API Well Number: 43013518610000

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 3

AMENDED REPORT ☐

APPLICATION FOR PERMIT TO DRILL

1. WELL NAME and NUMBER
Tomlin 4-6-3-1WH

2. TYPE OF WORK
DRILL NEW WELL ■ REENTER P&A WELL ☐ DEEPEN WELL ☐

3. FIELD OR WILDCAT
WILDCAT

4. TYPE OF WELL
Oil Well Coalbed Methane Well: NO

5. UNIT or COMMUNITIZATION AGREEMENT NAME

6. NAME OF OPERATOR
NEWFIELD PRODUCTION COMPANY

7. OPERATOR PHONE
435 646-4825

8. ADDRESS OF OPERATOR
Rt 3 Box 3630 , Myton, UT, 84052

9. OPERATOR E-MAIL
mcrozier@newfield.com

10. MINERAL LEASE NUMBER (FEDERAL, INDIAN, OR STATE)
Patented

11. MINERAL OWNERSHIP
FEDERAL ☐ INDIAN ☐ STATE ☐ FEE ■

12. SURFACE OWNERSHIP
FEDERAL ☐ INDIAN ☐ STATE ☐ FEE ■

13. NAME OF SURFACE OWNER (if box 12 = 'fee')
Farrer Family Partnership

14. SURFACE OWNER PHONE (if box 12 = 'fee')
435-748-5180

15. ADDRESS OF SURFACE OWNER (if box 12 = 'fee')
P.O. Box 241, ,

16. SURFACE OWNER E-MAIL (if box 12 = 'fee')

17. INDIAN ALLOTTEE OR TRIBE NAME (if box 12 = 'INDIAN')

18. INTEND TO COMMINGLE PRODUCTION FROM MULTIPLE FORMATIONS
YES ☐ (Submit Commingling Application) NO ■

19. SLANT
VERTICAL ☐ DIRECTIONAL ☐ HORIZONTAL ■

20. LOCATION OF WELL	FOOTAGES	QTR-QTR	SECTION	TOWNSHIP	RANGE	MERIDIAN
LOCATION AT SURFACE	453 FNL 1161 FWL	NWNW	6	3.0 S	1.0 W	U
Top of Uppermost Producing Zone	660 FNL 660 FWL	NWNW	6	3.0 S	1.0 W	U
At Total Depth	660 FSL 660 FWL	SWSW	6	3.0 S	1.0 W	U

21. COUNTY
DUCHESNE

22. DISTANCE TO NEAREST LEASE LINE (Feet)
453

23. NUMBER OF ACRES IN DRILLING UNIT
40

25. DISTANCE TO NEAREST WELL IN SAME POOL (Applied For Drilling or Completed)
2030

26. PROPOSED DEPTH
MD: 13586 TVD: 9082

27. ELEVATION - GROUND LEVEL
5233

28. BOND NUMBER
B001834

29. SOURCE OF DRILLING WATER / WATER RIGHTS APPROVAL NUMBER IF APPLICABLE
437478

Hole, Casing, and Cement Information

String	Hole Size	Casing Size	Length	Weight	Grade & Thread	Max Mud Wt.	Cement	Sacks	Yield	Weight
Cond	17.5	14	0 - 60	37.0	H-40 ST&C	0.0	Class G	35	1.17	15.8
Surf	12.25	9.625	0 - 2500	36.0	J-55 LT&C	8.3	Type III	216	3.33	11.0
							Type III	95	1.9	13.0
I1	8.75	7	0 - 9638	26.0	P-110 Other	10.5	35/65 Poz	305	2.59	11.5
							50/50 Poz	275	1.62	13.0
Prod	6.125	4.5	8714 - 13586	13.5	P-110 Other	10.5	No Used	0	0.0	0.0

ATTACHMENTS

VERIFY THE FOLLOWING ARE ATTACHED IN ACCORDANCE WITH THE UTAH OIL AND GAS CONSERVATION GENERAL RULES

- ✔ WELL PLAT OR MAP PREPARED BY LICENSED SURVEYOR OR ENGINEER
- ✔ COMPLETE DRILLING PLAN
- ✔ AFFIDAVIT OF STATUS OF SURFACE OWNER AGREEMENT (IF FEE SURFACE)
- ☐ FORM 5. IF OPERATOR IS OTHER THAN THE LEASE OWNER
- ✔ DIRECTIONAL SURVEY PLAN (IF DIRECTIONALLY OR HORIZONTALLY DRILLED)
- ✔ TOPOGRAPHICAL MAP

NAME Don Hamilton **TITLE** Permitting Agent **PHONE** 435 719-2018

SIGNATURE **DATE** 11/08/2012 **EMAIL** starpoint@etv.net

API NUMBER ASSIGNED
43013518610000

APPROVAL
Permit Manager

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RECEIVED: December 11, 2012

Newfield Production Company
4-6-3-1WH
Surface Hole Location: 453' FNL, 1161' FWL, Section 6, T3S, R1W
Bottom Hole Location: 660' FSL, 660' FWL, Section 6, T3S, R1W
Duchesne County, UT

Drilling Program

1. Formation Tops

Uinta	surface			
Green River	3,050'			
Garden Gulch member	7,064'			
Uteland Butte	9,235'			
Lateral TD	9,082'	TVD /	13,586'	MD

2. Depth to Oil, Gas, Water, or Minerals

Base of moderately saline	578'		(water)
Green River	7,064'	- 9,082'	(oil)

3. Pressure Control

Section	BOP Description
Surface	12-1/4" diverter
Interm/Prod	The BOP and related equipment shall meet the minimum requirements of Onshore Oil and Gas Order No. 2 for equipment and testing requirements, procedures, etc for a 5M system. A 5M BOP system will consist of 2 ram preventers (double or two singles) and an annular preventer (see attached diagram). A choke manifold rated to at least 5,000 psi will be used.

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4. Casing

Description	Interval		Weight (ppf)	Grade	Coup	Pore Press @ Shoe	MW @ Shoe	Frac Grad @ Shoe	Safety Factors		
	Top	Bottom (TVD/MD)							Burst	Collapse	Tension
Conductor	0'	60'	37	H-40	Weld	--	--	--	--	--	--
14									--	--	--
Surface	0'	2,500'	36	J-55	LTC	8.33	8.33	12	3,520	2,020	453,000
9 5/8									2.51	2.54	5.03
Intermediate	0'	9,285'	26	P-110	BTC	10	10.5	15	9,960	6,210	830,000
7		9,638'							2.55	1.50	3.31
Production	8,714'	9,082'	13.5	P-110	BTC	10	10.5	--	12,410	10,670	422,000
4 1/2		13,586'							3.25	2.63	6.42

Assumptions:

Surface casing MASP = (frac gradient + 1.0 ppg) - (gas gradient)
Intermediate casing MASP = (reservoir pressure) - (gas gradient)

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Production casing MASP = (reservoir pressure) - (gas gradient)
All collapse calculations assume fully evacuated casing with a gas gradient
All tension calculations assume air weight of casing
Gas gradient = 0.1 psi/ft

All casing shall be new.
All casing strings shall have a minimum of 1 centralizer on each of the bottom 3 joints.

5. Cement

Job	Hole Size	Fill	Slurry Description	ft^3 / sacks	OH excess	Weight (ppg)	Yield (ft^3/sk)
Conductor	17 1/2	60'	Class G w/ 2% KCl + 0.25 lbs/sk Cello Flake	41 / 35	15%	15.8	1.17
Surface Lead	12 1/4	2,000'	Type III + .125 lbs/sk Cello Flakes	720 / 216	15%	11.0	3.33
Surface Tail	12 1/4	500'	Type III + .125 lbs/sk Cello Flakes	180 / 95	15%	13.0	1.9
Intermediate Lead	8 3/4	4,564'	Premium - 65% Class G / 35% Poz + 10% Bentonite	789 / 305	15%	11.5	2.59
Intermediate Tail	8 3/4	2,574'	50/50 Poz/Class G + 1% bentonite	445 / 275	15%	13.0	1.62
Production	6 1/8	--	Liner will not be cemented. It will be isolated with a liner top packer.	-- / --	--	--	--

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The surface casing will be cemented to surface. In the event that cement does not reach surface during the primary cement job, a remedial job will be performed.

Actual cement volumes for the intermediate casing string will be calculated from an open hole caliper log, plus 15% excess.

The cement slurries will be adjusted for hole conditions and blend test results.

The production liner will be left uncemented. Individual frac stages will be isolated with open hole packers. A liner top hanger and packer will be installed 50' above KOP.

6. Type and Characteristics of Proposed Circulating Medium

Interval — **Description**

Surface - 2,500'

An air and/or fresh water system will be utilized. If an air rig is used, the blooie line discharge may be less than 100' from the wellbore in order to minimize location size. The blooie line is not equipped with an automatic igniter. The air compressor may be located less than 100' from the well bore due to the low possibility of combustion with the air/dust mixture. Water will be on location to be used as kill fluid, if necessary.

2,500' - TD

A water based mud system will be utilized. Hole stability may be improved with additions of KCl or a similar inhibitive substance. In order to control formation pressure the system will be weighted with additions of bentonite, and

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if conditions warrant, with barite.
Anticipated maximum mud weight is 10.5 ppg.

7. Logging, Coring, and Testing

Logging: A dual induction, gamma ray, and caliper log will be run in the intermediate section from the top of the curve to the base of the surface casing. A compensated neutron/formation density log will be run in the intermediate section from the top of the curve to the top of the Garden Gulch formation. A cement bond log will be run from the top of the curve to the cement top behind the intermediate casing.

Cores: As deemed necessary.

DST: There are no DST's planned for this well.

8. Anticipated Abnormal Pressure or Temperature

Maximum anticipated bottomhole pressure will be approximately equal to total depth (feet) multiplied by a 0.52 psi/ft gradient.

9,082' x 0.52 psi/ft = 4723 psi

No abnormal temperature is expected. No H_2S is expected.

9. Other Aspects

An 8-3/4" vertical hole will be drilled to a kick off point of 8,764' .
Directional tools will then be used to build to 92.95 degrees inclination.
The 7" intermediate casing string will be set once the well is landed horizontally in the target zone.

The lateral will be drilled to the bottomhole location shown on the plat.
A liner with a system of open hole packers will be used to provide multi-stage frac isolation in the lateral. The top of the liner will be place 50' above KOP and will be isolated with a liner top packer.

Newfield requests the following variances from Onshore Order #2:
- Variance from Onshoer Order #2, III.E.1
  Refer to Newfield Production Company Standard Operating Practices "Ute Tribal Green River Development Program" paragraph 9.0

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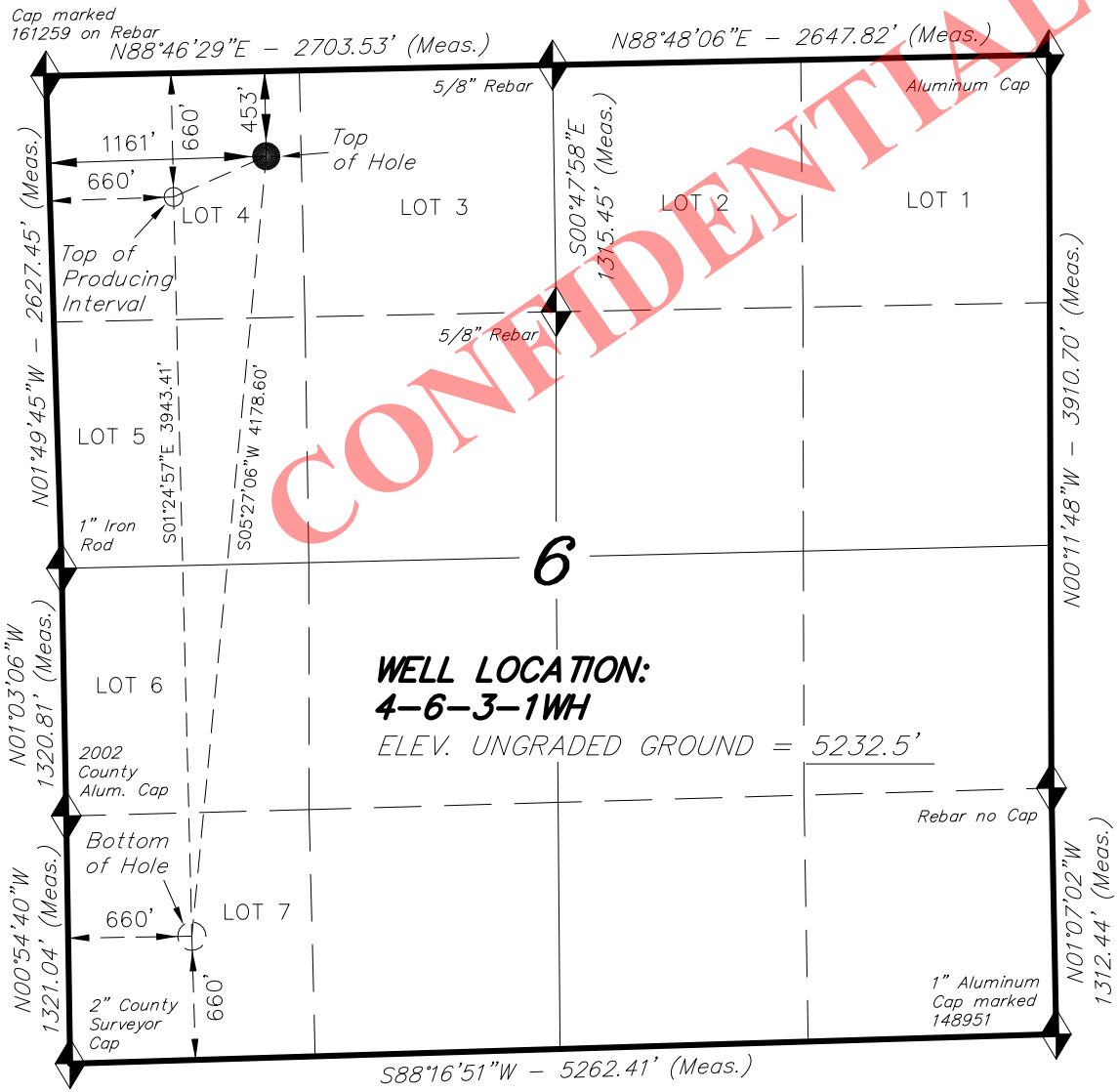
T3S, R1W, U.S.B.&M.



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NEWFIELD EXPLORATION COMPANY

WELL LOCATION, 4–6–3–1WH, LOCATED AS SHOWN IN THE NW 1/4 NW 1/4 (LOT 4) OF SECTION 6, T3S, R1W, U.S.B.&M. DUCHESNE COUNTY, UTAH.

TARGET BOTTOM HOLE, 4–6–3–1WH, LOCATED AS SHOWN IN THE SW 1/4 SW 1/4 (LOT 7) OF SECTION 6, T3S, R1W, U.S.B&M. DUCHESNE COUNTY, UTAH.

1000' 500' 0' 1000'

BAR SCALE

N

NOTES:

1. *Well footages are measured at right angles to the Section Lines.*
2. *Bearings are based on Global Positioning Satellite observations.*
3. *The Top of Producing Interval bears S66°15'20"W 540.16' from the Top of Hole.*

THIS IS TO CERTIFY THAT THE ABOVE PLAT WAS PREPARED FROM FIELD NOTES OF ACTUAL SURVEYS MADE BY ME OR UNDER MY SUPERVISION AND THAT THE SAME ARE TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.

REGISTERED LAND SURVEYOR No.189377 03-16-12 STACY W. STEWART STATE OF UTAH

REGISTERED LAND SURVEYOR
REGISTRATION No. 189377
STATE OF UTAH

= SECTION CORNERS LOCATED

BASIS OF ELEV; Elevations are based on an N.G.S. OPUS Correction. LOCATION: LAT. 40°04'09.56" LONG. 110°00'43.28" (Tristate Aluminum Cap) Elev. 5281.57'

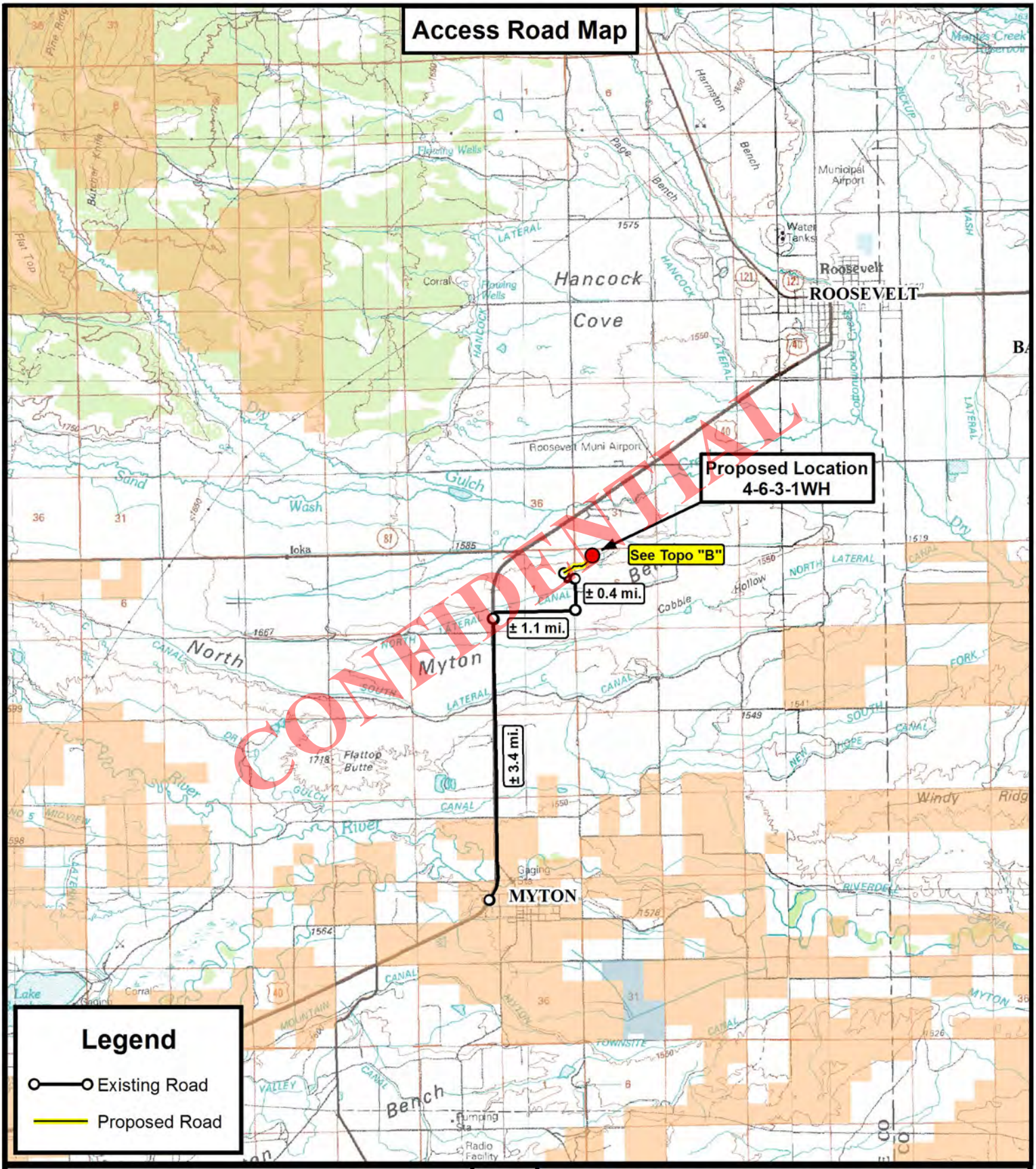
4–6–3–1WH (Surface Location) NAD 83
LATITUDE = 40° 15' 26.39"
LONGITUDE = 110° 02' 39.92"

TRI STATE LAND SURVEYING & CONSULTING
180 NORTH VERNAL AVE. – VERNAL, UTAH 84078
(435) 781–2501

DATE SURVEYED: 02–20–12	SURVEYED BY: P.H.	VERSION:
DATE DRAWN: 03–01–12	DRAWN BY: R.B.T.	V1
REVISED:	SCALE: 1" = 1000'	

RECEIVED: November 08, 2012

API Well Number: 43013518610000



Tri State Land Surveying, Inc.
180 NORTH VERNAL AVE. VERNAL, UTAH 84078
P: (435) 781-2501
F: (435) 781-2518

N

NEWFIELD EXPLORATION COMPANY

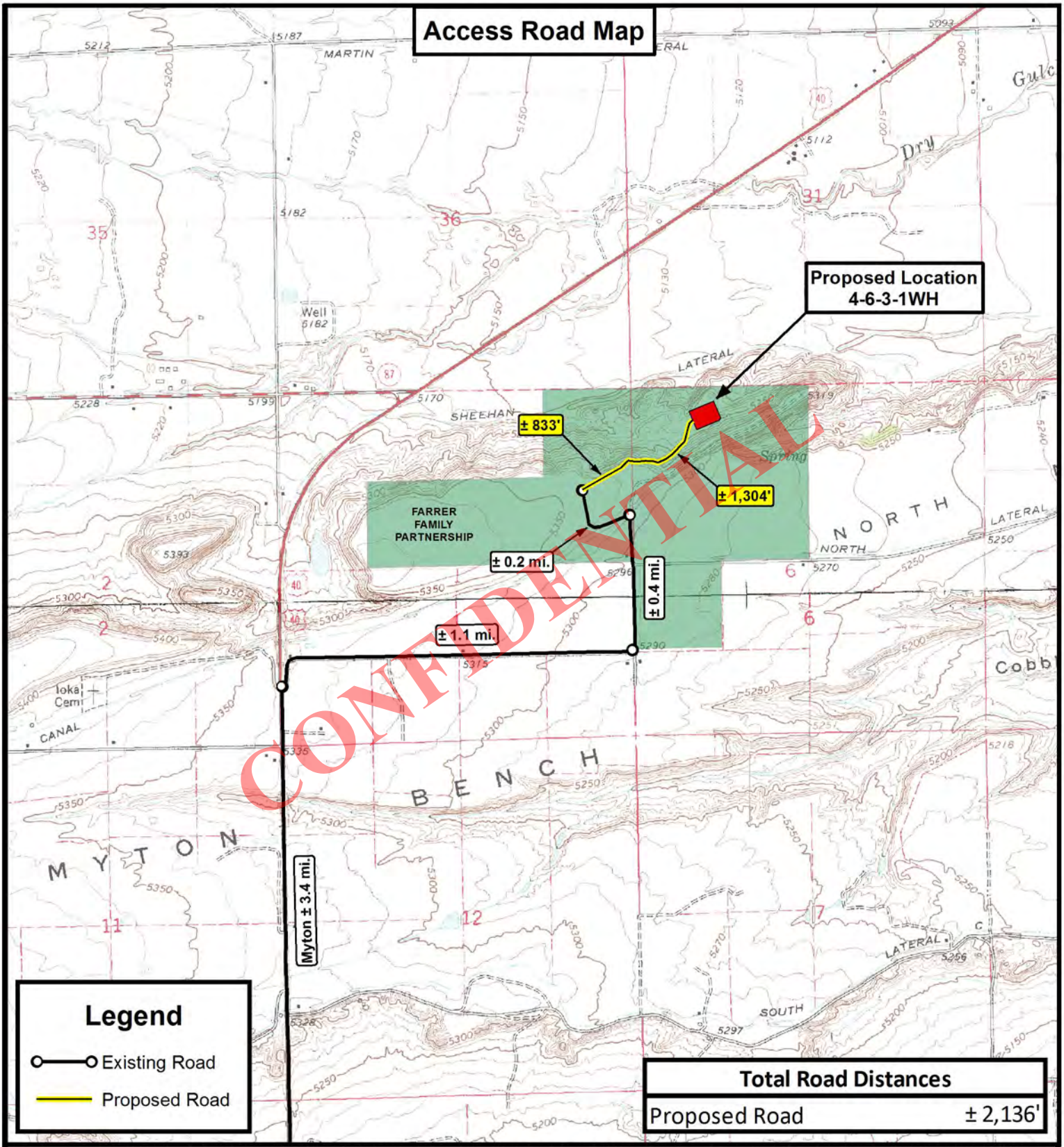
4-6-3-1WH
SEC. 6, T3S, R1W, U.S.B.&M.
Duchesne County, UT.

DRAWN BY: A.P.C.	REVISED:	VERSION:	
DATE: 03-16-2012		V1	
SCALE: 1:100,000			

TOPOGRAPHIC MAP

SHEET A

API Well Number: 43013518610000



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THE PARCEL INFORMATION SHOWN HAS NOT BEEN SURVEYED BY TRI-STATE LAND SURVEYING, INC. - TRI-STATE DOES NOT WARRANTY PROPERTY PARCEL DATA OR ANY ASSOCIATED INFORMATION. A PROPERTY SURVEY IS REQUIRED TO DETERMINE THE ACTUAL LOCATION OF PROPERTY LINES AND SHOW ACCURATE DISTANCES ACROSS PARCELS.

Tri State Land Surveying, Inc.
180 NORTH VERNAL AVE. VERNAL, UTAH 84078
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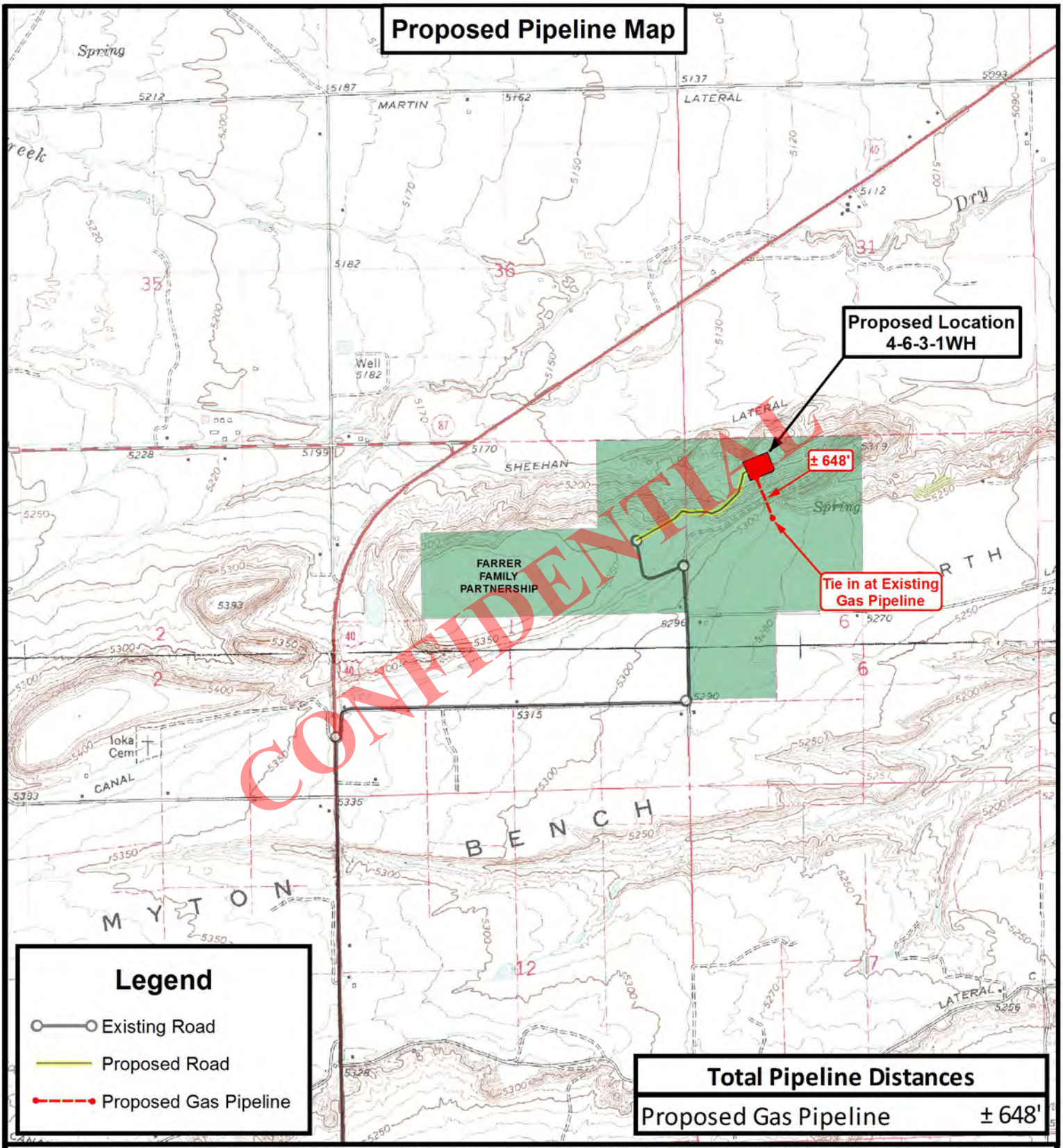
NEWFIELD EXPLORATION COMPANY

4-6-3-1WH
SEC. 6, T3S, R1W, U.S.B.&M.
Duchesne County, UT.

DRAWN BY: A.P.C.	REVISED:	VERSION:	TOPOGRAPHIC MAP
DATE: 03-16-2012		V1	SHEET B
SCALE: 1 " = 2,000 '			

API Well Number: 43013518610000

Proposed Pipeline Map



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Total Pipeline Distances	
Proposed Gas Pipeline	± 648'

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Tri State Land Surveying, Inc.
180 NORTH VERNAL AVE. VERNAL, UTAH 84078
P: (435) 781-2501
F: (435) 781-2518

N

NEWFIELD EXPLORATION COMPANY

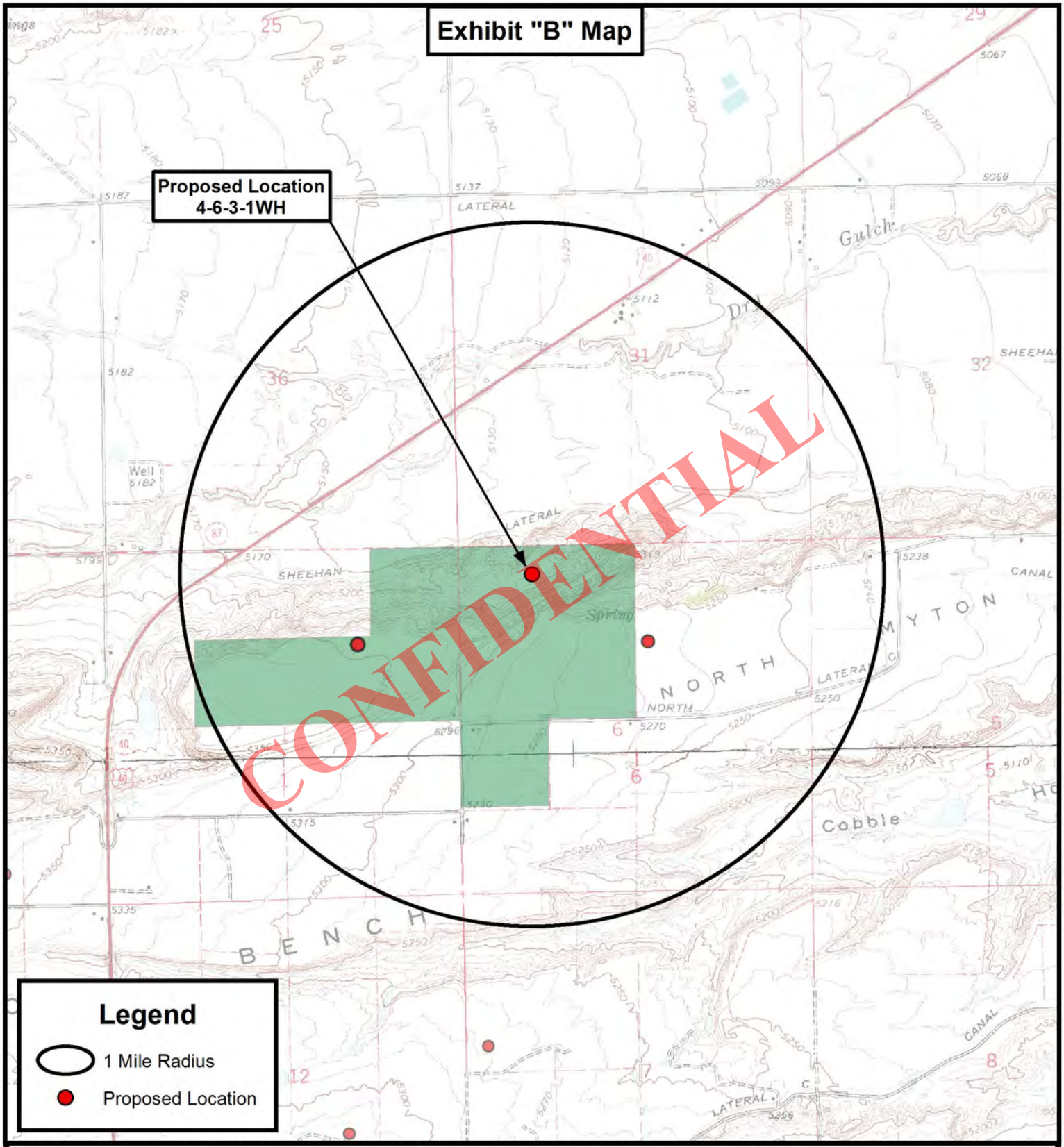
4-6-3-1WH
SEC. 6, T3S, R1W, U.S.B.&M.
Duchesne County, UT.

DRAWN BY:	A.P.C.	REVISED:	VERSION:
DATE:	03-16-2012		V1
SCALE:	1 " = 2,000 '		

TOPOGRAPHIC MAP

SHEET C

API Well Number: 43013518610000



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F: (435) 781-2518

N

NEWFIELD EXPLORATION COMPANY

4-6-3-1WH
SEC. 6, T3S, R1W, U.S.B.&M.
Duchesne County, UT.

DRAWN BY:	A.P.C.	REVISED:	VERSION:
DATE:	03-16-2012		V1
SCALE:	1 " = 2,000 '		

TOPOGRAPHIC MAP

SHEET D

API Well Number: 43013518610000

Weatherford®

NEWFIELD EXPLORATION CO.

