18	.15	879.90	.05	.15	6.48	6.71
884	2.5	17	.17	883.89	.05	.17	6.53	6.88
888	2.7	17	.19	887.89	.06	.18	6.58	7.06
892	2.6	19	.18	891.88	.06	.17	6.64	7.23
896	2.6	20	.18	895.88	.06	.17	6.71	7.40
900	2.6	19	.18	899.88	.06	.17	6.76	7.57
904	2.8	20	.20	903.87	.07	.18	6.83	7.75
908	2.8	20	.20	907.87	.07	.18	6.90	7.94
912	2.6	18	.18	911.86	.06	.17	6.95	8.11
916	2.5	18	.17	915.86	.05	.17	7.01	8.28
920	2.6	17	.18	919.85	.05	.17	7.06	8.45
924	2.6	18	.18	923.85	.06	.17	7.12	8.62
928	2.8	18	.20	927.84	.06	.19	7.18	8.81
932	3.0	18	.21	931.84	.06	.20	7.24	9.01
936	3.1	18	.22	935.83	.07	.21	7.31	9.21
940	3.0	20	.21	939.83	.07	.20	7.38	9.41
944	3.0	18	.21	943.82	.06	.20	7.45	9.61
948	3.0	17	.21	947.82	.06	.20	7.51	9.81
952	3.1	17	.22	951.81	.06	.21	7.57	10.02
956	2.9	18	.20	955.81	.06	.19	7.63	10.21
960	3.0	18	.21	959.80	.06	.20	7.70	10.41
964	3.2	18	.22	963.79	.07	.21	7.77	10.62
968	3.2	17	.22	967.79	.07	.21	7.83	10.83
972	3.2	17	.22	971.78	.07	.21	7.90	11.05
976	3.3	17	.23	975.78	.07	.22	7.96	11.27
980	3.3	17	.23	979.77	.07	.22	8.03	11.49
984	3.3	18	.23	983.76	.07	.22	8.10	11.71
988	3.3	18	.23	987.76	.07	.22	8.17	11.93
992	3.1	17	.22	991.75	.06	.21	8.24	12.13
996	3.3	17	.23	995.74	.07	.22	8.30	12.35
1000	3.4	18	.24	999.74	.07	.23	8.38	12.58
1004	3.4	19	.24	1003.73	.08	.22	8.45	12.80
1008	3.3	20	.23	1007.72	.08	.22	8.53	13.02
1012	3.3	22	.23	1011.72	.09	.21	8.62	13.23
1016	3.4	22	.24	1015.71	.09	.22	8.71	13.45
1020	3.3	21	.23	1019.70	.08	.21	8.79	13.67
1024	3.3	21	.23	1023.70	.08	.21	8.87	13.88
1028	3.2	20	.22	1027.69	.08	.21	8.95	14.09
1032	3.2	19	.22	1031.68	.07	.21	9.02	14.30
1036	3.3	20	.23	1035.68	.08	.22	9.10	14.52
1040	3.3	19	.23	1039.67	.07	.22	9.18	14.74
1044	3.2	18	.22	1043.66	.07	.21	9.25	14.95
1048	3.3	17	.23	1047.66	.07	.22	9.31	15.17

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
1052	3.4	17	.24	1051.65	.07	.23	9.38	15.40
1056	3.5	17	.24	1055.64	.07	.23	9.45	15.63
1060	3.5	18	.24	1059.63	.08	.23	9.53	15.86
1064	3.3	17	.23	1063.63	.07	.22	9.60	16.08
1068	3.1	16	.22	1067.62	.06	.21	9.66	16.29
1072	3.4	16	.24	1071.62	.07	.23	9.72	16.52
1076	3.7	17	.26	1075.61	.08	.25	9.80	16.77
1080	3.5	17	.24	1079.60	.07	.23	9.87	17.00
1084	3.3	18	.23	1083.59	.07	.22	9.94	17.22
1088	3.4	17	.24	1087.59	.07	.23	10.01	17.44
1092	3.4	16	.24	1091.58	.07	.23	10.07	17.67
1096	3.3	15	.23	1095.57	.06	.22	10.13	17.90
1100	3.3	15	.23	1099.57	.06	.22	10.19	18.12
1104	3.5	15	.24	1103.56	.06	.24	10.26	18.35
1108	3.6	15	.25	1107.55	.07	.24	10.32	18.60
1112	3.5	14	.24	1111.54	.06	.24	10.38	18.83
1116	3.5	14	.24	1115.54	.06	.24	10.44	19.07
1120	3.4	13	.24	1119.53	.05	.23	10.49	19.30
1124	3.5	14	.24	1123.52	.06	.24	10.55	19.54
1128	3.4	14	.24	1127.51	.06	.23	10.61	19.77
1132	3.4	14	.24	1131.51	.06	.23	10.67	20.00
1136	3.6	13	.25	1135.50	.06	.24	10.72	20.24
1140	3.7	13	.26	1139.49	.06	.25	10.78	20.49
1144	3.6	12	.25	1143.48	.05	.25	10.83	20.74
1148	3.5	12	.24	1147.47	.05	.24	10.88	20.98
1152	3.5	12	.24	1151.47	.05	.24	10.94	21.22
1156	3.6	11	.25	1155.46	.05	.25	10.98	21.46
1160	3.6	10	.25	1159.45	.04	.25	11.03	21.71
1164	3.5	8	.24	1163.44	.03	.24	11.06	21.95
1168	3.5	7	.24	1167.44	.03	.24	11.09	22.20
1172	3.6	7	.25	1171.43	.03	.25	11.12	22.45
1176	3.6	5	.25	1175.42	.02	.25	11.14	22.70
1180	3.6	5	.25	1179.41	.02	.25	11.16	22.95
1184	3.7	6	.26	1183.40	.03	.26	11.19	23.20
1188	3.7	7	.26	1187.40	.03	.26	11.22	23.46
1192	3.6	8	.25	1191.39	.03	.25	11.26	23.71
1196	3.5	8	.24	1195.38	.03	.24	11.29	23.95
1200	3.2	7	.22	1199.37	.03	.22	11.32	24.17
1204	3.0	8	.21	1203.37	.03	.21	11.35	24.38
1208	3.2	9	.22	1207.36	.03	.22	11.38	24.60
1212	3.6	7	.25	1211.36	.03	.25	11.41	24.85
1216	3.7	6	.26	1215.35	.03	.26	11.44	25.10
1220	3.5	8	.24	1219.34	.03	.24	11.47	25.35
1224	3.4	6	.24	1223.33	.02	.24	11.50	25.58
1228	3.4	5	.24	1227.33	.02	.24	11.52	25.82

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
1232	3.4	5	.24	1231.32	.02	.24	11.54	26.05
1236	3.3	5	.23	1235.31	.02	.23	11.56	26.28
1240	3.5	5	.24	1239.30	.02	.24	11.58	26.53
1244	3.7	5	.26	1243.30	.02	.26	11.60	26.78
1248	3.7	6	.26	1247.29	.03	.26	11.63	27.04
1252	3.6	5	.25	1251.28	.02	.25	11.65	27.29
1256	3.5	6	.24	1255.27	.03	.24	11.68	27.53
1260	3.4	5	.24	1259.27	.02	.24	11.70	27.77
1264	3.6	2	.25	1263.26	.01	.25	11.71	28.02
1268	3.8	3	.27	1267.25	.01	.26	11.72	28.29
1272	3.6	5	.25	1271.24	.02	.25	11.74	28.54
1276	3.5	7	.24	1275.23	.03	.24	11.77	28.78
1280	3.4	7	.24	1279.23	.03	.24	11.80	29.01
1284	3.4	8	.24	1283.22	.03	.23	11.84	29.25
1288	3.4	8	.24	1287.21	.03	.23	11.87	29.48
1292	3.3	7	.23	1291.21	.03	.23	11.90	29.71
1296	3.2	7	.22	1295.20	.03	.22	11.92	29.93
1300	3.3	8	.23	1299.19	.03	.23	11.96	30.16
1304	3.3	5	.23	1303.19	.02	.23	11.98	30.39
1308	3.3	4	.23	1307.18	.02	.23	11.99	30.62
1312	3.3	7	.23	1311.17	.03	.23	12.02	30.85
1316	3.5	7	.24	1315.17	.03	.24	12.05	31.09
1320	3.6	7	.25	1319.16	.03	.25	12.08	31.34
1324	3.3	6	.23	1323.15	.02	.23	12.11	31.57
1328	3.2	5	.22	1327.14	.02	.22	12.12	31.79
1332	3.6	6	.25	1331.14	.03	.25	12.15	32.04
1336	3.9	4	.27	1335.13	.02	.27	12.17	32.31
1340	3.6	3	.25	1339.12	.01	.25	12.18	32.57
1344	3.3	4	.23	1343.11	.02	.23	12.20	32.80
1348	3.6	2	.25	1347.10	.01	.25	12.21	33.05
1352	3.6	5	.25	1351.10	.02	.25	12.23	33.30
1356	3.5	6	.24	1355.09	.03	.24	12.26	33.54
1360	3.6	4	.25	1359.08	.02	.25	12.27	33.79
1364	3.5	0	.24	1363.07	.00	.24	12.27	34.03
1368	3.6	1	.25	1367.07	.00	.25	12.28	34.29
1372	3.9	3	.27	1371.06	.01	.27	12.29	34.56
1376	4.0	3	.28	1375.05	.01	.28	12.31	34.84
1380	4.1	2	.29	1379.04	.01	.29	12.32	35.12
1384	3.9	358	.27	1383.03	-.01	.27	12.31	35.39
1388	3.8	358	.27	1387.02	-.01	.26	12.30	35.66
1392	3.8	1	.27	1391.01	.00	.27	12.30	35.92
1396	3.8	1	.27	1395.00	.00	.27	12.31	36.19
1400	3.8	359	.27	1398.99	-.00	.27	12.30	36.45
1404	3.9	358	.27	1402.98	-.01	.27	12.29	36.73
1408	4.0	357	.28	1406.97	-.01	.28	12.28	37.00

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
1412	4.0	355	.28	1410.96	-.02	.28	12.25	37.28
1416	4.1	355	.29	1414.95	-.02	.28	12.23	37.57
1420	4.3	353	.30	1418.94	-.04	.30	12.19	37.86
1424	4.1	352	.29	1422.93	-.04	.28	12.15	38.15
1428	4.1	352	.29	1426.92	-.04	.28	12.11	38.43
1432	4.5	353	.31	1430.91	-.04	.31	12.07	38.74
1436	4.4	353	.31	1434.90	-.04	.30	12.04	39.05
1440	4.2	354	.29	1438.89	-.03	.29	12.01	39.34
1444	4.3	356	.30	1442.88	-.02	.30	11.99	39.64
1448	4.4	354	.31	1446.86	-.03	.31	11.95	39.94
1452	4.5	352	.31	1450.85	-.04	.31	11.91	40.25
1456	4.4	353	.31	1454.84	-.04	.30	11.87	40.56
1460	4.5	354	.31	1458.83	-.03	.31	11.84	40.87
1464	4.5	354	.31	1462.82	-.03	.31	11.81	41.18
1468	4.5	354	.31	1466.80	-.03	.31	11.77	41.49
1472	4.6	354	.32	1470.79	-.03	.32	11.74	41.81
1476	4.5	354	.31	1474.78	-.03	.31	11.71	42.13
1480	4.7	351	.33	1478.76	-.05	.32	11.66	42.45
1484	5.1	344	.36	1482.75	-.10	.34	11.56	42.79
1488	4.9	340	.34	1486.73	-.12	.32	11.44	43.11
1492	4.5	342	.31	1490.72	-.10	.30	11.34	43.41
1496	4.5	343	.31	1494.71	-.09	.30	11.25	43.71
1500	4.8	344	.33	1498.69	-.09	.32	11.16	44.03
1504	5.1	348	.36	1502.68	-.07	.35	11.09	44.38
1508	5.2	354	.36	1506.66	-.04	.36	11.05	44.74
1512	5.4	353	.38	1510.64	-.05	.37	11.00	45.11
1516	5.7	351	.40	1514.63	-.06	.39	10.94	45.51
1520	5.9	349	.41	1518.60	-.08	.40	10.86	45.91
1524	5.7	346	.40	1522.58	-.10	.39	10.77	46.30
1528	5.4	346	.38	1526.57	-.09	.37	10.67	46.66
1532	5.2	346	.36	1530.55	-.09	.35	10.59	47.01
1536	5.2	346	.36	1534.53	-.09	.35	10.50	47.36
1540	5.2	345	.36	1538.52	-.09	.35	10.41	47.71
1544	5.7	343	.40	1542.50	-.12	.38	10.29	48.09
1548	6.1	342	.43	1546.47	-.13	.40	10.16	48.50
1552	6.0	343	.42	1550.45	-.12	.40	10.04	48.90
1556	5.8	345	.40	1554.43	-.10	.39	9.93	49.29
1594	6.0	343	3.97	1592.22	-1.16	3.80	8.77	53.09
1598	6.0	342	.42	1596.20	-.13	.40	8.64	53.49
1602	5.8	342	.40	1600.18	-.12	.38	8.52	53.87
1606	5.7	344	.40	1604.16	-.11	.38	8.41	54.25
1610	5.7	344	.40	1608.14	-.11	.38	8.30	54.63
1614	5.6	343	.39	1612.12	-.11	.37	8.18	55.01
1618	5.7	344	.40	1616.10	-.11	.38	8.07	55.39
1622	5.9	345	.41	1620.08	-.11	.40	7.97	55.79

