

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 3

AMENDED REPORT

APPLICATION FOR PERMIT TO DRILL						1. WELL NAME and NUMBER Morrill 4-23-3-2WH								
2. TYPE OF WORK DRILL NEW WELL <input checked="" type="checkbox"/> REENTER P&A WELL <input type="checkbox"/> DEEPEN WELL <input type="checkbox"/>						3. FIELD OR WILDCAT WILDCAT								
4. TYPE OF WELL Oil Well Coalbed Methane Well: NO						5. UNIT or COMMUNITIZATION AGREEMENT NAME								
6. NAME OF OPERATOR NEWFIELD PRODUCTION COMPANY						7. OPERATOR PHONE 435 646-4825								
8. ADDRESS OF OPERATOR Rt 3 Box 3630 , Myton, UT, 84052						9. OPERATOR E-MAIL mcrozier@newfield.com								
10. MINERAL LEASE NUMBER (FEDERAL, INDIAN, OR STATE) Patented			11. MINERAL OWNERSHIP FEDERAL <input type="checkbox"/> INDIAN <input type="checkbox"/> STATE <input type="checkbox"/> FEE <input checked="" type="checkbox"/>			12. SURFACE OWNERSHIP FEDERAL <input type="checkbox"/> INDIAN <input type="checkbox"/> STATE <input type="checkbox"/> FEE <input checked="" type="checkbox"/>								
13. NAME OF SURFACE OWNER (if box 12 = 'fee') V. John and Debra C. Morrill & Jerry and Delia Antonetti						14. SURFACE OWNER PHONE (if box 12 = 'fee') 209-392-2280								
15. ADDRESS OF SURFACE OWNER (if box 12 = 'fee') 5464 Tip Top Road, Mariposa, CA 95338						16. SURFACE OWNER E-MAIL (if box 12 = 'fee')								
17. INDIAN ALLOTTEE OR TRIBE NAME (if box 12 = 'INDIAN')			18. INTEND TO COMMINGLE PRODUCTION FROM MULTIPLE FORMATIONS YES <input type="checkbox"/> (Submit Commingling Application) NO <input checked="" type="checkbox"/>			19. SLANT VERTICAL <input type="checkbox"/> DIRECTIONAL <input type="checkbox"/> HORIZONTAL <input checked="" type="checkbox"/>								
20. LOCATION OF WELL		FOOTAGES		QTR-QTR		SECTION		TOWNSHIP		RANGE		MERIDIAN		
LOCATION AT SURFACE		168 FNL 1423 FWL		NENW		23		3.0 S		2.0 W		U		
Top of Uppermost Producing Zone		660 FNL 660 FWL		NWNW		23		3.0 S		2.0 W		U		
At Total Depth		660 FSL 660 FWL		SWSW		23		3.0 S		2.0 W		U		
21. COUNTY DUCHESNE			22. DISTANCE TO NEAREST LEASE LINE (Feet) 68			23. NUMBER OF ACRES IN DRILLING UNIT 40								
			25. DISTANCE TO NEAREST WELL IN SAME POOL (Approved For Drilling or Completed) 1225			26. PROPOSED DEPTH MD: 13094 TVD: 8448								
27. ELEVATION - GROUND LEVEL 5271			28. BOND NUMBER B001834			29. SOURCE OF DRILLING WATER / WATER RIGHTS APPROVAL NUMBER IF APPLICABLE 437478								
Hole, Casing, and Cement Information														
String	Hole Size	Casing Size	Length	Weight	Grade & Thread	Max Mud Wt.	Cement		Sacks	Yield	Weight			
COND	17.5	14	0 - 60	37.0	H-40 ST&C	0.0	Class G		35	1.17	15.8			
SURF	12.25	9.625	0 - 2500	36.0	J-55 ST&C	8.3	Premium Lite High Strength		204	3.53	11.0			
							Class G		154	1.17	15.8			
I1	8.75	7	0 - 9111	26.0	P-110 Other	11.5	Premium Lite High Strength		259	3.53	11.0			
							50/50 Poz		392	1.24	14.3			
L1	6.125	4.5	8010 - 13094	13.5	P-110 Other	11.5	No Used		0	0.0	0.0			
ATTACHMENTS														
VERIFY THE FOLLOWING ARE ATTACHED IN ACCORDANCE WITH THE UTAH OIL AND GAS CONSERVATION GENERAL RULES														
<input checked="" type="checkbox"/> WELL PLAT OR MAP PREPARED BY LICENSED SURVEYOR OR ENGINEER						<input checked="" type="checkbox"/> COMPLETE DRILLING PLAN								
<input checked="" type="checkbox"/> AFFIDAVIT OF STATUS OF SURFACE OWNER AGREEMENT (IF FEE SURFACE)						<input type="checkbox"/> FORM 5. IF OPERATOR IS OTHER THAN THE LEASE OWNER								
<input checked="" type="checkbox"/> DIRECTIONAL SURVEY PLAN (IF DIRECTIONALLY OR HORIZONTALLY DRILLED)						<input checked="" type="checkbox"/> TOPOGRAPHICAL MAP								
NAME Don Hamilton				TITLE Permitting Agent				PHONE 435 719-2018						
SIGNATURE				DATE 04/26/2012				EMAIL starpoint@etv.net						
API NUMBER ASSIGNED 43013513900000				APPROVAL  Permit Manager										

Newfield Production Company
Morrill 4-23-3-2WH
Surface Hole Location: 168' FNL, 1423' FWL, Section 23, T3S, R2W
Bottom Hole Location: 660' FSL, 660' FWL, Section 23, T3S, R2W
Duchesne County, UT

Drilling Program

1. Formation Tops

Uinta	surface
Green River	3,508'
Garden Gulch member	6,296'
Wasatch	8,685'
Pilot Hole TD	8,935'
Lateral TD	8,448' TVD / 13,094' MD

2. Depth to Oil, Gas, Water, or Minerals

Base of moderately saline	1,060'	(water)
Green River	6,296' - 8,448'	(oil)

Note: The pilot hole will be drilled into the Wasatch formation for evaluation and targeting purposes only. The lateral will be drilled in the Green River formation.

3. Pressure Control

<u>Section</u>	<u>BOP Description</u>
Surface	12 1/4" diverter

Interm/Prod The BOP and related equipment shall meet the minimum requirements of Onshore Oil and Gas Order No. 2 for equipment and testing requirements, procedures, etc for a 5M system.

A 5M BOP system will consist of 2 ram preventers (double or two singles) and an annular preventer (see attached diagram). A choke manifold rated to at least 5,000 psi will be used.

4. Casing

Description	Interval		Weight (ppf)	Grade	Coup	Pore Press @ Shoe	MW @ Shoe	Frac Grad @ Shoe	Safety Factors		
	Top	Bottom (TVD/MD)							Burst	Collapse	Tension
Conductor 14	0'	60'	37	H-40	Weld	--	--	--	--	--	--
Surface 9 5/8	0'	2,500'	36	J-55	LTC	8.33	8.33	14	3,520 2.12	2,020 2.54	453,000 5.03
Intermediate 7	0'	8,598' 9,111'	26	P-110	BTC	11	11.5	15	9,960 2.45	6,210 1.45	853,000 3.60
Production 4 1/2	8,010'	8,448' 13,094'	13.5	P-110	BTC	11	11.5	--	12,410 3.11	10,670 2.54	422,000 6.15

Assumptions:

Surface casing MASP = (frac gradient + 1.0 ppg) - (gas gradient)

Intermediate casing MASP = (reservoir pressure) - (gas gradient)

Production casing MASP = (reservoir pressure) - (gas gradient)

All collapse calculations assume fully evacuated casing with a gas gradient

All tension calculations assume air weight of casing

Gas gradient = 0.1 psi/ft

All casing shall be new.

All casing strings shall have a minimum of 1 centralizer on each of the bottom 3 joints.

5. Cement

Job	Hole Size	Fill	Slurry Description	ft ³	OH excess	Weight (ppg)	Yield (ft ³ /sk)
				sacks			
Conductor	17 1/2	60'	Class G w/ 2% KCl + 0.25 lbs/sk Cello Flake	41	15%	15.8	1.17
				35			
Surface Lead	12 1/4	2,000'	Premium Lite II w/ 3% KCl + 10% bentonite	20	15%	11.0	3.53
				204			
Surface Tail	12 1/4	500'	Class G w/ 2% KCl + 0.25 lbs/sk Cello Flake	180	15%	15.8	1.17
				154			
Pilot Hole Plug Back	8 3/4	875'	50/50 Poz/Class G w/ 3% KCl + 2% bentonite	420	15%	14.3	1.24
				339			
Intermediate Lead	8 3/4	5,296'	Premium Lite II w/ 3% KCl + 10% bentonite	916	15%	11.0	3.53
				259			
Intermediate Tail	8 3/4	2,815'	50/50 Poz/Class G w/ 3% KCl + 2% bentonite	487	15%	14.3	1.24
				392			
Production	6 1/8	--	Liner will not be cemented. It will be isolated with a liner top packer.	--	--	--	--
				--			

The surface casing will be cemented to surface. In the event that cement does not reach surface during the primary cement job, a remedial job will be performed.

Actual cement volumes for the pilot hole plug back and the intermediate casing string will be calculated from an open hole caliper log, plus 15% excess.

The production liner will be left uncemented. Individual frac stages will be isolated with open hole packers. A liner top hanger and packer will be installed 50' above KOP.

6. Type and Characteristics of Proposed Circulating Medium

<u>Interval</u>	<u>Description</u>
-----------------	--------------------

Surface - 2,500'

An air and/or fresh water system will be utilized. If an air rig is used, the blooie line discharge may be less than 100' from the wellbore in order to minimize location size. The blooie line is not equipped with an automatic igniter. The air compressor may be located less than 100' from the well bore due to the low possibility of combustion with the air/dust mixture. Water will be on location to be used as kill fluid, if necessary.

2,500' - TD A water based mud system will be utilized. Hole stability may be improved with additions of KCl or a similar inhibitive substance. In order to control formation pressure the system will be weighted with additions of bentonite, and if conditions warrant, with barite.

Anticipated maximum mud weight is 11.5 ppg.

7. Logging, Coring, and Testing

Logging: A dual induction, gamma ray, and caliper log will be run from TD to the base of the surface casing. A compensated neutron/formation density log will be run from TD to the top of the Garden Gulch formation. A cement bond log will be run from PBSD to the cement top behind the production casing.

Cores: As deemed necessary.

DST: There are no DST's planned for this well.

8. Anticipated Abnormal Pressure or Temperature

Maximum anticipated bottomhole pressure will be approximately equal to total depth (feet) multiplied by a 0.57 psi/ft gradient.

$$8,448' \times 0.57 \text{ psi/ft} = 4832 \text{ psi}$$

No abnormal temperature is expected. No H₂S is expected.

9. Other Aspects

An 8-3/4" pilot hole will be drilled in order to determine the depth to the lateral target zone. The pilot hole will be logged, and then plugged back in preparation for horizontal operations. Directional tools will then be used to build to 92.15 degrees inclination. The 7" intermediate casing string will be set once the well is landed horizontally in the target zone.

The lateral will be drilled to the bottomhole location shown on the plat.

A liner with a system of open hole packers will be used to provide multi-stage frac isolation in the lateral. The top of the liner will be placed 50' above KOP and will be isolated with a liner top packer.

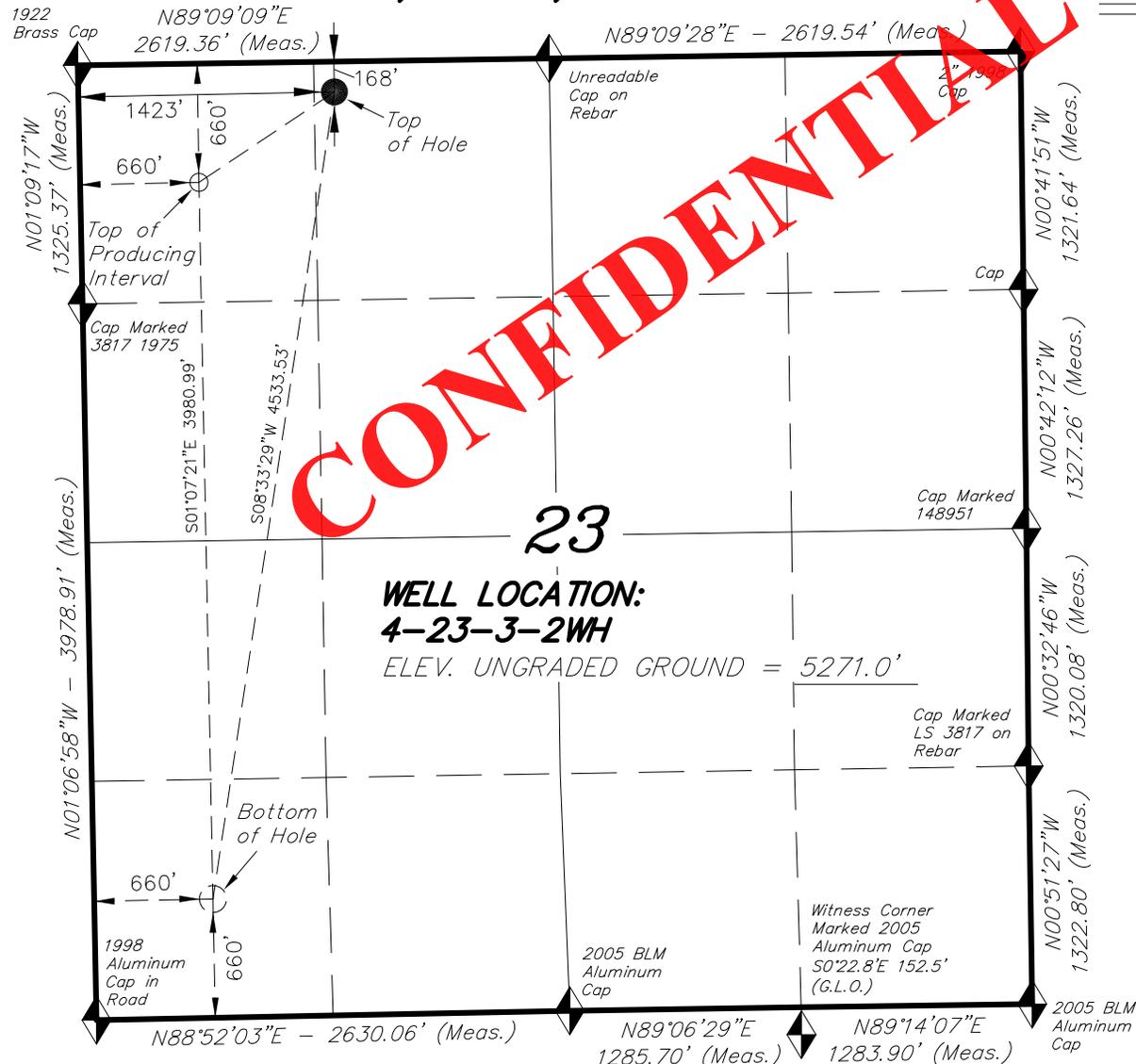
Newfield requests the following variances from Onshore Order #2:

- Variance from Onshore Order #2, III.E.1

Refer to Newfield Production Company Standard Operating Practices "Ute Tribal Green River Development Program" paragraph 9.0

T3S, R2W, U.S.B.&M.

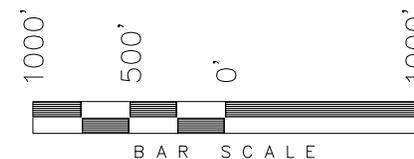
NEWFIELD EXPLORATION COMPANY



23
WELL LOCATION:
4-23-3-2WH
 ELEV. UNGRADED GROUND = 5271.0'

WELL LOCATION, 4-23-3-2WH, LOCATED AS SHOWN IN THE NE 1/4 NW 1/4 OF SECTION 23, T3S, R2W, U.S.B.&M. DUCHESNE COUNTY, UTAH.

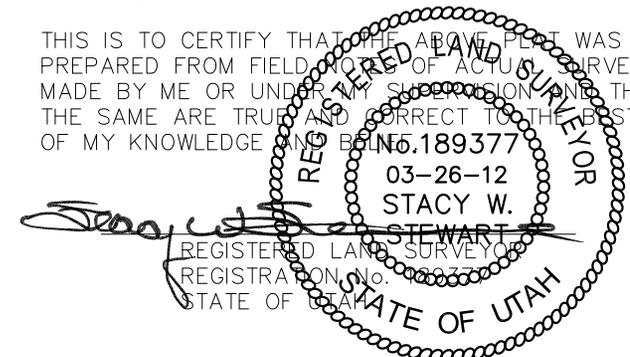
TARGET BOTTOM HOLE, 4-23-3-2WH, LOCATED AS SHOWN IN THE SW 1/4 SW 1/4 OF SECTION 23, T3S, R2W, U.S.B.&M. DUCHESNE COUNTY, UTAH.



NOTES:

1. Well footages are measured at right angles to the Section Lines.
2. Bearings are based on Global Positioning Satellite observations.
3. The Top of Producing Interval bears S56°15'12"W 905.14' from the Top of Hole.

THIS IS TO CERTIFY THAT THE ABOVE PLAT WAS PREPARED FROM FIELD NOTES OF ACTUAL SURVEYS MADE BY ME OR UNDER MY SUPERVISION AND THAT THE SAME ARE TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.



◆ = SECTION CORNERS LOCATED

BASIS OF ELEV; Elevations are based on an N.G.S. OPUS Correction. LOCATION: LAT. 40°04'09.56" LONG. 110°00'43.28" (Tristate Aluminum Cap) Elev. 5281.57'

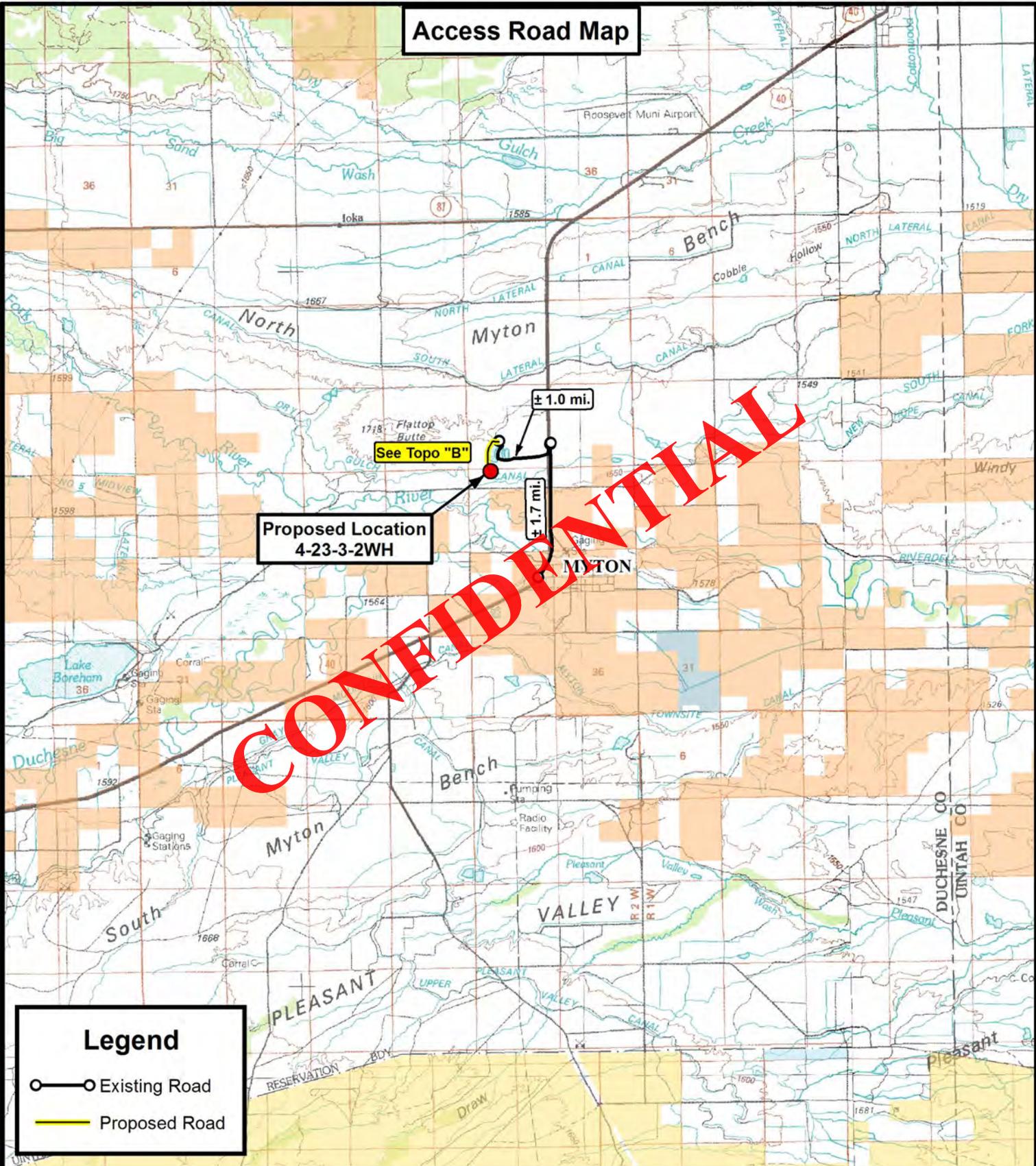
4-23-3-2WH
 (Surface Location) NAD 83
 LATITUDE = 40° 12' 52.35"
 LONGITUDE = 110° 04' 51.27"

TRI STATE LAND SURVEYING & CONSULTING

180 NORTH VERNAL AVE. - VERNAL, UTAH 84078
 (435) 781-2501

DATE SURVEYED: 03-15-12	SURVEYED BY: S.H.	VERSION:
DATE DRAWN: 03-22-12	DRAWN BY: R.B.T.	V2
REVISED: 03-26-12 R.B.T.	SCALE: 1" = 1000'	

Access Road Map



**Proposed Location
4-23-3-2WH**

See Topo "B"

± 1.0 mi.

± 1.7 mi.

Legend

- Existing Road
- Proposed Road

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**Tri State
Land Surveying, Inc.**
180 NORTH VERNAL AVE. VERNAL, UTAH 84078

P: (435) 781-2501
F: (435) 781-2518



NEWFIELD EXPLORATION COMPANY

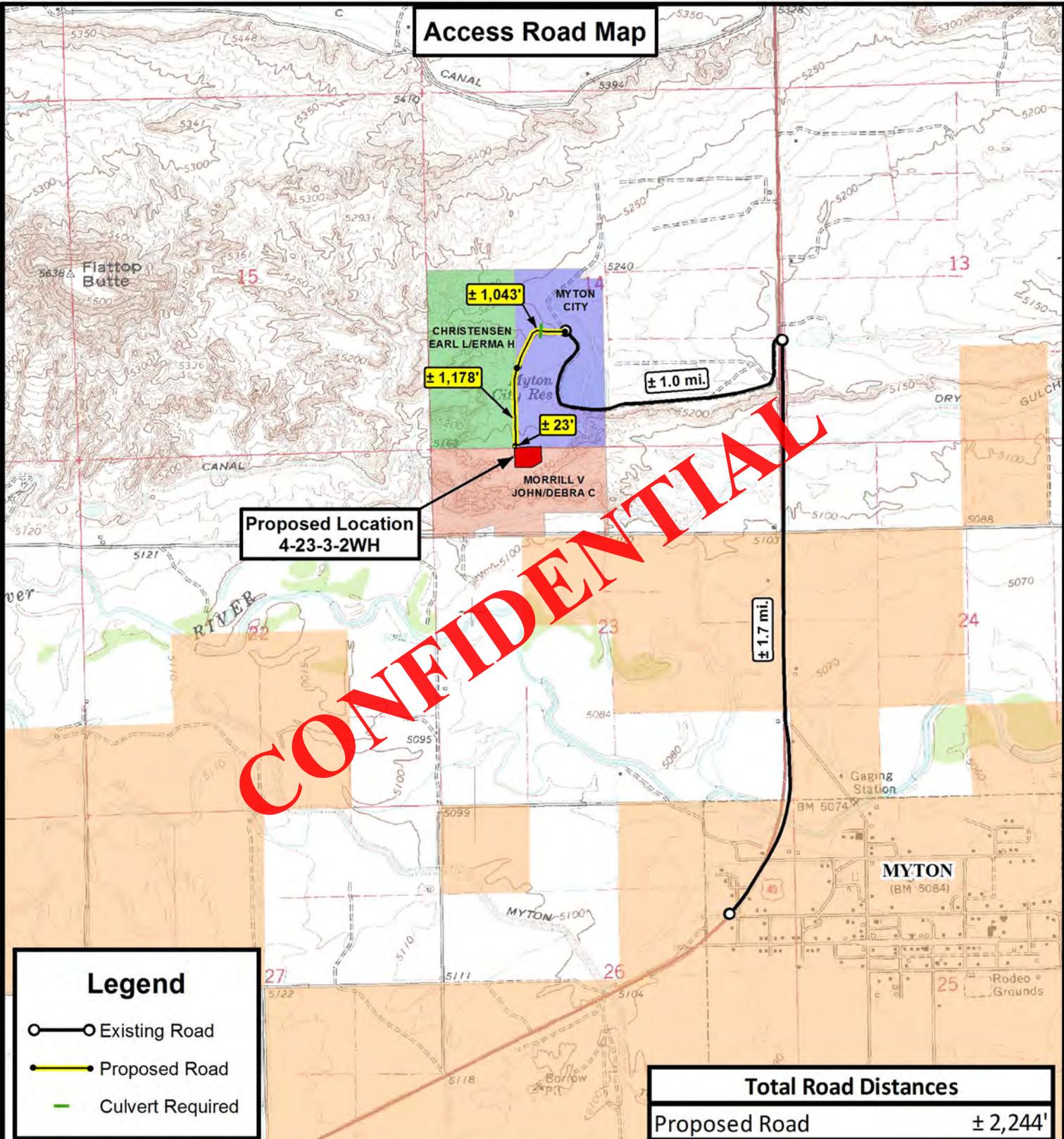
**4-23-3-2WH
SEC. 23, T3S, R2W, U.S.B.&M.
Duchesne County, UT.**

DRAWN BY:	D.C.R.	REVISED:	03-26-12 A.P.C	VERSION:
DATE:	03-22-2012			V2
SCALE:	1:100,000			

TOPOGRAPHIC MAP

SHEET
A

Access Road Map



**Proposed Location
4-23-3-2WH**

Legend

- Existing Road
- Proposed Road
- Culvert Required

Total Road Distances	
Proposed Road	± 2,244'

THE PARCEL INFORMATION SHOWN HAS NOT BEEN SURVEYED BY TRI-STATE LAND SURVEYING, INC. - TRI-STATE DOES NOT WARRANTY PROPERTY PARCEL DATA OR ANY ASSOCIATED INFORMATION. A PROPERTY SURVEY IS REQUIRED TO DETERMINE THE ACTUAL LOCATION OF PROPERTY LINES AND SHOW ACCURATE DISTANCES ACROSS PARCELS.