DUCHESNE COUNTY, UT
TOMLIN 4-6-3-1WH
TOMLIN 4-6-3-1WH

TOMLIN 4-6-3-1WH

Plan: PLAN 1

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Standard Planning Report

25 September, 2012

Weatherford®

RECEIVED: November 08, 2012

API Well Number: 43013518610000

NEWFIELD

Weatherford®

Project:	DUCHESNE COUNTY, UT
Site:	TOMLIN 4-6-3-1WH
Well:	TOMLIN 4-6-3-1WH
Wellbore:	TOMLIN 4-6-3-1WH
Design:	PLAN 1
Latitude:	40° 15' 26.390 N
Longitude:	110° 2' 39.920 W
GL:	5232.50
KB:	KB @ 5250.50ft (Original Well Elev)

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WELLBORE TARGET DETAILS (LAT/LONG)

Name	TVD	+N/-S	+E/-W	Latitude	Longitude	Shape
PBHL - TOMLIN 4-6-3-1WH	9082.00	-4159.82	-396.87	40° 14' 45.280 N	110° 2' 45.038 W	Point
LP - TOMLIN	9285.00	-217.62	-494.31	40° 15' 24.239 N	110° 2' 46.296 W	Point

WELL DETAILS: TOMLIN 4-6-3-1WH

Ground Level: 5232.50

+N/-S	+E/-W	Northing	Easting	Latitude	Longitude	Slot
0.00	0.00	7265764.91	2046632.79	40° 15' 26.390 N	110° 2' 39.920 W	

SECTION DETAILS

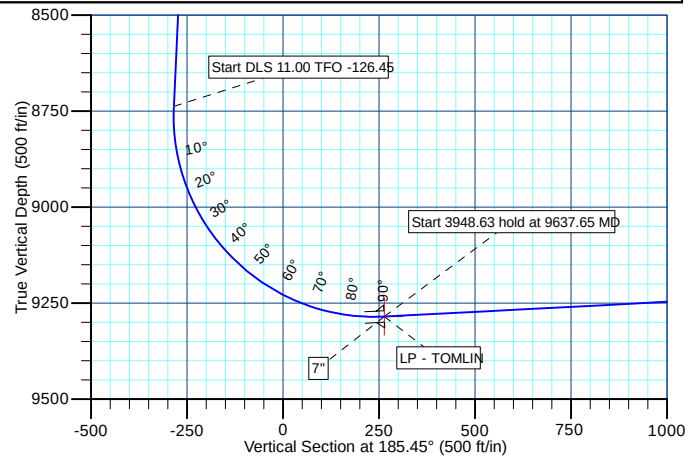
MD	Inc	Azi	TVD	+N/-S	+E/-W	Dleg	TFace	VSect	Annotation
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
2500.00	0.00	0.00	2500.00	0.00	0.00	0.00	0.00	0.00	Start Build 3.00
2676.59	5.30	305.37	2676.34	4.72	-6.65	3.00	305.37	-4.07	Start 6087.35 hold at 2676.59 MD
8763.94	5.30	305.37	8737.69	330.05	-464.97	0.00	0.00	-284.39	Start DLS 11.00 TFO -126.45
9637.65	92.95	178.58	9285.00	-217.62	-494.31	11.00	-126.45	263.58	Start 3948.63 hold at 9637.65 MD
13586.28	92.95	178.58	9082.00	-4159.82	-396.87	0.00	0.00	4178.71	TD at 13586.28

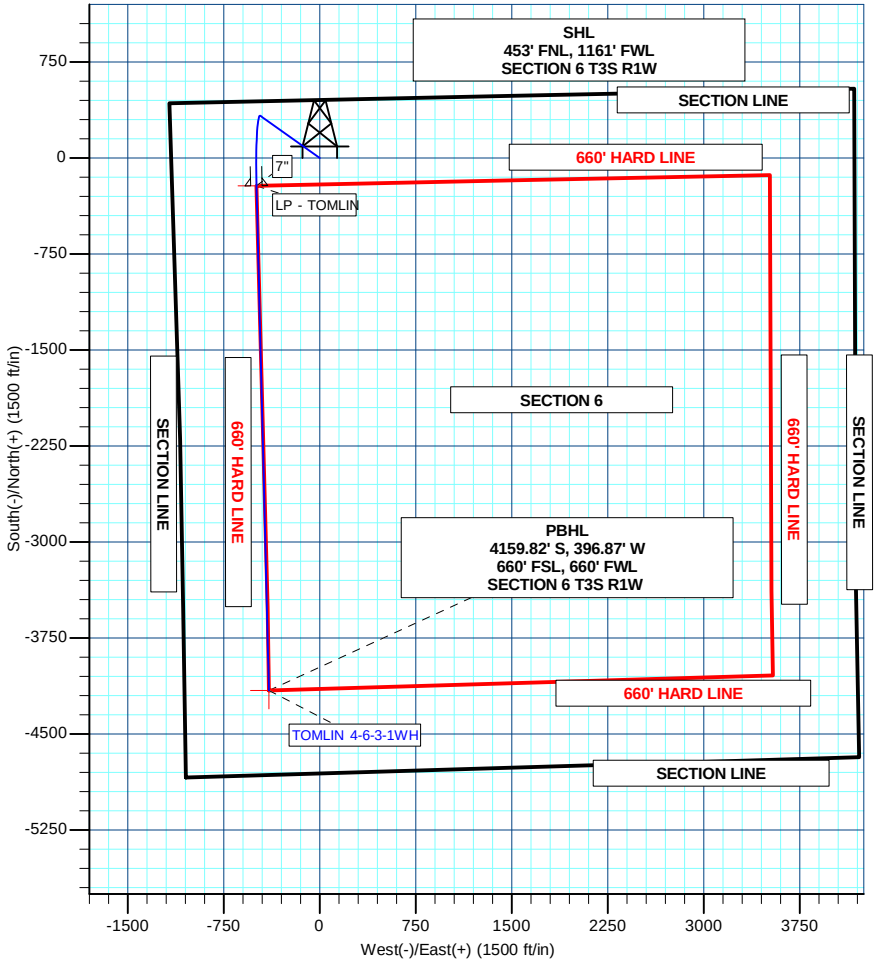
Azimuths to True North
Magnetic North: 11.20°

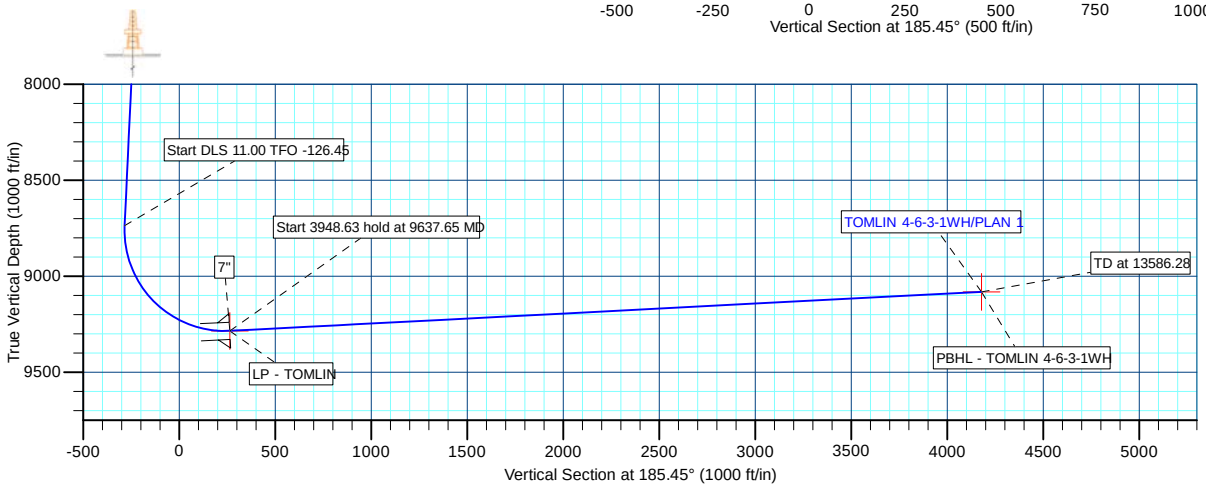
Magnetic Field
Strength: 52206.9snT
Dip Angle: 65.92°
Date: 9/25/2012
Model: BGGM2012

CASING DETAILS

TVD	MD	Name	Size
9285.00	9637.65	7"	7







Plan: PLAN 1 (TOMLIN 4-6-3-1WH/TOMLIN 4-6-3-1WH)

Created By: MATT MAYDEW Date: 13:15, September 25 2012

Weatherford International Ltd.

Planning Report

Database:	EDM 5000.1 Single User Db	**Local Co-ordinate Reference:**	Well TOMLIN 4-6-3-1WH
Company:	NEWFIELD EXPLORATION CO.	**TVD Reference:**	KB @ 5250.50ft (Original Well Elev)
Project:	DUCHESNE COUNTY, UT	**MD Reference:**	KB @ 5250.50ft (Original Well Elev)
Site:	TOMLIN 4-6-3-1WH	**North Reference:**	True
Well:	TOMLIN 4-6-3-1WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	TOMLIN 4-6-3-1WH		
Design:	PLAN 1		

Project DUCHESNE COUNTY, UT

Map System:	US State Plane 1983	**System Datum:**	Mean Sea Level
Geo Datum:	North American Datum 1983		
Map Zone:	Utah Central Zone		

Site TOMLIN 4-6-3-1WH

Site Position:		**Northing:**	7,265,764.91 usft	**Latitude:**	40° 15' 26.390 N
From:	Lat/Long	**Easting:**	2,046,632.79 usft	**Longitude:**	110° 2' 39.920 W
Position Uncertainty:	0.00 ft	**Slot Radius:**	13-3/16"	**Grid Convergence:**	0.93 °

Well TOMLIN 4-6-3-1WH

Well Position	**+N/-S**	0.00 ft	**Northing:**	7,265,764.91 usft	**Latitude:**	40° 15' 26.390 N
	+E/-W	0.00 ft	**Easting:**	2,046,632.79 usft	**Longitude:**	110° 2' 39.920 W
Position Uncertainty		0.00 ft	**Wellhead Elevation:**	ft	**Ground Level:**	5,232.50 ft

Wellbore TOMLIN 4-6-3-1WH

Magnetics	Model Name	Sample Date	Declination (°)	Dip Angle (°)	Field Strength (nT)
	BGGM2012	9/25/2012	11.20	65.92	52,207

Design PLAN 1

Audit Notes:

Version:	**Phase:** PLAN	**Tie On Depth:**	0.00

Vertical Section:	Depth From (TVD) (ft)	+N/-S (ft)	+E/-W (ft)	Direction (°)
	0.00	0.00	0.00	185.45

Plan Sections

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)	TFO (°)	Target
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
2,500.00	0.00	0.00	2,500.00	0.00	0.00	0.00	0.00	0.00	0.00	
2,676.59	5.30	305.37	2,676.34	4.72	-6.65	3.00	3.00	0.00	305.37	
8,763.94	5.30	305.37	8,737.69	330.05	-464.97	0.00	0.00	0.00	0.00	
9,637.65	92.95	178.58	9,285.00	-217.62	-494.31	11.00	10.03	-14.51	-126.45	LP - TOMLIN
13,586.28	92.95	178.58	9,082.00	-4,159.82	-396.87	0.00	0.00	0.00	0.00	PBHL - TOMLIN 4-6-3

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RECEIVED: November 08, 2012

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Weatherford International Ltd.

Planning Report

Weatherford

Database:	EDM 5000.1 Single User Db	**Local Co-ordinate Reference:**	Well TOMLIN 4-6-3-1WH
Company:	NEWFIELD EXPLORATION CO.	**TVD Reference:**	KB @ 5250.50ft (Original Well Elev)
Project:	DUCHESNE COUNTY, UT	**MD Reference:**	KB @ 5250.50ft (Original Well Elev)
Site:	TOMLIN 4-6-3-1WH	**North Reference:**	True
Well:	TOMLIN 4-6-3-1WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	TOMLIN 4-6-3-1WH		
Design:	PLAN 1		

Planned Survey

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.00	200.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00	0.00	0.00	300.00	0.00	0.00	0.00	0.00	0.00	0.00
400.00	0.00	0.00	400.00	0.00	0.00	0.00	0.00	0.00	0.00
500.00	0.00	0.00	500.00	0.00	0.00	0.00	0.00	0.00	0.00
600.00	0.00	0.00	600.00	0.00	0.00	0.00	0.00	0.00	0.00
700.00	0.00	0.00	700.00	0.00	0.00	0.00	0.00	0.00	0.00
800.00	0.00	0.00	800.00	0.00	0.00	0.00	0.00	0.00	0.00
900.00	0.00	0.00	900.00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.00	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00
1,100.00	0.00	0.00	1,100.00	0.00	0.00	0.00	0.00	0.00	0.00
1,200.00	0.00	0.00	1,200.00	0.00	0.00	0.00	0.00	0.00	0.00
1,300.00	0.00	0.00	1,300.00	0.00	0.00	0.00	0.00	0.00	0.00
1,400.00	0.00	0.00	1,400.00	0.00	0.00	0.00	0.00	0.00	0.00
1,500.00	0.00	0.00	1,500.00	0.00	0.00	0.00	0.00	0.00	0.00
1,600.00	0.00	0.00	1,600.00	0.00	0.00	0.00	0.00	0.00	0.00
1,700.00	0.00	0.00	1,700.00	0.00	0.00	0.00	0.00	0.00	0.00
1,800.00	0.00	0.00	1,800.00	0.00	0.00	0.00	0.00	0.00	0.00
1,900.00	0.00	0.00	1,900.00	0.00	0.00	0.00	0.00	0.00	0.00
2,000.00	0.00	0.00	2,000.00	0.00	0.00	0.00	0.00	0.00	0.00
2,100.00	0.00	0.00	2,100.00	0.00	0.00	0.00	0.00	0.00	0.00
2,200.00	0.00	0.00	2,200.00	0.00	0.00	0.00	0.00	0.00	0.00
2,300.00	0.00	0.00	2,300.00	0.00	0.00	0.00	0.00	0.00	0.00
2,400.00	0.00	0.00	2,400.00	0.00	0.00	0.00	0.00	0.00	0.00
Start Build 3.00									
2,500.00	0.00	0.00	2,500.00	0.00	0.00	0.00	0.00	0.00	0.00
2,600.00	3.00	305.37	2,599.95	1.52	-2.13	-1.31	3.00	3.00	0.00
Start 6087.35 hold at 2676.59 MD									
2,676.59	5.30	305.37	2,676.34	4.72	-6.65	-4.07	3.00	3.00	0.00
2,700.00	5.30	305.37	2,699.65	5.97	-8.42	-5.15	0.00	0.00	0.00
2,800.00	5.30	305.37	2,799.22	11.32	-15.94	-9.75	0.00	0.00	0.00
2,900.00	5.30	305.37	2,898.79	16.66	-23.47	-14.36	0.00	0.00	0.00
3,000.00	5.30	305.37	2,998.37	22.01	-31.00	-18.96	0.00	0.00	0.00
3,100.00	5.30	305.37	3,097.94	27.35	-38.53	-23.57	0.00	0.00	0.00
3,200.00	5.30	305.37	3,197.51	32.69	-46.06	-28.17	0.00	0.00	0.00
3,300.00	5.30	305.37	3,297.09	38.04	-53.59	-32.78	0.00	0.00	0.00
3,400.00	5.30	305.37	3,396.66	43.38	-61.12	-37.38	0.00	0.00	0.00
3,500.00	5.30	305.37	3,496.23	48.73	-68.65	-41.99	0.00	0.00	0.00
3,600.00	5.30	305.37	3,595.80	54.07	-76.18	-46.59	0.00	0.00	0.00
3,700.00	5.30	305.37	3,695.38	59.42	-83.71	-51.20	0.00	0.00	0.00
3,800.00	5.30	305.37	3,794.95	64.76	-91.24	-55.80	0.00	0.00	0.00
3,900.00	5.30	305.37	3,894.52	70.10	-98.76	-60.41	0.00	0.00	0.00
4,000.00	5.30	305.37	3,994.10	75.45	-106.29	-65.01	0.00	0.00	0.00
4,100.00	5.30	305.37	4,093.67	80.79	-113.82	-69.62	0.00	0.00	0.00
4,200.00	5.30	305.37	4,193.24	86.14	-121.35	-74.22	0.00	0.00	0.00
4,300.00	5.30	305.37	4,292.81	91.48	-128.88	-78.83	0.00	0.00	0.00
4,400.00	5.30	305.37	4,392.39	96.83	-136.41	-83.43	0.00	0.00	0.00
4,500.00	5.30	305.37	4,491.96	102.17	-143.94	-88.04	0.00	0.00	0.00
4,600.00	5.30	305.37	4,591.53	107.51	-151.47	-92.64	0.00	0.00	0.00
4,700.00	5.30	305.37	4,691.11	112.86	-159.00	-97.25	0.00	0.00	0.00
4,800.00	5.30	305.37	4,790.68	118.20	-166.53	-101.85	0.00	0.00	0.00
4,900.00	5.30	305.37	4,890.25	123.55	-174.06	-106.46	0.00	0.00	0.00
5,000.00	5.30	305.37	4,989.82	128.89	-181.58	-111.06	0.00	0.00	0.00

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RECEIVED: November 08, 2012

Weatherford

Weatherford International Ltd.

Planning Report

Weatherford

Database:	EDM 5000.1 Single User Db	**Local Co-ordinate Reference:**	Well TOMLIN 4-6-3-1WH
Company:	NEWFIELD EXPLORATION CO.	**TVD Reference:**	KB @ 5250.50ft (Original Well Elev)
Project:	DUCHESNE COUNTY, UT	**MD Reference:**	KB @ 5250.50ft (Original Well Elev)
Site:	TOMLIN 4-6-3-1WH	**North Reference:**	True
Well:	TOMLIN 4-6-3-1WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	TOMLIN 4-6-3-1WH		
Design:	PLAN 1		

Planned Survey

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
5,100.00	5.30	305.37	5,089.40	134.24	-189.11	-115.67	0.00	0.00	0.00
5,200.00	5.30	305.37	5,188.97	139.58	-196.64	-120.27	0.00	0.00	0.00
5,300.00	5.30	305.37	5,288.54	144.92	-204.17	-124.88	0.00	0.00	0.00
5,400.00	5.30	305.37	5,388.12	150.27	-211.70	-129.48	0.00	0.00	0.00
5,500.00	5.30	305.37	5,487.69	155.61	-219.23	-134.09	0.00	0.00	0.00
5,600.00	5.30	305.37	5,587.26	160.96	-226.76	-138.69	0.00	0.00	0.00
5,700.00	5.30	305.37	5,686.83	166.30	-234.29	-143.30	0.00	0.00	0.00
5,800.00	5.30	305.37	5,786.41	171.65	-241.82	-147.90	0.00	0.00	0.00
5,900.00	5.30	305.37	5,885.98	176.99	-249.35	-152.51	0.00	0.00	0.00
6,000.00	5.30	305.37	5,985.55	182.33	-256.88	-157.11	0.00	0.00	0.00
6,100.00	5.30	305.37	6,085.13	187.68	-264.40	-161.72	0.00	0.00	0.00
6,200.00	5.30	305.37	6,184.70	193.02	-271.93	-166.32	0.00	0.00	0.00
6,300.00	5.30	305.37	6,284.27	198.37	-279.46	-170.93	0.00	0.00	0.00
6,400.00	5.30	305.37	6,383.84	203.71	-286.99	-175.53	0.00	0.00	0.00
6,500.00	5.30	305.37	6,483.42	209.06	-294.52	-180.14	0.00	0.00	0.00
6,600.00	5.30	305.37	6,582.99	214.40	-302.05	-184.74	0.00	0.00	0.00
6,700.00	5.30	305.37	6,682.56	219.74	-309.58	-189.35	0.00	0.00	0.00
6,800.00	5.30	305.37	6,782.14	225.09	-317.11	-193.95	0.00	0.00	0.00
6,900.00	5.30	305.37	6,881.71	230.43	-324.64	-198.56	0.00	0.00	0.00
7,000.00	5.30	305.37	6,981.28	235.78	-332.17	-203.16	0.00	0.00	0.00
7,100.00	5.30	305.37	7,080.85	241.12	-339.70	-207.77	0.00	0.00	0.00
7,200.00	5.30	305.37	7,180.43	246.47	-347.22	-212.37	0.00	0.00	0.00
7,300.00	5.30	305.37	7,280.00	251.81	-354.75	-216.98	0.00	0.00	0.00
7,400.00	5.30	305.37	7,379.57	257.15	-362.28	-221.58	0.00	0.00	0.00
7,500.00	5.30	305.37	7,479.15	262.50	-369.81	-226.19	0.00	0.00	0.00
7,600.00	5.30	305.37	7,578.72	267.84	-377.34	-230.79	0.00	0.00	0.00
7,700.00	5.30	305.37	7,678.29	273.19	-384.87	-235.40	0.00	0.00	0.00
7,800.00	5.30	305.37	7,777.86	278.53	-392.40	-240.00	0.00	0.00	0.00
7,900.00	5.30	305.37	7,877.44	283.88	-399.93	-244.61	0.00	0.00	0.00
8,000.00	5.30	305.37	7,977.01	289.22	-407.46	-249.21	0.00	0.00	0.00
8,100.00	5.30	305.37	8,076.58	294.56	-414.99	-253.82	0.00	0.00	0.00
8,200.00	5.30	305.37	8,176.15	299.91	-422.52	-258.43	0.00	0.00	0.00
8,300.00	5.30	305.37	8,275.73	305.25	-430.04	-263.03	0.00	0.00	0.00
8,400.00	5.30	305.37	8,375.30	310.60	-437.57	-267.64	0.00	0.00	0.00
8,500.00	5.30	305.37	8,474.87	315.94	-445.10	-272.24	0.00	0.00	0.00
8,600.00	5.30	305.37	8,574.45	321.29	-452.63	-276.85	0.00	0.00	0.00
8,700.00	5.30	305.37	8,674.02	326.63	-460.16	-281.45	0.00	0.00	0.00
Start DLS 11.00 TFO -126.45									
8,763.94	5.30	305.37	8,737.69	330.05	-464.97	-284.39	0.00	0.00	0.00
8,800.00	4.34	257.98	8,773.63	330.73	-467.67	-284.82	11.00	-2.67	-131.41
8,850.00	7.61	212.68	8,823.38	327.54	-471.31	-281.30	11.00	6.55	-90.61
8,900.00	12.55	198.35	8,872.60	319.60	-474.81	-273.06	11.00	9.87	-28.65
8,950.00	17.81	192.21	8,920.84	306.96	-478.14	-260.16	11.00	10.53	-12.30
9,000.00	23.19	188.82	8,967.66	289.74	-481.26	-242.72	11.00	10.75	-6.78
9,050.00	28.61	186.65	9,012.62	268.11	-484.16	-220.91	11.00	10.84	-4.33
9,100.00	34.05	185.13	9,055.32	242.26	-486.80	-194.93	11.00	10.89	-3.04
9,150.00	39.51	183.99	9,095.35	212.43	-489.16	-165.01	11.00	10.91	-2.29
9,200.00	44.97	183.08	9,132.35	178.89	-491.22	-131.43	11.00	10.93	-1.81
9,250.00	50.44	182.33	9,165.99	141.96	-492.95	-94.50	11.00	10.94	-1.50
9,300.00	55.92	181.69	9,195.94	101.97	-494.35	-54.56	11.00	10.95	-1.28
9,350.00	61.40	181.13	9,221.93	59.30	-495.39	-11.98	11.00	10.96	-1.12
9,400.00	66.88	180.63	9,243.73	14.33	-496.08	32.85	11.00	10.96	-1.01
9,450.00	72.36	180.16	9,261.14	-32.52	-496.40	79.52	11.00	10.97	-0.93
9,500.00	77.85	179.72	9,273.99	-80.83	-496.35	127.60	11.00	10.97	-0.88

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Planning Report

Weatherford

Database:	EDM 5000.1 Single User Db	**Local Co-ordinate Reference:**	Well TOMLIN 4-6-3-1WH
Company:	NEWFIELD EXPLORATION CO.	**TVD Reference:**	KB @ 5250.50ft (Original Well Elev)
Project:	DUCHESNE COUNTY, UT	**MD Reference:**	KB @ 5250.50ft (Original Well Elev)
Site:	TOMLIN 4-6-3-1WH	**North Reference:**	True
Well:	TOMLIN 4-6-3-1WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	TOMLIN 4-6-3-1WH		
Design:	PLAN 1		

Planned Survey

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100usft)	Build Rate (°/100usft)	Turn Rate (°/100usft)
9,550.00	83.33	179.30	9,282.16	-130.13	-495.93	176.64	11.00	10.97	-0.84
9,600.00	88.82	178.89	9,285.58	-179.99	-495.14	226.20	11.00	10.97	-0.82
Start 3948.63 hold at 9637.65 MD - 7" - LP - TOMLIN									
9,637.65	92.95	178.58	9,285.00	-217.62	-494.31	263.58	11.00	10.97	-0.82
9,700.00	92.95	178.58	9,281.79	-279.87	-492.77	325.40	0.00	0.00	0.00
9,800.00	92.95	178.58	9,276.65	-379.70	-490.30	424.55	0.00	0.00	0.00
9,900.00	92.95	178.58	9,271.51	-479.54	-487.84	523.70	0.00	0.00	0.00
10,000.00	92.95	178.58	9,266.37	-579.38	-485.37	622.86	0.00	0.00	0.00
10,100.00	92.95	178.58	9,261.23	-679.21	-482.90	722.01	0.00	0.00	0.00
10,200.00	92.95	178.58	9,256.09	-779.05	-480.43	821.16	0.00	0.00	0.00
10,300.00	92.95	178.58	9,250.95	-878.89	-477.97	920.31	0.00	0.00	0.00
10,400.00	92.95	178.58	9,245.81	-978.73	-475.50	1,019.46	0.00	0.00	0.00
10,500.00	92.95	178.58	9,240.67	-1,078.56	-473.03	1,118.61	0.00	0.00	0.00
10,600.00	92.95	178.58	9,235.53	-1,178.40	-470.56	1,217.77	0.00	0.00	0.00
10,700.00	92.95	178.58	9,230.38	-1,278.24	-468.09	1,316.92	0.00	0.00	0.00
10,800.00	92.95	178.58	9,225.24	-1,378.08	-465.63	1,416.07	0.00	0.00	0.00
10,900.00	92.95	178.58	9,220.10	-1,477.91	-463.16	1,515.22	0.00	0.00	0.00
11,000.00	92.95	178.58	9,214.96	-1,577.75	-460.69	1,614.37	0.00	0.00	0.00
11,100.00	92.95	178.58	9,209.82	-1,677.59	-458.22	1,713.52	0.00	0.00	0.00
11,200.00	92.95	178.58	9,204.68	-1,777.42	-455.76	1,812.68	0.00	0.00	0.00
11,300.00	92.95	178.58	9,199.54	-1,877.26	-453.29	1,911.83	0.00	0.00	0.00
11,400.00	92.95	178.58	9,194.40	-1,977.10	-450.82	2,010.98	0.00	0.00	0.00
11,500.00	92.95	178.58	9,189.26	-2,076.94	-448.35	2,110.13	0.00	0.00	0.00
11,600.00	92.95	178.58	9,184.12	-2,176.77	-445.89	2,209.28	0.00	0.00	0.00
11,700.00	92.95	178.58	9,178.97	-2,276.61	-443.42	2,308.43	0.00	0.00	0.00
11,800.00	92.95	178.58	9,173.83	-2,376.45	-440.95	2,407.59	0.00	0.00	0.00
11,900.00	92.95	178.58	9,168.69	-2,476.29	-438.48	2,506.74	0.00	0.00	0.00
12,000.00	92.95	178.58	9,163.55	-2,576.12	-436.01	2,605.89	0.00	0.00	0.00
12,100.00	92.95	178.58	9,158.41	-2,675.96	-433.55	2,705.04	0.00	0.00	0.00
12,200.00	92.95	178.58	9,153.27	-2,775.80	-431.08	2,804.19	0.00	0.00	0.00
12,300.00	92.95	178.58	9,148.13	-2,875.63	-428.61	2,903.34	0.00	0.00	0.00
12,400.00	92.95	178.58	9,142.99	-2,975.47	-426.14	3,002.49	0.00	0.00	0.00
12,500.00	92.95	178.58	9,137.85	-3,075.31	-423.68	3,101.65	0.00	0.00	0.00
12,600.00	92.95	178.58	9,132.70	-3,175.15	-421.21	3,200.80	0.00	0.00	0.00
12,700.00	92.95	178.58	9,127.56	-3,274.98	-418.74	3,299.95	0.00	0.00	0.00
12,800.00	92.95	178.58	9,122.42	-3,374.82	-416.27	3,399.10	0.00	0.00	0.00
12,900.00	92.95	178.58	9,117.28	-3,474.66	-413.81	3,498.25	0.00	0.00	0.00
13,000.00	92.95	178.58	9,112.14	-3,574.50	-411.34	3,597.40	0.00	0.00	0.00
13,100.00	92.95	178.58	9,107.00	-3,674.33	-408.87	3,696.56	0.00	0.00	0.00
13,200.00	92.95	178.58	9,101.86	-3,774.17	-406.40	3,795.71	0.00	0.00	0.00
13,300.00	92.95	178.58	9,096.72	-3,874.01	-403.93	3,894.86	0.00	0.00	0.00
13,400.00	92.95	178.58	9,091.58	-3,973.84	-401.47	3,994.01	0.00	0.00	0.00
13,500.00	92.95	178.58	9,086.44	-4,073.68	-399.00	4,093.16	0.00	0.00	0.00
TD at 13586.28 - PBHL - TOMLIN 4-6-3-1WH									
13,586.28	92.95	178.58	9,082.00	-4,159.82	-396.87	4,178.71	0.00	0.00	0.00

CONFIDENTIAL

RECEIVED: November 08, 2012

Weatherford

Weatherford International Ltd.

Planning Report

Weatherford

Database:	EDM 5000.1 Single User Db	**Local Co-ordinate Reference:**	Well TOMLIN 4-6-3-1WH
Company:	NEWFIELD EXPLORATION CO.	**TVD Reference:**	KB @ 5250.50ft (Original Well Elev)
Project:	DUCHESNE COUNTY, UT	**MD Reference:**	KB @ 5250.50ft (Original Well Elev)
Site:	TOMLIN 4-6-3-1WH	**North Reference:**	True
Well:	TOMLIN 4-6-3-1WH	**Survey Calculation Method:**	Minimum Curvature
Wellbore:	TOMLIN 4-6-3-1WH		
Design:	PLAN 1		

Design Targets

Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (ft)	+N/-S (ft)	+E/-W (ft)	Northing (usft)	Easting (usft)	Latitude	Longitude
PBHL - TOMLIN 4-6-3-1 - plan hits target center - Point	0.00	0.00	9,082.00	-4,159.82	-396.87	7,261,599.19	2,046,303.67	40° 14' 45.280 N	110° 2' 45.038 W
LP - TOMLIN - plan hits target center - Point	0.00	0.00	9,285.00	-217.62	-494.31	7,265,539.27	2,046,142.09	40° 15' 24.239 N	110° 2' 46.296 W

Casing Points

Measured Depth (ft)	Vertical Depth (ft)	Name	Casing Diameter (")	Hole Diameter (")
9,637.65	9,285.00	7"	7	8-3/4

Plan Annotations

Measured Depth (ft)	Vertical Depth (ft)	Local Coordinates +N/-S (ft)	+E/-W (ft)	Comment
2,500.00	2,500.00	0.00	0.00	Start Build 3.00
2,676.59	2,676.34	4.72	-6.65	Start 6087.35 hold at 2676.59 MD
8,763.94	8,737.69	330.05	-464.97	Start DLS 11.00 TFO -126.45
9,637.65	9,285.00	-217.62	-494.31	Start 3948.63 hold at 9637.65 MD
13,586.28	9,082.00	-4,159.82	-396.87	TD at 13586.28

CONFIDENTIAL

RECEIVED: November 08, 2012

AFFIDAVIT OF EASEMENT, RIGHT-OF-WAY AND SURFACE USE AGREEMENT

Peter Burns personally appeared before me, being duly sworn, deposes and with respect to State of Utah R649-3-34.7 says:

1. My name is Peter Burns. I am a Land Associate for Newfield Production Company, whose address is 1001 17th Street, Suite 2000, Denver, CO 80202 ("Newfield").

2. Newfield is the Operator of the proposed Tomlin 4-6-3-1WH well with a surface location to be positioned in the NWNW of Section 6, Township 3 South, Range 1 West (the "Drillsite Location"), and a bottom hole location to be positioned in the SWSW of Section 6, Township 3 South, Range 1 West, Duchesne County, Utah. The surface owner of the Drillsite Location is Farrer Family Partnership, whose address is P.O. Box 241, Orangeville, UT 84537 ("Surface Owner").

3. Newfield and the Surface Owner have agreed upon an Easement, Right-of-Way and Surface Use Agreement dated September 24, 2012 covering the Drillsite Location and access to the Drillsite Location.

FURTHER AFFIANT SAYETH NOT.

Peter Burns

CONFIDENTIAL

ACKNOWLEDGEMENT

STATE OF COLORADO §
§
COUNTY OF DENVER §

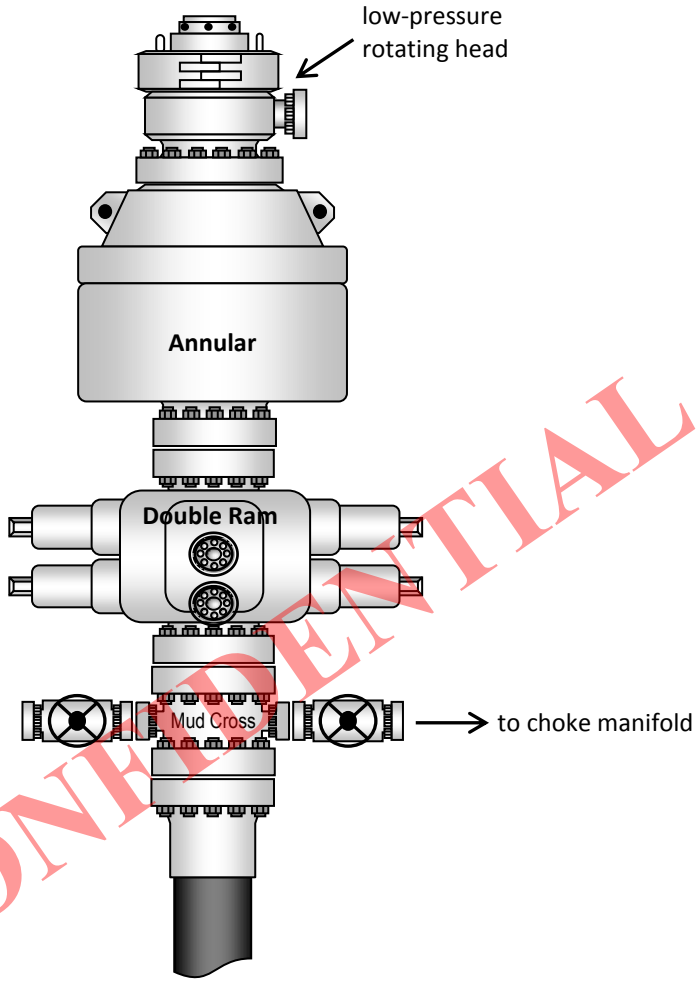
Before me, a Notary Public, in and for the State, on this 1st day of October, 2012, personally appeared Peter Burns, to me known to be the identical person who executed the foregoing instrument, and acknowledged to me that he executed the same as his own free and voluntary act and deed for the uses and purposes therein set forth.

NOTARY PUBLIC

My Commission Expires:

ALAN D. WILD NOTARY PUBLIC STATE OF COLORADO MY COMMISSION EXPIRES 2/17/2015

Typical 5M BOP stack configuration



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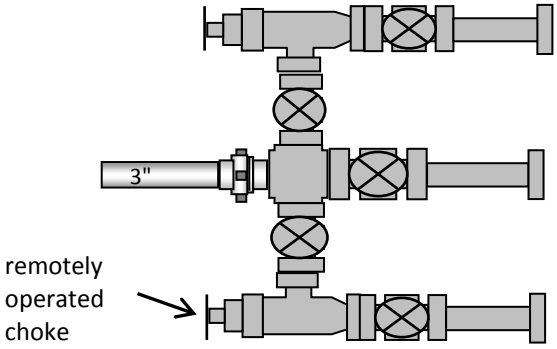
Typical 5M choke manifold configuration



RECEIVED: November 08, 2012

API Well Number: 43013518610000

NEWFIELD
ROCKY MOUNTAINS

October 3, 2012

State of Utah
Division of Oil, Gas & Mining
ATTN: Brad Hill
PO Box 145801
Salt Lake City, UT 84114

RE: Tomlin 4-6-3-1WH
T3S R1W Section 6
Duchesne County, Utah

CONFIDENTIAL

Dear Brad,

Newfield Production Company proposes to drill the Tomlin 4-6-3-1WH from a surface location of 453' FNL and 1161' FWL of Section 6, T3S R1W to a bottom hole location of 660' FSL and 660' FWL of Section 6, T3S R1W. Newfield shall case and cement the Tomlin 4-6-3-1WH wellbore from the surface location to the point where the wellbore reaches the legal setback of 660' FNL of Section 6, T3S R1W. The cased and cemented portion of the wellbore shall not be perforated nor produced. In the event a future recompletion into the cased and cemented portion of the wellbore is proposed, Newfield shall file the appropriate application with the State.

Newfield is the operator of the Emerald Phoenix 15-31-2-1W located in the northern offset drilling and spacing unit (Section 31, T2S R1W). Due to the above circumstances, Newfield respectfully requests that DOGM administratively grant an exception location for the Tomlin 4-6-3-1WH.