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
1626	5.8	345	.40	1624.06	-.10	.39	7.86	56.18
1630	5.8	346	.40	1628.04	-.10	.39	7.76	56.57
1634	5.9	347	.41	1632.02	-.09	.40	7.67	56.97
1638	5.9	347	.41	1636.00	-.09	.40	7.58	57.37
1642	5.7	347	.40	1639.98	-.09	.39	7.49	57.76
1646	5.7	347	.40	1643.96	-.09	.39	7.40	58.14
1650	6.1	346	.43	1647.94	-.10	.41	7.30	58.56
1654	6.1	345	.43	1651.91	-.11	.41	7.19	58.97
1658	5.6	344	.39	1655.89	-.11	.38	7.08	59.34
1662	5.5	343	.38	1659.88	-.11	.37	6.97	59.71
1666	5.4	343	.38	1663.86	-.11	.36	6.86	60.07
1670	5.4	343	.38	1667.84	-.11	.36	6.75	60.43
1674	5.8	345	.40	1671.82	-.10	.39	6.64	60.82
1678	6.1	345	.43	1675.80	-.11	.41	6.53	61.23
1682	6.0	345	.42	1679.78	-.11	.40	6.42	61.63
1686	5.8	347	.40	1683.76	-.09	.39	6.33	62.03
1690	5.7	346	.40	1687.74	-.10	.39	6.24	62.41
1694	5.5	345	.38	1691.72	-.10	.37	6.14	62.78
1698	5.4	345	.38	1695.70	-.10	.36	6.04	63.15
1702	5.2	344	.36	1699.68	-.10	.35	5.94	63.50
1706	5.1	346	.36	1703.67	-.09	.35	5.86	63.84
1710	5.3	344	.37	1707.65	-.10	.36	5.75	64.20
1714	5.5	341	.38	1711.63	-.12	.36	5.63	64.56
1718	5.5	341	.38	1715.61	-.12	.36	5.50	64.92
1722	5.3	340	.37	1719.60	-.13	.35	5.38	65.27
1726	5.2	342	.36	1723.58	-.11	.34	5.27	65.61
1730	5.2	341	.36	1727.56	-.12	.34	5.15	65.96
1734	5.6	337	.39	1731.54	-.15	.36	4.99	66.31
1738	5.9	340	.41	1735.52	-.14	.39	4.85	66.70
1742	5.2	344	.36	1739.51	-.10	.35	4.75	67.05
1746	4.9	344	.34	1743.49	-.09	.33	4.66	67.38
1750	5.1	345	.36	1747.48	-.09	.34	4.57	67.72
1754	4.9	346	.34	1751.46	-.08	.33	4.49	68.05
1758	5.0	347	.35	1755.45	-.08	.34	4.41	68.39
1762	5.1	346	.36	1759.43	-.09	.35	4.32	68.74
1766	4.9	346	.34	1763.42	-.08	.33	4.24	69.07
1770	4.9	346	.34	1767.40	-.08	.33	4.16	69.40
1774	4.7	346	.33	1771.39	-.08	.32	4.08	69.72
1778	4.9	346	.34	1775.37	-.08	.33	3.99	70.05
1782	5.0	347	.35	1779.36	-.08	.34	3.92	70.39
1786	4.8	346	.33	1783.34	-.08	.32	3.83	70.71
1790	4.6	345	.32	1787.33	-.08	.31	3.75	71.02
1794	4.7	345	.33	1791.32	-.08	.32	3.67	71.34
1798	4.7	346	.33	1795.30	-.08	.32	3.59	71.66
1802	4.5	347	.31	1799.29	-.07	.31	3.52	71.97

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
1806	4.6	348	.32	1803.28	-.07	.31	3.45	72.28
1810	4.5	347	.31	1807.27	-.07	.31	3.38	72.58
1814	4.6	347	.32	1811.25	-.07	.31	3.31	72.90
1818	4.8	347	.33	1815.24	-.08	.33	3.23	73.22
1822	4.5	348	.31	1819.23	-.07	.31	3.17	73.53
1826	4.5	348	.31	1823.21	-.07	.31	3.10	73.84
1830	4.4	348	.31	1827.20	-.06	.30	3.04	74.14
1834	4.1	347	.29	1831.19	-.06	.28	2.97	74.42
1838	4.1	347	.29	1835.18	-.06	.28	2.91	74.69
1842	4.4	347	.31	1839.17	-.07	.30	2.84	74.99
1846	4.4	347	.31	1843.16	-.07	.30	2.77	75.29
1850	4.3	348	.30	1847.15	-.06	.29	2.71	75.59
1854	4.3	347	.30	1851.14	-.07	.29	2.64	75.88
1858	4.3	345	.30	1855.13	-.08	.29	2.56	76.17
1862	4.3	343	.30	1859.11	-.09	.29	2.48	76.45
1866	4.2	343	.29	1863.10	-.09	.28	2.39	76.74
1870	4.1	342	.29	1867.09	-.09	.27	2.30	77.01
1874	4.1	341	.29	1871.08	-.09	.27	2.21	77.28
1878	4.0	342	.28	1875.07	-.09	.27	2.12	77.54
1882	4.2	343	.29	1879.06	-.09	.28	2.04	77.82
1886	4.0	343	.28	1883.05	-.08	.27	1.96	78.09
1890	3.9	342	.27	1887.04	-.08	.26	1.87	78.35
1894	4.1	343	.29	1891.03	-.08	.27	1.79	78.62
1898	4.2	343	.29	1895.02	-.09	.28	1.70	78.90
1902	3.9	344	.27	1899.01	-.07	.26	1.63	79.16
1906	3.9	343	.27	1903.00	-.08	.26	1.55	79.42
1910	3.9	344	.27	1906.99	-.07	.26	1.47	79.69
1914	3.6	345	.25	1910.99	-.07	.24	1.41	79.93
1918	3.6	345	.25	1914.98	-.07	.24	1.34	80.17
1922	3.6	345	.25	1918.97	-.07	.24	1.28	80.41
1926	3.5	346	.24	1922.96	-.06	.24	1.22	80.65
1930	3.8	345	.27	1926.95	-.07	.26	1.15	80.91
1934	3.9	345	.27	1930.95	-.07	.26	1.08	81.17
1938	3.6	346	.25	1934.94	-.06	.24	1.02	81.41
1942	3.6	345	.25	1938.93	-.07	.24	.95	81.66
1946	3.7	344	.26	1942.92	-.07	.25	.88	81.90
1950	3.7	344	.26	1946.91	-.07	.25	.81	82.15
1954	3.7	344	.26	1950.90	-.07	.25	.74	82.40
1958	3.6	344	.25	1954.90	-.07	.24	.67	82.64
1962	3.4	344	.24	1958.89	-.07	.23	.61	82.87
1966	3.4	344	.24	1962.88	-.07	.23	.54	83.10
1970	3.4	344	.24	1966.88	-.07	.23	.47	83.33
1974	3.5	344	.24	1970.87	-.07	.23	.41	83.56
1978	3.7	344	.26	1974.86	-.07	.25	.34	83.81
1982	3.6	344	.25	1978.85	-.07	.24	.27	84.05

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
1986	3.3	344	.23	1982.85	-.06	.22	.20	84.27
1990	3.2	343	.22	1986.84	-.07	.21	.14	84.48
1994	3.4	341	.24	1990.83	-.08	.22	.06	84.71
1998	3.2	341	.22	1994.83	-.07	.21	-.01	84.92
2002	3.2	341	.22	1998.82	-.07	.21	-.08	85.13
2006	3.3	342	.23	2002.81	-.07	.22	-.16	85.35
2010	3.3	344	.23	2006.81	-.06	.22	-.22	85.57
2014	3.3	344	.23	2010.80	-.06	.22	-.28	85.79
2018	3.3	343	.23	2014.79	-.07	.22	-.35	86.01
2022	3.1	343	.22	2018.79	-.06	.21	-.41	86.22
2026	3.1	345	.22	2022.78	-.06	.21	-.47	86.43
2030	3.1	348	.22	2026.78	-.04	.21	-.51	86.64
2034	3.0	349	.21	2030.77	-.04	.21	-.55	86.85
2038	3.2	349	.22	2034.76	-.04	.22	-.60	87.06
2042	3.2	350	.22	2038.76	-.04	.22	-.64	87.28
2044	3.2	341	.11	2040.75	-.04	.11	-.67	87.39
2048	3.0	342	.21	2044.75	-.06	.20	-.74	87.59
2052	2.7	341	.19	2048.74	-.06	.18	-.80	87.77
2056	2.6	340	.18	2052.74	-.06	.17	-.86	87.94
2060	2.6	341	.18	2056.74	-.06	.17	-.92	88.11
2064	2.8	341	.20	2060.73	-.06	.18	-.98	88.29
2068	2.7	342	.19	2064.73	-.06	.18	-1.04	88.47
2072	2.4	345	.17	2068.72	-.04	.16	-1.08	88.64
2076	2.3	346	.16	2072.72	-.04	.16	-1.12	88.79
2080	2.5	345	.17	2076.72	-.05	.17	-1.17	88.96
2084	2.5	345	.17	2080.71	-.05	.17	-1.21	89.13
2088	2.3	344	.16	2084.71	-.04	.15	-1.26	89.28
2092	2.4	345	.17	2088.71	-.04	.16	-1.30	89.44
2096	2.7	347	.19	2092.70	-.04	.18	-1.34	89.63
2100	2.5	348	.17	2096.70	-.04	.17	-1.38	89.80
2104	2.4	350	.17	2100.69	-.03	.16	-1.41	89.96
2108	2.4	351	.17	2104.69	-.03	.17	-1.43	90.13
2112	2.3	352	.16	2108.69	-.02	.16	-1.46	90.29
2116	2.3	352	.16	2112.68	-.02	.16	-1.48	90.45
2120	2.4	353	.17	2116.68	-.02	.17	-1.50	90.61
2124	2.4	357	.17	2120.68	-.01	.17	-1.51	90.78
2128	2.4	359	.17	2124.67	-.00	.17	-1.51	90.95
2132	2.3	1	.16	2128.67	.00	.16	-1.51	91.11
2136	2.3	1	.16	2132.67	.00	.16	-1.51	91.27
2140	2.3	2	.16	2136.66	.01	.16	-1.50	91.43
2148	2.4	4	.34	2144.66	.02	.33	-1.48	91.76
2152	2.3	5	.16	2148.65	.01	.16	-1.46	91.92
2156	2.2	5	.15	2152.65	.01	.15	-1.45	92.08
2160	2.3	5	.16	2156.65	.01	.16	-1.44	92.24
2164	2.3	6	.16	2160.64	.02	.16	-1.42	92.40

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
2168	2.2	5	.15	2164.64	.01	.15	-1.41	92.55
2172	2.4	5	.17	2168.64	.01	.17	-1.39	92.72
2176	2.5	4	.17	2172.63	.01	.17	-1.38	92.89
2180	2.6	4	.18	2176.63	.01	.18	-1.37	93.07
2184	2.6	5	.18	2180.63	.02	.18	-1.35	93.25
2188	2.5	5	.17	2184.62	.02	.17	-1.34	93.43
2192	2.5	6	.17	2188.62	.02	.17	-1.32	93.60
2196	2.5	7	.17	2192.61	.02	.17	-1.30	93.77
2200	2.4	7	.17	2196.61	.02	.17	-1.28	93.94
2204	2.2	7	.15	2200.61	.02	.15	-1.26	94.09
2208	2.4	6	.17	2204.60	.02	.17	-1.24	94.26
2212	2.6	7	.18	2208.60	.02	.18	-1.22	94.44
2216	2.5	11	.17	2212.60	.03	.17	-1.18	94.61
2220	2.7	12	.19	2216.59	.04	.18	-1.14	94.79
2224	2.6	12	.18	2220.59	.04	.18	-1.11	94.97
2228	2.5	13	.17	2224.58	.04	.17	-1.07	95.14
2232	2.5	14	.17	2228.58	.04	.17	-1.03	95.31
2236	2.3	14	.16	2232.58	.04	.16	-.99	95.47
2240	2.3	14	.16	2236.57	.04	.16	-.95	95.62
2244	2.4	15	.17	2240.57	.04	.16	-.90	95.78
2248	2.5	15	.17	2244.57	.05	.17	-.86	95.95
2252	2.4	16	.17	2248.56	.05	.16	-.81	96.11
2256	2.4	15	.17	2252.56	.04	.16	-.77	96.27
2260	2.5	15	.17	2256.56	.05	.17	-.72	96.44
2264	2.5	15	.17	2260.55	.05	.17	-.68	96.61
2268	2.4	15	.17	2264.55	.04	.16	-.64	96.77
2272	2.5	14	.17	2268.54	.04	.17	-.59	96.94
2276	2.6	14	.18	2272.54	.04	.18	-.55	97.12
2280	2.2	15	.15	2276.54	.04	.15	-.51	97.27
2284	2.3	15	.16	2280.53	.04	.16	-.47	97.42
2288	2.5	15	.17	2284.53	.05	.17	-.42	97.59
2292	2.2	15	.15	2288.53	.04	.15	-.38	97.74
2296	2.0	16	.14	2292.53	.04	.13	-.34	97.87
2300	2.0	18	.14	2296.52	.04	.13	-.30	98.01
2304	2.1	18	.15	2300.52	.05	.14	-.26	98.15
2308	1.9	18	.13	2304.52	.04	.13	-.22	98.27
2312	1.8	18	.13	2308.52	.04	.12	-.18	98.39
2316	1.9	18	.13	2312.51	.04	.13	-.14	98.52
2320	1.8	17	.13	2316.51	.04	.12	-.10	98.64
2324	1.8	17	.13	2320.51	.04	.12	-.06	98.76
2328	2.0	17	.14	2324.51	.04	.13	-.02	98.89
2332	2.1	19	.15	2328.50	.05	.14	.03	99.03
2336	2.0	21	.14	2332.50	.05	.13	.08	99.16
2340	2.0	22	.14	2336.50	.05	.13	.13	99.29
2344	1.9	24	.13	2340.50	.05	.12	.18	99.41