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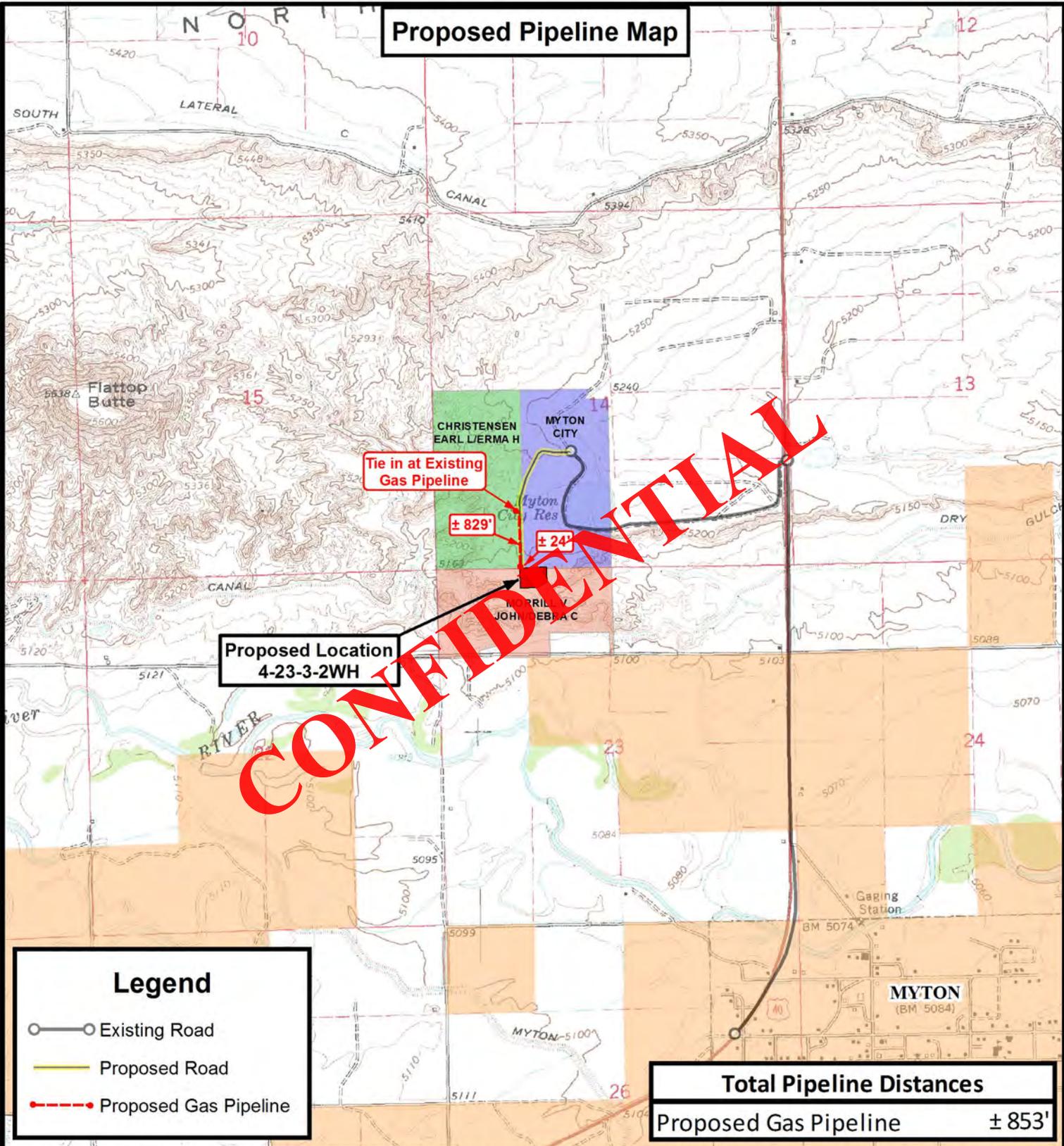
4-23-3-2WH
SEC. 23, T3S, R2W, U.S.B.&M.
Duchesne County, UT.

DRAWN BY:	D.C.R.	REVISED:	03-26-12 A.P.C.	VERSION:
DATE:	03-22-2012			V2
SCALE:	1" = 2,000'			

TOPOGRAPHIC MAP

SHEET **B**

Proposed Pipeline Map



**Proposed Location
4-23-3-2WH**

**Tie in at Existing
Gas Pipeline**

± 829'

± 24'

Legend

- Existing Road
- Proposed Road
- Proposed Gas Pipeline

Total Pipeline Distances	
Proposed Gas Pipeline	± 853'

THE PARCEL INFORMATION SHOWN HAS NOT BEEN SURVEYED BY TRI-STATE LAND SURVEYING, INC. - TRI-STATE DOES NOT WARRANTY PROPERTY PARCEL DATA OR ANY ASSOCIATED INFORMATION. A PROPERTY SURVEY IS REQUIRED TO DETERMINE THE ACTUAL LOCATION OF PROPERTY LINES AND SHOW ACCURATE DISTANCES ACROSS PARCELS.

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NEWFIELD EXPLORATION COMPANY

**4-23-3-2WH
SEC. 23, T3S, R2W, U.S.B.&M.
Duchesne County, UT.**

DRAWN BY:	D.C.R.	REVISED:	03-26-12 A.P.C	VERSION:	
DATE:	03-22-2012			V2	
SCALE:	1" = 2,000'				

TOPOGRAPHIC MAP

SHEET
C

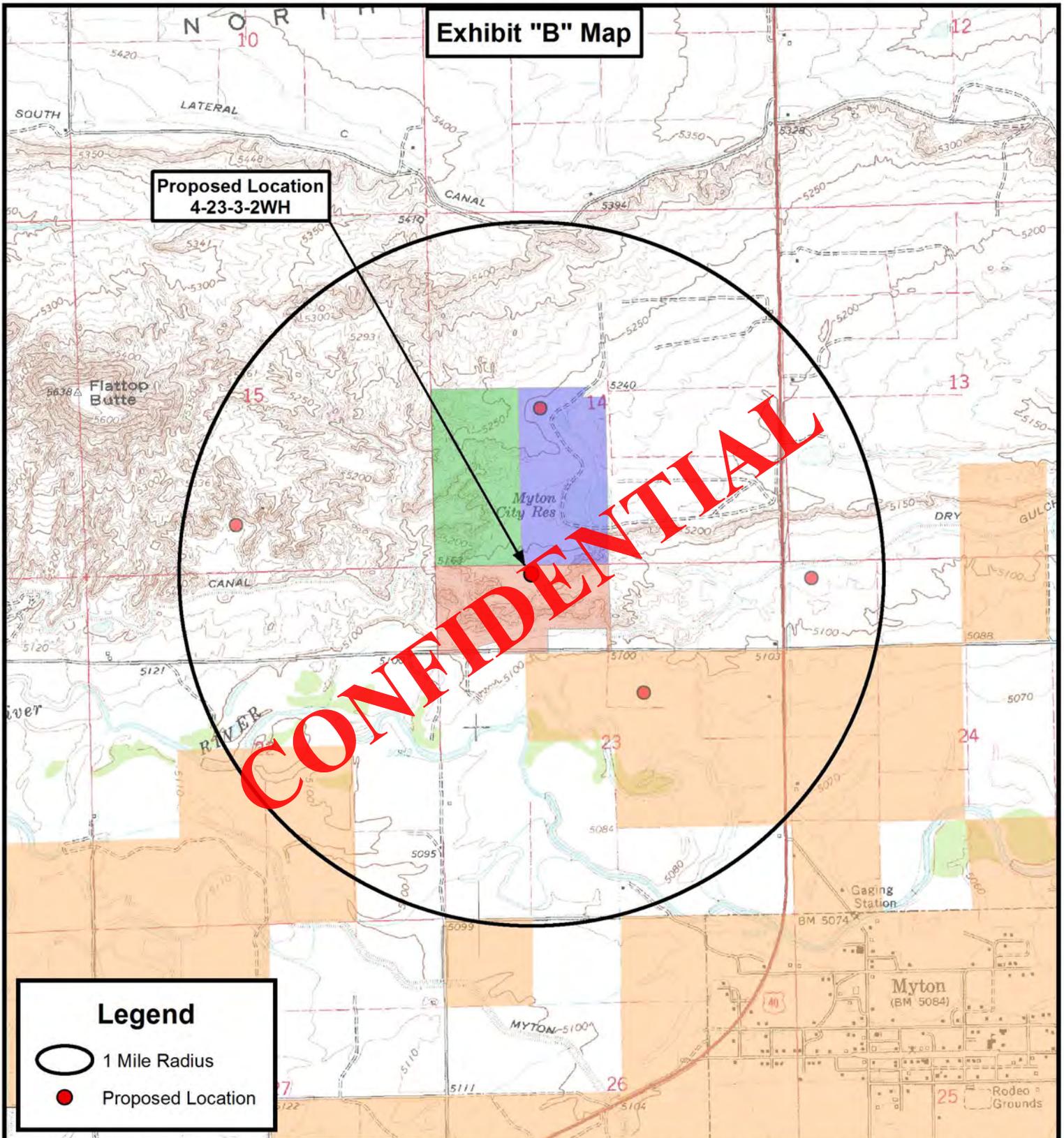


Exhibit "B" Map

**Proposed Location
4-23-3-2WH**

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Legend

-  1 Mile Radius
-  Proposed Location

THE PARCEL INFORMATION SHOWN HAS NOT BEEN SURVEYED BY TRI-STATE LAND SURVEYING, INC. - TRI-STATE DOES NOT WARRANTY PROPERTY PARCEL DATA OR ANY ASSOCIATED INFORMATION. A PROPERTY SURVEY IS REQUIRED TO DETERMINE THE ACTUAL LOCATION OF PROPERTY LINES AND SHOW ACCURATE DISTANCES ACROSS PARCELS.



**Tri State
Land Surveying, Inc.**
180 NORTH VERNAL AVE. VERNAL, UTAH 84078

P: (435) 781-2501
F: (435) 781-2518



NEWFIELD EXPLORATION COMPANY

4-23-3-2WH
SEC. 23, T3S, R2W, U.S.B.&M.
Duchesne County, UT.

DRAWN BY:	D.C.R.	REVISED:	03-26-12 A.P.C.	VERSION:
DATE:	03-22-2012			V2
SCALE:	1" = 2,000'			

TOPOGRAPHIC MAP

SHEET **D**

NEWFIELD



NEWFIELD EXPLORATION CO.
DUCHESNE COUNTY, UT

MORRILL 4-23-3-2WH

Plan: Design #1

Standard Survey Report

25 APRIL, 2012

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Weatherford®



Project: DUCHESNE COUNTY, UT
 Site: MORRILL 4-23-3-2WH
 Well: MORRILL 4-23-3-2WH
 Wellbore: MORRILL 4-23-3-2WH
 Design: Design #1
 Latitude: 40° 12' 52.350 N
 Longitude: 110° 4' 51.270 W
 GL: 5271.00
 KB: WELL @ 5285.00ft (Original Well Elev)



WELLBORE TARGET DETAILS (LAT/LONG)						
Name	TVD	+N/-S	+E/-W	Latitude	Longitude	Shape Point
PBHL MORRILL 4-23-3-2WH	8448.00	-4483.42	-675.02	40° 12' 8.041 N	110° 4' 59.970 W	

WELL DETAILS: MORRILL 4-23-3-2WH						
+N/-S	+E/-W	Northing	Ground Level: Easting	5271.00 Latitude	Longitude	Slot
0.00	0.00	7250016.40	2036698.56	40° 12' 52.350 N	110° 4' 51.270 W	

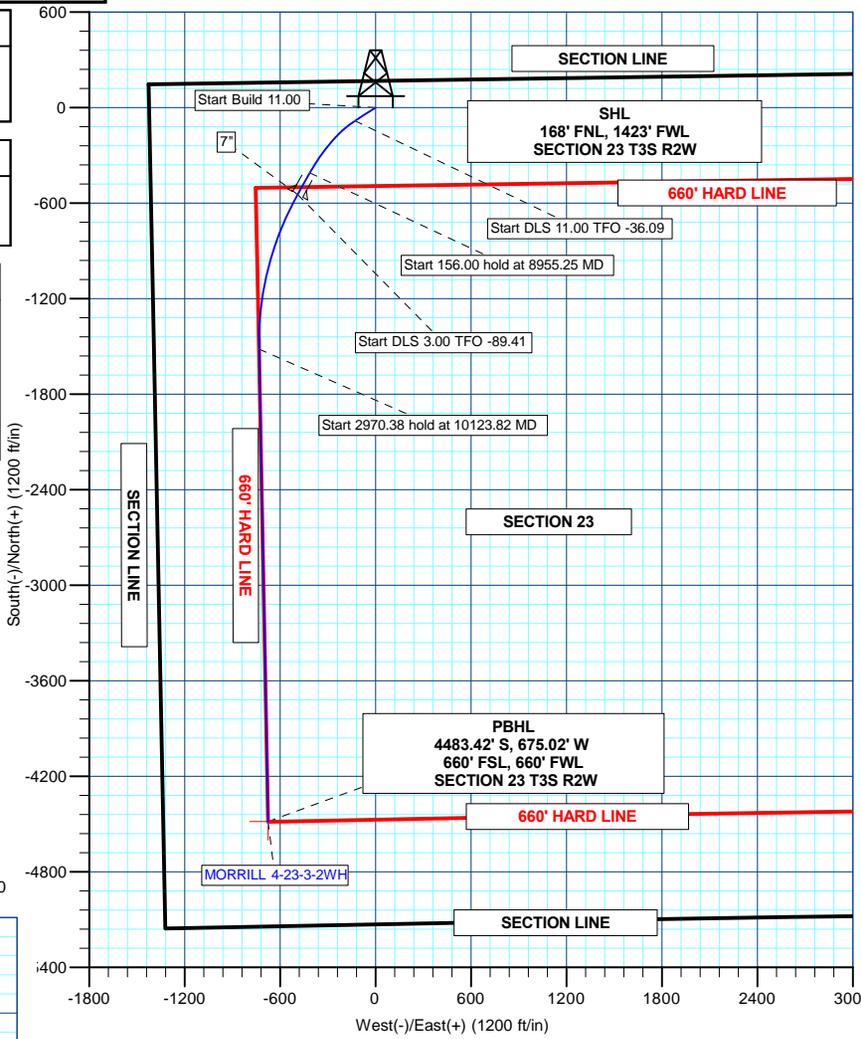
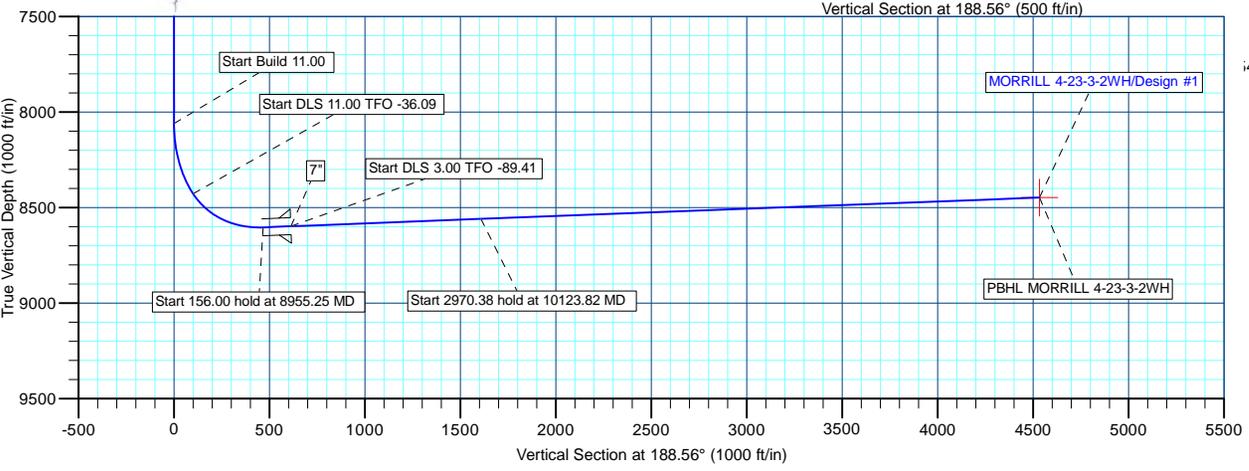
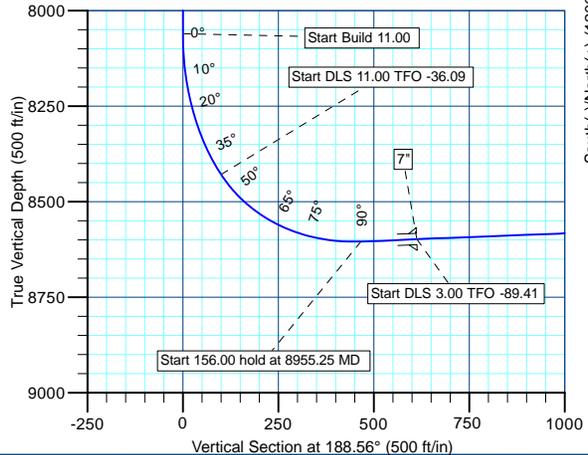
SECTION DETAILS									
MD	Inc	Azi	TVD	+N/-S	+E/-W	DLog	TFace	VSec	Annotation
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
8060.50	0.00	0.00	8060.50	0.00	0.00	0.00	0.00	0.00	Start Build 11.00
8469.59	45.00	237.54	8428.81	81.88	-128.72	11.00	237.54	100.13	Start DLS 11.00 TFO -36.09
8955.25	92.15	209.28	8604.32	09.80	-13.21	11.00	-36.09	466.75	Start 156.00 hold at 8955.25 MD
9111.25	92.15	209.28	8595.48	85.76	-89.46	0.00	0.00	612.55	Start DLS 3.00 TFO -89.41
10123.82	92.15	178.88	8559.57	-15.70	-732.81	3.00	-89.41	1607.91	Start 2970.38 hold at 10123.82 MD
13094.20	92.15	178.88	8448.00	-4483.42	-675.02	0.00	0.00	4533.95	TD at 13094.20

T M

Azimuths to True North
 Magnetic North: 11.27°

Magnetic Field
 Strength: 52222.1snT
 Dip Angle: 65.89°
 Date: 4/25/2012
 Model: BGGM2011

CASING DETAILS				
TVD	MD	Name	Size	
8598.48	9111.25		7"	7



NEWFIELD



NEWFIELD EXPLORATION CO.

DUCHESNE COUNTY, UT

MORRILL 4-23-3-2WH

MORRILL 4-23-3-2WH

MORRILL 4-23-3-2WH

Plan: Design #1

Standard Planning Report

25 April, 2012

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Weatherford®



Database:	EDM 2003.21 Single User Db	Local Co-ordinate Reference:	Well MORRILL 4-23-3-2WH
Company:	NEWFIELD EXPLORATION CO.	TVD Reference:	WELL @ 5289.00ft (Original Well Elev)
Project:	DUCHESNE COUNTY, UT	MD Reference:	WELL @ 5289.00ft (Original Well Elev)
Site:	MORRILL 4-23-3-2WH	North Reference:	True
Well:	MORRILL 4-23-3-2WH	Survey Calculation Method:	Minimum Curvature
Wellbore:	MORRILL 4-23-3-2WH		
Design:	Design #1		

Project	DUCHESNE COUNTY, UT		
Map System:	US State Plane 1983	System Datum:	Mean Sea Level
Geo Datum:	North American Datum 1983		
Map Zone:	Utah Central Zone		

Site	MORRILL 4-23-3-2WH				
Site Position:		Northing:	7,250,016.40ft	Latitude:	40° 12' 52.350 N
From:	Lat/Long	Easting:	2,036,698.56ft	Longitude:	110° 4' 51.270 W
Position Uncertainty:	0.00 ft	Slot Radius:	"	Grid Convergence:	0.91 °

Well	MORRILL 4-23-3-2WH					
Well Position	+N/-S	0.00 ft	Northing:	7,250,016.40 ft	Latitude:	40° 12' 52.350 N
	+E/-W	0.00 ft	Easting:	2,036,698.56 ft	Longitude:	110° 4' 51.270 W
Position Uncertainty		0.00 ft	Wellhead Elevation:	ft	Ground Level:	5,271.00ft

Wellbore	MORRILL 4-23-3-2WH				
Magnetics	Model Name	Sample Date	Declination (°)	Dip Angle (°)	Field Strength (nT)
	BGGM2011	4/25/2012	11.27	65.89	52,222

Design	Design #1			
Audit Notes:				
Version:	Phase:	PLAN	Tie On Depth:	0.00
Vertical Section:	Depth From (TVD) (ft)	+N/-S (ft)	+E/-W (ft)	Direction (°)
	0.00	0.00	0.00	188.56

Plan Sections										
Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)	TFO (°)	Target
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	
8,060.50	0.00	0.00	8,060.50	0.00	0.00	0.00	0.00	0.00	0.00	
8,469.59	45.00	237.54	8,428.81	-81.88	-128.72	11.00	11.00	0.00	237.54	
8,955.25	92.15	209.28	8,604.32	-409.80	-413.21	11.00	9.71	-5.82	-36.09	
9,111.25	92.15	209.28	8,598.48	-545.76	-489.46	0.00	0.00	0.00	0.00	
10,123.82	92.15	178.88	8,559.57	-1,515.70	-732.81	3.00	0.00	-3.00	-89.41	
13,094.20	92.15	178.88	8,448.00	-4,483.42	-675.02	0.00	0.00	0.00	0.00	PBHL MORRILL 4-



Database:	EDM 2003.21 Single User Db	Local Co-ordinate Reference:	Well MORRILL 4-23-3-2WH
Company:	NEWFIELD EXPLORATION CO.	TVD Reference:	WELL @ 5289.00ft (Original Well Elev)
Project:	DUCHESNE COUNTY, UT	MD Reference:	WELL @ 5289.00ft (Original Well Elev)
Site:	MORRILL 4-23-3-2WH	North Reference:	True
Well:	MORRILL 4-23-3-2WH	Survey Calculation Method:	Minimum Curvature
Wellbore:	MORRILL 4-23-3-2WH		
Design:	Design #1		

Planned Survey

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
100.00	0.00	0.00	100.00	0.00	0.00	0.00	0.00	0.00	0.00
200.00	0.00	0.00	200.00	0.00	0.00	0.00	0.00	0.00	0.00
300.00	0.00	0.00	300.00	0.00	0.00	0.00	0.00	0.00	0.00
400.00	0.00	0.00	400.00	0.00	0.00	0.00	0.00	0.00	0.00
500.00	0.00	0.00	500.00	0.00	0.00	0.00	0.00	0.00	0.00
600.00	0.00	0.00	600.00	0.00	0.00	0.00	0.00	0.00	0.00
700.00	0.00	0.00	700.00	0.00	0.00	0.00	0.00	0.00	0.00
800.00	0.00	0.00	800.00	0.00	0.00	0.00	0.00	0.00	0.00
900.00	0.00	0.00	900.00	0.00	0.00	0.00	0.00	0.00	0.00
1,000.00	0.00	0.00	1,000.00	0.00	0.00	0.00	0.00	0.00	0.00
1,100.00	0.00	0.00	1,100.00	0.00	0.00	0.00	0.00	0.00	0.00
1,200.00	0.00	0.00	1,200.00	0.00	0.00	0.00	0.00	0.00	0.00
1,300.00	0.00	0.00	1,300.00	0.00	0.00	0.00	0.00	0.00	0.00
1,400.00	0.00	0.00	1,400.00	0.00	0.00	0.00	0.00	0.00	0.00
1,500.00	0.00	0.00	1,500.00	0.00	0.00	0.00	0.00	0.00	0.00
1,600.00	0.00	0.00	1,600.00	0.00	0.00	0.00	0.00	0.00	0.00
1,700.00	0.00	0.00	1,700.00	0.00	0.00	0.00	0.00	0.00	0.00
1,800.00	0.00	0.00	1,800.00	0.00	0.00	0.00	0.00	0.00	0.00
1,900.00	0.00	0.00	1,900.00	0.00	0.00	0.00	0.00	0.00	0.00
2,000.00	0.00	0.00	2,000.00	0.00	0.00	0.00	0.00	0.00	0.00
2,100.00	0.00	0.00	2,100.00	0.00	0.00	0.00	0.00	0.00	0.00
2,200.00	0.00	0.00	2,200.00	0.00	0.00	0.00	0.00	0.00	0.00
2,300.00	0.00	0.00	2,300.00	0.00	0.00	0.00	0.00	0.00	0.00
2,400.00	0.00	0.00	2,400.00	0.00	0.00	0.00	0.00	0.00	0.00
2,500.00	0.00	0.00	2,500.00	0.00	0.00	0.00	0.00	0.00	0.00
2,600.00	0.00	0.00	2,600.00	0.00	0.00	0.00	0.00	0.00	0.00
2,700.00	0.00	0.00	2,700.00	0.00	0.00	0.00	0.00	0.00	0.00
2,800.00	0.00	0.00	2,800.00	0.00	0.00	0.00	0.00	0.00	0.00
2,900.00	0.00	0.00	2,900.00	0.00	0.00	0.00	0.00	0.00	0.00
3,000.00	0.00	0.00	3,000.00	0.00	0.00	0.00	0.00	0.00	0.00
3,100.00	0.00	0.00	3,100.00	0.00	0.00	0.00	0.00	0.00	0.00
3,200.00	0.00	0.00	3,200.00	0.00	0.00	0.00	0.00	0.00	0.00
3,300.00	0.00	0.00	3,300.00	0.00	0.00	0.00	0.00	0.00	0.00
3,400.00	0.00	0.00	3,400.00	0.00	0.00	0.00	0.00	0.00	0.00
3,500.00	0.00	0.00	3,500.00	0.00	0.00	0.00	0.00	0.00	0.00
3,600.00	0.00	0.00	3,600.00	0.00	0.00	0.00	0.00	0.00	0.00
3,700.00	0.00	0.00	3,700.00	0.00	0.00	0.00	0.00	0.00	0.00
3,800.00	0.00	0.00	3,800.00	0.00	0.00	0.00	0.00	0.00	0.00
3,900.00	0.00	0.00	3,900.00	0.00	0.00	0.00	0.00	0.00	0.00
4,000.00	0.00	0.00	4,000.00	0.00	0.00	0.00	0.00	0.00	0.00
4,100.00	0.00	0.00	4,100.00	0.00	0.00	0.00	0.00	0.00	0.00
4,200.00	0.00	0.00	4,200.00	0.00	0.00	0.00	0.00	0.00	0.00
4,300.00	0.00	0.00	4,300.00	0.00	0.00	0.00	0.00	0.00	0.00
4,400.00	0.00	0.00	4,400.00	0.00	0.00	0.00	0.00	0.00	0.00
4,500.00	0.00	0.00	4,500.00	0.00	0.00	0.00	0.00	0.00	0.00
4,600.00	0.00	0.00	4,600.00	0.00	0.00	0.00	0.00	0.00	0.00
4,700.00	0.00	0.00	4,700.00	0.00	0.00	0.00	0.00	0.00	0.00
4,800.00	0.00	0.00	4,800.00	0.00	0.00	0.00	0.00	0.00	0.00
4,900.00	0.00	0.00	4,900.00	0.00	0.00	0.00	0.00	0.00	0.00
5,000.00	0.00	0.00	5,000.00	0.00	0.00	0.00	0.00	0.00	0.00
5,100.00	0.00	0.00	5,100.00	0.00	0.00	0.00	0.00	0.00	0.00
5,200.00	0.00	0.00	5,200.00	0.00	0.00	0.00	0.00	0.00	0.00
5,300.00	0.00	0.00	5,300.00	0.00	0.00	0.00	0.00	0.00	0.00

CONFIDENTIAL



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Well:	MORRILL 4-23-3-2WH	Survey Calculation Method:	Minimum Curvature
Wellbore:	MORRILL 4-23-3-2WH		
Design:	Design #1		

