001

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 3

AMENDED REPORT ☐
(highlight changes)

# APPLICATION FOR PERMIT TO DRILL

| 5. MINERAL LEASE NO: | 6. SURFACE: |
|---|---|
| UTU 77513 | Federal |

1A. TYPE OF WORK: DRILL ☑ REENTER ☐ DEEPEN ☐

7. IF INDIAN, ALLOTTEE OR TRIBE NAME: ---

B. TYPE OF WELL: OIL ☐ GAS ☑ OTHER _____ SINGLE ZONE ☑ MULTIPLE ZONE ☐

8. UNIT or CA AGREEMENT NAME: Prickly Pear Unit

2. NAME OF OPERATOR: BILL BARRETT CORPORATION

9. WELL NAME and NUMBER: Prickly Pear Unit Federal #12-24

3. ADDRESS OF OPERATOR: 1099 18th St, Ste 2300 CITY Denver STATE CO ZIP 80202

PHONE NUMBER: (303) 312-8120

10. FIELD AND POOL, OR WILDCAT: ~~Prickly Pear Unit/Mesaverde~~ undesignated

4. LOCATION OF WELL (FOOTAGES)

AT SURFACE: 1271' FSL x 483' FWL 559659 X 4480539 Y 39.75456 -110.30360

AT PROPOSED PRODUCING ZONE: Same as above

11. QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E

14. DISTANCE IN MILES AND DIRECTION FROM NEAREST TOWN OR POST OFFICE: 67 miles northeast of Wellington, Utah

12. COUNTY: CARBON

13. STATE: UTAH

| 15. DISTANCE TO NEAREST PROPERTY OR LEASE LINE (FEET) | 16. NUMBER OF ACRES IN LEASE: | 17. NUMBER OF ACRES ASSIGNED TO THIS WELL: |
|---|---|---|
| 483' | 640.0 | 160 |
| **18. DISTANCE TO NEAREST WELL (DRILLING, COMPLETED, OR APPLIED FOR) ON THIS LEASE (FEET)** | **19. PROPOSED DEPTH:** | **20. BOND DESCRIPTION:** |
| n/a | 10,000 | Nationwide Bond #WYB000040 |
| **21. ELEVATIONS (SHOW WHETHER DF, RT, GR, ETC.):** | **22. APPROXIMATE DATE WORK WILL START:** | **23. ESTIMATED DURATION:** |
| 7795' GR | 6/20/2004 | 60 days |

24. **PROPOSED CASING AND CEMENTING PROGRAM**

| SIZE OF HOLE | CASING SIZE, GRADE, AND WEIGHT PER FOOT | SETTING DEPTH | CEMENT TYPE, QUANTITY, YIELD, AND SLURRY WEIGHT |
|---|---|---|---|
| 12-1/4" | 9-5/8" JorK-55 36# STC | 1,000 | To surface +/- 240 sx Lite and +/- 180 sx Class "G" ---------- |
| 7-7/8" | 5-1/2" N-80 17# LTC | 10,000 | TD to 2,500' +/- 1095 sx 50/50 Poz Class "G" --- |
| | | | |
| | | | |
| | | | |
| | | | |
| | | | |

25. **ATTACHMENTS**

VERIFY THE FOLLOWING ARE ATTACHED IN ACCORDANCE WITH THE UTAH OIL AND GAS CONSERVATION GENERAL RULES:

☑ WELL PLAT OR MAP PREPARED BY LICENSED SURVEYOR OR ENGINEER
☑ COMPLETE DRILLING PLAN
☑ EVIDENCE OF DIVISION OF WATER RIGHTS APPROVAL FOR USE OF WATER
☐ FORM 5, IF OPERATOR IS PERSON OR COMPANY OTHER THAN THE LEASE OWNER

NAME (PLEASE PRINT) Debra K. Stanberry TITLE Permit Specialist

SIGNATURE [signature] DATE 4/23/2004

(This space for State use only)

API NUMBER ASSIGNED: 43-007-30953

Approved by the Utah Division of Oil, Gas and Mining
APPROVAL:
Date: 06-14-04
By: [signature]

RECEIVED
APR 27 2004
DIV. OF OIL, GAS & MINING

(11/2001) (See Instructions on Reverse Side)

**Federal Approval of this Action is Necessary**

Form 3160-3
(April 2004)

FORM APPROVED
OMB No. 1004-0137
Expires March 31, 2007

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

# APPLICATION FOR PERMIT TO DRILL OR REENTER

5. Lease Serial No.
**UTU 77513**

6. If Indian, Allotee or Tribe Name
**n/a**

1a. Type of work: ☑ DRILL ☐ REENTER

7. If Unit or CA Agreement, Name and No.
**PRICKLY PEAR UNIT**

1b. Type of Well: ☐ Oil Well ☑ Gas Well ☐ Other ☑ Single Zone ☐ Multiple Zone

8. Lease Name and Well No.
**Prickly Pear Unit Federal #12-24**

2. Name of Operator
**BILL BARRETT CORPORATION**

9. API Well No.
~~pending~~ 43-007-30953

3a. Address **1099 18th Street, Suite 2300 Denver CO 80202**

3b. Phone No. *(include area code)*
**(303) 312-8120**

10. Field and Pool, or Exploratory
**Prickly Pear Unit/Mesaverde**

4. Location of Well *(Report location clearly and in accordance with any State requirements.*)*
At surface **SW/4 SW/4 1271' FSL x 483' FWL**
At proposed prod. zone **same**

11. Sec., T. R. M. or Blk. and Survey or Area
**Section 24-T12S-R14E S.L.B.&M.**

14. Distance in miles and direction from nearest town or post office*
**67 miles northeast of Wellington, Utah**

12. County or Parish
**Carbon**

13. State
**UT**

| 15. Distance from proposed* location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any) | 16. No. of acres in lease | 17. Spacing Unit dedicated to this well |
|---|---|---|
| **483'** | **640 acres** | **160 acres** |
| 18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft. | 19. Proposed Depth | 20. BLM/BIA Bond No. on file |
| **n/a** | **10,000'** | **Nationwide Bond #WYB000040** |
| 21. Elevations (Show whether DF, KDB, RT, GL, etc.) | 22. Approximate date work will start* | 23. Estimated duration |
| **7795' ungraded ground** | **06/20/2004** | **60 days** |

## 24. Attachments

The following, completed in accordance with the requirements of Onshore Oil and Gas Order No.1, shall be attached to this form:

1. Well plat certified by a registered surveyor.
2. A Drilling Plan.
3. A Surface Use Plan (if the location is on National Forest System Lands, the SUPO shall be filed with the appropriate Forest Service Office).
4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above).
5. Operator certification
6. Such other site specific information and/or plans as may be required by the authorized officer.

| 25. Signature | Name *(Printed/Typed)* | Date |
|---|---|---|
| | **Debra K. Stanberry** | **04/23/2004** |
| Title **Permit Specialist** | | |

| Approved by *(Signature)* | Name *(Printed/Typed)* | Date |
|---|---|---|
| Title | Office | |

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.
Conditions of approval, if any, are attached.

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

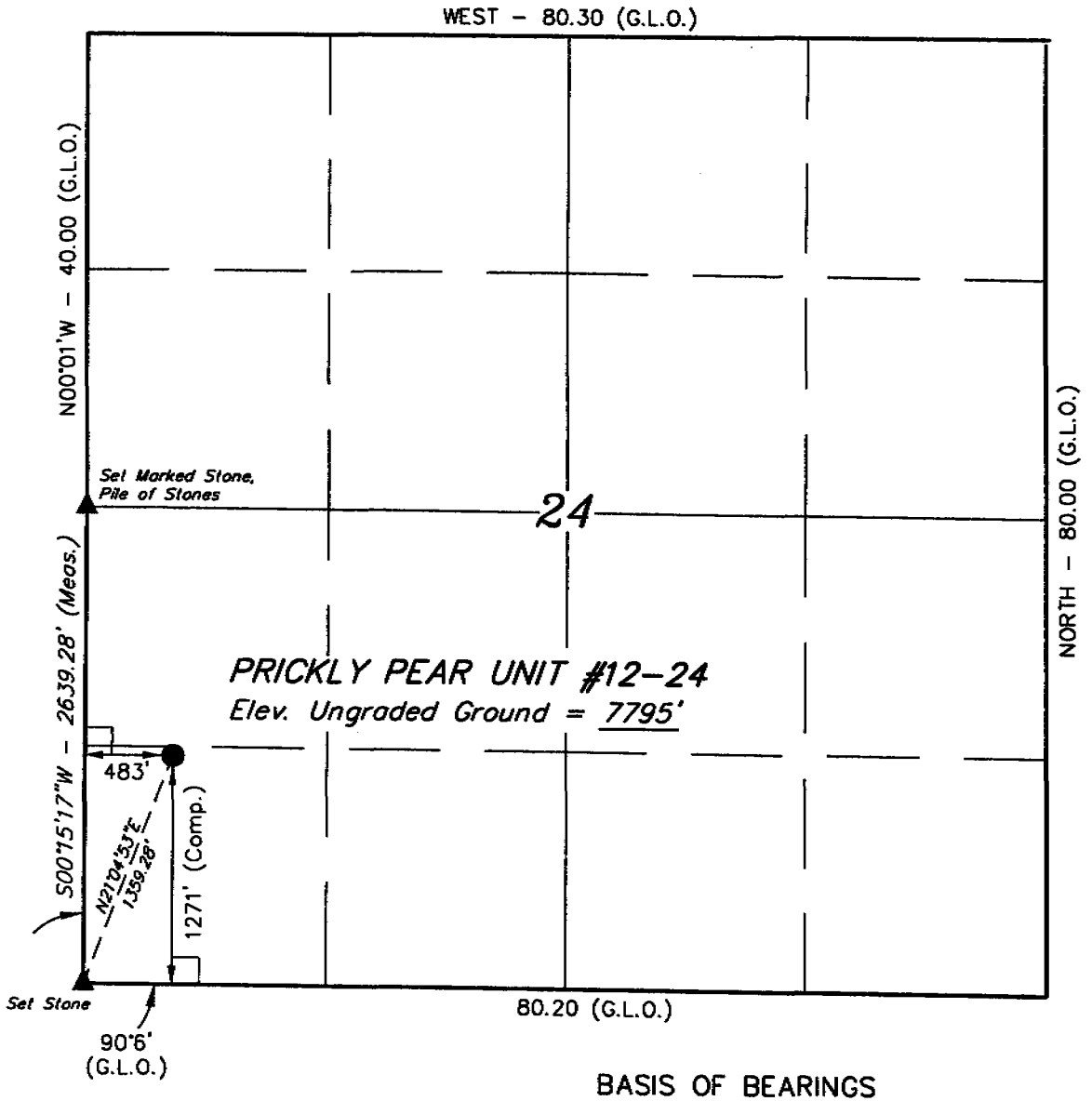
**(Instructions on page 2)*

RECEIVED
APR 2 7 2004
DIV. OF OIL, GAS & MINING

# BILL BARRETT CORPORATION

Well location, PRICKLY PEAR UNIT #12-24, located as shown in the SW 1/4 SW 1/4 of Section 24, T12S, R14E, S.L.B.&M., Carbon County, Utah.

## T12S, R14E, S.L.B.&M.



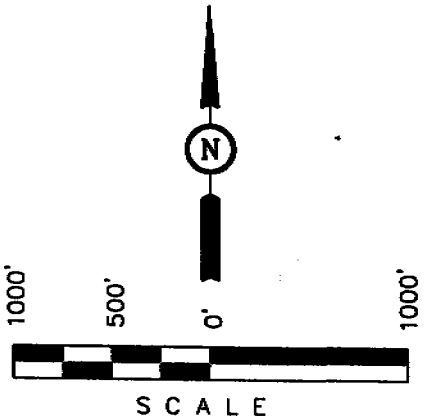

## BASIS OF BEARINGS

BASIS OF BEARINGS IS A G.P.S. OBSERVATION.

(AUTONOMOUS NAD 83)
LATITUDE = 39°45'16.71" (39.754642)
LONGITUDE = 110°18'15.76" (110.304378)

## BASIS OF ELEVATION

SPOT ELEVATION AT THE SOUTHWEST CORNER OF SECTION 7, T12S, R15E, S.L.B.&M. TAKEN FROM THE COWBOY BENCH QUADRANGLE, UTAH, 7.5 MINUTE QUAD. (TOPOGRAPHIC MAP) PUBLISHED BY THE UNITED STATES DEPARTMENT OF THE INTERIOR, GEOLOGICAL SURVEY. SAID ELEVATION IS MARKED AS BEING 7563 FEET.




## CERTIFICATE

THIS IS TO CERTIFY THAT THE ABOVE PLAT WAS PREPARED FROM FIELD NOTES OF ACTUAL SURVEYS MADE BY ME OR UNDER MY SUPERVISION AND THAT THE SAME ARE TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.

No. 161319
ROGER A. KAY
REGISTERED LAND SURVEYOR
REGISTRATION NO. 161319
STATE OF UTAH

REVISED: 8-11-03

## LEGEND:

- = 90° SYMBOL
- ● = PROPOSED WELL HEAD.
- ▲ = SECTION CORNERS LOCATED.


**UINTAH ENGINEERING & LAND SURVEYING**
*85 SOUTH 200 EAST - VERNAL, UTAH 84078*
(435) 789-1017


| | | |
|---|---|---|
| SCALE: 1" = 1000' | DATE SURVEYED: 6-19-03 | DATE DRAWN: 6-24-03 |
| PARTY: B.B. J.W. C.G. | REFERENCES: G.L.O. PLAT | |
| WEATHER: WARM | FILE: BILL BARRETT CORPORATION | |

**Bill Barrett Corporation**

June 8, 2004

Ms. Diana Whitney
Utah Division of Oil, Gas & Mining
1594 W. North Temple, Suite 1210
Salt Lake City, Utah 84114-5801

RE: Prickly Pear Unit Federal #12-24
Section 24, Township 12 South, Range 14 East
Carbon County, Utah

Dear Ms. Whitney:

Bill Barrett Corporation (BBC) has submitted an Application for Permit to Drill the above captioned well. As we discussed in our recent telephone conversation, the requested location requires an exception location. In compliance with R649-3-3 Exception to Location and Siting of Wells, BBC submits the following required information with its request for administrative approval for the exception location:

1. BBC is the only owner within a 460-foot radius of the proposed well.

2. BBC is requesting the exception location because of Topographic conditions.

3. BBC has provided a plat with the APD package reflecting the requested location at 1271' FSL and 483' FWL.

We sincerely appreciate your prompt attention to this matter. Should you require additional information, please contact the undersigned at 303-312-8184 or by email at dgundry-white@billbarrettcorp.com.

Sincerely
Bill Barrett Corporation

Doug Gundry-White
Consulting Landman



1099 18TH STREET
SUITE 2300
DENVER, CO 80202
P 303.293.9100
F 303.291.0420

# SELF-CERTIFICATION STATEMENT

The following self -certification statement is provided per federal requirements dated June 15, 1988.

Please be advised that Bill Barrett Corporation is considered to be the operator of the following well.

Prickly Pear Unit Federal 12-24
SW 1/4, SW 1/4, 1271' FSL, 483' FWL, Section 24, T. 12 S., R. 14 E., S.L.B.&M.
Lease UTU 77513
Carbon, County, Utah

Bill Barrett Corporation is responsible under the terms of the lease for the operations conducted upon the lease lands.

Debra K. Stanberry
Permit Specialist
Bill Barrett Corporation
1099 18th Street, Suite 2300
Denver, Colorado 80201
303-312-8120

# HAZARDOUS MATERIAL DECLARATION

FOR WELL NO. PRICKLY PEAR UNIT FEDERAL 12-24 LEASE NO. UTU 77513

Bill Barrett Corporation guarantees that during the drilling and completion of the above referenced well, we will not use, produce, or store, transport or dispose 10,000# annually of any of the hazardous chemicals contained in the Environmental Protection Agency's consolidated list of chemicals subject to reporting under Title III Super Amendments and Reauthorization Act (SARA) of 1986.

Bill Barrett Corporation guarantees that during the drilling and completion of the above referenced well, we will use, produce, store, transport, or dispose less than the threshold planning quantity (TPQ) of any extremely hazardous substances as defined in 40 CFR 355.

# TEN POINT PLAN

BILL BARRETT CORPORATION
Prickly Pear Unit Federal 12-24
Surface location SW 1/4, SW 1/4, 1271' FSL 483' FWL, Section 24, T. 12 S., R. 14 E., .S.L.B.&M.
Carbon County, Utah

**1,2,3 Estimated Tops of Geological Markers and Formations Expected to Contain Water, Oil and Gas and Other Minerals**

| Formation | Depth |
|---|---|
| Green River | surface |
| Wasatch | 3040'* |
| North Horn | 4785'* |
| Price River | 6700'* |
| Base of Upper PR | 7020' |
| Bluecastle | 7880'* |
| Sego U | 8140' |
| Castlegate | 8560'* |
| Blackhawk | 8810'* |
| Star Point 1 | 9135'* |
| Star Point 2 | 9260'* |
| Star Point 3 | 9335'* |
| TD | 10,000' |

Mancos Shale

*PROSPECTIVE PAY
Star Point Sands 1, 2, & 3 are primary objectives for oil/gas
All other formations identified "*" are secondary objectives for oil/gas

**4 Casing Program**

| HOLE SIZE | SETTING DEPTH from | to | SIZE | WEIGHT | GRADE | THREAD | CONDITION |
|---|---|---|---|---|---|---|---|
| 12-1/4" | surface | 1,000' | 9-5/8" | 36# | J or K 55 | ST&C | New |
| 7-7/8" | surface | 10,000' | 5-1/2" | 17# | N-80 | LT&C | New |

**5 Cementing Program**

| | |
|---|---|
| 9-5/8" Surface Casing | approximately 240 sx Halliburton Light Premium with additives mixed at 12.7 ppg (yield = 1.85 $ft^3$/sx) and 180 sx Premium cement with additives mixed at 15.8 ppg (yield = 1.16 $ft^3$/sx) circulated to surface with 100% excess |
| 5-1/2" Production Casing | approximately 1095 sx 50/50 Poz Premium cement with additives mixed at 13.4 ppg (yield = 1.49 $ft^3$/sx). Top of cement to be determined by log and sample evaluation; estimated TOC 2500'. |

**6. Mud Program**

| INTERVAL | WEIGHT | VISCOSITY | FLUID LOSS | REMARKS |
|---|---|---|---|---|
| 0 – 40' | 8.3 – 8.6 | 27-40 | -- | Native Spud Mud |
| 40 – 1000' | 8.3 – 8.6 | 27-40 | 15 cc or less | Native/Gel/Lime |
| 1000 – TD | 8.6 – 9.5 | 38-46 | 15 cc or less | LSND/DAP |

Sufficient mud materials to maintain mud properties, control lost circulation and to contain "kick" will be available at wellsite.

**7. BOP and Pressure Containment Data**

| Depth Intervals | BOP Equipment |
|---|---|
| 0 - 1000' | No Pressure Control Required |
| 1000 – TD | 11" 3000# Ram Type BOP<br>11" 3000# Annular BOP |

Drilling spool to accommodate choke and kill lines.
Ancillary and choke manifold to be rated at 3000 psi.

ANCILLARY EQUIPMENT AND CHOKE MANIFOLD RATED AT 3000#.
ALL BOP AND BOPE TESTS WILL BE IN ACCORDANCE WITH THE REQUIREMENTS OF ONSHORE ORDER NO. 2.

THE BLM AND THE STATE OF UTAH DIVISION OF OIL, GAS AND MINING WILL BE NOTIFIED 24 HOURS IN ADVANCE OF ALL BOP PRESSURE TESTS.

**8. Auxiliary equipment**

a) Upper kelly cock; lower Kelly cock will be installed while drilling
b) Inside BOP or stab-in valve (available on rig floor)
c) Safety valve(s) and subs to fit all string connections in use
d) Mud monitoring will be visually observed

**9. Testing, Logging and Core Programs**

| | |
|---|---|
| Cores | None anticipated |
| Testing | None anticipated; drill stem tests may be run on shows of interest |
| Sampling | 30' to 50' samples; surface casing to TD<br>Preserve samples all show intervals |
| Surveys | Run every 1000' and on trips |
| Logging Program | DIL-GR-SP, FDC-CNL-GR-CALIPER-Pe-Microlog, Sonic-GR all TD to surface |

**10. Anticipated Abnormal Pressures or Temperatures**

No abnormal pressures or temperatures or other hazards are anticipated.

**11. Drilling Schedule**

| | |
|---|---|
| Spud: | Approximately June 20, 2004 |
| Duration: | 25 days drilling time |
| | 35 days completion time |

Well name: **Utah Nine Mile**
Operator: **Bill Barrett Corporation**
String type: Surface
Location: Uintah County

**Design parameters:**

**Collapse**
Mud weight: 9.500 ppg
Design is based on evacuated pipe.

**Burst**
Max anticipated surface pressure: 2,735 psi
Internal gradient: 0.220 psi/ft
Calculated BHP 2,955 psi
Annular backup: 9.50 ppg

**Minimum design factors:**

**Collapse:**
Design factor 1.125

**Burst:**
Design factor 1.00

**Tension:**
8 Round STC: 1.60 (J)
8 Round LTC: 1.60 (J)
Buttress: 1.60 (J)
Premium: 1.60 (J)
Body yield: 1.60 (B)

Tension is based on buoyed weight.
Neutral point: 859 ft

**Environment:**
H2S considered? No
Surface temperature: 60 °F
Bottom hole temperature: 74 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 1,000 ft
Minimum Drift: 8.750 in
Cement top: Surface

Non-directional string.

**Re subsequent strings:**
Next setting depth: 10,000 ft
Next mud weight: 9.500 ppg
Next setting BHP: 4,935 psi
Fracture mud wt: 10.000 ppg
Fracture depth: 10,000 ft
Injection pressure 5,195 psi

| Run Seq | Segment Length (ft) | Size (in) | Nominal Weight (lbs/ft) | Grade | End Finish | True Vert Depth (ft) | Measured Depth (ft) | Drift Diameter (in) | Est. Cost (USD) |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 1000 | 9.625 | 36.00 | J-55 | ST&C | 1000 | 1000 | 8.796 | 0 |

| Run Seq | Collapse Load (psi) | Collapse Strength (psi) | Collapse Design Factor | Burst Load (psi) | Burst Strength (psi) | Burst Design Factor | Tension Load (Kips) | Tension Strength (Kips) | Tension Design Factor |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 493 | 2020 | 4.094 | 2735 | 3613 | 1.32 | 31 | 453 | 14.64 J |

Prepared by: Troy Schindler
Bill Barrett
Phone: (303) 312-8156
FAX: (303) 312-8195
Date: March 25,2003
Denver, Colorado

Remarks:
Collapse is based on a vertical depth of 1000 ft, a mud weight of 9.5 ppg The casing is considered to be evacuated for collapse purposes.
Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

In addition, burst strength is biaxially adjusted for tension.