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
2348	1.7	24	.12	2344.50	.05	.11	.23	99.52
2352	1.9	25	.13	2348.49	.06	.12	.29	99.64
2356	2.2	29	.15	2352.49	.07	.13	.36	99.77
2360	2.0	33	.14	2356.49	.08	.12	.44	99.89
2364	1.7	30	.12	2360.49	.06	.10	.50	99.99
2368	1.6	25	.11	2364.48	.05	.10	.54	100.09
2372	1.8	25	.13	2368.48	.05	.11	.60	100.21
2376	2.0	30	.14	2372.48	.07	.12	.67	100.33
2380	2.0	35	.14	2376.48	.08	.11	.75	100.44
2384	1.8	35	.13	2380.48	.07	.10	.82	100.55
2388	1.6	35	.11	2384.47	.06	.09	.88	100.64
2392	1.6	37	.11	2388.47	.07	.09	.95	100.73
2396	1.7	39	.12	2392.47	.07	.09	1.02	100.82
2400	1.7	40	.12	2396.47	.08	.09	1.10	100.91
2404	1.7	42	.12	2400.47	.08	.09	1.18	101.00
2408	1.6	44	.11	2404.47	.08	.08	1.26	101.08
2412	1.6	44	.11	2408.46	.08	.08	1.34	101.16
2416	1.6	45	.11	2412.46	.08	.08	1.41	101.24
2420	1.6	49	.11	2416.46	.08	.07	1.50	101.31
2424	1.5	52	.10	2420.46	.08	.06	1.58	101.38
2428	1.5	51	.10	2424.46	.08	.07	1.66	101.44
2432	1.6	49	.11	2428.46	.08	.07	1.75	101.51
2436	1.5	50	.10	2432.46	.08	.07	1.83	101.58
2440	1.5	55	.10	2436.45	.09	.06	1.91	101.64
2444	1.5	59	.10	2440.45	.09	.05	2.00	101.70
2448	1.4	62	.10	2444.45	.09	.05	2.09	101.74
2452	1.5	65	.10	2448.45	.09	.04	2.18	101.79
2456	1.8	65	.13	2452.45	.11	.05	2.30	101.84
2460	1.8	63	.13	2456.45	.11	.06	2.41	101.90
2464	1.6	65	.11	2460.44	.10	.05	2.51	101.94
2468	1.4	67	.10	2464.44	.09	.04	2.60	101.98
2472	1.3	68	.09	2468.44	.08	.03	2.69	102.02
2476	1.4	70	.10	2472.44	.09	.03	2.78	102.05
2480	1.4	76	.10	2476.44	.09	.02	2.87	102.07
2484	1.4	82	.10	2480.44	.10	.01	2.97	102.09
2488	1.4	83	.10	2484.44	.10	.01	3.07	102.10
2492	1.4	84	.10	2488.44	.10	.01	3.16	102.11
2496	1.4	89	.10	2492.44	.10	.00	3.26	102.11
2500	1.3	93	.09	2496.43	.09	-.00	3.35	102.11
2504	1.5	95	.10	2500.43	.10	-.01	3.46	102.10
2508	1.6	96	.11	2504.43	.11	-.01	3.57	102.08
2512	1.8	97	.13	2508.43	.12	-.02	3.69	102.07
2516	1.9	99	.13	2512.43	.13	-.02	3.82	102.05
2520	1.7	100	.12	2516.43	.12	-.02	3.94	102.03
2524	1.7	100	.12	2520.42	.12	-.02	4.06	102.01

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
2528	1.7	101	.12	2524.42	.12	-.02	4.17	101.98
2532	1.7	102	.12	2528.42	.12	-.02	4.29	101.96
2536	1.7	103	.12	2532.42	.12	-.03	4.40	101.93
2540	1.9	102	.13	2536.42	.13	-.03	4.53	101.91
2544	2.2	103	.15	2540.41	.15	-.03	4.68	101.87
2548	2.3	104	.16	2544.41	.16	-.04	4.84	101.83
2552	2.5	104	.17	2548.41	.17	-.04	5.01	101.79
2556	2.4	104	.17	2552.40	.16	-.04	5.17	101.75
2560	2.4	107	.17	2556.40	.16	-.05	5.33	101.70
2564	2.6	108	.18	2560.40	.17	-.06	5.50	101.64
2568	2.5	108	.17	2564.39	.17	-.05	5.67	101.59
2572	2.5	108	.17	2568.39	.17	-.05	5.84	101.54
2576	2.6	106	.18	2572.38	.17	-.05	6.01	101.49
2580	2.8	104	.20	2576.38	.19	-.05	6.20	101.44
2584	3.0	104	.21	2580.37	.20	-.05	6.40	101.39
2588	2.9	103	.20	2584.37	.20	-.05	6.60	101.34
2592	3.0	103	.21	2588.36	.20	-.05	6.80	101.30
2596	3.1	103	.22	2592.36	.21	-.05	7.01	101.25
2600	3.1	103	.22	2596.35	.21	-.05	7.23	101.20
2604	3.2	104	.22	2600.34	.22	-.05	7.44	101.15
2608	3.3	106	.23	2604.34	.22	-.06	7.66	101.08
2612	3.1	107	.22	2608.33	.21	-.06	7.87	101.02
2616	3.2	107	.22	2612.33	.21	-.07	8.08	100.95
2620	3.5	107	.24	2616.32	.23	-.07	8.32	100.88
2624	3.5	107	.24	2620.31	.23	-.07	8.55	100.81
2628	3.6	107	.25	2624.30	.24	-.07	8.79	100.74
2632	3.5	107	.24	2628.30	.23	-.07	9.02	100.67
2636	3.3	108	.23	2632.29	.22	-.07	9.24	100.59
2640	3.2	107	.22	2636.28	.21	-.07	9.46	100.53
2644	3.3	107	.23	2640.28	.22	-.07	9.68	100.46
2648	3.4	105	.24	2644.27	.23	-.06	9.91	100.40
2652	3.4	105	.24	2648.26	.23	-.06	10.14	100.34
2656	3.4	106	.24	2652.25	.23	-.07	10.36	100.27
2660	3.6	107	.25	2656.25	.24	-.07	10.60	100.20
2664	3.7	107	.26	2660.24	.25	-.08	10.85	100.12
2668	3.5	107	.24	2664.23	.23	-.07	11.08	100.05
2672	3.7	107	.26	2668.22	.25	-.08	11.33	99.98
2676	3.7	107	.26	2672.21	.25	-.08	11.58	99.90
2680	3.5	107	.24	2676.21	.23	-.07	11.81	99.83
2684	3.5	107	.24	2680.20	.23	-.07	12.05	99.76
2688	3.7	107	.26	2684.19	.25	-.08	12.29	99.68
2692	3.8	107	.27	2688.18	.25	-.08	12.55	99.61
2696	3.7	108	.26	2692.17	.25	-.08	12.79	99.53
2700	3.5	108	.24	2696.17	.23	-.08	13.02	99.45
2704	3.3	107	.23	2700.16	.22	-.07	13.24	99.38

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
2708	3.5	107	.24	2704.15	.23	-.07	13.48	99.31
2712	3.6	108	.25	2708.14	.24	-.08	13.72	99.24
2716	3.4	109	.24	2712.14	.22	-.08	13.94	99.16
2720	3.4	109	.24	2716.13	.22	-.08	14.16	99.08
2724	3.5	110	.24	2720.12	.23	-.08	14.39	99.00
2728	3.5	110	.24	2724.12	.23	-.08	14.62	98.91
2732	3.5	111	.24	2728.11	.23	-.09	14.85	98.83
2736	3.7	111	.26	2732.10	.24	-.09	15.09	98.73
2740	3.5	111	.24	2736.09	.23	-.09	15.32	98.65
2744	3.4	111	.24	2740.09	.22	-.09	15.54	98.56
2748	3.4	112	.24	2744.08	.22	-.09	15.76	98.47
2752	3.2	113	.22	2748.07	.21	-.09	15.97	98.38
2756	3.3	114	.23	2752.07	.21	-.09	16.18	98.29
2760	3.4	114	.24	2756.06	.22	-.10	16.39	98.19
2764	3.2	115	.22	2760.05	.20	-.09	16.60	98.10
2768	3.2	115	.22	2764.05	.20	-.09	16.80	98.01
2772	3.3	115	.23	2768.04	.21	-.10	17.01	97.91
2776	3.2	115	.22	2772.03	.20	-.09	17.21	97.81
2780	3.1	115	.22	2776.03	.20	-.09	17.41	97.72
2784	3.3	115	.23	2780.02	.21	-.10	17.61	97.63
2788	3.2	114	.22	2784.01	.20	-.09	17.82	97.53
2792	3.1	116	.22	2788.01	.19	-.09	18.01	97.44
2796	3.4	117	.24	2792.00	.21	-.11	18.22	97.33
2800	3.2	117	.22	2796.00	.20	-.10	18.42	97.23
2804	3.1	117	.22	2799.99	.19	-.10	18.62	97.13
2808	3.1	116	.22	2803.98	.19	-.09	18.81	97.04
2812	3.1	113	.22	2807.98	.20	-.08	19.01	96.95
2816	3.2	111	.22	2811.97	.21	-.08	19.22	96.87
2820	3.3	111	.23	2815.96	.21	-.08	19.43	96.79
2824	3.4	111	.24	2819.96	.22	-.09	19.65	96.71
2828	3.2	112	.22	2823.95	.21	-.08	19.86	96.62
2832	3.2	111	.22	2827.95	.21	-.08	20.07	96.54
2836	3.4	111	.24	2831.94	.22	-.09	20.29	96.46
2840	3.3	111	.23	2835.93	.21	-.08	20.51	96.37
2844	3.4	111	.24	2839.92	.22	-.09	20.73	96.29
2848	3.3	114	.23	2843.92	.21	-.09	20.94	96.20
2852	3.2	116	.22	2847.91	.20	-.10	21.14	96.10
2856	3.2	117	.22	2851.91	.20	-.10	21.34	96.00
2860	3.0	116	.21	2855.90	.19	-.09	21.53	95.90
2864	2.9	115	.20	2859.89	.18	-.09	21.71	95.82
2868	3.0	113	.21	2863.89	.19	-.08	21.90	95.74
2872	3.2	113	.22	2867.88	.21	-.09	22.11	95.65
2876	3.3	113	.23	2871.88	.21	-.09	22.32	95.56
2880	3.4	112	.24	2875.87	.22	-.09	22.54	95.47
2884	3.3	111	.23	2879.86	.21	-.08	22.75	95.39

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
2888	3.2	111	.22	2883.86	.21	-.08	22.96	95.31
2892	3.3	111	.23	2887.85	.21	-.08	23.18	95.23
2896	3.2	111	.22	2891.84	.21	-.08	23.39	95.15
2900	3.1	110	.22	2895.84	.20	-.07	23.59	95.07
2904	3.2	110	.22	2899.83	.21	-.08	23.80	95.00
2908	3.1	110	.22	2903.83	.20	-.07	24.00	94.92
2912	3.0	110	.21	2907.82	.20	-.07	24.20	94.85
2916	3.1	110	.22	2911.81	.20	-.07	24.40	94.78
2920	3.1	110	.22	2915.81	.20	-.07	24.61	94.70
2924	3.0	110	.21	2919.80	.20	-.07	24.80	94.63
2928	2.9	109	.20	2923.80	.19	-.07	24.99	94.57
2932	2.9	109	.20	2927.79	.19	-.07	25.19	94.50
2936	3.1	110	.22	2931.79	.20	-.07	25.39	94.43
2940	3.2	111	.22	2935.78	.21	-.08	25.60	94.35
2944	3.1	111	.22	2939.78	.20	-.08	25.80	94.27
2948	2.9	111	.20	2943.77	.19	-.07	25.99	94.20
2952	3.0	110	.21	2947.76	.20	-.07	26.18	94.12
2956	3.1	111	.22	2951.76	.20	-.08	26.39	94.05
2960	3.0	113	.21	2955.75	.19	-.08	26.58	93.96
2964	2.9	115	.20	2959.75	.18	-.09	26.76	93.88
2968	2.9	116	.20	2963.74	.18	-.09	26.94	93.79
2972	2.8	116	.20	2967.74	.18	-.09	27.12	93.70
2976	2.9	117	.20	2971.73	.18	-.09	27.30	93.61
2980	2.9	118	.20	2975.73	.18	-.10	27.48	93.52
2984	3.0	119	.21	2979.72	.18	-.10	27.66	93.42
2988	3.1	118	.22	2983.72	.19	-.10	27.85	93.31
2992	3.1	116	.22	2987.71	.19	-.09	28.05	93.22
2996	3.1	113	.22	2991.70	.20	-.08	28.25	93.13
3000	3.1	112	.22	2995.70	.20	-.08	28.45	93.05
3004	3.1	114	.22	2999.69	.20	-.09	28.65	92.97
3008	3.3	114	.23	3003.69	.21	-.09	28.86	92.87
3012	3.2	113	.22	3007.68	.21	-.09	29.06	92.79
3016	3.1	115	.22	3011.67	.20	-.09	29.26	92.69
3020	3.1	118	.22	3015.67	.19	-.10	29.45	92.59
3024	3.1	120	.22	3019.66	.19	-.11	29.64	92.48
3028	3.0	121	.21	3023.66	.18	-.11	29.81	92.38
3032	2.8	121	.20	3027.65	.17	-.10	29.98	92.28
3036	2.9	122	.20	3031.65	.17	-.11	30.15	92.17
3040	3.1	122	.22	3035.64	.18	-.11	30.34	92.05
3044	3.0	122	.21	3039.64	.18	-.11	30.52	91.94
3048	2.9	122	.20	3043.63	.17	-.11	30.69	91.84
3052	2.9	121	.20	3047.63	.17	-.10	30.86	91.73
3056	3.0	120	.21	3051.62	.18	-.10	31.04	91.63
3060	3.0	120	.21	3055.61	.18	-.10	31.22	91.52
3064	3.0	121	.21	3059.61	.18	-.11	31.40	91.41