Planned Survey

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)	
5,400.00	0.00	0.00	5,400.00	0.00	0.00	0.00	0.00	0.00	0.00	
5,500.00	0.00	0.00	5,500.00	0.00	0.00	0.00	0.00	0.00	0.00	
5,600.00	0.00	0.00	5,600.00	0.00	0.00	0.00	0.00	0.00	0.00	
5,700.00	0.00	0.00	5,700.00	0.00	0.00	0.00	0.00	0.00	0.00	
5,800.00	0.00	0.00	5,800.00	0.00	0.00	0.00	0.00	0.00	0.00	
5,900.00	0.00	0.00	5,900.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,000.00	0.00	0.00	6,000.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,100.00	0.00	0.00	6,100.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,200.00	0.00	0.00	6,200.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,300.00	0.00	0.00	6,300.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,400.00	0.00	0.00	6,400.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,500.00	0.00	0.00	6,500.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,600.00	0.00	0.00	6,600.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,700.00	0.00	0.00	6,700.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,800.00	0.00	0.00	6,800.00	0.00	0.00	0.00	0.00	0.00	0.00	
6,900.00	0.00	0.00	6,900.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,000.00	0.00	0.00	7,000.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,100.00	0.00	0.00	7,100.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,200.00	0.00	0.00	7,200.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,300.00	0.00	0.00	7,300.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,400.00	0.00	0.00	7,400.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,500.00	0.00	0.00	7,500.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,600.00	0.00	0.00	7,600.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,700.00	0.00	0.00	7,700.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,800.00	0.00	0.00	7,800.00	0.00	0.00	0.00	0.00	0.00	0.00	
7,900.00	0.00	0.00	7,900.00	0.00	0.00	0.00	0.00	0.00	0.00	
8,000.00	0.00	0.00	8,000.00	0.00	0.00	0.00	0.00	0.00	0.00	
Start Build 11.00										
8,060.50	0.00	0.00	8,060.50	0.00	0.00	0.00	0.00	0.00	0.00	
8,100.00	4.34	237.54	8,099.96	-0.80	-1.26	0.98	11.00	11.00	0.00	
8,150.00	9.84	237.54	8,149.56	-4.12	-6.47	5.03	11.00	11.00	0.00	
8,200.00	15.34	237.54	8,198.34	-9.97	-15.67	12.19	11.00	11.00	0.00	
8,250.00	20.84	237.54	8,245.85	-18.30	-28.77	22.38	11.00	11.00	0.00	
8,300.00	26.34	237.54	8,291.65	-29.04	-45.65	35.51	11.00	11.00	0.00	
8,350.00	31.84	237.54	8,335.32	-42.08	-66.15	51.46	11.00	11.00	0.00	
8,400.00	37.34	237.54	8,376.47	-57.31	-90.10	70.08	11.00	11.00	0.00	
8,450.00	42.84	237.54	8,414.70	-74.59	-117.26	91.21	11.00	11.00	0.00	
Start DLS 11.00 TFO -36.09										
8,469.59	45.00	237.54	8,428.81	-81.88	-128.72	100.13	11.00	11.00	0.00	
8,500.00	47.73	234.88	8,449.79	-94.13	-147.00	114.96	11.00	8.99	-8.75	
8,550.00	52.35	230.97	8,481.90	-117.25	-177.54	142.38	11.00	9.23	-7.81	
8,600.00	57.08	227.53	8,510.79	-143.91	-208.42	173.33	11.00	9.46	-6.89	
8,650.00	61.89	224.44	8,536.17	-173.85	-239.36	207.55	11.00	9.63	-6.18	
8,700.00	66.77	221.61	8,557.83	-206.79	-270.07	244.70	11.00	9.75	-5.65	
8,750.00	71.69	218.99	8,575.56	-242.45	-300.29	284.45	11.00	9.85	-5.25	
8,800.00	76.65	216.51	8,589.19	-280.47	-329.71	326.44	11.00	9.91	-4.95	
8,850.00	81.63	214.13	8,598.61	-320.53	-358.09	370.27	11.00	9.96	-4.75	
8,900.00	86.62	211.82	8,603.73	-362.24	-385.14	415.54	11.00	9.99	-4.63	
8,950.00	91.62	209.52	8,604.49	-405.22	-410.64	461.84	11.00	10.00	-4.59	
Start 156.00 hold at 8955.25 MD										
8,955.25	92.15	209.28	8,604.32	-409.80	-413.21	466.75	11.00	10.00	-4.59	
9,000.00	92.15	209.28	8,602.65	-448.80	-435.09	508.57	0.00	0.00	0.00	
9,100.00	92.15	209.28	8,598.90	-535.96	-483.96	602.04	0.00	0.00	0.00	



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Project:	DUCHESNE COUNTY, UT	MD Reference:	WELL @ 5289.00ft (Original Well Elev)
Site:	MORRILL 4-23-3-2WH	North Reference:	True
Well:	MORRILL 4-23-3-2WH	Survey Calculation Method:	Minimum Curvature
Wellbore:	MORRILL 4-23-3-2WH		
Design:	Design #1		

Planned Survey

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)	Build Rate (°/100ft)	Turn Rate (°/100ft)
Start DLS 3.00 TFO -89.41 - 7"									
9,111.25	92.15	209.28	8,598.48	-545.76	-489.46	612.55	0.00	0.00	0.00
9,200.00	92.17	206.62	8,595.13	-624.10	-531.03	696.20	3.00	0.03	-3.00
9,300.00	92.20	203.62	8,591.32	-714.56	-573.44	791.98	3.00	0.02	-3.00
9,400.00	92.21	200.61	8,587.47	-807.13	-611.06	889.11	3.00	0.02	-3.00
9,500.00	92.22	197.61	8,583.60	-901.53	-643.77	987.33	3.00	0.01	-3.00
9,600.00	92.23	194.61	8,579.72	-997.52	-671.50	1,086.28	3.00	0.00	-3.00
9,700.00	92.23	191.61	8,575.83	-1,094.83	-694.16	1,185.98	3.00	0.00	-3.00
9,800.00	92.22	188.61	8,571.95	-1,193.19	-711.70	1,285.85	3.00	-0.01	-3.00
9,900.00	92.21	185.60	8,568.09	-1,292.34	-724.05	1,385.74	3.00	-0.01	-3.00
10,000.00	92.19	182.60	8,564.26	-1,392.00	-731.20	1,485.35	3.00	-0.02	-3.00
10,100.00	92.16	179.60	8,560.47	-1,491.90	-733.12	1,584.42	3.00	-0.03	-3.00
Start 2970.38 hold at 10123.82 MD									
10,123.82	92.15	178.88	8,559.57	-1,545.76	-722.81	1,607.91	3.00	-0.03	-3.00
10,200.00	92.15	178.88	8,556.71	-1,597.81	-731.32	1,682.95	0.00	0.00	0.00
10,300.00	92.15	178.88	8,552.95	-1,697.72	-729.38	1,781.46	0.00	0.00	0.00
10,400.00	92.15	178.88	8,549.20	-1,791.33	-727.43	1,879.97	0.00	0.00	0.00
10,500.00	92.15	178.88	8,545.44	-1,881.54	-725.49	1,978.47	0.00	0.00	0.00
10,600.00	92.15	178.88	8,541.69	-1,991.45	-723.54	2,076.98	0.00	0.00	0.00
10,700.00	92.15	178.88	8,537.93	-2,091.36	-721.60	2,175.49	0.00	0.00	0.00
10,800.00	92.15	178.88	8,534.17	-2,191.27	-719.65	2,274.00	0.00	0.00	0.00
10,900.00	92.15	178.88	8,530.42	-2,291.18	-717.71	2,372.50	0.00	0.00	0.00
11,000.00	92.15	178.88	8,526.66	-2,391.09	-715.76	2,471.01	0.00	0.00	0.00
11,100.00	92.15	178.88	8,522.90	-2,491.01	-713.82	2,569.52	0.00	0.00	0.00
11,200.00	92.15	178.88	8,519.15	-2,590.92	-711.87	2,668.02	0.00	0.00	0.00
11,300.00	92.15	178.88	8,515.39	-2,690.83	-709.93	2,766.53	0.00	0.00	0.00
11,400.00	92.15	178.88	8,511.64	-2,790.74	-707.98	2,865.04	0.00	0.00	0.00
11,500.00	92.15	178.88	8,507.88	-2,890.65	-706.04	2,963.55	0.00	0.00	0.00
11,600.00	92.15	178.88	8,504.12	-2,990.56	-704.09	3,062.05	0.00	0.00	0.00
11,700.00	92.15	178.88	8,500.37	-3,090.47	-702.14	3,160.56	0.00	0.00	0.00
11,800.00	92.15	178.88	8,496.61	-3,190.38	-700.20	3,259.07	0.00	0.00	0.00
11,900.00	92.15	178.88	8,492.86	-3,290.29	-698.25	3,357.58	0.00	0.00	0.00
12,000.00	92.15	178.88	8,489.10	-3,390.20	-696.31	3,456.08	0.00	0.00	0.00
12,100.00	92.15	178.88	8,485.34	-3,490.11	-694.36	3,554.59	0.00	0.00	0.00
12,200.00	92.15	178.88	8,481.59	-3,590.02	-692.42	3,653.10	0.00	0.00	0.00
12,300.00	92.15	178.88	8,477.83	-3,689.93	-690.47	3,751.61	0.00	0.00	0.00
12,400.00	92.15	178.88	8,474.08	-3,789.84	-688.53	3,850.11	0.00	0.00	0.00
12,500.00	92.15	178.88	8,470.32	-3,889.75	-686.58	3,948.62	0.00	0.00	0.00
12,600.00	92.15	178.88	8,466.56	-3,989.66	-684.64	4,047.13	0.00	0.00	0.00
12,700.00	92.15	178.88	8,462.81	-4,089.57	-682.69	4,145.63	0.00	0.00	0.00
12,800.00	92.15	178.88	8,459.05	-4,189.48	-680.75	4,244.14	0.00	0.00	0.00
12,900.00	92.15	178.88	8,455.29	-4,289.39	-678.80	4,342.65	0.00	0.00	0.00
13,000.00	92.15	178.88	8,451.54	-4,389.30	-676.85	4,441.16	0.00	0.00	0.00
TD at 13094.20 - PBHL MORRILL 4-23-3-2WH									
13,094.20	92.15	178.88	8,448.00	-4,483.42	-675.02	4,533.95	0.00	0.00	0.00



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Well:	MORRILL 4-23-3-2WH	Survey Calculation Method:	Minimum Curvature
Wellbore:	MORRILL 4-23-3-2WH		
Design:	Design #1		

Design Targets										
Target Name	- hit/miss target	Dip Angle (°)	Dip Dir. (°)	TVD (ft)	+N/-S (ft)	+E/-W (ft)	Northing (ft)	Easting (ft)	Latitude	Longitude
PBHL MORRILL 4-23		0.00	0.00	8,448.00	-4,483.42	-675.02	7,245,522.85	2,036,094.76	40° 12' 8.041 N	110° 4' 59.970 W
	- plan hits target center									
	- Point									

Casing Points					
Measured Depth (ft)	Vertical Depth (ft)	Name	Casing Diameter (")	Hole Diameter (")	
9,111.25	8,598.48	7"	7	8-3/4	

Plan Annotations				
Measured Depth (ft)	Vertical Depth (ft)	Local Coordinates		Comment
		+N/-S (ft)	+E/-W (ft)	
8,060.50	8,060.50	0.00	0.00	Start Build 11.00
8,469.59	8,428.81	-81.88	-128.72	Start DLS 11.00 TFO -36.09
8,955.25	8,604.32	-409.80	-413.21	Start 156.00 hold at 8955.25 MD
9,111.25	8,598.48	-3,482.5	-489.46	Start DLS 3.00 TFO -89.41
10,123.82	8,559.57	-1,515.70	-732.81	Start 2970.38 hold at 10123.82 MD
13,094.20	8,448.00	-4,483.42	-675.02	TD at 13094.20

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AFFIDAVIT OF EASEMENT, RIGHT-OF-WAY AND SURFACE USE AGREEMENT

Greg Boggs personally appeared before me, being duly sworn, deposes and with respect to State of Utah R649-3-34.7 says:

1. My name is Greg Boggs. I am a Landman for Newfield Production Company, whose address is 1001 17th Street, Suite 2000, Denver, CO 80202 (“Newfield”).
2. Newfield is the Operator of the proposed Morrill 4-23-3-2WH well with a surface location to be positioned in the NWNW of Section 23, Township 3 South, Range 2 West, Duchesne County, Utah (the “Drillsite Location”) with a bottom hole location in the SWSW of Section 23, Township 3 South, Range 2 West, Duchesne County, Utah. The surface owner of the Drillsite Location is J. John and Debra C. Morrill along with Jerry and Delia Antonetti, whose address is 5464 Tip Top Road, Mariposa, CA 95338 (“Surface Owner”).
3. Newfield and the Surface Owner have agreed upon an Easement, Right-of-Way and Surface Use Agreement dated March 20, 2012 covering the Drillsite Location and access to the Drillsite Location.

FURTHER AFFIANT SAYETH NOT.

CONFIDENTIAL

Greg Boggs

ACKNOWLEDGEMENT

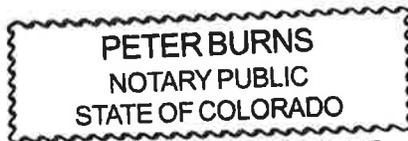
STATE OF COLORADO §
 §
COUNTY OF DENVER §

Before me, a Notary Public, in and for the State, on this 11 day of April 2012, personally appeared Greg Boggs, to me known to be the identical person who executed the foregoing instrument, and acknowledged to me that he executed the same as his own free and voluntary act and deed for the uses and purposes therein set forth.

P. Burns

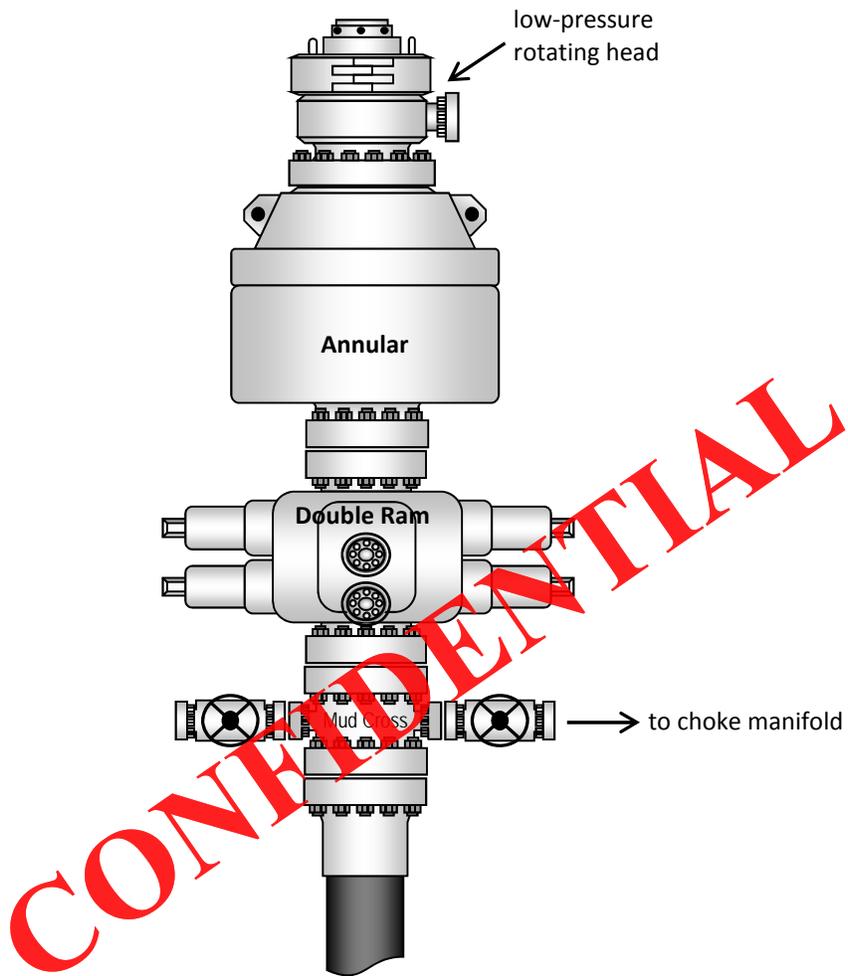
NOTARY PUBLIC

My Commission Expires:

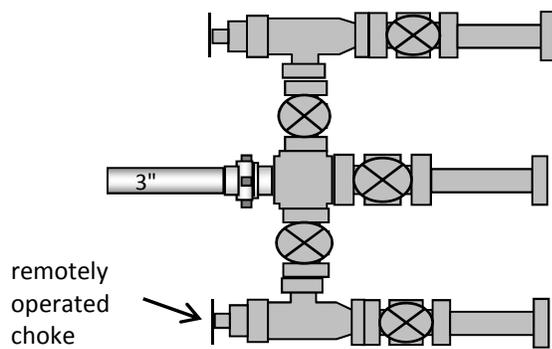


My Commission Expires 8/09/2015

Typical 5M BOP stack configuration



Typical 5M choke manifold configuration



NEWFIELD EXPLORATION COMPANY

WELL PAD INTERFERENCE PLAT

4-23-3-2WH (Proposed Well)

Pad Location: NENW Section 23, T3S, R2W, U.S.B.&M.

Proposed Access Road

Section Line

Questar Gas Line

1/16 Section Line

Edge of Proposed Pad



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TOP HOLE FOOTAGES
 4-23-3-2WH (PROPOSED)
 168' FNL & 1423' FWL

TOP OF PRODUCING INTERVAL FOOTAGES
 4-23-3-2WH (PROPOSED)
 660' FNL & 660' FWL

BOTTOM HOLE FOOTAGES
 4-23-3-2WH (PROPOSED)
 660' FSL & 660' FWL

4-23-3-2WH (PROPOSED)

N87°33'41"E

556°15'12"W - 905.14'
 (To Top of Producing Interval)

S08°33'29"W - 4533.53'
 (To Bottom Hole)

Proposed Pit

RELATIVE COORDINATES
 From Top Hole to Bottom Hole

WELL	NORTH	EAST
4-23-3-2WH	-4,483'	-675'

LATITUDE & LONGITUDE
 Surface position of Wells (NAD 83)

WELL	LATITUDE	LONGITUDE
4-23-3-2WH	40° 12' 52.35"	110° 04' 51.27"

SURVEYED BY: S.H.	DATE SURVEYED: 03-15-12	VERSION:
DRAWN BY: R.B.T.	DATE DRAWN: 03-22-12	V2
SCALE: 1" = 60'	REVISED: R.B.T. 03-26-12	

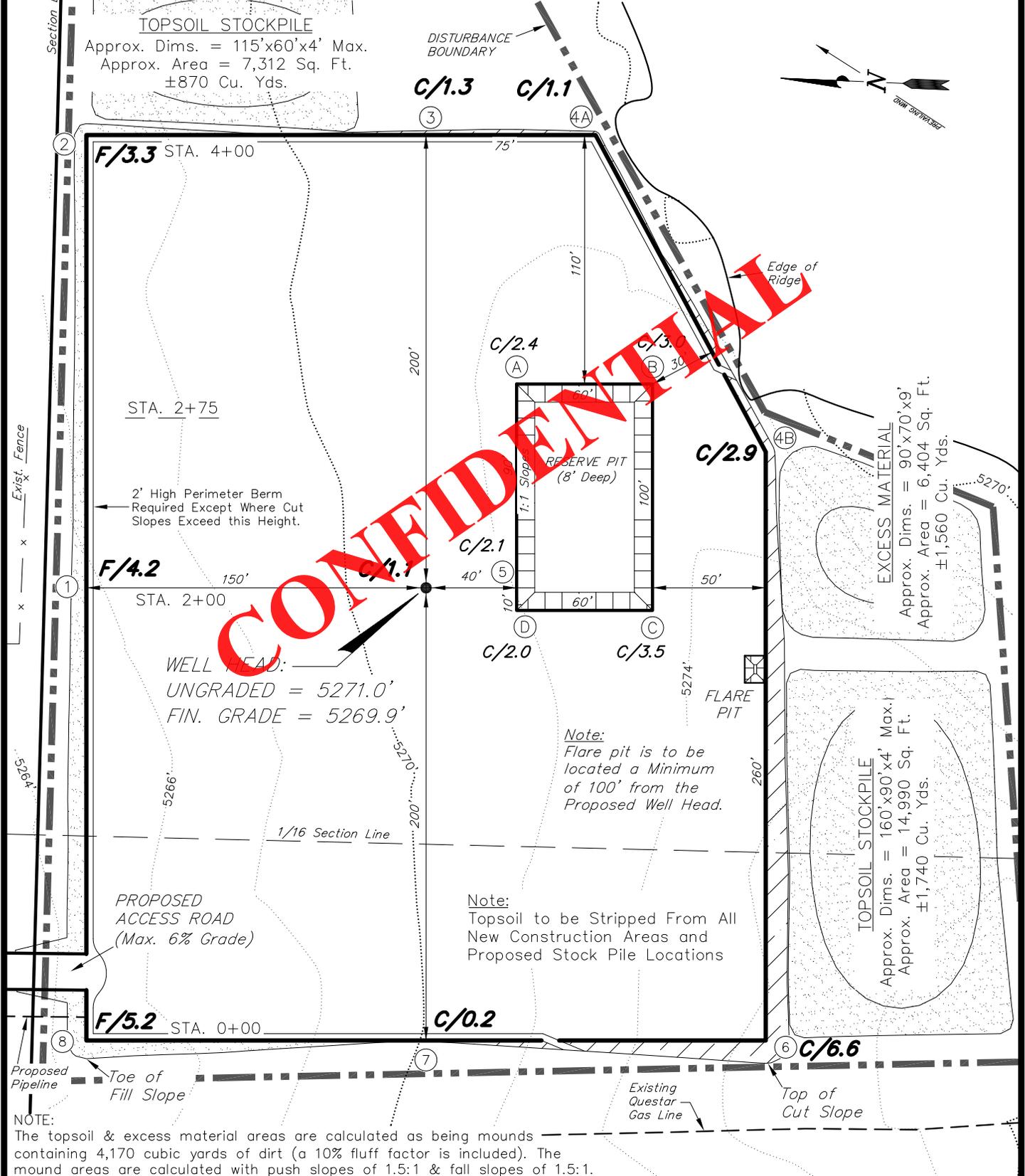
Tri State (435) 781-2501
 Land Surveying, Inc.
 180 NORTH VERNAL AVE. VERNAL, UTAH 84078

NEWFIELD EXPLORATION COMPANY

PROPOSED LOCATION LAYOUT

4-23-3-2WH

Pad Location: NENW Section 23, T3S, R2W, U.S.B.&M.



SURVEYED BY:	S.H.	DATE SURVEYED:	03-15-12	VERSION:
DRAWN BY:	R.B.T.	DATE DRAWN:	03-22-12	V2
SCALE:	1" = 60'	REVISED:	R.B.T. 03-26-12	

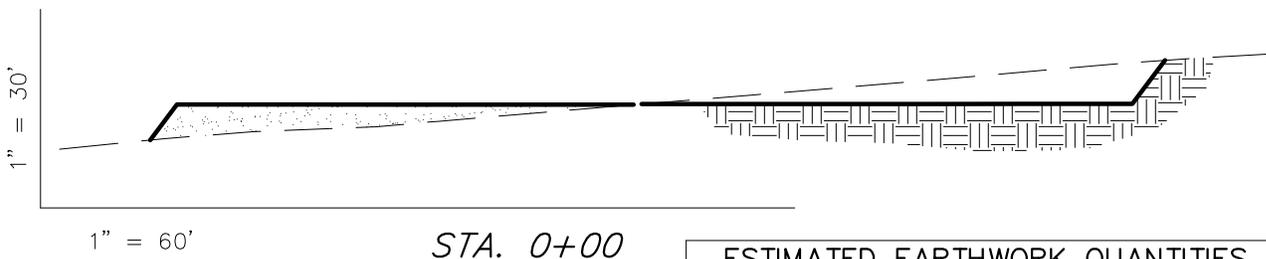
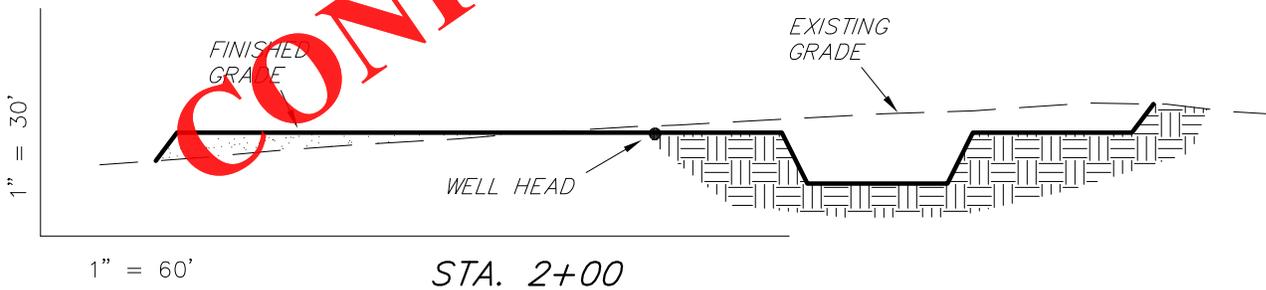
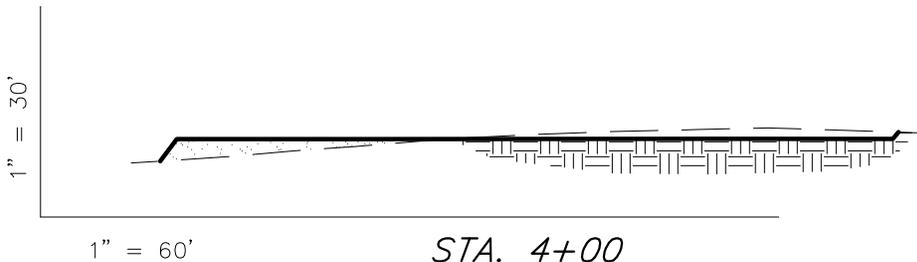
Tri State Land Surveying, Inc. (435) 781-2501
180 NORTH VERNAL AVE. VERNAL, UTAH 84078

NEWFIELD EXPLORATION COMPANY

CROSS SECTIONS

4-23-3-2WH

Pad Location: NENW Section 23, T3S, R2W, U.S.B.&M.



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ESTIMATED EARTHWORK QUANTITIES (No Shrink or swell adjustments have been used) (Expressed in Cubic Yards)				
ITEM	CUT	FILL	6" TOPSOIL	EXCESS
PAD	4,930	4,930	Topsoil is not included in Pad Cut Volume	0
PIT	1,420	0		1,420
TOTALS	6,350	4,930	2,380	1,420

NOTE:
UNLESS OTHERWISE
NOTED ALL CUT/FILL
SLOPES ARE AT 1.5:1

SURVEYED BY: S.H.	DATE SURVEYED: 03-15-12	VERSION:
DRAWN BY: R.B.T.	DATE DRAWN: 03-22-12	V2
SCALE: 1" = 60'	REVISED: R.B.T. 03-26-12	

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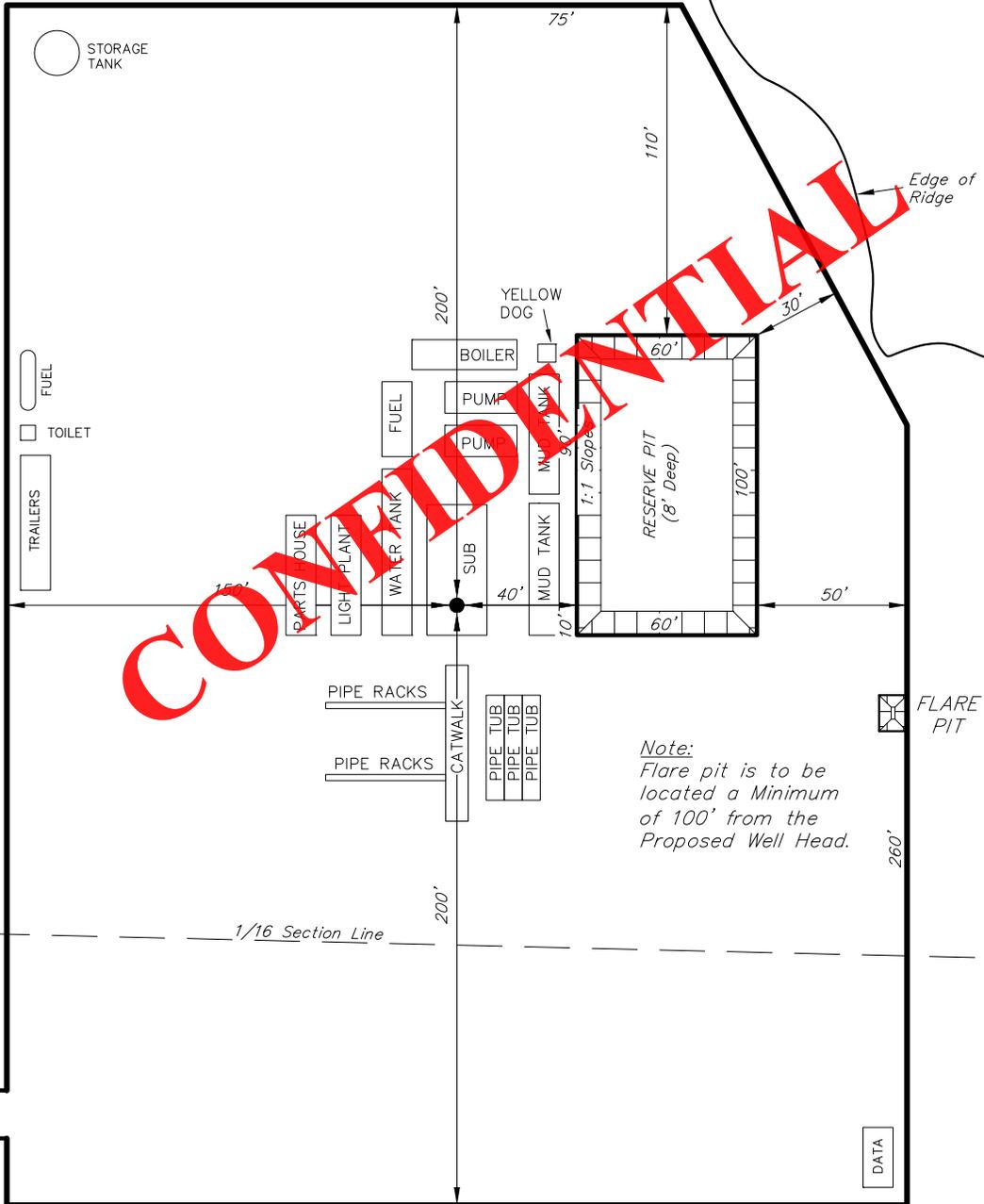
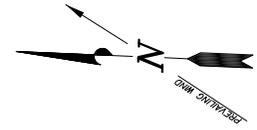
NEWFIELD EXPLORATION COMPANY

TYPICAL RIG LAYOUT

4-23-3-2WH

Pad Location: NENW Section 23, T3S, R2W, U.S.B.&M.