*Engineering responsibility for use of this design will be that of the purchaser.*

Well name: **Utah Nine Mile**
Operator: **Bill Barrett Corporation**
String type: Production: Frac
Location: Uintah County

**Design parameters:**

**Collapse**
Mud weight: 9.500 ppg
Design is based on evacuated pipe.

**Burst**
Max anticipated surface pressure: 6,000 psi
Internal gradient: 0.023 psi/ft
Calculated BHP 6,234 psi
Annular backup: 9.50 ppg

**Minimum design factors:**

**Collapse:**
Design factor 1.125

**Burst:**
Design factor 1.20

**Tension:**
8 Round STC: 1.80 (J)
8 Round LTC: 1.80 (J)
Buttress: 1.80 (J)
Premium: 1.80 (J)
Body yield: 1.80 (B)

Tension is based on buoyed weight.
Neutral point: 8,559 ft

**Environment:**
H2S considered? No
Surface temperature: 60 °F
Bottom hole temperature: 200 °F
Temperature gradient: 1.40 °F/100ft
Minimum section length: 0,000 ft
Minimum Drift: 4.750 in
Cement top: 2,375 ft

Non-directional string.

| Run Seq | Segment Length (ft) | Size (in) | Nominal Weight (lbs/ft) | Grade | End Finish | True Vert Depth (ft) | Measured Depth (ft) | Drift Diameter (in) | Est. Cost (USD) |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 10000 | 5.5 | 17.00 | N-80 | LT&C | 10000 | 10000 | 4.767 | 0 |

| Run Seq | Collapse Load (psi) | Collapse Strength (psi) | Collapse Design Factor | Burst Load (psi) | Burst Strength (psi) | Burst Design Factor | Tension Load (Kips) | Tension Strength (Kips) | Tension Design Factor |
|---|---|---|---|---|---|---|---|---|---|
| 1 | 4935 | 6290 | 1.275 | 6000 | 8758 | 1.46 | 146 | 348 | 2.39 J |

Prepared by: Troy Schindler
Bill Barrett
Phone: (303) 312-8156
FAX: (303) 312-8195
Date: March 25,2003
Denver, Colorado

Remarks:
Collapse is based on a vertical depth of 10000 ft, a mud weight of 9.5 ppg The casing is considered to be evacuated for collapse purposes.
Collapse strength is based on the Westcott, Dunlop & Kemler method of biaxial correction for tension.

In addition, burst strength is biaxially adjusted for tension.

*Engineering responsibility for use of this design will be that of the purchaser.*

**HALLIBURTON**

## *Job Recommendation* — *Surface Casing*

Fluid Instructions
Fluid 1: Water Spacer
Water Spacer w/Gel

| | |
|---|---|
| Fluid Density: | 8.50 lbm/gal |
| Fluid Volume: | 20 bbl |

Fluid 2: Lead Cement – (700 – 0')
Halliburton Light Premium, 6% gel standard
2 % Calcium Chloride (Accelerator)
0.125 lbm/sk Poly-E-Flake (Lost Circulation Additive)

| | |
|---|---|
| Fluid Weight | 12.7 lbm/gal |
| Slurry Yield: | 1.85 $ft^3$/sk |
| Total Mixing Fluid: | 9.90 Gal/sk |
| Top of Fluid: | 0 ft |
| Calculated Fill: | 700 ft |
| Volume: | 78.09 bbl |
| Calculated Sacks: | 237.01 sks |
| **Proposed Sacks:** | **240 sks** |

Fluid 3: Primary Cement – (TD – 700')
Premium Cement
94 lbm/sk Premium Cement (Cement-api)
2 % Calcium Chloride (Accelerator)
0.125 lbm/sk Poly-E-Flake (Lost Circulation Additive)

| | |
|---|---|
| Fluid Weight | 15.8 lbm/gal |
| Slurry Yield: | 1.16 $ft^3$/sk |
| Total Mixing Fluid: | 4.97 Gal/sk |
| Top of Fluid: | 700 ft |
| Calculated Fill: | 300 ft |
| Volume: | 36.56 bbl |
| Calculated Sacks: | 176.81 sks |
| **Proposed Sacks:** | **180 sks** |

HALLIBURTON

## Job Recommendation — Production Casing

Fluid Instructions

Fluid 1: Water Spacer
Water Spacer

| | |
|---|---|
| Fluid Density: | 8.40 lbm/gal |
| Fluid Volume: | 5 bbl |

Fluid 2: Reactive Spacer
SUPER FLUSH 101

| | |
|---|---|
| Fluid Density: | 10 lbm/gal |
| Fluid Volume: | 20 bbl |

Fluid 3: Water Spacer
Water Spacer

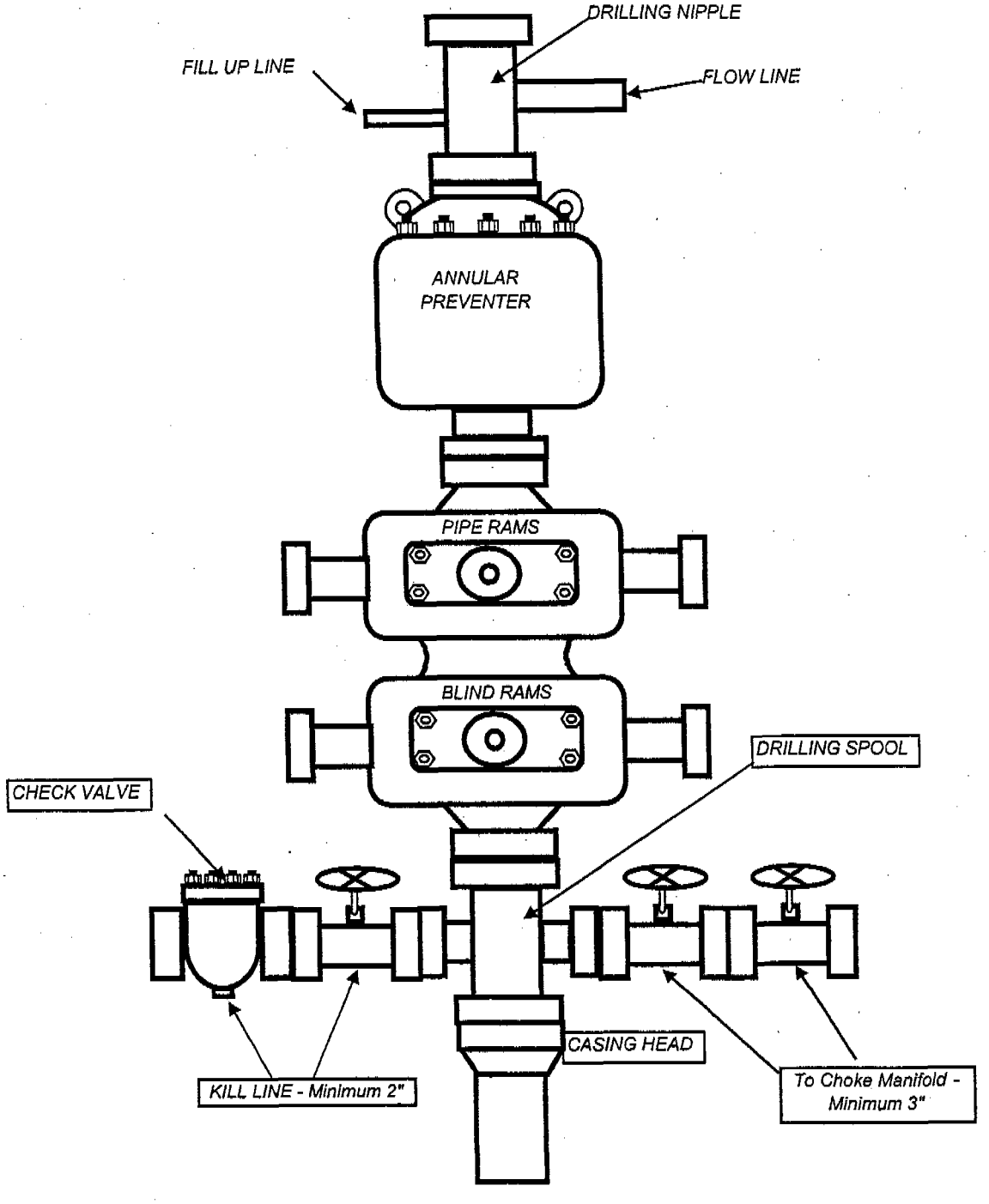
| | |
|---|---|
| Fluid Density: | 8.40 lbm/gal |
| Fluid Volume: | 5 bbl |

Fluid 4: Primary Cement – (TD – 2500')
50/50 Poz Premium, 2% gel standard

| | | | |
|---|---|---|---|
| 3 % | KCL (Additive Material) | Fluid Weight | 13.40 lbm/gal |
| 0.75 % | Halad(R)-322 (Low Fluid Loss Control) | Slurry Yield: | 1.49 $ft^3$/sk |
| 3 lbm/sk | Silicalite Compacted (Light Weight Additive) | Total Mixing Fluid: | 7.06 Gal/sk |
| 0.2 % | FWCA (Free Water Control) | Top of Fluid: | 2500 ft |
| 0.125 lbm/sk | Poly-E-Flake (Lost Circulation Additive) | Calculated Fill: | 7500 ft |
| 1 lbm/sk | Granulite TR 1/4 (Lost Circulation Additive) | Volume: | 290.22 bbl |
| | | Calculated Sacks: | 1093.61 sks |
| | | **Proposed Sacks:** | **1095 sks** |

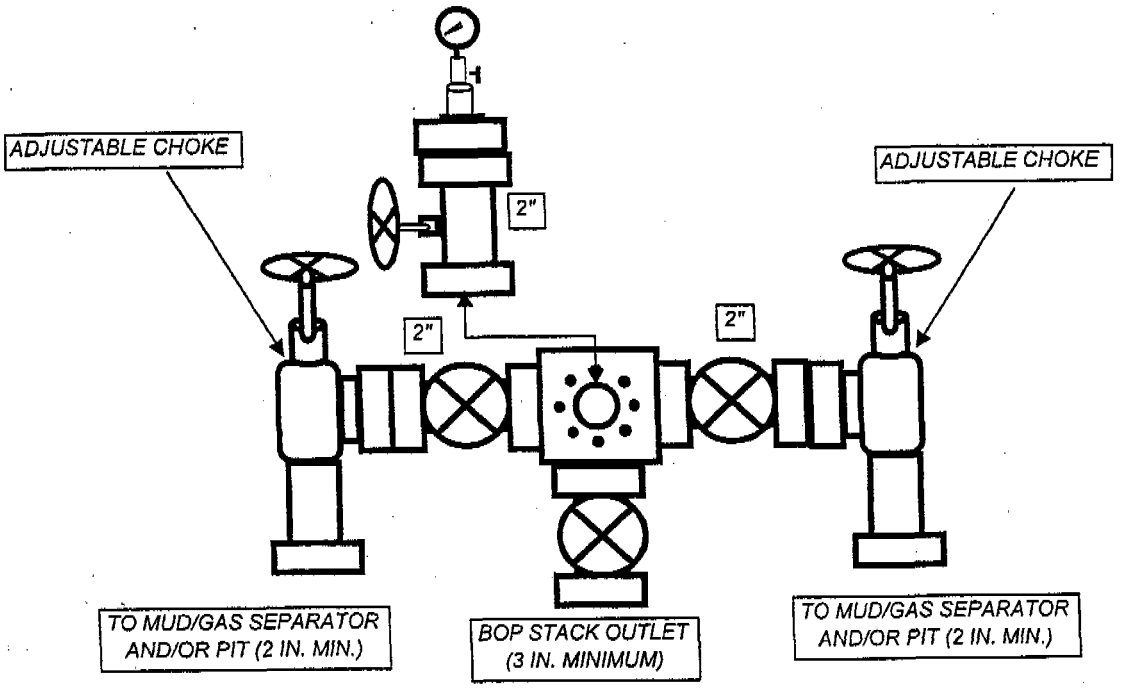
# BILL BARRETT CORPORATION

## TYPICAL 3,000 p.s.i. BLOWOUT PREVENTER



# BILL BARRETT CORPORATION

## *TYPICAL 3,000 p.s.i. CHOKE MANIFOLD*



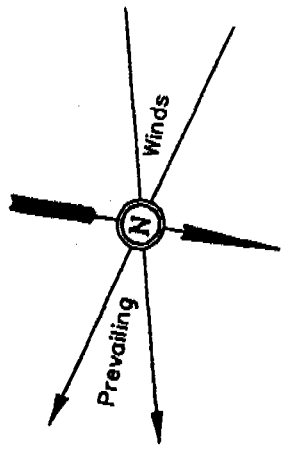
# BILL BARRETT CORPORATION

## LOCATION LAYOUT FOR

## PRICKLY PEAR UNIT #12-24

SECTION 24, T12S, R14E, S.L.B.&M.

~~1856'~~ FSL ~~711'~~ 1271 FWL 483




SCALE: 1" = 50'
DATE: 6-24-03
DRAWN BY: C.G.

**NOTE:**
*Flare Pit is to be located a min. of 100' from the Well Head.*

C-6.4'
El. 51.3'

C-4.3'
El. 49.2'

F-0.6'
El. 44.3'

Topsoil Stockpile

Sta. 3+25

CONSTRUCT DIVERSION DITCH

Topsoil Stockpile

DATA

150'

400BBL OIL TK

400BBL WTR TK

CATWALK

Approx. Top of Cut Slope

PIPE RACKS

El. 47.9'
C-3.0'

Flare Pit

C-1.0'
El. 45.9'

DOG HOUSE

RIG

35'

115'

Sta. 1+75

F-2.5'
El. 42.4'

El. 53.3'
C-16.4'
(Btm. Pit)

75'

PIT CAPACITY WITH 2' OF FREEBOARD = 5,480 Bbls.

10' WIDE BENCH

100'

1 1/2:1 (TYP.)

RESERVE PIT 8' DEEP

Reserve Pit Backfill & Spoils Stockpile

MUD TANKS

WATER

PUMP

MUD SHED

Hook up lines

TRAILER

TOILET

HOPPER

Sta. 1+00

FUEL

POWER

TOOLS

Seperator

Approx. Toe of Fill Slope

FUEL

STORAGE TANK

El. 47.9'
C-11.0'
(Btm. Pit)

El. 44.3'
F-0.6'

75'

175'

F-5.3'
El. 39.6'

Round Corners as Needed

TRASH

F-3.6'
El. 41.3'

Sta. 0+00

F-3.0'
El. 41.9'

4" Gas Sales line

Proposed Access Road

Elev. Ungraded Ground at Location Stake = 7745.9'

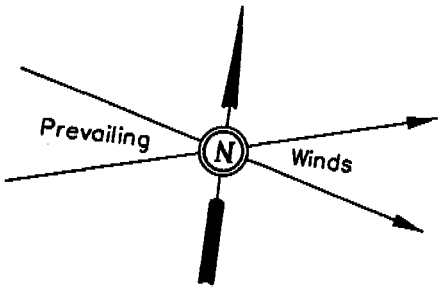
Elev. Graded Ground at Location Stake = 7744.9'


UINTAH ENGINEERING & LAND SURVEYING
85 So. 200 East • Vernal, Utah 84078 • (435) 789-1017

# BILL BARRETT CORPORATION

## LOCATION LAYOUT FOR

PRICKLY PEAR UNIT #12-24
SECTION 24, T12S, R14E, S.L.B.&M.
1271' FSL 483' FEL




SCALE: 1" = 50'
DATE: 8-11-03
DRAWN BY: C.G.

*NOTE:*
*Flare Pit is to be located a min. of 100' from the Well Head.*

F-6.0'
El. 786.9'

F-5.0'
El. 787.9'

F-9.2'
El. 783.7'

Topsoil Stockpile

Sta. 3+25

Existing 2-Track

DATA

CATWALK

150'

PIPE RACKS

Approx. Top of Cut Slope

El. 797.7'
C-4.8'

Flare Pit

C-2.4'
El. 795.3'

RIG

DOG HOUSE

35'

115'

El. 801.6'
C-16.7'
(Btm. Pit)

75'

PIT CAPACITY WITH 2' OF FREEBOARD = 5,480 Bbls.

RESERVE PIT 8' DEEP

100'

10' WIDE BENCH

1 1/2:1 (TYP.)

Reserve Pit Backfill & Spoils Stockpile

MUD TANKS

WATER

TRAILER

PUMP

TOILET

MUD SHED

HOPPER

Sta. 1+00

FUEL

POWER

TOOLS

FUEL

STORAGE TANK

Sta. 1+75

F-10.0'
El. 782.9'

Approx. Toe of Fill Slope

El. 805.7'
C-20.8'
(Btm. Pit)

El. 800.6'
C-7.7'

75'

175'

TRASH

Round Corners as Needed

F-10.5'
El. 782.4'

Sta. 0+00

C-6.6'
El. 799.5'

Topsoil Stockpile

C-10.1'
El. 803.0'

Use As Proposed Acces Road

Elev. Ungraded Ground at Location Stake = 7795.3'

Elev. Graded Ground at Location Stake = 7792.9'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# BILL BARRETT CORPORATION

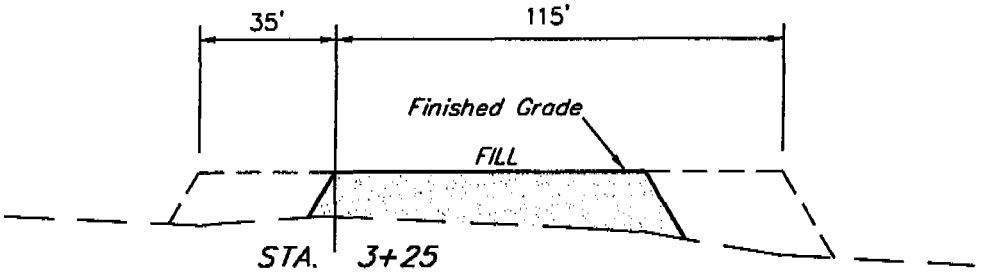
## TYPICAL CROSS SECTIONS FOR

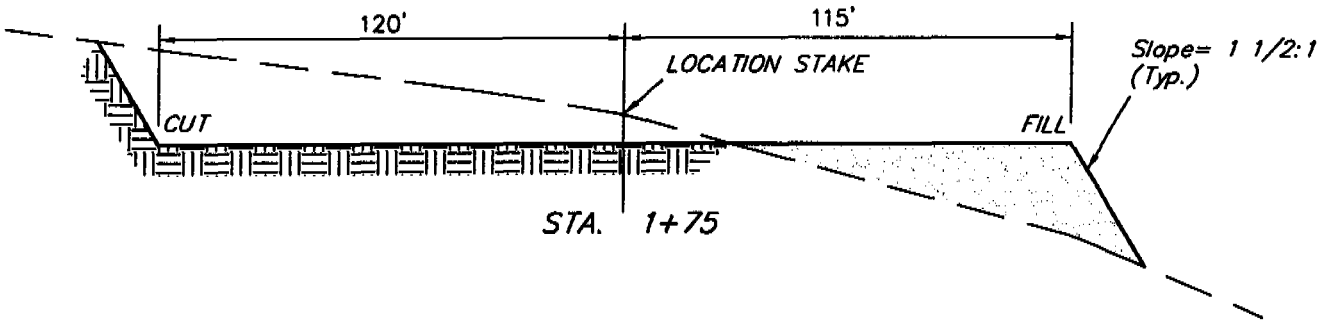
PRICKLY PEAR UNIT #12-24
SECTION 24, T12S, R14E, S.L.B.&M.
1271' FSL 483' FWL

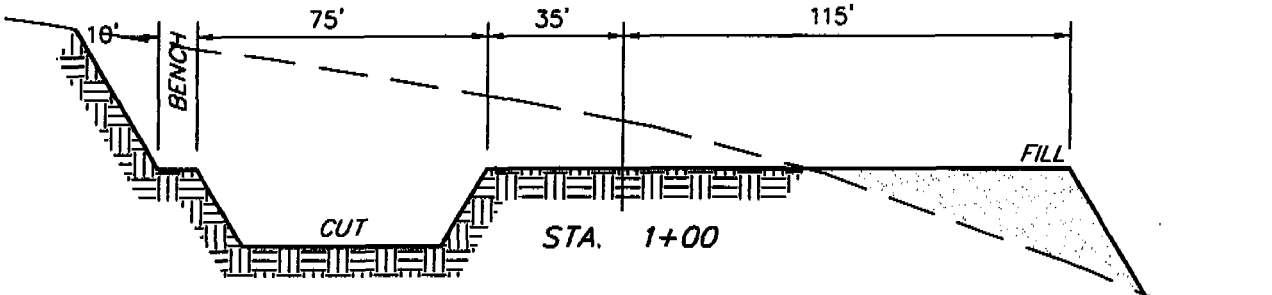
REGISTERED LAND SURVEYOR
No. 161319
STATE OF UTAH

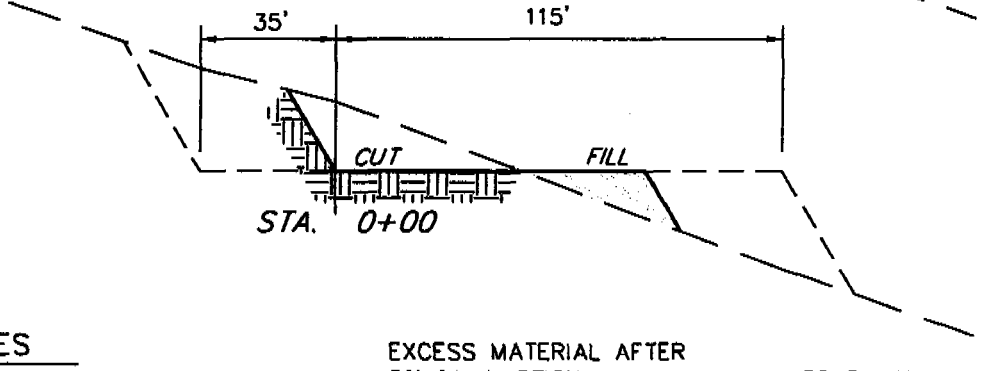
1" = 20'
X-Section
Scale
1" = 50'

DATE: 8-11-03
DRAWN BY: C.G.




## APPROXIMATE YARDAGES

CUT
(6") Topsoil Stripping = 1,090 Cu. Yds.
Remaining Location = 8,440 Cu. Yds.
TOTAL CUT = 9,530 CU.YDS.
FILL = 7,230 CU.YDS.