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
3068	2.9	123	.20	3063.60	.17	-.11	31.57	91.30
3072	2.9	123	.20	3067.60	.17	-.11	31.74	91.19
3076	3.0	122	.21	3071.59	.18	-.11	31.92	91.08
3080	3.0	122	.21	3075.59	.18	-.11	32.10	90.97
3084	2.9	121	.20	3079.58	.17	-.10	32.27	90.87
3088	2.9	121	.20	3083.58	.17	-.10	32.44	90.76
3092	3.1	122	.22	3087.57	.18	-.11	32.63	90.65
3096	3.2	123	.22	3091.57	.19	-.12	32.81	90.53
3100	2.9	123	.20	3095.56	.17	-.11	32.98	90.42
3104	2.9	123	.20	3099.56	.17	-.11	33.15	90.31
3108	2.9	124	.20	3103.55	.17	-.11	33.32	90.19
3112	2.7	123	.19	3107.55	.16	-.10	33.48	90.09
3116	2.7	123	.19	3111.54	.16	-.10	33.64	89.99
3120	2.9	123	.20	3115.54	.17	-.11	33.81	89.88
3124	2.9	123	.20	3119.53	.17	-.11	33.98	89.77
3128	3.0	123	.21	3123.53	.18	-.11	34.15	89.65
3132	2.9	123	.20	3127.52	.17	-.11	34.32	89.54
3136	2.8	124	.20	3131.52	.16	-.11	34.48	89.43
3140	2.7	124	.19	3135.51	.16	-.11	34.64	89.33
3144	2.6	124	.18	3139.51	.15	-.10	34.79	89.23
3148	2.6	124	.18	3143.50	.15	-.10	34.94	89.13
3152	2.5	124	.17	3147.50	.14	-.10	35.09	89.03
3156	2.6	124	.18	3151.50	.15	-.10	35.24	88.93
3160	2.7	124	.19	3155.49	.16	-.11	35.39	88.82
3164	2.6	125	.18	3159.49	.15	-.10	35.54	88.72
3168	2.4	125	.17	3163.48	.14	-.10	35.68	88.62
3172	2.3	126	.16	3167.48	.13	-.09	35.81	88.53
3176	2.4	126	.17	3171.48	.14	-.10	35.94	88.43
3180	2.5	127	.17	3175.47	.14	-.11	36.08	88.32
3184	2.4	128	.17	3179.47	.13	-.10	36.22	88.22
3188	2.5	129	.17	3183.47	.14	-.11	36.35	88.11
3192	2.4	132	.17	3187.46	.12	-.11	36.48	88.00
3196	2.2	135	.15	3191.46	.11	-.11	36.58	87.89
3200	2.2	135	.15	3195.46	.11	-.11	36.69	87.78
3204	2.2	135	.15	3199.45	.11	-.11	36.80	87.67
3208	1.9	136	.13	3203.45	.09	-.10	36.89	87.58
3212	1.7	138	.12	3207.45	.08	-.09	36.97	87.49
3216	1.8	140	.13	3211.45	.08	-.10	37.05	87.39
3220	1.7	143	.12	3215.45	.07	-.09	37.12	87.30
3224	1.6	145	.11	3219.44	.06	-.09	37.19	87.21
3228	1.7	147	.12	3223.44	.06	-.10	37.25	87.11
3232	1.6	150	.11	3227.44	.06	-.10	37.31	87.01
3236	1.5	149	.10	3231.44	.05	-.09	37.36	86.92
3240	1.4	148	.10	3235.44	.05	-.08	37.42	86.84
3244	1.4	148	.10	3239.44	.05	-.08	37.47	86.75

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
3248	1.4	147	.10	3243.44	.05	-.08	37.52	86.67
3252	1.4	147	.10	3247.43	.05	-.08	37.57	86.59
3256	1.4	147	.10	3251.43	.05	-.08	37.63	86.51
3260	1.4	145	.10	3255.43	.06	-.08	37.68	86.43
3264	1.5	143	.10	3259.43	.06	-.08	37.75	86.35
3268	1.5	142	.10	3263.43	.06	-.08	37.81	86.26
3272	1.6	142	.11	3267.43	.07	-.09	37.88	86.17
3276	1.7	141	.12	3271.43	.07	-.09	37.95	86.08
3280	1.7	140	.12	3275.42	.08	-.09	38.03	85.99
3284	1.6	140	.11	3279.42	.07	-.09	38.10	85.91
3288	1.6	140	.11	3283.42	.07	-.09	38.17	85.82
3292	1.8	139	.13	3287.42	.08	-.09	38.26	85.73
3296	1.7	136	.12	3291.42	.08	-.09	38.34	85.64
3300	1.7	135	.12	3295.42	.08	-.08	38.42	85.56
3304	1.9	137	.13	3299.41	.09	-.10	38.51	85.46
3308	1.9	137	.13	3303.41	.09	-.10	38.60	85.36
3312	1.8	137	.13	3307.41	.09	-.09	38.69	85.27
3316	1.8	136	.13	3311.41	.09	-.09	38.78	85.18
3320	1.9	136	.13	3315.40	.09	-.10	38.87	85.08
3324	1.9	136	.13	3319.40	.09	-.10	38.96	84.99
3328	2.0	133	.14	3323.40	.10	-.10	39.06	84.89
3332	2.1	130	.15	3327.40	.11	-.09	39.17	84.80
3336	2.2	130	.15	3331.39	.12	-.10	39.29	84.70
3340	2.3	132	.16	3335.39	.12	-.11	39.41	84.59
3344	2.3	133	.16	3339.39	.12	-.11	39.53	84.48
3348	2.3	133	.16	3343.38	.12	-.11	39.65	84.38
3352	2.3	133	.16	3347.38	.12	-.11	39.76	84.27
3356	2.6	133	.18	3351.38	.13	-.12	39.90	84.14
3360	2.7	133	.19	3355.37	.14	-.13	40.03	84.01
3364	2.6	133	.18	3359.37	.13	-.12	40.17	83.89
3368	2.6	134	.18	3363.36	.13	-.13	40.30	83.76
3372	2.8	134	.20	3367.36	.14	-.14	40.44	83.63
3376	2.8	134	.20	3371.36	.14	-.14	40.58	83.49
3380	2.8	135	.20	3375.35	.14	-.14	40.72	83.35
3384	2.8	134	.20	3379.35	.14	-.14	40.86	83.22
3388	2.9	134	.20	3383.34	.15	-.14	41.00	83.08
3392	3.1	134	.22	3387.33	.16	-.15	41.16	82.93
3396	3.3	135	.23	3391.33	.16	-.16	41.32	82.76
3400	3.3	137	.23	3395.32	.16	-.17	41.48	82.60
3404	3.3	139	.23	3399.31	.15	-.17	41.63	82.42
3408	3.3	140	.23	3403.31	.15	-.18	41.78	82.25
3412	3.4	140	.24	3407.30	.15	-.18	41.93	82.06
3416	3.5	140	.24	3411.29	.16	-.19	42.09	81.88
3420	3.5	140	.24	3415.29	.16	-.19	42.24	81.69
3424	3.5	140	.24	3419.28	.16	-.19	42.40	81.50

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
3428	3.6	141	.25	3423.27	.16	-.20	42.56	81.31
3432	3.7	142	.26	3427.26	.16	-.20	42.72	81.10
3436	3.7	142	.26	3431.25	.16	-.20	42.88	80.90
3440	3.8	141	.27	3435.25	.17	-.21	43.04	80.69
3444	3.8	141	.27	3439.24	.17	-.21	43.21	80.49
3448	3.8	140	.27	3443.23	.17	-.20	43.38	80.29
3452	4.0	140	.28	3447.22	.18	-.21	43.56	80.07
3456	4.0	140	.28	3451.21	.18	-.21	43.74	79.86
3460	4.0	142	.28	3455.20	.17	-.22	43.91	79.64
3464	4.1	141	.29	3459.19	.18	-.22	44.09	79.42
3468	4.3	140	.30	3463.18	.19	-.23	44.28	79.19
3472	4.3	141	.30	3467.17	.19	-.23	44.47	78.95
3476	4.2	141	.29	3471.16	.18	-.23	44.66	78.73
3480	4.2	141	.29	3475.14	.18	-.23	44.84	78.50
3484	4.2	141	.29	3479.13	.18	-.23	45.03	78.27
3488	4.3	141	.30	3483.12	.19	-.23	45.21	78.04
3492	4.4	139	.31	3487.11	.20	-.23	45.42	77.81
3496	4.6	139	.32	3491.10	.21	-.24	45.63	77.56
3500	4.6	139	.32	3495.08	.21	-.24	45.84	77.32
3504	4.7	137	.33	3499.07	.22	-.24	46.06	77.08
3508	4.9	135	.34	3503.06	.24	-.24	46.30	76.84
3512	4.7	135	.33	3507.04	.23	-.23	46.53	76.61
3516	4.7	136	.33	3511.03	.23	-.24	46.76	76.37
3520	5.0	135	.35	3515.01	.25	-.25	47.01	76.13
3524	5.1	134	.36	3519.00	.26	-.25	47.26	75.88
3528	5.3	135	.37	3522.98	.26	-.26	47.52	75.62
3532	5.4	134	.38	3526.96	.27	-.26	47.80	75.36
3536	5.5	136	.38	3530.95	.27	-.28	48.06	75.08
3540	5.5	138	.38	3534.93	.26	-.28	48.32	74.80
3544	5.6	137	.39	3538.91	.27	-.29	48.58	74.51
3548	5.7	136	.40	3542.89	.28	-.29	48.86	74.22
3552	5.7	135	.40	3546.87	.28	-.28	49.14	73.94
3556	5.7	134	.40	3550.85	.29	-.28	49.43	73.67
3560	5.7	134	.40	3554.83	.29	-.28	49.71	73.39
3564	5.9	135	.41	3558.81	.29	-.29	50.00	73.10
3568	6.1	134	.43	3562.79	.31	-.30	50.31	72.81
3572	6.0	133	.42	3566.76	.31	-.29	50.62	72.52
3576	6.0	132	.42	3570.74	.31	-.28	50.93	72.24
3580	6.2	131	.43	3574.72	.33	-.28	51.25	71.96
3584	6.2	130	.43	3578.69	.33	-.28	51.58	71.68
3588	6.1	130	.43	3582.67	.33	-.27	51.91	71.41
3592	6.2	130	.43	3586.65	.33	-.28	52.24	71.13
3596	6.0	130	.42	3590.63	.32	-.27	52.56	70.86
3600	6.1	130	.43	3594.60	.33	-.27	52.89	70.59
3604	6.1	131	.43	3598.58	.32	-.28	53.21	70.31

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
3608	6.1	132	.43	3602.56	.32	-.28	53.52	70.02
3612	6.2	131	.43	3606.54	.33	-.28	53.85	69.74
3616	6.3	132	.44	3610.51	.33	-.29	54.17	69.45
3620	6.4	132	.45	3614.49	.33	-.30	54.51	69.15
3624	6.2	131	.43	3618.46	.33	-.28	54.83	68.86
3628	6.2	131	.43	3622.44	.33	-.28	55.16	68.58
3632	6.2	133	.43	3626.42	.32	-.29	55.47	68.29
3636	6.1	133	.43	3630.39	.31	-.29	55.78	68.00
3640	6.2	132	.43	3634.37	.32	-.29	56.11	67.71
3644	6.3	131	.44	3638.35	.33	-.29	56.44	67.42
3648	6.4	132	.45	3642.32	.33	-.30	56.77	67.12
3652	6.4	134	.45	3646.30	.32	-.31	57.09	66.81
3656	6.3	132	.44	3650.27	.33	-.29	57.42	66.52
3660	6.2	130	.43	3654.25	.33	-.28	57.75	66.24
3664	6.3	129	.44	3658.22	.34	-.28	58.09	65.96
3668	6.5	129	.45	3662.20	.35	-.28	58.44	65.68
3672	6.4	129	.45	3666.17	.35	-.28	58.79	65.40
3676	6.3	129	.44	3670.15	.34	-.28	59.13	65.12
3680	6.0	129	.42	3674.13	.32	-.26	59.45	64.86
3684	5.9	128	.41	3678.11	.32	-.25	59.78	64.61
3688	5.9	127	.41	3682.09	.33	-.25	60.10	64.36
3692	6.0	128	.42	3686.06	.33	-.26	60.43	64.10
3696	6.0	128	.42	3690.04	.33	-.26	60.76	63.84
3700	6.0	127	.42	3694.02	.33	-.25	61.10	63.59
3704	6.1	129	.43	3698.00	.33	-.27	61.43	63.32
3708	6.1	130	.43	3701.97	.33	-.27	61.75	63.05
3712	6.0	129	.42	3705.95	.32	-.26	62.08	62.79
3716	6.3	129	.44	3709.93	.34	-.28	62.42	62.51
3720	6.3	130	.44	3713.90	.34	-.28	62.76	62.23
3724	6.2	130	.43	3717.88	.33	-.28	63.09	61.95
3728	6.3	128	.44	3721.86	.35	-.27	63.43	61.68
3732	6.4	129	.45	3725.83	.35	-.28	63.78	61.40
3736	6.3	130	.44	3729.81	.34	-.28	64.11	61.12
3740	6.1	130	.43	3733.78	.33	-.27	64.44	60.85
3744	6.1	130	.43	3737.76	.33	-.27	64.77	60.57
3748	6.1	129	.43	3741.74	.33	-.27	65.10	60.31
3752	5.9	128	.41	3745.72	.32	-.25	65.42	60.05
3756	5.9	128	.41	3749.70	.32	-.25	65.74	59.80
3760	5.9	128	.41	3753.68	.32	-.25	66.07	59.55
3764	5.9	129	.41	3757.65	.32	-.26	66.39	59.29
3768	6.0	131	.42	3761.63	.32	-.27	66.70	59.01
3772	6.1	131	.43	3765.61	.32	-.28	67.02	58.73
3776	6.0	133	.42	3769.59	.31	-.29	67.33	58.45
3780	6.1	133	.43	3773.57	.31	-.29	67.64	58.16
3784	6.2	132	.43	3777.54	.32	-.29	67.96	57.87