Section Line



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Note:
Flare pit is to be located a Minimum of 100' from the Proposed Well Head.

PROPOSED ACCESS ROAD
(Max. 6% Grade)

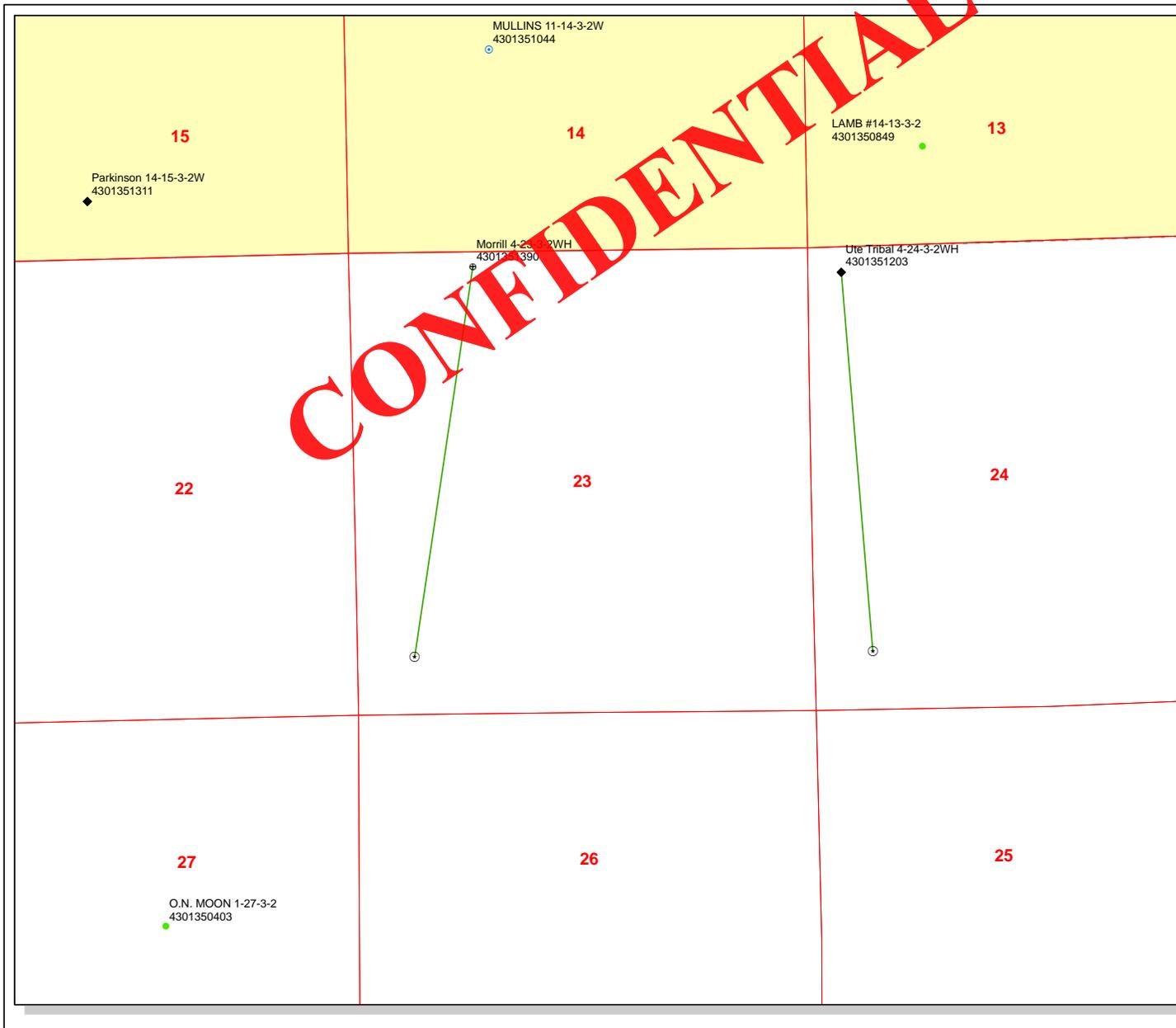
Existing Questar Gas Line

SURVEYED BY: S.H.	DATE SURVEYED: 03-15-12	VERSION:
DRAWN BY: R.B.T.	DATE DRAWN: 03-22-12	V2
SCALE: 1" = 60'	REVISED: R.B.T. 03-26-12	

(435) 781-2501

Tri State
Land Surveying, Inc.

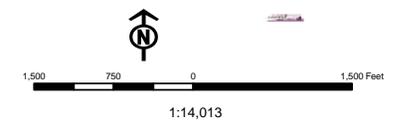
180 NORTH VERNAL AVE. VERNAL, UTAH 84078



API Number: 4301351390
Well Name: Morrill 4-23-3-2WH
Township T0.3 . Range R0.2 . Section 23
Meridian: UBM
 Operator: NEWFIELD PRODUCTION COMPANY

Map Prepared:
 Map Produced by Diana Mason

Units Status	Wells Query Status
ACTIVE	APD - Approved Permit
EXPLORATORY	DRL - Spudded (Drilling Commenced)
GAS STORAGE	GIW - Gas Injection
NF PP OIL	GS - Gas Storage
NF SECONDARY	LA - Location Abandoned
PI OIL	LOC - New Location
PP GAS	OPS - Operation Suspended
PP GEOTHERMAL	PA - Plugged Abandoned
PP OIL	PGW - Producing Gas Well
SECONDARY	POW - Producing Oil Well
TERMINATED	RET - Returned APD
Unknown	SGW - Shut-in Gas Well
ABANDONED	SOW - Shut-in Oil Well
ACTIVE	TA - Temp. Abandoned
COMBINED	TW - Test Well
INACTIVE	WDW - Water Disposal
STORAGE	WW - Water Injection Well
TERMINATED	WSW - Water Supply Well



Well Name	NEWFIELD PRODUCTION COMPANY Morrill 4-23-3-2WH 430135139			
String	COND	SURF	I1	L1
Casing Size(")	14.000	9.625	7.000	4.500
Setting Depth (TVD)	60	2500	9111	13094
Previous Shoe Setting Depth (TVD)	0	60	2500	9111
Max Mud Weight (ppg)	8.3	8.3	11.5	11.5
BOPE Proposed (psi)	0	500	5000	5000
Casing Internal Yield (psi)	1000	3520	9950	12410
Operators Max Anticipated Pressure (psi)	4832			7.1

Calculations	COND String	14.000	"
Max BHP (psi)	.052*Setting Depth*MW=	26	
			BOPE Adequate For Drilling And Setting Casing at Depth?
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	19	NO diverter
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	13	NO
			*Can Full Expected Pressure Be Held At Previous Shoe?
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	13	NO
Required Casing/BOPE Test Pressure=		60	psi
*Max Pressure Allowed @ Previous Casing Shoe=		0	psi *Assumes 1psi/ft frac gradient

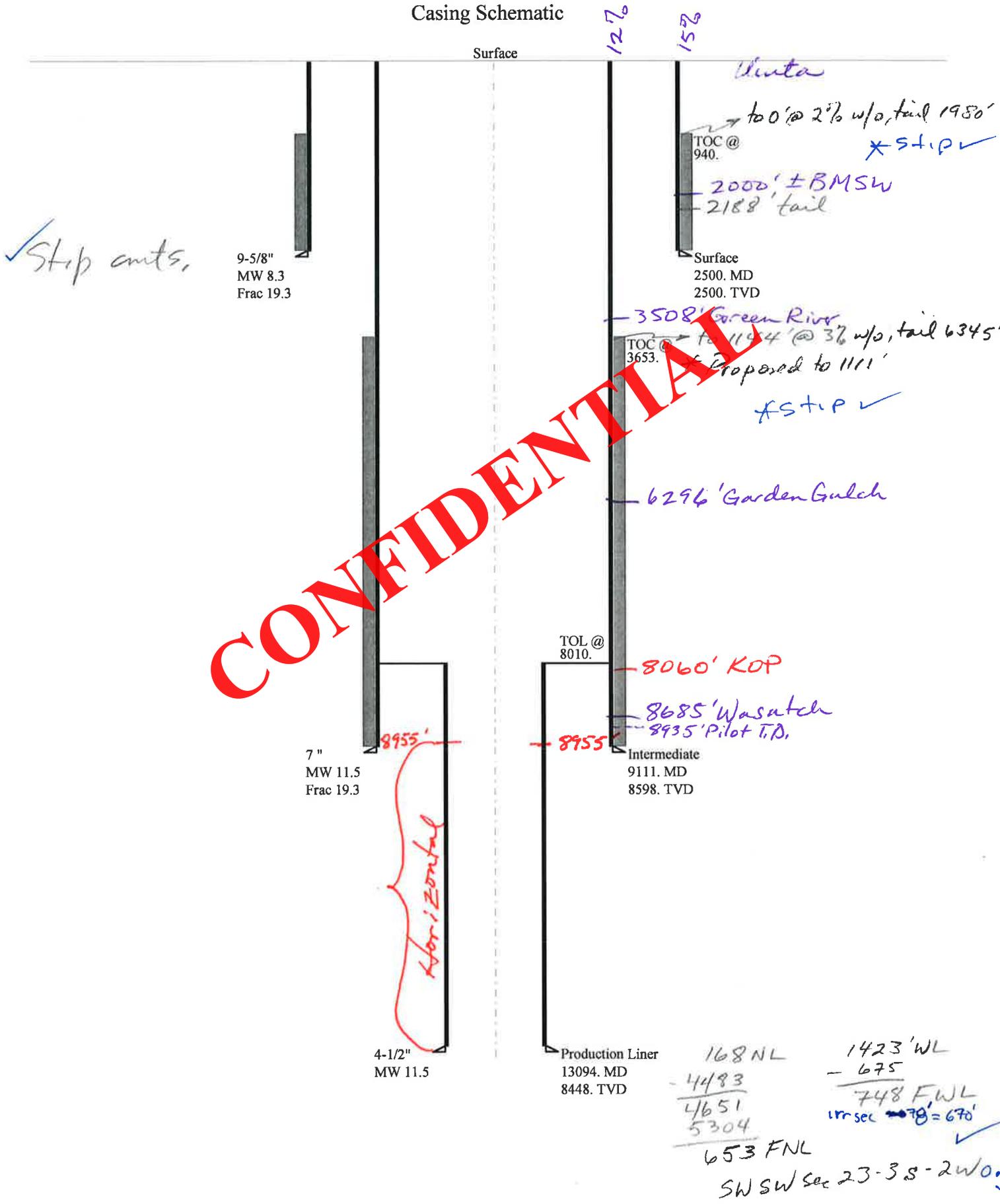
Calculations	SURF String	9.625	"
Max BHP (psi)	.052*Setting Depth*MW=	109	
			BOPE Adequate For Drilling And Setting Casing at Depth?
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	779	NO
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	529	NO No pressures, Reasonable depth
			*Can Full Expected Pressure Be Held At Previous Shoe?
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	542	NO
Required Casing/BOPE Test Pressure=		2464	psi
*Max Pressure Allowed @ Previous Casing Shoe=		60	psi *Assumes 1psi/ft frac gradient

Calculations	I1 String	7.000	"
Max BHP (psi)	.052*Setting Depth*MW=	5448	
			BOPE Adequate For Drilling And Setting Casing at Depth?
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	4355	YES
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	3444	YES OK
			*Can Full Expected Pressure Be Held At Previous Shoe?
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	3994	NO Reasonable
Required Casing/BOPE Test Pressure=		5000	psi
*Max Pressure Allowed @ Previous Casing Shoe=		2500	psi *Assumes 1psi/ft frac gradient

Calculations	L1 String	4.500	"
Max BHP (psi)	.052*Setting Depth*MW=	7830	
			BOPE Adequate For Drilling And Setting Casing at Depth?
MASP (Gas) (psi)	Max BHP-(0.12*Setting Depth)=	6259	NO
MASP (Gas/Mud) (psi)	Max BHP-(0.22*Setting Depth)=	4949	YES OK
			*Can Full Expected Pressure Be Held At Previous Shoe?
Pressure At Previous Shoe	Max BHP-.22*(Setting Depth - Previous Shoe Depth)=	6954	YES
Required Casing/BOPE Test Pressure=		5000	psi
*Max Pressure Allowed @ Previous Casing Shoe=		9111	psi *Assumes 1psi/ft frac gradient

43013513900000 Morrill 4-23 WH

Casing Schematic



Well name:	43013513900000 Morrill 4-23WH	
Operator:	NEWFIELD PRODUCTION COMPANY	
String type:	Surface	Project ID: 43-013-51390
Location:	DUCHESNE COUNTY	

Design parameters:

Collapse

Mud weight: 8.330 ppg
Internal fluid density: 1.000 ppg

Burst

Max anticipated surface pressure: 1,950 psi
Internal gradient: 0.220 psi/ft
Calculated BHP: 2,500 psi

No backup mud specified.

Minimum design factors:

Collapse:

Design factor: 1.125

Burst:

Design factor: 1.00

Tension:

8 Round STC: 1.80 (J)
8 Round LTC: 1.70 (J)
Buttress: 1.50 (J)
Premium: 1.50 (J)
Body yield: 1.80 (B)

Tension is based on air weight.
Neutral point: 2,192 ft

Environment:

H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 109 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 100 ft
Cement top: 940 ft

Non-directional string.

Re subsequent strings:

Next setting depth: 8,598 ft
Next mud weight: 11.500 ppg
Next setting BHP: 5,137 psi
Fracture mud wt: 19.250 ppg
Fracture depth: 2,500 ft
Injection pressure: 2,500 psi

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost (\$)
1	2500	9.625	36.00	J-55	LT&C	2500	2500	8.796	20443
Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	952	2020	2.122	2500	3520	1.41	90	453	5.03 J

Prepared by: Helen Sadik-Macdonald
Div of Oil, Gas & Mining

Phone: 801 538-5357
FAX: 801-359-3940

Date: July 12, 2012
Salt Lake City, Utah

Remarks:

Collapse is based on a vertical depth of 2500 ft, a mud weight of 8.33 ppg. An internal gradient of .052 psi/ft was used for collapse from TD. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Well name:	43013513900000 Morrill 4-23WH	
Operator:	NEWFIELD PRODUCTION COMPANY	
String type:	Intermediate	Project ID: 43-013-51390
Location:	DUCHESNE COUNTY	

Design parameters:

Collapse

Mud weight: 11.500 ppg
Design is based on evacuated pipe.

Burst

Max anticipated surface pressure: 3,245 psi
Internal gradient: 0.220 psi/ft
Calculated BHP: 5,137 psi

No backup mud specified.

Minimum design factors:

Collapse:

Design factor: 1.125

Burst:

Design factor: 1.00

Tension:

8 Round STC: 1.80 (J)
8 Round LTC: 1.80 (J)
Buttress: 1.60 (B)
Premium: 1.50 (J)
Body yield: 1.80 (B)

Tension is based on air weight.
Neutral point: 7,107 ft

Environment:

H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 194 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 1,000 ft

Cement top: 3,653 ft

Directional Info - Build & Hold

Kick off point: 8061 ft
Departure at shoe: 732 ft
Maximum dogleg: 11 °/100ft
Inclination at shoe: 92.15 °

Re subsequent strings:

Next setting depth: 8,448 ft
Next mud weight: 11.500 ppg
Next setting BHP: 5,047 psi
Fracture mud wt: 19.250 ppg
Fracture depth: 8,598 ft
Injection pressure: 8,598 psi

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost (\$)
1	9111	7	26.00	P-110	Buttress	8598	9111	6.151	101323
Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	5137	6185	1.204	5138	9950	1.94	223.6	830.4	3.71 B

Prepared by: Helen Sadik-Macdonald
Div of Oil, Gas & Mining

Phone: 801 538-5357
FAX: 801-359-3940

Date: July 10, 2012
Salt Lake City, Utah

Remarks:

Collapse is based on a vertical depth of 8598 ft, a mud weight of 11.5 ppg. The casing is considered to be evacuated for collapse purposes. Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

Engineering responsibility for use of this design will be that of the purchaser.

Well name:	43013513900000 Morrill 4-23WH	
Operator:	NEWFIELD PRODUCTION COMPANY	
String type:	Production Liner	Project ID: 43-013-51390
Location:	DUCHESNE COUNTY	

Design parameters:

Collapse

Mud weight: 11.500 ppg
Internal fluid density: 1.500 ppg

Minimum design factors:

Collapse:

Design factor 1.125

Burst:

Design factor 1.00

Environment:

H2S considered? No
Surface temperature: 74 °F
Bottom hole temperature: 192 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 1,000 ft

Burst

Max anticipated surface pressure: 3,188 psi
Internal gradient: 0.220 psi/ft
Calculated BHP 5,047 psi

No backup mud specified.

Tension:

8 Round STC: 1.80 (J)
8 Round LTC: 1.80 (J)
Buttress: 1.60 (J)
Premium: 1.50 (J)
Body yield: 1.60 (B)

Tension is based on air weight.
Neutral point: 8,395 ft

Liner top: 8,010 ft
Directional Info - Build & Hold
Kick off point: 8061 ft
Departure at shoe: 4540 ft
Maximum dogleg: 11 °/100ft
Inclination at shoe: 92.15 °

Run Seq	Segment Length (ft)	Size (in)	Nominal Weight (lbs/ft)	Grade	End Finish	True Vert Depth (ft)	Measured Depth (ft)	Drift Diameter (in)	Est. Cost (\$)
1	5094	4.5	13.50	P-110	Buttress	8448	13094	3.795	30561
Run Seq	Collapse Load (psi)	Collapse Strength (psi)	Collapse Design Factor	Burst Load (psi)	Burst Strength (psi)	Burst Design Factor	Tension Load (kips)	Tension Strength (kips)	Tension Design Factor
1	4389	10680	2.434	5081	12410	2.44	6.1	421.9	69.71 B

Prepared by: Helen Sadik-Macdonald
Div of Oil, Gas & Mining

Phone: 801 538-5357
FAX: 801-359-3940

Date: July 10, 2012
Salt Lake City, Utah

Remarks:

For this liner string, the top is rounded to the nearest 100 ft. Collapse is based on a vertical depth of 8448 ft, a mud weight of 11.5 ppg. An Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

Burst strength is not adjusted for tension.

Collapse strength is (biaxially) derated for doglegs in directional wells by multiplying the tensile stress by the cross section area to calculate a

ON-SITE PREDRILL EVALUATION

Utah Division of Oil, Gas and Mining

Operator NEWFIELD PRODUCTION COMPANY
Well Name Morrill 4-23-3-2WH
API Number 43013513900000 **APD No** 5738 **Field/Unit** WILDCAT
Location:
1/4,1/4 NENW **Sec** 23 **Tw** 3.0S **Rng** 2.0W 168 FNL 1423 FWL
GPS Coord
(UTM) 578207 4451974 **Surface Owner** V. John and Debra C. Morrill & Jerry and Delia Antonetti

Participants

T. Eaton, F. Bird, Z. McIntyre - Newfield; J. Simonson - BLM; C. Jensen - DOGM

Regional/Local Setting & Topography

Location is placed on a terrace below and associated with the North Myton Bench on the West side of HWY 40 alongside the pipeline and accessed by the abandoned Myton Reservoir embankments. The soils are very silty sands with clastic fragments littering the surface that drains gently north. Sparsely vegetated Galletta and Atriplex spp are the dominant types found here.

The city of Myton can be found 3 road miles South.

The region is described by benches with exposed sandstone cliffs and associated terracing from the current flow of the Duchesne River and similar topographical features from historical flows. Much of these lands are in a floodplain and have rather high water tables. Agricultural activities are the predominant industry with increasing development for petroleum extraction dotting the landscape. The Duchesne River, New Hope, South Lateral and Dry Gulch canals, Eastern slopes of the Flattop Butte and Hwy 40 can all be found in a one mile radius.

Surface Use Plan

Current Surface Use
Grazing

New Road Miles	Well Pad	Src Const Material	Surface Formation
0.42	Width 300 Length 400	Onsite	UNTA

Ancillary Facilities N

Waste Management Plan Adequate? Y

Environmental Parameters

Affected Floodplains and/or Wetlands N

Flora / Fauna

Dominant vegetation;

Galletta, shadscale and rabbit brush surround the proposed site.

Wildlife;

Habitat contains forbs that may be suitable browse for deer, antelope, prairie dogs and rabbits, though none were observed.

Soil Type and Characteristics

silty sands with clastic fragments

Erosion Issues N**Sedimentation Issues** N**Site Stability Issues** N**Drainage Diversion Required?** N**Berm Required?** Y

pit edge is near the edge of the ridge. Berming will help contain spills

Erosion Sedimentation Control Required? N**Paleo Survey Run?** Y **Paleo Potential Observed?** N **Cultural Survey Run?** Y **Cultural Resources?** N**Reserve Pit****Site-Specific Factors****Site Ranking**

Distance to Groundwater (feet)	100 to 200	5
Distance to Surface Water (feet)	300 to 1000	2
Dist. Nearest Municipal Well (ft)	1320 to 5280	5
Distance to Other Wells (feet)	>1320	0
Native Soil Type	Mod permeability	10
Fluid Type	Fresh Water	5
Drill Cuttings	Normal Rock	0
Annual Precipitation (inches)	10 to 20	5

Affected Populations**Presence Nearby Utility Conduits** Not Present 0**Final Score** 32 1 Sensitivity Level**Characteristics / Requirements**

Pit to be dug to a depth of 8'. Pit should be fenced to prevent entry by deer, other wildlife and domestic animals. Pit to be closed within one year after drilling activities are complete. Pit is to be lined with a synthetic liner

Closed Loop Mud Required? N **Liner Required?** Y **Liner Thickness** 16 **Pit Underlayment Required?** N**Other Observations / Comments**Chris Jensen
Evaluator5/30/2012
Date / Time

Application for Permit to Drill Statement of Basis

Utah Division of Oil, Gas and Mining

APD No	API WellNo	Status	Well Type	Surf Owner	CBM
5738	43013513900000	LOCKED	OW	P	No
Operator	NEWFIELD PRODUCTION COMPANY		Surface Owner-APD	V. John and Debra C. Morrill & Jerry and Delia Antonetti	
Well Name	Morrill 4-23-3-2WH		Unit		
Field	WILDCAT		Type of Work	DRILL	
Location	NENW 23 3S 2W U 168 FNL 1423 FWL GPS Coord (UTM) 578201E 4451966N				

Geologic Statement of Basis

Newfield proposes to set 60' of conductor and 2,500' of surface casing at this location. The base of the moderately saline water at this location is estimated to be at a depth of 2,000'. A search of Division of Water Rights records shows 7 water wells within a 10,000 foot radius of the center of Section 23. All wells are privately owned. Depth is listed as ranging from 36 to 300 feet. Depth is not listed for 2 wells. Water use is listed as irrigation, stock watering, and domestic use. The surface formation at this site is the Uinta Formation. The Uinta Formation is made up of interbedded shales and sandstones. The sandstones are mostly lenticular and discontinuous and should not be a significant source of useable ground water. The proposed casing and cement should adequately protect usable ground water in the area.

Brad Hill
APD Evaluator

6/20/2012
Date / Time

Surface Statement of Basis

This location is proposed approximately 3 road miles northwest of Myton, Utah in the North Myton Bench area of Duchesne County. The surrounding topography is mostly flat. The edge of the terrace borders the south edge of the pad. For this reason, berming is needed to prevent spill from contaminating lands below. The site is characterized by shadscale, Galleta grasses, cheat grass, broom snakeweed, and cactus. The landowner was invited but was not in attendance for the pre-site inspection. Fencing around the reserve pit will be necessary once the well is drilled to prevent wildlife and livestock from entering. Drainages should be diverted around and away from wellpad and access road. A synthetic liner of 16 mils (minimum) should be utilized in the reserve pit. This wells surface location is proposed outside the window and in the next quarter quarter section. however a common sense look at the topography and given the top of the producing interval will be in the correct place, this well is staked in the best location on the ground.

Operator has a surface agreement in place with the landowner. Access to the site is from a road built on the embankment of the Myton reservoir.

The soil type and topography at present do not combine to pose a significant threat to erosion or sediment/ pollution transport in these regional climate conditions. Construction standards of the Operator appear to be adequate for the proposed purpose. I recognize no special flora or animal species or cultural resources on site that the proposed action may harm.

Chris Jensen
Onsite Evaluator

5/30/2012
Date / Time

Conditions of Approval / Application for Permit to Drill

Category	Condition
Pits	A synthetic liner with a minimum thickness of 16 mils shall be properly installed and maintained in the reserve pit.
Surface	The well site shall be bermed to prevent fluids from leaving the pad.
Surface	The reserve pit shall be fenced upon completion of drilling operations.

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WORKSHEET APPLICATION FOR PERMIT TO DRILL

APD RECEIVED: 4/26/2012

API NO. ASSIGNED: 43013513900000

WELL NAME: Morrill 4-23-3-2WH

OPERATOR: NEWFIELD PRODUCTION COMPANY (N2695)

PHONE NUMBER: 435 719-2018

CONTACT: Don Hamilton

PROPOSED LOCATION: NENW 23 030S 020W

Permit Tech Review:

SURFACE: 0168 FNL 1423 FWL

Engineering Review:

BOTTOM: 0660 FSL 0660 FWL

Geology Review:

COUNTY: DUCHESNE

LATITUDE: 40.21447

LONGITUDE: -110.08099

UTM SURF EASTINGS: 578201.00

NORTHINGS: 4451966.00

FIELD NAME: WILDCAT

LEASE TYPE: 4 - Fee

LEASE NUMBER: Patented

PROPOSED PRODUCING FORMATION(S): GREEN RIVER

SURFACE OWNER: 4 - Fee

COALBED METHANE: NO

RECEIVED AND/OR REVIEWED:

- PLAT
- Bond: STATE - B001834
- Potash
- Oil Shale 190-5
- Oil Shale 190-3
- Oil Shale 190-13
- Water Permit: 437478
- RDCC Review: 2012-07-18 00:00:00.0
- Fee Surface Agreement
- Intent to Commingle

Commingling Approved

LOCATION AND SITING:

- R649-2-3.
- Unit:
- R649-3-2. General
- R649-3-3. Exception
- Drilling Unit
- Board Cause No: R649-3-2.6
- Effective Date:
- Siting:
- R649-3-11. Directional Drill

Comments: Presite Completed
TEMP 640 ACRE SPACING:

Stipulations: 5 - Statement of Basis - bhll
12 - Cement Volume (3) - hmadonald
21 - RDCC - dmason
23 - Spacing - dmason
25 - Surface Casing - hmadonald
26 - Temporary Spacing - bhll

RECEIVED: July 23, 2012



GARY R. HERBERT
Governor

GREGORY S. BELL
Lieutenant Governor

State of Utah

DEPARTMENT OF NATURAL RESOURCES

MICHAEL R. STYLER
Executive Director

Division of Oil, Gas and Mining

JOHN R. BAZA
Division Director

Permit To Drill

Well Name: Morrill 4-23-3-2WH
API Well Number: 43013513900000
Lease Number: Patented
Surface Owner: FEE (PRIVATE)
Approval Date: 7/23/2012

Issued to:

NEWFIELD PRODUCTION COMPANY , Rt 3 Box 3630 , Myton, UT 84052

Authority:

Pursuant to Utah Code Ann. 40-6-1 et seq., and Utah Administrative Code R649-3-1 et seq., the Utah Division of Oil, Gas and Mining issues conditions of approval, and permit to drill the listed well. This permit is issued in accordance with the requirements of R649-3-2.6. The expected producing formation or pool is the GREEN RIVER Formation(s), completion into any other zones will require filing a Sundry Notice (Form 9). Completion and commingling of more than one pool will require approval in accordance with R649-3-22.