EXCESS MATERIAL AFTER
5% COMPACTION = 1,920 Cu. Yds.
Topsoil & Pit Backfill (1/2 Pit Vol.) = 1,920 Cu. Yds.
EXCESS UNBALANCE (After Rehabilitation) = 1 Cu. Yds.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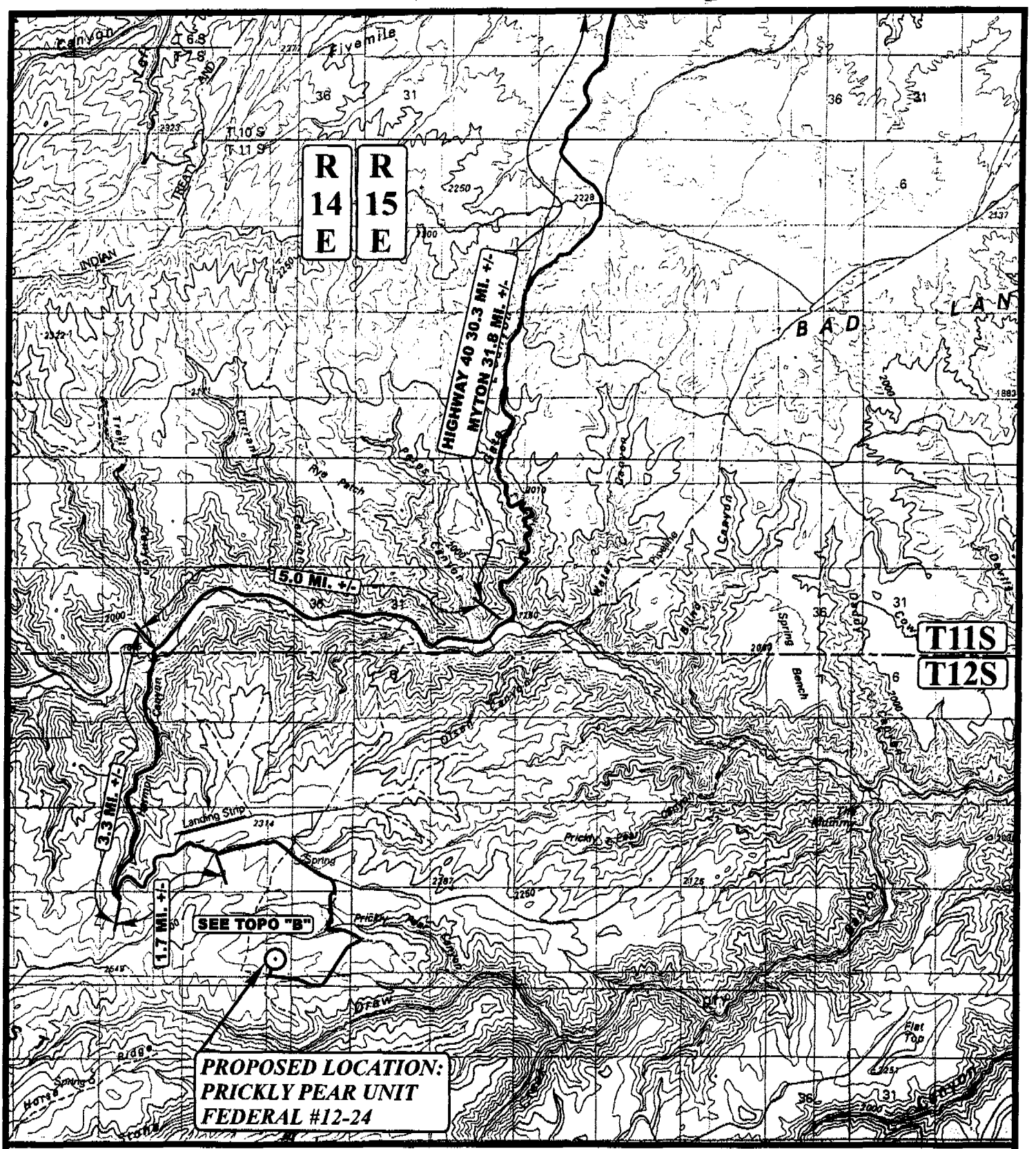



**LEGEND:**

⊙ PROPOSED LOCATION

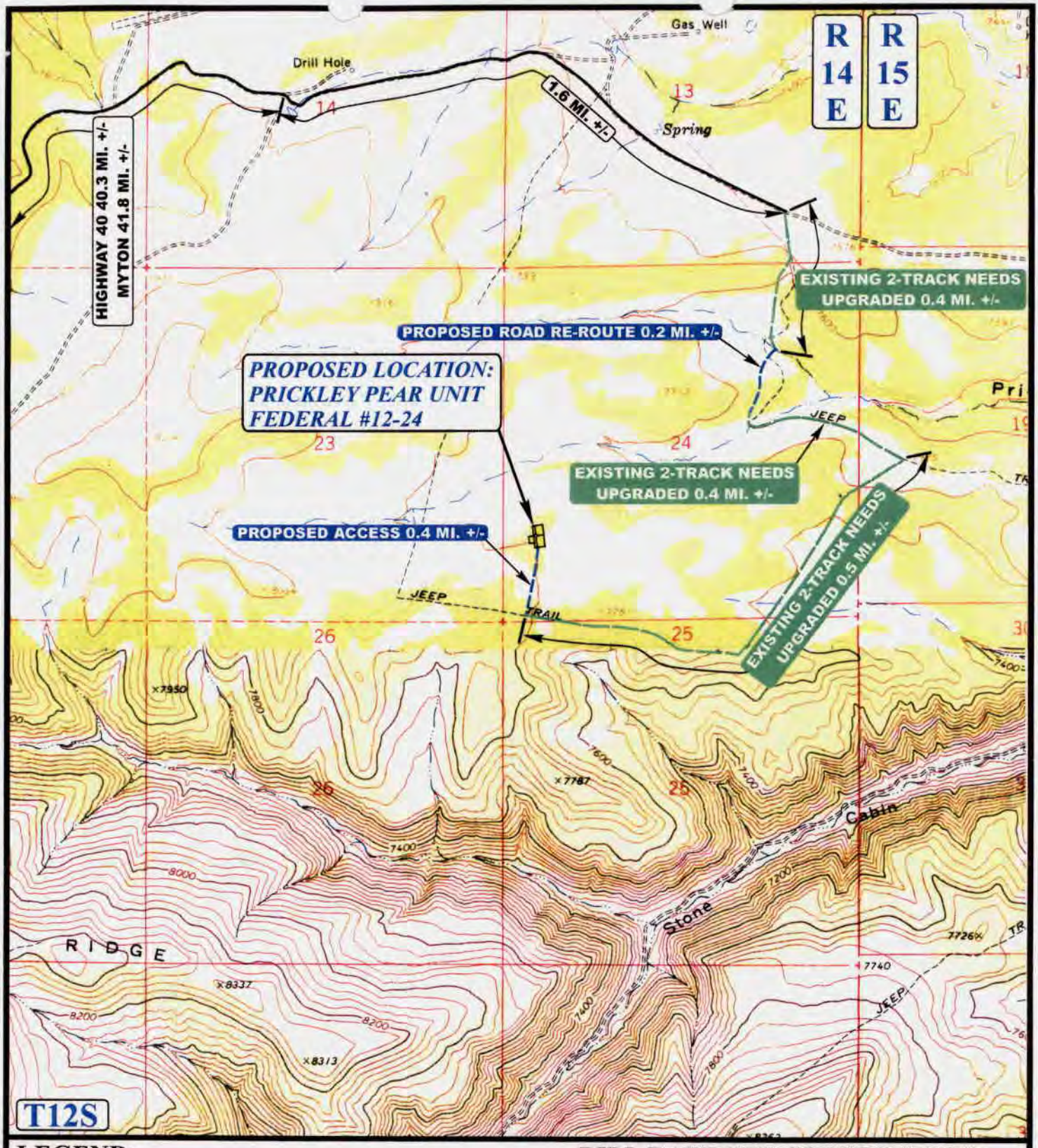
N

**BILL BARRETT CORPORATION**

**PRICKLEY PEAR UNIT FEDERAL #12-24**
**SECTION 24, T12S, R14E, S.L.B.&M.**
**1271' FSL 483' FWL**


Uintah Engineering & Land Surveying
85 South 200 East Vernal, Utah 84078
(435) 789-1017 * FAX (435) 789-1813


| TOPOGRAPHIC MAP | 6 MONTH | 20 DAY | 03 YEAR | A TOPO |
|---|---|---|---|---|
| SCALE: 1:100,000 | DRAWN BY: K.G. | REVISED: 8-11-03 | | |




**LEGEND:**

PROPOSED ACCESS ROAD
EXISTING ROAD
EXISTING 2-TRACK NEEDS UPGRADED

N

**BILL BARRETT CORPORATION**

**PRICKLEY PEAR UNIT FEDERAL #12-24**
**SECTION 24, T12S, R14E, S.L.B.&M.**
**1271' FSL 483' FWL**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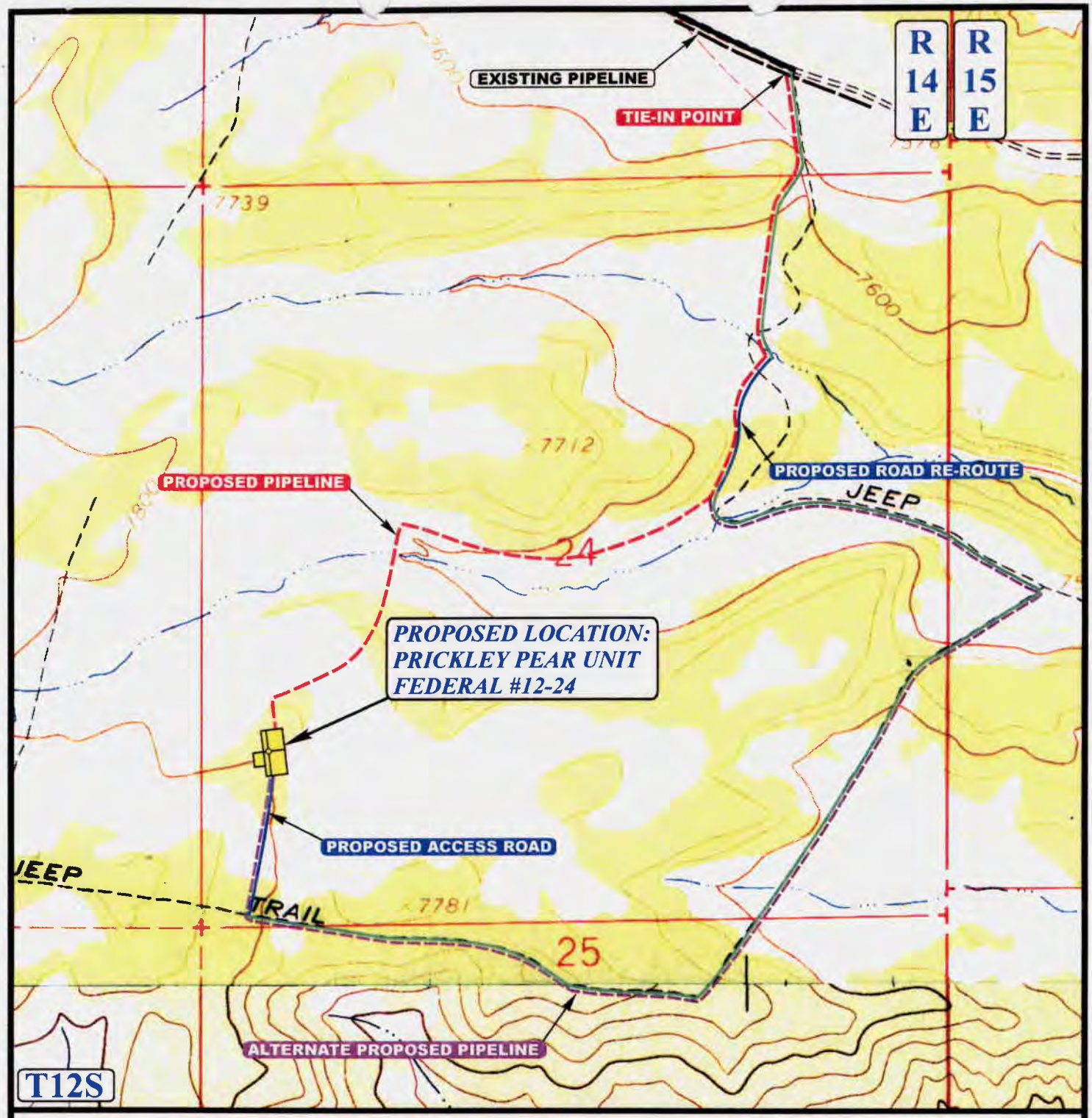
85 South 200 East Vernal, Utah 84078
(435) 789-1017 * FAX (435) 789-1813


TOPOGRAPHIC MAP | 6 MONTH | 20 DAY | 03 YEAR | B TOPO

SCALE: 1" = 2000' | DRAWN BY: K.G. | REVISED: 8-11-03




APPROXIMATE TOTAL PIPELINE DISTANCE = 7,390' +/-

APPROXIMATE TOTAL ALTERNATE PIPELINE DISTANCE = 13,890' +/-

**LEGEND:**

EXISTING PIPELINE

PROPOSED PIPELINE

PROPOSED ACCESS

N

**BILL BARRETT CORPORATION**

**PRICKLEY PEAR UNIT FEDERAL #12-24**
**SECTION 24, T12S, R14E, S.L.B.&M.**
**1271' FSL 483' FWL**


Uintah Engineering & Land Surveying
85 South 200 East Vernal, Utah 84078
(435) 789-1017 * FAX (435) 789-1813


TOPOGRAPHIC MAP | 6 MONTH | 20 DAY | 03 YEAR

SCALE: 1" = 1000' | DRAWN BY: K.G. | REVISED: 8-11-03

C TOPO

**BILL BARRETT CORPORATION**

**13 POINT SURFACE USE PLAN**

**FOR**

**WELL LOCATION**

**PRICKLY PEAR UNIT FEDERAL 12-24**

**LOCATED IN**

**SW ¼ SW ¼, 1271' FSL, 483' FWL**
**SECTION 24, T. 12 S. , R. 14 E., S.L.B.&M.**

**CARBON COUNTY, UTAH**

**LEASE NUMBER: UTU 77513**
**SURFACE OWNERSHIP: STATE OF UTAH**
**SCHOOL AND INSTITUTIONAL TRUST LANDS ADMINISTRATION**

## 1. Existing Roads

To reach the Bill Barrett Corporation well, Prickly Pear Unit Federal 12-24 location, in Section 24-T12S-R14E:

Beginning at the intersection of the bridge over the Duchesne River and US Highway 40 in the town of Myton, Utah travel southwesterly for approximately 1.8 miles to coinciding Utah State Highways 53 and 126. Turn left and travel southerly, then southwesterly, then southerly on Highways 53 and 126 for approximately 1.7 miles to the dedicated Utah State Highway 53. Turn left and travel Highway 53 southwesterly for approximately 2.7 miles to Pleasant Valley, then travel for approximately 6.0 miles to Wells Draw Canyon. Continue travel for approximately 15 miles in Wells Draw Canyon on Highway 53 and then travel in Gate Canyon on Highway 53 for approximately 6.3 miles to an intersection with an existing resource road. Turn right at Gates Canyon and travel west approximately 4.5 miles, continuing on Harmon Canyon Road traveling southwest for approximately 3 miles and then following Harman Canyon Road as it turns back east approximately another 3 miles to an existing jeep trail. Turn right onto this jeep trail and traveling south, then southeasterly and then again south for approximately 1.5 miles to the staked proposed access road heading due north. Continue travel on staked access for approximately 4/10ths of a mile to the proposed location.

The entire 1.5 miles of the existing jeep trail access road will be upgraded in order to accommodate heavy truck traffic during the drilling and completion operations and 2/10ths of a mile of this road will be rerouted. Bill Barrett Corporation, as operator, or its contractors or subcontractors, will secure material from private sources to facilitate these road improvements. This existing to-be-improved road will be maintained in the same or better condition as existed prior to the commencement of operations and said maintenance will continue until final abandonment and reclamation of said well location.

Please see the attached Topo A map for additional details.

## 2. Planned access road

Approximately 3250 feet of new access road will be required.
±3250 feet, on lease, Section 24-T12S-R14E, BLM
approximately ±1050 feet in the SWNE for the rerouted portion and ±2200 in the SW/4 of Section 24 for new access to the location

Details of the construction are as follows;
Length- 3,250 ft (approx)
Width- 32 ft (approx)
Grade- 10% or less

Please see the attached Topo B map for additional details.

No right of way will be required. All new construction will be conducted within the Prickly Pear Federal Unit.

All travel will be confined to existing road right of ways.
Access roads and surface disturbing activities will conform to standards outlined in the USGS publication (1978) Surface Operation Standards for Oil and Gas Development.

**3. Location of existing wells.**

There are no producing wells, water wells or abandoned or temporarily abandoned wells within a one mile radius of the location site.

**4. Location of Tank Batteries, Production Facilities and Production Gathering and Service Lines**

The proposed location of production facilities on the well pad is shown on the well site layout drawing included herein. All production facilities are to be contained within the proposed location site. Production facilities consisting of one oil tank and one water tank, one gas separator and a meter will be placed on cut portions of the pad and be located so as to maintain minimum distances between equipment and tanks for safety purposes. Facilities will be located a minimum of 25' from the tow of the back cut.

All permanent (on site for six months or longer) structures constructed or installed will be painted a desert brown color. All facilities will be painted within six months of installation. Facilities required to comply with O.S.H.A. (Occupational Safety and Health Act) will be excluded. The required paint color is desert brown (Munsell standard color #10 YR 6/3).

A dike will be constructed around the tank (s). The dike will be constructed of compacted subsoil, be impervious, and hold 1.5 times the capacity of the largest tank.

An 8 or 10-inch steel gas line will be installed cross-country to the south through Section 24 covering 7,390' as the proposed pipeline is laid out on Topo C. There is also depicted on Topo C an alternate proposed pipeline covering 13,890' and following the access and improved jeep trail. Both lines go north and tie into an existing gas line that runs along the south side of the main road. (Please refer to Topo C of the plat package.)

All site security guidelines identified in 43 CFR 3126.7 regulation will be adhered to. All off-lease storage, off-lease measurement, or commingling on lease or off lease will have prior written approval from the authorized officer.

If a gas meter run is constructed, it will be located within approximately 100 feet of the wellhead. The gas line will be buried, or anchored down from the wellhead to the meter. Meter runs will be housed and/or fenced.

The gas meter will be calibrated and the tank strapped in place prior to any deliveries. Tests for the meter accuracy will be conducted monthly for the first three months on new meter installations and at least quarterly thereafter. The authorized officer will be provided with a date and time for the initial meter calibration and all future meter proving schedules. A copy of the meter calibration report will be submitted to the Moab field office. All measurement facilities will conform to API and AGA standards for gas and liquid hydrocarbon measurement.

**5. Location and Type of Water Supply**

Bill Barrett Corporation will utilize an existing water well located on BLM lands in the SW/4 SE/4 of Section 13-T12S-R14E. Bill Barrett Corporation has been granted this authorization by the State of Utah Application Number 90-1826 (T74077) on August 20, 2002.

**6. Source of Construction Materials**

All construction material for this location site and access road shall be borrow material accumulated during construction of the location site and access road. Additional gravel or pit lining material will be obtained from private sources.

## 7. Methods for Handling Waste Disposal

A) Pit construction and liners:

The reserve pit will be approximately 8 feet deep and at least one-half of the depth shall be below the surface of the existing ground.

The reserve pit will be lined with a 16 mil pit liner with felt underneath where necessary. The pit liner will be torn and perforated after the pit dries and before backfilling the reserve pit. The reserve pit will be reasonably free of hydrocarbons before the pit is backfilled.

B) Produced Fluids:

Produced water will be confined to the reserve pit, or if deemed necessary, a storage tank for a period not to exceed 90 days after initial production. Thereafter, produced water will be trucked to R & I Disposal, a State approved disposal facility.

C) Garbage:

A trash cage, fabricated from expanded metal, will be used to hold trash on location and will be removed to an authorized landfill location.

D) A portable chemical toilet will be supplied for human waste.

E) Site clean-up:

After the rig is moved out, the area around the wellsite will be cleaned and all refuse removed.

## 8. Ancillary Facilities

There are no ancillary facilities planned for at this time and none are foreseen in the future.

**9. Wellsite Layout**

Location dimensions are as follows:

| | |
|---|---|
| A) PAD LENGTH | 325 FT |
| B) PAD WIDTH | 150 FT |
| C) PIT DEPTH | 8 FT |
| D) PIT LENGTH | 100 FT |
| E) PIT WIDTH | 75 FT |
| F) MAX CUT | 20.8 FT |
| G) MAX FILL | 10.5 FT |
| H) TOTAL CUT YARDS | 9,530 CU YDS |
| I) PIT LOCATION | WEST SIDE |
| J) TOP SOIL LOCATION | NORTH END & SOUTH END |
| K)ACCESS ROAD LOCATION | FROM THE SOUTH |
| L) FLARE PIT | WEST SIDE |

Please see the attached location diagram for additional details.

Prior to commencement of drilling operations, the reserve pit will be fenced on three (3) sides with four strand barbed wire held in place by metal side posts and wooden corner "H" braces in order to protect livestock and wildlife.

A) Corner posts shall be braced in such a manner as to keep the fence tight at all times.

B) Standard steel, wood or pipe posts shall be used between the corner braces. Distance between any two posts shall be no greater than 16 ft.

C) All wire shall be stretched, by using a stretching device, before it is attached to the corner posts.

D) The fourth ($4^{th}$) side of the reserve pit will be fenced immediately upon removal of the drilling rig and the fencing will be maintained until the pit is backfilled.

E) Any hydrocarbons on the pit will be removed immediately

**10. Plans for Restoration of the Surface**

Prior to the construction of the location, the top 6 inches of soil material will be stripped and stockpiled. This will amount to 1,090 cubic yards of material. Placement of the topsoil is noted on the attached location plat. When all drilling and completion activities have been completed, the unused portion of the location (the area outside the deadmen) will be recontoured and the topsoil spread over the area.

The dirt contractor will be provided with an approved copy of the surface use plan prior to construction activities.

Any drainage rerouted during the construction activities shall be restored to its original line of flow or as near as possible.

All disturbed areas will be recontoured to the approximate natural contours. Prior to backfilling the pit, the fences around the reserve pit will be removed. The pit liner will be cut off at the water or mud line and disposed of at an approved landfill site. The liner will also be torn and perforated after the pit dries and before backfilling of the reserve pit.

The reserve pit will be reclaimed within one (1) year of well completion. If the reserve pit has not dried sufficiently to allow backfilling, an extension on the time requirement for backfilling the pit will be requested. Once reclamation activities have begun, they shall be completed within 30 days.

After the reserve pit has been reclaimed, no depressions in the soil covering the reserve pit will be allowed. The objective is to keep seasonal rainfall and runoff from seeping into the soil used to cover the reserve pit. Diversion ditches and water bars will be used to divert runoff as needed.

When restoration activities have been completed, the location site and new access road cuts and shoulders shall be reseeded as recommended by the BLM. Prior to reseeding, all disturbed areas, including the old access road, will be scarified and left with a rough surface. Seeding will take place either during the fall (prior to ground frost) or spring (after frost leaves the ground) months.

Seed will be broadcast or drilled at the time specified by the BLM. If broadcast, a harrow or some other implement will be dragged over the seeded area to assure seed coverage and the seed mixture will be proportionately larger (double the pounds per acre).

At such time the well is plugged and abandoned, the operator will submit a surface reclamation plan to the Surface Management Agency for prescribed seed mixture and reseeding requirements.

**11. Surface Ownership:**

State of Utah; School and Institutional Trust Lands Administration

**12. Other Information**

A) Vegetation:

The trees in the area are cedar and pinion. The vegetation coverage is intermittent. The majority of the existing understory vegetation is made up of rabbitbrush, sage, and bitter brush. Also found on the location is prickly pear and various grasses.

B) Dwellings:

There are no occupied dwellings, or other facilities within a one mile radius of this location.

C) Archaeology:

The location has been surveyed and is being recommended for clearance. No archaeological, historical, or cultural sites near the proposed site and access road will be directly impacted. A copy of the written archaeological report dated July 9, 2003 should be in your files.

If, during operations, any archaeological or historical sites, or any objects of antiquity (subject to the Antiquities Act of June 8, 1906) are discovered, all operations which would affect such sites are to be suspended and the discovery reported promptly to the surface management agency.

D) Water:

The nearest water would be in Stone Cabin Draw approximately one and one-half miles to the south.

E) Chemicals:

No pesticides, herbicides or other possible hazardous chemicals shall be used without prior application.

F) Notification:

BLM, Moab, Utah: (435-259-2100)
24 to 48 hours before construction of the location.
Also after site construction and before the rig moves in.

H) Flare Pit:

The flare pit will be located 15 feet from the reserve pit fence and 100 feet from the bore hole on the west side of the location, immediately above point C on the location layout plat. All fluids will be removed from the pit within 48 hours of occurrence.

I) Grazing Permittee:

George and Gloria Fasselin
P. O. Box 18
Wellington, Utah 84542
Home: 435-637-1708

**13. Lessees or Operators Representative and Certification**

A) Representative

| | |
|---|---|
| NAME: | Debra K. Stanberry |
| ADDRESS: | Bill Barrett Corporation<br>1099 18th Street, Suite 2300<br>Denver, Colorado 80201 |
| PHONE: | 303-312-8120 |

All lease and/or unit operations will be conducted in such a manner that full compliance is made with all applicable laws, regulations and onshore oil and gas orders. The operator is fully responsible for the actions of its contractors and subcontractors. A copy of these conditions will be furnished to the field representative to ensure compliance.

The drilling permit will be valid for a period of one year from the date of approval. After permit termination, a new application will be filed for approval for any future operations.

B) Certification:

I hereby certify that the statements made in this plan are, to the best of my knowledge and belief, true and correct; and that the work associated with the operations proposed herein will be performed by Bill Barrett Corporation and its contractors and subcontractors in conformity with this plan and the terms and conditions under which it is approved. This statement is subject to the provisions of 18 U.S.C. 1001 for the filing of a false statement.