If you have any questions or require further information, please do not hesitate to contact the undersigned at 303-382-4444 or by email at reveland@newfield.com . Your consideration of this matter is greatly appreciated.

Sincerely,

Roxann Eveland

Roxann Eveland
Landman

1001 17th Street, Suite 2000 Denver, CO 80202 (303) 893-0102 Fax (303) 893-0103

NEWFIELD EXPLORATION COMPANY

WELL PAD INTERFERENCE PLAT

4-6-3-1WH (Proposed Well)

Pad Location: NWNW (Lot 4) Section 6, T3S, R1W, U.S.B.&M.

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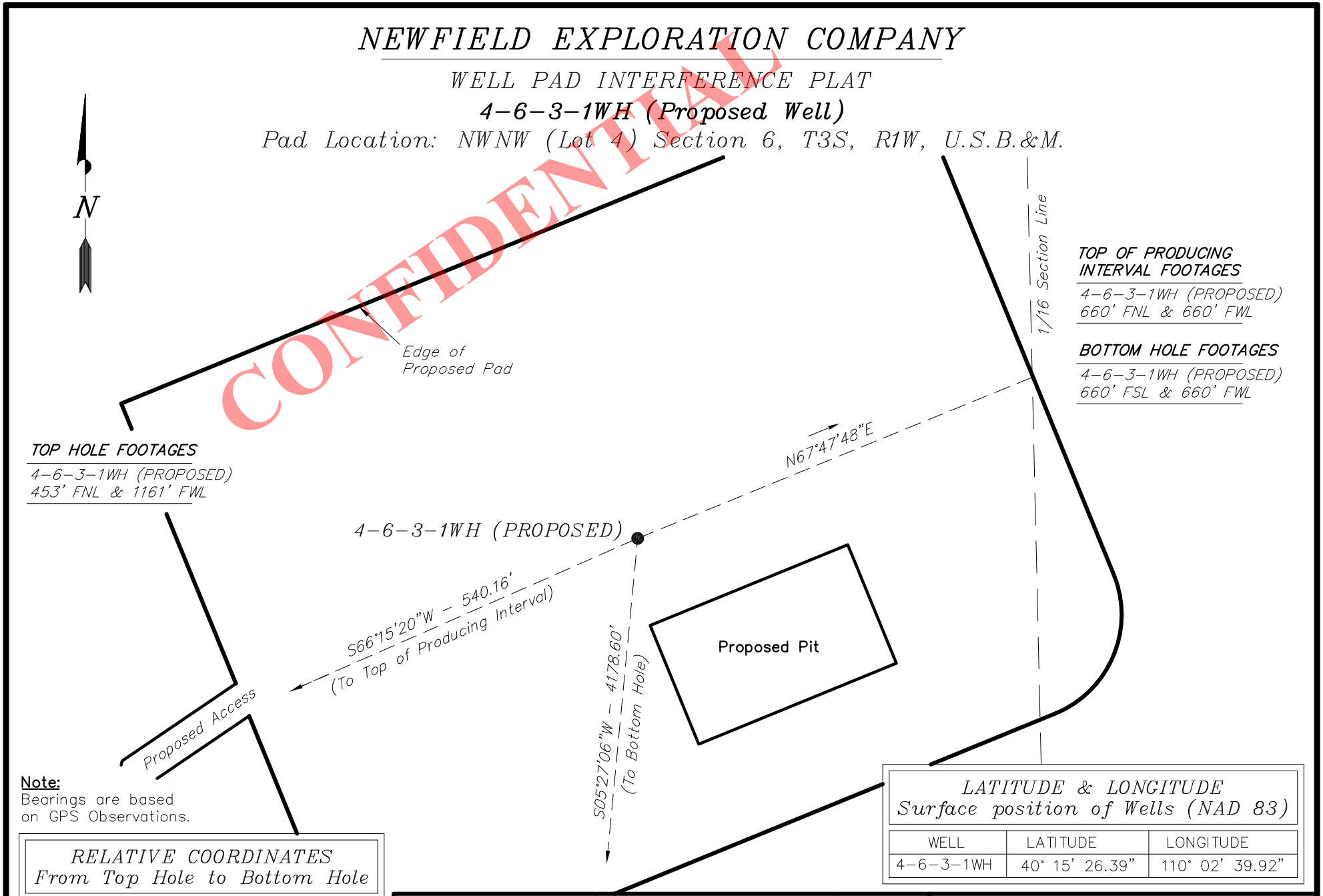


Note:
Bearings are based on GPS Observations.

RELATIVE COORDINATES
From Top Hole to Bottom Hole

WELL	NORTH	EAST
4-6-3-1WH	-4,160'	-397'

LATITUDE & LONGITUDE
Surface position of Wells (NAD 83)

WELL	LATITUDE	LONGITUDE
4-6-3-1WH	40° 15' 26.39"	110° 02' 39.92"

SURVEYED BY: P.H.	DATE SURVEYED: 02-20-12	VERSION:	Tri State Land Surveying, Inc. (435) 781-2501
DRAWN BY: R.B.T.	DATE DRAWN: 03-01-12	V1	180 NORTH VERNAL AVE. VERNAL, UTAH 84078
SCALE: 1" = 60'	REVISED:		

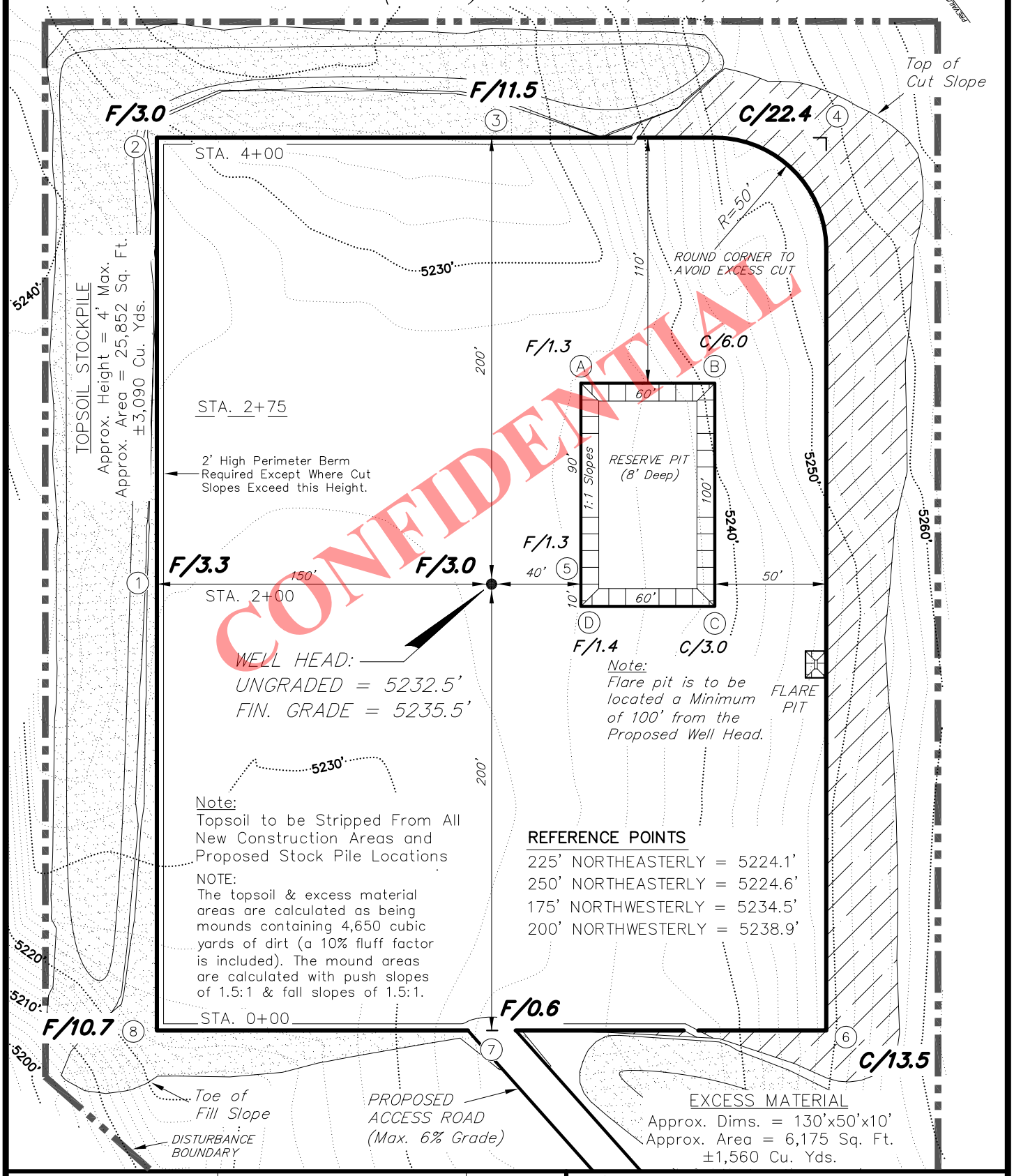
RECEIVED: November 08, 2012

NEWFIELD EXPLORATION COMPANY

PROPOSED LOCATION LAYOUT

4-6-3-1WH

Pad Location: NWNW (Lot 4) Section 6, T3S, R1W, U.S.B.&M.



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SURVEYED BY: P.H.	DATE SURVEYED: 02-20-12	VERSION:	Tri State Land Surveying, Inc. (435) 781-2501
DRAWN BY: R.B.T.	DATE DRAWN: 03-13-12	V1	180 NORTH VERNAL AVE. VERNAL, UTAH 84078
SCALE: 1" = 60'	REVISED:		

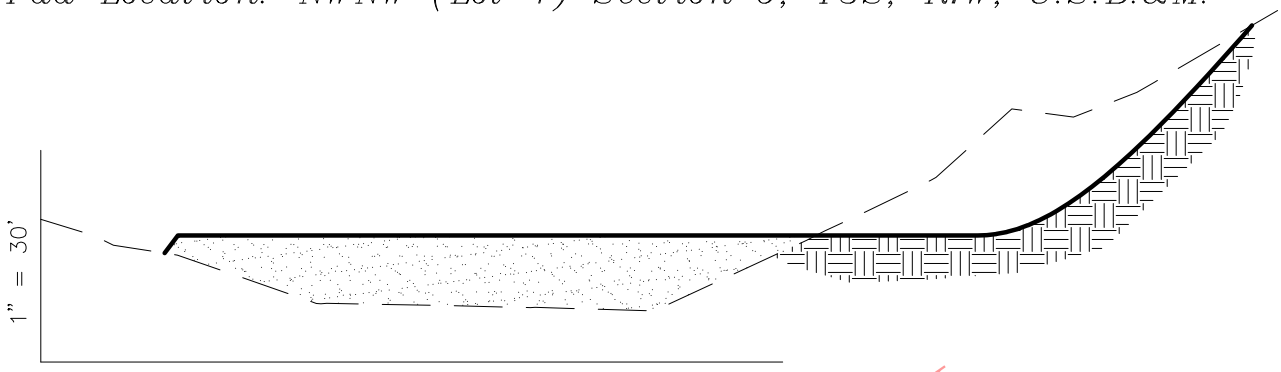
RECEIVED: November 08, 2012

NEWFIELD EXPLORATION COMPANY

CROSS SECTIONS

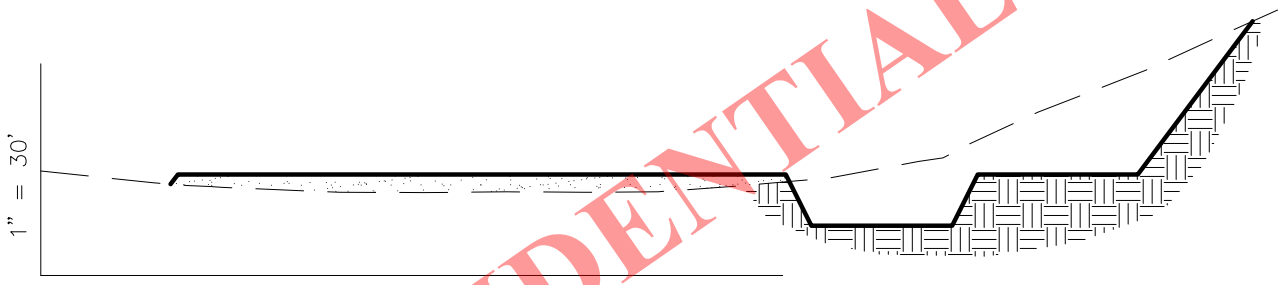
4-6-3-1WH

Pad Location: NWNW (Lot 4) Section 6, T3S, R1W, U.S.B.&M.



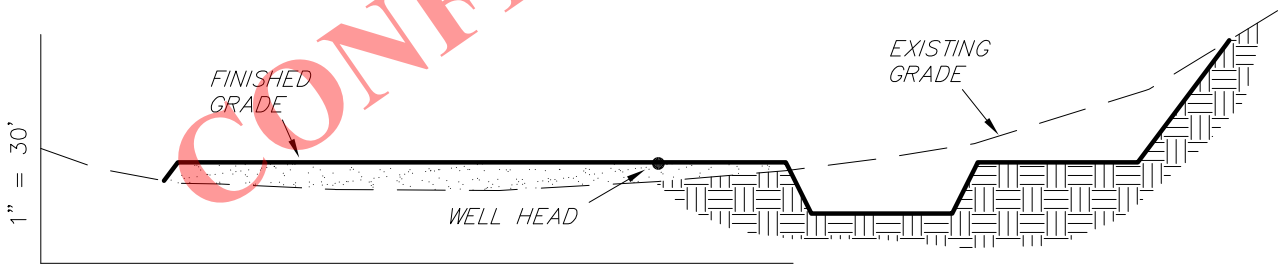
1" = 60'

STA. 4+00



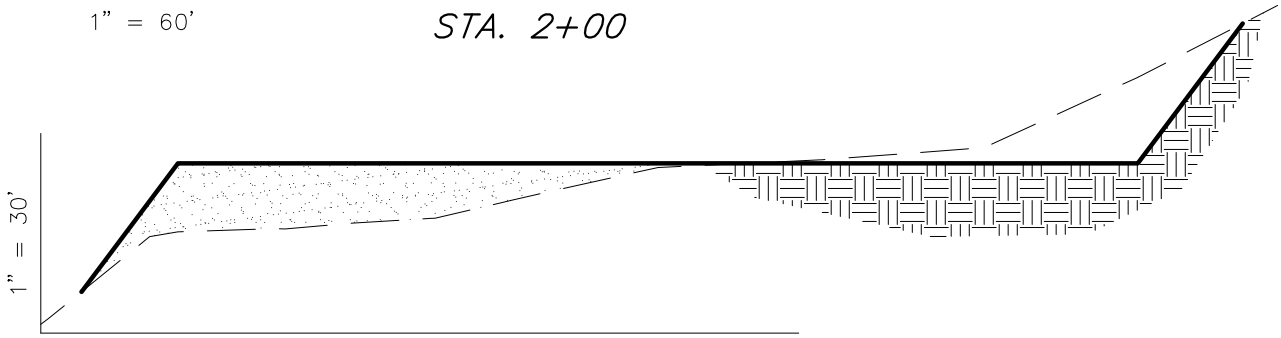
1" = 60'

STA. 2+75



1" = 60'

STA. 2+00



1" = 60'

STA. 0+00

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NOTE:
UNLESS OTHERWISE NOTED ALL CUT/FILL SLOPES ARE AT 1.5:1

ESTIMATED EARTHWORK QUANTITIES
(No Shrink or swell adjustments have been used)
(Expressed in Cubic Yards)

ITEM	CUT	FILL	6" TOPSOIL	EXCESS
PAD	13,630	13,630	Topsoil is not included in Pad Cut Volume	0
PIT	1,420	0		1,420
TOTALS	15,050	13,630	2,810	1,420

SURVEYED BY: P.H.	DATE SURVEYED: 02-20-12	VERSION:	Tri State Land Surveying, Inc. (435) 781-2501
DRAWN BY: R.B.T.	DATE DRAWN: 03-13-12	V1	180 NORTH VERNAL AVE. VERNAL, UTAH 84078
SCALE: 1" = 60'	REVISED:		

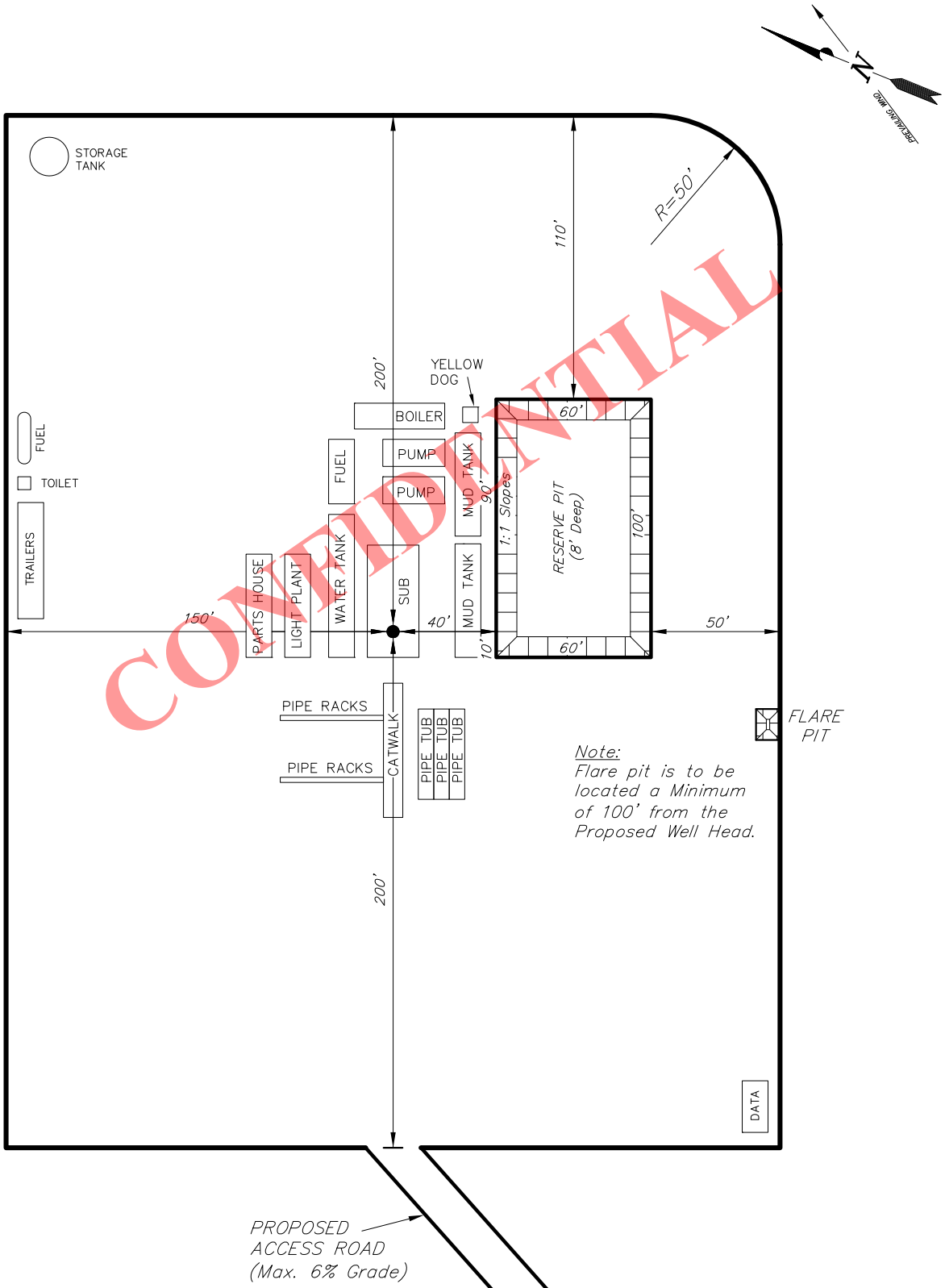
RECEIVED: November 08, 2012

NEWFIELD EXPLORATION COMPANY

TYPICAL RIG LAYOUT

4-6-3-1WH

Pad Location: NWNW (Lot 4) Section 6, T3S, R1W, U.S.B.&M.



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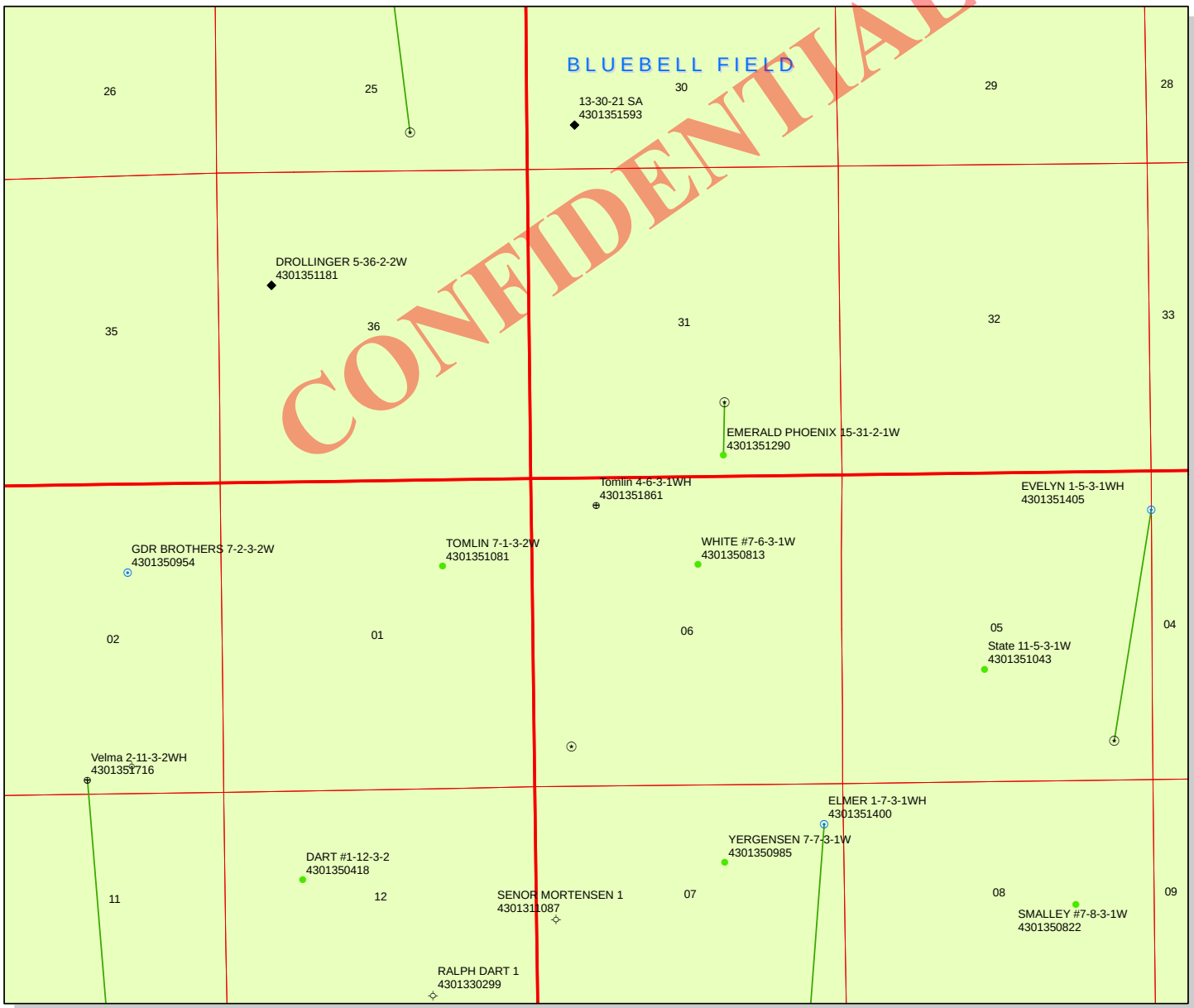
SURVEYED BY: P.H.	DATE SURVEYED: 02-20-12	VERSION:	Tri State Land Surveying, Inc. (435) 781-2501
DRAWN BY: R.B.T.	DATE DRAWN: 03-13-12	V1	180 NORTH VERNAL AVE. VERNAL, UTAH 84078
SCALE: 1" = 60'	REVISED:		

RECEIVED: November 08, 2012

API Well Number: 43013518610000



API Number: 4301351861

Well Name: Tomlin 4-6-3-1WH

Township T03.0S Range R01.0W Section 06

Meridian: UBM

Operator: NEWFIELD PRODUCTION COMPANY

Map Prepared:
Map Produced by Diana Mason

Units
STATUS
ACTIVE
EXPLORATORY
GAS STORAGE
NF PP OIL
NF SECONDARY
PI OIL
PP GAS
PP GEOTHERML
PP OIL
SECONDARY
TERMINATED

Fields
STATUS
Unknown
ABANDONED
ACTIVE
COMBINED
INACTIVE
STORAGE
TERMINATED

Wells Query
Status
APD - Aproved Permit
DRL - Spuded (Drilling Commenced)
GIW - Gas Injection
GS - Gas Storage
LOC - New Location
OPS - Operation Suspended
PA - Plugged Abandoned
PGW - Producing Gas Well
POW - Producing Oil Well
SGW - Shut-in Gas Well
SOW - Shut-in Oil Well
TA - Temp. Abandoned
TW - Test Well
WDW - Water Disposal
WIW - Water Injection Well
WSW - Water Supply Well
Bottom Hole Location - OilGasDb

2,200 1,100 0 2,200 Feet

1:21,059

RECEIVED: November 09, 2012

API Well Number: 43013518610000

BOPE REVIEW NEWFIELD PRODUCTION COMPANY Tomlin 4-6-3-1WH 43013518610000

Well Name	NEWFIELD PRODUCTION COMPANY Tomlin 4-6-3-1WH 4301351861			
String	Cond	Surf	I1	Prod
Casing Size(")	14.000	9.625	7.000	4.500
Setting Depth (TVD)	60	2500	9285	9082
Previous Shoe Setting Depth (TVD)	0	60	2500	9285
Max Mud Weight (ppg)	8.3	8.3	10.5	10.5
BOPE Proposed (psi)	0	500	5000	5000
Casing Internal Yield (psi)	1000	3520	9950	12410
Operators Max Anticipated Pressure (psi)	4723			10.0

Calculations	Cond String	14.000	"
Max BHP (psi)	.052*Setting Depth*MW=	26	
			BOPE Adequate For Drilling And Setting Casing at Depth?
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	19	NO
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	13	NO
			*Can Full Expected Pressure Be Held At Previous Shoe?
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	13	NO
Required Casing/BOPE Test Pressure=		60	psi
*Max Pressure Allowed @ Previous Casing Shoe=		0	psi *Assumes 1psi/ft frac gradient

Calculations	Surf String	9.625	"
Max BHP (psi)	.052*Setting Depth*MW=	1079	
			BOPE Adequate For Drilling And Setting Casing at Depth?
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	779	NO diverter
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	529	NO Reasonable depth in area
			*Can Full Expected Pressure Be Held At Previous Shoe?
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	542	NO
Required Casing/BOPE Test Pressure=		2464	psi
*Max Pressure Allowed @ Previous Casing Shoe=		60	psi *Assumes 1psi/ft frac gradient

Calculations	I1 String	7.000	"
Max BHP (psi)	.052*Setting Depth*MW=	5070	
			BOPE Adequate For Drilling And Setting Casing at Depth?
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	3956	YES
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	3027	YES OK
			*Can Full Expected Pressure Be Held At Previous Shoe?
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	3577	NO OK
Required Casing/BOPE Test Pressure=		5000	psi
*Max Pressure Allowed @ Previous Casing Shoe=		2500	psi *Assumes 1psi/ft frac gradient

Calculations	Prod String	4.500	"
Max BHP (psi)	.052*Setting Depth*MW=	4959	
			BOPE Adequate For Drilling And Setting Casing at Depth?
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	3869	YES
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	2961	YES OK
			*Can Full Expected Pressure Be Held At Previous Shoe?
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	5004	YES
Required Casing/BOPE Test Pressure=		5000	psi
*Max Pressure Allowed @ Previous Casing Shoe=		9285	psi *Assumes 1psi/ft frac gradient

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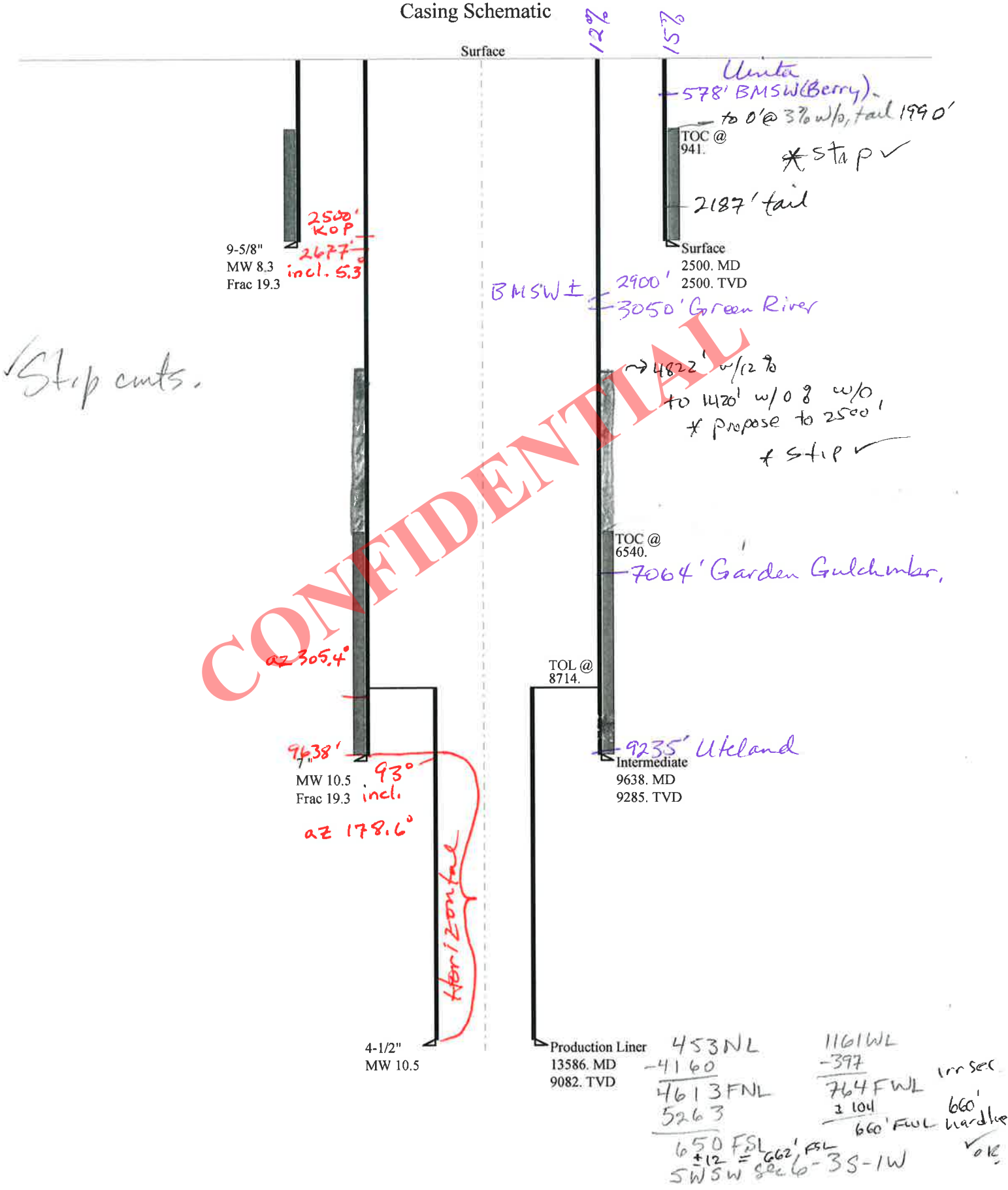
RECEIVED: December 11, 2012

API Well Number: 43013518610000

43013518610000 Tomlin 4-6-3-1WH

Casing Schematic



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API Well Number: 43013518610000

Well name:	**43013518610000 Tomlin 4-6-3-1WH**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Surface
Project ID:	43-013-51861
Location:	DUCHESNE COUNTY

Design parameters:

Collapse

Mud weight: 8.330 ppg

Design is based on evacuated pipe.

Burst

Max anticipated surface pressure: 1,950 psi

Internal gradient: 0.220 psi/ft

Calculated BHP 2,500 psi

No backup mud specified.

Minimum design factors:

Collapse:

Design factor 1.125

Burst:

Design factor 1.00

Tension:

8 Round STC: 1.80 (J)

8 Round LTC: 1.70 (J)

Buttress: 1.60 (J)

Premium: 1.50 (J)

Body yield: 1.50 (B)

Tension is based on air weight.

Neutral point: 2,191 ft

Environment:

H2S considered? No

Surface temperature: 74 °F

Bottom hole temperature: 109 °F

Temperature gradient: 1.40 °F/100ft

Minimum section length: 100 ft

Cement top: 940 ft

Non-directional string.

Re subsequent strings:

Next setting depth: 9,285 ft

Next mud weight: 10.500 ppg

Next setting BHP: 5,065 psi

Fracture mud wt: 19.250 ppg

Fracture depth: 2,500 ft

Injection pressure: 2,500 psi

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	2499	9.625	36.00	J-55	LT&C	2499	2499	8.796	20439

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	1082	2020	1.868	2500	3520	1.41	90	453	5.03 J

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940

Date: December 5,2012
Salt Lake City, Utah

Remarks:

Collapse is based on a vertical depth of 2499 ft, a mud weight of 8.33 ppg The casing is considered to be evacuated for collapse purposes.
Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Engineering responsibility for use of this design will be that of the purchaser.

CONFIDENTIAL

API Well Number: 43013518610000

Well name:	**43013518610000 Tomlin 4-6-3-1WH**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Intermediate
Project ID:	43-013-51861
Location:	DUCHESNE COUNTY

Design parameters:

Collapse

Mud weight: 10.500 ppg

Design is based on evacuated pipe.

Burst

Max anticipated surface pressure: 3,022 psi

Internal gradient: 0.220 psi/ft

Calculated BHP 5,065 psi

No backup mud specified.

Minimum design factors:

Collapse:

Design factor 1.125

Burst:

Design factor 1.00

Tension:

8 Round STC: 1.80 (J)

8 Round LTC: 1.80 (J)

Buttress: 1.60 (J)

Premium: 1.50 (J)

Body yield: 1.60 (B)

Tension is based on air weight.

Neutral point: 7,837 ft

Environment:

H2S considered? No

Surface temperature: 74 °F

Bottom hole temperature: 204 °F

Temperature gradient: 1.40 °F/100ft

Minimum section length: 1,000 ft

Cement top: 6,540 ft

Directional well information:

Kick-off point 2500 ft

Departure at shoe: 540 ft

Maximum dogleg: 11 °/100ft

Inclination at shoe: 92.95 °

Re subsequent strings:

Next setting depth: 9,285 ft

Next mud weight: 10.500 ppg

Next setting BHP: 5,065 psi

Fracture mud wt: 19.250 ppg

Fracture depth: 9,285 ft

Injection pressure: 9,285 psi

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Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	9638	7	26.00	P-110	Buttress	9285	9638	6.151	107184

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	5065	6230	1.230	5065	9950	1.96	241.4	830.4	3.44 B

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940

Date: December 5,2012
Salt Lake City, Utah

Remarks:

Collapse is based on a vertical depth of 9285 ft, a mud weight of 10.5 ppg The casing is considered to be evacuated for collapse purposes.
Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.
Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

API Well Number: 43013518610000

Well name:	**43013518610000 Tomlin 4-6-3-1WH**
Operator:	**NEWFIELD PRODUCTION COMPANY**
String type:	Production Liner
Project ID:	43-013-51861
Location:	DUCHESNE COUNTY

Design parameters:

Collapse

Mud weight: 10.500 ppg

Design is based on evacuated pipe.