Duration:

This approval shall expire one year from the above date unless substantial and continuous operation is underway, or a request for extension is made prior to the expiration date

General:

Compliance with the requirements of Utah Admin. R. 649-1 et seq., the Oil and Gas Conservation General Rules, and the applicable terms and provisions of the approved Application for permit to drill.

Conditions of Approval:

The Application for Permit to Drill has been forwarded to the Resource Development Coordinating Committee for review of this action. The operator will be required to comply with any applicable recommendations resulting from this review. (See attached)

This proposed well is located in an area for which drilling units (well spacing patterns) have not been established through an order of the Board of Oil, Gas and Mining (the "Board"). In order to avoid the possibility of waste or injury to correlative rights, the operator is requested, once the well has been drilled, completed, and has produced, to analyze geological and engineering data generated therefrom, as well as any similar data from surrounding areas if available. As soon as is practicable after completion of its analysis, and if the analysis suggests an area larger than the quarter-quarter section upon which the well is located is being drained, the operator is requested to seek an appropriate order from the Board establishing drilling and spacing units in conformance with such analysis by filing a Request for Agency Action with the Board.

A temporary 640 acre spacing unit is hereby established in Section 23, Township 3 S, Range 2 W, USBM for the drilling of this well (R649-3-2.6). No other horizontal wells may be drilled in this section unless approved by the Board of Oil, Gas and Mining.

Compliance with the Conditions of Approval/Application for Permit to Drill outlined in the Statement of Basis (copy attached).

Cement volume for the 7" intermediate string shall be determined from actual hole diameter in order to place cement from the pipe setting depth back to 1111' MD as indicated in the submitted drilling plan.

Surface casing shall be cemented to the surface.

Additional Approvals:

The operator is required to obtain approval from the Division of Oil, Gas and mining before performing any of the following actions during the drilling of this well:

- Any changes to the approved drilling plan - contact Dustin Doucet
- Significant plug back of the well - contact Dustin Doucet
- Plug and abandonment of the well - contact Dustin Doucet

Notification Requirements:

The operator is required to notify the Division of Oil, Gas and Mining of the following actions during drilling of this well:

- Within 24 hours following the spudding of the well - contact Carol Daniels
OR
submit an electronic sundry notice (pre-registration required) via the Utah Oil & Gas website
at <http://oilgas.ogm.utah.gov>
- 24 hours prior to testing blowout prevention equipment - contact Dan Jarvis
- 24 hours prior to cementing or testing casing - contact Dan Jarvis
- Within 24 hours of making any emergency changes to the approved drilling program
- contact Dustin Doucet
- 24 hours prior to commencing operations to plug and abandon the well - contact Dan Jarvis

Contact Information:

The following are Division of Oil, Gas and Mining contacts and their telephone numbers (please leave a voicemail message if the person is not available to take the call):

- Carol Daniels 801-538-5284 - office
- Dustin Doucet 801-538-5281 - office
801-733-0983 - after office hours
- Dan Jarvis 801-538-5338 - office
801-231-8956 - after office hours

Reporting Requirements:

All reports, forms and submittals as required by the Utah Oil and Gas Conservation General Rules will be promptly filed with the Division of Oil, Gas and Mining,

including but not limited to:

- Entity Action Form (Form 6) - due within 5 days of spudding the well
- Monthly Status Report (Form 9) - due by 5th day of the following calendar month
- Requests to Change Plans (Form 9) - due prior to implementation
- Written Notice of Emergency Changes (Form 9) - due within 5 days
- Notice of Operations Suspension or Resumption (Form 9) - due prior to implementation
- Report of Water Encountered (Form 7) - due within 30 days after completion
- Well Completion Report (Form 8) - due within 30 days after completion or plugging

Approved By:

A handwritten signature in black ink, appearing to read "John Rogers", written in a cursive style.

For John Rogers
Associate Director, Oil & Gas

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BLM - Vernal Field Office - Notification Form

Operator Newfield Exploration Rig Name/# Ross # 31 Submitted
By Mike Braithwaite Phone Number 435-401-8392
Well Name/Number Morrill 4-23-3-2W~~H~~
Qtr/Qtr NENW Section 23 Township 3S Range 2W
Lease Serial Number FEE
API Number 43-013513900000

Spud Notice – Spud is the initial spudding of the well, not drilling out below a casing string.

Date/Time 9/12/2012 3:00 AM PM

Casing – Please report time casing run starts, not cementing times.

- Surface Casing
- Intermediate Casing
- Production Casing
- Liner
- Other

Date/Time 9/14/2012 8:00 AM PM

BOPE

- Initial BOPE test at surface casing point
- BOPE test at intermediate casing point
- 30 day BOPE test
- Other

Date/Time _____ AM PM

Remarks _____

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

5. LEASE DESIGNATION AND SERIAL NUMBER:
FEE

SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

6. IF INDIAN, ALLOTTEE OR TRIBE NAME:

7. UNIT or CA AGREEMENT NAME:
UINTA CB -BASAL CARB

1. TYPE OF WELL: OIL WELL GAS WELL OTHER

8. WELL NAME and NUMBER:
MORRILL 4-23-3-2WH

2. NAME OF OPERATOR:
NEWFIELD PRODUCTION COMPANY

9. API NUMBER:
4301351390

3. ADDRESS OF OPERATOR:
Route 3 Box 3630 CITY Myton STATE UT ZIP 84052

PHONE NUMBER
435.646.3721

10. FIELD AND POOL, OR WILDCAT:
UINTA CENTRAL BASIN

4. LOCATION OF WELL:
FOOTAGES AT SURFACE:

COUNTY: DUCHESNE

OTR/OTR. SECTION. TOWNSHIP. RANGE. MERIDIAN: NWNW, 23, T3S, R2W

STATE: UT

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

TYPE OF SUBMISSION	TYPE OF ACTION		
<input type="checkbox"/> NOTICE OF INTENT (Submit in Duplicate) Approximate date work will _____	<input type="checkbox"/> ACIDIZE	<input type="checkbox"/> DEEPEN	<input type="checkbox"/> REPERFORATE CURRENT FORMATION
	<input type="checkbox"/> ALTER CASING	<input type="checkbox"/> FRACTURE TREAT	<input type="checkbox"/> SIDETRACK TO REPAIR WELL
	<input type="checkbox"/> CASING REPAIR	<input type="checkbox"/> NEW CONSTRUCTION	<input type="checkbox"/> TEMPORARITLY ABANDON
	<input type="checkbox"/> CHANGE TO PREVIOUS PLANS	<input type="checkbox"/> OPERATOR CHANGE	<input type="checkbox"/> TUBING REPAIR
	<input type="checkbox"/> CHANGE TUBING	<input type="checkbox"/> PLUG AND ABANDON	<input type="checkbox"/> VENT OR FLAIR
<input checked="" type="checkbox"/> SUBSEQUENT REPORT (Submit Original Form Only) Date of Work Completion: 09/12/2012	<input type="checkbox"/> CHANGE WELL NAME	<input type="checkbox"/> PLUG BACK	<input type="checkbox"/> WATER DISPOSAL
	<input type="checkbox"/> CHANGE WELL STATUS	<input type="checkbox"/> PRODUCTION (START/STOP)	<input type="checkbox"/> WATER SHUT-OFF
	<input type="checkbox"/> COMMINGLE PRODUCING FORMATIONS	<input type="checkbox"/> RECLAMATION OF WELL SITE	<input checked="" type="checkbox"/> OTHER: - Spud Notice
	<input type="checkbox"/> CONVERT WELL TYPE	<input type="checkbox"/> RECOMPLETE - DIFFERENT FORMATION	

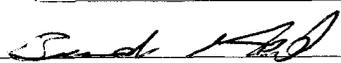
12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

On 9/11/12 MIRU Ross #31. Spud well @8:00 AM. Drill 82' of 17 1/2" hole with air mist. TIH W/ 2 Jt's 14" H-40 36.75# csgn. Set @ 82.
On 9/12/12 cement with 160 sks of class "G" w/ 2% CaCL2 + 0.25#/sk Cello- Flake Mixed @ 15.8ppg w/ 1.17ft3/sk yield. Returned 6 barrels cement to pit. WOC.

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NAME (PLEASE PRINT) Branden Arnold

TITLE _____

SIGNATURE 

DATE 09/27/2012

(This space for State use only)

RECEIVED

OCT 05 2012

DIV. OF OIL, GAS & MINING

Casing / Liner Detail

Well Morrill 4-23-3-2WH
Prospect Central Basin
Foreman
Run Date:
String Type Surface, 9.625", 36#, J-55, LTC (Generic)

- Detail From Top To Bottom -

Depth	Length	JTS	Description	OD	ID
2,567.12			18' KB		
18.00	1.42		Wellhead		
19.42	2501.95	57	9 5/8" Casing	9.625	
2,521.37	1.57		Float Collar	9.625	
2,522.94	42.20	1	Shoe Joint	9.625	
2,565.14	1.98		Guide Shoe	9.625	
2,567.12			-		

Cement Detail

Cement Company: BJ

Slurry	# of Sacks	Weight (ppg)	Yield	Volume (ft ³)	Description - Slurry Class and Additives
Slurry 2	240	15.8	1.17	280.8	G Neat 2%Cal 12 .25#skcf5#blsf
Slurry 1	556	12.5	1.97	1095.32	Premium Lite II Cement

Stab-In-Job?	No	Cement To Surface?	Yes
3HT:	0	Est. Top of Cement:	0
Initial Circulation Pressure:		Plugs Bumped?	Yes
Initial Circulation Rate:		Pressure Plugs Bumped:	1412
Final Circulation Pressure:		Floats Holding?	No
Final Circulation Rate:		Casing Stuck On / Off Bottom?	No
Displacement Fluid:	Water	Casing Reciprocated?	No
Displacement Rate:		Casing Rotated?	No
Displacement Volume:	194	CIP:	8:41
Fluid Returns:		Casing Wt Prior To Cement:	
Centralizer Type And Placement:		Casing Weight Set On Slips:	
Middle of the first and every other for a total of six.			

STATE OF UTAH
DIVISION OF OIL, GAS AND MINING
ENTITY ACTION FORM - FORM 6

OPERATOR: **NEWFIELD PRODUCTION COMPANY**
ADDRESS: **RT. 3 BOX 3630**
MYTON, UT 84052

OPERATOR ACCT NO **N2895**

ACTION CODE	CURRENT ENTITY NO	NEW ENTITY NO	API NUMBER	WELL NAME	WELL LOCATION					SPUD DATE	EFFECTIVE DATE
					DQ	SC	TP	RG	COUNTY		
B	99999	17400	4301350880	GMBU 8-14T-9-16	SENE	14	9S	16E	DUCHESNE	9/13/2012	10/24/12
WELL 1 COMMENTS GRRV											
A	99999	18753	4301351390	MORRILL 4-23-3-2WH	NWNW	23	3S	2W	DUCHESNE	9/11/2012	10/24/12
WELL 1 COMMENTS GRRV											
B	99999	17400	4301350821	GMBU Y-35-8-17	NENE	3	9S	17E	DUCHESNE	9/26/2012	10/24/12
WELL 1 COMMENTS GRRV BHL: 9S 17E SWSW This well's range is 9S-17E at the surface of the whole, and 8S-17E at the bottom of the whole											
B	99999	17400	4301351174	GMBU O-10-9-16	SENE	9	9S	16E	DUCHESNE	9/29/2012	10/24/12
WELL 1 COMMENTS GRRV S10 NWSW											
B	99999	17400	4301351173	GMBU L-9-9-16	SENE	9	9S	16E	DUCHESNE	9/18/2012	10/24/12
WELL 1 COMMENTS GRRV BHL: NWSW											
A	99999	18754	4301351412	LUSTY 1-11-3-3W	NENE	11	3S	3W	DUCHESNE	9/28/2012	10/24/12
WELL 1 COMMENTS WSTC NENE											
B	99999	17400	4301351249	GMBU E-16-9-17	SESE	8	9S	17E	DUCHESNE	10/1/2012	10/24/12
WELL 1 COMMENTS GRRV BHL: 16 NWNW											

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- A - Establish new entity for new well (single well only)
- B - Add new well to existing entity (group or unit well)
- C - Reassign well from one existing entity to another existing entity
- D - Reassign well from one existing entity to a new entity
- E - Other (explain in Comments section)

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OCT 12 2012


Signature
Tasha Robison
Production Clerk
10/03/12

NOTE: Use COMMENT section to explain why each Action Code was selected.

UNITED STATES
 DEPARTMENT OF THE INTERIOR
 BUREAU OF LAND MANAGEMENT

FORM APPROVED
 OMB NO. 1 004-0137
 Expires: October 31, 2014

WELL COMPLETION OR RECOMPLETION REPORT AND LOG

5. Lease Serial No.
PATENTED

1a. Type of Well Oil Well Gas Well Dry Other
 b. Type of Completion: New Well Work Over Deepen Plug Back Diff. Resrv.,
 Other: _____

6. If Indian, Allottee or Tribe Name

7. Unit or CA Agreement Name and No.

2. Name of Operator
NEWFIELD PRODUCTION COMPANY

8. Lease Name and Well No.
MORRILL 4-23-3-ZWH

3. Address **ROUTE #3 BOX 3630
 MYTON, UT 84052**

3a. Phone No. (include area code)
Ph:435-646-3721

9. API Well No.
43-013-51390

4. Location of Well (Report location clearly and in accordance with Federal requirements)*

At surface **168' FNL 1423' FWL (NE/NW) SEC 23 T3S R2W**

10. Field and Pool or Exploratory

At top prod. interval reported below **823' FNL 770' FWL (NW/NW) SEC 23 T3S R2W**

11. Sec., T., R., M., on Block and Survey or Area
SEC 23 T3S R2W

At total depth **717' FSL 845' FWL (SW/SW) SEC 23 T3S R2W**

12. County or Parish **DUCHESNE** 13. State **UT**

14. Date Spudded **09/11/2012** 15. Date T.D. Reached **10/28/2012**

16. Date Completed **11/19/2012**
 D & A Ready to Prod.

17. Elevations (DF, RKB, RT, GL)*
5271' GL 5289' KB

18. Total Depth: MD **12720'**
 TVD **8408'**

19. Plug Back T.D.: MD **12,696'**
 TVD

20. Depth Bridge Plug Set: MD
 TVD

21. Type Electric & Other Mechanical Logs Run (Submit copy of each)
DUAL IND GRD, SP, COMP. NEUTRON, GR, CALIPER, CMT BOND

22. Was well cored? No Yes (Submit analysis)
 Was DST run? No Yes (Submit report)
 Directional Survey? No Yes (Submit copy)

23. Casing and Liner Record (Report all strings set in well)

Hole Size	Size/Grade	Wt. (#/ft.)	Top (MD)	Bottom (MD)	Stage Cementer Depth	No. of Sk. & Type of Cement	Slurry Vol. (BBL)	Cement Top*	Amount Pulled
13-1/2"	9-5/8" J-55	36	0'	2567'		240 Class G			
						556 Premium lite			
8-7/8"	7" P-110	26	0'	8891'		355 Bondcem		4892'	
						660 Versacem			
6-1/4"	4.5" P-110	13.5	7941'	12709'					

24. Tubing Record

Size	Depth Set (MD)	Packer Depth (MD)	Size	Depth Set (MD)	Packer Depth (MD)	Size	Depth Set (MD)	Packer Depth (MD)
2-7/8"	EOT@7856'	XN@7820'						

25. Producing Intervals

Formation	Top	Bottom	Perforated Interval	Size	No. Holes	Perf. Status
A) Green River	8944'	12440'	8944' - 12440' MD			SLIDING SLEEVE
B)						
C)						
D)						

27. Acid, Fracture, Treatment, Cement Squeeze, etc.

Depth Interval	Amount and Type of Material
8944' - 12440' MD	Frac w/81,500#s of 100 mesh and 1,696,020#s of 20/40 sand in 34,491 bbls of Lightning 17 fluid, in 19 stages.

28. Production - Interval A

Date First Produced	Test Date	Hours Tested	Test Production	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
11/20/14	11/30/14	24	➔	522	305	208			GAS LIFT
Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status	
			➔					PRODUCING	

28a. Production - Interval B

Date First Produced	Test Date	Hours Tested	Test Production	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
			➔						
Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status	
			➔						

*(See instructions and spaces for additional data on page 2)

28b. Production - Interval C

Date First Produced	Test Date	Hours Tested	Test Production →	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate →	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status	

28c. Production - Interval D

Date First Produced	Test Date	Hours Tested	Test Production →	Oil BBL	Gas MCF	Water BBL	Oil Gravity Corr. API	Gas Gravity	Production Method
Choke Size	Tbg. Press. Flwg. SI	Csg. Press.	24 Hr. Rate →	Oil BBL	Gas MCF	Water BBL	Gas/Oil Ratio	Well Status	

29. Disposition of Gas (Solid, used for fuel, vented, etc.)

30. Summary of Porous Zones (Include Aquifers):

Show all important zones of porosity and contents thereof: Cored intervals and all drill-stem tests, including depth interval tested, cushion used, time tool open, flowing and shut-in pressures and recoveries.

31. Formation (Log) Markers
GEOLOGICAL MARKERS

Formation	Top	Bottom	Descriptions, Contents, etc.	Name	Top
					Meas. Depth
				GARDEN GULCH MARK GARDEN GULCH 1	6499' 6651'
				DOUGLAS CREEK B LIMESTONE	7367' 7857'
				CASTLEL PEAK UTELAND BUTTE	8228' 8522'
				UTELAND BUTTE C WASATCH	8578' 8655'

32. Additional remarks (include plugging procedure):

33. Indicate which items have been attached by placing a check in the appropriate boxes:

- Electrical/Mechanical Logs (1 full set req'd.)
 Geologic Report
 DST Report
 Directional Survey
 Sundry Notice for plugging and cement verification
 Core Analysis
 Other: Drilling daily activity

34. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records (see attached instructions)*

Name (please print) Heather Calder Title Regulatory Technician
 Signature Heather Calder Date 04/02/2014

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

Newfield Exploration Company

Duchesne County, UT

Sec. 23-T3S-R2W

Morrill 4-23-3-2WH

Plan D Rev 0

Survey: Sperry Surveys

Job No. Combined as per Customer

Sperry Drilling Services

Standard Report

24 October, 2012

Well Coordinates: 7,250,016.37 N, 2,036,698.56 E (40° 12' 52.35" N, 110° 04' 51.27" W)

Ground Level: 5,270.00 ft

Local Coordinate Origin:	Centered on Well Morrill 4-23-3-2WH
Viewing Datum:	RKB 18' @ 5288.00ft (Pioneer 69)
TVDs to System:	N
North Reference:	True
Unit System:	API - US Survey Feet - Custom

Geodetic Scale Factor Applied

Version: 2003.16 Build: 43I

HALLIBURTON

RECEIVED: Apr. 02, 2014

HALLIBURTON**Survey Report for Morrill 4-23-3-2WH - Sperry Surveys**

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)
2,501.00	0.20	84.30	2,500.84	-11.67	7.29	10.49	0.00
2,577.00	0.29	57.41	2,576.84	-11.55	7.58	10.33	0.19
2,639.00	1.32	317.33	2,638.83	-10.94	7.23	9.78	2.26
2,670.00	1.98	312.58	2,669.82	-10.31	6.59	9.25	2.17
2,701.00	3.20	295.91	2,700.79	-9.57	5.42	8.69	4.59
2,732.00	4.63	291.47	2,731.72	-8.74	3.48	8.14	4.71
2,763.00	5.92	291.17	2,762.59	-7.70	0.82	7.50	4.16
2,794.00	6.92	287.90	2,793.39	-6.55	-2.45	6.84	3.43
2,825.00	7.92	289.74	2,824.13	-5.26	-6.23	6.10	3.32
2,857.00	8.67	288.10	2,855.80	-3.76	-10.60	5.25	2.46
2,888.00	8.89	288.45	2,886.43	-2.28	-15.10	4.43	0.73
2,919.00	9.19	287.65	2,917.05	-0.77	-19.73	3.61	1.05
2,981.00	9.42	283.30	2,978.23	1.90	-29.38	2.37	1.19
3,013.00	9.35	277.88	3,009.80	2.86	-34.51	2.16	2.77
3,074.00	9.21	274.41	3,070.01	3.91	-44.28	2.53	0.95
3,105.00	9.43	274.20	3,100.60	4.29	-49.29	2.88	0.72
3,137.00	9.50	273.41	3,132.16	4.64	-54.54	3.29	0.46
3,168.00	8.20	269.48	3,162.79	4.77	-59.30	3.85	4.62
3,199.00	8.18	269.19	3,193.48	4.72	-63.72	4.54	0.15
3,229.00	8.47	266.31	3,223.16	4.55	-68.06	5.33	1.69
3,260.00	8.05	269.73	3,253.84	4.39	-72.51	6.13	2.08
3,322.00	8.32	270.73	3,315.21	4.43	-81.33	7.37	0.49
3,384.00	7.81	266.90	3,376.59	4.26	-90.02	8.80	1.19
3,446.00	7.21	268.59	3,438.06	3.93	-98.12	10.29	1.03
3,509.00	7.18	266.30	3,500.57	3.58	-106.00	11.77	0.46
3,570.00	7.09	267.94	3,561.09	3.20	-113.57	13.24	0.37
3,632.00	7.64	265.82	3,622.58	2.76	-121.50	14.82	0.99
3,694.00	7.11	267.03	3,684.07	2.26	-129.44	16.46	0.89
3,756.00	6.51	265.02	3,745.63	1.76	-136.78	18.02	1.04
3,818.00	6.72	274.44	3,807.22	1.73	-143.90	19.08	1.78
3,880.00	6.66	277.53	3,868.80	2.49	-151.08	19.37	0.59
3,942.00	7.00	275.65	3,930.36	3.33	-158.40	19.59	0.66
4,004.00	7.93	279.06	3,991.83	4.38	-166.38	19.71	1.66
4,066.00	7.59	275.57	4,053.26	5.45	-174.68	19.85	0.94
4,128.00	7.47	277.81	4,114.73	6.39	-182.75	20.08	0.51
4,190.00	7.03	271.48	4,176.24	7.04	-190.54	20.57	1.47
4,252.00	6.64	272.60	4,237.79	7.30	-197.91	21.38	0.66
4,314.00	6.64	271.74	4,299.38	7.57	-205.07	22.14	0.16
4,345.00	7.63	270.12	4,330.14	7.63	-208.92	22.64	3.26
4,408.00	6.80	269.11	4,392.64	7.58	-216.84	23.83	1.33
4,470.00	8.26	272.16	4,454.10	7.69	-224.96	24.90	2.44
4,532.00	8.02	272.84	4,515.48	8.07	-233.73	25.79	0.42
4,594.00	7.62	265.05	4,576.90	7.93	-242.14	27.14	1.83
4,656.00	8.11	271.50	4,638.32	7.69	-250.61	28.60	1.63
4,718.00	7.41	271.44	4,699.75	7.91	-258.98	29.60	1.13
4,780.00	7.18	268.86	4,761.25	7.93	-266.85	30.71	0.65
4,811.00	7.18	270.09	4,792.01	7.89	-270.72	31.31	0.50
4,842.00	7.03	273.12	4,822.77	8.00	-274.56	31.76	1.30
4,905.00	7.41	270.46	4,885.27	8.24	-282.47	32.66	0.80
4,967.00	6.45	267.30	4,946.82	8.11	-289.94	33.87	1.67

HALLIBURTON**Survey Report for Morrill 4-23-3-2WH - Sperry Surveys**

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)
5,029.00	7.14	269.76	5,008.38	7.93	-297.28	35.11	1.21
5,091.00	7.45	276.06	5,069.88	8.34	-305.13	35.84	1.38
5,153.00	7.15	274.59	5,131.38	9.07	-312.97	36.25	0.57
5,215.00	5.88	266.23	5,192.98	9.17	-319.98	37.16	2.55
5,277.00	5.99	271.35	5,254.65	9.04	-326.39	38.22	0.87
5,340.00	5.62	260.75	5,317.32	8.62	-332.72	39.55	1.80
5,402.00	6.08	275.67	5,379.01	8.46	-338.98	40.61	2.55
5,433.00	5.77	275.80	5,409.84	8.78	-342.17	40.76	1.00
5,464.00	6.22	279.95	5,440.67	9.22	-345.37	40.78	2.01
5,526.00	8.44	283.86	5,502.16	10.89	-353.10	40.24	3.67
5,588.00	7.91	274.69	5,563.53	12.33	-361.77	40.07	2.27
5,650.00	6.63	275.05	5,625.03	13.00	-369.59	40.54	2.07
5,712.00	6.99	270.32	5,686.60	13.33	-376.92	41.27	1.07
5,775.00	8.17	277.38	5,749.05	13.93	-385.20	41.87	2.38
5,837.00	7.69	272.38	5,810.45	14.67	-393.71	42.37	1.35
5,899.00	8.32	273.30	5,871.85	15.10	-402.33	43.19	1.04
5,930.00	7.53	267.64	5,902.55	15.14	-406.60	43.77	3.58
5,992.00	6.94	265.73	5,964.06	14.70	-414.40	45.33	1.03
6,054.00	7.90	263.38	6,025.54	13.93	-422.36	47.25	1.62
6,116.00	8.50	266.02	6,086.91	13.12	-431.17	49.32	1.14
6,178.00	7.85	263.19	6,148.28	12.30	-439.94	51.40	1.23
6,240.00	7.37	260.20	6,209.73	11.12	-448.07	53.74	1.00
6,302.00	7.44	265.59	6,271.21	10.13	-455.99	55.86	1.13
6,364.00	8.20	268.95	6,332.64	9.74	-464.41	57.46	1.43
6,426.00	7.82	266.21	6,394.03	9.38	-473.04	59.07	0.87
6,488.00	7.81	265.09	6,455.46	8.75	-481.45	60.91	0.25
6,550.00	7.01	260.22	6,516.94	7.74	-489.37	63.05	1.64
6,612.00	6.72	261.98	6,578.49	6.59	-496.69	65.24	0.58
6,643.00	7.35	261.51	6,609.26	6.05	-500.45	66.33	2.04
6,674.00	6.46	258.11	6,640.03	5.40	-504.12	67.50	3.16
6,705.00	6.35	260.45	6,670.84	4.75	-507.51	68.63	0.91
6,767.00	5.84	254.92	6,732.49	3.36	-513.94	70.93	1.25
6,829.00	6.73	255.78	6,794.12	1.65	-520.51	73.58	1.44
6,891.00	6.18	252.24	6,855.72	-0.26	-527.21	76.44	1.09
6,953.00	5.40	244.94	6,917.41	-2.52	-533.03	79.51	1.73
7,015.00	4.64	238.32	6,979.17	-5.07	-537.81	82.72	1.54
7,077.00	4.95	241.68	7,040.95	-7.65	-542.29	85.93	0.67
7,139.00	5.40	239.98	7,102.70	-10.38	-547.18	89.34	0.77
7,201.00	5.53	240.51	7,164.42	-13.31	-552.30	92.98	0.22
7,263.00	5.17	234.41	7,226.15	-16.41	-557.17	96.74	1.08
7,325.00	4.97	232.60	7,287.91	-19.67	-561.58	100.60	0.41
7,387.00	4.24	223.28	7,349.71	-22.97	-565.28	104.40	1.68
7,449.00	4.36	221.97	7,411.53	-26.39	-568.43	108.24	0.25
7,511.00	3.93	215.29	7,473.37	-29.87	-571.23	112.10	1.04
7,573.00	3.82	219.66	7,535.23	-33.20	-573.78	115.76	0.51
7,604.00	3.78	224.32	7,566.16	-34.72	-575.15	117.46	1.00
7,665.00	3.64	218.29	7,627.03	-37.68	-577.76	120.77	0.68
7,728.00	3.50	210.83	7,689.91	-40.90	-579.98	124.28	0.77
7,790.00	3.42	213.10	7,751.80	-44.08	-581.96	127.70	0.26
7,851.00	3.47	217.50	7,812.69	-47.07	-584.08	130.97	0.44