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
3788	6.3	132	.44	3781.52	.33	-.29	68.29	57.58
3792	6.2	133	.43	3785.49	.32	-.29	68.60	57.28
3796	6.2	135	.43	3789.47	.31	-.31	68.91	56.98
3800	6.1	134	.43	3793.45	.31	-.30	69.22	56.68
3804	6.0	132	.42	3797.43	.31	-.28	69.53	56.40
3808	6.2	131	.43	3801.40	.33	-.28	69.85	56.12
3812	6.2	133	.43	3805.38	.32	-.29	70.17	55.82
3816	6.2	134	.43	3809.36	.31	-.30	70.48	55.52
3820	6.3	133	.44	3813.33	.32	-.30	70.80	55.22
3824	6.4	133	.45	3817.31	.33	-.30	71.13	54.92
3828	6.5	134	.45	3821.28	.33	-.31	71.45	54.60
3832	6.6	133	.46	3825.25	.34	-.31	71.79	54.29
3836	6.6	131	.46	3829.23	.35	-.30	72.13	53.99
3840	6.7	129	.47	3833.20	.36	-.29	72.50	53.70
3844	6.7	128	.47	3837.17	.37	-.29	72.87	53.41
3848	6.7	128	.47	3841.15	.37	-.29	73.23	53.12
3852	6.7	129	.47	3845.12	.36	-.29	73.60	52.83
3856	6.7	129	.47	3849.09	.36	-.29	73.96	52.53
3860	6.8	128	.47	3853.06	.37	-.29	74.33	52.24
3864	6.8	127	.47	3857.04	.38	-.29	74.71	51.96
3868	6.8	126	.47	3861.01	.38	-.28	75.09	51.68
3872	6.8	126	.47	3864.98	.38	-.28	75.48	51.40
3876	6.8	126	.47	3868.95	.38	-.28	75.86	51.12
3880	6.8	127	.47	3872.92	.38	-.29	76.24	50.84
3884	6.9	127	.48	3876.89	.38	-.29	76.62	50.55
3888	6.9	127	.48	3880.87	.38	-.29	77.01	50.26
3892	6.9	126	.48	3884.84	.39	-.28	77.39	49.98
3896	6.9	126	.48	3888.81	.39	-.28	77.78	49.69
3900	6.9	125	.48	3892.78	.39	-.28	78.18	49.42
3904	6.9	125	.48	3896.75	.39	-.28	78.57	49.14
3908	7.0	126	.49	3900.72	.39	-.29	78.96	48.86
3912	7.0	126	.49	3904.69	.39	-.29	79.36	48.57
3916	7.0	126	.49	3908.66	.39	-.29	79.75	48.28
3920	7.0	126	.49	3912.63	.39	-.29	80.15	48.00
3924	7.0	126	.49	3916.60	.39	-.29	80.54	47.71
3928	7.0	125	.49	3920.57	.40	-.28	80.94	47.43
3932	7.0	124	.49	3924.54	.40	-.27	81.35	47.16
3936	6.9	125	.48	3928.51	.39	-.28	81.74	46.88
3940	6.9	126	.48	3932.48	.39	-.28	82.13	46.60
3944	7.0	126	.49	3936.45	.39	-.29	82.52	46.31
3948	7.0	125	.49	3940.42	.40	-.28	82.92	46.03
3952	6.9	125	.48	3944.39	.39	-.28	83.32	45.76
3956	7.0	125	.49	3948.36	.40	-.28	83.71	45.48
3960	6.9	124	.48	3952.34	.40	-.27	84.11	45.21
3964	6.9	125	.48	3956.31	.39	-.28	84.51	44.93

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
3968	6.9	125	.48	3960.28	.39	-.28	84.90	44.66
3972	6.9	124	.48	3964.25	.40	-.27	85.30	44.39
3976	6.9	124	.48	3968.22	.40	-.27	85.70	44.12
3980	6.8	124	.47	3972.19	.39	-.26	86.09	43.86
3984	6.8	124	.47	3976.16	.39	-.26	86.48	43.59
3988	6.9	124	.48	3980.13	.40	-.27	86.88	43.32
3992	6.9	124	.48	3984.11	.40	-.27	87.28	43.05
3996	6.8	125	.47	3988.08	.39	-.27	87.67	42.78
4000	6.8	125	.47	3992.05	.39	-.27	88.05	42.51
4004	6.8	124	.47	3996.02	.39	-.26	88.45	42.25
4008	6.7	125	.47	3999.99	.38	-.27	88.83	41.98
4012	6.8	125	.47	4003.97	.39	-.27	89.22	41.71
4016	6.9	124	.48	4007.94	.40	-.27	89.62	41.44
4020	7.0	124	.49	4011.91	.40	-.27	90.02	41.16
4024	6.9	124	.48	4015.88	.40	-.27	90.42	40.90
4028	6.9	123	.48	4019.85	.40	-.26	90.82	40.63
4032	6.9	123	.48	4023.82	.40	-.26	91.22	40.37
4036	6.9	122	.48	4027.79	.41	-.25	91.63	40.12
4040	6.8	122	.47	4031.76	.40	-.25	92.03	39.87
4044	6.7	121	.47	4035.74	.40	-.24	92.43	39.63
4048	6.6	121	.46	4039.71	.39	-.24	92.83	39.39
4052	6.5	121	.45	4043.68	.39	-.23	93.22	39.16
4056	6.5	120	.45	4047.66	.39	-.23	93.61	38.93
4060	6.5	121	.45	4051.63	.39	-.23	94.00	38.70
4064	6.5	121	.45	4055.61	.39	-.23	94.38	38.46
4068	6.5	122	.45	4059.58	.38	-.24	94.77	38.22
4072	6.6	122	.46	4063.55	.39	-.24	95.16	37.98
4076	6.6	122	.46	4067.53	.39	-.24	95.55	37.74
4080	6.7	121	.47	4071.50	.40	-.24	95.95	37.50
4084	6.7	121	.47	4075.47	.40	-.24	96.35	37.26
4088	6.7	121	.47	4079.45	.40	-.24	96.75	37.02
4092	6.7	121	.47	4083.42	.40	-.24	97.15	36.77
4096	6.7	121	.47	4087.39	.40	-.24	97.55	36.53
4100	6.8	122	.47	4091.36	.40	-.25	97.95	36.28
4104	6.8	122	.47	4095.33	.40	-.25	98.35	36.03
4108	6.8	122	.47	4099.31	.40	-.25	98.75	35.78
4112	6.9	122	.48	4103.28	.41	-.25	99.16	35.53
4116	6.9	122	.48	4107.25	.41	-.25	99.57	35.27
4120	7.1	121	.49	4111.22	.42	-.25	99.99	35.02
4124	7.3	120	.51	4115.18	.44	-.25	100.43	34.76
4128	7.4	120	.52	4119.15	.45	-.26	100.88	34.51
4132	7.5	120	.52	4123.12	.45	-.26	101.33	34.24
4136	7.5	121	.52	4127.08	.45	-.27	101.78	33.98
4140	7.7	121	.54	4131.05	.46	-.28	102.24	33.70
4144	7.8	120	.54	4135.01	.47	-.27	102.71	33.43

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
4148	8.0	120	.56	4138.97	.48	-.28	103.19	33.15
4152	8.3	120	.58	4142.93	.50	-.29	103.69	32.86
4156	8.5	121	.59	4146.89	.51	-.30	104.20	32.56
4160	8.5	121	.59	4150.84	.51	-.30	104.70	32.25
4164	8.4	122	.58	4154.80	.50	-.31	105.20	31.94
4168	8.3	122	.58	4158.76	.49	-.31	105.69	31.64
4172	8.4	123	.58	4162.71	.49	-.32	106.18	31.32
4176	8.4	122	.58	4166.67	.50	-.31	106.67	31.01
4180	8.5	123	.59	4170.63	.50	-.32	107.17	30.69
4184	8.6	123	.60	4174.58	.50	-.33	107.67	30.36
4188	8.5	122	.59	4178.54	.50	-.31	108.17	30.05
4192	8.5	122	.59	4182.49	.50	-.31	108.67	29.73
4196	8.5	123	.59	4186.45	.50	-.32	109.17	29.41
4200	8.4	123	.58	4190.41	.49	-.32	109.66	29.09
4204	8.4	123	.58	4194.36	.49	-.32	110.15	28.78
4208	8.5	122	.59	4198.32	.50	-.31	110.65	28.46
4212	8.5	123	.59	4202.28	.50	-.32	111.15	28.14
4216	8.4	123	.58	4206.23	.49	-.32	111.64	27.82
4220	8.4	122	.58	4210.19	.50	-.31	112.13	27.51
4224	8.4	121	.58	4214.15	.50	-.30	112.63	27.21
4228	8.5	122	.59	4218.10	.50	-.31	113.14	26.90
4232	8.5	123	.59	4222.06	.50	-.32	113.63	26.58
4236	8.6	123	.60	4226.01	.50	-.33	114.13	26.25
4240	8.6	122	.60	4229.97	.51	-.32	114.64	25.93
4244	8.6	122	.60	4233.92	.51	-.32	115.15	25.62
4248	8.7	122	.61	4237.88	.51	-.32	115.66	25.30
4252	8.8	122	.61	4241.83	.52	-.32	116.18	24.97
4256	9.0	122	.63	4245.78	.53	-.33	116.71	24.64
4260	9.2	122	.64	4249.73	.54	-.34	117.25	24.30
4264	9.4	122	.65	4253.68	.55	-.35	117.81	23.96
4268	9.5	122	.66	4257.62	.56	-.35	118.37	23.61
4272	9.5	122	.66	4261.57	.56	-.35	118.93	23.26
4276	9.6	123	.67	4265.51	.56	-.36	119.49	22.89
4280	9.7	123	.67	4269.45	.57	-.37	120.05	22.53
4284	9.8	123	.68	4273.40	.57	-.37	120.62	22.15
4288	9.8	124	.68	4277.34	.56	-.38	121.19	21.77
4292	9.9	125	.69	4281.28	.56	-.39	121.75	21.38
4296	9.9	125	.69	4285.22	.56	-.39	122.31	20.98
4300	9.9	125	.69	4289.16	.56	-.39	122.88	20.59
4304	10.0	125	.69	4293.10	.57	-.40	123.45	20.19
4308	10.2	125	.71	4297.04	.58	-.41	124.03	19.79
4312	10.1	125	.70	4300.97	.57	-.40	124.60	19.38
4316	10.1	125	.70	4304.91	.57	-.40	125.18	18.98
4320	10.1	124	.70	4308.85	.58	-.39	125.76	18.59
4324	10.1	125	.70	4312.79	.57	-.40	126.33	18.19

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
4328	10.2	124	.71	4316.72	.59	-.40	126.92	17.79
4332	10.2	124	.71	4320.66	.59	-.40	127.51	17.39
4336	10.3	124	.72	4324.60	.59	-.40	128.10	16.99
4340	10.3	124	.72	4328.53	.59	-.40	128.69	16.59
4344	10.3	123	.72	4332.47	.60	-.39	129.29	16.20
4348	10.3	124	.72	4336.40	.59	-.40	129.88	15.80
4352	10.3	125	.72	4340.34	.59	-.41	130.47	15.39
4356	10.4	126	.72	4344.27	.58	-.42	131.05	14.97
4360	10.4	126	.72	4348.21	.58	-.42	131.64	14.55
4364	10.4	126	.72	4352.14	.58	-.42	132.22	14.12
4368	10.5	125	.73	4356.07	.60	-.42	132.82	13.70
4372	10.6	125	.74	4360.01	.60	-.42	133.42	13.28
4376	10.6	125	.74	4363.94	.60	-.42	134.03	12.86
4380	10.6	126	.74	4367.87	.60	-.43	134.62	12.43
4384	10.7	127	.74	4371.80	.59	-.45	135.21	11.98
4388	10.7	127	.74	4375.73	.59	-.45	135.81	11.53
4392	10.8	127	.75	4379.66	.60	-.45	136.41	11.08
4396	10.8	126	.75	4383.59	.61	-.44	137.01	10.64
4400	10.7	126	.74	4387.52	.60	-.44	137.61	10.20
4404	10.8	127	.75	4391.45	.60	-.45	138.21	9.75
4408	10.9	127	.76	4395.38	.60	-.46	138.82	9.30
4412	10.9	126	.76	4399.30	.61	-.44	139.43	8.85
4416	11.0	126	.76	4403.23	.62	-.45	140.04	8.41
4420	11.0	125	.76	4407.16	.63	-.44	140.67	7.97
4424	10.9	124	.76	4411.08	.63	-.42	141.30	7.54
4428	10.9	124	.76	4415.01	.63	-.42	141.92	7.12
4432	10.9	124	.76	4418.94	.63	-.42	142.55	6.70
4436	10.9	124	.76	4422.87	.63	-.42	143.18	6.28
4440	10.9	124	.76	4426.80	.63	-.42	143.81	5.85
4444	10.9	124	.76	4430.72	.63	-.42	144.43	5.43
4448	10.9	124	.76	4434.65	.63	-.42	145.06	5.01
4452	10.9	124	.76	4438.58	.63	-.42	145.69	4.58
4456	11.0	124	.76	4442.51	.63	-.43	146.32	4.16
4460	11.0	125	.76	4446.43	.63	-.44	146.94	3.72
4464	11.0	124	.76	4450.36	.63	-.43	147.58	3.29
4468	11.0	123	.76	4454.29	.64	-.42	148.22	2.88
4472	11.0	123	.76	4458.21	.64	-.42	148.86	2.46
4476	11.0	123	.76	4462.14	.64	-.42	149.50	2.05
4480	11.0	124	.76	4466.07	.63	-.43	150.13	1.62
4484	11.0	124	.76	4469.99	.63	-.43	150.76	1.19
4488	11.0	124	.76	4473.92	.63	-.43	151.40	.76
4492	11.0	124	.76	4477.84	.63	-.43	152.03	.34
4496	11.1	124	.77	4481.77	.64	-.43	152.67	-.09
4500	11.1	123	.77	4485.70	.65	-.42	153.31	-.51
4504	11.1	122	.77	4489.62	.65	-.41	153.97	-.92