Burst

Max anticipated surface pressure: 2,956 psi

Internal gradient: 0.220 psi/ft

Calculated BHP 4,954 psi

No backup mud specified.

Minimum design factors:

Collapse:

Design factor 1.125

Burst:

Design factor 1.00

Tension:

8 Round STC: 1.80 (J)

8 Round LTC: 1.80 (J)

Buttress: 1.60 (J)

Premium: 1.50 (J)

Body yield: 1.60 (B)

Tension is based on air weight.

Neutral point: 9,068 ft

Environment:

H2S considered? No

Surface temperature: 74 °F

Bottom hole temperature: 201 °F

Temperature gradient: 1.40 °F/100ft

Minimum section length: 1,000 ft

Liner top: 8,714 ft

Directional well information:

Kick-off point 2500 ft

Departure at shoe: 4178 ft

Maximum dogleg: 11 °/100ft

Inclination at shoe: 92.95 °

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Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost ($)
1	4886	4.5	13.50	P-110	Buttress	9082	13586	3.795	29313

Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	4954	10680	2.156	4998	12410	2.48	5.5	421.9	76.64 B

Prepared by: Helen Sadik-Macdonald
Div of Oil,Gas & Mining
Phone: 801 538-5357
FAX: 801-359-3940

Date: December 5,2012
Salt Lake City, Utah

Remarks:

For this liner string, the top is rounded to the nearest 100 ft.Collapse is based on a vertical depth of 9082 ft, a mud weight of 10.5 ppg The Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

ON-SITE PREDRILL EVALUATION
Utah Division of Oil, Gas and Mining

Operator NEWFIELD PRODUCTION COMPANY
Well Name Tomlin 4-6-3-1WH
API Number 43013518610000 **APD No** 7113 **Field/Unit** WILDCAT
Location: 1/4,1/4 NWNW **Sec** 6 **Tw** 3.0S **Rng** 1.0W 453 FNL 1161 FWL
GPS Coord (UTM) 581260 4456762 **Surface Owner** Farrer Family Partnership

Participants

Tim Eaton, Forrest Bird, Zander McIntyre - Newfield; Jim Thayne, Bill Farrer - Landowners

Regional/Local Setting & Topography

The location is on a hillside immediately south of Hwy 40 and adjacent Cobble Hollow. The immediate area is deeply incised hillside comprised of large cobbles to gravels with a portion of soils. It appears that this plot of land may have historically used as a gravel pit as multiple man made topographic features dominate the landscape. There are substantial portions of the hillsides, within the footprint of the pad and hillsides immediately adjacent and below, that have experienced quite recent sluffing and other slope stability problems as evidenced by lack of vegetation within the scars. Regionally, the area is shared by farms and the majority of industrial areas for the city of Roosevelt. There are a few wells in the immediate vicintiy that have been drilled recently and continued development is expected.

CONFIDENTIAL

Surface Use Plan

Current Surface Use
Industrial
Recreational

New Road Miles	Well Pad	Src Const Material	Surface Formation
0.85	**Width** 300 **Length** 400	Onsite	UNTA

Ancillary Facilities N

Waste Management Plan Adequate? Y

Environmental Parameters

Affected Floodplains and/or Wetlands N

Flora / Fauna

High desert shrubland ecosystem. Expected vegetation consists of black sagebrush, shadscale, Atriplex spp., mustard spp, rabbit brush, horsebrush, broom snakeweed, Opuntia spp and spring annuals.
Dominant vegetation;
Galletta, Ephedra and opuntia spp. Surround the proposed site.
Wildlife;
Adjacent habitat contains forbs that may be suitable browse for deer, antelope, prairie dogs or rabbits, though none were observed. Disturbed soils onsite do not support habitat for wildlife.

Soil Type and Characteristics

RECEIVED: December 11, 2012

very gravelly loams with cobbles

Erosion Issues Y
hill side has experienced mass wasting in recent past

Sedimentation Issues Y
erodible soils and gravels

Site Stability Issues Y
slopes and unstable soils are present under pad footprint

Drainage Diverson Required? N

Berm Required? Y

Erosion Sedimentation Control Required? Y
steps to be taken to stabilize or remove hillside where wasting has occurred

Paleo Survey Run? **Paleo Potental Observed?** N **Cultural Survey Run?** **Cultural Resources?** N

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Reserve Pit

Site-Specific Factors		Site Ranking
Distance to Groundwater (feet)	100 to 200	5
Distance to Surface Water (feet)	200 to 300	10
Dist. Nearest Municipal Well (ft)	>5280	0
Distance to Other Wells (feet)	>1320	0
Native Soil Type	High permeability	20
Fluid Type	Fresh Water	5
Drill Cuttings	Normal Rock	0
Annual Precipitation (inches)	10 to 20	5
Affected Populations		
Presence Nearby Utility Conduits	Present	15
	Final Score	60 1 Sensitivity Level

Characteristics / Requirements
A 60’ x 100' x 8' deep reserve pit is planned in an area of cut on the northwest side of the location. A pit liner is required. Newfield commonly uses a 30 mil liner with a felt underliner. Pit should be fenced to prevent entry by deer, other wildlife and domestic animals. Pit to be closed within one year after drilling activities are complete.

Closed Loop Mud Required? N **Liner Required?** Y **Liner Thickness** 16 **Pit Underlayment Required?** Y

Other Observations / Comments

Chris Jensen
Evaluator

11/14/2012
Date / Time

RECEIVED: December 11, 2012

Application for Permit to Drill
Statement of Basis
Utah Division of Oil, Gas and Mining

APD No	API WellNo	Status	Well Type	Surf Owner	CBM
7113	43013518610000	LOCKED	OW	P	No

Operator	NEWFIELD PRODUCTION COMPANY	**Surface Owner-APD**	Farrer Family Partnership
Well Name	Tomlin 4-6-3-1WH	**Unit**	
Field	WILDCAT	**Type of Work**	DRILL
Location	NWNW 6 3S 1W U 453 FNL 1161 FWL GPS Coord (UTM) 581260E 4456757N		

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Geologic Statement of Basis

Newfield proposes to set 60' of conductor and 2,500' of surface casing at this location. The base of the moderately saline water at this location is estimated to be at a depth of 2,900'. A search of Division of Water Rights records shows 15 water wells within a 10,000 foot radius of the center of Section 6. Three wells are located within 1/2 mile of the proposed location. Depth is listed for 2 of these wells as 32 and 225 feet. Depth for all wells is listed as ranging from 32 to 800 feet. Average depth is approximately 150 feet. Water use is listed as irrigation, stock watering, industrial and domestic use. The surface formation at this site is the Uinta Formation. The Uinta Formation is made up of interbedded shales and sandstones. The sandstones are mostly lenticular and discontinuous and should not be a significant source of useable ground water. Intermediate casing cement should be brought up to or above the base of the moderately saline ground water in order to isolate it from fresher waters uphole.

Brad Hill	11/26/2012
APD Evaluator	**Date / Time**

Surface Statement of Basis

Location is proposed in a good location although outside the spacing window which is typical for a horizontal well. Access road enters the pad from the West. The landowner and its representative was in attendance for the pre-site inspection.
The soil type and topography at present do combine to pose a significant threat to erosion or sediment/ pollution transport in these regional climate conditions as evidenced by mass wasting of the hillside.
Construction standards of the Operator do not appear to be adequate for the proposed purpose as submitted. Plans lack measures for importing materials, using a geogrid or compacting native soils to improve stability. Operator has no plans for protection of slopes. Corner A of the reserve pit is planned in 5 feet of fill. For this reason I have asked for a felt subliner. Onsite conversations considered terrracing of the hillside above and "keying" in the slopes between 8 and 2 to correct stability. Plots to be submitted as a sundry detailing plans for the terracing or other measures to correct location problems.
I recognize no special flora or animal species or cultural resources on site that the proposed action may harm. A riparian area can be found adjacent the site below and to the East. The location was previously surveyed for cultural and paleontological resources as the operator saw fit. I have advised an informal ESA consultation to be initiated to insure no disturbance to TES species that may have not been seen during onsite visit.
The location should be bermed to prevent spills from leaving the confines of the pad.

RECEIVED: December 11, 2012

Fencing around the reserve pit will be necessary once the well is drilled to prevent wildlife and livestock from entering. A synthetic liner of 30 mils (minimum) should be utilized in the reserve pit. Measures (BMP's) shall be taken to protect steep slopes and topsoil pile from erosion to steep slopes North, as well as sedimentation and stability issues.

Chris Jensen	11/14/2012
Onsite Evaluator	**Date / Time**

Conditions of Approval / Application for Permit to Drill

Category	Condition
Pits	A synthetic liner with a minimum thickness of 16 mils with a felt subliner shall be properly installed and maintained in the reserve pit.
Surface	Hillside is to be stabilized or removed to prevent further wasting (sluffing) and loss of material or pad to drainage to the east or other slopes below (north)
Surface	The well site shall be bermed to prevent fluids from leaving the pad.
Surface	The reserve pit shall be fenced upon completion of drilling operations.

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RECEIVED: December 11, 2012

WORKSHEET
APPLICATION FOR PERMIT TO DRILL

APD RECEIVED: 11/8/2012
API NO. ASSIGNED: 43013518610000
WELL NAME: Tomlin 4-6-3-1WH
OPERATOR: NEWFIELD PRODUCTION COMPANY (N2695)
PHONE NUMBER: 435 719-2018
CONTACT: Don Hamilton

PROPOSED LOCATION: NWNW 06 030S 010W
Permit Tech Review: ✔

SURFACE: 0453 FNL 1161 FWL
Engineering Review: ✔

BOTTOM: 0660 FSL 0660 FWL
Geology Review: ✔

COUNTY: DUCHESNE
LATITUDE: 40.25733
LONGITUDE: -110.04443
UTM SURF EASTINGS: 581260.00
NORTHINGS: 4456757.00
FIELD NAME: WILDCAT
LEASE TYPE: 4 - Fee
LEASE NUMBER: Patented
PROPOSED PRODUCING FORMATION(S): GREEN RIVER
SURFACE OWNER: 4 - Fee
COALBED METHANE: NO

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RECEIVED AND/OR REVIEWED:

- ✔ **PLAT**
- ✔ **Bond:** STATE/FEE - B001834
- ☐ **Potash**
- ☐ **Oil Shale 190-5**
- ☐ **Oil Shale 190-3**
- ☐ **Oil Shale 190-13**
- ✔ **Water Permit:** 437478
- ☐ **RDCC Review:**
- ✔ **Fee Surface Agreement**
- ☐ **Intent to Commingle**

Commingling Approved

LOCATION AND SITING:

- ☐ **R649-2-3.**

Unit:

- ☐ **R649-3-2. General**
- ✔ **R649-3-3. Exception**
- ✔ **Drilling Unit**

Board Cause No: Cause 139-90
Effective Date: 5/9/2012
Siting: 4 Prod LGRRV-WSTC Wells

- ☐ **R649-3-11. Directional Drill**

Comments: Presite Completed

Stipulations:
1 - Exception Location - bhill
5 - Statement of Basis - bhill
12 - Cement Volume (3) - hmacdonald
25 - Surface Casing - hmacdonald
27 - Other - bhill

RECEIVED: December 11, 2012

GARY R. HERBERT
Governor

GREGORY S. BELL
Lieutenant Governor

State of Utah

DEPARTMENT OF NATURAL RESOURCES

MICHAEL R. STYLER
Executive Director

Division of Oil, Gas and Mining

JOHN R. BAZA
Division Director

Permit To Drill

****

Well Name: Tomlin 4-6-3-1WH
API Well Number: 43013518610000
Lease Number: Patented
Surface Owner: FEE (PRIVATE)
Approval Date: 12/11/2012

Issued to:
NEWFIELD PRODUCTION COMPANY , Rt 3 Box 3630 , Myton, UT 84052

Authority:
Pursuant to Utah Code Ann. 40-6-1 et seq., and Utah Administrative Code R649-3-1 et seq., the Utah Division of Oil, Gas and Mining issues conditions of approval, and permit to drill the listed well. This permit is issued in accordance with the requirements of Cause 139-90. The expected producing formation or pool is the GREEN RIVER Formation(s), completion into any other zones will require filing a Sundry Notice (Form 9). Completion and commingling of more than one pool will require approval in accordance with R649-3-22.

Duration:
This approval shall expire one year from the above date unless substantial and continuous operation is underway, or a request for extension is made prior to the expiration date

Exception Location:
Appropriate information has been submitted to DOGM and administrative approval of the requested exception location is hereby granted.

General:
Compliance with the requirements of Utah Admin. R. 649-1 et seq., the Oil and Gas Conservation General Rules, and the applicable terms and provisions of the approved Application for permit to drill.

Conditions of Approval:
Compliance with the Conditions of Approval/Application for Permit to Drill outlined in the Statement of Basis (copy attached).

In accordance with Utah Admin. R.649-3-21, the operator shall submit a complete angular deviation and directional survey report to the Division within 30 days following completion of the well.

Cement volume for the 7" interemediate string shall be determined from actual hole diameter in order to place cement from the pipe setting depth back to 2300' MD as indicated in the submitted drilling plan.

Surface casing shall be cemented to the surface.

Additional Approvals:
The operator is required to obtain approval from the Division of Oil, Gas and mining before performing any of the following actions during the drilling of this well:

- Any changes to the approved drilling plan - contact Dustin Doucet
- Significant plug back of the well - contact Dustin Doucet
- Plug and abandonment of the well - contact Dustin Doucet

Notification Requirements:
The operator is required to notify the Division of Oil, Gas and Mining of the following actions during drilling of this well:

- Within 24 hours following the spudding of the well - contact Carol Daniels OR submit an electronic sundry notice (pre-registration required) via the Utah Oil & Gas website at http://oilgas.ogm.utah.gov
- 24 hours prior to testing blowout prevention equipment - contact Dan Jarvis
- 24 hours prior to cementing or testing casing - contact Dan Jarvis
- Within 24 hours of making any emergency changes to the approved drilling program - contact Dustin Doucet
- 24 hours prior to commencing operations to plug and abandon the well - contact Dan Jarvis

Contact Information:
The following are Division of Oil, Gas and Mining contacts and their telephone numbers (please leave a voicemail message if the person is not available to take the call):

- Carol Daniels 801-538-5284 - office
- Dustin Doucet 801-538-5281 - office
  801-733-0983 - after office hours
- Dan Jarvis 801-538-5338 - office
  801-231-8956 - after office hours

Reporting Requirements:
All reports, forms and submittals as required by the Utah Oil and Gas Conservation General Rules will be promptly filed with the Division of Oil, Gas and Mining, including but not limited to:

- Entity Action Form (Form 6) - due within 5 days of spudding the well
- Monthly Status Report (Form 9) - due by 5th day of the following calendar month
- Requests to Change Plans (Form 9) - due prior to implementation
- Written Notice of Emergency Changes (Form 9) - due within 5 days
- Notice of Operations Suspension or Resumption (Form 9) - due prior to implementation
- Report of Water Encountered (Form 7) - due within 30 days after completion
- Well Completion Report (Form 8) - due within 30 days after completion or plugging

Approved By:

Approved By:

For John Rogers
Associate Director, Oil & Gas

CONFIDENTIAL

BLM - Vernal Field Office - Notification Form

Operator Newfield Exploration Rig Name/# Ross 31 Submitted By Branden Arnold Phone Number 435-401-0223
Well Name/Number Tomlin 4-6-3-1WH
Qtr/Qtr NW/NW Section 6 Township 3S Range 1W
Lease Serial Number Patented
API Number 43-013-51861

Spud Notice – Spud is the initial spudding of the well, not drilling out below a casing string.

Date/Time 1/15/13 9:00 AM ☒ PM ☐

Casing – Please report time casing run starts, not cementing times.

☒ Surface Casing
☐ Intermediate Casing
☐ Production Casing
☐ Liner
☐ Other

Date/Time 1/15/13 5:00 AM ☐ PM ☒

BOPE

☐ Initial BOPE test at surface casing point
☐ BOPE test at intermediate casing point
☐ 30 day BOPE test
☐ Other

Date/Time _____ _____ AM ☐ PM ☐

Remarks _____

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS, AND MINING

FORM 9

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

5.LEASE DESIGNATION AND SERIAL NUMBER: Patented

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

7.UNIT or CA AGREEMENT NAME:

1. TYPE OF WELL Oil Well

8. WELL NAME and NUMBER: Tomlin 4-6-3-1WH

2. NAME OF OPERATOR: NEWFIELD PRODUCTION COMPANY

9. API NUMBER: 43013518610000

3. ADDRESS OF OPERATOR: Rt 3 Box 3630 , Myton, UT, 84052

PHONE NUMBER: 435 646-4825 Ext

9. FIELD and POOL or WILDCAT: WILDCAT

4. LOCATION OF WELL
FOOTAGES AT SURFACE: 0453 FNL 1161 FWL
QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: Qtr/Qtr: NWNW Section: 06 Township: 03.0S Range: 01.0W Meridian: U

COUNTY: DUCHESNE

STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

TYPE OF SUBMISSION

- ✓ NOTICE OF INTENT — Approximate date work will start: 2/15/2013
- ☐ SUBSEQUENT REPORT — Date of Work Completion:
- ☐ SPUD REPORT — Date of Spud:
- ☐ DRILLING REPORT — Report Date:

TYPE OF ACTION

☐ ACIDIZE	☐ ALTER CASING	☐ CASING REPAIR
✓ CHANGE TO PREVIOUS PLANS	☐ CHANGE TUBING	☐ CHANGE WELL NAME
☐ CHANGE WELL STATUS	☐ COMMINGLE PRODUCING FORMATIONS	☐ CONVERT WELL TYPE
☐ DEEPEN	☐ FRACTURE TREAT	☐ NEW CONSTRUCTION
☐ OPERATOR CHANGE	☐ PLUG AND ABANDON	☐ PLUG BACK
☐ PRODUCTION START OR RESUME	☐ RECLAMATION OF WELL SITE	☐ RECOMPLETE DIFFERENT FORMATION
☐ REPERFORATE CURRENT FORMATION	☐ SIDETRACK TO REPAIR WELL	☐ TEMPORARY ABANDON
☐ TUBING REPAIR	☐ VENT OR FLARE	☐ WATER DISPOSAL
☐ WATER SHUTOFF	☐ SI TA STATUS EXTENSION	☐ APD EXTENSION
☐ WILDCAT WELL DETERMINATION	☐ OTHER	OTHER:

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

Newfield Production Company respectfully requests approval to install a swellable packer on the 4.5" liner at the heel of this well during the pending completion process. The completion design is a 20 stage open-hole swellable packer/sleeve assembly on a 4.5" liner. The packer set at 9676' MD will provide casing integrity to 670 foot from the north section line (10' past the 660' setback). The liner is necessary since the proposed 7-inch casing became stuck during the drilling operations and was set 70 feet short of the required setback depth. The well will not be completed above this measured depth (9676' MD).

Approved by the Utah Division of Oil, Gas and Mining

Date: February 14, 2013

By: Dark K Quist

NAME (PLEASE PRINT)	PHONE NUMBER	TITLE
Don Hamilton	435 719-2018	Permitting Agent

SIGNATURE	DATE
N/A	2/12/2013

RECEIVED: Feb. 12, 2013

STATE OF UTAH
DIVISION OF OIL, GAS AND MINING
ENTITY ACTION FORM -FORM 6

OPERATOR: NEWFIELD PRODUCTION COMPANY
ADDRESS: RT. 3 BOX 3630
MYTON, UT 84052

OPERATOR ACCT. NO. N2695

ACTION CODE	CURRENT ENTITY NO.	NEW ENTITY NO.	API NUMBER	WELL NAME	WELL LOCATION QQ	SC	TP	RG	COUNTY	SPUD DATE	EFFECTIVE DATE
B	99999	17400	4301351138	GMBU I-8-9-16	SENE	8	9S	16E	DUCHESNE	1/15/2013	1/31/13

WELL 1 COMMENTS: GRRV bhl NWNE

ACTION CODE	CURRENT ENTITY NO.	NEW ENTITY NO.	API NUMBER	WELL NAME	WELL LOCATION QQ	SC	TP	RG	COUNTY	SPUD DATE	EFFECTIVE DATE
A	99999	18869	4301351861	TOMLIN 4-6-3-1WH	NWNW	6	3S	1W	DUCHESNE	1/15/2013	1/31/13

GRRV bhl SWSW

CONFIDENTIAL

ACTION B	CURRENT ENTITY NO.	NEW ENTITY NO.	API NUMBER	WELL NAME	WELL LOCATION QQ	SC	TP	RG	COUNTY	SPUD DATE	EFFECTIVE
B	99999	17400	4301351481	GMBU F-7-9-17	SENE	12	9S	16E	DUCHESNE	1/8/2013	1/31/13

GRRV bhl S7 NWNW

ACTION CODE	CURRENT ENTITY NO.	NEW ENTITY NO.	API NUMBER	WELL NAME	WELL LOCATION QQ	SC	TP	RG	COUNTY	SPUD DATE	EFFECTIVE DATE
B	99999	17400	4301351471	GMBU O-7-9-17	SENE	12	9S	16E	DUCHESNE	1/7/2013	1/31/13

GRRV bhl S7 NWSW

ACTION CODE	CURRENT ENTITY NO.	NEW ENTITY NO.	API NUMBER	WELL NAME	WELL LOCATION QQ	SC	TP	RG	COUNTY	SPUD DATE	EFFECTIVE DATE

ACTION CODE	CURRENT ENTITY NO.	NEW ENTITY NO.	API NUMBER	WELL NAME	WELL LOCATION QQ	SC	TP	RG	COUNTY	SPUD DATE	EFFECTIVE DATE

ACTION CODE	CURRENT ENTITY NO.	NEW ENTITY NO.	API NUMBER	WELL NAME	WELL LOCATION QQ	SC	TP	RG	COUNTY	SPUD DATE	EFFECTIVE DATE

A - Establish new entity for new well (single well only)
B - Add new well to existing entity (group or unit well)
C - Re-assign well from one existing entity to another existing entity
D - Re-assign well from one existing entity to a new entity
E - Other (explain in comments section)

NOTE: Use COMMENT section to explain why each Action Code was selected

RECEIVED
JAN 28 2013
Div. of Oil, Gas & Mining

Signature: Tabitha Timothy
Production Clerk 01/08/13

EAGER BEAVER TESTERS INC.

P.O. BOX 1616
ROCK SPRINGS, WY 82902

PHONE:
CASPER - (307) 265-8147
ROCK SPRINGS - (307) 382-3350

BOP TEST REPORT

DATE: 3/15/13 OPERATOR: New Field RIG OR SITE#: Pioneer 69 SEC: 6 TNSHIP: 3S RANGE: 1W

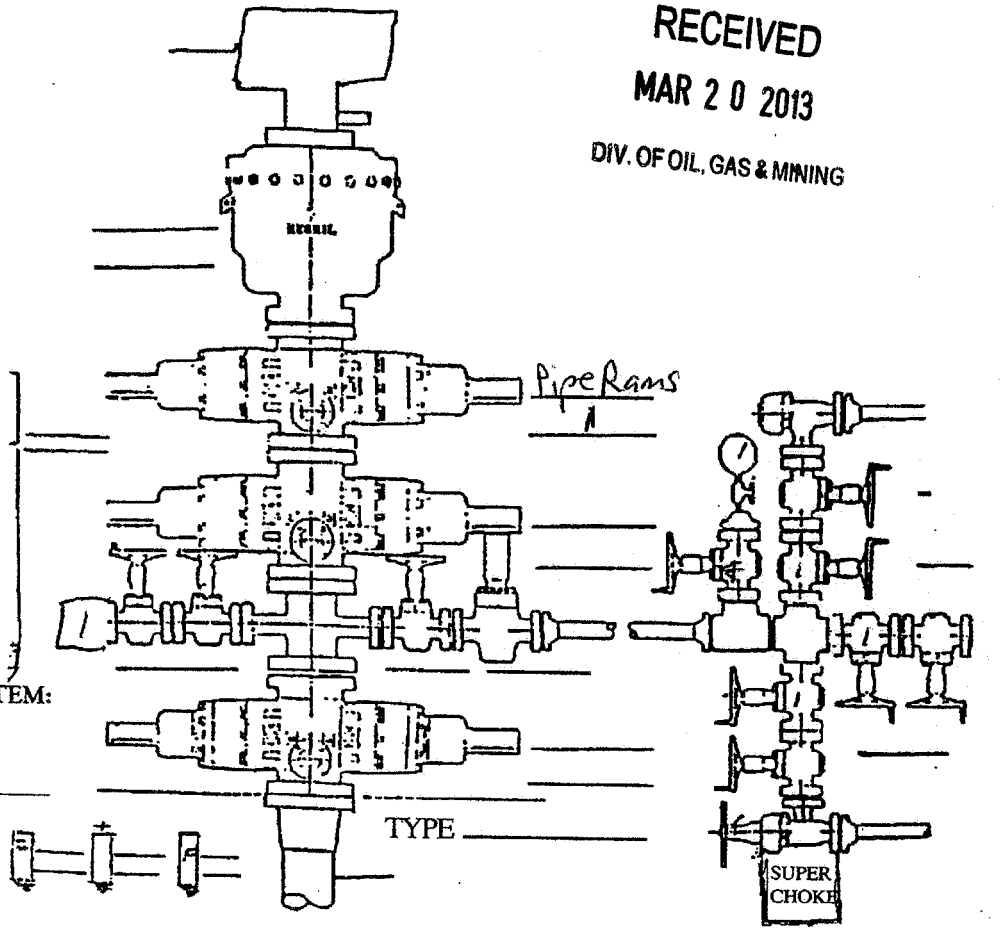
FIELD: Central Basin WELL#: Tomlin 4-6-3-1WH TEST PRESSURE: 250/5000

API# 43-013-51861

EQUIPMENT PRESSURE TESTED:

ANNULAR 50%	—
UPPER PIPE RAMS	/
LOWER PIPE RAMS	—
BLIND RAMS	—
KILL LINE VALVES	/
HCR VALVE	—
CHOKE VALVES	—
MANIFOLD VALVES	/
SUPER CHOKE	—
MANUAL CHOKE	—
UPPER KELLY VALVE	—
LOWER KELLY VALVE	—
INSIDE BOP	—
FLOOR VALVE	—
CASING PRE._____	—

RECEIVED
MAR 20 2013
DIV. OF OIL, GAS & MINING



ACCUMULATOR AND CLOSING SYSTEM:

NITROGEN PRECHARGE PSI_____
FIELD CHECK_____ GUAGE CHECK_____
BOTTLES_____ SPHERES_____

TYPE _____

FUNCTION CHECK_____
PUMP CHECK_____
REMOTE OPERATION CHECK_____
HYDRAULIC FLUID LEVEL_____

OTHER TESTS:

EQUIPMENT TYPE_____ PRESSURE_____

REPAIRS OR POTENTIAL PROBLEMS:

EAGER BEAVER TESTERS

DATE: 3/15/13 COMPANY: Newfield RIG: Pioneer 69 WELL NAME & #: Tomlin 4-6-3-1WH

Time	Test No.		Results
9:35 AM ☒PM☐	1	Pipe Rams, check, Inside manifold valves	Pass ☐Fail ☐
AM ☐PM☐	2		Pass ☐Fail ☐
AM ☐PM☐	3		Pass ☐Fail ☐
AM ☐PM☐	4		Pass ☐Fail ☐
AM ☐PM☐	5		Pass ☐Fail ☐
AM ☐PM☐	6		Pass ☐Fail ☐
AM ☐PM☐	7		Pass ☐Fail ☐
AM ☐PM☐	8		Pass ☐Fail ☐
AM ☐PM☐	9		Pass ☐Fail ☐
AM ☐PM☐	10		Pass ☐Fail ☐
AM ☐PM☐	11		Pass ☐Fail ☐
AM ☐PM☐	12		Pass ☐Fail ☐
AM ☐PM☐	13		Pass ☐Fail ☐
AM ☐PM☐	14		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐
AM ☐PM☐	Retest		Pass ☐Fail ☐

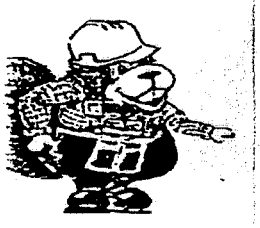
Acc. Tank Size (inches) (_____ W _____ D _____ L) ÷ 231= _____ gal.

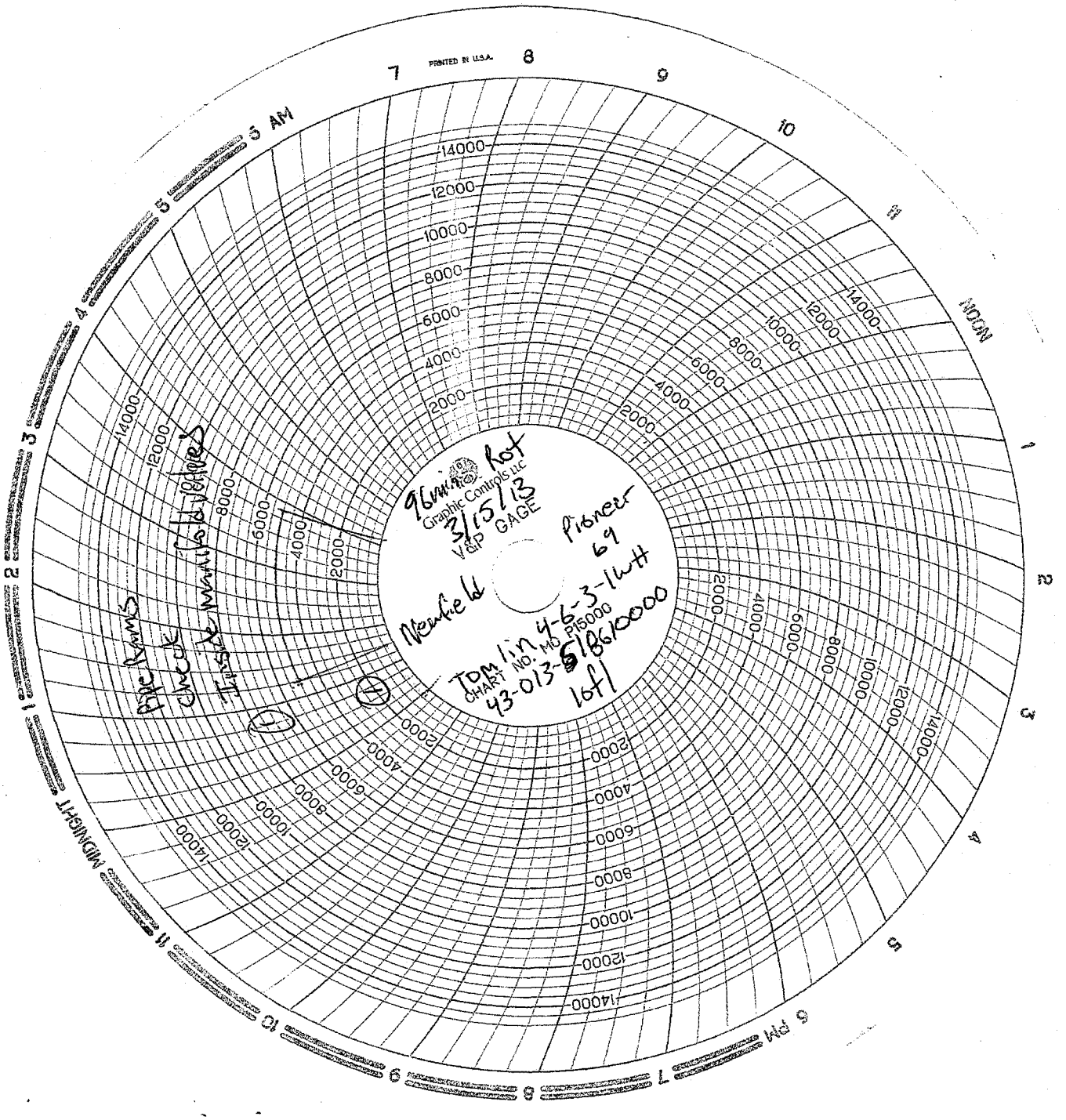
Rock Springs, WY (307) 382-3350

BOP TESTING, CASING TESTING, LEAK OFF TESTING, & INTEGRITY TESTING
NIPPLE UP CREWS, NITROGEN CHARGING SERVICE

Prompt & Efficient

24 Hr. Service




PRINTED IN U.S.A.
96min Rot
Graphic Controls LLC
3/15/13
V&P GAGE
Pioneer
69
Newfield
Tomlin 4-6-3-1WH
CHART NO. MC P15000
43-013-5186 10000
1 of 1
Pipe Rams
Check
Inside Manifold Valves
MIDNIGHT
NOON
6 PM
5 AM

EAGER BEAVER TESTERS INC.

P.O. BOX 1616

ROCK SPRINGS WY. 82902

ROCK SPRINGS WY 829 B2
PM
18 MAR
2013

Equality
FOREVER

UTAH OIL & GAS COMMISSION
1594 WEST N. TEMPLE STE.1210
SALT LAKE CITY, UT
84114-5801

84116$3154

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS, AND MINING

FORM 9

5.LEASE DESIGNATION AND SERIAL NUMBER: Patented

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

7.UNIT or CA AGREEMENT NAME:

1. TYPE OF WELL
Oil Well

8. WELL NAME and NUMBER:
Tomlin 4-6-3-1WH

2. NAME OF OPERATOR:
NEWFIELD PRODUCTION COMPANY

9. API NUMBER:
43013518610000

3. ADDRESS OF OPERATOR:
Rt 3 Box 3630 , Myton, UT, 84052

PHONE NUMBER:
435 646-4825 Ext

9. FIELD and POOL or WILDCAT:
WILDCAT

4. LOCATION OF WELL
FOOTAGES AT SURFACE:
0453 FNL 1161 FWL
QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN:
Qtr/Qtr: NWNW Section: 06 Township: 03.0S Range: 01.0W Meridian: U

COUNTY:
DUCHESNE

STATE:
UTAH

11.
CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

TYPE OF SUBMISSION	TYPE OF ACTION		
☐ NOTICE OF INTENT Approximate date work will start:	☐ ACIDIZE	☐ ALTER CASING	☐ CASING REPAIR
	☐ CHANGE TO PREVIOUS PLANS	☐ CHANGE TUBING	☐ CHANGE WELL NAME
☐ SUBSEQUENT REPORT Date of Work Completion:	☐ CHANGE WELL STATUS	☐ COMMINGLE PRODUCING FORMATIONS	☐ CONVERT WELL TYPE
	☐ DEEPEN	☐ FRACTURE TREAT	☐ NEW CONSTRUCTION
	☐ OPERATOR CHANGE	☐ PLUG AND ABANDON	☐ PLUG BACK
✓ SPUD REPORT Date of Spud: 1/17/2013	☐ PRODUCTION START OR RESUME	☐ RECLAMATION OF WELL SITE	☐ RECOMPLETE DIFFERENT FORMATION
	☐ REPERFORATE CURRENT FORMATION	☐ SIDETRACK TO REPAIR WELL	☐ TEMPORARY ABANDON
	☐ TUBING REPAIR	☐ VENT OR FLARE	☐ WATER DISPOSAL
☐ DRILLING REPORT Report Date:	☐ WATER SHUTOFF	☐ SI TA STATUS EXTENSION	☐ APD EXTENSION
	☐ WILDCAT WELL DETERMINATION	☐ OTHER	OTHER:

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

On 1/17/13 Ross #31 spud and drilled 65' of 17 1/2" hole, P/U and run 2 jts of 14" Conductor set @ 83'KB. On 1/21/13 cement w/BJ w/94sks of class G+2%kcl+.25#CF mixed@ 15.8ppg and 1.17 yield. Returned 2 bbls to pit.