HALLIBURTON**Survey Report for Morrill 4-23-3-2WH - Sperry Surveys**

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)
7,913.00	2.88	210.49	7,874.59	-49.90	-586.01	134.05	1.14
7,970.00	2.54	214.40	7,931.53	-52.17	-587.45	136.51	0.68
8,041.00	5.45	204.27	8,002.35	-56.55	-589.73	141.16	4.20
8,072.00	9.56	196.75	8,033.08	-60.35	-591.08	145.13	13.60
8,103.00	13.54	193.67	8,063.45	-66.35	-592.68	151.29	12.99
8,134.00	17.04	192.62	8,093.34	-74.31	-594.53	159.43	11.33
8,165.00	18.92	194.23	8,122.83	-83.61	-596.75	168.96	6.27
8,196.00	19.87	200.34	8,152.07	-93.43	-599.82	179.12	7.22
8,227.00	20.92	203.17	8,181.13	-103.45	-603.83	189.62	4.65
8,258.00	23.41	201.45	8,209.84	-114.28	-608.26	200.97	8.30
8,289.00	26.08	200.03	8,237.99	-126.41	-612.85	213.64	8.82
8,320.00	28.49	196.12	8,265.54	-139.92	-617.23	227.64	9.68
8,351.00	31.73	194.03	8,292.35	-154.94	-621.27	243.08	10.98
8,382.00	35.10	192.68	8,318.23	-171.54	-625.20	260.08	11.13
8,413.00	38.22	189.97	8,343.09	-189.69	-628.82	278.56	11.34
8,444.00	40.54	187.32	8,367.05	-209.13	-631.76	298.22	9.24
8,475.00	43.48	185.62	8,390.09	-229.74	-634.09	318.95	10.17
8,506.00	46.85	184.60	8,411.94	-251.64	-636.04	340.90	11.12
8,537.00	50.17	183.94	8,432.47	-274.79	-637.77	364.06	10.83
8,568.00	52.59	182.66	8,451.82	-298.97	-639.16	388.18	8.45
8,599.00	55.59	182.13	8,470.00	-324.05	-640.20	413.16	9.78
8,630.00	58.22	182.09	8,486.93	-350.00	-641.16	438.97	8.48
8,661.00	61.18	181.66	8,502.57	-376.75	-642.03	465.57	9.62
8,692.00	64.24	181.30	8,516.78	-404.29	-642.74	492.92	9.92
8,723.00	68.84	181.77	8,529.12	-432.71	-643.51	521.15	14.90
8,754.00	73.25	182.31	8,539.18	-462.00	-644.55	550.29	14.32
8,785.00	78.15	182.18	8,546.84	-492.01	-645.73	580.15	15.81
8,816.00	82.84	181.87	8,551.96	-522.55	-646.81	610.53	15.16
8,847.00	87.45	182.05	8,554.58	-553.42	-647.86	641.22	14.88
8,902.00	91.48	183.60	8,555.09	-608.33	-650.57	695.95	7.85
8,920.00	91.67	183.67	8,554.60	-626.29	-651.72	713.89	1.12
8,949.00	92.35	183.18	8,553.58	-655.22	-653.45	742.76	2.89
8,981.00	94.70	182.96	8,551.61	-687.11	-655.16	774.57	7.38
9,013.00	96.00	182.35	8,548.63	-718.94	-656.63	806.27	4.48
9,045.00	94.76	181.42	8,545.63	-750.78	-657.68	837.93	4.84
9,076.00	94.70	181.22	8,543.07	-781.67	-658.39	868.60	0.67
9,108.00	94.70	180.60	8,540.45	-813.55	-658.90	900.22	1.93
9,140.00	93.90	179.70	8,538.05	-845.46	-658.98	931.81	3.76
9,172.00	93.71	179.71	8,535.93	-877.39	-658.82	963.38	0.59
9,203.00	93.21	179.68	8,534.06	-908.33	-658.65	993.97	1.62
9,236.00	92.72	179.08	8,532.35	-941.29	-658.30	1,026.53	2.35
9,267.00	91.79	179.07	8,531.13	-972.26	-657.80	1,057.10	3.00
9,299.00	92.90	179.52	8,529.82	-1,004.23	-657.40	1,088.68	3.74
9,331.00	91.48	180.30	8,528.60	-1,036.21	-657.35	1,120.31	5.06
9,363.00	92.41	181.52	8,527.51	-1,068.18	-657.86	1,152.03	4.79
9,395.00	90.43	180.82	8,526.72	-1,100.16	-658.51	1,183.77	6.56
9,427.00	89.69	180.51	8,526.69	-1,132.16	-658.89	1,215.48	2.51
9,458.00	90.00	180.00	8,526.77	-1,163.16	-659.02	1,246.18	1.93
9,490.00	93.71	181.54	8,525.73	-1,195.13	-659.45	1,277.88	12.55
9,522.00	93.09	181.10	8,523.84	-1,227.07	-660.19	1,309.59	2.37
9,553.00	91.73	180.55	8,522.53	-1,258.04	-660.63	1,340.29	4.73

HALLIBURTON**Survey Report for Morrill 4-23-3-2WH - Sperry Surveys**

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)
9,585.00	92.65	180.34	8,521.31	-1,290.01	-660.88	1,371.97	2.95
9,617.00	93.10	180.74	8,519.70	-1,321.97	-661.18	1,403.64	1.88
9,648.00	92.65	180.33	8,518.15	-1,352.93	-661.47	1,434.31	1.96
9,680.00	92.35	180.07	8,516.75	-1,384.90	-661.58	1,465.96	1.24
9,712.00	92.65	180.71	8,515.36	-1,416.87	-661.80	1,497.63	2.21
9,743.00	93.03	180.81	8,513.82	-1,447.83	-662.21	1,528.32	1.27
9,775.00	93.46	180.95	8,512.01	-1,479.77	-662.70	1,560.00	1.41
9,807.00	91.98	180.64	8,510.49	-1,511.73	-663.15	1,591.69	4.73
9,838.00	91.42	181.02	8,509.57	-1,542.72	-663.60	1,622.41	2.18
9,870.00	89.69	180.12	8,509.26	-1,574.71	-663.91	1,654.12	6.09
9,902.00	89.75	181.28	8,509.42	-1,606.71	-664.31	1,685.83	3.63
9,933.00	90.37	181.19	8,509.39	-1,637.70	-664.97	1,716.60	2.02
9,965.00	90.37	181.35	8,509.18	-1,669.69	-665.68	1,748.36	0.50
9,997.00	91.86	179.62	8,508.56	-1,701.68	-665.95	1,780.05	7.13
10,028.00	92.47	179.31	8,507.39	-1,732.66	-665.66	1,810.66	2.21
10,060.00	93.16	179.14	8,505.81	-1,764.62	-665.23	1,842.22	2.22
10,092.00	90.74	178.91	8,504.73	-1,796.59	-664.69	1,873.78	7.60
10,124.00	90.74	179.28	8,504.31	-1,828.58	-664.18	1,905.37	1.16
10,155.00	92.90	179.94	8,503.33	-1,859.57	-663.97	1,935.99	7.29
10,187.00	93.71	180.47	8,501.48	-1,891.51	-664.09	1,967.62	3.02
10,219.00	94.32	179.81	8,499.24	-1,923.43	-664.16	1,999.22	2.80
10,251.00	95.50	180.39	8,496.50	-1,955.32	-664.22	2,030.77	4.11
10,283.00	95.01	180.11	8,493.57	-1,987.18	-664.36	2,062.32	1.76
10,314.00	94.15	180.19	8,491.10	-2,018.08	-664.44	2,092.91	2.79
10,346.00	94.20	180.32	8,488.77	-2,050.00	-664.58	2,124.51	0.43
10,378.00	94.45	179.63	8,486.35	-2,081.90	-664.57	2,156.08	2.29
10,409.00	94.39	179.55	8,483.96	-2,112.81	-664.35	2,186.63	0.32
10,441.00	95.01	179.66	8,481.34	-2,144.70	-664.13	2,218.16	1.97
10,473.00	93.95	178.77	8,478.84	-2,176.60	-663.69	2,249.66	4.32
10,505.00	93.27	178.45	8,476.83	-2,208.53	-662.91	2,281.14	2.35
10,537.00	92.10	177.75	8,475.33	-2,240.47	-661.85	2,312.60	4.26
10,568.00	91.61	176.96	8,474.33	-2,271.43	-660.42	2,343.02	3.00
10,600.00	90.74	177.35	8,473.67	-2,303.38	-658.84	2,374.40	2.98
10,632.00	90.87	177.00	8,473.22	-2,335.34	-657.26	2,405.80	1.17
10,663.00	90.43	176.93	8,472.87	-2,366.29	-655.62	2,436.19	1.44
10,695.00	90.25	176.82	8,472.68	-2,398.24	-653.87	2,467.56	0.66
10,727.00	90.68	176.85	8,472.42	-2,430.19	-652.11	2,498.92	1.35
10,759.00	89.26	177.49	8,472.44	-2,462.15	-650.53	2,530.31	4.87
10,790.00	88.46	177.54	8,473.05	-2,493.12	-649.18	2,560.76	2.59
10,822.00	89.07	177.95	8,473.74	-2,525.09	-647.92	2,592.21	2.30
10,854.00	90.74	178.70	8,473.80	-2,557.07	-646.99	2,623.72	5.72
10,886.00	92.78	178.64	8,472.81	-2,589.04	-646.25	2,655.25	6.38
10,917.00	92.85	179.39	8,471.29	-2,620.00	-645.71	2,685.81	2.43
10,949.00	93.77	179.44	8,469.44	-2,651.95	-645.39	2,717.37	2.88
10,981.00	93.52	179.32	8,467.41	-2,683.88	-645.04	2,748.92	0.87
11,013.00	92.23	179.35	8,465.80	-2,715.84	-644.67	2,780.49	4.03
11,044.00	91.55	178.72	8,464.78	-2,746.82	-644.15	2,811.07	2.99
11,076.00	92.22	179.17	8,463.73	-2,778.79	-643.56	2,842.62	2.52
11,108.00	92.23	179.10	8,462.49	-2,810.76	-643.08	2,874.19	0.22
11,139.00	90.99	178.38	8,461.61	-2,841.74	-642.40	2,904.74	4.62
11,171.00	90.56	178.27	8,461.18	-2,873.73	-641.46	2,936.26	1.39

HALLIBURTON

Duchesne County, UT

Survey Report for Morrill 4-23-3-2WH - Sperry Surveys

Measured Depth (ft)	Inclination (°)	Azimuth (°)	Vertical Depth (ft)	+N/-S (ft)	+E/-W (ft)	Vertical Section (ft)	Dogleg Rate (°/100ft)
11,203.00	90.06	178.23	8,461.01	-2,905.71	-640.48	2,967.76	1.57
11,235.00	91.11	178.83	8,460.68	-2,937.70	-639.66	2,999.30	3.78
11,267.00	91.79	179.83	8,459.87	-2,969.69	-639.29	3,030.89	3.78
11,298.00	92.78	180.42	8,458.64	-3,000.66	-639.36	3,061.55	3.72
11,329.00	93.89	180.96	8,456.83	-3,031.61	-639.73	3,092.23	3.98
11,360.00	93.89	180.47	8,454.73	-3,062.53	-640.12	3,122.89	1.58
11,392.00	93.28	180.41	8,452.73	-3,094.47	-640.36	3,154.52	1.92
11,424.00	90.80	180.04	8,451.59	-3,126.45	-640.49	3,186.18	7.84
11,455.00	90.99	179.54	8,451.11	-3,157.44	-640.37	3,216.84	1.73
11,487.00	90.62	179.52	8,450.66	-3,189.44	-640.11	3,248.46	1.16
11,518.00	90.31	180.00	8,450.40	-3,220.44	-639.98	3,279.11	1.84
11,550.00	93.34	181.58	8,449.39	-3,252.41	-640.42	3,310.82	10.68
11,582.00	92.66	181.05	8,447.71	-3,284.36	-641.15	3,342.53	2.69
11,613.00	90.74	179.67	8,446.79	-3,315.34	-641.35	3,373.22	7.63
11,644.00	91.92	180.13	8,446.07	-3,346.33	-641.29	3,403.88	4.09
11,676.00	90.68	179.49	8,445.35	-3,378.32	-641.19	3,435.52	4.36
11,707.00	92.47	180.04	8,444.49	-3,409.31	-641.06	3,466.16	6.04
11,738.00	91.61	179.51	8,443.39	-3,440.29	-640.94	3,496.80	3.26
11,770.00	92.35	179.39	8,442.28	-3,472.27	-640.63	3,528.40	2.34
11,802.00	91.79	178.29	8,441.13	-3,504.24	-639.99	3,559.94	3.86
11,833.00	90.49	177.30	8,440.51	-3,535.21	-638.79	3,590.41	5.27
11,865.00	91.79	177.59	8,439.87	-3,567.17	-637.37	3,621.83	4.16
11,897.00	91.73	177.26	8,438.89	-3,599.13	-635.93	3,653.24	1.05
11,929.00	91.73	177.55	8,437.93	-3,631.08	-634.48	3,684.65	0.91
11,991.00	92.60	177.47	8,435.58	-3,692.97	-631.79	3,745.51	1.41
12,055.00	91.30	176.55	8,433.41	-3,756.85	-628.45	3,808.23	2.49
12,118.00	92.35	176.88	8,431.40	-3,819.71	-624.85	3,869.91	1.75
12,182.00	92.78	176.83	8,428.54	-3,883.55	-621.34	3,932.58	0.68
12,245.00	92.72	176.84	8,425.51	-3,946.38	-617.86	3,994.25	0.10
12,308.00	92.22	176.75	8,422.80	-4,009.23	-614.34	4,055.92	0.81
12,370.00	92.16	176.45	8,420.43	-4,071.07	-610.67	4,116.59	0.49
12,434.00	92.35	175.88	8,417.91	-4,134.88	-606.39	4,179.11	0.94
12,496.00	92.22	174.95	8,415.44	-4,196.63	-601.44	4,239.49	1.51
12,559.00	91.67	173.91	8,413.30	-4,259.29	-595.33	4,300.62	1.87
12,622.00	92.41	174.24	8,411.06	-4,321.92	-588.83	4,361.65	1.29
12,662.00	91.79	173.79	8,409.59	-4,361.67	-584.66	4,400.38	1.91
12,720.00	91.79	173.79	8,407.78	-4,419.30	-578.39	4,456.50	0.00

Projection To Bit

Survey Annotations

Measured Depth (ft)	Vertical Depth (ft)	Local Coordinates		Comment
		+N/-S (ft)	+E/-W (ft)	
12,720.00	8,407.78	-4,419.30	-578.39	Projection To Bit

HALLIBURTON

Survey Report for Morrill 4-23-3-2WH - Sperry Surveys

Vertical Section Information

Angle Type	Target	Azimuth (°)	Origin Type	Origin +N/_S (ft)	Origin +E/-W (ft)	Start TVD (ft)
User	No Target (Freehand)	188.31	Slot	0.00	0.00	0.00

Survey tool program

From (ft)	To (ft)	Survey/Plan	Survey Tool
73.00	2,501.00	Payzone Directional	NS-GYRO-MS
2,577.00	12,720.00	Sperry Surveys	MWD

Targets

Target Name - hit/miss target - Shape	Dip Angle (°)	Dip Dir. (°)	TVD (ft)	+N/-S (ft)	+E/-W (ft)	Northing (ft)	Easting (ft)	Latitude	Longitude
Morrill 4-23-3-2WH_! - survey misses target center by 2500.88ft at 2501.00ft MD (2500.84 TVD, -11.67 N, 7.29 E) - Point	0.00	0.00	0.00	0.02	0.00	7,250,016.40	2,036,698.56	40° 12' 52.350 N	110° 4' 51.270 W
Morrill 4-23-3-2WH_! - survey misses target center by 2500.88ft at 2501.00ft MD (2500.84 TVD, -11.67 N, 7.29 E) - Polygon	0.00	0.00	0.00	0.02	0.00	7,250,016.40	2,036,698.56	40° 12' 52.350 N	110° 4' 51.270 W
Morrill 4-23-3-2WH_! - survey misses target center by 2500.88ft at 2501.00ft MD (2500.84 TVD, -11.67 N, 7.29 E) - Polygon	0.00	0.00	0.00	0.02	0.00	7,250,016.40	2,036,698.56	40° 12' 52.350 N	110° 4' 51.270 W
Morrill 4-23-3-2WH_ - survey misses target center by 71.20ft at 12712.77ft MD (8408.01 TVD, -4412.12 N, -579.17 E) - Point	0.00	0.00	8,432.75	-4,420.11	-645.45	7,245,586.93	2,036,123.36	40° 12' 8.670 N	110° 4' 59.588 W
Morrill 4-23-3-2WH_ - survey misses target center by 13.20ft at 8835.10ft MD (8553.87 TVD, -541.54 N, -647.45 E) - Point	0.00	0.00	8,558.05	-540.76	-659.94	7,249,465.26	2,036,047.34	40° 12' 47.006 N	110° 4' 59.777 W



North Reference Sheet for Sec. 23-T3S-R2W - Morrill 4-23-3-2WH - Plan D Rev 0

All data is in US Feet unless otherwise stated. Directions and Coordinates are relative to True North Reference.

Vertical Depths are relative to RKB 18' @ 5288.00ft (Pioneer 69). Northing and Easting are relative to Morrill 4-23-3-2WH
 Coordinate System is US State Plane 1983, Utah Central Zone using datum North American Datum 1983, ellipsoid GRS 1980
 Projection method is Lambert Conformal Conic (2 parallel)
 Central Meridian is 111° 30' 0.000 W°, Longitude Origin:0° 0' 0.000 E°, Latitude Origin:40° 39' 0.000 N°
 False Easting: 1,640,416.67ft, False Northing: 6,561,666.67ft, Scale Reduction: 0.99992072

Grid Coordinates of Well: 7,250,016.37 ft N, 2,036,698.56 ft E
 Geographical Coordinates of Well: 40° 12' 52.35" N, 110° 04' 51.27" W
 Grid Convergence at Surface is: 0.91°

Based upon Minimum Curvature type calculations, at a Measured Depth of 12,720.00ft
 the Bottom Hole Displacement is 4,456.99ft in the Direction of 187.46° (True).

Magnetic Convergence at surface is: -10.30° (30 September 2012, , BGGM2012)

Magnetic Model: BGGM2012
 Date: 30-Sep-12
 Declination: 11.21°
 Inclination/Dip: 65.88°
 Field Strength: 52177

Grid North is 0.91° East of True North (Grid Convergence)
 Magnetic North is 11.21° East of True North (Magnetic Declination)
 Magnetic North is 10.30° East of Grid North (Magnetic Convergence)

To convert a True Direction to a Grid Direction, Subtract 0.91°
 To convert a Magnetic Direction to a True Direction, Add 11.21° East
 To convert a Magnetic Direction to a Grid Direction, Add 10.30°

Daily Activity Report

Format For Sundry

MORRILL 4-23-3-2WH

11/1/2012 To 3/28/2013

11/1/2012 Day: 1

Completion

Rigless on 11/1/2012 - MIRU WSU and bop stack - 2145 PM Weatherford BOP's arrived, NU stack consisting of 7 1/16 frac Valve already on well, 7 1/16? 10K X 7 1/16? 5K adaptor spool, 7 1/16? 5K double BOP Blind rams on bottom with 2 1/16? duel outlets with two 2 1/16 valves on each side, 4 ?? pipe rams on top, 7 1/16? 5K single BOP dressed with 4 ?? pipe rams. Start NU bop stack, prepare to pressure test stack. - Spot in EWL trk and crane. NU WL BOP and lubricator. PU 3.71 gauge ring and junk basket. Pressure test lubricator to 5000 psi for 5 minutes, no leak off. RIH. Could not get in liner top at 7929?. POH. LD gauge ring and junk basket. PU GR and CBL tools. Test lubricator to 5000 psi for 5 minutes, OK. Run GR/CCL/CBL logs from 8096? to 7096?. Run GR/CCL/CBL logs from 8096? to surface under 1500 psi. Correlate logs to Halliburton Open Hole log dated 10/10/12. TOC at 4892?. ND lubricator and WL BOP. Move off EWL equipment. - MIRU Western W.S. Rig #1. - Wait on BOP.

Daily Cost: \$0

Cumulative Cost: \$22,172

11/2/2012 Day: 2

Completion

Rigless on 11/2/2012 - TIH with 4 1/2" frac string, nu frac stack - 2300 PM Cameron arrived with adaptor flange for extended neck hanger resume NU frac stack - 2000 PM Weatherford 4 1/16? 10K frac stack arrived, ND 7 1/16? 10K frac valve and NU 4 1/16? frac stack consisting of 7 1/16? 10K X 4 1/16? 10K adaptor spool, 4 1/16? 10K HCR, 4 1/16? 10K manual frac valve, 4 1/16? 10K flow cross with duel 2 1/16? 10K valves, 4 1/16? 10K manual frac valve, 4 1/16? 10K tree cap with 10K needle valve with Gauge. 2030 PM Shut down waiting on Cameron to bring out adaptor flange for extended neck hanger. - Stand by for 4 1/16" 10K frac stack - ND BOP stack. - Continue to NU BOP stack, rig up floor on rig, prepare to start pressure testing - Circulate 280 bbl water with biocide. PU 187 jts 4 ??, 13.5#, P110, BT&C pipe. Tag liner at 7929?. Displace hole with 280 bbl water with biocide. Land tbg with frac string as follows: Halliburton Versaflex seal bore assembly (5.20" OD x 3.92" ID x 14.20' L); 185 jts 4 ??, 13.5#, P110, BT&C pipe; 1-10?, 1-8?, 1-6?, 2-4? x 4 ??, 13.5#, P110, BT&C pups; and 1 jt 4 ??, 13.5#, P110, BT&C pipe. String wt 134K. - PU Halliburton Versaflex seal bore assembly and 187 jts 4 ??, 13.5#, P110, BT&C frac string. Tag liner at 7929'. - Finish tallying 4 ?? frac string. RU csg crew. - 0130 AM BOP stack rigged up, start pressure testing 250 PSI low and 5,000 PSI high, MIRU weatherford CSG crew, set pipe racks and unload 4 ?? frac string, start cleaning threads and drifting CSG. 0500 AM pressure testing completed, Test good, 4 ?? frac string unloaded (193 JTS) Continue to drift, inspect, and clean threads. - Test annulus to 4010 psi for 10 minutes, lost 90 psi. Good test. RD csg crew. RD floor.

Daily Cost: \$0

Cumulative Cost: \$69,837

11/3/2012 Day: 3

Completion

Rigless on 11/3/2012 - NU and test frac tree. RDMO WOR. Prep for frac. - 0000 AM Continue rigging up Weatherford 4 1/16? 10K frac stack arrived, ND 7 1/16? 10K frac valve and NU 4 1/16? frac stack consisting of 7 1/16? 10K X 4 1/16? 10K adaptor spool, 4 1/16? 10K HCR, 4 1/16? 10K manual frac valve, 4 1/16? 10K flow cross with duel 2 1/16? 10K valves, 4 1/16? 10K manual frac valve, 4 1/16? 10K tree cap with 10K needle valve with Gauge. Start pressure testing frac stack 250 PSI low and 10,000 PSI high 0530 AM Pressure testing

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completed on frac stack 250 PSI low, 10,000 PSI high test good. RDMO weatherford test unit and stand by to RDMO WSU. - RDMO WOR.

Daily Cost: \$0

Cumulative Cost: \$89,410

11/5/2012 Day: 4**Completion**

Rigless on 11/5/2012 - Prep for frac - Stand by for weatherford to deliver HCR for ball drop manifold. - PJSM with all crew members on location, ND Weatherford 4 1/16" frac stack & NU Bronco 4 1/16" frac stack with 4 1/16" 10K ball catcher, and pressure test frac stack and flow back iron. frac tanks filled and heated to 90 degrees, water transfer rigged up and pump and lines filled and tested. Test good - MIRU Baker HF equipment, Drift pump lines with dummy plug drift good,

Daily Cost: \$0

Cumulative Cost: \$115,006

11/6/2012 Day: 5**Completion**

Rigless on 11/6/2012 - frac - Location Safety Mtg. Prime pumps and test lines to 9,650 psi, OK. Hydraulic Fracture Wasatch stage 3k as follows: Break down 8.8 bpm @ 4195 psi. Avg rate: 34.5 bpm, Avg press: 7275 psi, Max rate: 38.6 bpm, Max press: 7930 psi. FG.434. Total 0.5-1 ppg 100 mesh: 5406 lbs, Total .5-4 ppg 20/40 sand: 79560 lbs. Avg HHP: 6,152. Total load to recover 2,532 bbl. 100% of the designed proppant was placed on formation. GW-3LDF-8.8% (21.3), XLW-10A-4.2% (5.9), FRW-20-27.3% (6.8), CRB-LT-3.9% (4.8), NE-900-22.7% (37.1) Enzyme G HT III-26.8% (19.8), ClayCare-23.8% (25.3), Alpha 1427-5.9% (1.6) - 1615 PM Stage 2 completed pumped 85,729 LBS, Purposed 82,500, Dropped ball #3 (2.236?) Ball seated at 4,824 PSI, at 14.5 BPM and broke 4,934 PSI. had to shut down for check valve on 1 pump and check fluid ends on 4 pumps 1700 PM Started going through pumps and found rocks, nuts, found several seats and valves bad, presently changing seats and valves out on 4 pumps, and checking remaining pumps. FRW-20-25.8% (3.8), Scalesorb 3-3.5% (13.4), NE-900-18.7% (29.2) Enzyme G HT III-6.4% (4.5), ClayCare-8.9% (7.6), Alpha 1427-11.3% (2.4) - 1210 PM Start stage 1 HF. Stage #1 Pump Ball (2.099") @ 20 Reduced rate to 10.3 BPM at 5,700 - 4,690 psi- Ball Hit at 179 BBL before shift 4,690 PSI. Shifted at 6,209 PSI. after Shift 4,653 PSI. Start frac w/ 3,050 PSI. on Back Side . Rate 35 BPM 6,825 psi Frac w/ 3,000 LBS of 100 mesh, 50,620 LBS of 20/40 Prop in 1,372 BBL. Of X-Link. Avg treating pressure was 6,825 PSI @ Average rate 35 BPM. Pressure on N2 Bottle was 1,450 PSI. Regulator 236 PSI. 1300 PM Stage 1 completed pumped 53,620 LBS, Purposed 55,000, Dropped ball #2 (2.167?) 1315 PM Pumped 187 BBLS to sleeve and another 50 BBLS over and did not see ball seat, shut down and check lines for ball 1445 PM Pressure tested lines to 9,917 PSI test good resume HF stage 2 Stage #2 Pump Ball (2.167") @ 14.5 BPM 5,253 PSI Ball Hit at 160 BBL. Shifted at 5,253 PSI. Start frac w/ 3,121 PSI. on Back Side . Rate 34 BPM 6,772 PSI Frac w/ 5,449 LBS of 100 mesh, 80,280 LBS of 20/40 sand in 1,519 BBL. Of slick water. Avg treating pressure was 6,772 PSI @ Average rate 34 BPM. Pressure on N2 Bottle was 1,500 PSI. Regulator 236 PSI. - Stand by for weatherford to deliver HCR for ball drop manifold. - 0830 AM PJSM with all crews on location, All pumps and Ball drop rigged up with single pump, back side pump rigged up on 4 ?? X ?? with manual pop off, prepare to start pressure testing lines and setting pop offs - HCR for ball drop manifold on location. Install HCR. - 1030 AM Start pressure testing lines and pop offs. 1200 PM Pressure testing completed tested lines 9,933 PSI. main line pop off 9,700 PSI, Bottle 1,450 PSI, Regulator 236 PSI. Ball drop line tested to 10,000 PSI. pop off 8,800 psi. Back side line tested to 5,300 PSI. manual pop off 3,600 PSI. 9 5/8? CSG 4 PSI. 4 ?? X ?? holding 3,011 PSI. 1210 PM Start stage 1 HF.