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
4508	11.1	121	.77	4493.55	.66	-.40	154.63	-1.32
4512	11.1	121	.77	4497.47	.66	-.40	155.29	-1.71
4516	11.1	122	.77	4501.40	.65	-.41	155.94	-2.12
4520	11.1	123	.77	4505.32	.65	-.42	156.59	-2.54
4524	11.2	124	.78	4509.24	.64	-.43	157.23	-2.98
4528	11.4	125	.79	4513.17	.65	-.45	157.88	-3.43
4532	11.4	124	.79	4517.09	.66	-.44	158.53	-3.87
4536	11.4	123	.79	4521.01	.66	-.43	159.20	-4.30
4540	11.4	123	.79	4524.93	.66	-.43	159.86	-4.73
4544	11.4	123	.79	4528.85	.66	-.43	160.52	-5.16
4548	11.4	123	.79	4532.77	.66	-.43	161.18	-5.59
4552	11.4	123	.79	4536.69	.66	-.43	161.85	-6.02
4556	11.3	122	.78	4540.61	.66	-.42	162.51	-6.44
4560	11.4	121	.79	4544.54	.68	-.41	163.19	-6.85
4564	11.4	121	.79	4548.46	.68	-.41	163.87	-7.25
4568	11.4	122	.79	4552.38	.67	-.42	164.54	-7.67
4572	11.4	123	.79	4556.30	.66	-.43	165.20	-8.10
4576	11.4	124	.79	4560.22	.66	-.44	165.86	-8.55
4580	11.4	125	.79	4564.14	.65	-.45	166.50	-9.00
4584	11.4	124	.79	4568.06	.66	-.44	167.16	-9.44
4588	11.5	123	.80	4571.98	.67	-.43	167.83	-9.88
4592	11.6	124	.80	4575.90	.67	-.45	168.50	-10.33
4596	11.5	125	.80	4579.82	.65	-.46	169.15	-10.78
4600	11.5	124	.80	4583.74	.66	-.45	169.81	-11.23
4604	11.6	124	.80	4587.66	.67	-.45	170.48	-11.68
4608	11.8	125	.82	4591.57	.67	-.47	171.15	-12.15
4612	12.0	127	.83	4595.49	.66	-.50	171.81	-12.65
4616	12.2	128	.85	4599.40	.67	-.52	172.48	-13.17
4620	12.3	128	.85	4603.30	.67	-.52	173.15	-13.69
4624	12.3	128	.85	4607.21	.67	-.52	173.82	-14.22
4628	12.4	129	.86	4611.12	.67	-.54	174.49	-14.76
4632	12.6	129	.87	4615.02	.68	-.55	175.17	-15.31
4636	12.7	123	.88	4618.92	.74	-.48	175.90	-15.79
4640	12.7	123	.88	4622.83	.74	-.48	176.64	-16.27
4644	12.8	123	.89	4626.73	.74	-.48	177.38	-16.75
4648	12.7	122	.88	4630.63	.75	-.47	178.13	-17.21
4652	12.8	122	.89	4634.53	.75	-.47	178.88	-17.68
4656	12.8	123	.89	4638.43	.74	-.48	179.62	-18.17
4660	12.8	123	.89	4642.33	.74	-.48	180.37	-18.65
4664	12.7	123	.88	4646.23	.74	-.48	181.11	-19.13
4668	12.6	122	.87	4650.14	.74	-.46	181.85	-19.59
4672	12.6	122	.87	4654.04	.74	-.46	182.59	-20.05
4676	12.5	124	.87	4657.95	.72	-.48	183.30	-20.54
4680	12.5	124	.87	4661.85	.72	-.48	184.02	-21.02
4684	12.5	123	.87	4665.76	.73	-.47	184.75	-21.49

Schlumberger

DEPTH	DRIFT	AZM	H.D.	TRUE DEPTH	X	Y	SUMX	SUMY
4688	12.6	123	.87	4669.66	.73	-.48	185.48	-21.97
4692	12.5	124	.87	4673.57	.72	-.48	186.20	-22.45
4696	12.4	126	.86	4677.47	.69	-.50	186.89	-22.96
4700	12.4	126	.86	4681.38	.69	-.50	187.59	-23.46
4704	12.3	124	.85	4685.29	.71	-.48	188.29	-23.94
4708	12.2	122	.85	4689.20	.72	-.45	189.01	-24.39
4712	12.1	124	.84	4693.11	.70	-.47	189.70	-24.85
4716	12.1	126	.84	4697.02	.68	-.49	190.38	-25.35
4720	12.1	125	.84	4700.93	.69	-.48	191.07	-25.83
4724	12.1	125	.84	4704.84	.69	-.48	191.76	-26.31
4728	12.1	126	.84	4708.75	.68	-.49	192.43	-26.80
4732	11.8	125	.82	4712.67	.67	-.47	193.10	-27.27
4736	11.8	124	.82	4716.58	.68	-.46	193.78	-27.73
4740	11.8	125	.82	4720.50	.67	-.47	194.45	-28.20
4744	11.9	130	.82	4724.41	.63	-.53	195.08	-28.73
4748	11.9	134	.82	4728.33	.59	-.57	195.68	-29.30
4752	12.0	134	.83	4732.24	.60	-.58	196.28	-29.88
4756	12.1	134	.84	4736.15	.60	-.58	196.88	-30.46
4760	12.1	133	.84	4740.06	.61	-.57	197.49	-31.03
4764	12.0	134	.83	4743.97	.60	-.58	198.09	-31.61
4768	12.0	135	.83	4747.89	.59	-.59	198.68	-32.20
4772	12.0	132	.83	4751.80	.62	-.56	199.30	-32.76
4776	12.0	129	.83	4755.71	.65	-.52	199.94	-33.28
4780	12.0	128	.83	4759.62	.66	-.51	200.60	-33.79
4784	12.0	128	.83	4763.54	.66	-.51	201.25	-34.30
4788	12.0	128	.83	4767.45	.66	-.51	201.91	-34.81
4792	12.0	128	.83	4771.36	.66	-.51	202.56	-35.33
4796	11.9	126	.82	4775.28	.67	-.48	203.23	-35.81
4800	11.9	123	.82	4779.19	.69	-.45	203.92	-36.26
4804	11.8	124	.82	4783.11	.68	-.46	204.60	-36.72
4808	11.7	125	.81	4787.02	.66	-.47	205.27	-37.18
4812	11.6	125	.80	4790.94	.66	-.46	205.93	-37.64
4816	11.5	124	.80	4794.86	.66	-.45	206.59	-38.09
4820	11.4	125	.79	4798.78	.65	-.45	207.23	-38.54
4824	11.4	129	.79	4802.70	.61	-.50	207.85	-39.04
4830	11.4	129	1.19	4808.58	.92	-.75	208.77	-39.79

Schlumberger

TANGENTIAL METHOD

DRIFT DISTANCE= 212.53 FEET
AZIMUTH OF DRIFT= 100 DEGREES

MEASURED DEPTH= 4830 FEET
TRUE VERTICAL DEPTH= 4808.58 FEET
SUMX= 208.77 (EAST)
SUMY= -39.79 (SOUTH)

PLOT SCALE= 30. FEET/IN.

XMAX= 208.77 XMIN= -1.51
YMAX= 102.11 YMIN= -39.79

JOHNSTON

Schlumberger

technical report

F.R. #04250 C

COMPANY WESTATES PETROLEUM CO. WELL TULLY FEDERAL #1 TEST NO. 2 COUNTY UINTAH STATE UTAH

JOHNSTON

PRESSURE LOG*

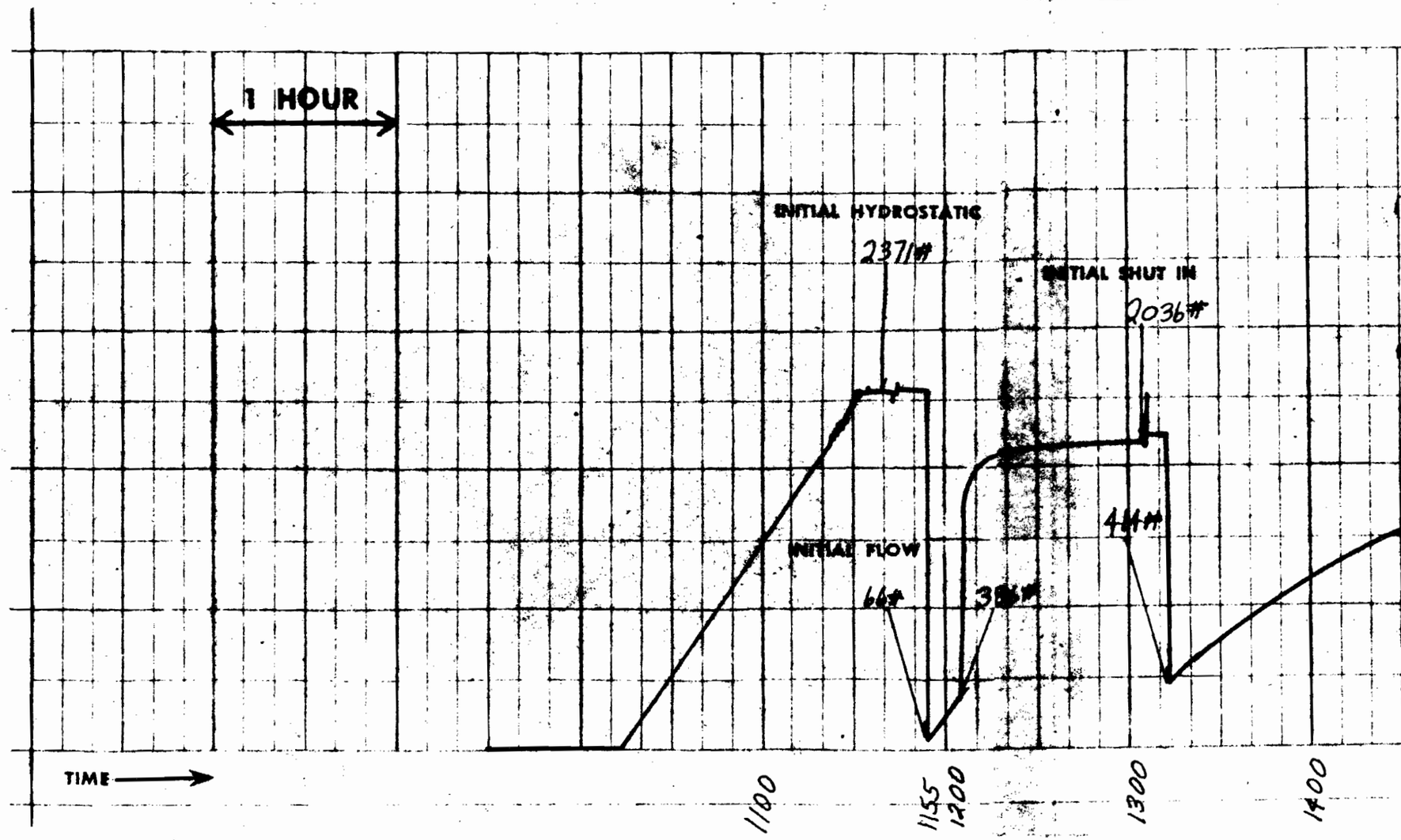
Field Report No. 04250C

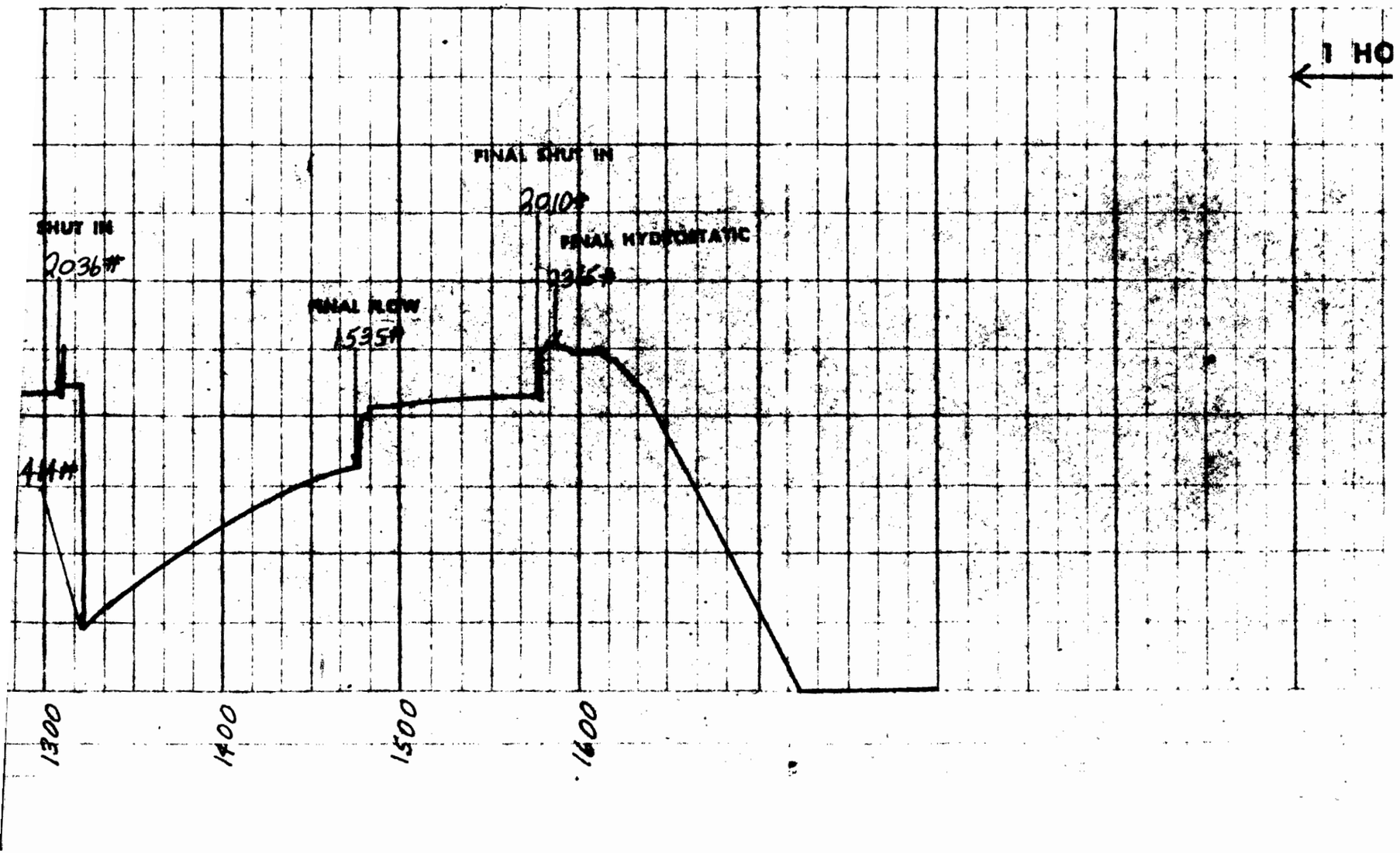
Instrument: Number J-445

Capacity 4700 p.s.i.