Accepted by the Utah Division of Oil, Gas and Mining
FOR RECORD ONLY
April 18, 2013

NAME (PLEASE PRINT)
Cherei Neilson

PHONE NUMBER
435 646-4883

TITLE
Drilling Techinacian

SIGNATURE
N/A

DATE
4/18/2013

RECEIVED: Apr. 18, 2013

Casing / Liner Detail

Well	Tomlin 4-6-3-1WH
Prospect	Central Basin
Foreman	
Run Date:	
String Type	Conductor, 14", 36.75#, H-40, W (Welded)

- Detail From Top To Bottom -

Depth	*Length*	*JTS*	*Description*	*OD*	*ID*
83.00			18' KB		
18.00	65.00	2	Conductor	14.000	13.500
83.00			-		

Cement Detail

Cement Company: Other

Slurry	# of Sacks	Weight (ppg)	Yield	Volume (ft^3)	Description - Slurry Class and Additives
Slurry 1	94	15.8	1.17	109.98	G Neat

Stab-In-Job?	No	Cement To Surface?	Yes
BHT:	0	Est. Top of Cement:	0
Initial Circulation Pressure:		Plugs Bumped?	No
Initial Circulation Rate:		Pressure Plugs Bumped:	
Final Circulation Pressure:		Floats Holding?	No
Final Circulation Rate:		Casing Stuck On / Off Bottom?	No
Displacement Fluid:	Water	Casing Reciprocated?	No
Displacement Rate:		Casing Rotated?	No
Displacement Volume:	10	CIP:	
Mud Returns:		Casing Wt Prior To Cement:	
Centralizer Type And Placement:		Casing Weight Set On Slips:	

RECEIVED: Apr. 18, 2013

Casing / Liner Detail

Well	Tomlin 4-6-3-1WH
Prospect	Central Basin
Foreman	
Run Date:	
String Type	Surface, 9.625", 36#, J-55, LTC (Generic)

- Detail From Top To Bottom -

Depth	*Length*	*JTS*	*Description*	*OD*	*ID*
2,506.20			18' KB		
18.00	1.42		Wellhead		
19.42	2441.24	56	9 5/8 Casing	9.625	
2,460.66	1.78		Float collar	9.625	
2,462.44	41.86	1	Shoe Joint	9.625	
2,504.30	1.90		Guide Shoe	9.625	
2,506.20			-		

Cement Detail

Cement Company: BJ

Slurry	# of Sacks	Weight (ppg)	Yield	Volume (ft^3)	Description - Slurry Class and Additives
Slurry 2	244	15.8	1.17	285.48	Class G+2%kcl+.25#CF
Slurry 1	540	12.5	1.97	1063.8	Premium Lite II Cement

Stab-In-Job?	No	Cement To Surface?	Yes
BHT:	0	Est. Top of Cement:	0
Initial Circulation Pressure:		Plugs Bumped?	Yes
Initial Circulation Rate:		Pressure Plugs Bumped:	1356
Final Circulation Pressure:		Floats Holding?	Yes
Final Circulation Rate:		Casing Stuck On / Off Bottom?	No
Displacement Fluid:	Water	Casing Reciprocated?	No
Displacement Rate:		Casing Rotated?	No
Displacement Volume:	189	CIP:	17:49
Mud Returns:		Casing Wt Prior To Cement:	
Centralizer Type And Placement:		Casing Weight Set On Slips:	

Middle of first, top of second and every other for a total of six

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Casing / Liner Detail

Well	Tomlin 4-6-3-1WH
Prospect	Central Basin
Foreman	Jim Loudermilk Craig Smith
Run Date:	2/11/2013
String Type	Inter 1, 7", 29#, HCP-110, BTC (Generic)

- Detail From Top To Bottom -

Depth	*Length*	*JTS*	*Description*	*OD*	*ID*
9,558.79			RKB 18 FT	7.000	6.184
9,558.79	4.45	1	7' PUP JT ON MANDRILL HANGER	7.000	6.184
9,563.24	16.59	1	7' MKR JOINT	7.000	6.184
18.00	6930.57	163	7' CASING JOINT	7.000	6.184
6,948.57	15.44	1	7' MKR JOINT	7.000	6.184
6,964.01	2557.56	61	7' CASING JOINT	7.000	6.184
9,521.57	1.50		7' FLOAT COLLAR	7.000	6.184
9,523.07	33.92	1	7' CASING JOINT	7.000	6.184
9,556.99	1.80		7' FLOAT SHOE	7.000	6.184
9,579.83			-		

Cement Detail

Cement Company:

Slurry	# of Sacks	Weight (ppg)	Yield	Volume (ft^3)	Description - Slurry Class and Additives
Slurry 4		12.3			displacement 320 bbl
Slurry 3	415	14	1.34	556.1	bondcem [tm] system [452977]
Slurry 2	770	12.7	1.87	1439.9	versachem [tm] system [452010]
Slurry 1	7	12.5	7	49	20 bbl tuned spacer 111- sbm[483826]

Stab-In-Job?		Cement To Surface?	
BHT:	0	Est. Top of Cement:	0
Initial Circulation Pressure:	375	Plugs Bumped?	
Initial Circulation Rate:	3	Pressure Plugs Bumped:	900
Final Circulation Pressure:	900	Floats Holding?	
Final Circulation Rate:	3	Casing Stuck On / Off Bottom?	
Displacement Fluid:	Mud	Casing Reciprocated?	
Displacement Rate:	4	Casing Rotated?	
Displacement Volume:	323	CIP:	17:30
Mud Returns:	Full	Casing Wt Prior To Cement:	180
Centralizer Type And Placement:		Casing Weight Set On Slips:	

RECEIVED: Apr. 18, 2013

Casing / Liner Detail

Well	Tomlin 4-6-3-1WH
Prospect	Central Basin
Foreman	Alvin Nielsen Craig Smith
Run Date:	3/7/2013
String Type	Liner 1, 4.5", 13.5#, P-110, BTC (Generic)

- Detail From Top To Bottom -

Depth	*Length*	*JTS*	*Description*	*OD*	*ID*
8,651.00	16.80		TBR		
8,667.80	10.84		Hanger		
8,678.64	1042.26	24	4.5" Casing	4.500	3.920
9,720.90	5.08		Swell Packer Pup Jt		
9,725.98	8.75		Swell Packer 20		
9,734.73	85.55	2	4.5" Casing	4.500	3.920
9,820.28	5.08		Frac Sleeve Pup Jt		
9,825.36	4.12		Frac Sleeve		3.405
9,829.48	87.51	2	4.5" Casing	4.500	3.920
9,916.99	5.08		Swell Packer Pup Jt		
9,922.07	8.75		Swell Packer 19		
9,930.82	88.69	2	4.5" Casing	4.500	3.920
10,019.51	5.08		Frac Sleeve Pup Jt		

Cement Detail

Cement Company:

Slurry	# of Sacks	Weight (ppg)	Yield	Volume (ft^3)	Description - Slurry Class and Additives

Stab-In-Job?		Cement To Surface?	
BHT:	0	Est. Top of Cement:	
Initial Circulation Pressure:		Plugs Bumped?	
Initial Circulation Rate:		Pressure Plugs Bumped:	
Final Circulation Pressure:		Floats Holding?	
Final Circulation Rate:		Casing Stuck On / Off Bottom?	
Displacement Fluid:		Casing Reciprocated?	
Displacement Rate:		Casing Rotated?	
Displacement Volume:		CIP:	
Mud Returns:		Casing Wt Prior To Cement:	
Centralizer Type And Placement:		Casing Weight Set On Slips:	

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OCT 01 2013
DIV. OF OIL, GAS & MINING

United States Department of the Interior

BUREAU OF LAND MANAGEMENT
Utah State Office
440 West 200 South, Suite 500
Salt Lake City, UT 84101
http://www.blm.gov/ut/st/en.html

IN REPLY REFER TO:
3180 (UTU89807)
UT-922000

SEP 27 2013

Ms. Jessica Dembeck
Newfield Exploration Company
1001 17th Street, Suite 2000
Denver, Colorado 80202

Dear Ms. Dembeck:

Enclosed is one approved copy of Communitization Agreement No. UTU89807. This agreement communitizes all rights as to oil, gas and associated liquid hydrocarbons producible from the Green River-Wasatch Formation, covering All of Section 6, Township 3 South, Range 1 West, USM, Duchesne County, Utah. This agreement conforms to the spacing set forth in Order No. 139-90 issued by the Utah Board of Oil, Gas and Mining on May 9, 2012.

This agreement is effective as of February 11, 2012, the date of first production of the Fee well White 7-6-3-1W. The communitized area covers 639.65 acres and includes portions of Federal oil and gas lease UTU88630.

Office of Natural Resources Revenue Form MMS-4054, "Oil & Gas Operations Report", must be submitted for this agreement beginning with the month in which drilling operations commenced for the Fee well White 7-6-3-1W, with a surface location in the SWNE, Section 6, Township 3 South, Range 1 West, USM, Duchesne County, Utah, API # 43-013-50813. Form MMS-4054 is to be mailed to the Office of Natural Resources Revenue, P.O. Box 25165, Denver, Colorado 80225-0627.

Approval of this agreement does not warrant or certify that the operator thereof and other holders of operating rights hold legal or equitable title to those rights in the subject leases which are committed hereto. Please furnish all interested principals with necessary evidence of this approval.

If you have any questions, please contact Judy Nordstrom at (801) 539-4108.

Sincerely,

Roger L. Bankert

Roger L. Bankert
Chief, Branch of Minerals

Enclosure

cc: UDOGM
SITLA
ONRR w/enclosure (Attn: Nancy McCarty)
BLM FOM - Vernal w/enclosure

API Well Number: 43013518610000

Form 3160-4
(August 2007)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

BHL 669 FSL,
PBTVD 9006

FORM APPROVED
OMB NO. 1004-0137
Expires: July 31, 2010

WELL COMPLETION OR RECOMPLETION REPORT AND LOG

5. Lease Serial No.: PATENTED (FEE)

1a. Type of Well: ☑ Oil Well ☐ Gas Well ☐ Dry ☐ Other
b. Type of Completion: ☑ New Well ☐ Work Over ☐ Deepen ☐ Plug Back ☐ Diff. Resvr.,
Other: _____

6. If Indian, Allottee or Tribe Name

7. Unit or CA Agreement Name and No.

2. Name of Operator: NEWFIELD EXPLORATION COMPANY

8. Lease Name and Well No.: TOMLIN 4-6-3-1WH

3. Address: 1401 17TH ST. SUITE 1000 DENVER, CO 80202

3a. Phone No. *(include area code)*: (435) 646-3721

9. AFI Well No.: 43-013-51861

4. Location of Well *(Report location clearly and in accordance with Federal requirements)**

At surface 453' FNL & 1161' FWL (NW/NW) SEC. 6, T3S, R1W

At top prod. interval reported below 823' FNL & 722' FWL (NW/NW) SEC. 6, T3S, R1W

At total depth 787' FSL & 803' FWL (SW/SW) SEC. 6, T3S, R1W

10. Field and Pool or Exploratory: WILDCAT

11. Sec., T., R., M., on Block and Survey or Area: SEC. 6, T3S, R1W

12. County or Parish: DUCHESNE

13. State: UT

14. Date Spudded: 01/17/2013

15. Date T.D. Reached: 03/16/2013

16. Date Completed: 04/17/2013 ☐ D & A ☑ Ready to Prod.

17. Elevations (DF, RKB, RT, GL)*: 5233' GL 5251' KB

18. Total Depth: MD 13600' TVD 9087'

19. Plug Back T.D.: MD 13583' TVD

20. Depth Bridge Plug Set: MD TVD

21. Type Electric & Other Mechanical Logs Run (Submit copy of each): DUAL IND GRD, SP, COMP. DENSITY,COMP. NEUTRON,GR,CALIPER, CMT BOND

22. Was well cored? ☑ No ☐ Yes (Submit analysis)
Was DST run? ☑ No ☐ Yes (Submit report)
Directional Survey? ☐ No ☑ Yes (Submit copy)

23. Casing and Liner Record *(Report all strings set in well)*

Hole Size	Size/Grade	Wt. (#/ft.)	Top (MD)	Bottom (MD)	Stage Cementer Depth	No. of Sks. & Type of Cement	Slurry Vol. (BBL)	Cement Top*	Amount Pulled
12-1/4"	9-5/8" J-55	36#	0	2506'		244 CLASS G			
						540 PREMLITE			
8-3/4"	7" HCP-110	29#	0	9580'		415 BONDCEM		Surface	
						770 VERSACM			
6-1/8"	4-1/2" P-110	13.5#	8648'	13579'		Swell Packers			

24. Tubing Record

Size	Depth Set (MD)	Packer Depth (MD)	Size	Depth Set (MD)	Packer Depth (MD)	Size	Depth Set (MD)	Packer Depth (MD)
2-7/8"	EOT@ 8752'	Hornet @ 8580'						

25. Producing Intervals

Formation	Top	Bottom
A) Wasatch Basal Carbonate	9822' MD	13482' MD
B)		
C)		
D)		

26. Perforation Record

Perforated Interval	Size	No. Holes	Perf. Status
9822-13482' MD	Sliding Slv	20	

27. Acid, Fracture, Treatment, Cement Squeeze, etc.

Depth Interval	Amount and Type of Material
9822-13482' MD	Frac w/ 2429000#s 30/50 white sand in 32634 bbls of Lightning 25 fluid, in 20 stages.

28. Production - Interval A

Date First Produced	Test Date	Hours Tested	Test Production	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
4/18/13	4/28/13	24	→	504	347	134			Sliding Sleeves

Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status
			→					PRODUCING

28a. Production - Interval B

Date First Produced	Test Date	Hours Tested	Test Production	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
			→						

Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status
			→					

*(See instructions and spaces for additional data on page 2)

RECEIVED: Jun. 28, 2013

28b. Production - Interval C

Date First Produced	Test Date	Hours Tested	Test Production →	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate →	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status	

28c. Production - Interval D

Date First Produced	Test Date	Hours Tested	Test Production →	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate →	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status	

29. Disposition of Gas *(Solid, used for fuel, vented, etc.)*

SOLD AND USED FOR FUEL

30. Summary of Porous Zones (Include Aquifers):

Show all important zones of porosity and contents thereof: Cored intervals and all drill-stem tests, including depth interval tested, cushion used, time tool open, flowing and shut-in pressures and recoveries.

31. Formation (Log) Markers

GEOLOGICAL MARKERS

Formation	Top	Bottom	Descriptions, Contents, etc.	Name	Top Meas. Depth
				GARDEN GULCH MRK	7119'
				POINT 3	7973'
				DOUGLAS CREEK	8384'
				B LIMESTONE	8794'
				CASTLE PEAK	9023'
				BASAL CARBONATE	9416'

32. Additional remarks (include plugging procedure):

33. Indicate which items have been attached by placing a check in the appropriate boxes:

- ☐ Electrical/Mechanical Logs (1 full set req'd.)
- ☐ Geologic Report
- ☐ DST Report
- ☑ Directional Survey
- ☐ Sundry Notice for plugging and cement verification
- ☐ Core Analysis
- ☑ Other: Drilling Daily Activity

34. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records (see attached instructions)*

Name *(please print)* Jennifer Peatross Title Production Technician

Signature Peatross Date 05/20/2013

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 3)

RECEIVED: Jun. 28, 2013

API Well Number: 43013518610000

RECEIVED: Jun. 28, 2013

Client:	NEWFIELD EXPLORATION COMPANY			Calculation Method	Minimum Curvature
Directional:	Weatherford	Dates:	1/29/2013 to 3/3/2013	Proposed Azi.	184.77
County/State:	DUCHESNE, UTAH	Surface Location:	453' FNL, 161' FWL	Main Lateral	
Well Name:	TOMLIN 4-6-3-1WH		Sec. 6 - T3S - R1W	Target Ang	89.2
Drill Rig:	PIONEER 69	Depth Reference:	GL: 5232' / KB: 5250'	Target TVD.=	9271
SPUD Date:	1/29/13	Geologist:	MAX MODERN / HANS HOWELL	BHA =	GTB = 50' PTB= 47

Tool Type	BR	BRN	Survey Depth	Incl (°)	Azi (°)	CL (ft)	TVD (ft)	VS (ft)	Coordinates N/S (ft)	Coordinates E/W (ft)	Closure Dist (ft)	Closure Ang (°)	DLS (°/100')	Bld Rate (°/100')	Wlk Rate (°/100')
Tie-In			0	0	0		0	0	0	0					
MWD	0.215686	0.622471	102	0.22	206.24	102	101.9996	0.182237	-0.175646 S	-0.086581 W	0.195825	206.24	0.215686	0.215686	202.1961
MWD	0.3	0.62353	132	0.31	187.69	30	131.9993	0.316888	-0.307734 S	-0.122906 W	0.33137	201.7712	0.410777	0.3	-61.83333
MWD	0	0.625583	162	0.31	193.58	30	161.9989	0.47814	-0.46705 S	-0.152822 W	0.491416	198.1184	0.106179	0	19.63333
MWD	0.586207	0.625709	191	0.48	192.79	29	190.9981	0.675952	-0.661768 S	-0.198134 W	0.690792	196.6677	0.586494	0.586207	-2.724138
MWD	-0.137931	0.628156	220	0.44	187.43	29	219.9972	0.907468	-0.890644 S	-0.239425 W	0.922264	195.0467	0.20245	-0.137931	-18.48276
MWD	0	0.630245	250	0.44	183.91	30	249.9963	1.137713	-1.119789 S	-0.262175 W	1.150071	193.1773	0.09009	0	-11.73333
MWD	0.433333	0.630901	280	0.57	188	30	279.9951	1.401876	-1.382483 S	-0.290798 W	1.412736	191.8787	0.449412	0.433333	13.63333
MWD	0	0.633155	312	0.57	180.75	32	311.9935	1.719575	-1.699263 S	-0.315034 W	1.728219	190.5031	0.225239	0	-22.65625
MWD	0	0.635282	342	0.57	189.18	30	341.9921	2.017212	-1.995785 S	-0.340794 W	2.024673	189.6902	0.279293	0	28.1
MWD	0.6	0.635401	372	0.75	190.2	30	371.99	2.361456	-2.336338 S	-0.39937 W	2.370226	189.7003	0.601253	0.6	3.4
MWD	-0.166667	0.638114	402	0.7	190.72	30	401.9876	2.739187	-2.709636 S	-0.468227 W	2.749793	189.8039	0.168102	-0.166667	1.733333
MWD	0.433333	0.638809	432	0.83	195.42	30	431.9849	3.134998	-3.099157 S	-0.560088 W	3.149361	190.2441	0.480823	0.433333	15.66667
MWD	-0.133333	0.641438	462	0.79	194.94	30	461.9819	3.552106	-3.508445 S	-0.671182 W	3.572068	190.8301	0.135237	-0.133333	-1.6
MWD	0	0.64363	492	0.79	197.45	30	491.9791	3.957443	-3.905566 S	-0.786518 W	3.983975	191.3862	0.115348	0	8.366667
MWD	0.133333	0.645379	522	0.83	200.17	30	521.9761	4.368698	-4.306823 S	-0.923458 W	4.404714	192.102	0.184913	0.133333	9.066667
MWD	0.466667	0.645994	552	0.97	193.36	30	551.9724	4.829267	-4.757845 S	-1.057056 W	4.873855	192.526	0.586509	0.466667	-22.7
MWD	-0.3	0.64926	582	0.88	191.34	30	581.9684	5.309213	-5.230783 S	-1.161031 W	5.358086	192.5146	0.31904	-0.3	-6.733333
MWD	-1.033333	0.655089	612	0.57	193.05	30	611.966	5.685744	-5.60203 S	-1.240024 W	5.737631	192.4813	1.035732	-1.033333	5.7
MWD	-0.433333	0.658873	642	0.44	168.53	30	641.9648	5.944006	-5.86029 S	-1.250813 W	5.992289	192.0484	0.830896	-0.433333	-81.73333
MWD	-0.433333	0.662684	672	0.31	167.34	30	671.9642	6.132031	-6.052364 S	-1.21012 W	6.172155	191.3067	0.434087	-0.433333	-3.966667
MWD	0	0.665004	702	0.31	121.95	30	701.9637	6.246534	-6.174495 S	-1.12347 W	6.275873	190.3123	0.797369	0	-151.3
MWD	-0.3	0.668394	732	0.22	116.89	30	731.9634	6.305293	-6.243492 S	-1.003239 W	6.323581	189.1286	0.309687	-0.3	-16.86667
MWD	0.133333	0.67028	762	0.26	160.88	30	761.9631	6.389216	-6.333853 S	-0.929575 W	6.401704	188.3493	0.61186	0.133333	146.6333
MWD	0.4	0.671236	792	0.38	143.45	30	791.9626	6.526167	-6.478085 S	-0.848035 W	6.533356	187.4581	0.510697	0.4	-58.1
MWD	0.066667	0.673383	822	0.4	155.26	30	821.9619	6.692016	-6.65311 S	-0.744966 W	6.694688	186.3889	0.275582	0.066667	39.36667
MWD	-0.166667	0.676376	852	0.35	154.69	30	851.9613	6.862439	-6.831051 S	-0.661968 W	6.863051	185.535	0.167128	-0.166667	-1.9
MWD	-0.133333	0.679272	882	0.31	160.53	30	881.9608	7.01573	-6.990401 S	-0.595744 W	7.015741	184.8712	0.174045	-0.133333	19.46667
MWD	0.3	0.680633	912	0.4	182.42	30	911.9602	7.194363	-7.171543 S	-0.573115 W	7.194407	184.5691	0.53728	0.3	72.96667
MWD	-0.3	0.684165	942	0.31	170.51	30	941.9596	7.377651	-7.356216 S	-0.564156 W	7.377817	184.3855	0.386417	-0.3	-39.7
MWD	0.133333	0.686156	972	0.35	169.06	30	971.9591	7.544514	-7.526226 S	-0.533385 W	7.545103	184.0538	0.136198	0.133333	-4.833333
MWD	0.166667	0.688041	1002	0.4	154.16	30	1001.958	7.722847	-7.710439 S	-0.470353 W	7.724772	183.4908	0.363846	0.166667	-49.66667
MWD	-0.166667	0.691153	1032	0.35	165.1	30	1031.958	7.899256	-7.893236 S	-0.40115 W	7.903423	182.9094	0.290374	-0.166667	36.46667
MWD	0.2	0.692948	1062	0.41	190.2	30	1061.957	8.092393	-8.087425 S	-0.396596 W	8.097143	182.8075	0.58406	0.2	83.66667
MWD	0.4	0.694022	1092	0.53	200.13	30	1091.956	8.333044	-8.323341 S	-0.463356 W	8.336228	183.1863	0.482016	0.4	33.1
MWD	0.3	0.695473	1122	0.62	190.2	30	1121.955	8.628424	-8.613364 S	-0.53985 W	8.630265	183.5864	0.446531	0.3	-33.1

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MWD	0	0.698042	1152	0.62	200.57	30	1151.953	8.946188	-8.925075	S	-0.625622	W	8.946976	184.0097	0.37353	0	34.56667
MWD	0.266667	0.699642	1182	0.7	191.47	30	1181.951	9.284371	-9.256634	S	-0.719092	W	9.284523	184.442	0.43874	0.266667	-30.33333
MWD	0.166667	0.701626	1212	0.75	201.71	30	1211.948	9.654199	-9.618647	S	-0.828163	W	9.654233	184.921	0.462166	0.166667	34.13333
MWD	0.266667	0.703251	1242	0.83	201.18	30	1241.946	10.05046	-10.00367	S	-0.979297	W	10.05149	185.5911	0.267774	0.266667	-1.766667
MWD	-0.1	0.706263	1272	0.8	202.2	30	1271.943	10.45871	-10.40019	S	-1.136935	W	10.46215	186.2387	0.111076	-0.1	3.4
MWD	0.266667	0.707918	1302	0.88	192.57	30	1301.939	10.88677	-10.81895	S	-1.266204	W	10.89279	186.6753	0.539952	0.266667	-32.1
MWD	-0.733333	0.713364	1332	0.66	183.6	30	1331.937	11.28776	-11.21624	S	-1.32719	W	11.29449	186.7483	0.834036	-0.733333	-29.9
MWD	-0.3	0.717207	1362	0.57	173.94	30	1361.935	11.60707	-11.53708	S	-1.322286	W	11.6126	186.5382	0.456654	-0.3	-32.2
MWD	-0.133333	0.720446	1392	0.53	173.1	30	1391.934	11.88952	-11.82321	S	-1.289863	W	11.89336	186.2261	0.136012	-0.133333	-2.8
MWD	-0.433333	0.724855	1422	0.4	180.18	30	1421.932	12.12979	-12.06568	S	-1.273523	W	12.1327	186.0252	0.472968	-0.433333	23.6
MWD	0.133333	0.727125	1452	0.44	175.52	30	1451.932	12.34786	-12.28523	S	-1.264854	W	12.35018	185.8783	0.175232	0.133333	-15.53333
MWD	0.3	0.72877	1482	0.53	184.57	30	1481.931	12.60031	-12.53838	S	-1.266912	W	12.60223	185.7697	0.393077	0.3	30.16667
MWD	0.3	0.730427	1512	0.62	191.21	30	1511.929	12.90035	-12.83591	S	-1.309521	W	12.90254	185.8252	0.3728	0.3	22.13333
MWD	0.133333	0.732745	1542	0.66	189.89	30	1541.927	13.23373	-13.16534	S	-1.370753	W	13.23651	185.9441	0.142094	0.133333	-4.4
MWD	-0.066667	0.73586	1572	0.64	189.54	30	1571.925	13.57279	-13.50079	S	-1.428198	W	13.57612	186.0386	0.067967	-0.066667	-1.166667
MWD	0.366667	0.737304	1602	0.75	190.99	30	1601.923	13.93495	-13.85876	S	-1.493398	W	13.93899	186.1504	0.371295	0.366667	4.833333
MWD	0	0.740199	1632	0.75	189.84	30	1631.92	14.32571	-14.24496	S	-1.564383	W	14.3306	186.2671	0.050176	0	-3.833333
MWD	-0.166667	0.743774	1662	0.7	189.45	30	1661.918	14.70393	-14.61918	S	-1.628026	W	14.70956	186.3544	0.167475	-0.166667	-1.3
MWD	0.3	0.74553	1692	0.79	201.92	30	1691.916	15.08419	-14.99182	S	-1.73532	W	15.09191	186.6027	0.616351	0.3	41.56667
MWD	-0.3	0.749685	1722	0.7	193.49	30	1721.913	15.46295	-15.36188	S	-1.855275	W	15.47351	186.8863	0.47198	-0.3	-28.1
MWD	0.3	0.751479	1752	0.79	203.55	30	1751.91	15.83989	-15.72967	S	-1.980657	W	15.85388	187.1768	0.528135	0.3	33.53333
MWD	0.133333	0.753955	1782	0.83	196.52	30	1781.907	16.24843	-16.12757	S	-2.125075	W	16.26698	187.5064	0.35681	0.133333	-23.43333
MWD	0.166667	0.756317	1812	0.88	200.96	30	1811.904	16.6824	-16.55102	S	-2.269269	W	16.70586	187.807	0.276558	0.166667	14.8
MWD	0.433333	0.757621	1842	1.01	197.58	30	1841.9	17.16146	-17.01821	S	-2.431537	W	17.19104	188.1313	0.471309	0.433333	-11.26667
MWD	0	0.760692	1872	1.01	212.34	30	1871.895	17.65366	-17.49365	S	-2.652838	W	17.69366	188.623	0.864849	0	49.2
MWD	-0.733333	0.766774	1902	0.79	205.8	30	1901.892	18.08108	-17.90324	S	-2.884291	W	18.13409	189.152	0.808178	-0.733333	-21.8
MWD	-0.3	0.771134	1932	0.7	208.3	30	1931.889	18.44214	-18.2508	S	-3.061183	W	18.50574	189.5215	0.318898	-0.3	8.333333
MWD	-0.133333	0.774846	1962	0.66	218.7	30	1961.887	18.75352	-18.54699	S	-3.256093	W	18.83064	189.9573	0.431783	-0.133333	34.66667
MWD	0.433333	0.776253	1992	0.79	213.4	30	1991.885	19.07841	-18.8545	S	-3.477973	W	19.1726	190.4515	0.487146	0.433333	-17.66667
MWD	0	0.779466	2022	0.79	211.2	30	2021.882	19.44514	-19.20406	S	-3.698956	W	19.55705	190.9024	0.101103	0	-7.333333
MWD	0	0.782704	2052	0.79	222.89	30	2051.879	19.79304	-19.53249	S	-3.946849	W	19.92726	191.4237	0.536328	0	38.96667
MWD	-0.133333	0.786527	2082	0.75	219.55	30	2081.876	20.11701	-19.83541	S	-4.212628	W	20.27781	191.9903	0.200353	-0.133333	-11.13333
MWD	0.566667	0.787448	2112	0.92	222.01	30	2111.873	20.47002	-20.16576	S	-4.498838	W	20.66149	192.5763	0.579	0.566667	8.2
MWD	0	0.790761	2142	0.92	226.27	30	2141.869	20.84214	-20.5112	S	-4.834062	W	21.07314	193.2614	0.227948	0	14.2
MWD	-0.133333	0.794666	2172	0.88	227.94	30	2171.865	21.19054	-20.83201	S	-5.179138	W	21.46617	193.9615	0.159433	-0.133333	5.566667
MWD	-0.6	0.800584	2202	0.7	237.04	30	2201.862	21.4707	-21.08605	S	-5.503938	W	21.79254	194.6291	0.729575	-0.6	30.33333
MWD	0	0.803996	2232	0.7	227.94	30	2231.86	21.71649	-21.30851	S	-5.793755	W	22.08212	195.2109	0.370193	0	-30.33333
MWD	0	0.807437	2262	0.7	238.27	30	2261.858	21.95915	-21.52765	S	-6.085677	W	22.3713	195.7851	0.420103	0	34.43333
MWD	0	0.810907	2292	0.7	231.81	30	2291.856	22.19304	-21.73733	S	-6.385574	W	22.65584	196.3707	0.262933	0	-21.53333
MWD	0.3	0.813113	2322	0.79	243.54	30	2321.853	22.42516	-21.94278	S	-6.714756	W	22.94719	197.0147	0.588745	0.3	39.1
MWD	0	0.816638	2352	0.79	244.73	30	2351.85	22.63592	-22.12322	S	-7.08693	W	23.23061	197.7623	0.05469	0	3.966667
MWD	0.133333	0.819613	2382	0.83	238.72	30	2381.847	22.86732	-22.32432	S	-7.459655	W	23.53767	198.477	0.312827	0.133333	-20.03333
MWD	-0.133333	0.82378	2412	0.79	240.31	30	2411.844	23.11221	-22.53958	S	-7.82502	W	23.85925	199.1454	0.15293	-0.133333	5.3
MWD	0.266667	0.826227	2442	0.87	239.4	30	2441.841	23.36107	-22.75795	S	-8.200724	W	24.19042	199.8164	0.270254	0.266667	-3.033333
MWD	0.1	0.827292	2452	0.88	238.4	10	2451.84	23.45056	-22.83684	S	-8.331476	W	24.30915	200.0433	0.182535	0.1	-10
MWD	0.303922	0.835238	2554	1.19	237.07	102	2553.823	24.56275	-23.82304	S	-9.887609	W	25.79345	202.5406	0.304812	0.303922	-1.303922

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MWD	-0.107527	0.848471	2647	1.09	212.32	93	2646.805	25.93757	-25.09555	S	-11.1711	W	27.46962	203.9959	0.535766	-0.107527	-26.6129
MWD	-0.903226	0.873414	2740	0.25	346.58	93	2739.8	26.52911	-25.64574	S	-11.69114	W	28.18487	204.5069	1.373216	-0.903226	144.3656
MWD	1.397849	0.865838	2833	1.55	27.05	93	2832.787	25.1724	-24.32812	S	-11.1662	W	26.7683	204.6543	1.472536	1.397849	-343.5806
MWD	2.83871	0.836958	2926	4.19	23.6	93	2925.663	20.79208	-20.09384	S	-9.233678	W	22.11387	204.6801	2.843496	2.83871	-3.709677
MWD	2.225806	0.816386	3019	6.26	25.04	93	3018.271	12.81919	-12.38585	S	-5.727075	W	13.64583	204.8153	2.230094	2.225806	1.548387
MWD	1.064516	0.812665	3112	7.25	14.05	93	3110.628	2.270666	-2.098637	S	-2.156167	W	3.008876	225.7747	1.746175	1.064516	-11.8172
MWD	0.16129	0.822568	3205	7.4	0.17	93	3202.877	-9.491423	9.583962	N	-0.713656	W	9.610496	355.7414	1.905031	0.16129	-14.92473
MWD	-0.505376	0.843074	3298	6.93	350.78	93	3295.153	-20.9057	21.11144	N	-1.594873	W	21.1716	355.6798	1.355051	-0.505376	377
MWD	-0.774194	0.868471	3391	6.21	337.45	93	3387.547	-30.8195	31.29569	N	-4.422995	W	31.60669	351.9557	1.808022	-0.774194	-14.33333
MWD	0.797872	0.86961	3485	6.96	325.1	94	3480.931	-39.72096	40.66272	N	-9.631578	W	41.78784	346.6742	1.700196	0.797872	-13.1383
MWD	0.172043	0.880911	3578	7.12	310.26	93	3573.238	-47.40493	49.00948	N	-17.25439	W	51.95809	340.6048	1.957792	0.172043	-15.95699
MWD	0.043011	0.894704	3671	7.16	309.78	93	3665.517	-54.0762	56.44262	N	-26.10679	W	62.18789	335.1777	0.077236	0.043011	-0.516129
MWD	-1.258065	0.930781	3764	5.99	312.65	93	3757.904	-60.38107	63.43893	N	-34.13024	W	72.03728	331.7197	1.306362	-1.258065	3.086022
MWD	-0.095745	0.94849	3858	5.9	313.03	94	3851.398	-66.38425	70.05869	N	-41.26929	W	81.31035	329.4991	0.104499	-0.095745	0.404255
MWD	0.086022	0.963466	3951	5.98	312.29	93	3943.899	-72.29453	76.58011	N	-48.347	W	90.56459	327.7347	0.119079	0.086022	-0.795699
MWD	-0.043011	0.981251	4044	5.94	311.56	93	4036.396	-78.12689	83.03224	N	-55.5314	W	99.89039	326.2257	0.092156	-0.043011	-0.784946
MWD	-0.129032	1.001226	4137	5.82	312.14	93	4128.907	-83.87078	89.38832	N	-62.62855	W	109.1449	324.9836	0.143982	-0.129032	0.623656
MWD	-0.172043	1.022727	4230	5.66	309.38	93	4221.44	-89.3376	95.46169	N	-69.6698	W	118.1813	323.8773	0.343024	-0.172043	-2.967742
PRJ	-0.978495	1.060119	4323	4.75	302.37	93	4314.057	-93.72652	100.4331	N	-76.46706	W	126.23	322.7153	1.19202	-0.978495	-7.537634
MWD	0.064516	1.079088	4416	4.81	310.74	93	4406.735	-97.80071	105.0393	N	-82.67364	W	133.672	321.7947	0.752066	0.064516	9
MWD	0.731183	1.08584	4509	5.49	313.48	93	4499.359	-102.8731	110.6453	N	-88.85608	W	141.9076	321.233	0.777337	0.731183	2.946237
MWD	-0.695652	1.12072	4601	4.85	308.65	92	4590.984	-107.7935	116.1026	N	-95.08689	W	150.0711	320.6829	0.840687	-0.695652	-5.25
MWD	0.255319	1.138389	4695	5.09	304.04	94	4684.631	-112.0474	120.9187	N	-101.6457	W	157.9657	319.9492	0.495485	0.255319	-4.904255
MWD	0.225806	1.157198	4788	5.3	306.6	93	4777.249	-116.3298	125.789	N	-108.5125	W	166.126	319.2171	0.336267	0.225806	2.752688
MWD	-0.021505	1.181999	4881	5.28	299.76	93	4869.854	-120.4029	130.4739	N	-115.6756	W	174.3683	318.4404	0.678033	-0.021505	-7.354839
MWD	0.290323	1.20116	4974	5.55	306.94	93	4962.44	-124.6052	135.3007	N	-122.9849	W	182.843	317.73	0.783635	0.290323	7.72043
MWD	0.451613	1.21761	5067	5.97	314.73	93	5054.972	-130.1059	141.4072	N	-130.0154	W	192.0938	317.4033	0.953236	0.451613	8.376344
MWD	-0.623656	1.258934	5160	5.39	309.61	93	5147.515	-135.7075	147.5958	N	-136.8165	W	201.2543	317.1705	0.827572	-0.623656	-5.505376
MWD	0.83871	1.268579	5253	6.17	309.68	93	5240.042	-141.0631	153.5718	N	-144.0281	W	210.5431	316.8368	0.838744	0.83871	0.075269
MWD	-1.784946	1.340374	5346	4.51	291.95	93	5332.641	-145.0038	158.1303	N	-151.2668	W	218.8306	316.2708	2.496785	-1.784946	-19.06452
MWD	0.27957	1.365943	5439	4.77	294.99	93	5425.337	-147.4203	161.1306	N	-158.163	W	225.7844	315.5325	0.384723	0.27957	3.268817
MWD	0.086022	1.397549	5532	4.85	309.63	93	5518.013	-151.004	165.2719	N	-164.6959	W	233.3229	315.1	1.319188	0.086022	15.74194
MWD	1.344086	1.3989	5625	6.1	322.73	93	5610.59	-156.9214	171.7122	N	-170.7166	W	242.1348	315.1666	1.892529	1.344086	14.08602
MWD	-0.397849	1.445485	5718	5.73	320.23	93	5703.095	-163.9002	179.2129	N	-176.6789	W	251.6598	315.4079	0.484706	-0.397849	-2.688172
MWD	0.27957	1.476521	5811	5.99	321.13	93	5795.609	-170.721	186.5593	N	-182.694	W	261.1158	315.5997	0.296507	0.27957	0.967742
MWD	-1.526882	1.558742	5904	4.57	311.09	93	5888.214	-176.4276	192.7728	N	-188.532	W	269.6399	315.6372	1.816057	-1.526882	-10.7957
MWD	-0.129032	1.606303	5997	4.45	302.89	93	5980.927	-180.3225	197.1671	N	-194.354	W	276.8544	315.4117	0.704591	-0.129032	-8.817204
MWD	0.430108	1.640401	6090	4.85	308.43	93	6073.621	-184.2021	201.57	N	-200.4635	W	284.2817	315.1577	0.646219	0.430108	5.956989
MWD	1.333333	1.649554	6183	6.09	314.11	93	6166.196	-189.5087	207.4476	N	-207.0856	W	293.1194	315.05	1.453313	1.333333	6.107527
MWD	0.663043	1.679484	6275	6.7	314.73	92	6257.623	-196.0493	214.6215	N	-214.4024	W	303.3657	315.0292	0.667269	0.663043	0.673913
MWD	0.542553	1.715812	6369	7.21	316.22	94	6350.932	-203.4759	222.7396	N	-222.3795	W	314.7468	315.0464	0.57546	0.542553	1.585106
MWD	-1.698925	1.827418	6462	5.63	310.41	93	6443.346	-209.9978	229.911	N	-229.8915	W	325.1294	315.0024	1.834816	-1.698925	-6.247312
MWD	0.107527	1.885611	6555	5.73	308.84	93	6535.89	-215.2568	235.7798	N	-236.9811	W	334.2935	314.8544	0.198682	0.107527	-1.688172
MWD	-0.258065	1.960693	6648	5.49	310.48	93	6628.444	-220.4542	241.5794	N	-243.9811	W	343.3473	314.7166	0.310321	-0.258065	1.763441
MWD	-0.473118	2.049084	6741	5.05	305.22	93	6721.051	-225.1253	246.8282	N	-250.7089	W	351.8225	314.5531	0.702179	-0.473118	-5.655914
MWD	0.903226	2.092249	6834	5.89	304.67	93	6813.627	-229.5784	251.9033	N	-257.9774	W	360.5657	314.3175	0.904973	0.903226	-0.591398