Daily Cost: \$0

Cumulative Cost: \$182,880

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11/7/2012 Day: 6**Completion**

Rigless on 11/7/2012 - Frac - - Flowing well. 19:00-20:00 Recover 65 bbl water with 15% sand, 48/64? choke, 50 psi. 20:00-21:00 Recover 30 bbl water, paraffin, and oil. Light sand. 48/64? choke, 30-40 psi. 21:00-22:00 Recover 47 bbl water with light sand. 48/64? choke, 20 psi. 22:00-23:00 Recover 36 bbl water with trace sand. 48/64? choke, 20 psi. 23:00-24:00 Recover 35 bbl water with trace sand. 48/64? choke, 20 psi. Ttl water recovered since surge 302. - 1700 PM Well started lightly to tank at 25 PSI flowed back 55 BBLS on 48/64 ADJ choke, Started flowing from 25 to 50 PSI. Continue flowing well to tank. - 1545 PM Shut in flow back, pressure built up from 0 PSI to 3,229 PSI, started pumping 2.2 BPM and pressured up to 3,974 PSI to 9,513 PSI opened to tanks on 32/64 choke and bleed off to 0 PSI, Pressure up to 3,974 PSI to 9,513 PSI and surged back 6 times, surging back and shutting in, Opened choke and bleed off to 0 PSI and continue to monitor pressure - Location Safety Mtg. Prime pumps and test lines to 9,978 psi, OK. Hydraulic Fracture Wasatch stage 4 as follows: Break down 9.6 bpm @ 7705 psi. Avg rate: 27 bpm, Avg press: 8075 psi, Max rate: 31 bpm, Max press: 9425 psi. FG 0.434. Total 0.5-1 ppg 100 mesh: 5640 lbs, Total .5-4 ppg 20/40 sand: 67970 lbs. Avg HHP: 65403. Total load to recover 1841 bbls. 66.7% of the designed proppant was placed in formation. 1. 247 psi on N2 regulator, 1400 psi on bottle, Pop off set at 9660 psi. 2. Treating pressures higher than previous jobs, saw some large bumps in pressure when sand reached formation. 3. Lost three of six pumps during job, pumps jacking. Appear to be caused by rocks. 4. Had pressure start to climb during the 3.0ppg, cut sand and went to flush. 5. Had to kept reducing rate to stay under max pressure during flush. 6. Had approx 3,200psi drop in pressure during flush. Able to flush completely. 7. Pumped approx 73,610lbs of prop or 66.7% of designed volume. 8. Good job by crew working thru issues. Repair pumps. GW-3LDF-3.2% (7.7), XLW-10A-4.9% (6.8), FRW-20-51.7% (8.5), Scalesorb 3-5.9% (21.9), CRB-LT-13.9% (15.9), NE-900-17.6% (25.2) Enzyme G HT III-24% (16.8), ClayCare-8% (7.1), Alpha 1427-26% (5.8) - 0945 AM Pressure Tested lines 9,910 PSI test good open well with 3,048 PSI, opened to tanks on 24/64 choke and bleed off to 0 PSI, Pressure up to 3,700 PSI to 7,700 PSI and surged back 15 times, surged back and shut in pressure built up to 1,248 PSI for 30 MIN and opened to tank and bleed to 0 PSI with no flow. - 0740 AM Pressure testing completed tested lines 9,910 PSI. main line pop off 9,793 PSI, Bottle 2,100 PSI, Regulator 253 PSI. 9 5/8? CSG 0 PSI. 4 ?? X ?? holding 3,017 PSI. Well went to 0 PSI., close in flow back, start pumping at 3.8 BPM, pressure climbed to 9,639 PSI. Pumped 12 BBLS. and leveled out, surged well and bleed to 0 psi. brought pumps back on line at 3.5 BPM and pressured out at 9,453 PSI. Pumped 8 BBLS, Bleed off to 0 PSI. pressured up to 2950 PSI and held for 2 MIN, bring pressure up to 5,145 PSI and held for 2 MIN with no bleed off, pressure up to 7,578 PSI and hold for 2 MIN with no bleed off, pressure up to 9,142 PSI and hold for 2 MIN with no bleed off. Open to Tanks and bbleed down to 0 PSI and shut in and monitor pressure. Built 0 pressure in 15 MIN. Open up to tank with no flow - SICP 6950 psi. Flow well back. Recovered ball after 138 bbl. - Location Safety Mtg. Prime pumps and test lines to 9,950 psi, OK. Hydraulic Fracture Wasatch stage 5 as follows: Break down 21.8 bpm @ 7045 psi. Avg rate: 35 bpm, Avg press: 7120 psi, Max rate: 36 bpm, Max press: 9525 psi. FG 0.434. Total 0.5-1 ppg 100 mesh: 2,962 lbs, Total .5-6 ppg 20/40 sand: 107,320 lbs. Avg HHP: 6090. Total load to recover 1326 bbls. 78.2% of the designed proppant was placed on formation. 1. 247 psi on N2 regulator, 1400 psi on bottle, Pop off set at 9660 psi. 2. Lost pump in 2.0ppg sand stage, leaking suction cap, made rate up with rest of pumps. 3. Had a couple of pumps jacking through out job, adjusted rate as needed. 4. Had pressure increase with 5ppg sand on formation and 6ppg sand in the pipe. Went to flush a little early. 5. Were only able to flush well with 3,371gal before reaching max pressure., left approx 24,250lbs of prop in the pipe. Placed approx 86,032lbs or 78.2% on formation. Turned well over to flow back. - 1245 PM Shut in flow back, pressure built up from 0 PSI to 70 PSI, started pumping 2.2 BPM and pressured up to 3,925 PSI to 6,224 PSI opened to tanks on 24/64 choke and bleed off to 0 PSI, Pressure up to 3,700 PSI to 6,224 PSI and surged back 20 times, surging back and shutting in, pressured up to 5,715 psi at .25 BPM and bled back to 3,370 psi and

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shut in to monitor pressure
Daily Cost: \$0
Cumulative Cost: \$270,062

11/8/2012 Day: 7

Completion

Rigless on 11/8/2012 - RU CTU - JSA and safety meeting about high pressure. Pressure test weld on connection to 250 psi for five minute, OK. BO pressure. Increase pressure to 5000 psi, no leak off. BO pressure. Pull test weld on connection to 25,000, OK. - JSA and safety meeting. Install well control stack with Weatherford 4" 10K rental gate valve per PC 3 Service. NU well control stack. - 1630 PM IPS CTU arrived hold PJSM with all crew members on location, Weld on coil connector off location, 1800 PM MIRU IPS CTU, pump and related equipment. - 1330 PM Shut in well and start to rig down van and pumps to make room for CTU, ETA on CTU 1630 PM - 24:00-01:00 Recover 30 bbl water with trace sand. 48/64? choke, 20 psi. - Open well on 32/64 choke. - SWI. Pressure build up from 10 psi to 800 psi. Open well on 32/64 choke - 03:50-04:50 Recover 14 bbl water, 2? line, 10 psi. 04:50-05:35 Recover 5 bbl water, 2? line, 10 psi - Pump 140 bbl at 3-6 bpm, pressure up to 9500 psi. SD and allow pressure to bleed off. Repeat several times, pump 140 bbl total. Surge back, pressure up to 9000 psi, surge, pressure up, surge. After third surge, well flowing 1.5 bpm at 20 psi on 48/64 choke. Attempt to pump into formation. Could not pump into formation, pumping just enough volume to pressure up. Open well on 2? line. - 0700 AM FCP 5 PSI recovered 4 BBLS last hour 0800 AM FCP 5 PSI recovered 4 BBLS last hour 0900 AM FCP 3 PSI recovered 6.5 BBLS last hour 1000 AM Well open to tank FCP 3 PSI 1230 PM Pressure testing completed tested good, Bring pumps online at 2.2BPM and pressured up to 8,235 PSI and surge back to 0 PSI 3 times, pressured up to 8,094 PSI and let pressure bleed down to 5,040 PSI 3 times, pressure up to 8,010 PSI and bleed down through choke to 0 PSI. Shut in well and start to rig down van and pumps to make room for CTU, ETA on CTU 1630 PM
Daily Cost: \$0
Cumulative Cost: \$353,382

11/9/2012 Day: 8

Completion

Rigless on 11/9/2012 - Test CT well control stack. Start in hole with wash nozzle. - RIH hole with high velocity wash nozzle(2? OD x .29? L), hydraulic disconnect(2.13? OD x .53? ID x 1.74? L), Dual back pressure valve(2.13? OD x 1? ID x 1.7? L), weld on connector(2? OD x 1? ID x .17? L), and 2? CT. WH pressure 2900 psi. - Test CT stack. Test dbl flapper check to 4000 psi for 10 minutes, OK. - Test 2" seervice lines and bleed off line. Mitigated leaks as necessary. Wing valves on flow cross leaking, waiting on additional replacement valves.-----
 ---- - Waiting on 2X2 valves - 0630 AM J&A Arrived with 10 new 2X2 valves, start replacing valves and prepare to start pressure testing 1000 AM Currently pressure testing with 4 pressure test completed 1200 PM While testing flow cross inner valves, valves would not test, Currently waiting on rebuild kits for MSI 2X2 Flanged valves 1400 PM ISP arrived with rebuild kits for MSI 2X2 valves, currently rebuilding valves to continue pressure testing. 1700 PM Continue pressure testing, CT stack with 3 tests remaining
Daily Cost: \$0
Cumulative Cost: \$1,301,387

11/10/2012 Day: 9

Completion

Rigless on 11/10/2012 - Work CT free. POH. Establih inj rate. - RU to establish injection rate. JSA and safety meeting. Test lines to 9975 psi, OK. WH pressure 3900 psi. Pump 1 bpm at 4400 psi. Pump 2 bpm at 4900 psi. Pump 3 bpm at 5400 psi. Pump 3.7 bpm, pressured up to 9300 psi. ISIP 9000 psi. 5 min SIP 5900 psi. 30 min SIP 4250 psi. - POH with CT. Inspect

tools, saw slight abasion on wash nozzle where it rubbed on csg, otherwise in good condition.
 - RIH with CT at 60 fpm and ? bpm. Stop at 7500? (429? above liner top). Weight check 14,000. Increase pump rate to 2.5 bpm. Proceed through liner top at 45 fpm and 2.5 bpm in/ 3 bpm out. At KOP (8025?) reduce speed to 45 fpm, pump rate 2.5 bpm. At 8850? Reduced speed to 25-30 fpm. Hit sand bridge at 11,265?, pump 10 bbl sweep. 2.5 bbl in/ 3.5 bbl out. Hit sand bridge at 11,275?. At 11,300? reduced pump rate to 1.2 bpm while switching water tanks. Made 200? short trip with 2.5 bpm pump rate. Continue cleaning out to 11430?. At 11430? set weight on sand, saw increase in pump pressure, decrease in WH pressure. PUH to 11,371'. Flow returns decreased to 1.2 bpm with pump rate at 2.5 bpm. Unable to cycle pipe up or down. Presently pump rate 2.5 bpm, 1.25 bpm returns. Surge well while attempting to cycle pipe. Cripple pump, continue to surge 10 times.. Pump 2.5 bpm in, returns .25 bpm. Start pumping 1200 SCF N2 with 1.75 bbl water. - 0730 AM Start N2 at 1,500 SCFM and 1 BPM Fluid. Continue circulating with returns at .3 BPM with returns not increasing continue working coil from 40K to 0 LBS. 0900 AM Shut in back side and let pressure build up to 1,395 PSI and surge to tank pressure fell to 50 PSI, shut in back side and let pressure build up to 2,882 PSI and open to choke on 8/64 choke and continue working TBG from 40K to 0 LBS. open choke to 10/64 with returns .3 to .4 BPM back, continue flowing and working coil from 40K to 0 LBS. 1100 AM shut in back side and let pressure build up to 2,832 PSI shut down pumps and let pressure equalize. 1300 PM Circulating pressure at 5,705 PSI and well head 4,363 PSI. continue to let pressure equalize and occasionally work TBG from 40K to 0 LBS. mostly leaving coil in compression. 1419 PM Open back side on 6/64 choke with 3,953 PSI and increased to 8/64 choke, pressure decreased to 1,797 PSI. Shut back in pump gel sweep and bring on N2 at 1,200 SCFM. 1522 PM Gel sweep out of coil, open choke to 12/64 with 3,228 PSI. pick up on coil to 46K 1730 PM Coil started moving continue pulling up to 8,900? - 1730 PM Sweep with dye is back and returns clean, prepare to get injection rate 1840 PM BJ cement pump rigged up and tested, continue pumping down coil at 2 BPM at 4,000 PSI. Shut in back side with 2,230 PSI. and start pumping down back side at 1.5 BPM and pressured up to 8,800 Psi. pumped 10 BBLS before pressuring out, pressure slowly fell to 6,000 PSI. start pumping down back side at 1 BPM and pressured out at 8,000 PSI. 1915 PM Start pulling out of hole.

Daily Cost: \$0

Cumulative Cost: \$1,326,671

11/11/2012 Day: 10

Completion

Rigless on 11/11/2012 - perforate - POH to KOP at 8025. - TTS begin mixing .6 ppg 100 mesh sand and abrasive perforated interval 11348?-50?, 11,338?-40?. All intervals 6 spf, 60 degree phasing. Total 12 holes. Make short trip from 11,350' ? 10,900'. PU weight 23K. Run back in hole to 11,355' and wash through perforations 11,348-? ? 11,350?. PU off bottom, PU wt. 23K. Clean pick up. - RU BJ Hughes and Re-RU TTS for abrasive perf. Pressure test lines-250 L/10K High. Hold PJSA discuss procedures w/ TTS, BJ, IPS and NFX - Flush hole clean for another attempt @ perf w/ +- 175 BBL of fresh water - At 1507 hrs lost prime on pump truck and SD. TTS blending unit not keeping up w/ rate. Pump back online @ 1509. Continue pumping sand?lost prime/pump again @ 1511 hours. Go to flush. - Establish injection rate by pumping 1 BPM at 6790 psi. Pump 1.25 BPM at 8070 psi. Pump 1.5 BPM at 8050 psi then broke back to 7850 psi. Pump 1.75 BPM at 7820 psi. Pump 2 BPM at 8800 psi the broke back to 8460. Pumped 45 bbl ttl fluid. ISIP 7900 psi. 5 min SIP 5415 psi. 30 min ISIP 4100 psi. - Continue circulating hole. Made short trip to 10800? due to pressure increase-possible restriction due to sleeves. Pressure fell and returned to 10350 w/ Circ Press @ 5500 psig, WH Press @ 2150 psig. Return rate 2.5 BPM Prep to perf well - 10:40 Continuing to wash down Depth 10375?, Circ Press ? 6300 psig, WH Press ? 2425 psig CT FPM ? 18, Running WT - 8600, Pump Rate 2.5 BPM/Return Rate - 2.5 BPM 1050 Stop @ 10600?. Chase EOT back uphole 200?. WH Press ? 2200, Circ Press ? 5500, Wt- 16000, Circulate 10 BBL gel sweep, Pump Rate 2.5 BPM/Return Rate - 2.5 BPM 1125 Stop @ 11000?. WH Press ? 2100, Circ Press ? 5200, WT ? 9100 CT FPM ? 20 FPM. Chase EOT back uphole 200? to 10800', Pump

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Rate 2.5 BPM/Return Rate - 2.5 BPM. Looks OK 1205 On Bottom @ 11355'. WH Press ? 2000, Circ Press ? 5150 . Pump Rate ? 2.5 BPM. Return Rate ? 2.5 BPM, PU WT ? 24000. Stop and circulate bottoms up w/ 2-10 BBL gel sweeps. Working CT 10-20' making sure it is free. Looks OK. - 0651 AM Currently at 9,731' CTM pump sweep and pick up to 9,570' PU WT 18K, SO WT 10K pumping 2.5 BPM at 3,980 PSI returning 2.5 BPM at 1,575 PSI. with RIH speed 20 FPM. 0730 AM Currently at 9,960' CTM started washing, pump dye sweep and pick up to 9,700' PU WT 21K, SO WT 12K pumping 2.5 BPM at 4,000 PSI returning 2.5 BPM at 1,550 PSI. 0743 AM Currently at 9,934' CTM tagged and washed to 9,943' CTM, pump dye sweep and pick up to 9,880' PU WT 21K, SO WT 11K pumping 2.5 BPM at 4,300 PSI returning 2.5 BPM at 1,525 PSI. 0757 AM Currently at 10,080' CTM tagged and washed to 10,103' CTM, pump dye sweep and pick up to 9,900' PU WT 22K, SO WT 10K pumping 2.5 BPM at 4,415 PSI returning 2.5 BPM at 1,560 PSI. 0818 AM Currently at 10,046' CTM tagged and washing to 10,175' CTM, pump dye sweep and pick up to 9,900' PU WT 24K, SO WT 11K pumping 2.5 BPM at 4,300 PSI returning 2.5 BPM at 1,180 PSI. 0852 AM Currently at 10,201' CTM run in hole smooth with no issues, pump packing started leaking and had to lower pump rate to 1 BPM and swap tanks due to running low on water got tanks swapped and got rate back up to 2.5 BPM, continue to pick up to 8,100' PU WT 24K, pumping 2.5 BPM at 4,000 PSI returning 2.5 BPM at 580 PSI. 0945 AM Got packing replaced, RIH to continue washing - RU CT on well. RIH with Ctto 7500' while circulating ? BPM in/1/2 BPM out. At 7500' PU weight 10,000, increase pump rate to 2.5 bbl in, 3 bbl out. Continue IH at 45 fpm. At 8450' reduce speed to 20 fpm. Circ pressure 5300 psi, WH pressure 3935 psi on 18/64 choke. No sand in returns. - Pressure test stripper to 9500 psi for 10 minutes, OK. PU TTS 2' OD x .38 ID x .42' L Ball Seat Wash Nozzle, 2.13 OD x .53' ID x 2.00' L Spiral Abrasive Perforator with 6 ports at 60 deg., 2.13' OD x .53' ID x 1.74' L Hydraulic Disconnect, 2.13' OD x 1' ID x 1.70' L Dual Back Pressure Valve, and 2' OD x 1' ID .17' Weld On Connector. - Dropped ball and start rate for perf-ball on seat @ 1420. Switch over to feed from TTS and est rate @ 2.5 BPM. Circ Press. 8400 psig and falling, WH Press-2100 PSIG and falling. 1455 hrs-Increased rate to 2.75 BPM and start sand.

Daily Cost: \$0

Cumulative Cost: \$1,456,021

11/12/2012 Day: 11

Completion

Rigless on 11/12/2012 - RU frac equipment. Frac. - POH with CT. Blow down coil with N2. Remove BHA. RD and move CT pump, hard lines, and N2 trucks. Remove CT well control stack. RD CTU, left in place for next two stages. MIRU Baker Frac. - Establish injection rate at 7 BPM and 5360 psi. 5 minute SIP 4530 psi. Ttl 117 bbl water pumped. - Hydraulic Fracture Wasatch stage 10 as follows: Pump 358 bbl slick water spacer. Acidize with 32 bbl 15% HCl. Avg rate: 35 bpm, Avg press: 7130 psi, Max rate: 38 bpm, Max press: 9735 psi. FG 0.434. Total 0.5-1 ppg 100 mesh: 2877 lbs, Total .5-5 ppg 20/40 sand: 108,223 lbs. Avg HHP: 6099. Total load to recover 1397 bbls. 81.8% of the designed proppant was placed in formation. 1. 260 psi on N2 regulator, 1775 psi on bottle, Pop off set at 9700 psi. 2. Overloaded the Scale Hopper, had to dump in by hand into the tub during job. 3. Had pressure increase during the 5ppg sand stage to the end of the job. Only able to flush 3,234 gal before reaching max pressure. 4. Placed approx 89,950lbs of Prop on formation or 81.8% of designed volume. 5. Overall good effort by crew. GW-3LDF-4.8% (8.3), XLW-10A-5% (5), FRW-20-58% (6.9), CRB-LT-4.7% (4.4), NE-900-5% (4.9) Enzyme G HT III-18.3% (7.4), ClayCare-2.9% (1.7), - Change pump that charges ball injector - Repair Baker Hughes frac equipment. Prime pumps and test lines to 9,801 psi, OK. WH pressure 3780 psi. Hydraulic Fracture Wasatch stage 9 as follows: Pump 286 bbl slick water spacer. Acidize with 32 bbl 15% HCl. Avg rate: 35 bpm, Avg press: 6865 psi, Max rate: 36 bpm, Max press: 8015 psi. FG 0.434. Total 0.5-1 ppg 100 mesh: 2927 lbs, Total .5-4 ppg 20/40 sand: 118714 lbs. Avg HHP: 6042. Total load to recover 1214 bbls. 100% of the designed proppant was placed in formation. 1. 260 psi on N2 regulator, 1795 psi on bottle, Pop off set at 9700 psi. 2. Had problems getting Ball pump to start, dropped ball at top of WH. 3. No other problems, overall good job by crew. GW-3LDF-

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4.3% (8.5), XLW-10A-10.1% (10.6), FRW-20-36% (2.8), CRB-LT-8% (7.9), NE-900-2.9% (2.9) Enzyme G HT III-14.8% (6.3), ClayCare-3.2% (1.9), - Repair frac pumps. - Hydraulic Fracture Wasatch stage 8 as follows: Pump 20 bbl slick water spacer. Acidize with 32 bbl 15% HCl. Avg rate: 34 bpm, Avg press: 7110 psi, Max rate: 39 bpm, Max press: 8575 psi. FG 0.434. Total 0.5-1 ppg 100 mesh: 5339 lbs, Total .5-4 ppg 20/40 sand: 112,263 lbs. Avg HHP: 5960. Total load to recover 1783 bbls. 100% of the designed proppant was placed in formation. 1. 247 psi on N2 regulator, 1400 psi on bottle, Pop off set at 9660 psi. 2. Lost a pump at the start of 3.0ppg sand, packing, made rate up with rest of pumps. 3. Had trouble lining out rate from pumps jacking from 3.0ppg sand to the end of job, rock thru pumps. 4. Shut down to go thru pumps after sleeve shifted. 5. No other issues, overall good job by crew. Ball Seat Stage Pressures and Rate: 8410 psi @ 12.2 bpm , 6700 psi Pressure before Seating , 6360 psi Pressure after Seating GW-3LDF-6.8% (18.1), XLW-10A-13.5% (21.3), Scalesorb 3-16% (71.4), CRB-LT-4.4% (5.9), NE-900-17.3% (27) Enzyme G HT III-13.2% (9.9), ClayCare-13.3% (10.9), Alpha 1427-7.4% (1.5) - Location Safety Mtg. RU Baker Hughes frac equipment. Prime pumps and test lines to 9,978 psi, OK. Hydraulic Fracture Wasatch stage 7 as follows: Pump 615 bbl slick water spacer. Acidize with 32 bbl 15% HCl. Avg rate: 32 bpm, Avg press: 7370 psi, Max rate: 36 bpm, Max press: 8307 psi. FG 0.434. Total 0.5-1 ppg 100 mesh: 5448 lbs, Total .5-4 ppg 20/40 sand: 84520 lbs. Avg HHP: 5762. Total load to recover 2314 bbls. 100% of the designed proppant was placed in formation. 260 psi on N2 regulator, 1885 psi on bottle. Pop off set at 9700 psi. Stage 6 was skipped due to stage 5 screen out. Abrasive sut perf for stage 7. 11338?-40?. 11348?-50?. 12 holes Started into job and came offline to fix leak on a pump. Saw ball seat on schedule, pressure came up to 9300 psi. Tried again with same result. Surged back. Got on 3rd time, didn?t see a clean shift. Worked up rate slow and went to stage 8. Good job execution. Ball Seat Stage Pressures and Rate: 9237 psi at 10.6 bpm, 5204 psi before seating, 6542 psi after seating. GW-3LDF ? 13.9% (33.5), XLW-10A ? 9.2% (13), FRW-20 ? 15.7% (3.2), CRB-LT ? 2.6% (3.3), Enzyme G HT III ? 7.1% (5), ClayCare ? 16.&% (16.7), Alpha 1427 ? 6.6% (1.6)

Daily Cost: \$0

Cumulative Cost: \$1,713,716

11/13/2012 Day: 12

Completion

Rigless on 11/13/2012 - Frac - RU repaired Baker pump unit and dropped ball for Stg 16. Pressure test lines. Hydraulic Fracture Uteland Butte stage 16 as follows: Pump 237 bbl slick water spacer. Avg rate: 36 bpm, Avg press: 6581 psi, Max rate: 37 bpm, Max press: 7448 psi. Total 0.5-1 ppg 100 mesh: 3000lbs, Total .5-4 ppg 20/40sand:104013 lbs. ISDP-6350, 5-min 5320, 10-min 4430, 15-min 4073. Avg HHP: 5726. Total load to recover 2018 bbls. 100% of the designed proppant was placed in formation. 252 psi on N2 regulator, 1,723 psi on bottle, Pop off set at 9700 psi. Went back to 5 ppa max design after s15 problems. Had couple pumps rocking during the job, able to pass through and lined out. Lost a pump on 4 ppa, able to make up rate with remaining pumps. Good job execution by the crew. Will send s17 ball and open sleeve, come off line to work on pumps. Flush volume includes s17 ball displacement. Did not see good ball action for s17, had a slight pressure drop, brought up rate for another 62 bbls before shutting down. Ball Seat Stage Pressures and Rate: 5167 psi @ 12.7 bpm , 5378 psi Pressure before Seating , 5289 psi Pressure after Seating. Scalesorb 3-3.9% (17.3), CRB-LT-7.4% (9.7), NE-900-5% (7.4) Enzyme G HT III-5.8% (3.6), ClayCare 19.7% (16.7), Alpha 1427-8.6%(1.8),Went back to 5 ppa max design after s15 problems. Had a couple of pumps rocking during the job, able to pass through and lined out. Lost a pump on 4 ppa, able to make up rate with remaining pumps. Good job execution by the crew. Will send s17 ball and open sleeve, come off line to work on pumps. Flush volume includes s17 ball displacement. Did not see good ball action for s17, had a slight pressure drop, brought up rate for another 62 bbls before shutting down. Ball Seat Stage Pressures and Rate: 5167 psi @ 12.7 bpm , 5378 psi Pressure before Seating , 5289 psi Pressure after Seating XLW-10A-2.2% (3.4), Scalesorb 3-3.9% (17.3) CRB-LT-7.4% (9.7),Drop Ball for Stg 17. Pressure Test lines as per procedure. Open WH@3930 psi - Hold PJSM, Pressure test lines.