DATE April 23, 2004

Debra K. Stanberry
Permit Specialist
Bill Barrett Corporation

**BILL BARRETT CORPORATION**

**13 POINT SURFACE USE PLAN**

**FOR**

**WELL LOCATION**

**PRICKLY PEAR UNIT FEDERAL 12-24**

**LOCATED IN**

**SW ¼ SW ¼, 1271' FSL, 483' FWL**
**SECTION 24, T. 12 S. , R. 14 E., S.L.B.&M.**

**CARBON COUNTY, UTAH**

**LEASE NUMBER: UTU 77513**

**SURFACE OWNERSHIP: UNITED STATES GOVERNMENT**

## 1. Existing Roads

To reach the Bill Barrett Corporation well, Prickly Pear Unit Federal 12-24 location, in Section 24-T12S-R14E:

Beginning at the intersection of the bridge over the Duchesne River and US Highway 40 in the town of Myton, Utah travel southwesterly for approximately 1.8 miles to coinciding Utah State Highways 53 and 126. Turn left and travel southerly, then southwesterly, then southerly on Highways 53 and 126 for approximately 1.7 miles to the dedicated Utah State Highway 53. Turn left and travel Highway 53 southwesterly for approximately 2.7 miles to Pleasant Valley, then travel for approximately 6.0 miles to Wells Draw Canyon. Continue travel for approximately 15 miles in Wells Draw Canyon on Highway 53 and then travel in Gate Canyon on Highway 53 for approximately 6.3 miles to an intersection with an existing resource road. Turn right at Gates Canyon and travel west approximately 4.5 miles, continuing on Harmon Canyon Road traveling southwest for approximately 3 miles and then following Harman Canyon Road as it turns back east approximately another 3 miles to an existing jeep trail. Turn right onto this jeep trail and traveling south, then southeasterly and then again south for approximately 1.5 miles to the staked proposed access road heading due north. Continue travel on staked access for approximately 4/10ths of a mile to the proposed location.

The entire 1.5 miles of the existing jeep trail access road will be upgraded in order to accommodate heavy truck traffic during the drilling and completion operations and 2/10ths of a mile of this road will be rerouted. Bill Barrett Corporation, as operator, or its contractors or subcontractors, will secure material from private sources to facilitate these road improvements. This existing to-be-improved road will be maintained in the same or better condition as existed prior to the commencement of operations and said maintenance will continue until final abandonment and reclamation of said well location.

Please see the attached Topo A map for additional details.

## 2. Planned access road

Approximately 3250 feet of new access road will be required.
±3250 feet, on lease, Section 24-T12S-R14E, BLM
approximately ±1050 feet in the SWNE for the rerouted portion and ±2200 in the SW/4 of Section 24 for new access to the location

Details of the construction are as follows;
Length- 3,250 ft (approx)
Width- 32 ft (approx)
Grade- 10% or less

Please see the attached Topo B map for additional details.

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All travel will be confined to existing road right of ways.
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**3. Location of existing wells.**

There are no producing wells, water wells or abandoned or temporarily abandoned wells within a one mile radius of the location site.

**4. Location of Tank Batteries, Production Facilities and Production Gathering and Service Lines**

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A dike will be constructed around the tank (s). The dike will be constructed of compacted subsoil, be impervious, and hold 1.5 times the capacity of the largest tank.

An 8 or 10-inch steel gas line will be installed cross-country to the south through Section 24 covering 7,390' as the proposed pipeline is laid out on Topo C. There is also depicted on Topo C an alternate proposed pipeline covering 13,890' and following the access and improved jeep trail. Both lines go north and tie into an existing gas line that runs along the south side of the main road. (Please refer to Topo C of the plat package.)

All site security guidelines identified in 43 CFR 3126.7 regulation will be adhered to. All off-lease storage, off-lease measurement, or commingling on lease or off lease will have prior written approval from the authorized officer.

If a gas meter run is constructed, it will be located within approximately 100 feet of the wellhead. The gas line will be buried, or anchored down from the wellhead to the meter. Meter runs will be housed and/or fenced.

The gas meter will be calibrated and the tank strapped in place prior to any deliveries. Tests for the meter accuracy will be conducted monthly for the first three months on new meter installations and at least quarterly thereafter. The authorized officer will be provided with a date and time for the initial meter calibration and all future meter proving schedules. A copy of the meter calibration report will be submitted to the Moab field office. All measurement facilities will conform to API and AGA standards for gas and liquid hydrocarbon measurement.

**5. Location and Type of Water Supply**

Bill Barrett Corporation will utilize an existing water well located on BLM lands in the SW/4 SE/4 of Section 13-T12S-R14E. Bill Barrett Corporation has been granted this authorization by the State of Utah Application Number 90-1826 (T74077) on August 20, 2002.

**6. Source of Construction Materials**

All construction material for this location site and access road shall be borrow material accumulated during construction of the location site and access road. Additional gravel or pit lining material will be obtained from private sources.

## 7. Methods for Handling Waste Disposal

A) Pit construction and liners:

The reserve pit will be approximately 8 feet deep and at least one-half of the depth shall be below the surface of the existing ground.

The reserve pit will be lined with a 16 mil pit liner with felt underneath where necessary. The pit liner will be torn and perforated after the pit dries and before backfilling the reserve pit. The reserve pit will be reasonably free of hydrocarbons before the pit is backfilled.

B) Produced Fluids:

Produced water will be confined to the reserve pit, or if deemed necessary, a storage tank for a period not to exceed 90 days after initial production. Thereafter, produced water will be trucked to R & I Disposal, a State approved disposal facility.

C) Garbage:

A trash cage, fabricated from expanded metal, will be used to hold trash on location and will be removed to an authorized landfill location.

D) A portable chemical toilet will be supplied for human waste.

E) Site clean-up:

After the rig is moved out, the area around the wellsite will be cleaned and all refuse removed.

## 8. Ancillary Facilities

There are no ancillary facilities planned for at this time and none are foreseen in the future.

**9. Wellsite Layout**

Location dimensions are as follows:

| | |
|---|---|
| A) PAD LENGTH | 325 FT |
| B) PAD WIDTH | 150 FT |
| C) PIT DEPTH | 8 FT |
| D) PIT LENGTH | 100 FT |
| E) PIT WIDTH | 75 FT |
| F) MAX CUT | 20.8 FT |
| G) MAX FILL | 10.5 FT |
| H) TOTAL CUT YARDS | 9,530 CU YDS |
| I) PIT LOCATION | WEST SIDE |
| J) TOP SOIL LOCATION | NORTH END & SOUTH END |
| K)ACCESS ROAD LOCATION | FROM THE SOUTH |
| L) FLARE PIT | WEST SIDE |

Please see the attached location diagram for additional details.

Prior to commencement of drilling operations, the reserve pit will be fenced on three (3) sides with four strand barbed wire held in place by metal side posts and wooden corner "H" braces in order to protect livestock and wildlife.

A) Corner posts shall be braced in such a manner as to keep the fence tight at all times.

B) Standard steel, wood or pipe posts shall be used between the corner braces. Distance between any two posts shall be no greater than 16 ft.

C) All wire shall be stretched, by using a stretching device, before it is attached to the corner posts.

D) The fourth ($4^{th}$) side of the reserve pit will be fenced immediately upon removal of the drilling rig and the fencing will be maintained until the pit is backfilled.

E) Any hydrocarbons on the pit will be removed immediately

**10. Plans for Restoration of the Surface**

Prior to the construction of the location, the top 6 inches of soil material will be stripped and stockpiled. This will amount to 1,090 cubic yards of material. Placement of the topsoil is noted on the attached location plat. When all drilling and completion activities have been completed, the unused portion of the location (the area outside the deadmen) will be recontoured and the topsoil spread over the area.

The dirt contractor will be provided with an approved copy of the surface use plan prior to construction activities.

Any drainage rerouted during the construction activities shall be restored to its original line of flow or as near as possible.

All disturbed areas will be recontoured to the approximate natural contours. Prior to backfilling the pit, the fences around the reserve pit will be removed. The pit liner will be cut off at the water or mud line and disposed of at an approved landfill site. The liner will also be torn and perforated after the pit dries and before backfilling of the reserve pit.

The reserve pit will be reclaimed within one (1) year of well completion. If the reserve pit has not dried sufficiently to allow backfilling, an extension on the time requirement for backfilling the pit will be requested. Once reclamation activities have begun, they shall be completed within 30 days.

After the reserve pit has been reclaimed, no depressions in the soil covering the reserve pit will be allowed. The objective is to keep seasonal rainfall and runoff from seeping into the soil used to cover the reserve pit. Diversion ditches and water bars will be used to divert runoff as needed.

When restoration activities have been completed, the location site and new access road cuts and shoulders shall be reseeded as recommended by the BLM. Prior to reseeding, all disturbed areas, including the old access road, will be scarified and left with a rough surface. Seeding will take place either during the fall (prior to ground frost) or spring (after frost leaves the ground) months.

Seed will be broadcast or drilled at the time specified by the BLM. If broadcast, a harrow or some other implement will be dragged over the seeded area to assure seed coverage and the seed mixture will be proportionately larger (double the pounds per acre).

At such time the well is plugged and abandoned, the operator will submit a surface reclamation plan to the Surface Management Agency for prescribed seed mixture and reseeding requirements.

**11. Surface Ownership:**

United States Government

**12. Other Information**

A) Vegetation:

The trees in the area are cedar and pinion. The vegetation coverage is intermittent. The majority of the existing understory vegetation is made up of rabbitbrush, sage, and bitter brush. Also found on the location is prickly pear and various grasses.

B) Dwellings:

There are no occupied dwellings, or other facilities within a one mile radius of this location.

C) Archaeology:

The location has been surveyed and is being recommended for clearance. No archaeological, historical, or cultural sites near the proposed site and access road will be directly impacted. A copy of the written archaeological report dated July 9, 2003 should be in your files.

If, during operations, any archaeological or historical sites, or any objects of antiquity (subject to the Antiquities Act of June 8, 1906) are discovered, all operations which would affect such sites are to be suspended and the discovery reported promptly to the surface management agency.

D) Water:

The nearest water would be in Stone Cabin Draw approximately one and one-half miles to the south.

E) Chemicals:

No pesticides, herbicides or other possible hazardous chemicals shall be used without prior application.

F) Notification:

BLM, Moab, Utah: (435-259-2100)
24 to 48 hours before construction of the location.
Also after site construction and before the rig moves in.

H) Flare Pit:

The flare pit will be located 15 feet from the reserve pit fence and 100 feet from the bore hole on the west side of the location, immediately above point C on the location layout plat. All fluids will be removed from the pit within 48 hours of occurrence.

I) Grazing Permittee:

George and Gloria Fasselin
P. O. Box 18
Wellington, Utah 84542
Home: 435-637-1708

**13. Lessees or Operators Representative and Certification**

A) Representative

| | |
|---|---|
| NAME: | Debra K. Stanberry |
| ADDRESS: | Bill Barrett Corporation<br>1099 18th Street, Suite 2300<br>Denver, Colorado 80201 |
| PHONE: | 303-312-8120 |

All lease and/or unit operations will be conducted in such a manner that full compliance is made with all applicable laws, regulations and onshore oil and gas orders. The operator is fully responsible for the actions of its contractors and subcontractors. A copy of these conditions will be furnished to the field representative to ensure compliance.

The drilling permit will be valid for a period of one year from the date of approval. After permit termination, a new application will be filed for approval for any future operations.

B) Certification:

I hereby certify that the statements made in this plan are, to the best of my knowledge and belief, true and correct; and that the work associated with the operations proposed herein will be performed by Bill Barrett Corporation and its contractors and subcontractors in conformity with this plan and the terms and conditions under which it is approved. This statement is subject to the provisions of 18 U.S.C. 1001 for the filing of a false statement.

DATE April 23, 2004

Debra K. Stanberry
Permit Specialist
Bill Barrett Corporation

003

**WORKSHEET**

**APPLICATION FOR PERMIT TO DRILL**

APD RECEIVED: 04/27/2004

API NO. ASSIGNED: 43-007-30953

WELL NAME: PRICKLY PEAR U FED 12-24

OPERATOR: BILL BARRETT CORP ( N2165 )

CONTACT: DEBRA STANBERRY

PHONE NUMBER: 303-312-8120

PROPOSED LOCATION:

SWSW 24 120S 140E

SURFACE: 1271 FSL 0483 FWL

BOTTOM: 1271 FSL 0483 FWL

CARBON

UNDESIGNATED ( 2 )

LEASE TYPE: 1 - Federal

LEASE NUMBER: UTU-77513

SURFACE OWNER: 1 - Federal

PROPOSED FORMATION: MVRD

COALBED METHANE WELL? NO

INSPECT LOCATN BY: / /

| Tech Review | Initials | Date |
|---|---|---|
| Engineering | | |
| Geology | | |
| Surface | | |

LATITUDE: 39.75456

LONGITUDE: 110.30360

RECEIVED AND/OR REVIEWED:

✓ Plat

✓ Bond: Fed[1] Ind[] Sta[] Fee[]
(No. WYB000040 )

N Potash (Y/N)

N Oil Shale 190-5 (B) or 190-3 or 190-13

✓ Water Permit
(No. 90-1826 )

N RDCC Review (Y/N)
(Date: )

N/A Fee Surf Agreement (Y/N)

LOCATION AND SITING:

___ R649-2-3.

Unit PRICKLY PEAR OK

___ R649-2-2. General

Siting: 460 From Qtr/Qtr & 920' Between Wells

✓ R649-3-3. Exception

___ Drilling Unit

Board Cause No:

Eff Date:

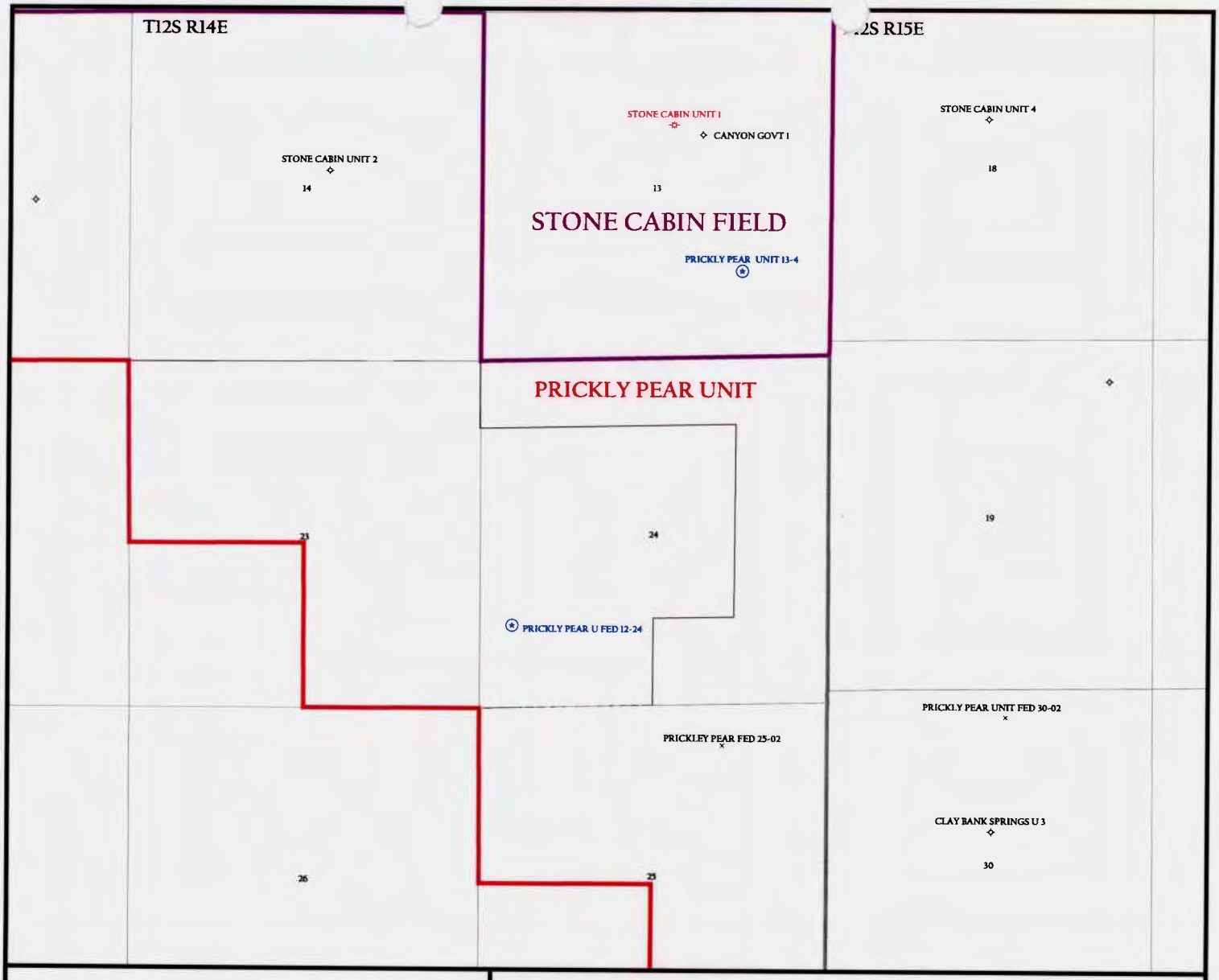
Siting:

___ R649-3-11. Directional Drill

COMMENTS:

STIPULATIONS: 1- Federal Approval

2- Spacing Stip




OPERATOR: BILL BARRETT CORP (N2165)

SEC. 24 T.12S, R.14E

FIELD: UNDESIGNATED (002)

COUNTY: CARBON

SPACING: R649-3-3 / EXCEPTION LOCATION

Utah Oil Gas and Mining

**Well Status**

- GAS INJECTION
- GAS STORAGE
- LOCATION ABANDONED
- NEW LOCATION
- PLUGGED & ABANDONED
- PRODUCING GAS
- PRODUCING OIL
- SHUT-IN GAS
- SHUT-IN OIL
- TEMP. ABANDONED
- TEST WELL
- WATER INJECTION
- WATER SUPPLY
- WATER DISPOSAL

**Unit Status**

- EXPLORATORY
- GAS STORAGE
- NF PP OIL
- NF SECONDARY
- PENDING
- PI OIL
- PP GAS
- PP GEOTHERML
- PP OIL
- SECONDARY
- TERMINATED

**Field Status**

- ABANDONED
- ACTIVE
- COMBINED
- INACTIVE
- PROPOSED
- STORAGE
- TERMINATED

N

W E

S

PREPARED BY: DIANA WHITNEY
DATE: 30-APRIL-2004

004

OLENE S. WALKER
*Governor*

GAYLE F. McKEACHNIE
*Lieutenant Governor*

State of Utah

Department of
Natural Resources

ROBERT L. MORGAN
*Executive Director*

Division of
Oil, Gas & Mining

LOWELL P. BRAXTON
*Division Director*

June 14. 2004

Bill Barrett Corporation
1099 18th Street, Suite 2300
Denver, CO 80202

Re: Prickly Pear Unit Federal 12-24 Well, 1271' FSL, 483' FWL, SW SW, Sec. 24, T. 12 South, R. 14 East, Carbon County, Utah

Gentlemen:

Pursuant to the provisions and requirements of Utah Code Ann.§ 40-6-1 *et seq.*, Utah Administrative Code R649-3-1 *et seq.*, and the attached Conditions of Approval, approval to drill the referenced well is granted.

Appropriate information has been submitted to DOGM and administrative approval of the requested exception location is hereby granted.

This approval shall expire one year from the above date unless substantial and continuous operation is underway, or a request for extension is made prior to the expiration date. The API identification number assigned to this well is 43-007-30953.

Sincerely,

John R. Baza
Associate Director

pab
Enclosures

cc: Carbon County Assessor
Bureau of Land Management, Moab District Office

**Operator:** Bill Barrett Corporation

**Well Name & Number** Prickly Pear Unit Federal 12-24

**API Number:** 43-007-30953

**Lease:** UTU-77513

**Location:** SW SW **Sec.** 24 **T.** 12 South **R.** 14 East

**Conditions of Approval**

1. General

   Compliance with the requirements of Utah Admin. R. 649-1 *et seq.*, the Oil and Gas Conservation General Rules, and the applicable terms and provisions of the approved Application for permit to drill.

2. Notification Requirements

   Notify the Division within 24 hours of spudding the well.

   - Contact Carol Daniels at (801) 538-5284.

   Notify the Division prior to commencing operations to plug and abandon the well.

   - Contact Dan Jarvis at (801) 538-5338

3. Reporting Requirements

   All required reports, forms and submittals will be promptly filed with the Division, including but not limited to the Entity Action Form (Form 6), Report of Water Encountered During Drilling (Form 7), Weekly Progress Reports for drilling and completion operations, and Sundry Notices and Reports on Wells requesting approval of change of plans or other operational actions.

4. State approval of this well does not supersede the required federal approval, which must be obtained prior to drilling.

5. This proposed well is located in an area for which drilling units (well spacing patterns) have not been established through an order of the Board of Oil, Gas and Mining (the "Board"). In order to avoid the possibility of waste or injury to correlative rights, the operator is requested, once the well has been drilled, completed, and has produced, to analyze geological and engineering data generated therefrom, as well as any similar data from surrounding areas if available. As soon as is practicable after completion of its analysis, and if the analysis suggests an area larger than the quarter-quarter section upon which the well is located is being drained, the operator is requested to seek an appropriate order from the Board establishing drilling and spacing units in conformance with such analysis by filing a Request for Agency Action with the Board.

RECEIVED
MOAB FIELD OFFICE

Form 3160-3
(April 2004)

FORM APPROVED
OMB No. 1004-0137
Expires March 31, 2007

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

005

# APPLICATION FOR PERMIT TO DRILL OR REENTER

2004 APR 27 A 9:36
DEPT OF THE INTERIOR
BUREAU OF LAND MGMT

5. Lease Serial No. **UTU 77513**

6. If Indian, Allotee or Tribe Name **n/a**

7. If Unit or CA Agreement, Name and No. **PRICKLY PEAR UNIT** UTU79487X

8. Lease Name and Well No. **Prickly Pear Unit Federal #12-24**

1a. Type of work: ☑ DRILL ☐ REENTER

1b. Type of Well: ☐ Oil Well ☑ Gas Well ☐ Other ☑ Single Zone ☐ Multiple Zone

9. API Well No. ~~pending~~ 4300730953

2. Name of Operator **BILL BARRETT CORPORATION**

3a. Address **1099 18th Street, Suite 2300 Denver CO 80202**

3b. Phone No. *(include area code)* **(303) 312-8120**

10. Field and Pool, or Exploratory **Prickly Pear Unit/Mesaverde**

4. Location of Well *(Report location clearly and in accordance with any State requirements.*)*
At surface **SW/4 SW/4 1271' FSL x 483' FWL**
At proposed prod. zone **same**

11. Sec., T. R. M. or Blk. and Survey or Area **Section 24-T12S-R14E S.L.B.&M.**

14. Distance in miles and direction from nearest town or post office* **67 miles northeast of Wellington, Utah**

12. County or Parish **Carbon**

13. State **UT**

| 15. Distance from proposed* location to nearest property or lease line, ft. (Also to nearest drig. unit line, if any) **483'** | 16. No. of acres in lease **640 acres** | 17. Spacing Unit dedicated to this well **160 acres** |
|---|---|---|
| 18. Distance from proposed location* to nearest well, drilling, completed, applied for, on this lease, ft. **n/a** | 19. Proposed Depth **10,000'** | 20. BLM/BIA Bond No. on file **Nationwide Bond #WYB000040** |
| 21. Elevations (Show whether DF, KDB, RT, GL, etc.) **7795' ungraded ground** | 22. Approximate date work will start* **06/20/2004** | 23. Estimated duration **60 days** |

24. Attachments

The following, completed in accordance with the requirements of Onshore Oil and Gas Order No.1, shall be attached to this form:

1. Well plat certified by a registered surveyor.
2. A Drilling Plan.
3. A Surface Use Plan (if the location is on National Forest System Lands, the SUPO shall be filed with the appropriate Forest Service Office).
4. Bond to cover the operations unless covered by an existing bond on file (see Item 20 above).
5. Operator certification
6. Such other site specific information and/or plans as may be required by the authorized officer.

| 25. Signature | Name *(Printed/Typed)* | Date |
|---|---|---|
| Title **Permit Specialist** | **Debra K. Stanberry** | **04/23/2004** |

| Approved by *(Signature)* /s/ Eric C. Jones | Name *(Printed/Typed)* | Date AUG 9 2004 |
|---|---|---|
| Title Acting Assistant Field Manager, Division of Resources | Office | |

Application approval does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.
Conditions of approval, if any, are attached.