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MWD	0.946237	2.137037	6927	6.77	308.62	93	6906.06	-235.0106	258.0392	N	-266.1849	W	370.7272	314.1098	1.055232	0.946237	4.247312
MWD	0.301075	2.211622	7020	7.05	307.64	93	6998.384	-241.1615	264.9459	N	-274.9871	W	381.8563	313.9346	0.326668	0.301075	-1.053763
MWD	-1.849462	2.383848	7113	5.33	300.39	93	7090.84	-246.1272	270.617	N	-283.2331	W	391.7328	313.6951	2.02795	-1.849462	-7.795699
MWD	0.344086	2.4743	7206	5.65	303.7	93	7183.413	-250.2095	275.3422	N	-290.7678	W	400.4488	313.4392	0.483955	0.344086	3.55914
MWD	0.870968	2.548617	7299	6.46	303.05	93	7275.894	-254.9028	280.7356	N	-298.9618	W	410.1105	313.1992	0.874069	0.870968	-0.698925
MWD	0.129032	2.666117	7392	6.58	308.73	93	7368.293	-260.3581	286.9226	N	-307.5038	W	420.5749	313.017	0.705107	0.129032	6.107527
MWD	0.043011	2.799978	7485	6.62	311.84	93	7460.677	-266.566	293.8323	N	-315.6544	W	431.2483	312.9495	0.386711	0.043011	3.344086
MWD	-0.27957	2.965625	7578	6.36	318.23	93	7553.082	-273.3406	301.25	N	-323.0796	W	441.7375	312.9975	0.824892	-0.27957	6.870968
MWD	0.172043	3.124446	7671	6.52	315.33	93	7645.496	-280.3171	308.8469	N	-330.223	W	452.1433	313.0842	0.389721	0.172043	-3.11828
MWD	0.301075	3.294555	7764	6.8	316.3	93	7737.868	-287.4009	316.5824	N	-337.7388	W	462.9168	313.1481	0.324457	0.301075	1.043011
MWD	0.096774	3.499493	7857	6.89	313.06	93	7830.206	-294.5079	324.3716	N	-345.6184	W	473.9927	313.1836	0.426287	0.096774	-3.483871
MWD	-1.315217	3.825793	7949	5.68	311.02	92	7921.651	-300.6196	331.1276	N	-353.0856	W	484.0609	313.1619	1.337226	-1.315217	-2.217391
MWD	-2.182796	4.268978	8042	3.65	314.13	93	8014.338	-305.2188	336.2099	N	-358.6832	W	491.6205	313.1477	2.198876	-2.182796	3.344086
MWD	0.978495	4.531217	8135	4.56	311.58	93	8107.099	-309.3113	340.7247	N	-363.5735	W	498.276	313.1419	0.997747	0.978495	-2.741935
MWD	2.946237	4.668035	8228	7.3	319.7	93	8199.594	-315.7005	347.6859	N	-370.1618	W	507.8437	313.2066	3.073994	2.946237	8.731183
MWD	0.623656	5.048772	8321	7.88	319.39	93	8291.779	-324.3512	357.0319	N	-378.133	W	520.0542	313.3559	0.625206	0.623656	-0.333333
MWD	-1.419355	5.7216	8414	6.56	312.58	93	8384.041	-332.0863	365.4665	N	-386.1947	W	531.7068	313.4204	1.689232	-1.419355	-7.322581
MWD	0.569892	6.320264	8507	7.09	314.37	93	8476.382	-339.0015	373.0745	N	-394.2092	W	542.7573	313.4222	0.614013	0.569892	1.924731
MWD	-0.634409	7.23479	8600	6.5	318.33	93	8568.729	-346.2875	381.0202	N	-401.8118	W	553.741	313.4786	0.809763	-0.634409	4.258065
MWD	-0.376812	8.058464	8669	6.24	320.49	69	8637.303	-351.6636	386.8307	N	-406.7941	W	561.355	313.5591	0.512398	-0.376812	3.130435
MWD	-0.590909	8.367675	8691	6.11	321.03	22	8659.175	-353.3655	388.6635	N	-408.2911	W	563.7028	313.5892	0.647205	-0.590909	2.454545
MWD	1.516129	8.731077	8722	6.58	296.54	31	8689.991	-355.2165	390.7401	N	-410.9181	W	567.0375	313.5582	8.790967	1.516129	-79
MWD	10.16129	8.651467	8753	9.73	269.44	31	8720.684	-355.6321	391.5086	N	-415.1291	W	570.6235	313.3227	15.76828	10.16129	-87.41935
MWD	10.51613	8.542512	8784	12.99	256.98	31	8751.077	-354.3238	390.6977	N	-421.1456	W	574.4636	312.8521	13.1058	10.51613	-40.19355
MWD	6.096774	8.692798	8815	14.88	246	31	8781.169	-351.3428	388.2932	N	-428.1783	W	578.021	312.2033	10.45897	6.096774	-35.41935
MWD	5.806452	8.880079	8846	16.68	234.9	31	8811.006	-346.5736	384.1148	N	-435.4566	W	580.6605	311.4154	11.3118	5.806452	-35.80645
MWD	5.483871	9.113473	8877	18.38	223.27	31	8840.575	-339.8941	377.9956	N	-442.4492	W	581.9295	310.5081	12.53297	5.483871	-37.51613
MWD	4.483871	9.451859	8908	19.77	211.04	31	8869.884	-331.364	369.9412	N	-448.5053	W	581.3893	309.5169	13.62202	4.483871	-39.45161
MWD	3.258065	9.936305	8939	20.78	198.83	31	8898.976	-321.3235	360.2397	N	-452.9858	W	578.7649	308.4937	14.0061	3.258065	-39.3871
MWD	4.064516	10.43043	8970	22.04	188.28	31	8927.847	-310.179	349.2746	N	-455.5994	W	574.0762	307.4747	13.05178	4.064516	-34.03226
MWD	10.96774	10.38198	9001	25.44	184.43	31	8956.221	-297.7109	336.876	N	-456.9518	W	567.7062	306.3985	12.04828	10.96774	-12.41935
MWD	11.70968	10.25456	9032	29.07	181.98	31	8983.776	-283.5254	322.7058	N	-457.7265	W	560.047	305.1846	12.25399	11.70968	-7.903226
MWD	11.83871	10.09283	9063	32.74	181.57	31	9010.37	-267.628	306.7941	N	-458.2166	W	551.4391	303.8039	11.85812	11.83871	-1.322581
MWD	11.19355	9.973103	9094	36.21	181.78	31	9035.921	-250.1088	289.2569	N	-458.7308	W	542.3131	302.2339	11.2001	11.19355	0.677419
MWD	9.774194	9.996186	9125	39.24	180.96	31	9060.438	-231.177	270.2967	N	-459.1796	W	532.8286	300.4833	9.907104	9.774194	-2.645161
MWD	9.580645	10.04831	9156	42.21	179.31	31	9083.93	-211.0223	250.0752	N	-459.2185	W	522.8951	298.5713	10.18988	9.580645	-5.322581
MWD	10.51613	9.984715	9187	45.47	178.97	31	9106.286	-189.657	228.6086	N	-458.8944	W	512.685	296.4812	10.5435	10.51613	-1.096774
MWD	9.741935	10.02037	9218	48.49	179.17	31	9127.434	-167.107	205.9496	N	-458.5276	W	502.6557	294.1874	9.753338	9.741935	0.645161
MWD	9.16129	10.159	9249	51.33	178.82	31	9147.395	-143.5139	182.2397	N	-458.1101	W	493.0276	291.693	9.201892	9.16129	-1.129032
MWD	11.48387	9.924133	9280	54.89	177.58	31	9166.002	-118.8888	157.4635	N	-457.3252	W	483.6746	288.9993	11.92078	11.48387	-4
MWD	11.19355	9.677884	9311	58.36	176.78	31	9183.053	-93.2326	131.6116	N	-456.0482	W	474.6594	286.0977	11.39897	11.19355	-2.580645
MWD	11.16129	9.361443	9342	61.82	176.59	31	9198.508	-66.63275	104.7896	N	-454.4938	W	466.4177	282.9834	11.17392	11.16129	-0.612903
MWD	10.29032	9.141495	9373	65.01	177.47	31	9212.38	-39.16643	77.10823	N	-453.0606	W	459.5755	279.6589	10.59869	10.29032	2.83871
MWD	8.419355	9.336275	9404	67.62	179.31	31	9224.833	-10.95698	48.73457	N	-452.2677	W	454.8858	276.1502	10.02108	8.419355	5.935484
MWD	8.903226	9.473279	9435	70.38	179.16	31	9235.941	17.84624	19.79897	N	-451.881	W	452.3145	272.5088	8.914675	8.903226	-0.483871
MWD	11.3871	8.761275	9466	73.91	179.26	31	9245.444	47.2097	-9.700456	S	-451.4744	W	451.5786	268.7691	11.39123	11.3871	0.322581

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MWD	10.70968	7.916962	9497	77.23	179.6	31	9253.168	77.09727	-39.71677	S	-451.1765	W	452.9212	264.9693	10.7622	10.70968	1.096774
MWD	6.935484	8.450713	9528	79.38	179.39	31	9259.452	107.3234	-70.07024	S	-450.9087	W	456.3206	261.167	6.967131	6.935484	-0.677419
MWD	11.19355	6.508033	9559	82.85	178.67	31	9264.239	137.7928	-100.689	S	-450.3894	W	461.5072	257.3982	11.42626	11.19355	-2.322581
MWD	12.90323	2.035589	9590	86.85	177.79	31	9267.021	168.4602	-131.5425	S	-449.4352	W	468.2899	253.6861	13.20921	12.90323	-2.83871
MWD	2.483871	1.765523	9621	87.62	177.72	31	9268.517	199.192	-162.4824	S	-448.2223	W	476.7638	250.0742	2.49409	2.483871	-0.225806
MWD	0.333333	4.832923	9663	87.76	177.53	42	9270.21	240.8319	-204.4121	S	-446.4832	W	491.0515	245.4004	0.561629	0.333333	-0.452381
MWD	-1.25641	-6.601012	9702	87.27	177.41	39	9271.901	279.4793	-243.3373	S	-444.7633	W	506.9788	241.3162	1.293469	-1.25641	-0.307692
MWD	-0.5625	-2.759788	9734	87.09	177.76	32	9273.475	311.1895	-275.2701	S	-443.4165	W	521.9118	238.1683	1.228739	-0.5625	1.09375
MWD	0	-1.666128	9766	87.09	177.76	32	9275.099	342.9094	-307.2045	S	-442.1674	W	538.4112	235.2096	0	0	0
MWD	-0.290323	-1.280234	9797	87	177.23	31	9276.698	373.6188	-338.1335	S	-440.8143	W	555.5642	232.5094	1.731911	-0.290323	-1.709677
MWD	2.4375	-0.523017	9829	87.78	176.24	32	9278.155	405.2711	-370.0478	S	-438.9936	W	574.1522	229.8709	3.936077	2.4375	-3.09375
MWD	0.375	-0.393471	9861	87.9	175.91	32	9279.361	436.8808	-401.95	S	-436.8048	W	593.6011	227.3796	1.096627	0.375	-1.03125
MWD	5.064516	0.034544	9892	89.47	175.65	31	9280.072	467.491	-432.8568	S	-434.5243	W	613.3322	225.1101	5.133453	5.064516	-0.83871
MWD	6.46875	-0.171906	9924	91.54	176.16	32	9279.79	499.1057	-464.7721	S	-432.2393	W	634.6998	222.9229	6.662154	6.46875	1.59375
MWD	7.53125	-1.798441	9956	93.95	176.45	32	9278.258	530.7184	-496.6665	S	-430.1795	W	657.0632	220.8969	7.585447	7.53125	0.90625
MWD	9.548387	-9.494874	9987	96.91	176.33	31	9275.325	561.2464	-527.4627	S	-428.2367	W	679.4141	219.0725	9.556158	9.548387	-0.387097
MWD	0.21875	-92.04276	10019	96.98	175.9	32	9271.455	592.6498	-559.1549	S	-426.0844	W	702.9951	217.3079	1.351708	0.21875	-1.34375
MWD	-5.21875	8.091228	10051	95.31	176.7	32	9268.03	624.1176	-590.9033	S	-424.0317	W	727.303	215.6632	5.780422	-5.21875	2.5
MWD	-2.354839	3.143873	10082	94.58	176.7	31	9265.358	654.6961	-621.7365	S	-422.2539	W	751.5681	214.1825	2.354839	-2.354839	0
MWD	-2.34375	1.532013	10114	93.83	177.06	32	9263.011	686.3076	-653.6028	S	-420.517	W	777.1944	212.7565	2.598455	-2.34375	1.125
MWD	-2.806452	0.721292	10145	92.96	177.42	31	9261.176	716.986	-684.5121	S	-419.0269	W	802.5836	211.4731	3.036447	-2.806452	1.16129
MWD	-0.78125	0.512809	10177	92.71	177.68	32	9259.593	748.6933	-716.4437	S	-417.6607	W	829.2961	210.2406	1.126451	-0.78125	0.8125
MWD	-0.75	0.370731	10209	92.47	177.86	32	9258.147	780.4223	-748.3868	S	-416.4168	W	856.4378	209.0924	0.937155	-0.75	0.5625
MWD	-4	0.054985	10240	91.23	176.94	31	9257.146	811.1493	-779.3378	S	-415.0112	W	882.9506	208.0361	4.979756	-4	-2.967742
MWD	1.375	0.127884	10272	91.67	177.42	32	9256.336	842.8586	-811.2886	S	-413.4374	W	910.5601	207.0037	2.034496	1.375	1.5
MWD	-0.78125	0.077361	10304	91.42	176.77	32	9255.474	874.5602	-843.2357	S	-411.8162	W	938.4237	206.0298	2.17562	-0.78125	-2.03125
MWD	5.967742	0.522238	10335	93.27	178.29	31	9254.205	905.285	-874.1787	S	-410.4812	W	965.7552	205.153	7.72096	5.967742	4.903226
MWD	6.15625	1.22008	10367	95.24	179	32	9251.831	937.0128	-906.0798	S	-409.7263	W	994.4125	204.3323	6.541764	6.15625	2.21875
MWD	-1.16129	0.922804	10398	94.88	178.65	31	9249.097	967.7258	-936.9524	S	-409.0931	W	1022.368	203.5871	1.616598	-1.16129	-1.129032
MWD	-2.53125	0.569346	10430	94.07	178.84	32	9246.6	999.4518	-968.8469	S	-408.3944	W	1051.404	202.8567	2.599541	-2.53125	0.59375
MWD	0	0.522253	10461	94.07	178.33	31	9244.4	1030.194	-999.7592	S	-407.6308	W	1079.667	202.1821	1.641012	0	-1.645161
MWD	-1.34375	0.382617	10493	93.64	179.06	32	9242.248	1061.942	-1031.678	S	-406.9038	W	1109.022	201.5248	2.643145	-1.34375	2.28125
MWD	-2.806452	0.201297	10524	92.77	178.74	31	9240.515	1092.73	-1062.624	S	-406.3095	W	1137.654	200.9251	2.989712	-2.806452	-1.032258
MWD	-0.75	0.157263	10556	92.53	179.2	32	9239.036	1124.532	-1094.584	S	-405.7349	W	1167.363	200.3385	1.620027	-0.75	1.4375
MWD	0.193548	0.15877	10587	92.59	178.7	31	9237.651	1155.342	-1125.548	S	-405.1674	W	1196.252	199.7975	1.622876	0.193548	-1.612903
MWD	0.71875	0.183032	10619	92.82	178.29	32	9236.141	1187.115	-1157.501	S	-404.3279	W	1226.087	199.2549	1.467837	0.71875	-1.28125
MWD	0.83871	0.21173	10650	93.08	177.91	31	9234.545	1217.864	-1188.443	S	-403.3015	W	1255.009	198.7448	1.483932	0.83871	-1.225806
MWD	0.96875	0.247463	10682	93.39	177.41	32	9232.74	1249.567	-1220.365	S	-401.9971	W	1284.871	198.2323	1.836328	0.96875	-1.5625
MWD	-2.6875	0.125945	10714	92.53	177.67	32	9231.087	1281.27	-1252.293	S	-400.6254	W	1314.815	197.7402	2.807319	-2.6875	0.8125
MWD	0.193548	0.128212	10745	92.59	177.05	31	9229.703	1311.98	-1283.229	S	-399.199	W	1343.888	197.2804	2.007357	0.193548	-2
MWD	-1.75	0.071324	10777	92.03	177.23	32	9228.413	1343.671	-1315.163	S	-397.6037	W	1373.951	196.8213	1.83804	-1.75	0.5625
MWD	-3.354839	0.006838	10808	90.99	177.51	31	9227.596	1374.402	-1346.119	S	-396.1817	W	1403.209	196.3999	3.474215	-3.354839	0.903226
MWD	0	0.006752	10840	90.99	177.33	32	9227.043	1406.134	-1378.082	S	-394.7415	W	1433.503	195.984	0.562416	0	-0.5625
MWD	-0.419355	0.001955	10871	90.86	177.87	31	9226.542	1436.887	-1409.05	S	-393.4435	W	1462.949	195.6011	1.791481	-0.419355	1.741935
MWD	-1.53125	-0.0098	10903	90.37	177.43	32	9226.199	1468.639	-1441.021	S	-392.1315	W	1493.422	195.2228	2.057941	-1.53125	-1.375
MWD	-1	-0.012365	10934	90.06	177.65	31	9226.083	1499.392	-1471.993	S	-390.8009	W	1522.986	194.8685	1.226227	-1	0.709677

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MWD	1.75	-0.004945	10966	90.62	176.96	32	9225.893	1531.12	-1503.956	S	-389.2963	W	1553.524	194.5124	2.776997	1.75	-2.15625
MWD	5	0.081527	10998	92.22	176.77	32	9225.1	1562.805	-1535.898	S	-387.5469	W	1584.037	194.1616	5.035107	5	-0.59375
MWD	2.387097	0.149812	11029	92.96	177.32	31	9223.699	1593.492	-1566.824	S	-385.9504	W	1613.659	193.838	2.973133	2.387097	1.774194
MWD	3.0625	0.26376	11061	93.94	176.63	32	9221.773	1625.138	-1598.721	S	-384.2649	W	1644.253	193.5151	3.743176	3.0625	-2.15625
MWD	0.40625	0.269949	11093	94.07	176.71	32	9219.538	1656.741	-1630.589	S	-382.4107	W	1674.831	193.1986	0.476691	0.40625	0.25
MWD	-5.774194	0.074798	11124	92.28	175.68	31	9217.821	1687.346	-1661.472	S	-380.3565	W	1704.453	192.8944	6.659286	-5.774194	-3.322581
MWD	-2.875	0.019478	11156	91.36	174.51	32	9216.805	1718.874	-1693.338	S	-377.6218	W	1734.932	192.5715	4.649733	-2.875	-3.65625
MWD	0.580645	0.027485	11187	91.54	174.27	31	9216.021	1749.357	-1724.179	S	-374.5923	W	1764.402	192.2575	0.967543	0.580645	-0.774194
MWD	3.46875	0.099184	11219	92.65	174.63	32	9214.851	1780.818	-1756.007	S	-371.4995	W	1794.874	191.9453	3.646385	3.46875	1.125
MWD	-4.21875	0.016005	11251	91.3	173.39	32	9213.748	1812.235	-1787.812	S	-368.1621	W	1825.326	191.6362	5.726687	-4.21875	-3.875
MWD	1.580645	0.03852	11282	91.79	173.46	31	9212.912	1842.618	-1818.597	S	-364.6138	W	1854.788	191.337	1.596681	1.580645	0.225806
MWD	5.59375	0.178279	11314	93.58	173.27	32	9211.413	1873.951	-1850.347	S	-360.9207	W	1885.218	191.0373	5.625102	5.59375	-0.59375
MWD	3.46875	0.300955	11346	94.69	173.8	32	9209.106	1905.255	-1882.06	S	-357.3269	W	1915.68	190.7502	3.84201	3.46875	1.65625
MWD	2.387097	0.389218	11377	95.43	173.76	31	9206.372	1935.568	-1912.757	S	-353.9813	W	1945.236	190.4847	2.390554	2.387097	-0.129032
MWD	0.8125	0.408597	11409	95.69	173.53	32	9203.271	1966.819	-1944.411	S	-350.456	W	1975.741	190.2172	1.082547	0.8125	-0.71875
MWD	-1.59375	0.322823	11441	95.18	172.48	32	9200.24	1998.005	-1976.029	S	-346.5764	W	2006.192	189.9479	3.634553	-1.59375	-3.28125
MWD	0.193548	0.317878	11472	95.24	172.3	31	9197.425	2028.159	-2006.629	S	-342.488	W	2035.647	189.6858	0.609778	0.193548	-0.580645
MWD	-0.40625	0.290541	11504	95.11	173.88	32	9194.539	2059.368	-2038.266	S	-338.654	W	2066.208	189.4334	4.934124	-0.40625	4.9375
MWD	0.8125	0.309758	11536	95.37	175.36	32	9191.616	2090.734	-2069.991	S	-335.6662	W	2097.03	189.2108	4.676785	0.8125	4.625
MWD	-1.612903	0.245007	11567	94.87	175.71	31	9188.85	2121.21	-2100.773	S	-333.2625	W	2127.043	189.0142	1.966217	-1.612903	1.129032
MWD	-0.612903	0.218877	11598	94.68	176.16	31	9186.269	2151.736	-2131.588	S	-331.0726	W	2157.146	188.8285	1.571059	-0.612903	1.451613
MWD	-3.4375	0.122054	11630	93.58	176.41	32	9183.964	2183.303	-2163.437	S	-329.0047	W	2188.311	188.647	3.524709	-3.4375	0.78125
MWD	-0.96875	0.098608	11662	93.27	176.39	32	9182.053	2214.906	-2195.317	S	-326.999	W	2219.537	188.4721	0.970757	-0.96875	-0.0625
MWD	0.78125	0.11285	11694	93.52	176.55	32	9180.158	2246.515	-2227.2	S	-325.0322	W	2250.793	188.303	0.927078	0.78125	0.5
MWD	1	0.13184	11725	93.83	176.97	31	9178.171	2277.149	-2258.087	S	-323.2837	W	2281.111	188.1475	1.681678	1	1.354839
MWD	0	0.128873	11757	93.83	176.59	32	9176.033	2308.768	-2289.965	S	-321.4903	W	2312.422	187.9916	1.184848	0	-1.1875
MWD	-0.59375	0.113351	11789	93.64	176.75	32	9173.949	2340.381	-2321.843	S	-319.6354	W	2343.741	187.8383	0.77555	-0.59375	0.5
MWD	1.193548	0.13589	11820	94.01	177.16	31	9171.881	2371.025	-2352.73	S	-317.9924	W	2374.123	187.6974	1.779322	1.193548	1.322581
MWD	1.967742	0.178008	11851	94.62	177.43	31	9169.548	2401.674	-2383.608	S	-316.5335	W	2404.533	187.5644	2.150882	1.967742	0.870968
MWD	-0.375	0.164479	11883	94.5	177.76	32	9167.004	2433.323	-2415.478	S	-315.1949	W	2435.956	187.4345	1.094248	-0.375	1.03125
MWD	-1.90625	0.118892	11915	93.89	178.28	32	9164.663	2465.016	-2447.373	S	-314.0923	W	2467.446	187.3133	2.502051	-1.90625	1.625
MWD	-4.387097	0.046513	11946	92.53	179.17	31	9162.927	2495.794	-2478.316	S	-313.4038	W	2498.054	187.2073	5.2405	-4.387097	2.870968
MWD	-1.34375	0.030081	11978	92.1	179.55	32	9161.635	2527.625	-2510.288	S	-313.0467	W	2529.732	187.1084	1.792627	-1.34375	1.1875
MWD	-1.806452	0.013694	12009	91.54	179.58	31	9160.65	2558.482	-2541.271	S	-312.8115	W	2560.451	187.0174	1.809039	-1.806452	0.096774
MWD	-1.15625	0.005725	12041	91.17	179.42	32	9159.894	2590.337	-2573.261	S	-312.5323	W	2592.171	186.9249	1.259672	-1.15625	-0.5
MWD	1.387097	0.014979	12072	91.6	178.96	31	9159.144	2621.181	-2604.249	S	-312.0942	W	2622.883	186.8338	2.030915	1.387097	-1.483871
MWD	1.806452	0.031122	12103	92.16	179.39	31	9158.127	2652.017	-2635.228	S	-311.6481	W	2653.593	186.7446	2.277108	1.806452	1.387097
MWD	1.387097	0.046382	12134	92.59	178.93	31	9156.843	2682.842	-2666.198	S	-311.194	W	2684.298	186.6573	2.0303	1.387097	-1.483871
MWD	2.125	0.075747	12166	93.27	178.99	32	9155.207	2714.636	-2698.151	S	-310.614	W	2715.971	186.567	2.133234	2.125	0.1875
MWD	0.806452	0.087151	12197	93.52	179.03	31	9153.371	2745.425	-2729.092	S	-310.0793	W	2746.651	186.4821	0.816673	0.806452	0.129032
MWD	-2.53125	0.049005	12229	92.71	179.16	32	9151.632	2777.221	-2761.04	S	-309.5746	W	2778.341	186.3974	2.563547	-2.53125	0.40625
MWD	-1.580645	0.031003	12260	92.22	179.48	31	9150.299	2808.052	-2792.009	S	-309.2071	W	2809.079	186.3196	1.887331	-1.580645	1.032258
MWD	-1	0.021548	12291	91.91	179.49	31	9149.182	2838.9	-2822.988	S	-308.9286	W	2839.841	186.2452	1.000519	-1	0.032258
MWD	-0.1875	0.019762	12323	91.85	179.98	32	9148.132	2870.759	-2854.97	S	-308.7807	W	2871.62	186.1729	1.541869	-0.1875	1.53125
MWD	-0.1875	0.018062	12355	91.79	179.63	32	9147.116	2902.623	-2886.954	S	-308.6718	W	2903.409	186.1029	1.109161	-0.1875	-1.09375
MWD	0.387097	0.021019	12386	91.91	179.56	31	9146.115	2933.481	-2917.937	S	-308.4528	W	2934.195	186.0343	0.448084	0.387097	-0.225806

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MWD	3.65625	0.061123	12418	93.08	179.94	32	9144.722	2965.327	-2949.906	S	-308.3133	W	2965.974	185.9667	3.843904	3.65625	1.1875
MWD	2.15625	0.092371	12450	93.77	179.32	32	9142.81	2997.141	-2981.848	S	-308.1071	W	2997.723	185.8993	2.896528	2.15625	-1.9375
MWD	-0.806452	0.078761	12481	93.52	179.5	31	9140.839	3027.943	-3012.783	S	-307.7885	W	3028.464	185.8331	0.993051	-0.806452	0.580645
MWD	-1.1875	0.060931	12513	93.14	179.6	32	9138.981	3059.756	-3044.728	S	-307.5376	W	3060.22	185.7677	1.227796	-1.1875	0.3125
MWD	1.15625	0.076117	12545	93.51	179.83	32	9137.125	3091.578	-3076.674	S	-307.3787	W	3091.99	185.7053	1.3608	1.15625	0.71875
MWD	0.83871	0.087167	12576	93.77	179.87	31	9135.157	3122.402	-3107.611	S	-307.2977	W	3122.768	185.6474	0.848538	0.83871	0.129032
MWD	-2.34375	0.05372	12608	93.02	179.89	32	9133.262	3154.229	-3139.555	S	-307.2308	W	3154.551	185.5891	2.34458	-2.34375	0.0625
MWD	0.612903	0.060476	12639	93.21	180.39	31	9131.577	3185.082	-3170.509	S	-307.3064	W	3185.367	185.5362	1.723201	0.612903	1.612903
MWD	4.470588	0.093894	12656	93.97	180.76	17	9130.513	3202.003	-3187.474	S	-307.4767	W	3202.27	185.5099	4.970366	4.470588	2.176471
MWD	-1.25	0.074063	12688	93.57	181.55	32	9128.408	3233.87	-3219.398	S	-308.1204	W	3234.109	185.467	2.7624	-1.25	2.46875
MWD	0.806452	0.084183	12719	93.82	182.52	31	9126.411	3264.77	-3250.314	S	-309.2188	W	3264.99	185.4345	3.224985	0.806452	3.129032
MWD	-0.5625	0.075004	12751	93.64	182.53	32	9124.329	3296.678	-3282.215	S	-310.6256	W	3296.881	185.4063	0.563364	-0.5625	0.03125
MWD	1.71875	0.099132	12783	94.19	184.06	32	9122.144	3328.591	-3314.087	S	-312.4604	W	3328.784	185.3861	5.070276	1.71875	4.78125
MWD	-2.193548	0.067513	12814	93.51	184.61	31	9120.062	3359.52	-3344.928	S	-314.7983	W	3359.708	185.3764	2.818721	-2.193548	1.774194
MWD	-3.4375	0.029554	12846	92.41	183.86	32	9118.41	3391.475	-3376.797	S	-317.1581	W	3391.659	185.3656	4.158696	-3.4375	-2.34375
MWD	1.53125	0.044002	12878	92.9	185.15	32	9116.928	3423.44	-3408.663	S	-319.6688	W	3423.62	185.3576	4.308217	1.53125	4.03125
MWD	-0.258065	0.041	12909	92.82	185.69	31	9115.381	3454.399	-3439.486	S	-322.5933	W	3454.581	185.3582	1.758801	-0.258065	1.741935
MWD	-1.875	0.023831	12941	92.22	184.37	32	9113.974	3486.367	-3471.331	S	-325.3961	W	3486.549	185.3552	4.527494	-1.875	-4.125
MWD	0.225806	0.025388	12972	92.29	184.46	31	9112.754	3517.342	-3502.215	S	-327.7806	W	3517.521	185.3469	0.367621	0.225806	0.290323
MWD	-0.8125	0.01905	13004	92.03	184.28	32	9111.548	3549.319	-3534.1	S	-330.2172	W	3549.493	185.3381	0.987984	-0.8125	-0.5625
MWD	-1.125	0.011685	13036	91.67	184.28	32	9110.515	3581.301	-3565.994	S	-332.6041	W	3581.471	185.3286	1.125	-1.125	0
MWD	-0.225806	0.010383	13067	91.6	184.46	31	9109.63	3612.288	-3596.891	S	-334.9652	W	3612.454	185.3204	0.622786	-0.225806	0.580645
MWD	2	0.023042	13098	92.22	184.25	31	9108.597	3643.269	-3627.784	S	-337.3179	W	3643.432	185.3122	2.111488	2	-0.677419
MWD	-0.96875	0.016049	13130	91.91	184.37	32	9107.444	3675.247	-3659.673	S	-339.7213	W	3675.407	185.3035	1.03871	-0.96875	0.375
MWD	-0.375	0.013595	13162	91.79	184.6	32	9106.411	3707.23	-3691.558	S	-342.2223	W	3707.387	185.2964	0.810363	-0.375	0.71875
MWD	-0.612903	0.010124	13193	91.6	184.27	31	9105.494	3738.216	-3722.452	S	-344.6184	W	3738.37	185.2893	1.227946	-0.612903	-1.064516
MWD	-0.5625	0.007221	13225	91.42	183.42	32	9104.651	3770.201	-3754.368	S	-346.7635	W	3770.348	185.277	2.714252	-0.5625	-2.65625
MWD	-1.34375	0.001777	13257	90.99	183.13	32	9103.978	3802.183	-3786.309	S	-348.5912	W	3802.322	185.2602	1.620675	-1.34375	-0.90625
MWD	1.15625	0.006295	13289	91.36	183.79	32	9103.322	3834.167	-3818.244	S	-350.522	W	3834.299	185.2452	2.36411	1.15625	2.0625
MWD	6.34375	0.056022	13321	93.39	183.07	32	9101.996	3866.129	-3850.157	S	-352.4349	W	3866.254	185.2302	6.730263	6.34375	-2.25
MWD	-0.452632	0.040663	13416	92.96	180.76	95	9096.733	3960.859	-3944.951	S	-355.604	W	3960.946	185.1508	2.469673	-0.452632	-2.431579
MWD	0.6	0.057408	13511	93.53	182.7	95	9091.355	4055.568	-4039.751	S	-358.4668	W	4055.624	185.0709	2.125275	0.6	2.042105
MWD	-3.607143	0.02751	13539	92.52	181.65	28	9089.878	4083.5	-4067.691	S	-359.5279	W	4083.549	185.051	5.199466	-3.607143	-3.75