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Hydraulic Fracture Wasatch stage 15 as follows: Pump 249 bbl slick water spacer. Avg rate: 34 bpm, Avg press: 6680 psi, Max rate: 36 bpm, Max press: 7617 psi. FG 1.032. Total 0.5-1 ppg 100 mesh: 3000 lbs, Total .5-4 ppg 20/40 sand: 69,707 lbs. ISDP-5,032, 5-min 4,560, 10-min 4,070, 15-min 3,979. Avg HHP: 5534. Total load to recover 1333 bbls. 252 psi on N2 regulator, 1,737 psi on bottle, Pop off set at 9700 psi. Went back to 6 ppa max for this stage. Started to see an increase middle of 3 ppa on formation with 4 ppa in the pipe. Held 4 ppa to see reaction to formation. Cut prop when we gained approx. 1,000 psi of pressure. Able to flush the well. Placed approx. 66% of the job in formation. - Baker Frac down for repairs: Pump Trucks needing M & R: 2F978, 4F663, 1F89 - RDMO IPS-WO additional water from Rockwater. Hold PJSM. Pressure test all lines per procedure. Prep to treat Stg 14 - Flow well back on 28/64" choke. 2700 psi. Recover 430 bbl. - Hydraulic Fracture Wasatch stage 12 as follows: Pump 359 bbl slick water spacer. Acidize with 32 bbl 15% HCl. Avg rate: 36 bpm, Avg press: 6700 psi, Max rate: 37 bpm, Max press: 7770 psi. FG 0.434. Total 0.5-1 ppg 100 mesh: 5361 lbs, Total .5-5 ppg 20/40 sand: 109693 lbs. Avg HHP: 6720. Total load to recover 21965 bbls. 100% of the designed proppant was placed in formation. 1. 250 psi on N2 regulator, 1735 psi on bottle, Pop off set at 9700 psi. 2. Had pressure increase during the 3.0ppg to end of job. 3. Saw only small shift in pressure when ball hit, saw significant pressure decrease shortly after. 4. Overall good job by crew. Ball Seat Stage Pressures and Rate: 6380 psi @ 15.5 bpm , 6355 psi Pressure before Seating , 5820 psi Pressure after Seating GW-3LDF-15.8% (43.1) , FRW-20-20.3% (1.9) , Scalesorb 3-2.2% (9.6) , CRB-LT-5.7% (8.1) , NE-900-4% (5.8) Enzyme G HT III-8.6% (5.3) , ClayCare-6.7% (5.5) , - Conduct PJSM, Hydraulic Fracture Wasatch stage 13 as follows: Pump 586 bbl slick water spacer. Avg rate: 35 bpm, Avg press: 6315 psi, Max rate: 39 bpm, Max press: 7550 psi. FG 0.434. Total 0.5-1 ppg 100 mesh: 5381 lbs, Total .5-5 ppg 20/40 sand: 139,743 lbs. Avg HHP: 5448. Total load to recover 2420 bbls. 125% of the designed proppant was placed in formation. 1. 250 psi on N2 regulator, 1735 psi on bottle, Pop off set at 9700 psi. 2. Had to extends Pad and reduce rate to allow time to mix enzyme breaker 3. Had trouble getting water to CMG, sucked air on tank in the 1.0 PPG stage. Caused chemicals to fluctuate. 4. Had confusion on sand, went long on sand approx. 7,000gallons 5.Had increase in backside pressure at end of job, SD to check out backside - Hydraulic Fracture Wasatch stage 11 as follows: Pump 442 bbl slick water spacer. Acidize with 32 bbl 15% HCl. Avg rate: 33 bpm, Avg press: 7965 psi, Max rate: 36 bpm, Max press: 9195 psi. FG 0.434. Total 0.5-1 ppg 100 mesh: 1988 lbs, Total .5-5 ppg 20/40 sand: 106996 lbs. Avg HHP: 6364. Total load to recover 2050 bbls. 100% of the designed proppant was placed in formation. 1. 260 psi on N2 regulator, 1755 psi on bottle, Pop off set at 9700 psi. 2. Due to problems placing Stage 9, pumped Stage 4 design for interval. 3. At the start of the 0.5ppg 30/50 sand stage has sudden loss in pressure, 3150psi, similar to pressure loss at end of Stage 4. Backside pressure looked good and pop off looked good. Continued on with job. 4. Had pressure start to increase from 3.0ppg on formation to end of job. Had to reduce rate during flush to stay under max pressure. 5. Good job by crew making rate adjustments. Ball Seat Stage Pressures and Rate: 7340 psi @ 15.1 bpm , 7300 psi Pressure before Seating , 5985 psi Pressure after Seating GW-3LDF-9.4% (25.9) , XLW-10A-12.5% (20.3) , FRW-20-33.1% (2.2) , Scalesorb 3-3.4% (15) , CRB-LT-5% (7.3) , NE-900-6% (9) Enzyme G HT III-12.5% (7.7) , ClayCare-9.4% (8.1) , Alpha 1427-6.9% (1.5) - Repair pump. - Hydraulic Fracture Uteland Butte stage 17 as follows: Pump 127 bbl slick water spacer. Avg rate: 36 bpm, Avg press: 6705 psi, Max rate: 38 bpm, Max press: 8810 psi. FG 1.032. Total 0.5-1 ppg 100 mesh: 3000 lbs, Total .5-4 ppg 20/40 sand: 92585 lbs. ISDP-6320, 5-min 5330, 10-min 4,670, 15-min 4295. Avg HHP: 5850. Total load to recover 1881 bbls. 100% of the designed proppant was placed in formation. 1. 252 psi on N2 regulator, 1720 psi on bottle, Pop off set at 9700 psi. 2. Sanded off T-belt, during the 4ppg sand stage. We're not able to go to 5ppg before hopper dropped so went to flush. Placed approx 95,585lbs or 86.9% of design volume. 3. No other problems, otherwise good job be crew. Ball Seat Stage Pressures and Rate: 7115 psi @ 17.1 bpm , 6055 psi Pressure before Seating , 6375 psi Pressure after Seating XLW-10A-9.4% (14.6) , CRB-LT-6.8% (8) , NE-900-6.5% (9.2) Enzyme G HT III-8.2% (4.9) , ClayCare-6.3% (5) , Alpha 1427-29.1% (5.7) - Drop 3.531" ball. Hydraulic Fracture Uteland Butte stage 18 as follows: Pump 209 bbl slick water spacer. Avg rate: 34 bpm, Avg press: 7635 psi, Max rate: 38 bpm,

Max press: 9290 psi. FG 1434. Total 0.5-1 ppg 100 mesh: 5500 lbs, Total .5-5 ppg 20/40 sand: 63484 lbs. Avg HHP: 6400. Total load to recover 1832 bbls. 60.3% of the designed proppant was placed in formation. 1. 252 psi on N2 regulator, 1620 psi on bottle, Pop off set at 9700 psi. 2. Had pressure increase with 1.0ppg sand on formation, but pressure rolled over. 3. Had pressure increase with 2ppg & 3ppg on formation, cut sand and went to flush. Flushed well with 4850gal. 4. During flush had 3,000psi drop in pressure. 5. Placed approx 68,984lbs of prop or 60.3% of design volume. 6. Overall good effort by crew. Jim Baker 505-486-0755 - Hydraulic Fracture Wasatch stage 14 as follows: Pump 358 bbl slick water spacer. Avg rate: 35 bpm, Avg press: 6315 psi, Max rate: 37 bpm, Max press: 7267 psi. FG 1.1., FG 1.1. Total 0.5-1 ppg 100 mesh: 5416 lbs, Total .5-5 ppg 20/40 sand: 108,557 lbs. Avg HHP: 5650. Total load to recover 2148 bbls. 100% of the designed proppant was placed in formation. DP - 5600 psig, 5 min SIP 4715, 10 min SIP 4146, 15 min SIP - 4000 1. 252 psi on N2 regulator, 1,770 psi on bottle, Pop off set at 9700 psi. 2. Lost a pump on 3 ppa sand, made up rate with remaining pumps. 3. Lost a second pump on 3 ppa sand, made up rate, brought the ball launch pump on line. 4. Lost a third pump on 4 ppa sand, made up rate with remaining pumps. 5. Flush well to drop s15 ball through the WH. Seated ball for Stg15 6. And opened sleeves. Come off line to fix pumps before pumping s15.

Daily Cost: \$0

Cumulative Cost: \$1,924,680

11/14/2012 Day: 13**Completion**

Rigless on 11/14/2012 - Frac. MO frac equipment. Set plug in frac string. NU BOP. - Function and pressure 10K frac valve and blind rams to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, no leak off. Close 10K manual frac valve, BO pressure to 250 psi under blind rams to negative test frac valve for 10 minutes at 5000 psi, tested OK. BO pressure. Open blind rams. PU 4 ?? ported test sub, 2-8? x 4 ?? pups, and 4 ?? TIW valve. Screw pups and TIW into tbg hanger to test TIW while testing pipe rams. Function and pressure test lower 4 ?? pipe rams to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, no leak off. BO pressure and open lower pipe rams. - Install back pressure valves, ND 4 1/16? 10K frac stack and NU 7 1/16? 10K Manual frac valve, 7 1/16? 10K X 7 1/16? 5K adapter spool, 7 1/16? 5K double BOP (4.5? rams, Blind rams), with 5K 2 1/16? double wing valve outlet, 7 1/16? 5K flowcross with 2 1/16? double valves double outlets, 7 1/16? 5K single BOP with 4.5? rams, 7 1/16? 5K annular bag.. 0 Psi on well. - PUMU #2 - 4.5? 10K Kill Plug and set in second jt of casing below 4.5? liner top at 8,020?, POH with setting tool, all tools recovered, Bleed off well pressure and backside to 0 Psi, Monitor both for ? hrs, neg pressure on both plugs, RDMO Perforators Wireline unit. - Set down gauge and PU 4 1/2" Kill Plug and setting tool w/ WL assembly and RIH to 8065' (WLM) and set KP#1. Bled well down and performed negative test for 30 minutes on well while POOH w/ WL. Test OK. POOH to surface and all tools intact - RIH w/ CCI and 3.75" Gauge Ring to 8065' (WLM). No obstruction-POOH to surface-all tools intact. - MIRU Perforators Wireline, WF Testing. RU adapter flange and lubricator. Test all to 5K for 5 minutes. - Drop 3.650" ball. Hydraulic Fracture Wasatch stage 19 as follows: Pump 215 bbl slick water spacer. Avg rate: 34 bpm, Avg press: 6795 psi, Max rate: 35 bpm, Max press: 8780 psi. Total 0.5-1 ppg 100 mesh: 5500 lbs, Total .5-4 ppg 20/40 sand: 105,831 lbs. ISDP-5,245, 5-min 4,815, 10-min 4,335, 15-min 4135. Avg HHP: 5729. Total load to recover 1947 bbls. 100% of the designed proppant was placed in formation. 1. 252 psi on N2 regulator, 1600 psi on bottle, Pop off set at 9700 psi. 2. Good job with no problems, good effort by crew. GW-3LDF-7.1% (20.3), XLW-10A-3.5% (5.8), Scalesorb 3-10.6% (47.7), NE-900-4.1% (6.1) ClayCare-12.5% (10.2), Alpha 1427-7.6% (1.6) - Flow back well on 28/64" choke at 2800 psi. Recover 360 bbl. - RD MO frac equipment.

Daily Cost: \$0

Cumulative Cost: \$2,018,581

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11/15/2012 Day: 14**Completion**

Rigless on 11/15/2012 - LD frac string - Install and test flow back lines to 5000 psi for 10 minutes, OK. - 07:00 - 09:00 Finish testing 7 1/16" 5K drillout BOP stack and flowback lines. - 09:00 - 13:00 MIRU Mountain State's WOR to pull 4.5" frac string. MIRU Weatherford's rig pump, pipe racks, laydown machine, and ancillary equipment, Tie back on 6 lines, install line wt ind. - Close 10 K frac valve. Change pipe rams from 4 1/2" to 2 3/8". Test lower 2 3/8" rams to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, no leak off. Pressure test upper 2 3/8" pipe rams to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, OK. BO pressure. Move out 4 1/2" frac string. Set 2 3/8" tbg on pipe racks. - PUMU 4.5" pup jts and make up in tbg hanger with TIW valve in place. Unscrew locking pins in head, pick up on tbg and unstung from tie back. 127K string wt, tbg free and POH laying down frac string, 7,946' of 4.5" tbg, 186 jts and 5 pup jts of 4.5" 13.5# tbg in hole, 127,271 lbs, POH frac string as follows: 1 jt 4" 13.5# P110 BT&C, 1-10", 1-8", 1-6", 2-4" x 4" 13.5# P110 BT&C pups jts, 185 jts 4", 13.5#, P110, BT&C pipe, Halliburton Versaflex seal bore assembly (5.20" OD x 3.92" ID x 14.20' L). RD csg crew. - Close upper 4" pipe rams. Pressure to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, no leak off. Test inside wing valves on flow cross while testing upper pipe rams. Bleed off pressure. Test outside wing valves on flow cross to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, OK. BO pressure. Pressure test lower inside wing valve to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, No leak off. Test outside lower wing valve to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, OK. BO pressure. Open upper pipe rams. Function and pressure test annular preventer to 250 psi for five minutes, no leak off. BO pressure. Increase pressure to 3500 psi for 10 minutes, good test. TIW valve tested OK. LD pups and TIW valve.

Daily Cost: \$0**Cumulative Cost:** \$2,605,925**11/16/2012 Day: 15****Completion**

Rigless on 11/16/2012 - Drill out frac sleeves - Tie back on double line fast. Tally 2 3/8" WS.PU 3.729" OD x 1.20 ID x 1.59' L 4-blade mill, 2.975" OD x 1.31" ID x 1.5' L bit sub, 2.942" OD x 1" ID x 1.90' L double flapper check valve, 1 jt 2 3/8", 5.95#, P110, PH6 tbg, 2.9" OD x 1.75" ID x .75' L RN nipple, and 30 jts 2 3/8", 5.95#, P110, PH6 tbg. Break circulation every 1000' as running tbg. - RIH to tag #16 sleeve ball seat, jt 298 Tbg WT 30,000#, 32,000# ?, 30,000# ? Sleeve # 16 tag @ 9,336' establish pump rate, 2.0 bbls/min 4,400 psi @ wh, 3,000 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 13:05 hrs drill through @ 13:10 hrs, time to drill plug 5 min, 2.2 bbls in, x 2.0 bbls out, pump 10 bbl sweep circ.. RIH to tag #15 sleeve ball seat, jt 305 Tbg WT 30,000#, 32,000# ?, 30,000# ?, Sleeve #15 tag @ 9,552' establish pump rate, 2.0 bbls/min 4,400 psi @ wh, 3,000 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 13:30 hrs drill through @ 13:35 hrs, time to drill plug 5 min, 2.2 bbls in, x 2.0 bbls out, pump 10 bbl sweep circ. RIH to tag #14 sleeve ball seat, jt 311 Tbg WT 30,000#, 32,000# ?, 30,000# ?, Sleeve # 14 tag @ 9,727' establish pump rate, 2.5 bbls/min 4,400 psi @ wh, 3,100 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 13:35 hrs drill through @ 13:38 hrs, time to drill plug 9 min, 2.5 bbls in, x 3.3 bbls out, pump 10 bbl sweep circ. RIH to tag #13 sleeve ball seat, jt 318 Tbg WT 30,000#, 37,000# ?, 29,000# ?, Sleeve # 13 tag @ 9,946' establish pump rate, 2.6 bbls/min 4,600 psi @ wh, 3,100 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 14:00 hrs drill through @ 14:15 hrs, time to drill plug 15 min, 2.5 bbls in, x 3.4 bbls out, pump 10 bbl sweep circ. - RIH to tag #12 sleeve ball seat, jt 325 Tbg WT 31,000#, 33,000# ?, 28,000# ?, Sleeve # 12 tag @ 10,167' establish pump rate, 2.0 bbls/min 4,400 psi @ wh, 3,100 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 14:39 hrs drill through @ 14:46 hrs, time to drill plug 7 min, 2.6 bbls in, x 3.2 bbls out, pump 120 bbl and sweeps from bottom up. RIH to tag #11 sleeve ball seat, jt 332 Tbg

RECEIVED: Apr. 02, 2014

WT 32,000#, 36,000# ?, 29,000# ?, Sleeve # 11 tag @ 10,386? establish pump rate, 2.7 bbls/min 4,400 psi @ wh, 3,200 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 15:30 hrs drill through @ 15:40 hrs, time to drill plug 10 min, 2.7 bbls in, x 3.2 bbls out, pump 10 bbl sweep circ. RIH to tag #10 sleeve ball seat, jt 337 Tbg WT 32,000#, 36,000# ?, 24,000# ?, Sleeve # 10 tag @ 10,562? establish pump rate, 2.7 bbls/min 4,600 psi @ wh, 3,200 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 16:05 hrs drill through @ 16:30 hrs, time to drill plug 25 min, 2.7 bbls in, x 3.1 bbls out, pump 10 bbl sweep circ. Rig crew change: RIH to tag #9 sleeve ball seat, jt 344Tbg WT 32,000#, 36,000# ?, 24,000# ?, Sleeve # 9 tag @ 10,781? establish pump rate, 2.8 bbls/min 4,600 psi @ wh, 3,000 psi @ choke 22/64, Swivel rpm 110-120 wob 6-10k start drilling @ 17:15 hrs drill through @ 17:30 hrs, time to drill plug 15 min, 2.8 bbls in, x 3.5 bbls out, pump 10 bbl sweep circ. Circulate bottoms with 290 bbls while pumping sweeps. - Circulate 290 bbl. PU 7 jts. 20:18 Tag frac sleeve #8 EOT 10,998 on jt# 351. 2.25 BPM in -3.5 BPM out. Tbg 4400 psi. Well head 2900 psi on 18/64 choke. WOB 7K, 120 RPM. 12 minutes to drill plug, 5 bbl. Pump 1-10 bbl sweep and 40 bbl wtr. Plug cuttings, oil, and light sand in returns. PU 7 jt. RIH with tbg to tag frac sleeve #7. PU 7 jts. 21:00 Tag frac sleeve #7 EOT 11,218 on jt# 358. Pick up weight 32K, Hanging weight 32K, Slack off weight 24K. 2.3 BPM in -3.5 BPM out. Tbg 4500 psi. Well head 2900 psi on 18/64 choke. WOB 7K, 120 RPM. 17 minutes to drill plug. Pump 1-10 bbl sweep. Plug cuttings, oil, and light sand in returns. PU 6 jt. RIH with tbg to tag frac sleeve #6. - PU 6 jts. 22:10 Tag frac sleeve #6 EOT 11,393? on jt# 364. Pick up weight 32K, Hanging weight 32K, Slack off weight 24K. 2.5 BPM in -3.5 BPM out. Tbg 4700 psi. Well head 2900 psi on 18/64 choke. WOB 7K, 120 RPM. 34 minutes to drill plug. Pump 1-10 bbl sweep. Plug cuttings, light oil, and light sand in returns. PU 7 jt. RIH with tbg to tag frac sleeve #5. Tag frac sleeve #5 EOT 11,606? on jt# 371. Pick up weight 34K, Hanging weight 32K, Slack off weight 24K. 2.5 BPM in -3.5 BPM out. Tbg 4700 psi. Well head 2900 psi on 18/64 choke. WOB 7K, 120 RPM. 13 minutes to drill plug. Pump 10 bbl sweep, 20 bbl spacer, 10 bbl sweep. Circulate hole voume. Plug cuttings, light oil, and light sand in returns - Tag kill plug # 2 @ 8,020? establish pump rate, 3 bbls/min 2,000 psi @ wh, 50 psi @ choke 64/64, Swivel rpm 110-120 wob 6-10k start drilling @ 09:33 hrs drill through @ 09:43 hrs, time to drill plug 10 min, 3 bbls in, x 2.5 bbls out, pump sweep circ. RIH to tag Kill plug #1, jt 358 Tbg WT 44,000#, 46,000# ?, 42,000# ? Plug # 1 tag @ 8,065? establish pump rate, 3 bbls/min 4,400 psi @ wh, 2,700 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 10:02 hrs drill through @ 10:20 hrs, time to drill plug 18 min, 3 bbls in, x 3.0 bbls out, WH 2,700 Psi, Pump sweep circ. Drilled thru #1 kill plug with no noticeable pressure increased. Pick up & RIH with 28 jts to tag #18 ball seat sleeve. Well head 3,500 psi, Pressure increased while running in hole to tag sleeve #19. RIH to tag #18 sleeve ball seat, jt 286 Tbg WT 30,000#, 32,000# ?, 30,000# ? Sleeve # 18 tag @ 8,944? establish pump rate, 2.5 bbls/min 4,400 psi @ wh, 3,100 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 11:35 hrs drill through @ 11:45 hrs, time to drill plug 10 min, 2.5 bbls in, x 3.5 bbls out, pump 10 bbl sweep circ. RIH to tag #17 sleeve ball seat, jt 291 Tbg WT 30,000#, 32,000# ?, 30,000# ?, Sleeve # 17 tag @ 9,117? establish pump rate, 2.5 bbls/min 4,400 psi @ wh, 3,000 psi @ choke 18/64, Swivel rpm 110-120 wob 6-10k start drilling @ 12:00 hrs drill through @ 12:06 hrs, time to drill plug 6 min, 2.5 bbls in, x 3.0 bbls out, pump 10 bbl sweep circ.

Daily Cost: \$0

Cumulative Cost: \$2,638,422

11/17/2012 Day: 16

Completion

Rigless on 11/17/2012 - LD 2 3/8" WS. - POOH in to tight spot @ +- 8743? (Jt. #279). PU swivel to circulate/rotate/reciprocate out. Circulated bottoms up 3 BPM @ 4500 psig>Returns 3 BPM @ 2680 psig. At 1410 Hrs after circulating +- 250 BBL, decided to continue POOH in to intermediate casing. - POOH and LD 2 3/8" PH-6 singles. SICP - 2850 psig. - Finish circulating hole w/ 350 BBL of clean water w/ gel sweep off of bottom. SD on circulating pump and RD and hang back swivel and RU to POOH w/ 2 3/8 PH-6 workstring. - Rotated in to restriction

RECEIVED: Apr. 02, 2014

and stopped after 5?. PU and it required 22-25K over String weight to PO of restriction. CP increased to 5000 psi. Made one more attempt to set down and mill restriction w/ same results. Decision to PU tbg w/ tool joint above slips and circulate sweep to EOT. PU single and continue to circulate bottoms up. CP- 2.5 BPM @ 4500 psig, WH ? 2.5/2.75 BPM @ 2900 psig. Trace of sand and formation? In returns. No metal shavings or cuttings to surface. WOO - Pump 10 bbl sweep, 20 bbl, 10 bbl sweep and 1 hole volume. 2.5 bbl in, 3.5 bbl out. 4700 tbg pressure, 2900 psi on WH. 13/64" choke. - Mill from 11807' to 11811'. 2.5 bbl in, 3.5 bbl out. 4700 tbg pressure, 2900 psi on WH. 13/64" choke. 1 pt on mill, 120 rpm. Finish circulating hole volume. PU 6 jts tbg (377 jts in hole). Clean out sand on each jt. At 11807? set down on tight spot (Sleeve #5 at 11,825?). Pulled 10 pts over PU wt to pull free. Bit torqueing out when attempting to rotate through with 1 pt over neutral weight. Decision made to pump 10 bbl sweep, 20 bbl, then 10 bbl sweep, and 1 hole volume. - Continue to POOH w/ 2 3/8? PH-6 Tbg. SICP-2850 psig. Hang back swivel after pulling 10 jts. Continue to POOH w/ 267 jts total of 2 3/8" PH-6 Tbg to 4387". - RU Mountain States Snubbing Unit and test all components. POOH w/ 267 jts. 2 3/8? PH-6 tbg (+- 4387?). RU to snub out w/ remaining 2 3/8? (139 jts). Currently attempting to work 2 3/8? Tbg hanger through BOP's. Succeeded in working hanger through BOP's after 30 minutes. 2 7/8? L-80 Production on location. Weatherford on location to assist in Snubbing unit RU and test. Perforators, Baker Tools and Lufkin on standby. - RD tongs and floor. ND Annular preventer. NU snubbing unit. Test lower pipe rams to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, OK. BO pressure. Function and pressure test upper pipe rams to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 5000 psi for 10 minutes, OK. BO pressure. Function and pressure test annular preventer to 2509 psi for 5 minutes, OK. BO pressure. Increase pressure to 3000 psi for 10 minutes, OK. - Finish circulating hole volume. PU 6 jts tbg (377 jts in hole). Clean out sand on each jt. At 11807? set down on tight spot (Sleeve #5 at 11,825?). Pulled 10 pts over PU wt to pull free. Bit torqueing out when attempting to rotate through with 1 pt over neutral weight.

Daily Cost: \$0

Cumulative Cost: \$2,673,846

11/18/2012 Day: 17

Completion

Rigless on 11/18/2012 - LD WS - PU 5.495? OD x 2/313? ID x 1.55? L L-10 on/off tool with 2.313? BNX profile nipple; 1 jt 2 7/8?, 6.5#, L-80, EUE 8 rd tbg; 3.661? OD x 2.35? ID x 0.82? L BX profile nipple; Gas lift valve mandrel #1; 13 jts 2 7/8?, 6.5#, L-80, EUE 8 rd tbg; Gas lift valve mandrel #2; 15 jts 2 7/8?, 6.5#, L-80, EUE 8 rd tbg, Gas lift valve mandrel #3; 16 jts 2 7/8?, 6.5#, L-80, EUE 8 rd tbg; Gas lift valve mandrel #4; 15 jts 2 7/8?, 6.5#, L-80, EUE 8 rd tbg; Gas lift valve mandrel #5; 16 jts 2 7/8?, 6.5#, L-80, EUE 8 rd tbg, Gas lift valve mandrel #6; 15 jts 2 7/8?, 6.5#, L-80, EUE 8 rd tbg; Gas lift valve mandrel #7; 17 jts 2 7/8?, 6.5#, L-80, EUE 8 rd tbg; and Gas lift valve mandrel #8. - Change pipe rams from 2 3/8" to 2 7/8". NU annular preventer. Function and pressure test lower pipe rams to 250 psi for 5 minutes, OK BO pressure. Increase pressure to 5000 psi for 10 minutes, no leak off. BO pressure and open rams. Function and pressure test upper pipe rams to 250 psi for 5 minutes, OK BO pressure. Increase pressure to 5000 psi for 10 minutes, no leak off. BO pressure and open rams. Function and pressure test Annular preventer to 250 psi for 5 minutes, OK. BO pressure. Increase pressure to 3500 psi for 10 minutes, OK. BO pressure. - RUWL and test lubricator as per procedure w/ 250 psig for 5 minutes and 5000 psig for 10 minutes. Test OK. Open Well and RIH w/ BHA as follows: 2.875? EUE WLEG w/ Pump Out Plug Shear Rate @ 750 psig 3.675? OD x .84? L, 2.875? 8R EUE BXP L-80 Pup Joint 2.441? ID x 2.875? OD x 4.80? L, XN Profile Nipple (NO-GO) 2.305? ID x 2.875? OD EUE BX 3.675? OD x 1.12? L, 2.875? EUE 8R L-80 Pup Joint 2.441? ID x 2.875? OD x 4.80? L, 600-237 WL set Hornet Packer 2.37? ID x 6.0? OD x 8.60? L, On-Off Tool 2.875? 8R EUE L-10 ?X? Nipple 2.313? ID x 2.875? OD x 1.55? L. RIH @ -150 FPM @ 3140? . Set pkr in middle of second jt above liner hanger at 7,860'. POH. All tools recovered. RDMO WL trk. - RD Snubbing Unit. MIRU WL - Resume operations @ daylight. Continue POOH and LD 2 3/8? PH-6 singles. Will start snubbing as well dictates. St.

RECEIVED: Apr. 02, 2014

snubbing operations w/ 89 jts left in hole. - LD 50 jts 2 3/8" WS. Stand by to snub OH at daylight. - POOH to surface w/ remaining 2 3/8" PH-6 Tbg. All tools intact on BHA. RD Snubbing unit.

Daily Cost: \$0

Cumulative Cost: \$2,723,149

11/19/2012 Day: 18

Completion

Rigless on 11/19/2012 - Land Tbg, NU Tree, test and pump ceramic disk - Pump 50 bbl wtr down tbg, clean water in returns. Land tbg with 12pts compression. Pressure test hanger from above with 250 psi for 5 minutes, OK. BO pressure then increase to 5000 psi for 10 minutes, OK. BO pressure. RD tongs and floor. ND BOP stack. - NU Cameron 10K tree. Cameron testing tree to 10,000 psig for 10 min-good test. RU Weatherford to test remaining components to 250 psig/10000 psig. Weatherford tested all components of Production Tree as per procedure; 250 psig 5 minutes and 10000 psig for 10 minutes. Pull TWCV and RD Mtn States WOR. RU Weatherford pump to WH and pump off ceramic disc @ 3900 psig. Currently pumping additional 100 BBLs fluid to ensure disc is broken. - Pumped 100 Water @ 2.6 BPM @ 4500 psig. SD Pressure 3100 psig. RDMO Weatherford Pump Unit and turn well over to production. - PU 26 jts 2 7/8", 6.5#, L-80, EUE 8 rd tbg; Gas lift mandrel #9; 44 jts 2 7/8", 6.5#, L-80, EUE 8 rd tbg; Gas lift mandrel #10; 64 jts 2 7/8", 6.5#, L-80, EUE 8 rd tbg. Tag top of packer, LD 2 jts. PU 1-8" pup and 1 jt 2 7/8", 6.5#, L-80, EUE 8 rd tbg. Total 242 jts tbg and 10 gas lift mandrels.

Daily Cost: \$0

Cumulative Cost: \$2,864,462

12/2/2012 Day: 20

Completion

Rigless on 12/2/2012 - Capture Costs and Make Adjustments in DCR - Capture Costs in DCR, ITL Inv#9180(\$5020), Inv 9283(\$8598), ITL Tk#9893(\$1628), Western Water Solutions Tk#15174,175,167,176(\$1016)

Daily Cost: \$0

Cumulative Cost: \$2,101,635

1/27/2013 Day: 21

Completion

Rigless on 1/27/2013 - Capture Costs in DCR - Capture Costs in DCR

Daily Cost: \$0

Cumulative Cost: \$2,105,870

2/14/2013 Day: 22

Completion

Rigless on 2/14/2013 - Capture Costs in DCR - Capture Costs in DCR, updated costs 3/2/13

Daily Cost: \$0

Cumulative Cost: \$2,182,722

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