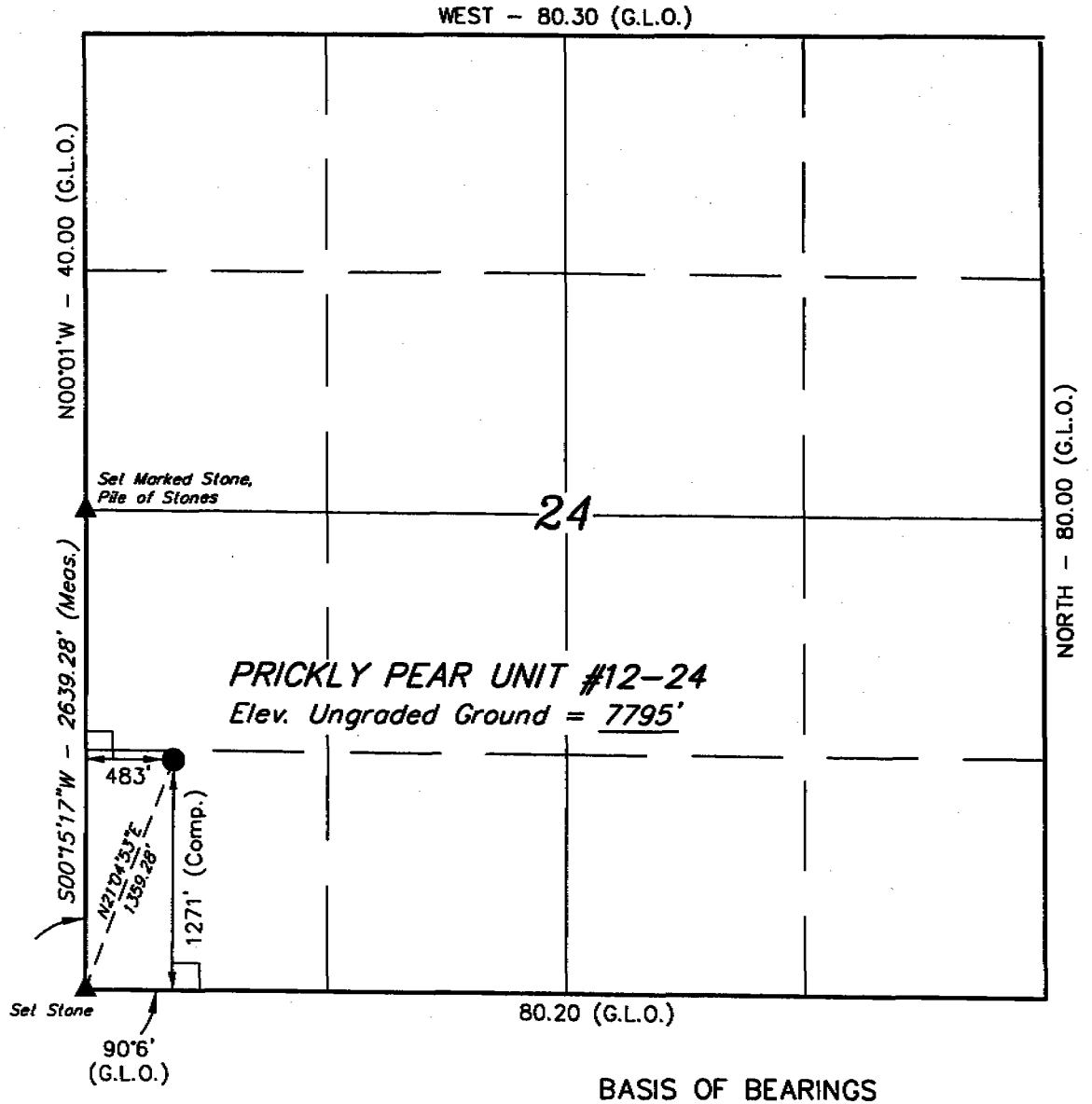
Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

**(Instructions on page 2)*

CONDITIONS OF APPROVAL ATTACHED

RECEIVED
AUG 12 2004
DIV. OF OIL, GAS & MINING

# T12S, R14E, S.L.B.&M.




## BASIS OF BEARINGS

BASIS OF BEARINGS IS A G.P.S. OBSERVATION.

(AUTONOMOUS NAD 83)
LATITUDE = 39°45'16.71" (39.754642)
LONGITUDE = 110°18'15.76" (110.304378)

LEGEND:

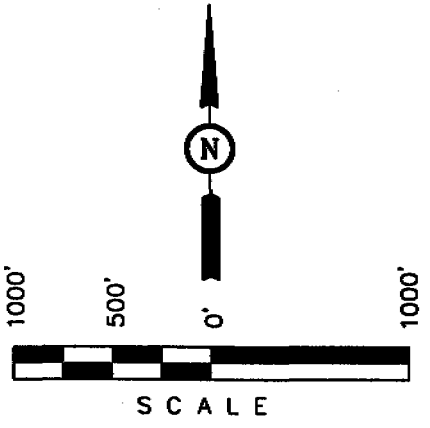
- └ = 90° SYMBOL
- ● = PROPOSED WELL HEAD.
- ▲ = SECTION CORNERS LOCATED.

## BILL BARRETT CORPORATION

Well location, PRICKLY PEAR UNIT #12-24, located as shown in the SW 1/4 SW 1/4 of Section 24, T12S, R14E, S.L.B.&M., Carbon County, Utah.

## BASIS OF ELEVATION

SPOT ELEVATION AT THE SOUTHWEST CORNER OF SECTION 7, T12S, R15E, S.L.B.&M. TAKEN FROM THE COWBOY BENCH QUADRANGLE, UTAH, 7.5 MINUTE QUAD. (TOPOGRAPHIC MAP) PUBLISHED BY THE UNITED STATES DEPARTMENT OF THE INTERIOR, GEOLOGICAL SURVEY. SAID ELEVATION IS MARKED AS BEING 7563 FEET.




## CERTIFICATE

THIS IS TO CERTIFY THAT THE ABOVE PLAT WAS PREPARED FROM FIELD NOTES OF ACTUAL SURVEYS MADE BY ME OR UNDER MY SUPERVISION AND THAT THE SAME ARE TRUE AND CORRECT TO THE BEST OF MY KNOWLEDGE AND BELIEF.

No. 161319
ROBERT L. KAY
REGISTERED LAND SURVEYOR
REGISTRATION NO. 161319
STATE OF UTAH

REVISED: 8-11-03


UINTAH ENGINEERING & LAND SURVEYING
85 SOUTH 200 EAST - VERNAL, UTAH 84078
(435) 789-1017


| SCALE | DATE SURVEYED: | DATE DRAWN: |
|---|---|---|
| 1" = 1000' | 6-19-03 | 6-24-03 |
| PARTY: B.B. J.W. C.G. | REFERENCES: G.L.O. PLAT | |
| WEATHER: WARM | FILE: BILL BARRETT CORPORATION | |

Bill Barrett Corporation
Prickly Pear Unit Federal 12-24
Lease UTU-77513
Prickly Pear Unit
SW/SW Sec. 24, T12S, R14E
Carbon County, Utah

**A COMPLETE COPY OF THIS PERMIT SHALL BE KEPT ON LOCATION from the beginning of site construction through well completion, and shall be available to contractors to ensure compliance.**

CONDITIONS OF APPROVAL

Approval of this application does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Be advised that Bill Barrett Corporation is considered to be the operator of the above well and is responsible under the terms and conditions of the lease for the operations conducted on the leased lands.

Bond coverage for this well is provided by UT1262 (Principal – Bill Barrett Corporation) via surety consent as provided for in 43 CFR 3104.2.

This office will hold the aforementioned operator and bond liable until the provisions of 43 CFR 3106.7-2 continuing responsibility are met.

This permit will be valid for a period of one year from the date of approval. After permit termination, a new application must be filed for approval.

All lease operations will be conducted in full compliance with applicable regulations (43 CFR 3100), Onshore Oil and Gas Orders, lease terms, notices to lessees, and the approved plan of operations. The operator is fully responsible for the actions of his subcontractors.

A. DRILLING PROGRAM

1. The proposed 3M BOP system (revised from the original proposal) is adequate for anticipated conditions. Installation, testing and operation of the system shall be in conformance with Onshore Oil and Gas Order No. 2.

2. Concurrent approval from the State of Utah, Division of Oil, Gas & Mining (DOGM) is required before conducting any surface disturbing activities.

3. Locally, the Green River Formation is known to contain oil, gas, oil shale and tar sand deposits. However, the lateral occurrence, distribution and grade of the oil shale and tar sand deposits are not well defined. The operator shall pay particular attention to this section, and shall attempt to identify and describe any of these resources that may be penetrated. The operator shall note the presence of these resources in drilling reports and Well Completion Report. All oil, gas, oil shale and tar sand resources shall be isolated behind cement.

4. In order to isolate and protect known hydrocarbon resources, production casing shall be cemented into place such that the top-of-cement is:

   1) not less than 300 feet above the top of the Wasatch Formation, and

   2) not less than 100 feet above the top of the highest hydrocarbon bearing zone that is not already isolated behind the surface casing.

5. A cement bond log (CBL) or other appropriate tool for determining top-of-cement, shall be run on the production casing string.

6. If logging reveals that the cementing objectives were not met, remedial cementing will be required.

## B. SURFACE USE

1. The following appendices are attached for your reference. They are to be followed as conditions of approval:

   SM-A, Seed Mixture for Berms, Topsoil Piles, Pad Margins
   SM-B, Seed Mixture for Final Reclamation (buried pipelines, abandoned pads, roads, etc.)
   TMC1, Browse Hand Planting Tubeling Mixtures
   Lease Stipulations, see attached Table 2.3 from EA for West Tavaputs Plateau Drilling Program.
   Applicant-committed environmental protection measures, see attached Appendix B

2. An archaeologist shall be present during construction and earth disturbing activities to monitor site 42Cb1927. The access route shall avoid site 42Cb1909.

3. The mud pit shall be lined with an impermeable liner. Fill from the pit shall be stockpiled within a drainage control berm along the edge of the pit and adjacent edge of the well pad.

4. Within six months of installation, surface structures shall be painted in the following flat, earth tone color: Olive Black (5WA20-6). This Fuller O'Brien color is for reference only. Any brand of paint may be used provided the colors match. Any facilities that must be painted to comply with OSHA standards are exempt.

5. In areas where the soil surface shows evidence of biological soil crusts, the top uppermost (1/4-inch) of undisturbed biological soils from adjacent an undisturbed area shall be randomly collected from small areas (approximately 12-inch squares) and cast over the reclaimed site immediately following final reclamation to the facilitate re-establishment of soil crusts. Such actions would mitigate impacts to soil crusts in the long-term, although short-term impacts would remain.

6. Where appropriate use brush-hog or similar equipment to minimize impact to vegetation and enhance re-growth and revegetation potential.

7. BBC shall provide the authorized officer with an annual report of water consumed for the entire field for drilling, completion, and dust-suppression

activities. This report shall detail the amounts used and the source of the water.

8. Feather edges of disturbed area by creating a vertical transition from taller to shorter vegetation along disturbed edges. Vary width of disturbance and preserve some plant masses to create a more naturally appearing edge and thereby avoid straight, sweeping, and converging lines in the landscape.

9. Reduce overall width of surface disturbance by working with equipment on the road, and taking advantage of the access already provided by the roadway.

10. BBC shall implement an effective revegetation plan, including installation of shrubs and tubelings, thus establishing larger caliper plants early.

11. Use rocks and downed vegetation to "break up" new textures created by disturbance and exposure of soils, and to provide "planting pockets" for the establishment of new plant materials.

12. At stream crossings keep all equipment away from edge of escarpments and stream banks thereby minimizing impacts to escarpment edge, and stabilize these edges pre-construction using vegetative or mechanical methods.

13. Refer to TMC1, Browse Hand Planting Tubeling Mixtures to easily establish fast-growing shrubs in seed mix and as tubelings.

14. To minimize the chance of undesirable plant species (especially seeds) from being carried into the WTPPA, equipment would be power-washed before being brought in.

15. Heavy equipment would not mobilize or demobilize through Nine Mile Canyon on weekends or holidays.

16. Recontour all disturbed surfaces to more natural-appearing landform, similar in topography to pre-disturbance and surrounding landscape. Prepare the soils for proper revegetation and implement best management practices for revegetation and erosion control.

17. No construction/drilling activities shall occur during the time of the year November 1 through May 15 for sage-grouse winter habitat.

18. Mule deer on critical winter ranges shall be protected by seasonal restrictions on construction from November 1 through May 15 where federal permits are required.

19. Elk on high priority and critical winter ranges would be protected by seasonal restrictions on construction from November 1 through May 15.

20. The Mexican Spotted Owl Conservation Measures to avoid impacts:
    a. Conduct annual surveys for nesting roosting habitat in areas proposed for construction activity within .5 miles of identified canyon habitat, based on the USFWS 2000, MSO habitat model.
    b. Upon discovery of individuals or sightings of this species, halt construction/drilling activities and notify the authorized official.

21. The Operator shall contact the authorized BLM official for an onsite prior to the placement of long-term structures occupying the pad longer than 6 months and higher than 14 feet above the original natural grade.

## GENERAL CONSTRUCTION

22. Operator shall contact the Price BLM Office at least forty-eight hours prior to the anticipated start of construction and/or any surface disturbing activities. The BLM may require and schedule a preconstruction conference with the operator prior to the operator commencing construction and/or surface disturbing activities. The operator and the operator's contractor, or agents involved with construction and/or any surface disturbing activities associated with the project, shall attend this conference to review the Conditions of Approval and plan of development. The operator's inspector will be designated at the pre-drill conference, and is to be given an approved copy of all maps, permits and conditions of approval before the start of construction. The BLM will also designate a representative for the project at the preconstruction conference.

23. The operator shall designate a representative(s) who shall have the authority to act upon and to implement instructions from the BLM. The operator's representative shall be available for communication with the BLM within a reasonable time when construction or other surface disturbing activities are underway.

24. Any archaeology/cultural resource discovered by the operator, or any person working on his behalf, on public land are to be immediately reported to the Price BLM Office. The operator will suspend all operations in the immediate area of such discovery until written authorization to proceed is issued by the Price BLM Office. An evaluation of the discovery will be made by the BLM to determine

appropriate actions to prevent the loss of significant cultural or scientific values. The operator is responsible for the cost of evaluation of any site found during construction. The BLM will determine what mitigation is necessary.

Any paleontology discovered by the operator, or any person working on his behalf, on public land is to be immediately reported to the Price BLM Office. The operator will suspend all operations in the immediate area of such discovery until written authorization to proceed is issued by the Price BLM Office. An evaluation of the discovery will be made by the BLM to determine appropriate actions to prevent the loss of significant cultural or scientific values. The operator is responsible for the cost of evaluation of any site found during construction. The BLM will determine what mitigation is necessary.

25. During project construction, surface disturbance and vehicle travel shall be limited to the approved location and access routes. Any additional area needed must be approved by the Price BLM Office prior to use.

26. The operator must provide a trash cage for the collection and containment of all trash. The trash shall be disposed in an authorized landfill. The location and access roads shall be kept litter free.

27. Vegetation removal necessitated by construction shall be confined to the limits of actual construction. Removed vegetation will be stockpiled for use in reclamation or removed from the construction site at the direction of the BLM.

28. Prior to surface disturbance, topsoil is to be separately removed and segregated from other material. Topsoil depth will be decided onsite by BLM. If the topsoil is less than 6 inches, a 6-inch layer that includes the A horizon and the unconsolidated material immediately below the A horizon shall be removed and the mixture segregated and redistributed as the surface soil layer.

Generally topsoil shall be stored within the pad site or adjacent to access roads. The company in consultation with BLM shall determine stockpile locations and dimensions at the onsite. If the topsoil stockpiles will not be redistributed for a period in excess of one (1) year, the stockpiles are to be seeded with seed mixture SM-A (attached).

## ROAD and PIPELINE CONSTRUCTION

29. Operator shall provide an inspector under the direction of a registered professional engineer (PE) at all times during road construction. A PE shall certify (statement with PE stamp) that the road was constructed to the required Bureau of Land Management (BLM) road standards.

30. Road construction or routine maintenance activities are to be performed during periods when the soil can adequately support construction equipment. If such equipment creates ruts more than 6 inches deep, the soil is deemed too wet to adequately support construction equipment. Whenever dust plumes exceed 200 feet the company shall water the road to abate the dust

31. The operator is responsible for maintenance of all roads authorized through the lease or a right-of-way. Construction and maintenance shall comply with Class II or III Road Standards as described in BLM Manual Section 9113 and the Moab District Road Standards, except as modified by BLM. Maintenance may include but is not limited to grading, applying gravel, snow removal, ditch cleaning, headcut restoration/prevention.

32. Topsoil from access roads and pipelines are to be wind rowed along the uphill side of the road or stored in an approved manner. When the road and pipeline is rehabilitated, this soil will then be used as a top coating for the seed bed.

33. Erosion-control structures such as water bars, diversion channels, and terraces will be constructed to divert water and reduce soil erosion on the disturbed area. Road ditch turnouts shall be equipped with energy dissipators as needed to avoid erosion. Where roads interrupt overland sheet-flow and convert this runoff to channel flow, ditch turnouts shall be designed to reconvert channel flow to sheet flow. Rock energy dissipators and gravel dispersion fans may be used or any other design which would accomplish the desired reconversion of flow regime. As necessary cut banks, road drainages, and road crossings shall be armored or otherwise engineered to prevent headcutting.

## PAD CONSTRUCTION

34. During the construction of the drill pad, suitable topsoil material is to be stripped and conserved in a stockpile on the pad. If stockpiles are to remain for more than a year, they shall be seeded with the seed mixture in appendix SM-A, attached.

35. Generally, drill pads are to be designed to prevent overland flow of water from entering or leaving the site. The pad is to be sloped to drain spills and water

into the reserve pit. The drill pad shall be designed to disperse diverted overland flow and to regulate flow velocity so as to prevent or minimize erosion. Well pad diversion outlets shall be equipped with rock energy and gravel-bedded dispersion fans.

36. In the event construction can't be completed prior to winter closures, measures to prevent erosion from upcoming spring snowmelt shall be taken as follows:

    a. Loose earth and debris will be removed from drainages, and flood plains.

    b. Earth and debris shall not be stockpiled on drainage banks.

    c. Road drainages shall be checked to ensure there are none with uncontrolled outlets.

        1. Be sure all ditch drainages have an outlet to prevent ponding.

        2. If necessary, build temporary sediment ponds to capture runoff from unreclaimed areas.

        3. Re-route ditches as needed to avoid channeling water through loosened soil.

37. Excess material from road blading must not be plowed into drainages. Remove excess material and deposit at approved locations.

## REHABILITATION PROCEDURES

### Site Preparation

38. The entire roadbed should be obliterated and brought back to the approximate original contour. Drainage control is to be reestablished as necessary. All areas affected by road construction are to be recontoured to blend in with the existing topography. All berms are to be removed unless determined to be beneficial by BLM. In recontouring the disturbed areas, care should be taken to not disturb additional vegetation.

### Seedbed Preparation

39. An adequate seedbed should be prepared for all sites to be seeded. Areas to be revegetated should be chiseled or disked to a depth of at least 12 inches unless restrained by bedrock.

40. Ripping of fill materials should be completed by a bulldozer equipped with single or a twin set of ripper shanks. Ripping should be done on 4-foot centers

to a depth of 12 inches. The process should be repeated until the compacted area is loose and friable, and then shall be followed by final grading. Seedbed preparation will be considered complete when the soil surface is completely roughened and the number of rocks (if present) on the site is sufficient to cause the site to match the surrounding terrain.

41. After final grading, the stockpiled topsoil shall be spread evenly across the disturbed area.

Fertilization

42. Commercial fertilizer with a formula of 16-16-8 is to be applied at a rate of 200 pounds per acre to the site. The rate may be adjusted depending on soil.

43. Fertilizer is to be applied not more than 48 hours before seeding, and shall be cultivated into the upper 3 inches of soil.

44. Fertilizer is to be broadcast over the soil using hand-operated "cyclone-type" seeders or rotary broadcast equipment attached to construction or revegetation machinery as appropriate to slope. All equipment should be equipped with a metering device. Fertilizer application is to take place before the final seeding preparation treatment. Fertilizer broadcasting operations should not be conducted when wind velocities would interfere with even distribution of the material.

Mulching

45. When it is time to reclaim this location, the Price BLM Office will determine whether it will be necessary to use mulch in the reclamation process. The type of mulch should meet the following requirements: Wood cellulose fiber shall be natural or cooked, shall disperse readily in water, and shall be nontoxic. Mulch shall be thermally produced and air dried. The homogeneous slurry or mixture shall be capable of application with power spray equipment. A colored dye that is noninjurious to plant growth may be used when specified. Wood cellulose fiber is to be packaged in new, labeled containers. A minimum application of 1500 pounds per acre shall be applied. A suitable tackifier shall be applied with the mulch at a rate of 60 to 80 pounds per acre.

An alternative method of mulching on small sites would be the application of straw or hay mulch at a rate of 2000 pounds per acre. Hay or straw shall be certified weed free. Following the application of straw or hay, crimping shall occur to ensure retention.

Reseeding

46. All disturbed areas are to be seeded with the seed mixture required by the BLM. The seed mixture(s) shall be planted in the fall of the year (Sept-Nov), in the amounts specified in pounds of pure live seed (PLS)/acre. If fall seeding is not feasible, the seed mixture(s) shall be planted April 30-May 31. There shall be no noxious weed seed in the seed mixture. Seed will be tested and the viability testing of seed shall be done in accordance with State law(s) and within 12 months prior to planting. Commercial seed will be either certified or registered seed. The seed mixture container shall be tagged in accordance with State law(s) and available for inspection by the BLM. Seed is to be planted using a drill equipped with a depth regulator to ensure proper depth of planting where drilling is possible. The seed mixture shall be evenly and uniformly planted over the disturbed area. (Smaller/heavier seeds tend to drop to the bottom of the drill and are planted first. Appropriate measures should be taken to ensure this does not occur.) Where drilling is not possible, seed is to be broadcast and the area raked or chained to cover the seed. Woody species with seeds that are too large for the drill will be broadcast. When broadcasting the seed, the pounds per acre noted below are to be increased by 50 percent.

    Reseeding may be required if a satisfactory stand is not established to the surface rights owner's specifications. Evaluation of the seeding's success will not be made before completion of the second growing season after the vegetation becomes established. The Price BLM Office is to be notified a minimum of seven days before seeding a project.

47. The disturbed areas for the road and pipeline must be seeded in the fall of the year, immediately after the topsoil is replaced. The prescribed seed mixture is attached as appendix SM-B.

General

48. Prior to the use of insecticides, herbicides, fungicides, rodenticides and other similar substances, the operator must obtain from BLM, approval of a written plan. The plan must describe the type and quantity of material to be used, the pest to be controlled, the method of application, the location for storage and disposal of containers, and other information that BLM may require. A pesticide may be used only in accordance with its registered uses and within other agency limitations. Pesticides must not be permanently stored on public lands.