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Daily Activity Report

Format For Sundry

TOMLIN 4-6-3-1WH

2/1/2013 To 6/30/2013

3/18/2013 Day: 1 **Completion**

Rigless on 3/18/2013 - Prep location. - Dig out saturated soil around Wekk head. Replace with dry soil.
Daily Cost: $0
Cumulative Cost: $6,470

3/20/2013 Day: 2 **Completion**

Rigless on 3/20/2013 - NU tbg head. NU and test BOP stack. - JSA and safety meeting. SICP 0 psi. Remove night cap from well head. Remove BPV and bushing. Install tbg head. Install tbg hanger with TWCV. Pressure test void in tbg head to 10,000 psi for 5 minutes, OK. NU 7? 10K manual frac valve and double BOP with blind and pipe rams. Test ram chambers to 1500 psi for 15 minutes each, OK. Function and pressure test blind rams against TWCV to 250 psi for 5 minutes. BO pressure. Pressure to 10,000 psi for 10 minutes, OK. Close manual frac valve, BO pressure below blind ram to 200 psi for 10 minutes. No pressure increase on blind rams, frac valve tested OK. Pressure blinds to 10,000 psi, open frac valve, BO pressure. Open blind rams and remove TWCV. Close manual valve. Continuing to NU BOP stack.Flow Cross ,upper pipe BOP& hydril bag All 7 1/16? 10k except hydril bag is 7 1/16? 5k. Continue test all to Newfield standards.Finished testing 7 1/16? 10k Flow Cross ,upper pipe BOP. Started testing 7 1/16? 5k Hydril annular . test all to Newfield standards. Shut in well and secure w/ 2 barrier close in . install night cap.
Daily Cost: $0
Cumulative Cost: $40,007

3/21/2013 Day: 3 **Completion**

Rigless on 3/21/2013 - MIRU WOR. RIH w/ 2 3/8" PH6 work string & overshot to catch setting For 7" 29# RBP.wind blowing not allowing rig to RU. - Finish dirt work on location. Set anchors. Spot in WOR. Wind gusting to 30 mph while setting T-sill for WOR. Spot in rig equipment and tanks. Ground all tanks and equipment. Unloading 2 3/8? PH-6 tbg. Cleaning, drifting, and inspecting work string. Rig up hard lines. W.O.W. - Continue Cleaning, drifting, and inspecting 2 3/8" PH 6 work string. Putting bags on ends to protect threads from dust. Waiting for wind to die down so rig derrick can be raised.load circulating tanks w/ fresh water.
Daily Cost: $0
Cumulative Cost: $134,443

3/22/2013 Day: 4 **Completion**

Rigless on 3/22/2013 - MIRU WOR. RIH w/ 2 3/8" PH6 work string & overshot to catch setting For 7" 29# RBP. Waiting for wind to die down . - Circulate drilling mud OH. PU 50 jts tbg. EOT 3160?. Currently circulating mud OH. Setting tubing on racks and talley.Circulate drilling mud OH. PU 49 jts tbg. Stacked out @ 7865.34?. Currently RU swivel to Attempt to circulate tbg volume of fresh water to make sure tbg is not plugged . Plan forward: Circulate Down thru Barite . - Operations meeting and JSA about picking up tools and tbg. Tally tbg. PU Kutrite shoe 5-3/4 Hyd (5-3/4? OD x 5-1/8? ID x 3.08?), XO bushing 5-3/4 OSG x 5-3/4 Hyd PX (5-3/4? OD x 4-13/16? ID x .77?), overshot 3-1/2 IF (4-3/4? OD x 2-5/8? x 2.86?), XO sub 2-

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3/8 IF x 3-1/2 IF (4-3/4? OD x 1-3/4? ID x 1.14?), drain sub 2 3/8 IF 3-5/8? OD x 1-15/16? x 1.02?), bumper sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-drill collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), intensifier 2-3/8? IF (3-3/4? OD x 1-1/2? ID x 11.65?), XO sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?) as BHA. - JSA and safety meeting. RU Mountain States WOR. Rig up floor and tongs. - Waiting for wind to die down so rig derrick can be raised.load circulating tanks w/ fresh water.Tanks are now loaded - Waiting for wind to die down so rig derrick can be raised.
Daily Cost: $0
Cumulative Cost: $206,096

3/23/2013 Day: 5 **Completion**

Rigless on 3/23/2013 - RIH w/ 2 3/8" PH6 work string & overshot to catch setting For 7" 29# RBP. CIR out mud every 1500'. Stacked out @ 7865.34?. Currently RU swivel to Attempt to circulate tbg volume of fresh water to make sure tbg is not plugged . - Continuing to Drilling down w/ swivel reverse circulating fresh water to clean out mud. Currently @jt 253 will not CIR down W/O engaging power swivel.current dept @ 7978.62'. - RIH w/ 2 3/8" tbg w/ fishing tools picked up jt 250. While RIH w/ tbg operator noticed weight indicator was losing weight stopped 20' out @ 7865.34?. POOH & LD jt 250 & 249. Currently RU swivel to Attempt to circulate tbg volume of fresh water to make sure tbg is not plugged .Drilling down w/ swivel reverse circulating fresh water to clean out mud . Currently we have 5 more Connections to get to the top of the fish @8141' - Engage fish (WL RBP setting tool). String wt 62K. Jar 3 times at 80K, 3 times at 90K, and once at 100K. Pipe came free. - Held safety meeting w/ rig Crew Review JSA RIH w/ 2-3/8? 5.95# PH6 PH6 tbg. w/ Weatherford retrieving head Drilling down w/ swivel on jt#262 engaged plug@ 8141 reverse circulating fresh water to clean out mud 40bbls Latched on fish Pulled 5k over string weight. Came back down 9? to 8150? continue to CIR out 50bbls fresh water. Picked up 1 jt2 3/8? #263 swiveled down to 8200.43? Continue to CIR out 40bbls ? bbl min @500psi. RD Swivel. Start POOH w/ 2 3/8? tbg w/ 7? 29# RBP. - Tie back on dbl line fast. Change pump lines. - PU 7? WRP retrieving head (5.5? OD x 1.75? ID x 1.75?), 2-3/8? IF x 2-7/8? EUE XO sub (3.75? OD x 1.50? ID x 1.08?), and 2-3/8 PH6 x 2-3/8? IF XO sub(3.375? OD x 1.75? ID x 1.27?). Run 1 jt 2-3/8? 5.95# PH6 P110 tbg, PU RN nipple (2-7/8? OD x 1.71? Id x .72?), run 1 jt 2-3/8? 5.95# PH6 P110 tbg, PU R nipple (2-7/8? OD x 1.71? ID x .64?). - TOH with 259 jts 2-3/8? 5.95# PH6 P110 tbg. LD XO sub, and intensifier. Stand back 2- 3 ?? DC?s. LD jars, bumper sub, drain sub, XO sub, and overshot with Kutrite shoe. Recover 9? WL RBP setting tool. Top of fish(RBP) now 8160? by tbg tally. - JSA and safety meeting. Clean drilling mud OH. Pumping down csg at 2.5 bpm and 800 psi, 80 RPM, and 2-4 pts on shoe. Clean out to fish at 8141?. Wash over fish.
Daily Cost: $0
Cumulative Cost: $235,918

3/24/2013 Day: 6 **Completion**

Rigless on 3/24/2013 - Circulate drilling mud OH. PU 49 jts tbg. RIH w/ 2 3/8" PH6 work string & overshot to catch setting For 7" 29# RBP. CIR out mud every 1500' - PU Globe junk basket. RIH w/ 2 3/8? tbg PH6 . currently @8675.2 .CIR down clean city water 240BBLS 2.5bbls min @ 1000psi. RD Power swivel. Double back Rig .POOH w/ 2 3/8" tbg LD 2- 2 3/8" collars, remove Rnipple& RN nipple , Break down junk basket. - TOH and LD bit, scraper, and x-overs. - Currently POOH w/ 2 3/8? tbg jt #223@6956? w/ 7? 29# RBP. Continue to POOH w/ tbg .OOH w/ 263jts 2 3/8? tbg & w/ 7? 29# RBP. Breaking down RBP & Retrieving head. Will MU & RIH w/ 7? 29# CSG scraper w/ Bit. Double rig back. - JSA and safety meeting. PU 5-7/8? tri cone rock bit w/ 3-1/2 reg pin, 7? csg scraper #-1/2 Reg (4-1/4? OD x 1 1/2? ID x 3.77?), bit sub 3-1/2 IF x 3-1/2 Reg (4-3/4? OD x 2-1/4? ID x 1.15?), XO sub 2-3/8? IF x 3-1/2? IF (4-3/4? OD x 1-3/4? ID x 1.14?), and XO sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?). RIH with 1 jt 2-3/8? 5.95# PH6 P110 tbg, RN nipple PH6 (2-7/8? OD x

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1.71? ID x .72?), 1 jt 2-3/8? 5.95# PH6 P110 tbg, and R nipple 2-7/8? OD x 1.71? ID x .64?). TIH with 276 jts 2-3/8? 5.95# PH6 P110 tbg. Tag liner top at 8655? by tbg tally. PU power swivel. - PU Globe junk basket (4-1/2? OD x 1? ID x 3.24?), bit sub 2-3/8 IF x 2-3/8 Reg (3-7/16? OD x 1-1/2?ID x1.14?), bumper sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-drill collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), intensifier 2-3/8? IF (3-3/4? OD x 1-1/2? ID x 11.65?), XO sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?) as BHA. Run 1 jt 2-3/8? 5.95# PH6 P110 tbg, RN nipple PH6 (2-7/8? OD x 1.71? ID x .72?), 1 jt 2-3/8? 5.95# PH6 P110 tbg, and R nipple 2-7/8? OD x 1.71? ID x .64?). RIH/ with 2-3/8? 5.95# PH6 P110 tbg. - Pump down csg at 4 bpm and 500 psi. Pump 150 bbl water until returns cleaned up. Recovered heavy drilling mud when started circulating. - w/ Weatherford retrieving head Drilling down w/ swivel on jt#262 engaged plug@ 8141 reverse circulating fresh water to clean out mud 40bbls Latched on fish Pulled 5k over string weight. Came back down 9? to 8150? continue to CIR out 50bbls fresh water. Picked up 1 jt2 3/8? #263 swiveled down to 8200.43?Continue to CIR out 40bbls ? bbl min @500psi. RD Swivel. Start POOH w/ 2 3/8? tbg w/ 7? 29# RBP.
Daily Cost: $0
Cumulative Cost: $301,953

3/25/2013 Day: 7 **Completion**

Rigless on 3/25/2013 - POOH w/ 2 3/8? tbg w/ 7? 29# RBP.LD RBP . RIH w/ 7" 29# scraper& bit to TOL CIR well clean. POOH w/ 7" 29# scraper & bit. - RIH with camera to 8673'. Top of fish at 8674'. Got good picture of spring colette cone , solid cone, releasing nut . looks like mandrel is possibly roll over from being hammered on. POOH w/ tbg & 4.5 wash shoe . LD Shoe & cross over's. - Pump 130 bbl clean water down csg at 4 bpm and 1,000 psi.Second load of water is milky. Rejected that load. Will wait on 1st trk to return (30 minutes) with clean water. Pump 70 bbl clean water down csg. RU WL trk. RIH with collar locator and sinker bar to EOT at 8671'. POH. Pump 60 bbl clean water down tbg. RIH with camera to 8673'. Top of fish at 8674'. Water is murky. Pump down tbg at 1/2 bpm to clean up. - RD Power swivel. Double back Rig .POOH w/ 2 3/8" tbg LD 2- 2 3/8" collars, remove Rnipple& RN nipple , Break down junk basket. - RIH w/ 4.5 wash shoe 2.85 w/ 2- xovers 2 3/8" x 2 7/8" x1.13 - 2 3/8" PH 6 x 2 3/8" euex1.31 & 278 jts 2 3/8" PH 6 tbg to get to TOF @ 8674 09 (corrected).
Daily Cost: $0
Cumulative Cost: $338,030

3/26/2013 Day: 8 **Completion**

Rigless on 3/26/2013 - POOh w/ 2 3/8" tbg LD 2 3/8" collars & junk basket. RD power swivel . RIH w/ 2 3/8" tbg W/ wire line re entry guide. RU wireline RIH w/ camera. - POOH w/ tbg & 4.5 wash shoe. LD wash shoe & crossover's . SDSIFN - JSA and safety meeting. Wait on fishing tool. - SICP 0 psi. Open blinds and 7?10K frac valve. PU spear 2-3/8 REG (3-1/4? OD x ?? ID x 1.96?), XO Sub 2-3/8 IF x 2-3/8 REG (3-3/4? OD x 1? ID x .99?), Bumper Sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), Jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-Drill Collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, and XO Sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?. TIH with 1 jt, RN nipple, 1 jt, R nipple and 274 jts 2-3/8? 5.95# PH6 P110 tbg. - POOH w/271 jts 2-3/8? 5.95# PH6 P110 tbg. Cones not latched onto Spear .Inspecting gappler to see if were any marks on it. - no work well closed in and Rig is secured.
Daily Cost: $0
Cumulative Cost: $378,716

3/27/2013 Day: 9 **Completion**

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Rigless on 3/27/2013 - RIH w/ spear 2 3/8" tbg , 2 3/8" collars to catch fish . POOH w/ 2 cone & releasing nut .wash over setting mandrel fish w/ wash shoe. - Wait on mill.Rig on standby discussing Plan moving forward. Making mill for mandrel - rig on stand by .Inspecting gappler to see if were any marks on it. And discussing plan moving forward. Wait on fishing tool.
Daily Cost: $0
Cumulative Cost: $404,458

3/28/2013 Day: 10 **Completion**

Rigless on 3/28/2013 - 0 - PU spear. RIH w/ spear w/ 1.998 grappler, jars ,excelrator,collars,274jts 2 3/8? PH6 tbg engage fish . - Dress top of mandrel at 8675? and polish ID to 8678.5?.POOH w/ 274 jts 2-3/8? 5.95# PH6 P110 tbg, LD 10? pup, & mill - Tie back on single line. PU swivel. - SICP slight vacuum. Open 7?10K frac valve and blind rams. PU Stinger Mill 3 1/2? IF (1.98? OD x ?? ID x 3.93?), Pony Collar 3 ?? IF (4 5/8? OD 2 9/16? ID x 9.93?, XO Sub 2 3/8 IF x 3 ? IF (4 ?? OD x 1 ?? ID x 1.14?), Drain Sub 2 3/8 IF (3 5/8? OD x 1 ?? ID x 1.02?), Bumper Sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), Jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-Drill Collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, and XO Sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?. TIH with 1 jt, RN nipple, 1 jt, R nipple and 274 jts 2-3/8? 5.95# PH6 P110 tbg, 10? pup, and jt #275. - Rig on standby discussing Plan moving forward. Making mill for mandrel , Grappler tool for spear.
Daily Cost: $0
Cumulative Cost: $433,120

3/29/2013 Day: 11 **Completion**

Rigless on 3/29/2013 - RIH w/milling tools. Mill into liner setting tools to dress fishing neck.POOH w/ mill - Rig broke down had to change out tongs & repair anti freeze line . - RD power swivel POOH w/ 1.98 Mill & 275 jts 2 3/8 tbg Pony Collar 3 ?? IF (4 5/8? OD 2 9/16? ID x 9.93?, XO Sub 2 3/8 IF x 3 ? IF (4 ?? OD x 1 ?? ID x 1.14?), Drain Sub 2 3/8 IF (3 5/8? OD x 1 ?? ID x 1.02?), Bumper Sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), Jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-Drill Collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, and XO Sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?. TIH with 1 jt, RN nipple, 1 jt, R nipple LD mill .Collars ,Jars , bumper sub, intensifier. - Tagged at 8675', same place as before. Milled 1.75 hrs. Milled 3". Reciprocate mill , taking weight at different places. Deepest tag was 7" deeper(ttl 10" into mandrel). - JSA and safety meeting. Finish TOH with spear, no fish. PU Stinger Mill 3 1/2? IF (1.98? OD x ?? ID x 3.93?), Pony Collar 3 ?? IF (4 5/8? OD 2 9/16? ID x 9.93?, XO Sub 2 3/8 IF x 3 ? IF (4 ?? OD x 1 ?? ID x 1.14?), Drain Sub 2 3/8 IF (3 5/8? OD x 1 ?? ID x 1.02?), Bumper Sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), Jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-Drill Collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, and XO Sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?. TIH with 1 jt, RN nipple, 1 jt, R nipple and 274 jts 2-3/8? 5.95# PH6 P110 tbg, 10? pup, and jt #275. - TOH. - PU swivel to turn as we go down into mandrel.RU power swivel to Attempt to engage fish @8675. Made several attempt's so far have not been able to stab into Mandrel. Tagged fish, Set down 5 points and went down with spear, 10 points, spear went down, 15 points, no movement of spear, Pick up with 3 - 5 points over string wt, lost over pull, Repeat trying to engage spear with no apparant engagement of spear. Hang back swivel and prep to POH. - RIH w/ spear & XO Sub 2 3/8 IF x 3 ? IF (4 ?? OD x 1 ?? ID x 1.14?), Drain Sub 2 3/8 IF (3 5/8? OD x 1 ?? ID x 1.02?), Bumper Sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), Jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-Drill Collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, and XO Sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?. TIH with 1 jt, RN nipple, 1 jt, R nipple and 274 jts 2-3/8? 5.95#

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PH6 P110 tbg, 10? pup, and jt #275.spear into 2" id on mandrel. - Tie back on single line. PU swivel.
Daily Cost: $0
Cumulative Cost: $499,170

3/30/2013 Day: 12 **Completion**

Rigless on 3/30/2013 - RIH w/milling tools. Mill into liner setting tools to dress fishing neck.POOH w/ mill - RU JW wireline . RIH w/ 2" magnet 3.5" magnet . Stack out @8674' w/ 3.5 magnet . Pulled up to 8650' then went back down .stacked out @ 8665' Pulled up to 8630' . Went back down . Stack out @8665' started POOH w/ 3.5 magnet to see what we got. - JSA and safety meeting. RIH with 4? magnet on WL. Tag top of fish at 8674?. POH, no recovery. RIH with 1.75? magnet on WL. Tagged top of fish. POH. Recover finger off segmented cone. RIH with magnet. Tagged top of fish. POH. Recover second finger off segmented cone. RIH with magnet. Tagged top of fish. POH. Recover soft rubber (2? ring shape). Make 4th run with 1.75? magnet. Tag top of fish. POH. No recovery. RD WL trk. - PU Stinger Mill 3 1/2? IF (1.98? OD x ?? ID x 3.93?), Pony Collar 3 ?? IF (4 5/8? OD 2 9/16? ID x 9.93?, XO Sub 2 3/8 IF x 3 ? IF (4 ?? OD x 1 ?? ID x 1.14?), Drain Sub 2 3/8 IF (3 5/8? OD x 1 ?? ID x 1.02?), Bumper Sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), Jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-Drill Collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, and XO Sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?. TIH with 1 jt, RN nipple, 1 jt, R nipple and 274 jts 2-3/8? 5.95# PH6 P110 tbg, 10? pup, and jt #275. - Tie back on single line. RU power swivel .Started mill @8675? -8677? torqueing up to 1888ft lbs. Started pumping 2.5 bbls min @500psi work mill up & down in mandrel. Made 1.5 ft w/ mill .Pulled up on mill to 86000 set of jar pulled up high came back down @stacked down @8675' pull back up passed PBR came back no drag .stack back out @8675'. RD power swivel . - POOH w/ 274 jts 2-3/8? 5.95# PH6 P110 tbg, 10? pup, XO Sub 2 3/8 IF x 3 ? IF (4 ?? OD x 1 ?? ID x 1.14?),, Bumper Sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), Jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-Drill Collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, and XO Drain Sub 2 3/8 IF (3 5/8? OD x 1 ?? ID x 1.02?)Sub Pony Collar 3 ?? IF (4 5/8? OD 2 9/16? ID x 9.93? Mill 3 1/2? IF (1.98? OD x ?? ID x 3.93?), LD mill & inspect mill. - We are POOH LD 3 ? ? Collars , 3 ?? Jars , 3 ?? bumper sub, 3 3/4 ? intensifier.cross over's & 1.98mill.inspect mill . Prepair to RU JW wireline.
Daily Cost: $0
Cumulative Cost: $533,177

3/31/2013 Day: 13 **Completion**

MWS #731 on 3/31/2013 - RIH w/milling tools. Mill into liner setting tools to dress fishing neck.POOH w/ mill. Rigged up wireline. Run gauge rings for 7" and 4-1/2" casing. Rih w/ Magnet on tbng to liner top. - Engage mandrel on liner hanger tool at 8674?. String weight 70K. Jar 2 times at 90K picking up to 100K. Jar 4 times at 100K picking up to 110K. Jar 15 times at 110K picking up to 115K. Jar 19 times at 115K picking up to 120K working up hole 4-6? with each jar. After 4? started pulling OH with 110K. Pulled out of liner top, weight dropped to 76K. LD power swivel. - JSA and safety meeting. PU power swivel and 2 jts 2 3/8? P110 tbg. - RIH w/spear 3 1/2? IF (1.98? OD x ?? ID x 3.93?), Pony Collar 3 ?? IF (4 5/8? OD 2 9/16? ID x 9.93?, XO Sub 2 3/8 IF x 3 ? IF (4 ?? OD x 1 ?? ID x 1.14?), Drain Sub 2 3/8 IF (3 5/8? OD x 1 ?? ID x 1.02?), Bumper Sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), Jars 3-3/4? OD x 1-1/2? ID x 12.97?) 2-Drill Collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, and XO Sub 2-3/8 PH6 x 2-3/8 IF (3-3/8? OD x 1-3/4? ID x 1.27?. TIH with 1 jt, RN nipple, 1 jt, R nipple and 274 jts 2-3/8? 5.95# PH6 P110 tbg. - POOH w/ 274 jts 2-3/8? 5.95# PH6 P110 tbg, 10? pup, XO Sub 2 3/8 IF x 3 ? IF (4 ?? OD x 1 ?? ID x 1.14?),, Bumper Sub 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 7.98?), Jars

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3-3/4? OD x 1-1/2? ID x 12.97?) 2-Drill Collars 2-3/8 IF (3-1/2? x 1-9/16? ID x 62.65?), Intensifier 2-3/8 IF (3-3/4? OD x 1-1/2? ID x 11.65?, and XO Drain Sub 2 3/8 IF (3 5/8? OD x 1 ?? ID x 1.02?)Sub Pony Collar 3 ?? IF (4 5/8? OD 2 9/16? ID x 9.93? Mill 3 1/2? IF (1.98? OD x ?? ID x 3.93?), LD mill & inspect mill. Lots of wear on mill. Sent pic's to engineer. - Make up Magnet Bha. 3.5" OD fishing magnet (1.26), Bit sub (1.16), Bumper sub (8.01), Fishing jar (10.83), X-over sub (1.28). Continue tripping in well w/ 2-3/8" 5.95# P-110 Ph-6 tbng. Talley singles and prepare to ease magnet through liner top. - PJSM with rig crew and wireline crew. Rig up wireline and rih w/5.50 OD magnet to liner top. Tagged up at 8655. Picked up and sat down on magnet 3 times each time pulling up 20 ft. Pooh with wireline and check magnet. Nothing recovered on magnet.Change out tools. Rih w/ 3.75" OD Gauge ring. Ran in to 9020. Pooh w/ wireline. RDMO wireline. - LD BHA while waiting on WL trk to run 5 ?? magnet and gauge ring 120? into 4 ??. - TOH. Recovered hanger setting tool. Solid cone missing. 9 fingers of segmented cone missing. Recovered 2 on magnet, 7 left in hole. Recovered pieces of fingers in setting tool.
Daily Cost: $0
Cumulative Cost: $562,860

4/1/2013 Day: 14 **Completion**

MWS #731 on 4/1/2013 - Make 2 magnet runs with 3.5" OD magnet. Make up Globe basket. Rih to 9483. Incresed pump pressure. Prepare to pooh w/ globe basket - PJSM with rig crew, flowback and Weatherford pump operator. Pressure test pump lines. Begin reverse circulating on well to circ junk into globe basket and circ drilling mud out of casing annulus.Pumping 2.5 bpm at 2000 psi.Pumped 34 bbls down casing and got mud returns to flat tank. Switch over to 500 bbl tank and continue circulating.@2330. Make connection. No tag and no drag. Rih to 9463. Tagged up. Kick pump back in. pumping 2.5 bbls per min @2150 psi. Rotate swivel at 60 rpm. Pump pressure steadily rising. Rih to 9483 on jt 304. All of the way down. Pump pressure rose to 3000 psi. Kicked out pump. Called for orders. Decision made to trip out of well and check globe basket. Total bbls pumped 128.6. - Rig in Weatherford pumping equipment. - Wait on Weatherford pump to arrive on location with certified pumping equipment. - PJSM with rig crew and flowback. Hazard hunt on location with night crew as flowback was rigged in on days. Found that rig pump manifold had not been certified since 2011. Continued going around location searching for the rest of the hazards on location. - TIH to liner top. Tie back on single line. TIH. Tagged up at 9446.20 on jt 303 4" stick up to tag. - Ran in the hole slowly. Tagged up on liner top @ 8655. Rotated throught the liner top. Continue in hole with magnet to 9200'. Tagged up solid with 295 jts in well. Set 10k down. Hard tag. - Tie back on double lines. TIH. - TOH. Recovered 3 small pieces of solid cone. LD 3 ?? magnet. PU 3 ?? Globe basket. - JSA and safety meeting. TIH with 2 3/8? P110 tbg. Went through tight spot at 9200?, saw no weight change on indicator. PU tbg and RIH to 9446? on jt #303 (pushed junk all the way, took wt at 9446?). - Run back in well with same 3.5" Magnet BHA-Make up Magnet Bha. 3.5" OD fishing magnet (1.26), Bit sub (1.16), Bumper sub (8.01), Fishing jar (10.83), X-over sub (1.28). Begin tripping in well. - Begin pulling out of well with magnet slowly. Out of the well with the magnet. Had 1 big piece of the finger off of the callet. Also had 2 smaller pieces and lots of metal on the magnet.Prepare to run back in well with 3.5" od magnet. - SD for lightning and wind
Daily Cost: $0
Cumulative Cost: $592,164

4/2/2013 Day: 15 **Completion**

MWS #731 on 4/2/2013 - Pooh w/globe basket. Recover metal. Rih w/ globe basket.Pooh w/ globe basket. No metal. Rih w/ magnet. Pooh w/ magnet. 2 small pieces. Prepare to rih and tag 1st sleeve - Lay down 2 jts. Continue pulling out of well slowly to liner top at 8655.. Continue tripping out of well. Out of well had 2 tiny pieces of metal on magnet. - TOH. LD

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junk basket. No recovery in Globe Basket. PU 3 ?? magnet 2 3/8 Reg (3 1/8? OD x 1 ?? ID x 1.26?). TIH with Bit sub 2 3/8 REG (3 1/8" OD x 1 1/4" ID x 1.16'), Bumper Sub 2 3/8 REG (3 1/8" OD x 1" ID x 8.01'), Jars 2 3/8" REG (3 1/8" x 1" x 10.83'), XO Sub 2 3/8" PH6 x 2 3/8 REG (2 7/8" OD x 1" ID x 1.28', and 2 3/8" 5.95# PH6 P110 tbg. Ran in well to 9800'. No tag no drag. Pull up 20'. Go back down to 9800. No tag no drag. Jt 315 17'ft in. - Rig down Pwr Swivel and begin Pooh with Globe basket.0240 130 jts left in well to be at 4042.00. Continue tripping out of well w/ globe basket. Break out bha. Had more pieces of metal in Basket. Make up BHA. Prepare to RIH - JSA and safety meeting. TIH with Globe junk basket 2 3/8 REG (3 5/8" OD x 1" ID x 3.03'), Bit sub 2 3/8 REG (3 1/8" OD x 1 1/4" ID x 1.16'), Bumper Sub 2 3/8 REG (3 1/8" OD x 1" ID x 8.01'), Jars 2 3/8" REG (3 1/8" x 1" x 10.83'), XO Sub 2 3/8" PH6 x 2 3/8 REG (2 7/8" OD x 1" ID x 1.28', and 2 3/8" 5.95# PH6 P110 tbg to 9421? on jt #302. - Begin tripping in well. - Swivel up on jt #303. Pump down csg at 2.5 bpm and 1000 psi. 45 RPM. Clean out to 9765? on jt #313. Pump pressure 2350 psi. Pump 10 bbl sweep. Circulate sweep to surface. LD power swivel.
Daily Cost: $0
Cumulative Cost: $656,565

4/3/2013 Day: 16 **Completion**

MWS #731 on 4/3/2013 - RIH with 3.5" Magnet. Tag up. Pooh with magnet. No recovery. Rih with Globe basket. CirculateKCL in the well. Pooh with globe basket. No recovery. Rig up Halliburton logging truck. - JSA and safety meeting. TOH with magnet. No recovery. LD magnet. TIH with Globe junk basket 2 3/8 REG (3 5/8" OD x 1" ID x 3.03'), Bit sub 2 3/8 REG (3 1/8" OD x 1 1/4" ID x 1.16'), Bumper Sub 2 3/8 REG (3 1/8" OD x 1" ID x 8.01'), Jars 2 3/8" REG (3 1/8" x 1" x 10.83'), XO Sub 2 3/8" PH6 x 2 3/8 REG (2 7/8" OD x 1" ID x 1.28', and 2 3/8" 5.95# PH6 P110 tbg to 9765?. Swivel up on jt #314.Establish circulation down csg at 3 bpm and 1200 psi. Clean out to frac sleeve at 9822? on jt #316. Pump sweep and circulate to surface. Pump second sweep and circulate.No metal recovered. - Begin tripping out of well w/ Magnet BHA. - PJSM with rig crew and fisherman. Rig down pwr swivel. Pull 34 jts out to be close to liner top. Tie rig ahead to double fast. Continue tripping out of well with the Globe basket BHA. Halliburton+ is on location-2000 pm. PJSM- spot Halliburton equipment on location while rig crew continues tripping out of well. Out of well with Globe basket. Break out and lay down RBS fishing tools.140 stands of 2-3/8" Ph-6 5.95 tbng in Derrick. - PJSM with rig crew and Halliburton logging crew. Rig down floor. Nipple down annular and Spool from 7-1/16" 10k to 7-1/16"5k. Rig up lubricator and pick up tools. Frac valve is closed. Blind rams are shut and locked.Gauge ring and Junk basket are loaded on tools for 7" 29# casing. - Prepare to run back in well w/ 3.5" OD magnet and BHA. BHA as follows- PU 3 ?? magnet 2 3/8 Reg (3 1/8? OD x 1 ?? ID x 1.26?). TIH with Bit sub 2 3/8 REG (3 1/8" OD x 1 1/4" ID x 1.16'), Bumper Sub 2 3/8 REG (3 1/8" OD x 1" ID x 8.01'), Jars 2 3/8" REG (3 1/8" x 1" x 10.83'), XO Sub 2 3/8" PH6 x 2 3/8 REG (2 7/8" OD x 1" ID x 1.28', and 2 3/8" 5.95# PH6 P110 tbg. 0315-at liner top. Tie back rig. Tagged 1st sleeve lightly 2pts down @9830'. 4' in on jt 316.
Daily Cost: $0
Cumulative Cost: $747,793

4/4/2013 Day: 17 **Completion**

MWS #731 on 4/4/2013 - Pressure test Lubricator. Make 4 junk basket runs recovering rubber. Rih with Multi finger caliper tool Log from 9210 to 1000' - PJSM with rig crew and logging crew. Rih w/ logging tool.. Found 4 anomilies in casing see pictures. The depth reference is on the left side of log.2255pm-running Caliper log-3800? in 7? 29# casing - Operations suspended until daylight. - JSA and safety meeting with rig crew, WL crew, and pressure tester. Torque lubricator studs. Test lubricator against 7?10K frac valve to 8000 psig for 5 minutes, OK. RIH with 4.83? gauge ring (10K lubricator is 5 1/8? ID) and junk basket to

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top of liner at 8654? WLM. POH. Double handful of soft, pliable rubber recovered in junk basket. PU same tool. Test lubricator to 8000 psig for 5 minutes, OK. Logging tool stuck in lubricator. LD lubricator to get tool freed. PU 5.91? drift. NU lubricator. RIH to liner top at 8655?. POH. No recovery. PU 3.68? gauge ring. RIH to 9210?(48 degree slope), quit going down. POH. No recovery in junk basket. LD gauge rings. PU 40 arm caliper logging tool. Calibrate tool. RIH.
Daily Cost: $0
Cumulative Cost: $784,065

4/5/2013 Day: 18 **Completion**

MWS #731 on 4/5/2013 - Run Caliper log and CBL log. RIH w/ RBP to liner top. - Make up 4-1/2" rbp and x-over sub. Begin tripping in well. Rih w/ 275 jts to be @ 8567.10 with KB correction and BHA added. - PJSM with rig crew and Weatherford tester.Nipple up 7" 10k X 7" 5K spool attached to annular. Pressure test Flange as per NFX testing guide lines. Finished with test. RDMO tester and prepare to trip in well with Halliburton RBP. - Continue logging from 1000' to surface with multi finger caliper log. 0115am. Out of the hole with caliper log. Break out caliper tools. Make up CBL logging tool. Calibrate tool. - Begin rih w/ bond log tools. On depth. Begin logging 1st 1000' up above liner top with 0 psi on well and hole full of KCL fluid. - Run a CAST-M, magnetic thickness tool. RIH to liner top and log 1000' up with 0 psi on well. Run back down to liner top and apply 1500psi on well. Log to surface at 15 ft/minute. TOC at 210?. LD lubricator and ND WLBOP.
Daily Cost: $0
Cumulative Cost: $853,208

4/6/2013 Day: 19 **Completion**

MWS #731 on 4/6/2013 - Rih and set RBP. Pressure test casing. Circ 2 bottoms up. Retrieve RBP and trip out of the well laying down the work string. Rig down rig and equipment. - Rig down pulling unit and move piperacks and skate. - Continue tripping out of well with RBP for 4.5" casing. Out of well w/ tbng and BHA> - PJSM with rig crew. Crew change. Layed down 20 jts. Shut down for 3 hrsDue to rig incident. Conducted investigation with rig pusher. - Service rig and wait on orders.Halliburton and Weatherford tester will be back on location at 0700 this morning. - Circulate 3 bottoms up down csg at 1900 psig and 3 bpm with 2% KCl water. - Set RBP. J off RBP and PU 10?. Close upper pipe rams. Pressure test csg to 8900 psig for 30 minutes, no bleed off. BO pressure - JSA and safety meeting. Wait on orders. - J on and release RBP. LD 240 jts 2 3/8? 5.95# PH6 P110 tbg.
Daily Cost: $0
Cumulative Cost: $886,509

4/7/2013 Day: 20 **Completion**

MWS #731 on 4/7/2013 - Rig down BOP stack Nipple up 4-1/16" frac stack and test. Rig down 4-1/16" frac stack. Nipple up 7" frac stack and test. Spot in frac tanks and begin filling with water. Spot sand cans and begin filling. - Continue testing frac tree as per NFX guidelines. Continue filling frac water and hauling frac sand. - Rig down Knight closing unit and roll up hoses. Spot and rig up Weatherford crane. Rig down Knight BOP stack to Cameron frac valve. Install 4-1/2" hanger with 2 way check for testing and lock pins on well head. ND Cameron frac valve. Nipple up Cameron 7" 10k X 4-1/16"10k spool. Nipple up 10k 4-1/16" Lower master hydraulic frac valve (HCR). Nipple up 10K 4-1/16" upper master manual frac valve. Nipple up 10K 4-1/16" flowcross with dual, double 2-1/16" outlets. Nipple up 10K 4-1/16" Crown manual frac valve. Test stack as per NFX frac stack testing guidelines. Rig in FMC/Pure Energy flowback equipment. Begin spotting frac tanks on location. - JSA and safety meeting.