Depth 4727 ft.

*a continuous tracing of the original chart




1 HO
FINAL SHUT IN
2010#
FINAL HYDROSTATIC
SHUT IN
2036#
FINAL FLOW
1535#
1300
1400
1500
1600

JOHNSTON
...found a better way

SURFACE INFORMATION

Description (Rate of Flow)	Time	Pressure (P.S.I.G.)	Surface Choke
Opened Tool	1155	-	-
LIGHT, MEDIUM BLOW			
CLOSED FOR INITIAL SHUT-IN	1205	-	-
FINISHED SHUT-IN	1305	-	-
RE-OPENED TOOL	1312	-	-
MEDIUM STRONG BLOW FOR			
BALANCE OF TEST			
CLOSED FOR FINAL SHUT-IN	1446	-	-
PULLED PACKER LOOSE	1546	-	-

Cushion Type	Amount	Pressure	Bottom Choke
	-		Size 3/4"

EQUIPMENT & HOLE DATA

Type Test: M.F.E. OPEN HOLE
Formation Tested: WEBER
Elevation: 5084 Ft.
Net Productive Interval: 80 Ft.
Estimated Porosity: 11.5 %
All Depths Measured From: KELLY BUSHING
Total Depth: 4836 Ft.
Main Hole/Casing Size: 8 3/4"
Rat Hole/Liner Size: -
Drill Collar Length: 126' I.D. 2 5.8"
Drill Pipe Length: 4584' I.D. 2.75"
Packer Depth(s): 4740' & 4746' Ft.

MULTI-FLOW EVALUATOR FLUID SAMPLE DATA

Sampler Pressure: - P.S.I.G. at Surface
Recovery: Cu. Ft. Gas: -
cc. Oil: -
cc. Water: 2500
cc. Mud: -
Tot. Liquid cc.: 2500
Gravity: - °API @ - °F.
Gas/Oil Ratio: - cu. ft./bbl.

	RESISTIVITY	CHLORIDE CONTENT
Recovery Water	4. @ 92 °F.	215 ppm
Recovery Mud	- @ - °F.	
Recovery Mud Filtrate	- @ - °F.	- ppm
Mud Pit Sample	1.0 @ 72 °F.	
Mud Pit Sample Filtrate	.85 @ 60 °F.	300 ppm

MUD DATA

Mud Type: GEL AND WATER Wt.: 9.2
Viscosity: 60 Water Loss: 6 C.C.
Resist: of Mud 1.0 @ 72 °F; of Filtrate .85 @ 60 °F
Chloride Content: 300 PPM

RECOVERY DESCRIPTION	FEET	BARRELS	% OIL	% WATER	% OTHERS	API GRAVITY	RESISTIVITY	CHL. PPM
DRILLING MUD	1800 900	6.57				@ °F.	@ °F.	
WATER	2370	17.25				@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	
						@ °F.	@ °F.	

Remarks:

Address: 1600 BROADWAY; ROOM 2360; DENVER, COLORADO 80202

Company: WESTATES PETROLEUM COMPANY Field: WILD CAT
Well: TULLY FEDERAL #1 Location: 17-4s-22E
Test Interval: 4746' TO 4836' Test #: 2 Date: 9-10-74

County: UINTAH State: UTAH
Technician: MOUDRY (VERNAL) Test Approved By: MR. STANLEY D. CONRAD

Field Report No.: 04250 C
No. Reports Requested: 5

JOHNSTON
...found a better way

PRESSURE DATA

Instrument No.		J-445		
Capacity (P.S.I.G.)		4700		
Instrument Depth		4727'		
Instrument Opening		INSIDE		
Pressure Gradient P.S.I./Ft.				
Well Temperature °F.		113		
Initial Hydrostatic Mud	A	2371		
Initial Shut-in	B	* 2036		
Initial Flow	C	66		
	C-1	386		
	C-2	414		
Final Flow	D	1535		
Final Shut-in	E	* 2010		
Final Hydrostatic Mud	F	2365		

Field Report No. 04250 C

TIME DATA

Time Given	Time Computed
60 Mins.	Mins.
10 Mins.	Mins.
- Mins.	Mins.
- Mins.	Mins.
94 Mins.	Mins.
60 Mins.	Mins.

Remarks:

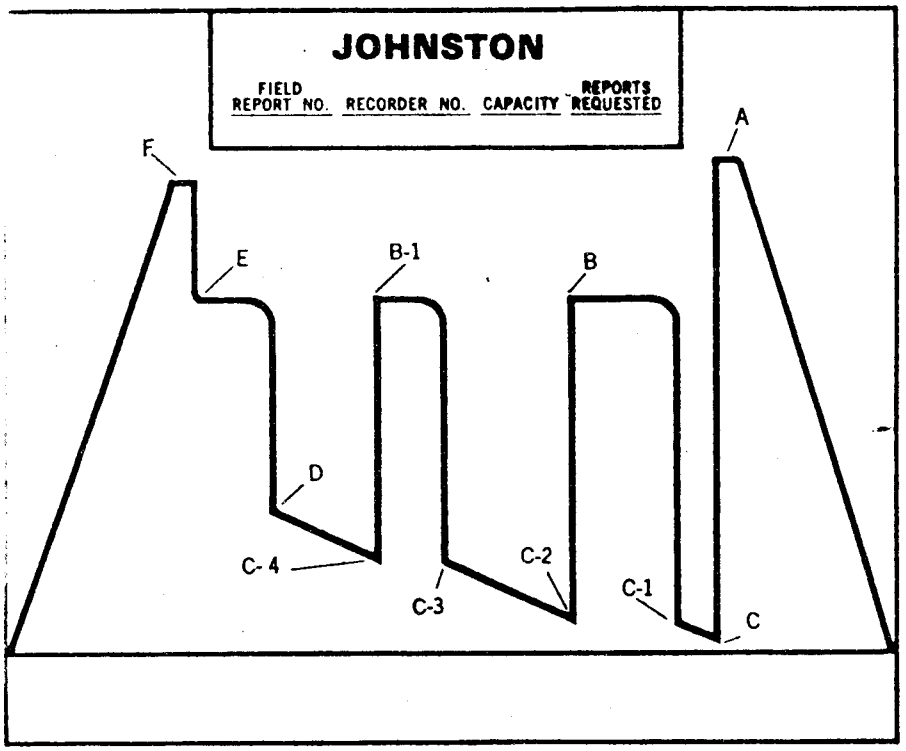
Shut In pressure did not reach static reservoir pressure.

Clock Travel _____ inches per min.

PRESSURE INCREMENTS

Point Minutes	Pressure	$\frac{T+\Delta t}{\Delta t}$	Point Minutes	Pressure	$\frac{T+\Delta t}{\Delta t}$	Point Minutes	Pressure	$\frac{T+\Delta t}{\Delta t}$

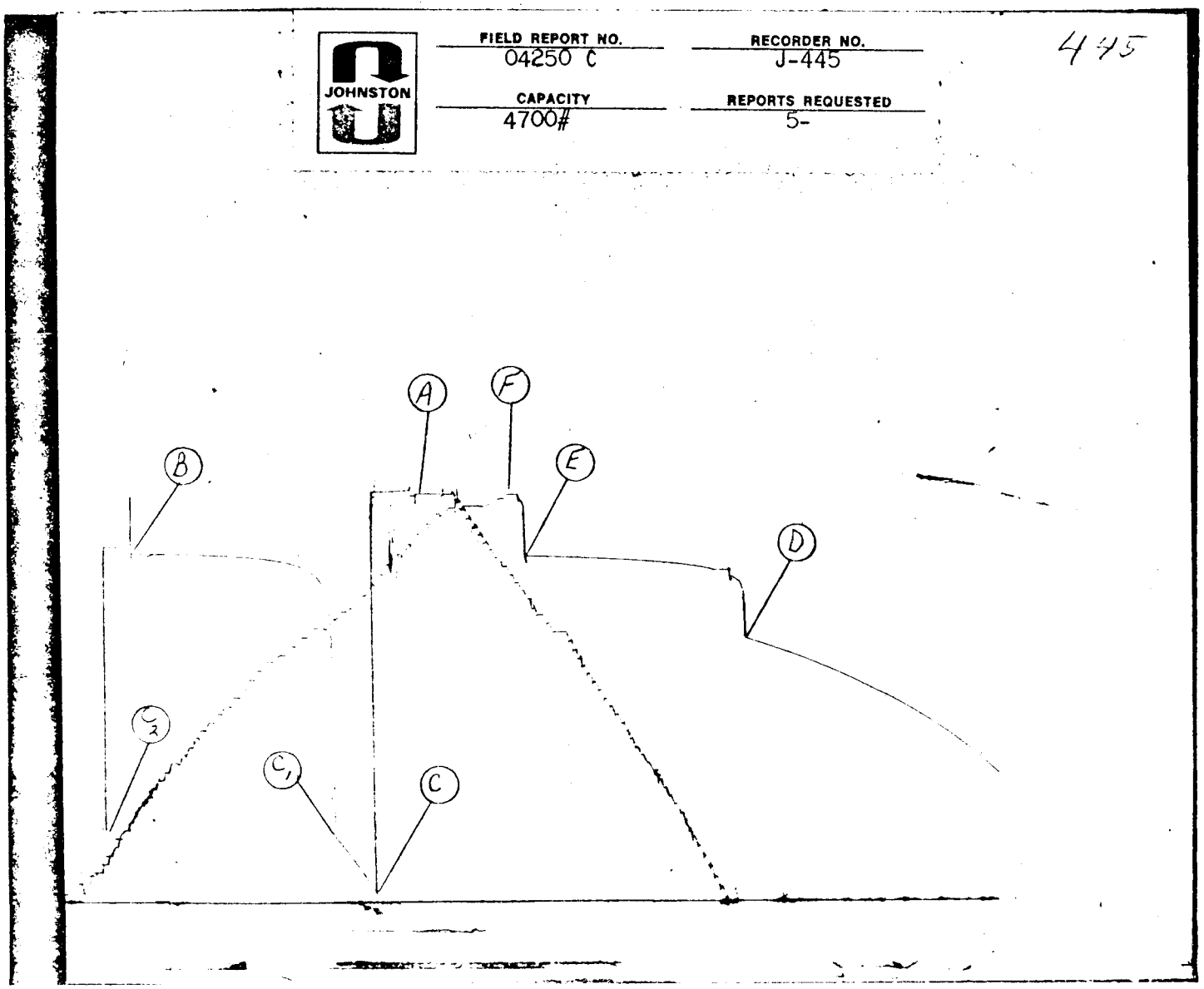
GUIDE TO IDENTIFICATION OF DRILL STEM TEST PRESSURE CHARTS



A. Initial Hyd. Mud
B. Initial Shut-in
C. Initial Flow
D. Final Flow
E. Final Shut-in
F. Final Hyd. Mud

The following points are either fluctuating pressures or points indicating other packer settings, (testing different zones).

A-1, A-2, A-3, etc. Initial Hyd. Pressures
B-1, B-2, B-3, etc. Subsequent Shut-in Pressures
C-1, C-2, C-3, etc. Flowing Pressures
D-1, D-2, D-3, etc. Subsequent Final Flow Pressures
E-1, E-2, E-3, etc. Subsequent Final Shut-in Pressures
F-1, F-2, F-3, etc. Final Hyd. Mud Pressures
Z — Special pressure points such as pumping pressure recorded for formation breakdown.



ATTACHMENT TO FORM #9-330 (Rev. 5-63)
PAGE 1

GEOLGIST'S FORMATION RECORD

FROM	TO	TOTAL FEET	FORMATION
Surface	600 KB	587	Mancos - shale, dark gray, carbonaceous fossiliferous with occasional fine sand beds
600	807	207	Frontier Sand - fine and medium grained gray sand and sandstone, soft to firm, fine sandy carbonaceous siltstone and coal, no shows of oil or gas
807	950	143	Lower Mancos (Mowry) - shale, dark gray and gray-brown, firm to hard, common bentonite fragments
950	1102	152	Dakota Sand - sand and sandstone fine to medium grained with some coarse grains and pebble fragments, some carbonaceous siltstone and coal, some dark dead oil stain and fluorescence but no gas kick on mud logger
1101	2082	980	Morrison - claystone and siltstone, gray, green-gray and red, often variagated, fine to coarse silty sand, some conglomerate intervals, particularly at about 1250 and 1950
2082	2220	138	Curtis Formation - shale, medium to dark gray, firm, silty sand quartzose with common glauconite grains and occasional pellets, some coarse grained sand and pebble fragments
2220	2512	292	Entrada Sand - sandstone, gray to red stained, fine and medium grained, friable to hard, no shows
2512	2670	158	Carmel Formation - siltstone and claystone, red, light gray and green, and sandstone fine to medium grained, white to red stained, silty
2670	3505	835	Navajo Sandstone - sandstone, white light gray and red stained, fine and medium grained, friable to hard green shale, no shows
3505	3710	205	Chinle Formation - shale, orange, maroon, pink and yellow, and silty red sandstone, lower 90' is mostly yellow and ochre shale
3710	3820	110	Shinarump Member - sandstone and conglomerate, gray to red stained, friable to hard, some intervals of red and green shale

GEOLOGIST'S FORMATION RECORD

FROM	TO	TOTAL FEET	FORMATION
3820	4556	736	Moenkopi Formation - shale, red, maroon and green, commonly variagated, and sandstone gray and red stained, fine to coarse grained, silty, occasional limestone and anhydrite fragments, lower 50' largely gray and green-gray shale
4556	4740	187	Phosphoria (Park City) - largely dolomitic siltstone and dolomite light to medium gray with some light gray limestone, occasional poor granular porosity with dark oil staining, occasional red siltstone and claystone beds
4740	4838	98	Weber Sandstone - fine and medium well-rounded quartz grains difficulty friable to hard, several hard shells, no staining but yellow fluorescence and cut

Form 9-331
(May 1963)

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SUBMIT IN TRIPLICATE*
(Other instructions on reverse side)

Form approved.
Budget Bureau No. 42-R1424.