**Seed Mix A**[1]

Temporary Disturbance

(for berms, topsoil piles, pad margins)

| **Forbes** | **Lbs** |
|---|---|
| Yellow Sweetclover | 2.0 lbs/acre |
| Ladak Alfalfa | 2.0 lbs/acre |
| Cicer Milkvetch | 1.0 lbs/acre |
| Palmer Penstemon | 0.5 lbs/acre |

| **Grasses** | **Lbs** |
|---|---|
| Crested Wheatgrass | 2.0 lbs/acre |
| Great Basin Wildrye | 2.0 lbs/acre |
| Intermediate Wheatgrass | 2.0 lbs/acre |

**Total** 11.5 lbs/acre

1 Seed mix A is designed for rapid establishment, soil holding ability, and nitrogen fixing capability.



**Seed Mix B**

Final Reclamation

(for buried pipe lines, abandoned pads, road, etc.)

| **Forbes** | **Lbs** |
|---|---|
| Palmer Penstemon | 0.5 lbs/acre |
| Golden Cryptantha | 0.25 lbs/acre |
| Utah Sweetvetch | 0.5 lbs/acre |
| Yellow Sweetclover[1] | 2.0 lbs/acre |
| Lewis Flax | 1.0 lbs/acre |

| **Grasses** | **Lbs** |
|---|---|
| Indian Ricegrass | 1.0 lbs/acre |
| Needle & Thread Grass | 1.0 lbs/acre |
| Intermediate Wheatgrass | 2.0 lbs/acre |
| Blue Grama | 0.5 lbs/acre |
| Galletta | 0.5 lbs/acre |
| Great Basin Wildrye | 2.0 lbs/acre |

| **Woody Plants** | **Lbs** |
|---|---|
| Fourwing Saltbush | 2.0 lbs/acre |
| Winterfat | 0.5 lbs/acre |
| Wyoming Big Sage brush | 0.25 lbs/acre |
| Utah Serviceberry | 1.0 lbs/acre |
| Blue Elderberry (Raw Seeds) | 1.0 lbs/acre |

**Total** 16.0 lbs/acre

1 Yellow Sweetclover is planted as a nurse crop to provide solar protection, soil binding and nitrogen fixing. It will normally be crowded out in 2 to 3 years.

**APPENDIX B:**

APPLICANT-COMMITTED ENVIRONMENTAL PROTECTION MEASURES

## 1.0 INTRODUCTION

Appendix B is part of BBC's Proposed Action for the WTPDP as described in Chapter 2.0, and BBC will comply with the standards, procedures, and requirements contained in Appendix B when implementing the Alternatives unless otherwise provided for by the BLM Authorized Officer (AO). Appendix B describes standard practices utilized to mitigate adverse effects caused by surface-disturbing activities.

## 2.0 STANDARD PRACTICES

The following BMPs/Applicant-Committed Protection Measures (ACEPM) will be applied to all federal lands within the WTPPA by BBC to minimize impacts to the environment. Exception, modification, or waiver of a mitigation requirement may be granted if a thorough analysis by BLM determines that the resource(s) for which the measure was developed will not be impacted by the project activity. Further site-specific mitigation measures may be identified during the application for permit to drill (APD) and/or right-of-way (ROW) application review processes.

### 2.1 PRECONSTRUCTION PLANNING AND DESIGN MEASURES

1. BBC and/or their contractors and subcontractors will conduct all phases of project implementation, including well location, road and pipeline construction, drilling and completion operations, maintenance, reclamation, and abandonment in full compliance with all applicable federal, state, and local laws and regulations and within the guidelines specified in approved APDs and ROW permits. BBC will be held fully accountable for their contractor's and subcontractor's compliance with the requirements of the approved permit and/or plan.

2. Implementation of site-specific activities/actions will be contingent on BLM determining that the activity/action complies with the following plans:
   - Surface Use Plan and/or Plan of Development; and
   - Site-specific APD plans/reports (e.g., road and wellpad design plans, cultural clearance, special status plant species clearance, etc.).

   The above plans may be prepared by the Companies for the project area or submitted incrementally with each APD, ROW application, or Sundry Notice (SN).

### 2.2 ROADS

1. BBC will construct roads on private surface in a safe and prudent manner to the specifications of landowners.

2. Roads on federal surface will be constructed as described in BLM Manual 9113. Where necessary, running surfaces of the roads will be graveled if the base does not already contain sufficient aggregate.

3. Existing roads will be used when the alignment is acceptable for the proposed use. Generally, roads will be required to follow natural contours; provide visual screening by constructing curves, etc.; and be reclaimed to BLM standards.

4. To control or reduce sediment from roads, guidance involving proper road placement and buffer strips to stream channels, graveling, proper drainage, seasonal closure, and in some cases, redesign or closure of old roads will be developed when necessary. Construction may also be prohibited during periods when soil material is saturated, frozen, or when watershed damage is likely to occur.

5. Available topsoil will be stripped from all road corridors prior to commencement of construction activities and will be redistributed and reseeded on backslope areas of the borrow ditch after completion of road construction activities. Borrow ditches will be reseeded in the first appropriate season after initial disturbance.

6. On newly constructed roads and permanent roads, the placement of topsoil, seeding, and stabilization will be required on all cut and fill slopes unless conditions prohibit this (e.g., rock). No unnecessary side-casting of material (e.g., maintenance) on steep slopes will be allowed.

7. Reclamation of abandoned roads will include requirements for reshaping, recontouring, resurfacing with topsoil, installation of water bars, and seeding on the contour. Road beds, wellpads, and other compacted areas will be ripped to a depth of 1.0 foot on 1.5 feet centers to reduce compaction prior to spreading the topsoil across the disturbed area. Stripped vegetation will be spread over the disturbance for nutrient recycling, where practical. Fertilization or fencing of these disturbances will not normally be required. Additional erosion control measures (e.g., fiber matting) and road barriers to discourage travel may be required. Graveled roads, wellpads, and other sites will be stripped of usable gravel and hauled to new construction sites prior to ripping as deemed necessary by the AO. The removal of structures such as bridges, culverts, cattleguards, and signs will usually be required.

8. Main artery roads, regardless of the primary user, will be crowned, ditched, drained, and, if deemed appropriate by the AO, surfaced with gravel.

9. Unnecessary topographic alterations will be mitigated by avoiding, where possible, steep slopes, rugged topography, and perennial and ephemeral/intermittent drainages, and by minimizing the area disturbed.

10. Upon completion of construction and/or production activities, the Companies will restore, to the extent practicable, the topography to near pre-existing contours at well sites, access roads, pipelines, and other facility sites.

11. Existing roads will be used to the maximum extent possible and upgraded as necessary.

12. BBC will comply with existing federal, state, and county requirements and restrictions to protect road networks and the traveling public.

13. Special arrangements will be made with the Utah Department of Transportation to transport oversize loads to the project area. Otherwise, load limits will be observed at all times to prevent damage to existing road surfaces.

14. All development activities along approved ROWs will be restricted to areas authorized in the approved ROW.

15. Roads and pipelines will be located adjacent to existing linear facilities wherever practical.

16. BBC and/or their contractors will post appropriate warning signs and require project vehicles to adhere to appropriate speed limits on project-required roads, as deemed necessary by the AO.

16. BBC will be responsible for necessary preventative and corrective road maintenance for the duration of the project. Maintenance responsibilities may include, but are not limited to, blading, gravel surfacing, cleaning ditches and drainage facilities, dust abatement, noxious weed control, or other requirements as directed by the AO.

## 2.3 WELLPADS AND FACILITIES

1. In conformance with Onshore Oil and Gas Order No. 1, BBC will prepare and submit individual comprehensive drill site design plans for BLM approval. These plans will show the drill location layout over the existing topography; dimensions of the location; volumes and cross sections of cut and fill; location and dimensions of reserve pits; existing drainage patterns; and access road egress and ingress. Plans will be submitted and approved prior to initiation of construction.

2. No surface disturbance is recommended on slopes in excess of 25% unless erosion controls can be ensured and adequate revegetation is expected. Engineering proposals and revegetation and restoration plans will be required in these areas.

3. Reserve pits will be constructed to ensure protection of surface and ground water. The review to determine the need for installation of lining material will be done on a case-by-case basis and consider soil permeability, water quality, and depth to ground water.

4. Reserve pit liners will have a mullen burst strength that is equal to or exceeds 300 pounds, a puncture strength that is equal to or exceeds 160 pounds, and grab tensile strengths that are equal to or exceed 150 pounds. There will be verified test results conducted according to ASTM test standards. The liner will be totally resistant to deterioration by hydrocarbons.

5. Produced water from oil and gas operations will be disposed of in accordance with the requirements of Onshore Oil and Gas Order #7.

6. Pits will be fenced as specified in individual authorizations. Any pit containing harmful fluids will be maintained in a manner that will prevent migratory bird mortality.

7. Disturbances will be managed/reclaimed for zero runoff from the wellpad or other facility until the area is stabilized. All excavations and pits will be closed by backfilling and contouring to conform to surrounding terrain. On wellpads and other facilities, the surface use plan will include objectives for successful reclamation including soil stabilization, plant community composition, and desired vegetation density and diversity.

8. On producing wells, BBC will reduce slopes to original contours (not to exceed 3:1 slopes). Areas not used for production purposes will be backfilled and blended into the surrounding terrain, reseeded, and erosion control measures installed. Erosion control measures will be required after slope reduction. Mulching, erosion control measures, and fertilization may be required to achieve acceptable stabilization.

9. Abandoned sites will be satisfactorily rehabilitated in accordance with the approved APD.

## 2.4 PIPELINES

1. Pipeline construction methods and practices will be completed in such a manner so as to obtain good reclamation and the re-establishment of the native plant community.

2. On ditches exceeding 24 inches in width, 6 to 12 inches of surface soil will be salvaged on the entire right-of-way, where practicable. When pipelines are buried, there will be at least 30 inches of backfill on top of the pipe. Backfill will not extend above the original ground level after the fill has settled. Guides for construction and water bar placement found in "Surface Operating Standards for Oil and

Gas Exploration and Development" (BLM and USFS 1989) will be followed. Bladed surface materials will be re-spread upon the cleared route once construction is completed. Disturbed areas that have been reclaimed will be fenced when the route is near livestock watering areas at the discretion of the AO.

3. Pipeline ROWs will be located to minimize soil disturbance to the greatest extent practicable. Mitigation will include locating pipeline ROWs adjacent to access roads to minimize ROW disturbance widths, or routing pipeline ROWs directly to minimize disturbance lengths.

4. Existing crowned and ditched roads will be used for access where possible to minimize surface disturbances. Clearing of pipeline ROWs will be accomplished with the least degree of disturbance to topsoil. Where topsoil removal is necessary, it will be stockpiled (windrowed) and re-spread over the disturbed area after construction and backfilling are completed. Vegetation removed from the ROW will also be re-spread to provide protection, nutrient recycling, and a seed source.

5. Temporary disturbances which do not require major excavation (e.g., small pipelines) may be stripped of vegetation to ground level using mechanical treatment, leaving topsoil intact and root masses relatively undisturbed.

6. To promote soil stability, backfill over the trench will be compacted so as not to extend above the original ground level after the fill has settled. Wheel or other methods of compacting the pipeline trench backfill will occur at two levels to reduce trench settling and water channeling--once after 3 feet of fill has been replaced and once within 6-12 inches of the surface. Water bars, mulching, and terracing will be installed, as needed, to minimize erosion. Instream protection structures (e.g., drop structures) in drainages crossed by a pipeline will be installed at the discretion of the AO to prevent erosion.

7. BBC will adhere to the following procedures regarding the installation of pipelines during periods when the earth is frozen.
   - The BLM Price Field Office will be contacted at least 10 days prior to anticipated start of project. The project will not proceed until such time as authorization from BLM has been received by the Companies.
   - A BLM representative will be on the ground at the beginning of construction.
   - Snow, if present, will be removed utilizing a motor grader.
   - Vegetation will be scalped and windrowed to one side of the right-of-way.
   - A wheel trencher will be used to remove approximately 6-8 inches of topsoil from the top of the pipeline ditch and windrow it to one side.
   - A trench approximately 4 feet deep will be dug using a wheel trencher and the soil will be stockpiled to one side, making sure the top soil or spoil do not get mixed together.
   - The pipeline will be installed, the trench backfilled, and the spoil compacted in the trench.
   - Stockpiled topsoil will be placed in the trench and compacted.
   - Scalped vegetation back will be placed back on right-of-way using a motor grader.
   - The entire right-of-way will be reseeded as normal in the spring after the thaw.

   These procedures will be incorporated in every Plan of Development where construction in frozen earth is anticipated.

## 2.5 AIR QUALITY

1. BBC will comply with all applicable local, state, and federal air quality laws, statutes, regulations, standards, and implementation plans.

2. BBC will obtain all necessary air quality permits from UDAQ to construct, test, and operate facilities.

3. All internal combustion equipment will be kept in good working order.

4. The Companies will use water at construction sites, as necessary, to abate fugitive dust.

5. The Companies will not allow any open burning of garbage or refuse at well sites or other facilities.

## 2.6 VEGETATION

1. Removal and disturbance of vegetation will be kept to a minimum through construction site management (e.g., using previously disturbed areas and existing easements, limiting equipment/materials storage yard and staging area size, etc.).

2. Wellpads and associated roads and pipelines will be located to avoid or minimize impacts in areas of high value (e.g., sensitive species habitats, wetland/riparian areas).

## 2.7 SOILS

1. Surface-disturbing activities will be examined on a site-specific basis, evaluating the potential for soil loss and the compatibility of soil properties with project design. Stipulations and mitigating measures will be developed on a case-by-case basis to ensure soil conservation and practical management.

2. BBC will restrict construction activities during periods when soils are saturated and excessive rutting (>4 inches with multiple passes) would occur.

3. Salvage and subsequent replacement of topsoil will occur for surface-disturbing activities wherever specified by the AO.

4. Before a surface-disturbing activity is undertaken, topsoil depth will be determined and the amount of topsoil to be removed, along with topsoil placement areas, will be specified in the authorization. The uniform distribution of topsoil over the area to be reclaimed will occur unless conditions warrant a varying depth. On large surface-disturbing projects topsoil will be stockpiled and seeded to reduce erosion. Where feasible, topsoil stockpiles will be designed to maximize surface area to reduce impacts to soil microorganisms. Areas used for spoil storage will be stripped of topsoil before spoil placement, and the replacement of topsoil after spoil removal will be required.

5. BBC will avoid adverse impacts to soils by:
   - minimizing the area of disturbance;
   - avoiding construction with frozen soil materials to the extent practicable;
   - avoiding areas with high erosion potential (e.g., unstable soil, dunal areas, slopes greater than 25%, floodplains), where practicable;
   - salvaging and selectively handling topsoil from disturbed areas;
   - adequately protecting stockpiled topsoil and replacing it on the surface during reclamation;
   - leaving the soil intact (scalping only) during pipeline construction, where practicable;

- using appropriate erosion and sedimentation control techniques including, but not limited to, diversion terraces, riprap, and matting;
- promptly revegetating disturbed areas using adapted species;
- applying temporary erosion control measures such as temporary vegetation cover, application of mulch, netting, or soil stabilizers; and/or
- constructing barriers, as appropriate, to minimize wind and water erosion and sedimentation prior to vegetation establishment.

6. Appropriate erosion control and revegetation measures will be employed. Grading and landscaping will be used to minimize slopes, and water bars will be installed on disturbed slopes in areas with unstable soils where seeding alone may not adequately control erosion. Erosion control efforts will be monitored by the Companies and necessary modifications made to control erosion.

7. Sufficient topsoil or other suitable material to facilitate revegetation will be segregated from subsoils during all construction operations requiring excavation and will be returned to the surface upon completion of operations. Soils compacted during construction will be ripped and tilled as necessary prior to reseeding. Cut and fill sections on all roads and along pipelines will be revegetated with native species.

8. Any accidental soil contamination by spills of petroleum products or other hazardous materials will be cleaned up by the Companies and the soil disposed of or rehabilitated according to applicable rules.

9. BBC will restrict off-road vehicle (ORV) activity by employees and contract workers to the immediate area of authorized activity or existing roads and trails.

## 2.8 RECLAMATION

1. BBC's reclamation goals will emphasize: 1) protection of existing native vegetation; 2) minimal disturbance of the existing environment; 3) soil stabilization through establishment of ground cover; and 4) establishment of native vegetation consistent with land use planning.

2. All reclamation will be accomplished as soon as possible after the disturbance occurs with efforts continuing until a satisfactory revegetation cover is established.

3. Seed mixtures for reclaimed areas will be site-specific, composed of native species, and will include species promoting soil stability. A pre-disturbance species composition list will be developed if the site includes several different plant communities. Livestock palatability and wildlife habitat needs will be given consideration during seed mix formulation. BLM Manual 1745, *Introduction, Transplant, Augmentation, and Reestablishment of Fish, Wildlife, and Plants*, and Executive Order No. 11987, *Exotic Organisms*, will be used as guidance.
4. Interseeding, secondary seeding, or staggered seeding may be used to accomplish revegetation objectives. During rehabilitation of areas in important wildlife habitat, provision will be made for the establishment of native browse and forb species. Follow-up seeding or corrective erosion control measures will occur on areas where initial reclamation efforts are unsuccessful.

5. Any mulch used by BBC will be weed free and free from mold, fungi, or noxious weed seeds. Mulch may include native hay, small grain straw, wood fiber, live mulch, cotton, jute, synthetic netting, and rock. Straw mulch will contain fibers long enough to facilitate crimping and provide the greatest cover.

6. BBC will be responsible for the control of all noxious weed infestations on disturbed surfaces. Aerial application of chemicals will be prohibited within 0.25 mile of special status plant locations, and hand application will be prohibited within 500 feet. Herbicide application will be monitored by the AO.

7. Recontouring and seedbed preparation will occur immediately prior to reseeding on the unused portion of wellpads, road ROWs, and entire pipeline ROWs outside of road ROWs. In the event of uneconomical wells, BBC will initiate reclamation of the entire wellpads, access road, and adjacent disturbed habitat as soon as possible. BBC assumes the responsibility to see that their exploration, development, production, and construction operations are conducted in a manner which results in the proper reclamation of disturbed lands. BBC will monitor reclamation to determine and ensure successful establishment of vegetation. No consent to termination of any bond will be given by the AO until all the terms and conditions of the approved permit(s) have been met.

8. Proper erosion and sediment control structures and techniques will be incorporated by the Companies into the design of wellpads, roads, pipelines, and other facilities. Revegetation using a BLM-approved, locally adapted seed mixture containing native grasses, forbs, and shrubs will begin in the first appropriate season following disturbance. Vegetation removed will be replaced with plants of equal forage value and growth form using procedures that include:
   - fall reseeding (September 15 to freeze-up), where feasible;
   - spring reseeding (April 30 - May 31) if fall seeding is not feasible;
   - deep ripping of compacted soils prior to reseeding;
   - surface pitting/roughening prior to reseeding;
   - utilization of native cool season grasses, forbs, and shrubs in the seed mix;
   - interseeding shrubs into an established stand of grasses and forbs at least one year after seeding;
   - appropriate, approved weed control techniques;
   - broadcast or drill seeding, depending on site conditions; and
   - fencing of certain sensitive reclamation sites (e.g., riparian areas, steep slopes, and areas within 0.5 mile of livestock watering facilities) as determined necessary through monitoring.

9. BBC will monitor noxious weed occurrence on the project area and implement a noxious weed control program in cooperation with BLM. Weed-free certification by county extension agents will be required for grain or straw used for mulching revegetated areas.

## 2.9 CANDIDATE PLANTS/SPECIAL STATUS PLANTS

1. Herbicide applications will be kept at least 500 feet from known special status plant species populations or other distances deemed safe by the AO.

2. Wellpads and associated roads and pipelines will be located to avoid or minimize impacts to areas of high value (e.g., special status plant species habitats, wetland/riparian areas).

## 2.10 WATERSHEDS

1. Crossings of ephemeral, intermittent, and perennial streams associated with road and utility line construction will generally be restricted until normal flows are established after spring runoff.

## 2.11 GEOLOGICAL/PALEONTOLOGICAL RESOURCES

1. Wells, pipelines, and ancillary facilities will be designed and constructed such that they will not be damaged by moderate earthquakes. Any facilities defined as critical according to the Uniform Building Code will be constructed in accordance with applicable Uniform Building Code Standards for Seismic Risk Zone 2B.

2. If paleontological resources are uncovered during surface-disturbing activities, BBC will suspend operations at the site that will further disturb such materials and immediately contact the AO, who will arrange for a determination of significance, and, if necessary, recommend a recovery or avoidance plan.

## 2.12 CULTURAL/HISTORICAL RESOURCES

1. BBC will follow the cultural resources and recovery plan for the project.

2. If cultural resources are located within frozen soils or sediments that preclude the possibility of adequately recording or evaluating the find, construction work will cease and the site will be protected for the duration of frozen soil conditions. Recordation, evaluation and recommendations concerning further management will be made to the AO following natural thaw. The AO will consult with the affected parties and construction work will resume once management of the threatened site has been finalized and the Notice to Proceed has been issued.

3. BBC will inform their employees, contractors and subcontractors about relevant federal regulations intended to protect archaeological and cultural resources. All personnel will be informed that collecting artifacts, including arrowheads, is a violation of federal law and that employees engaged in this activity may be subject to disciplinary action.

## 2.13 WATER RESOURCES

1. BBC will maintain a complete copy of the SPCC Plan at each facility if the facility is normally attended at least 8 hours per day, or at the nearest field office if the facility is not so attended (40 CFR 112.3(e)).

2. BBC will implement and adhere to SPCC Plans in a manner such that any spill or accidental discharge of oil will be remediated. An orientation will be conducted by the Companies to ensure that project personnel are aware of the potential impacts that can result from accidental spills, as well as the appropriate recourse if a spill does occur. Where applicable and/or required by law, streams at pipeline crossings will be protected from contamination by pipeline shutoff valves or other systems capable of minimizing accidental discharge.

3. If reserve pit leakage is detected, operations at the site will be curtailed, as directed by the BLM, until the leakage is corrected.

4. BBC will case and cement all gas wells to protect subsurface mineral and freshwater zones. Unproductive wells and wells that have completed their intended purpose will be properly abandoned and plugged using procedures identified by BLM (federal mineral estate) and/or WOGCC (state and fee mineral estate).

5. All water used in association with this project will be obtained from sources previously approved by the Utah State Engineer's Office.

6. Erosion-prone or high salinity areas will be avoided where practicable. Necessary construction in these areas will be timed to avoid periods of greatest runoff.

7. BBC will incorporate proper containment of condensate and produced water in tanks and drilling fluids in reserve pits, and will locate staging areas for storage of equipment away from drainages to prevent contaminants from entering surface waters.

8. Prudent use of erosion control measures, including diversion terraces, riprap, matting, temporary sediment traps, and water bars will be employed by the Companies as necessary. These erosion control measures will be used as appropriate to control surface runoff generated at wellpads. The type and location of sediment control structures, including construction methods, will be described in APD and ROW plans. If necessary, BBC may treat diverted water in detention ponds prior to release to meet applicable state or federal standards.

9. BBC will construct channel crossings by pipelines so that the pipe is buried at least 3 feet below the channel bottom.

10. Streams/channels crossed by roads will have culverts installed at all appropriate locations as specified in the BLM Manual 9112-*Bridges and Major Culverts* and Manual 9113-*Roads*. Streams will be crossed perpendicular to flow, where possible, and all stream crossing structures will be designed to carry the 25-year discharge event or other capacities as directed by the AO.

11. BBC will reshape disturbed channel beds to their approximate original configuration.

12. The disposal of all hydrostatic test water will be done in conformance with BLM Onshore Oil and Gas Order No. 7. BBC will comply with state and federal regulations for water discharged into an established drainage channel. The rate of discharge will not exceed the capacity of the channel to convey the increased flow. Waters that do not meet applicable state or federal standards will be evaporated, treated, or disposed of at an approved disposal facility.

13. BBC will prepare Storm Water Pollution Prevention Plans (SWPPPs) as required by WDEQ National Pollution Discharge Elimination System (NPDES) permit requirements on individual disturbances that exceed 5 acres in size or as required by future changes in regulations.

14. Any disturbances to wetlands and/or waters of the U.S. will be coordinated with the COE, and 404 permits will be secured as necessary prior to disturbance.

15. Where disturbance of wetlands, riparian areas, streams, or ephemeral/intermittent stream channels cannot be avoided, COE Section 404 permits will be obtained by BBC as required, and, in addition to applicable above-listed measures, the following measures will be applied where appropriate:
    - wetland areas will be crossed during dry conditions (i.e., late summer, fall, or dry winters);
    - streams, wetlands, and riparian areas disturbed during project construction will be restored to as near re-project conditions as practical and, if impermeable soils contributed to wetland formation, soils will be compacted to reestablish impermeability;
    - wetland topsoil will be selectively handled;
    - disturbed areas will be recontoured and BLM-approved species will be used for reclamation; and

- reclamation activities will begin on disturbed wetlands immediately after completion of project activities.