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Move off WOR. Finish spotting frac tanks. Spot in sand cans. Test frac tree. Move 2 3/8? WS to Runners yard. Received word to change from 10K 4 1/16? tree to a 10K 7? tree. ND frac tree. NU 7? 10K frac stack. Test frac stack.
Daily Cost: $0
Cumulative Cost: $914,676

4/8/2013 Day: 21 **Completion**

Rigless on 4/8/2013 - Finish heating water 14 frac tanks on location & 36 tanks above location . Finish testing flow back line, sand trap,slug catcher, & manifold . MIRU frac crew and rig up. - All frac Equipment is rigged up and ready for a 6am pump time. - Continue to heat frac tanks with superheater. Continue to rig in flowback. Flowback is rigged in. - Superheaters are heating frac tanks. Waiting on tester to come from Vernal to test flowback lines. FMC is testing flowback lines, manifold , sand trap, slug catcher. Test all using Newfield guidelines.Baker is on location RU frac equip. Installed goat head on to frac stack. Completed testing frac stack & flowback line. - Con't RU frac Equip.
Daily Cost: $0
Cumulative Cost: $956,292

4/9/2013 Day: 22 **Completion**

Rigless on 4/9/2013 - Frac 20stage frac w/ sliding sleeves w/ ball launch machine , and ball catcher. - Stage#3-242 psi on N2 regulator, 1,853 psi on bottle, Pop off set at 8700 psi. Pressure tested at 9500psi. Plugged of the hopper screens with wet sand at end of 1 ppa 30/50. Cut rate to give time to clear, pulled top screen and was able to continue. Average Horse power-5160 Change out frac pump. - stage #1 236 psi on N2 regulator, 2175 psi on bottle, Pop off set at 8700 psi. Overall good job execution.Ball Seat Stage Pressures and Rate: 7278 psi @ 12 bpm , 5051 psi Pressure before Seating , 5397 psi Pressure after Seating Average Horsepower-4134. Stage #2 248 psi on N2 regulator, 1,940 psi on bottle, Pop off set at 8700 psi. Pressure tested at 9500psi. 248 psi on N2 regulator, 1,940 psi on bottle, Pop off set at 8700 psi. Pressure tested at 9500psi. Staged to 100 Mesh stage but screw wouldn?t come on, operator error. Staged back to resume schedule. Had the Scale sorb screw lock up on 0.5 ppa 30/50 stage, able to free up.Lost packing on a pump prior to flush, lined out the rate at 30 bpm to launch ball and displace.Lost blender tub on flush swapping valves back from the acid transport. Good job execution by the crew. Ball Seat Stage Pressures and Rate: 6827 psi @ 12 bpm , 5315 psi Pressure before Seating , 5626 psi Pressure after Seating. Average Horsepower-5746 - Finish heating frac tanks at water depot. Waiting on Baker Hughes to prime up and test fro 6am pump time. - Baker frac crew on location starting equipment and preparing for frac. - Tried to prime up with blender for test. Blender broke down. Rig out and wait on new blender.blender is on location swapping Chemical will RU blender Move pump truck back in place. Start Pressure testing frac lines within the hour. 236 psi on N2 regulator, 2175 psi on bottle, Pop off set at 8700 psi. Pressure tested at 9500psi. Lost discharge pump, had to bring another blender from town. Transferred adds between Blenders. Hoses to accumulator not correct to HCR, SD to verify positioning. Swapped out crews during this time too. Lost pump while pumping acid, took off line & made rate up with rest of pumps.
Daily Cost: $0
Cumulative Cost: $1,066,315

4/10/2013 Day: 23 **Completion**

Rigless on 4/10/2013 - Frac stages 4 thru 18 - Stage -18 Pop off set at 8,700 psi. Pressure tested at 9400psi.Ball seated approx 80 bbls early just as dropping rate. Proceeded with

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job.Pumped approx 15,000 lbs extra on this stage to use up some extra prop. Inline denso started to drift on 3 ppa stage. Had a good reference at the start of the job. -Ball Seat Stage Pressures and Rate: 7039 psi @ 28.6 bpm , 6217 psi Pressure before Seating , 5637 psi Pressure after Seating GW-3LDF-4.4% (12.5), XLW-10A-6.2% (7), FRW-20-28.3% (2), Scalesorb 7-3.8% (9.9), , Scaletrol 720-9.2% (1) CRB-LT-4.4% (5.1), NE-900-3.7% (5.5) Enzyme G HT III-5.4% (2.8), ClayCare-3.7% (2.7), Alpha 452-9.2% (1.7) Average horsepower-4896. PUMPED: 143,838 LBS O - Rig in new pump. Retested popoff. - Stage 16- 220 psi on N2 regulator, 1,514 psi on bottle, Pop off set at 8,700 psi. Pressure tested at 9400psi Had to feed the Scalesorb in the blender tub, screw bound up during job. Had density drop staging to 6 ppa, swapped gates. Ball Seat Stage Pressures and Rate: 7837 psi @ 12.6 bpm , 5740 psi Pressure before Seating , 5587 psi Pressure after Seating.GW-3LDF-3.2% (8.6), XLW-10A-2.4% (2.6), FRW-20-27.3% (2.6) Enzyme G HT III-18.8% (9), ClayCare-10.6% (6.7), Alpha 452-8.5% (1.3) Average Horsepower-5228. PUMPED: 129,306 LBS OF 1-6 PPG 30/50 S - Stage #14- 220 psi on N2 regulator, 1715 psi on bottle, Pop off set at 8,700 psi. Pressure tested at 9500psi. Good job, able to place with no problems. Seated ball for stage 15, came off to mix Enzyme breaker and check Sand & Water. Continue to have adds off greater than 10%, trouble strapping the transport. Ball Seat Stage Pressures and Rate: 7425 psi @ 13.6 bpm , 5615 psi Pressure before Seating , 5625 psi Pressure after Seating. GW-3LDF-6.5% (17.3), XLW-10A-9.3% (9.9), Scaletrol 720-13.1% (1.2) CRB-LT-4.7% (4), Enzyme G HT III-10.5% (4.1), ClayCare-15.3% (9.4), Alpha 452-30.4% (4.7) Average Horsepower-5162. Pumped 129,812# of 30/50 sand. Stage 15-220 psi on N2 regulator, 1,586 psi on bottle, Pop off set at 8,700 psi. Pressure tested at 9400psi.Good job execution by the crew. Ball Seat Stage Pressures and Rate: 7345 psi @ 12.4 bpm , 5510 psi Pressure before Seating , 5340 psi Pressure after Seating.GW-3LDF-2.2% (5.7), XLW-10A-6.9% (7.3), FRW-20-51.7% (2.4), Scaletrol 720-12.2% (1.1) CRB-LT-5.6% (4.7), NE-900-2.9% (3.5) Enzyme G HT III-13.3% (5.2), Alpha 452-51.5% (7.8) - Pumping stage #13 1. 220 psi on N2 regulator, 1935 psi on bottle, Pop off set at 8,700 psi. Pressure tested at 9500psi. Good job overall, no problems placing job. Shifted sleeve for s11 then shutdown to work on pumps. Had a few adds off greater than 10%, will re-bucket test LA pumps while down working on Frac Pumps. Ball Seat Stage Pressures and Rate: 7260 psi @ 13.6 bpm , 5485 psi Pressure before Seating , 5695 psi Pressure after Seating GW-3LDF-6.8% (17.8), XLW-10A-4.7% (4.9), Scaletrol 720-25.1% (2.3) CRB-LT-5.2% (4.4), NE-900-7.7% (9.7) Enzyme G HT III-20.3% (4.3), ClayCare-3.7% (2.3), Alpha 452-42.2% (6.5) Aver5546. Pumped 129,282 # of sand. - Pumping stage #12 1. 220 psi on N2 regulator, 1840 psi on bottle, Pop off set at 8,700 psi. Pressure tested at 9500psi. Had pump jacking during the 3.0ppg sand stage, dropped a gear and made rate up with rest of pumps . Had confusion in van, reduced rate just before launching ball. Launched ball an brought rate back up. No other issues, overall good effort by crew . Ball Seat Stage Pressures and Rate: 7560 psi @ 13.6 bpm , 5680 psi Pressure before Seating , 5980 psi Pressure after Seating. - Pumping stage #11 220 psi on N2 regulator, 1880 psi on bottle, Pop off set at 8,700 psi. Pressure tested at 9500psi. Able to get back into job and place with no problems. Still had adds off greater than 10%, small volumes, but were much closer after bucket testing.Ball Seat Stage Pressures and Rate: 7120 psi @ 13.6 bpm. 5270 psi Pressure before Seating , 5580 psi Pressure after Seating - working on pumps that were broke down before starting stage #11 - pump stage #10 220 psi on N2 regulator, 1935 psi on bottle, Pop off set at 8,700 psi. Pressure tested to 9500psi.Good job overall, no problems placing job.Shifted sleeve for s11 then shutdown to work on pumps. Had a few adds off greater than 10%, will re-bucket test LA pumps while down working on Frac Pumps. Ball Seat Stage Pressures and Rate: 7260 psi @ 13.6 bpm , 5485 psi Pressure before Seating , 5695 psi Pressure after Seating - pump stage #9 220 psi on N2 regulator, 1965 psi on bottle, Pop off set at 8,700 psi. Pressure tested at 9500psi. Had drop in prop conc during the 5ppg sand stage, wet sand. Ball Seat Stage Pressures and Rate: 7295 psi @ 13.6 bpm , 5400 psi Pressure before Seating , 5830 psi Pressure after Seating. No other issues, overall good job. - Pump stage #8 220 psi on N2 regulator, 1970 psi on bottle, Pop off set at 8,700 psi. Pressure tested at 9500psi. Did not see any ball action before starting main body of job. No problems placing stage 8, overall good job. Saw good ball action for stage 9. - Pumping stage #7 220 psi on N2 regulator, 2035 psi on bottle, Pop off set at 8,650

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psi. Pressure tested at 9500psi. Overall good job, pumped per design.Had several adds that were off, appears to be consistent strapping issue. Did not see any ball action to shift s8, shut down to check lines for ball. Did not find ball in line. Surged the well and took rate to 20 bpm to try to seat ball. Did not see any ball action, dropped end ball. - Swap out frac pumps. Pressure test pump. - Pump stage-6 220 psi on N2 regulator, 1,524 psi on bottle, Pop off set at 8,640 psi. Pressure tested at 9600psi. Lost blender suction on 2 ppa. Shutdown quickly and got back. No apparent reason for losing the tub. Lost a pump on 4 ppa, made up best possible rate with remaining pumps. Had another pump with valve problem, rate ran rough until end of job. Lost some density on 6 ppa stage, had wet sand go through the hopper. Able to make it to the end of the job. Shift sleeve for s7, come off line to work on pumps. Ball Seat Stage Pressures and Rate: 7418 psi @ 9.4 bpm , 5165 psi Pressure before Seating , 5811 psi Pressure after Seating GW-3LDF-3.5% (9.4), XLW-10A-3.1% (3.4), CRB-LT-2.8% (2.4), NE-900-20.8% (21.9) Average Horsepower-4169. Pumped 129,938# of 30/50 - Begin fracing stage 4. 220 psi on N2 regulator, 1,670 psi on bottle, Pop off set at 8,640 psi. Pressure tested at 9600psi. Shut down after opening s4, swap discharge hose and rig out two pumps. Pressure test pop off. Had to drop a little rate with XL fluid on formation. Pressure lined out for remainder of job. Good job execution. GW-3LDF-3.2% (13.7), XLW-10A-3.7% (6.3), FRW-20-58.8% (7.1), Scaletrol 720-20.6% (2.9) CRB-LT-8.5% (11.2), NE-900-5.3% (8.4) Ball Seat Stage Pressures and Rate: 7562 psi @ 12 bpm , 5440 psi Pressure before Seating , 6233 psi Pressure after Seating ClayCare-18.8% (17.4), Alpha 452-17.1% (3.9) Average Horsepower-5,655. Pumped 131,060# of 300 sand. Stage 5-220 psi on N2 regulator, 1,576 psi on bottle, Pop off set at 8,640 psi. Pressure tested at 9600psi. Had a drop in prop con staginging into 5 ppa stage, swapping gates. Had a rate drop before dropping the ball, operator error. Good job execution by the crew. Ball Seat Stage Pressures and Rate: 7307 psi @ 12 bpm , 5371 psi Pressure before Seating , 5982 psi Pressure after Seating FRW-20-9.2% (1), CRB-LT-3.5% (3), NE-900-23.3% (24.5) Average horse power-5024. Pumped 135,600 of 30/50 sand - Stage 17-220 psi on N2 regulator, 1,453 psi on bottle, Pop off set at 8,700 psi. Pressure tested at 9400psi Flush well to drop s18 ball through WH.Good job execution by the crew. XLW-10A-7.5% (8.1), FRW-20-73.4% (5.5), Scaletrol 720-18.1% (2) CRB-LT-8.1% (9), NE-900-2.4% (3.6) Average Horsepower-5303. PUMPED: 131,604 LBS OF 1-6 PPG 30/50 Sa220 psi on N2 regulator, 1,383 psi on bottle.

Daily Cost: $0

Cumulative Cost: $2,154,393

4/11/2013 Day: 24 **Completion**

Rigless on 4/11/2013 - Finish frac. Rig out frac crew. Rig in wireline. Set 2 kill plugs. ND frac stack. NU BOP stack and test. - Rig down wireline. Nipple down frac stack and load out. Spot BOP skids over by wellhead and prepare to nipple up Knight BOP stack. Nipple up 10k Double bop stack with flowcross. Nipple up 10K BOP single with Xover flange Back to 5K and annular. Begin pressure testing stack as per NFX testing guidelines. Bottom BOP has Blind rams installed. Other 2 BOPs loaded with 2-3/8" rams for drillout. - RD baker frac equip & sand masters . Held safety meeting w/ JW wireline . MIRU JW wire line RU Lubricator test to 5000psi. RIH w/ 3.75 gauge ring. POOH w/ gauge . RIH w/ 4.5 10k comp BP set @8770' - 8720' RD JW wireline . ND FMC 7 1/16 10k frac stack. RU knight oil tool 7 1/16" 10k BOP stack. Weatherford on location to test BOP stack. Knight oil tools on location to NU BOP.Rock water is consoledating water in frac tanks. Above location. - Repair equipment.problems with Chemical pumps - waiting for parts for maifold to flow back 3 wheel choke valves washed out . New ones coming from vernal. Finished repair to manifold - Frac stage 19- then stage 20- pumped pad and 1# sand. Staged into 2#. As soon as 1# hit formation screened out. Flowing back 500 bbls before trying to pump again. Ball is miched for sleeve 20 on the desk. - Atempt to flow back well 300 bbls pressure bled down to 250psi decieded to make another attempt to frac into well stage 20 made 3 attempts well pressured up to 8400 psi each time engineer called it .220 psi on N2 regulator, 2.017 psi on bottle, Pop off set at 8,705 psi. Pressure tested at 9,160 psi. Saw higher treating pressure with sleeve open. Started into XL, ran a small XL

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pad and went to an extended 1 ppa stage. Kept getting small breaks and grabbing rate where possible. Well locked up with XL fluid on formation. Left approx 19,000 lbs in the pipe, flowed well back, did not get any balls back. Could not establish rate after flowback, came off and flowed back 2nd time. Only able to get 180bbls back before well died. Saw small break in pressure at start of 3rd attempt, but pressure increased shortly after. Attempted to pump on well 2 more times but were unable to establish rate. Decision was made to call job and rig down. Good job by crew working through well issues. Ball Seat Stage Pressures and Rate: 7774 psi @ 12 bpm , 5420 psi Pressure before Seating , 7120 psi Pressure Seating
Daily Cost: $0
Cumulative Cost: $2,335,043

4/12/2013 Day: 25 **Completion**

Rigless on 4/12/2013 - Finish frac. Rig out frac crew. Rig in wireline. Set 2 kill plugs. ND frac stack. NU BOP stack and test. - RU work floor & stairs . Measure drill out BHA 3.75 four blade mill, 2 7/8 bit sub,1 6' 2 3/8" PH6 pup jt, 2 7/8 double flapper sub,1 jt 2 3/8 PH 6 , 2 3/8 RN nipple, 157 jts 2-3/8? 5.95# PH6 P110 tbg, 2 3/8 R nipple, 47 jts 2-3/8? 5.95# PH6 P110 tbg, (6,119' in hole) - Pressure testing BOPs as per NFX BOP testing guidelines. Rig up Flowback line to Flow cross. Pressure test to 10,000 psi as per NFX guidelines. - Wait on Baker to pull sand cans out and Dalbo to pull out 3 frac tanks out of the way before rig arrives. - Baker is moving sand kings off location , moving in hydro walk & tbg racks , Runners on location off loading 466 Jts 2 3/8 PH6 tbg . Qt is cleaning & drifting 2 3/8 PH6 tbg. MIRU work over Rig . Guy out
Daily Cost: $0
Cumulative Cost: $2,464,780

4/13/2013 Day: 26 **Completion**

Rigless on 4/13/2013 - Continue RIH of BHA, drill out plugs, drill out sleeves, - RIH to tag #5 sleeve ball seat, jt 409 Tbg WT 56,000#, 61,000# ?, 55,000# ? Sleeve #5 tag @ 12,700? establish pump rate, 2.2 bbls/min 4,750 psi @ WH, 2,900 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 12 min, 2.2 bbls in, x 3.7 bbls out, pump 10 bbl sweep circ. - RIH to tag #10 sleeve ball seat, jt 377 Tbg WT 56,000#, 60,000# ?, 55,000# ? Sleeve # 10 tag @ 11,726? establish pump rate, 2.2 bbls/min 4,700 psi @ WH, 2,900 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 5 min, 2.2 bbls in, x 3.7 bbls out, pump 10 bbl sweep circ. RIH to tag #9 sleeve ball seat, jt 384 Tbg WT 56,000#, 60,000# ?, 52,000# ? Sleeve # 9 tag @ 11,923? establish pump rate, 2.2 bbls/min 4,750 psi @ WH, 2,900 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 8 min, 2.2 bbls in, x 3.6 bbls out, pump 10 bbl sweep circ. RIH to tag #8 sleeve ball seat, jt 390 Tbg WT 56,000#, 60,000# ?, 54,000# ? Sleeve # 8 tag @ 12,113? establish pump rate, 2.2 bbls/min 4,750 psi @ WH, 2,900 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 5 min, 2.2 bbls in, x 3.7 bbls out, pump 10 bbl sweep circ. RIH to tag #7 sleeve ball seat, jt 396 Tbg WT 56,000#, 60,000# ?, 54,000# ? Sleeve #7 tag @ 12,313? establish pump rate, 2.3 bbls/min 4,700 psi @ WH, 2,950 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 15 min, 2.3 bbls in, x 3.7 bbls out, pump 10 bbl sweep circ. RIH to tag #6 sleeve ball seat, jt 403 Tbg WT 56,000#, 61,000# ?, 55,000# ? Sleeve #6 tag @ 12,514? establish pump rate, 2.2 bbls/min 4,770 psi @ WH, 2,950 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 5 min, 2.2 bbls in, x 3.6 bbls out, pump 10 bbl sweep circ. - RIH to tag #15 sleeve ball seat, jt 348 Tbg WT 56,000#, 60,000# ?, 54,000# ? Sleeve # 15 tag @ 10,803? establish pump rate, 2.2 bbls/min 4,750 psi @ WH, 3,300 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 13 min, 2.2 bbls in, x 3.6 bbls out, pump 10 bbl sweep circ. RIH to tag #14 sleeve ball seat, jt 354 Tbg WT 56,000#, 60,000# ?, 54,000# ?, Sleeve # 14 tag @ 11,001? establish pump rate, 2.2 bbls/min 4,750 psi @ WH,2,900 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 32 min, 3.2 bbls in, x 3.2 bbls out, pump 10 bbl sweep circ. RIH to tag #13

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sleeve ball seat, jt 360 Tbg WT 56,000#, 60,000# ?, 54,000# ? Sleeve # 13 tag @ 11,188? establish pump rate, 2.2 bbls/min 4,750 psi @ WH, 2,900 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 22 min, 2.2 bbls in, x 3.6 bbls out, pump 10 bbl sweep circ. RIH to tag #12 sleeve ball seat, jt 366 Tbg WT 56,000#, 60,000# ?, 54,000# ? Sleeve # 12 tag @ 11,383? establish pump rate, 2.2 bbls/min 4,750 psi @ WH, 2,900 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 13 min, 2.2 bbls in, x 3.7 bbls out, pump 10 bbl sweep circ. RIH to tag #11 sleeve ball seat, jt 372 Tbg WT 56,000#, 60,000# ?, 54,000# ? Sleeve # 11 tag @ 11,574? establish pump rate, 2.3 bbls/min 4,700 psi @ WH, 2,900 psi @ choke 20/64, Swivel rpm 110-120 WOB 6-10k, drill plug in 32 min, 2.2 bbls in, x 3.6 bbls out, pump 10 bbl sweep circ. - RIH to sleeve# 15. Tag sleeve #15 @10805 wt up 60K wt down 54K. Neutal wgt-58K Sleeve drilled in 18 min WOB-4000 pump rate 2.1 bpm @4480 psi. returns 4.2 BPM @ 2900 psi. 24 choke. Jts in 348. Rih to sleeve #14. tag sleeve# 14.@ 11004'. WT up-K DWN-wt-K Neutal wgt-K sleeve drilled in min WOB-4000 pump rate 2.1 bpm @4880 psi. returns 4.2 BPM @ 2900 psi. 16 choke. Jts in 354. - Held safety meeting w/ rig crew Reviewed JSA . RU power swivel. Start Circulating well to set Back Pressure. Start drilling thru first Comp BP @8720' Clean up after drilling thru Plug .PU 2 jts 2 3/8" PH -6 taged 25' out . Started drilling out 2nd plug @ 8770' pump pressure 4000psi 3.5 bbls min flow back 16 choke 1100psi. 3.5 bbls min. - Tag sleeve#18 @ 10221' 66k wt up 62K wt dwn 64K Neutral. Sleeve drilled up in 25 min Wom-4000 lbs pump rate 2.5 bpm @ 4100 psi Returns 2.6 bpm @ 2900 psi. 23 choke.JTS in 323. Tag sleeve# 17 @ 10417 wt up-60K wt down-56K nt wgt-52K. Sleeve drilled in 17min. WOB- 4000. Pump rate-3.1 bpm @ 4500 psi. returns 4.5 bpm @ 2700 psi. 22 choke. JTs in 335. - Tie back blocks, PUMU swivel, break circ and pressurize system?s surface equipment before drilling out plug to live well. - Continue RIH of BHA 3.75 four blade mill, 2 7/8 bit sub,1 6' 2 3/8" PH6 pup jt, 2 7/8 double flapper sub,1 jt 2 3/8 PH 6 , 2 3/8 RN nipple, 156 jts 2-3/8? 5.95# PH6 P110 tbg, 2 3/8 R nipple, 124 jts 2-3/8? 5.95# PH6 P110 tbg, 281 jts and BHA 8,764' ? tagged kill plug #2 - RIH w/ 2 3/8 tbg 37 jts to jt 316 to first sleeve#20 @ 9825' started drilling out sleeve ,66k upwt 62k wt down 64k drill time 20min 3000psi 3bbls min w/ 2600psi back pressure on choke manifold. 3bbls to tank. Cir down 5' clean . RIH w/ 7 jts 2 3/8" PH-6 jt #322 to sleeve #19 @10024' Drill out sleeve w/Pump rate @ 3000psi 3bbls min w/ 2700psi back preesure 24choke 3bbls to flow back tanks. - RIH to sleeve# 16. Tag sleeve #16 @10609 wt up 60K wt down 54K. Neutal wgt-58K Sleeve drilled in 12 min WOB-4000 pump rate 3.0 bpm @4880 psi. returns 4.2 BPM @ 2900 psi. 16 choke. Jts in 341. Break thru pressure 4600-2650psi

Daily Cost: $0

Cumulative Cost: $2,491,392

4/14/2013 Day: 27 **Completion**

Rigless on 4/14/2013 - Drill out frac sleeves 1-20 Cir well clean POOH w/ drill string. LD & take picture of BHA mill. - Update Tomlin 4-6-3-1WH 08:00 AM Current Operations: Held Safety meeting w/ day light Crew Reviewed JSA .Start Snubbing out of the hole w/ 2 3/8 PH-6 tbg 170jts. Plan forward: RD snubbing Unit . RU JW wire line .Hold safety meeting w/ JW wireline Review JSA. RU Lubricator test Lubricator to 5000 psi. RIH w/ gauge ring for 7" 29# CSG. POOH w/ gauge ring. RIH w/ Wire line set 7" 29# 10K hornet Packer, BHA 2 7/8" 6.5# X4 L-80 pup jt ,2 7/8" XN nipple w/2.205" ID,2 7/8" 6.5# X4 L-80 pup jt, 10K ceramic burst disc, wireline re-entry Guide. - Establish pump rate, 2.5 bbls/min 4,700 psi @ WH, 2,900 psi @ choke 20/64, Swivel rpm 110-120, Circulate bottoms up (900 bbls) 2.5 times casing volume at 3.0 bbls in, x 4.5 bbls out. Getting back wax parrifin slowed down pump pressure to 2.7bbls. 4600psi .choke set @18/64, w/ 2900psi 3.5 bbls to flow back tanks. Move oil to prod tank #3. Choke set down to 10/64 w/ 2900psi holding bbl to bbl flowing back to tanks. - Swivel out first 3 jts 2 3/8" PH -6 tbg LD on tbg racks . RO power swivel . Est SICP @ 2500psi. POOH w/ 2 3/8" PH -6 tbg LD 155 jts 2 3/8" PH-6 .RU Pump to Circulate 135bbls 3bbl min 4000psi. Flow back 3bbls min @2700psi @ TOL 8655' SICP @2700 psi building to 2900 psi .Double Rig back .POOH w/ 109 2 3/8" PH-6 jts LD all Land on tbg hanger . RU snubbing unit when balanced point is reached @5294' jt# 170. Equalized well. Weatherford washed

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hanger bowl. Landed tbg hanger. Cameron set hanger pins. Tbg landed with 170 jts @5294'. - RD rig floor . ND hydril bag. RU snubbing unit.
Daily Cost: $0
Cumulative Cost: $2,591,941

4/15/2013 Day: 28 **Completion**

Rigless on 4/15/2013 - POOH w/ drill string. LD & take picture of BHA mill. - RU JW wire line .Hold safety meeting w/ JW wireline Review JSA. RU Lubricator test Lubricator to 5000 psi. RIH w/ gauge ring for 7" 29# CSG (6.00" OD). POOH w/ gauge ring. RIH w/ Wire line set 7" 29# 10K hornet Packer,BHA 2 7/8" 6.5# X4 L-80 pup jt ,2 7/8" XN nipple w/2.205" ID,2 7/8" 6.5# X4 L-80 pup jt, 10K ceramic burst disc, wireline re-entry Guide. Set Baker Hornet 7? packer @ 8,580? middle of second casing jt above 4.5 liner top, - Back to Snubbing out of the hole w/ 2 3/8 PH-6 tbg 170jts. RD snubbing Unit . RU work floor . - Testing snubbing unit. - Held Safety meeting w/ day light Crew Reviewed JSA .Start Snubbing out of the hole w/ 2 3/8 PH-6 tbg 170jts. RD snubbing Unit . RU JW wire line .Hold safety meeting w/ JW wireline Review JSA. RU Lubricator test Lubricator to 5000 psi. RIH w/ gauge ring for 7" 29# CSG. POOH w/ gauge ring. RIH w/ Wire line set 7" 29# 10K hornet Packer,BHA 2 7/8" 6.5# X4 L-80 pup jt ,2 7/8" XN nipple w/2.205" ID,2 7/8" 6.5# X4 L-80 pup jt, 10K ceramic burst disc,wireline re-entry Guide. - Equalize stack and Cameron hand backed out hanger pins, Pull tbg hanger and 2-3/8? 5.95# PH6 P110 tbg to slips, Remove Hanger. Cameron Pulled two way check valve. Install 2 3/8" TIW valve , waiting for daylight to snub tbg out .release Cameron tool hand. Sent in hanger to be rebuilt. - snubbing unit broke down had to remove & replace hydrualic hose . Picked up parts from vernal.
Daily Cost: $0
Cumulative Cost: $2,641,905

4/16/2013 Day: 29 **Completion**

Rigless on 4/16/2013 - RU JW wireline . RIH w/ wire line set Hornet packer & L-10 on off tool. **RESENDING TO CORRECT DETAIL ACT SUMMARY DATA** - RIH w/ on /off tool 7" 29# for hornet packer, 1 jt 2 7/8" L-80 6.5# eue 8rd tbg , 2 7/8 " X nipple , RIH w/ 2 7/8" L-80 6.5# 8rd tbg to surface. Space out well Circulate Packer fluid . Land on Ext neck tbg Hanger in 10,000lbs Compression. Tested tbng hanger 250 low and 10K high. For 30 min. Good test. Tested Annulus between 7? and 4-1/2? casing. 250 low and 5000 high for 30 min. Good test. Rig Mountain States work over rig down. - RDMO JW wireline. - Change 2 3/8" pipe rams to 2 7/8" pipe ram and add bag back to stack, test 7 1/16" 10K stack per Newfield procedure. 250 psi low, 5,000 psi high.
Daily Cost: $0
Cumulative Cost: $2,709,207

4/17/2013 Day: 30 **Completion**

Rigless on 4/17/2013 - Latch in to 7" hornet packer @8580' . RDMO .NU 10K Prod tree Pump out disc - Welder on location plumbing manifold to wellhead. Jessen electrical wiring up electrical should be finished with plumbing & elect within the hour - Wait on Welder to come to location and manifold wellhead and build flow lines. - Nipple down BOP stack and load out on hotshot to go back to Knight Oil tools yard. Nipple up production tree. NU 10K production tree with flow cross & test same to 250 psi low / 10,000 psi high. Pull 2 way check out of tbng hanger. RDMO tester. Release Cameron wellhead service tech. - wellhas been turned over to Production . Cleaning up location .Released all vender equip. - Turn well over to production group. Well opened up 3100psi. on 6/64 choke. Pure flowback RD sand trap, slug catcher, manifold, hard line. - Weatherford Pump off disc and 100bbls or 2 tbg volumes. Pumped up to

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4800psi disc broke & went down to 3100psi RD Weatherford pump.
Daily Cost: $0
Cumulative Cost: $2,817,170

Pertinent Files: Go to File List

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Amended

Form 3160-4
(August 2007)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB NO. 1004-0137
Expires: July 31, 2010

WELL COMPLETION OR RECOMPLETION REPORT AND LOG

5. Lease Serial No.: PATENTED (FEE)

1a. Type of Well: [x] Oil Well [ ] Gas Well [ ] Dry [ ] Other
b. Type of Completion: [x] New Well [ ] Work Over [ ] Deepen [ ] Plug Back [ ] Diff. Resvr.,
Other: _____

6. If Indian, Allottee or Tribe Name

7. Unit or CA Agreement Name and No.

2. Name of Operator: NEWFIELD EXPLORATION COMPANY

8. Lease Name and Well No.: TOMLIN 4-6-3-1WH

3. Address: 1401 17TH ST. SUITE 1000 DENVER, CO 80202

3a. Phone No. *(include area code)*: (435) 646-3721

9. AFI Well No.: 43-013-51861

4. Location of Well *(Report location clearly and in accordance with Federal requirements)**

At surface 453' FNL & 1161' FWL (NW/NW) SEC. 6, T3S, R1W

At top prod. interval reported below 823' FNL & 722' FWL (NW/NW) SEC. 6, T3S, R1W

At total depth 787' FSL & 803' FWL (SW/SW) SEC. 6, T3S, R1W

10. Field and Pool or Exploratory: WILDCAT

11. Sec., T., R., M., on Block and Survey or Area: SEC. 6, T3S, R1W

12. County or Parish: DUCHESNE

13. State: UT

14. Date Spudded: 01/17/2013

15. Date T.D. Reached: 03/16/2013

16. Date Completed: [ ] D & A [x] Ready to Prod. 04/17/2013

17. Elevations (DF, RKB, RT, GL)*: 5233' GL 5251' KB

18. Total Depth: MD 13600' TVD 9087'

19. Plug Back T.D.: MD 13583' TVD

20. Depth Bridge Plug Set: MD TVD

21. Type Electric & Other Mechanical Logs Run (Submit copy of each)
DUAL IND GRD, SP, COMP. DENSITY,COMP. NEUTRON,GR,CALIPER, CMT BOND

22. Was well cored? [x] No [ ] Yes (Submit analysis)
Was DST run? [x] No [ ] Yes (Submit report)
Directional Survey? [ ] No [x] Yes (Submit copy)

23. Casing and Liner Record *(Report all strings set in well)*

Hole Size	Size/Grade	Wt. (#/ft.)	Top (MD)	Bottom (MD)	Stage Cementer Depth	No. of Sks. & Type of Cement	Slurry Vol. (BBL)	Cement Top*	Amount Pulled
12-1/4"	9-5/8" J-55	36#	0	2506'		244 CLASS G			
						540 PREMLITE			
8-3/4"	7" HCP-110	29#	0	9580'		415 BONDCEM		Surface	
						770 VERSACM			
6-1/8"	4-1/2" P-110	13.5#	8648'	13579'		Swell Packers			

24. Tubing Record

Size	Depth Set (MD)	Packer Depth (MD)	Size	Depth Set (MD)	Packer Depth (MD)	Size	Depth Set (MD)	Packer Depth (MD)
2-7/8"	EOT@ 8752'	Hornet @ 8580'						

25. Producing Intervals

Formation	Top	Bottom
A) Green River - Utelandbutte	9822' MD	13482' MD
B)		
C)		
D)		

26. Perforation Record

Perforated Interval	Size	No. Holes	Perf. Status
9822-13482' MD	Sliding Slv	20	

27. Acid, Fracture, Treatment, Cement Squeeze, etc.

Depth Interval	Amount and Type of Material
9822-13482' MD	Frac w/ 2429000#s 30/50 white sand in 32634 bbls of Lightning 25 fluid, in 20 stages.

28. Production - Interval A

Date First Produced	Test Date	Hours Tested	Test Production	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
4/18/13	4/28/13	24	→	504	347	134			Sliding Sleeves

Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status
			→					PRODUCING

28a. Production - Interval B

Date First Produced	Test Date	Hours Tested	Test Production	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
			→						

Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status
			→					

*(See instructions and spaces for additional data on page 2)

28b. Production - Interval C

Date First Produced	Test Date	Hours Tested	Test Production →	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate →	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status	

28c. Production - Interval D

Date First Produced	Test Date	Hours Tested	Test Production →	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate →	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status	

29. Disposition of Gas *(Solid, used for fuel, vented, etc.)*

SOLD AND USED FOR FUEL

30. Summary of Porous Zones (Include Aquifers):

Show all important zones of porosity and contents thereof: Cored intervals and all drill-stem tests, including depth interval tested, cushion used, time tool open, flowing and shut-in pressures and recoveries.

31. Formation (Log) Markers

GEOLOGICAL MARKERS

Formation	Top	Bottom	Descriptions, Contents, etc.	Name	Top Meas. Depth
				GARDEN GULCH MRK	7119'
				POINT 3	7973'
				DOUGLAS CREEK	8384'
				B LIMESTONE	8794'
				CASTLE PEAK	9023'
				BASAL CARBONATE	9416'

32. Additional remarks (include plugging procedure):

33. Indicate which items have been attached by placing a check in the appropriate boxes:

- ☐ Electrical/Mechanical Logs (1 full set req'd.)
- ☐ Geologic Report
- ☐ DST Report
- ☑ Directional Survey
- ☐ Sundry Notice for plugging and cement verification
- ☐ Core Analysis
- ☑ Other: Drilling Daily Activity

34. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records (see attached instructions)*

Name *(please print)* Heather Calder Title Regulatory Technician

Signature Heather Calder Date 09/05/2014

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Continued on page 3)