SUNDRY NOTICES AND REPORTS ON WELLS

(Do not use this form for proposals to drill or to deepen or plug back to a different reservoir. Use "APPLICATION FOR PERMIT—" for such proposals.)

5. LEASE DESIGNATION AND SERIAL NO.: U 8350

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

1. OIL WELL ☐ GAS WELL ☐ OTHER: Dry Hole

7. UNIT AGREEMENT NAME:

2. NAME OF OPERATOR: Westates Petroleum Company

8. FARM OR LEASE NAME: Tully-Federal

3. ADDRESS OF OPERATOR: 1600 Broadway - Suite 2360, Denver, Colo. 80202

9. WELL NO.: 1

4. LOCATION OF WELL (Report location clearly and in accordance with any State requirements.* See also space 17 below.) At surface: 390' from SL, 2100' from EL

10. FIELD AND POOL, OR WILDCAT: Wildcat

11. SEC., T., R., M., OR BLK. AND SURVEY OR AREA: 27-4S-22E

14. PERMIT NO.:

15. ELEVATIONS (Show whether DF, RT, GR, etc.): 5084 KB, 5083 DF, 5071 Gr.

12. COUNTY OR PARISH: Uintah

13. STATE: Utah

16. **Check Appropriate Box To Indicate Nature of Notice, Report, or Other Data**

NOTICE OF INTENTION TO:				SUBSEQUENT REPORT OF:			
TEST WATER SHUT-OFF	☐	PULL OR ALTER CASING	☐	WATER SHUT-OFF	☐	REPAIRING WELL	☐
FRACTURE TREAT	☐	MULTIPLE COMPLETE	☐	FRACTURE TREATMENT	☐	ALTERING CASING	☐
SHOOT OR ACIDIZE	☐	ABANDON*	☐	SHOOTING OR ACIDIZING	☐	ABANDONMENT*	X
REPAIR WELL	☐	CHANGE PLANS	☐	(Other)			
(Other)				(NOTE: Report results of multiple completion on Well Completion or Recompletion Report and Log form.)			

17. DESCRIBE PROPOSED OR COMPLETED OPERATIONS (Clearly state all pertinent details, and give pertinent dates, including estimated date of starting any proposed work. If well is directionally drilled, give subsurface locations and measured and true vertical depths for all markers and zones pertinent to this work.)*

Well was spudded at 6:00 p.m., August 2, and drilled with rotary tools to 4838' T.D. in Weber Sand. Top of Weber was 4740. A drill stem test 4745 to 4835 recovered 1000 ft. of muddy water and 2370 ft. of clear fresh water (resistivity 4 ohms @ 90° F). A minor show of gas was noted 1722 to 1729 in a Morrison sand. An unsuccessful attempt was made to test. Otherwise, there were no significant shows either in samples or on a mechanical mud-logger, and verbal permission to plug was given by Mr. E. W. Guynn of the U.S. Geological Survey on September 10, 1974. Mr. Cleon Feight of the Utah State O. & G. Commission was notified of the plugging. Mr. Ronald Alexander, U.S.G.S., Vernal, was notified at that time. Log form 9-330 with electric logs will follow.
Surface casing - 277' of 36# 9 5/8" set at 289' K.B. was left in the hole.

18. I hereby certify that the foregoing is true and correct

SIGNED Peter C. Dunn TITLE Area Manager DATE 9/13/74

(This space for Federal or State office use)

APPROVED BY _____ TITLE _____ DATE _____
CONDITIONS OF APPROVAL, IF ANY:

*See Instructions on Reverse Side

Instructions

General: This form is designed for submitting proposals to perform certain well operations, and reports of such operations when completed, as indicated, on Federal and Indian lands pursuant to applicable Federal law and regulations, and, if approved or accepted by any State, on all lands in such State, pursuant to applicable State law and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from, the local Federal and/or State office.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 17: Proposals to abandon a well and subsequent reports of abandonment should include such special information as is required by local Federal and/or State offices. In addition, such proposals and reports should include reasons for the abandonment; data on any former or present productive zones, or other zones with present significant fluid contents not sealed off by cement or otherwise; depths (top and bottom) and method of placement of cement plugs; mud or other material placed below, between and above plugs; amount, size, method of parting of any casing, liner or tubing pulled and the depth to top of any left in the hole; method of closing top of well; and date well site conditioned for final inspection looking to approval of the abandonment.

U.S. GOVERNMENT PRINTING OFFICE: 1966 O-685229

847-485

Halliburton cementing services was used to emplace plugs in the well. 9.2 pound fresh water based gel mud was placed between plugs. Plugs were placed as follows:

#1	4775-4675	40 sx.
#2	3720-3620	40 sx.
#3	2220-2120	45 sx.
#4	1050-900	55 sx.
#5	650-550	35 sx.
#6	315-240	40 sx.

Surface plug and marker will be placed in the surface casing when rig is removed and surface graded.

Form 9-330
(Rev. 5-68)

UNITED STATES
DEPARTMENT OF THE INTERIOR
GEOLOGICAL SURVEY

SUBMIT IN DUPLICATE
(See other instructions on reverse side)

Form approved.
Budget Bureau No. 42-R355.5.

WELL COMPLETION OR RECOMPLETION REPORT AND LOG*

5. LEASE DESIGNATION AND SERIAL NO.: U-8350

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

7. UNIT AGREEMENT NAME:

8. FARM OR LEASE NAME:

9. WELL NO.: #1

10. FIELD AND POOL, OR WILDCAT: Wildcat

11. SEC., T., R., M., OR BLOCK AND SURVEY OR AREA: 27-4S-22E

1a. TYPE OF WELL: OIL WELL ☐ GAS WELL ☐ DRY ☒ Other

b. TYPE OF COMPLETION: NEW WELL ☒ WORK OVER ☐ DEEP-EN ☐ PLUG BACK ☐ DIFF. RESVR. ☐ Other

2. NAME OF OPERATOR: Westates Petroleum Company

3. ADDRESS OF OPERATOR: 1600 Broadway, Suite 2360 - Denver, Colorado 80202

4. LOCATION OF WELL (*Report location clearly and in accordance with any State requirements*)*
At surface 390' North of South Line, 2100' West of East Line
At top prod. interval reported below
At total depth 350.2 North of South Line 1891.2 West of East Line

14. PERMIT NO. | DATE ISSUED: July 5, 1974

12. COUNTY OR PARISH: Uintah | 13. STATE: Utah

15. DATE SPUDDED: August 2, 1974 | 16. DATE T.D. REACHED: September 3, 1974 | 17. DATE COMPL. (*Ready to prod.*): ---------- | 18. ELEVATIONS (DF, RKB, RT, GR, ETC.)*: 5071 Gr., 5084 KB | 19. ELEV. CASINGHEAD:

20. TOTAL DEPTH, MD & TVD: 4835 | 21. PLUG, BACK T.D., MD & TVD: | 22. IF MULTIPLE COMPL., HOW MANY*: | 23. INTERVALS DRILLED BY: → | ROTARY TOOLS: 0 - 4835 | CABLE TOOLS:

24. PRODUCING INTERVAL(S), OF THIS COMPLETION—TOP, BOTTOM, NAME (MD AND TVD)*:

25. WAS DIRECTIONAL SURVEY MADE: Yes

26. TYPE ELECTRIC AND OTHER LOGS RUN: I.E.S., Sonic Gamma Ray Cal., Directional Survey

27. WAS WELL CORED: No

28. CASING RECORD (*Report all strings set in well*)

CASING SIZE	WEIGHT, LB./FT.	DEPTH SET (MD)	HOLE SIZE	CEMENTING RECORD	AMOUNT PULLED
9-5/8"	36#	289 KB	13½"	235 sacks	None

29. LINER RECORD

SIZE	TOP (MD)	BOTTOM (MD)	SACKS CEMENT*	SCREEN (MD)

30. TUBING RECORD

SIZE	DEPTH SET (MD)	PACKER SET (MD)

31. PERFORATION RECORD (*Interval, size and number*)

32. ACID, SHOT, FRACTURE, CEMENT SQUEEZE, ETC.

DEPTH INTERVAL (MD)	AMOUNT AND KIND OF MATERIAL USED

33.* Dry hole

PRODUCTION

DATE FIRST PRODUCTION | PRODUCTION METHOD (*Flowing, gas lift, pumping—size and type of pump*) | WELL STATUS (*Producing or shut-in*)

DATE OF TEST	HOURS TESTED	CHOKE SIZE	PROD'N. FOR TEST PERIOD →	OIL—BBL.	GAS—MCF.	WATER—BBL.	GAS-OIL RATIO

FLOW. TUBING PRESS.	CASING PRESSURE	CALCULATED 24-HOUR RATE →	OIL—BBL.	GAS—MCF.	WATER—BBL.	OIL GRAVITY-API (CORR.)

34. DISPOSITION OF GAS (*Sold, used for fuel, vented, etc.*)

TEST WITNESSED BY

35. LIST OF ATTACHMENTS
2 I.E.S., 2 Sonic Gamma Ray, 2 Directional Surveys, 4 Johnson Formation Tests, 2 Formation Records

36. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records

SIGNED [signature] TITLE Area Manager DATE Sept. 23., 1974

*(See Instructions and Spaces for Additional Data on Reverse Side)

INSTRUCTIONS

General: This form is designed for submitting a complete and correct well completion report and log on all types of lands and leases to either a Federal agency or a State agency, or both, pursuant to applicable Federal and/or State laws and regulations. Any necessary special instructions concerning the use of this form and the number of copies to be submitted, particularly with regard to local, area, or regional procedures and practices, either are shown below or will be issued by, or may be obtained from, the local Federal and/or State office. See instructions on items 22 and 24, and 33, below regarding separate reports for separate completions.

If not filed prior to the time this summary record is submitted, copies of all currently available logs (drillers, geologists, sample and core analysis, all types electric, etc.), formation and pressure tests, and directional surveys, should be attached hereto, to the extent required by applicable Federal and/or State laws and regulations. All attachments should be listed on this form, see item 35.

Item 4: If there are no applicable State requirements, locations on Federal or Indian land should be described in accordance with Federal requirements. Consult local State or Federal office for specific instructions.

Item 18: Indicate which elevation is used as reference (where not otherwise shown) for depth measurements given in other spaces on this form and in any attachments.

Items 22 and 24: If this well is completed for separate production from more than one interval zone (multiple completion), so state in item 22, and in item 24 show the producing interval, or intervals, top(s), bottom(s) and name(s) (if any) for only the interval reported in item 33. Submit a separate report (page) on this form, adequately identified, for each additional interval to be separately produced, showing the additional data pertinent to such interval.

Item 29: *"Sacks Cement":* Attached supplemental records for this well should show the details of any multiple stage cementing and the location of the cementing tool.

Item 33: Submit a separate completion report on this form for each interval to be separately produced. (See instruction for items 22 and 24 above.)

37. SUMMARY OF POROUS ZONES:
SHOW ALL IMPORTANT ZONES OF POROSITY AND CONTENTS THEREOF; CORED INTERVALS; AND ALL DRILL-STEM TESTS, INCLUDING DEPTH INTERVAL TESTED, CUSHION USED, TIME TOOL OPEN, FLOWING AND SHUT-IN PRESSURES, AND RECOVERIES

FORMATION	TOP	BOTTOM	DESCRIPTION, CONTENTS, ETC.
Frontier Sand	600	805	Fine and medium grained sand, water bearing (e log)
Dakota Sand	950	1102	Fine, medium and coarse sandstone, water bearing (e log and cuttings)
Entrada Sand	2220	2510	Fine and medium grained sandstone, water bearing (e log and cuttings)
Shinarump Sd. & Cg.	3710	3820	Fine to coarse sandstone and conglomerate, water bearing (e log and cuttings)
Weber Sand	4740	TD 4835	Fine and medium grained sandstone, water bearing (D.S.T.)

D.S.T. #1 (1719 - 1735) Packers failed immediately

D.S.T. #2 (4745-4835) Open 10 min.; SI 1 hr.; open 90 min.; SI 1 hr.; rec. light to medium steady blow throughout test; rec. 900' mud and watery mud and 2370' fresh water, 215 ppm chlorides at 92°F

38. GEOLOGIC MARKERS

NAME	TOP MEAS. DEPTH	TOP TRUE VERT. DEPTH
Spud: Mancos		
Frontier	600	599.9
Lower Mancos (Mowry)	805	804.9
Dakota	950	949.8
Morrison	1102	1101.6
Curtis	2080	2076.7
Entrada	2220	2216.6
Carmel	2512	2508.4
Navajo	2670	2666
Chinle	3505	3500
Shinarump	3710	3703
Moenkopi	3820	3813.3
Phosphoria	4507	4492.5
Weber	4740	4720.5

U.S. GOVERNMENT PRINTING OFFICE: 1963—O-683636