## 2.14 NOISE

1. All engines required for project activities will be properly muffled and maintained in accordance with state and federal laws.

## 2.15 WILDLIFE, FISHERIES, AND THREATENED AND ENDANGERED (T&E) SPECIES

1. To minimize wildlife mortality due to vehicle collisions, BBC will advise project personnel regarding appropriate speed limits in the project area. Roads no longer required for operations will be reclaimed as soon as possible. Potential increases in poaching will be minimized through employee and contractor education regarding wildlife laws. If wildlife law violations are discovered, the offending employee will be subject to disciplinary action by BBC.
2. BBC will protect (e.g., fence or net) reserve, workover, and production pits potentially hazardous to prohibit wildlife access as directed by BLM.
3. BBC will utilize wildlife-proof fencing on reclaimed areas in accordance with standards specified in BLM Handbook 1741-1, *Fencing*, if it is determined that wildlife are interfering with successful reestablishment of vegetation.
4. Consultation and coordination with USFWS and UDWR will be conducted for all mitigation activities relating to raptors and T&E species and their habitats, and all permits required for movement, removal, and/or establishment of raptor nests will be obtained.
5. BBC will adhere to all survey, mitigation, and monitoring requirements identified in the Biological Assessment prepared for this project.

## 2.16 LIVESTOCK/GRAZING MANAGEMENT

1. BBC will reclaim nonessential areas disturbed during construction activities in the first appropriate season after well completion.
2. Nonessential areas include portions of the wellpads not needed for production operations, the borrow ditch and outslope portions of new road ROWs, entire pipeline ROWs outside of road ROWs, and all roads and associated disturbed areas at nonproductive wells.
3. BBC will repair or replace fences, cattleguards, gates, drift fences, and natural barriers to current BLM standards. Cattleguards will be used instead of gates for livestock control on most road ROWs. Livestock will be protected from pipeline trenches, and livestock access to existing water sources will be maintained.
4. BBC will review livestock impacts from roads or disturbance from construction and drilling activities at least annually with livestock permittees and BLM. Appropriate measures will be taken to correct any adverse impacts, should they occur.

## 2.17 RECREATION

1. BBC will instruct employees, contractors, and subcontractors that camp sites on federal lands or at federal recreation sites must not be occupied for more than 14 consecutive days.

2. BBC will require that employees, contractors, and subcontractors abide by all state and federal laws and regulations regarding hunting.

## 2.18 VISUAL RESOURCES

1. Pipeline ROWs will be located within existing ROWs whenever possible, and aboveground facilities not requiring safety coloration will be painted with appropriate nonreflective standard environmental colors (Carlsbad Canyon or Desert Brown, or other specified standard environmental colors) as determined by the AO. Topographic screening, vegetation manipulation, project scheduling, and traffic control procedures may all be employed, as practicable, to further reduce visual impacts.

2. Within VRM Class II areas, BBC will utilize existing topography to screen roads, pipeline corridors, drill rigs, wells, and production facilities from view where practicable. The Companies will paint all aboveground production facilities with appropriate colors (e.g., Carlsbad Canyon or Desert Brown) to blend with adjacent terrain, except for structures that require safety coloration in accordance with OSHA requirements.

## 2.19 HEALTH AND SAFETY/HAZARDOUS MATERIALS

1. BBC will utilize BLM-approved portable sanitation facilities at drill sites; place warning signs near hazardous areas and along roadways; place dumpsters at each construction site to collect and store garbage and refuse; ensure that all refuse and garbage is transported to a State-approved sanitary landfill for disposal; and institute a Hazard Communication Program for its employees and require subcontractor programs in accordance with OSHA (29 CFR 1910.1200).

2. In accordance with 29 CFR 1910.1200, a Material Safety Data Sheet for every chemical or hazardous material brought on-site will be kept on file BBC's field offices.

3. Chemicals and hazardous materials will be inventoried and reported by BBC in accordance with the SARA Title III (40 CFR 335). If quantities exceeding 10,000 pounds or the threshold planning quantity are to be produced or stored, BBC will submit appropriate Section 311 and 312 forms at the required times to the State and County Emergency Management Coordinators and the local fire departments.

4. BBC will transport and/or dispose of any hazardous wastes, as defined by the Resource Conservation and Recovery Act of 1976 (RCRA), as amended, in accordance with all applicable federal, state, and local regulations.

5. BBC commits to the following practices regarding hazardous material containment.

    - All storage tank batteries that contain any oil, glycol, produced water, or other fluid which may constitute a hazard to public health or safety will be surrounded by a secondary means of containment for the entire contents of the largest single tank in use plus freeboard for precipitation, or to contain 110% of the capacity of the largest vessel. The appropriate containment and/or diversionary structures or equipment, including walls and floor, will contain

any oil, glycol or produced water and shall be constructed so that any discharge from a primary containment system, such as a tank or pipe, will not drain, infiltrate, or otherwise escape to ground or surface waters before cleanup is completed.

- Treaters, dehydrators and other production facilities that have the potential to leak or spill oil, glycol, produced water, or other fluid which may constitute a hazard to public health or safety, shall be placed on or within appropriate containment and/or diversionary structure to prevent spilled or leaking fluid from reaching ground or surface waters. The appropriate containment and/or diversionary structure will be sufficiently impervious to oil, glycol, produced water, or other fluid and will be installed so that any spill or leakage will not drain, infiltrate, or otherwise escape to ground or surface waters prior to completion of cleanup.

- Notice of any spill or leakage, as defined in BLM NTL 3A, will be immediately reported to the AO by the Companies as well as to such other federal and state officials as required by law. Oral notice will be given as soon as possible, but within no more than 24 hours, and those oral notices will be confirmed in writing within 72 hours of any such occurrence.

Table 2.3 Lease Numbers, Oil and Gas Units, Federal ROW Requirements, and Lease Stipulations for the 12 Vertical Federal Wells Proposed by BBC.

| Well Number/Location | Federal Lease Number and Stipulations | Unit Name | Federal ROW Needs |
|---|---|---|---|
| **Federal Wells** | | | |
| 7-25 | UTU-59970 | Prickly Pear Unit | Lower Flat Iron Road |
| 16-34 | UTU-73671 | Prickly Pear Unit | Lower Flat Iron Road |
| 27-3 | UTU-73670 [1,2,3] | Prickly Pear Unit | None |
| 21-2 | UTU-73670 [1,2,3] | Prickly Pear Unit | None |
| 13-4 | UTU-74385 | Prickly Pear Unit | None |
| 5-13 | UTU-73665 | Prickly Pear Unit | None |
| 24-12 | UTU-77513 [1,2,3] | Prickly Pear Unit | None |
| 10-4 | UTU-74386 [1,2,3,4] | Prickly Pear Unit | None |
| 15-19 | UTU-66801 [1,2,3] | Jack Canyon Unit | None |
| **Existing Pads** | | | |
| UT-10 | UTU-66801 [1,2,3] | Peters Point Unit | None |
| PPH-8 | UTU-66801 [1,2,3] | Peters Point Unit | None |
| PP-11 | UTU-66801 [1,2,3] | Peters Point Unit | None |
| **State Wells** | | | |
| Section 2, T13 S, R15E | NA | Prickly Pear Unit | Lower Flat Iron Road |
| Section 36, T12S, R15E | NA | Prickly Pear Unit | Lower Flat Iron Road |
| Section 32, T12S, R16E | NA | Prickly Pear Unit | Lower Flat Iron Road |
| Section 2, T13S, R16E | NA | None | Peters Point Road Extension |

1 No occupancy or other surface disturbance will be allowed within 330 feet of the centerline or within the 100 year recurrence interval floodplain, whichever is greater, of the perennial streams, or within 660 feet of springs, whether flowing or not. This distance may be modified when specifically approved in writing by the authorized officer of the Bureau of Land Management.

2 In order to minimize watershed damage, exploration drilling and other development activity will be allowed only during the period from May 1 to October 31. This limitation does not apply to maintenance and operation of producing wells. Exceptions to this limitation in any year may be specifically approved in writing by the authorized officer of the Bureau of Land Management.

3 Construction of access roads and drill pads on slopes in excess of 30 percent will require special design standards to minimize watershed damage. Drilling operations and any associated construction activities on slopes in excess of 50 percent may require directional drilling to prevent damage to the watershed. Exceptions to the limitations may be specifically approved in writing by the authorized officer of the Bureau of Land Management.

4 Raptor surveys will be required whenever surface disturbance and/or occupancy proposed in association with oil/gas exploration occur within a known nesting complex for raptors located in the NWNW Sec. 10. T12S, R14E. Field surveys will be conducted by the lessee/operator as determined by the authorized officer of the BLM. When surveys are required of the lessee/operator, the consultant hired must be found acceptable to the authorized officer prior to the field survey being conducted. Based on the result of the field survey, the authorized officer will determine appropriate buffer zones.

C. REQUIRED APPROVALS, REPORTS AND NOTIFICATIONS

Required verbal notifications are summarized in Table 1, attached.

Building Location- Contact the BLM Price Field Office, Natural Resource Protection Specialist at least 48-hours prior to commencing construction of location.

Spud- The spud date will be reported to BLM 24-hours prior to spudding. Written notification in the form of a Sundry Notice (Form 3160-5) will be submitted to the Moab Field Office within 24-hours after spudding, regardless of whether spud was made with a dry hole digger or big rig.

Daily Drilling Reports- Daily drilling reports shall detail the progress and status of the well and shall be submitted to the Moab Field Office on a weekly basis.

Monthly Reports of Operations- In accordance with Onshore Oil and Gas Order No. 1, this well shall be reported on Minerals Management Service (MMS) Form 3160, "Monthly Report of Operations," starting the month in which operations commence and continuing each month until the well is physically plugged and abandoned. This report will be filed directly with MMS.

Sundry Notices- There will be no deviation from the proposed drilling and/or workover program without prior approval. "Sundry Notices and Reports on Wells" (Form 3160-5) will be filed with the Moab Field Office for approval of all changes of plans and subsequent operations in accordance with 43 CFR 3162.3-2. Safe drilling and operating practices must be observed.

Drilling Suspensions- Operations authorized by this permit shall not be suspended for more than 30 days without prior approval of the Moab Field Office. All conditions of this approval shall be applicable during any operations conducted with a replacement rig.

Undesirable Events- Spills, blowouts, fires, leaks, accidents, or any other unusual occurrences shall be immediately reported to the BLM in accordance with requirements of NTL-3A.

Cultural Resources- If cultural resources are discovered during construction, work that might disturb the resources is to stop, and the Price Field Office is to be notified.

First Production- Should the well be successfully completed for production, the Moab Field Office will be notified when the well is placed in producing status. Such notification may be made by phone, but must be followed by a sundry notice or letter not later than five business days following the date on which the well is placed into production.

A first production conference will be scheduled as soon as the productivity of the well is apparent. This conference should be coordinated through the Moab Field Office. The Moab Field Office shall be notified prior to the first sale.

Well Completion Report- Whether the well is completed as a dry hole or as a producer, "Well Completion and Recompletion Report and Log" (Form 3160-4) will be submitted to the Moab Field Office not later than thirty-days after completion of the well or after completion of operations being performed, in accordance with 43 CFR 3162.4-1. Two copies of all logs, core descriptions, core analyses, well test data, geologic summaries, sample description, and all other surveys or data obtained and compiled during the drilling, workover, and/or completion operations, will be filed with Form 3160-4. When requested, samples (cuttings and/or samples) will be submitted to the Moab Field Office.

Venting/Flaring of Gas- Gas produced from this well may not be vented/flared beyond an initial, authorized test period of 30 days or 50 MMcf, whichever first occurs, without the prior, written approval of the Moab Field Office. Should gas be vented or flared without approval beyond the authorized test period, the well may be ordered shut-in until the gas can be captured or approval to continue the venting/flaring as uneconomic is granted. In such case, compensation to the lessor (BLM) shall be required for that portion of the gas that is vented/flared without approval and which is determined to have been avoidably lost.

Produced Water- An application for approval of a permanent disposal method and location will be submitted to the Moab Field Office for approval pursuant to Onshore Oil and Gas Order No.7.

Off-Lease Measurement, Storage, Commingling- Prior approval must be obtained from the Moab Field Office for off-lease measurement, off-lease storage and/or commingling (either down-hole or at the surface).

Plugging and Abandonment- If the well is completed as a dry hole, plugging instructions must be obtained from the Moab Field Office prior to initiating plugging operations.

A "Subsequent Report of Abandonment" (Form 3160-5) will be filed with the Moab Field Office within thirty-days following completion of the well for abandonment. This report will indicate where plugs were placed and the current status of surface restoration. Upon completion of approved plugging, a regulation marker will be erected in accordance with 43 CFR 3162.6. Final abandonment will not be approved until the surface reclamation work required by the approved APD or approved abandonment notice has been completed to the satisfaction of the Price Field Office or the appropriate surface managing agency.

TABLE 1

NOTIFICATIONS

Notify Don Stephens (435-636-3608) of the BLM Price Field Office for the following:

2 days prior to commencement of dirt work, construction and reclamation;

1 day prior to spudding;

50 feet prior to reaching the surface casing setting depth;

3 hours prior to testing BOP equipment.

If the person at the above number cannot be reached, notify the Moab Field Office at 435-259-2100. If unsuccessful, contact the person listed below.

Well abandonment operations require 24 hour advance notice and prior approval. In the case of newly drilled dry holes, verbal approval can be obtained by calling the Moab Field Office at 435-259-2100. If approval is needed after work hours, you may contact the following:

| | |
|---|---|
| Eric Jones, Petroleum Engineer | Office: 435-259-2117<br>Home: 435-259-2214 |

# DIVISION OF OIL, GAS AND MINING

## *SPUDDING INFORMATION*

Name of Company: **BILL BARRETT CORP**

Well Name: **PRICKLY PEAR U FED 12-24**

Api No: **43-007-30953** Lease Type: **FEDERAL**

Section **24** Township **12S** Range **14E** County **CARBON**

Drilling Contractor **[PATTERSON** RIG # **77**

## SPUDDED:

Date **08/23/04**

Time

How **DRY**

***Drilling will commence:***

Reported by **CHARLY HICKS**

Telephone # **1-435-790-5342**

**Date** **08/24/2004** **Signed** **CHD**

007

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 6

# ENTITY ACTION FORM

Operator: BILL BARRETT CORPORATION
Operator Account Number: N 2165
Address: 1099 18th Street, Suite 2300
city Denver
state CO zip 80202
Phone Number: (303) 312-8120

**Well 1**

| API Number | Well Name | | QQ | Sec | Twp | Rng | County |
|---|---|---|---|---|---|---|---|
| 4300730953 | PRICKLY PEAR UNIT FEDERAL 12-24 | | SWSW | 24 | 12S | 14E | CARBON |
| **Action Code** | **Current Entity Number** | **New Entity Number** | **Spud Date** | | | **Entity Assignment Effective Date** | |
| KB | 99999 | 13605 | 8/23/2004 | | | 8/30/04 | K |

Comments: MVRD

**Well 2**

| API Number | Well Name | | QQ | Sec | Twp | Rng | County |
|---|---|---|---|---|---|---|---|
| | | | | | | | |
| **Action Code** | **Current Entity Number** | **New Entity Number** | **Spud Date** | | | **Entity Assignment Effective Date** | |
| | | | | | | | |

Comments:

**Well 3**

| API Number | Well Name | | QQ | Sec | Twp | Rng | County |
|---|---|---|---|---|---|---|---|
| | | | | | | | |
| **Action Code** | **Current Entity Number** | **New Entity Number** | **Spud Date** | | | **Entity Assignment Effective Date** | |
| | | | | | | | |

Comments:

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**ACTION CODES:**

- **A** - Establish new entity for new well (single well only)
- **B** - Add new well to existing entity (group or unit well)
- **C** - Re-assign well from one existing entity to another existing entity
- **D** - Re-assign well from one existing entity to a new entity
- **E** - Other (Explain in 'comments' section)

TRACEY FALLANG
**Name (Please Print)**
Tracey Fallang
**Signature**
Permit Analyst
**Title**
8/26/2004
**Date**

(5/2000)

008

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 9

# SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

| | |
|---|---|
| 5. LEASE DESIGNATION AND SERIAL NUMBER: | UTU-77513 |
| 6. IF INDIAN, ALLOTTEE OR TRIBE NAME: | n/a |
| 7. UNIT or CA AGREEMENT NAME: | Prickly Pear Unit |
| 1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☑ OTHER | 8. WELL NAME and NUMBER: Prickly Pear Unit Federal 12-24 |
| 2. NAME OF OPERATOR: BILL BARRETT CORPORATION | 9. API NUMBER: 43-007-30953 |
| 3. ADDRESS OF OPERATOR: 1099 18TH St. Ste2300 CITY Denver STATE CO ZIP 80202 / PHONE NUMBER: (303) 312-8120 | 10. FIELD AND POOL, OR WILDCAT: Prickly Pear Unit/Mesa Verde |

4. LOCATION OF WELL

FOOTAGES AT SURFACE: 1271' FSL & 483' FWL — COUNTY: Carbon

QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E — STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☐ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☐ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☑ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☑ OTHER: Weekly Chronological Reports |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

WEEKLY DRILLING ACTIVITY REPORT FROM SEPTEMBER 1, 2004 THROUGH SEPTEMBER 3, 2004.

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NAME (PLEASE PRINT) Tracey Fallang — TITLE Permit Analyst

SIGNATURE Tracey Fallang — DATE 9/3/2004

(This space for State use only)

(5/2000) (See Instructions on Reverse Side)

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/3/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 3

Spud Date : 9/3/2004 Days From Spud : 0 Depth At 06:00 : 100

Morning Operations : SPUD @04:30 9-3-04 Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 2:00:00 AM | WAIT ON RIG LEVELING JACKS & PREPARE FOR SPUD |
| 4:30:00 AM | LEVEL RIG "RAISE DRILLER SIDE 4 INCHES |
| 6:00:00 AM | DRILLING FROM 40 TO 100 |

Remarks :

RIG LEVEL JACKS WERE NESSARY FOR OPERATION AS SUB HAD SETTELED 4" NOTIFY DON STEPHENS B.L.M. DENNIS INGRAM STATE TM CASERS HALCO CEMENTERS WELL HEAD INC BARROID MUD PASON LOGGERS QUICK TEST OF STATUS OF WELL

---

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/2/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 2

Spud Date : 9/3/2004 Days From Spud : 0 Depth At 06:00 : 40

Morning Operations : WAIT ON RIG LEVELING JACKS Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

NOTIFY DON STEPHENS B.L.M. , DENNIS INGRAM STATE OF UTAH OF CURRENT STATIS OF WELL 15:00 9/1/04 ORDER CLOSEST JACKS AVAILABLE FROM MERMAC IN CASPER WYO. 21:00 9-1-04 E.T.A. 15:00 9-2-04

---

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/1/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 1

Spud Date : 9/3/2004 Days From Spud : 0 Depth At 06:00 : 40

Morning Operations : MOVE RIG Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

MOVE 50% COMPLETED RIG UP 25% COMPLETED LEFT MESSAGE WITH CAROL, STATE OF UTAH AND DON STEPHENS, B.L.M. ON FRIDAY 8/26/04 ON UPCOMING RIG MOVE AND SPUD. CALLED AND HAD CONVERSATION WITH DENNIS INGRAM, STATE OF UTAH, DON STEPHENS B.L.M. ON PRESENT STATUS OF RIG OPERATION 15:00 9/1/04 ORDER 1000 FEET OF 9.625 SURFACE CASING FROM REYNOLDS ON 8/31/04

009

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 9

# SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

| | |
|---|---|
| 5. LEASE DESIGNATION AND SERIAL NUMBER: | UTU-77513 |
| 6. IF INDIAN, ALLOTTEE OR TRIBE NAME: | n/a |
| 7. UNIT or CA AGREEMENT NAME: | Prickly Pear Unit |
| 1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☑ OTHER | 8. WELL NAME and NUMBER: Prickly Pear Unit Federal 12-24 |
| 2. NAME OF OPERATOR: BILL BARRETT CORPORATION | 9. API NUMBER: 43-007-30953 |
| 3. ADDRESS OF OPERATOR: 1099 18TH St. Ste2300 CITY Denver STATE CO ZIP 80202 | PHONE NUMBER: (303) 312-8120 |
| | 10. FIELD AND POOL, OR WILDCAT: Prickly Pear Unit/Mesa Verde |

4. LOCATION OF WELL

FOOTAGES AT SURFACE: 1271' FSL & 483' FWL COUNTY: Carbon

QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☐ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☐ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☑ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☑ OTHER: Weekly Chronological Reports |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

WEEKLY DRILLING ACTIVITY REPORT FROM SEPTEMBER 4, 2004 THROUGH SEPTEMBER 9, 2004.

NAME (PLEASE PRINT) Tracey Fallang TITLE Permit Analyst

SIGNATURE Tracey Fallang DATE 9/9/2004

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(5/2000) (See Instructions on Reverse Side)

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/5/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 5

Spud Date : 9/3/2004 Days From Spud : 2 Depth At 06:00 : 1725

Morning Operations : DRILLING AHEAD Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

NOTIFY DON STEVENS BLM OF BOP TEST AND STATUS OF WELL. DRAG OUT OF LOCATION HALCO CEMENTERS, TM CASERS WITH D8 BLADE. AFTER DRAGING SERVICE COMPANYS IN FOR CASING JOB

---

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/4/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 4

Spud Date : 9/3/2004 Days From Spud : 1 Depth At 06:00 : 1005

Morning Operations : CIRC 9 5/8" CSG ON BOTTOM - HALLIBURTON STUCK IN ROAD Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

NOTIFY DON STEPHENS B.L.M.@ 1800 9-3-04
NOTIFY T.M. CASERS HALCO CEMMENTERS WELL HEAD INC QUICK TEST @ 2100 HOURS 9-3-04.
#DAYS SINCE LTA = 471
SAFETY MEETING W/ CSG CREWS.

RUN 23 JTS 9 5/8" CSG, J-55, 36#, ST&C, W/ OPEN GUIDE SHOE & POS FLOAT COLLAR, LAND AT 1002' KB.

SUPERVISOR: C. HICKS

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/9/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 9

Spud Date : 9/3/2004 Days From Spud : 6 Depth At 06:00 : 6125

Morning Operations : DRILLING AHEAD Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 7:30:00 AM | WASH AND REAM FROM 5365 TO 5443 NO FILL |
| 11:30:00 AM | DRILLING FROM 5443 TO 5588 |
| 12:00:00 PM | LUBRICATE RIG |
| 6:00:00 AM | DRILLING FROM 5443 TO 6125 |

Remarks :
DENNIS INGRAM STATE OF UTAH STOPPED BY RIG TO SEE STATUS OF WELL 12:00 9-8-04 HELD B.O.P. DRILL ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS WELL SECURED 2MIN 12SEC DAILY SAFTY MEETING CLEANING DAYS SINCE LOST TIME ACCIDENT 470

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Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/8/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 8

Spud Date : 9/3/2004 Days From Spud : 5 Depth At 06:00 : 5443

Morning Operations : RUN IN HOLE WITH BIT #3 Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :
DAYS SINCE LOST TIME ACCIDENT 469 DAILY SAFETY MEETING WORKING ON MUD PUMPS HELD B.O.P. DRILL ALL PERSONAL AT STATIONS FUNCTION PIPE RAMS WELL SECURED 2MIN. 46SEC FUNCTION BLIND RAMS WHILE ON BANK

---

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/7/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 7

Spud Date : 9/3/2004 Days From Spud : 4 Depth At 06:00 : 4750

Morning Operations : DRILLING AHEAD THOUGH WASATCH Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :
DAYS SINCE LOST TIME ACCIDENT 468 SAFETY MEETING FORK LIFT OPERATION B.O.P. DRILL WHILE DRILLING PERSONAL TO STATIONS AND WELL SECURED 2 MIN. 10 SEC.

---

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/6/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 6

Spud Date : 9/3/2004 Days From Spud : 3 Depth At 06:00 : 3525

Morning Operations : DRILLING AHEAD "WASATCH" Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :
HELD BOP DRILL WHILE DRILLING FUNCTION PIPE RAMS ALL PERSONAL TO STATIONS WELL SECURED 1 MIN. 45 SEC. EXPERANCED PARTIAL LOST CIRCULATION @ 2775 CALL PATTERSON DRILLING SPOKE WITH JESSE ASK FOR MATTING BOARDS ....DAYS SINCE LOST TIME ACCIDENT 467 DAILY SAFETY MEETING WORKING ON MUD MIXING PUMP

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 9

008

# SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

| | |
|---|---|
| 5. LEASE DESIGNATION AND SERIAL NUMBER: | UTU-77513 |
| 6. IF INDIAN, ALLOTTEE OR TRIBE NAME: | n/a |
| 7. UNIT or CA AGREEMENT NAME: | Prickly Pear Unit |
| 1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☑ OTHER | 8. WELL NAME and NUMBER: Prickly Pear Unit Federal 12-24 |
| 2. NAME OF OPERATOR: BILL BARRETT CORPORATION | 9. API NUMBER: 43-007-30953 |
| 3. ADDRESS OF OPERATOR: 1099 18TH St. Ste2300 CITY Denver STATE CO ZIP 80202 / PHONE NUMBER: (303) 312-8120 | 10. FIELD AND POOL, OR WILDCAT: Prickly Pear Unit/Mesa Verde |

4. LOCATION OF WELL

FOOTAGES AT SURFACE: 1271' FSL & 483' FWL — COUNTY: Carbon

QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E — STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☐ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☐ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☑ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☑ OTHER: Weekly Chronological Reports |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

WEEKLY DRILLING ACTIVITY REPORT FROM SEPTEMBER 1, 2004 THROUGH SEPTEMBER 3, 2004.

RECEIVED
SEP 0 7 2004
DIV. OF OIL, GAS & MINING

NAME (PLEASE PRINT) Tracey Fallang — TITLE Permit Analyst

SIGNATURE Tracey Fallang — DATE 9/3/2004

(This space for State use only)

(5/2000) (See Instructions on Reverse Side)

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/3/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 3

Spud Date : 9/3/2004 Days From Spud : 0 Depth At 06:00 : 100

Morning Operations : SPUD @04:30 9-3-04 Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 2:00:00 AM | WAIT ON RIG LEVELING JACKS & PREPARE FOR SPUD |
| 4:30:00 AM | LEVEL RIG "RAISE DRILLER SIDE 4 INCHES |
| 6:00:00 AM | DRILLING FROM 40 TO 100 |

Remarks :

RIG LEVEL JACKS WERE NESSARY FOR OPERATION AS SUB HAD SETTELED 4" NOTIFY DON STEPHENS B.L.M. DENNIS INGRAM STATE TM CASERS HALCO CEMENTERS WELL HEAD INC BARROID MUD PASON LOGGERS QUICK TEST OF STATUS OF WELL

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/2/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 2

Spud Date : 9/3/2004 Days From Spud : 0 Depth At 06:00 : 40

Morning Operations : WAIT ON RIG LEVELING JACKS Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

NOTIFY DON STEPHENS B.L.M. , DENNIS INGRAM STATE OF UTAH OF CURRENT STATIS OF WELL 15:00 9/1/04 ORDER CLOSEST JACKS AVAILABLE FROM MERMAC IN CASPER WYO. 21:00 9-1-04 E.T.A. 15:00 9-2-04

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/1/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 1

Spud Date : 9/3/2004 Days From Spud : 0 Depth At 06:00 : 40

Morning Operations : MOVE RIG Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

MOVE 50% COMPLETED RIG UP 25% COMPLETED LEFT MESSAGE WITH CAROL, STATE OF UTAH AND DON STEPHENS, B.L.M. ON FRIDAY 8/26/04 ON UPCOMING RIG MOVE AND SPUD. CALLED AND HAD CONVERSATION WITH DENNIS INGRAM, STATE OF UTAH, DON STEPHENS B.L.M. ON PRESENT STATUS OF RIG OPERATION 15:00 9/1/04 ORDER 1000 FEET OF 9.625 SURFACE CASING FROM REYNOLDS ON 8/31/04

010

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 9

# SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

5. LEASE DESIGNATION AND SERIAL NUMBER: UTU-77513

6. IF INDIAN, ALLOTTEE OR TRIBE NAME: n/a

7. UNIT or CA AGREEMENT NAME: Prickly Pear Unit

1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☑ OTHER

8. WELL NAME and NUMBER: Prickly Pear Unit Federal 12-24

2. NAME OF OPERATOR: BILL BARRETT CORPORATION

9. API NUMBER: 43-007-30953

3. ADDRESS OF OPERATOR: 1099 18TH St. Ste2300 CITY Denver STATE CO ZIP 80202

PHONE NUMBER: (303) 312-8120

10. FIELD AND POOL, OR WILDCAT: Prickly Pear Unit/Mesa Verde

4. LOCATION OF WELL

FOOTAGES AT SURFACE: 1271' FSL & 483' FWL

COUNTY: Carbon

QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E

STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☐ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☐ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☑ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☑ OTHER: Weekly Chronological Reports |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

WEEKLY DRILLING ACTIVITY REPORT FROM SEPTEMBER 10, 2004 THROUGH SEPTEMBER 17, 2004.

NAME (PLEASE PRINT) Tracey Fallang TITLE Permit Analyst

SIGNATURE Tracey Fallang DATE 9/17/2004

(This space for State use only)

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SEP 20 2004
DIV. OF OIL, GAS & MINING

(5/2000) (See Instructions on Reverse Side)

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/17/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 17

Spud Date : 9/3/2004 Days From Spud : 14 Depth At 06:00 : 8356

Morning Operations : TRIP FOR BIT #5 Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 8:00:00 AM | REPLACE STAND PIPE SECTION THAT WAS BLOWN UP |
| 11:00:00 AM | RUN IN HOLE WITH BIT#5 |
| 12:00:00 PM | WASH & REAM FROM 8033 TO 8080 |
| 4:30:00 AM | DRILLING FROM 8080 TO 8356 |
| 6:00:00 AM | DROP SURVEY,PUMP SLUG,PULL OUT OF HOLE WITH BIT #5 |

Remarks :

DAILY SAFETY MEETING WORKING AROUND HIGH PRESSURE MUD LINES. DAYS SINCE LOST TIME ACCIDENT 477. HELD BOP DRILL WHILE TRIPPING ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS & INSTALL FLOOR VALVE WELL SECURED IN 1 MIN 48 SEC CONTACT PATTERSON SUPTS LYNNE, DAVID,JESSE T.P. KENNEY ABOUT NEED TO REPLACE MUD LINE IN SUB&STAND PIPE AFTER WELL FINISHED AND NEED FOR MATTING BOARDS FOR SAFETY&REDUCED DOWN TIME THIS STAND PIPE INCIDENT WAS A NEAR MISS ACCIDENT PATTERSON DRILLING WILL REPLACE AFTER WELL FINISHED , TO REMIDY SITUATION

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/16/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 16

Spud Date : 9/3/2004 Days From Spud : 13 Depth At 06:00 : 8080

Morning Operations : TRIPING Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

DAILY SAFTY MEETING B.O.P. TEST DAYS SINCE LOST TIME ACCIDENT 476 HELD BOP DRILL ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS WELL SECURED 2MIN 8 SEC CALL STATE O&G REP DENNIS INGRAM TO NOTIFY OF SUCCESFUL TEST &PRESENT WELL STATUS CALL RASSMSEN WELDING TO REPAIR STAND PIPE

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/15/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 15

Spud Date : 9/3/2004 Days From Spud : 12 Depth At 06:00 : 8057

Morning Operations : NIPPLE UP &TEST Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

CALL OUT K-BAR &JACK HAMMER RASSMESSON WELDING WELLHEAD INC STATE O & G DENNIS INGRAHM REP ON LOC & WITTNESSED CSG CUT OFF CALL OUT QUICK TEST .NOTIFY BLM REP DON STEPHENS &STATE O&G REP DENNIS INGRAM OF UPCOMING TEST RECIEVED 9800 FEET OF 5.5 CSG CALL 2 YARD CONCRETE FROM PETE MARTIN FOR TOP JOB DAYS SINCE LOST TIME ACCIDENT475 DAILY SAFTY MEETING DANGER OF CAVE DIGGING CELLAR DISSCUS OPTIONS OF PLUG FAILURE WITH NO BOP

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/14/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 14

Spud Date : 9/3/2004 Days From Spud : 11 Depth At 06:00 : 8057

Morning Operations : NIPPLE DOWN Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

DAYS SINCE LOST TIME ACCIDENT 475 DAILY SAFETY MEETING CONNECTIONS HELD B.O.P. DRILL ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS WELL SECURED IN 2 MIN AND 15 SEC CALL REYNOLDS TRANSPORTATION AND ORDER 9800 FEET OF 5.5 ", 17# N-80 L.T.C. GAVE DON STEPHENS B.L.M. AND DENNIS INGRAM UPDATE ON WELL STATUS REYNOLDS TRASPORTATION UNABLE TO PROCURE N-80 , L-80 CSG. INSTEAD CALL WEATHERFORD WIRELINE WELLHEAD INC RASMASSON WELDING K-BAR ROUSTABOUT

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Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/13/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 13

Spud Date : 9/3/2004 Days From Spud : 10 Depth At 06:00 : 7807

Morning Operations : DRILLING AHEAD Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

DAYS SINCE LOST TIME ACCIDENT 474 DAILY SAFETY MEETING AIR HOIST HELD B.O.P. DRILL ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS WELL SECURED IN 2 MIN. AND 22 SEC. INCREASE WATER FROM 25 G.P.M. TO 40 G.P.M. TO FIGHT MUD WEIGHT DESANDER OUTPUT 12 P.P.G.

---

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/12/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 12

Spud Date : 9/3/2004 Days From Spud : 9 Depth At 06:00 : 7357

Morning Operations : DRILLING AHEAD Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

CALL DON STEPHENS TO UPDATE ON WELL STATUS. DAYS SINCE LOST TIME ACCIDENT 473 DAILY SAFETY MEETING GREASING CROWN. HELD B.O.P. DRILL ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS WELL SECURED IN 2MIN AND 13SEC RECIEVED EXTRA 6.25 MUD MOTOR AND 12 JOINTS DRILL PIPE 2 DRILL COLLARS

---

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/11/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 11

Spud Date : 9/3/2004 Days From Spud : 8 Depth At 06:00 : 7007

Morning Operations : DRILLING AHEAD Estimated Total Depth : 9700

| Time To | Description |
|---|---|

Remarks :

DAYS SINCE LOST TIME ACCIDENT 472. DAILEYSAFETY MEETING CLEANIG MUD TANKS HELD B.O.P. DRILL ALL PERSONAL TO STATIONS FUNCTION ANNULAR WELL SECURED IN 1MIN AND 58 SEC CALL BRANDT THIS MORNING REPRESENATIVE CAME BY AFTERNOON STOCKED UP SHAKER SCREEN INVENTORY

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

| | | | |
|---|---|---|---|
| Well : **Prickly Pear #12-24-12-14** | | API # : 43-007-30953 | Operations Date : 9/10/2004 |
| Surface Location : SWSW-24-12S-14 E 26th PM | | Area : Nine Mile Canyon | Report # : 10 |
| Spud Date : 9/3/2004 | Days From Spud : 7 | | Depth At 06:00 : 6565 |
| Morning Operations : DRILLING AHEAD | | | Estimated Total Depth : 9700 |

Remarks :

SAFETY MEETING PROPER MUD STORAGE AND HANDLING. DAYS SINCE LOST TIME ACCIDENT 471. HELD B.O.P. DRILL ALL PERSONAL TO STATIONS & FUNCTION PIPE RAMS WELL SECURED IN 2MIN. 35SEC.

| Time To | Description |
|---|---|

FORM 9

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

011

5. LEASE DESIGNATION AND SERIAL NUMBER: UTU-77513

# SUNDRY NOTICES AND REPORTS ON WELLS

6. IF INDIAN, ALLOTTEE OR TRIBE NAME: n/a

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

7. UNIT or CA AGREEMENT NAME: Prickly Pear Unit

1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☑ OTHER

8. WELL NAME and NUMBER: Prickly Pear Unit Federal 12-24 -12-14

2. NAME OF OPERATOR: BILL BARRETT CORPORATION

43

9. API NUMBER: 007-30953

3. ADDRESS OF OPERATOR: 1099 18TH St. Ste230C CITY Denver STATE CO ZIP 80202

PHONE NUMBER: (303) 312-8120

10. FIELD AND POOL, OR WILDCAT: Prickly Pear Unit/Mesaverde

4. LOCATION OF WELL

FOOTAGES AT SURFACE: 1271' FSL & 483' FWL

COUNTY: Carbon

QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E

STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☐ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: _____ | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☐ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☑ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: _____ | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☑ OTHER: Weekly Chronological Reports |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

WEEKLY DRILLING ACTIVITY REPORT FROM SEPTEMBER 18, 2004 THROUGH SEPTEMBER 24, 2004.

NAME (PLEASE PRINT) Tracey Fallang TITLE Permit Analyst

SIGNATURE Tracey Fallang DATE 9/24/2004

(This space for State use only)

RECEIVED
SEP 27 2004
DIV. OF OIL, GAS & MINING

(5/2000) (See Instructions on Reverse Side)

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/24/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 24

Spud Date : 9/3/2004 Days From Spud : 21 Depth At 06:00 : 9218

Morning Operations : PULL OUT OF HOLE WITH BIT#11 Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 11:30:00 AM | CHANGE BIT&MUD MOTOR CHECK WEAR RING RUN IN HOLE WITH BIT#11 TO 9031 |
| 12:30:00 PM | WASH&REAM FROM 9031 TO9131 |
| 8:30:00 PM | DRILLING FROM 9131 TO 9195 |
| 9:00:00 PM | LUBRICATE DRILLING APARATUS |
| 1:00:00 AM | DRILLING FROM 9195 TO 9218 |
| 6:00:00 AM | CHECK FLOW, PUMP SLUG, PULL OUT OF HOLE WITH BIT#11 |

Remarks :

7DAILY SAFETY MEETING ALL PERSONAL REVIEW NEW PATTERSON DRILLING HANDBOOK DAYS SINCE LOST TIME ACCIDENT 484 CONTACT HALCO LOGING T.M. CASERS HALCO CEMENTERS STATE O.&G. REP. DENNIS INGRAM B.L.M. REP DON STEPHENS WELLHEAD INC ABOUT STATUS OF WELL AND PLANS FOR NEXT WELL P.P.21-2 MUD MOTOR HOURS-12.5 CORROSION RING HOURS W.J.=49.5 S.S.=115 HELD B.O.P. DRILL ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS WELL SECURED IN 2MIN 45SEC

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Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/23/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 23

Spud Date : 9/3/2004 Days From Spud : 20 Depth At 06:00 : 9131

Morning Operations : PULL OUT OF HOLE WITH BIT#10 Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 9:30:00 AM | TRIP IN HOLE W/ BIT # 10 |
| 10:00:00 AM | WASH & REAM FROM 8984 TO 9044 |
| 7:00:00 PM | DRILLING FROM 9044 TO 9099 |
| 7:30:00 PM | LUBRICATE DRILLING APARATUS |
| 12:30:00 AM | DRILLING FROM 9099 TO 9131 |
| 6:00:00 AM | PULL OUT OF HOLE WITH BIT#10 |

Remarks :

483 DAYS SINCE LAST LOST TIME ACCIDENT
SAFETY MEETING HELD, (SLIP DIE INSPECTION)
CORR. RING W.J.=36 S.S.=101.5
MUD MOTER HOURS105.5

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Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/22/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 22

Spud Date : 9/3/2004 Days From Spud : 19 Depth At 06:00 : 9044

Morning Operations : BIT TRIP Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 11:00:00 PM | DRILLING FROM 8755' TO 9044' |
| 4:00:00 AM | PUMP PILL, TRIP OUT FOR BIT |
| 6:00:00 AM | INSPECT WEAR BUSHING, TRIP IN W/ BIT # 10 |

Remarks :

482 DAYS SINCE L.T.ACC.
SAFETY MEETING - WORKING ON PUMPS
CORR. RINGS = 112 HOURS
TOTAL HOURS ON MUD MTR. (W/S.N.1006)91.50

WELL SUPERVISOR -

R.L. BOYLES

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/21/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 21

Spud Date : 9/3/2004 Days From Spud : 18 Depth At 06:00 : 8870

Morning Operations : DRILLING Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 1:00:00 PM | DRILLING FROM 8695' TO 8755' |
| 5:30:00 PM | PUMP PILL, DROP SURVEY, TRIP OUT FOR BIT |
| 6:30:00 PM | PULL AND INSPECT WEAR RING, FUNCTION TEST BLIND AND PIPE RAMS |
| 7:30:00 PM | TRIP IN TO CASING SHOE |
| 9:00:00 PM | SLIP AND CUT 120' DRILLING LINE |
| 12:30:00 AM | TRIP IN HOLE W/ BIT # 9, BREAK CIRC.@ 4500' |
| 1:00:00 AM | WASH AND REAM 70' TO BOTTOM ( NO FILL ) |
| 6:00:00 AM | DRILLING FROM 8755' TO 8870' |

Remarks :

481 DAYS SINCE LAST L.T. ACCIDENT
SAFETY MEETING - DERRICKMAN TIE OFF
SURVEY @ 8702' = 4 DEGREE
TRIP WENT GOOD W/ NO TIGHT SPOTS OR DRAG.
OFF BOTTOM PRESSURE @ 120 S.P.M.= 1470
CORR. RINGS = 88 HOURS
TOTAL HOURS ON MUD MTR.= 74.50 ( S.N. 1006 )

WELL

SUPERVISOR - R.L. BOYLES

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Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/20/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 20

Spud Date : 9/3/2004 Days From Spud : 17 Depth At 06:00 : 8695

Morning Operations : DRILLING Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 9:00:00 AM | TRIP IN W/ BIT # 8 |
| 9:30:00 AM | WASH AND REAM 60' TO BTM. ( NO FILL ) |
| 5:00:00 PM | DRLG. FROM 8530' TO 8590' |
| 5:30:00 PM | RIG SERVICE, FUNCTION TEST HYDRILL |
| 6:00:00 AM | DRLG. FROM 8590' TO 8695' |

Remarks :

480 DAYS SINCE LAST L.T.ACC., DAILY SAFETY MEETING ( TONG DIE INSPECTION AND PROPER EYE PROTECTION WHILE CHANGING SAME.) FUNCTION TEST PIPE RAMS AND B.O.P. DRILL,WELL SHUT IN AND SECURE IN 2 MINS. 15 SEC. - CALLED HALCO,T & M CSG., WELL HEAD INC., STATE OF UTAH OIL AND GAS, B.L.M., INFORMED ABOVE OF WELL STATIS.

OFF BTM. PRESSURE = 1400 @
120 S.P.M. REDUCED CIRC. PRESSURE = 340 @
53 S.P.M. ACC. PRESSURE = 2400 P.S.I.
ANN. PRESSURE = 1100 P.S.I.
MAN. PRESSURE = 1900 P.S.I.

TOTAL HOURS ON MUD MOTOR = 62.50

NOTE :
MUD REPORT SHOWING 0 % ON SAND AND SOLIDS CONTENT ( WISHFULL THINKING) I'LL HAVE ACTUAL CONTENTS ON 9-21-2004 REPORT. THKS. R.L.DRILL

SUPERVISOR: R. BOYLES

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/19/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 19

Spud Date : 9/3/2004 Days From Spud : 16 Depth At 06:00 : 8530

Morning Operations : TRIP IN HOLE W/ BIT # 8 Estimated Total Depth : 9700

Remarks :

DAILLY SAFETY MEETING HIGH PRESSURE HOSES DAYS SINCE LOST TIME ACCIDENT 479 HELD BOP DRILL ALL PERSONAL TO STATIONS FUNCTION BLIND RAMS WELL SECURED IN 1 MIN. AND 55 SEC. NOTIFY HALCO WIRELINE, T&M CASERS HALCO CEMENTERS, WELLHEAD INC. ,STATE O&G REPRESENITIVE OF WELL STATUS

| Time To | Description |
|---|---|
| 8:00:00 AM | RUN IN HOLE WITH BIT#7 |
| 9:00:00 AM | WASH&REAM FROM 8285 TO 8435 14 UNDERGAUGE HOLE |
| 3:00:00 PM | DRILLING FROM 8435 TO 8492 |
| 3:30:00 PM | LUBRICATE DRILLING APARATUS |
| 10:00:00 PM | DRILLING FROM 8492' TO 8530' |
| 2:30:00 AM | PUMP SLUG, TRIP OUT W/ BIT # 7 |
| 3:30:00 AM | CHANGE BITS, PULL AND INSPECT WEAR RING, B.O.P. DRILL |
| 6:00:00 AM | TRIP IN W BIT # 8 |

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/18/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 18

Spud Date : 9/3/2004 Days From Spud : 15 Depth At 06:00 : 8436

Morning Operations : RUN IN HOLE WITH BIT #7 Estimated Total Depth : 9700

Remarks :

DAILY SAFETY MEETING TRIPING DAYS SINCE LOST TIME ACCIDENT 478 HELD B.O.P. DRILL WHILE ON BANK ALL PERSONAL TO STATIONS FUCTION BLIND RAMS WELL SECURED IN 1MIN AND 19 SEC CONTACT HALCO WIRELINE TM CASERS HALCO CEMENT WELLHEAD INC ABOUT STATUS OF WELL

| Time To | Description |
|---|---|
| 9:00:00 AM | PULL OUT OF HOLE WITH BIT#5 |
| 10:00:00 AM | RETRIEVE SURVEY CHECK WEAR RING CHANGE BITS HELD BOP DRILL |
| 1:30:00 PM | RUN IN HOLE WITH BIT#6 NO FILL |
| 10:30:00 PM | DRILLING FROM 8080 TO 8436 |
| 2:30:00 AM | PULL OUT OF HOLE WITH BIT#6 |
| 3:30:00 AM | CHECK WEAR RING CHANGE BITS HELD BOP DRILL ALL PERSONAL TO STATIONS FUNCTION BLIND RAMS WELL SECURED IN 1MIN AND 55 SEC |
| 6:00:00 AM | RUN IN HOLE WITH BIT#7 |

012

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 9

# SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

| | |
|---|---|
| 5. LEASE DESIGNATION AND SERIAL NUMBER: | UTU-77513 |
| 6. IF INDIAN, ALLOTTEE OR TRIBE NAME: | n/a |
| 7. UNIT or CA AGREEMENT NAME: | Prickly Pear Unit |
| 1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☑ OTHER | 8. WELL NAME and NUMBER: Prickly Pear Unit Federal 12-24 |
| 2. NAME OF OPERATOR: BILL BARRETT CORPORATION | 9. API NUMBER: 43-007-30953 |
| 3. ADDRESS OF OPERATOR: 1099 18TH St. Ste230C CITY Denver STATE CO ZIP 80202 | PHONE NUMBER: (303) 312-8120 |
| | 10. FIELD AND POOL, OR WILDCAT: Prickly Pear Unit/Mesaverde |

4. LOCATION OF WELL

FOOTAGES AT SURFACE: 1271' FSL & 483' FWL — COUNTY: Carbon

QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E — STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☐ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☐ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☑ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☑ OTHER: Weekly Chronological Reports |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

WEEKLY DRILLING ACTIVITY REPORT FROM SEPTEMBER 25, 2004 THROUGH SEPTEMBER 29, 2004 (NO ACTIVITY ON SEPTEMBER 30 & OCTOBER 1).

NAME (PLEASE PRINT) Tracey Fallang — TITLE Permit Analyst

SIGNATURE Tracey Fallang — DATE 10/1/2004

RECEIVED
OCT 04 2004
DIV. OF OIL, GAS & MINING

(This space for State use only)

(5/2000) (See Instructions on Reverse Side)

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/29/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 29

Spud Date : 9/3/2004 Days From Spud : 26 Depth At 06:00 : 9496

Morning Operations : RIG DOWN Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 7:00:00 AM | LAY DOWN DRILL STRING PULL WEAR RING |
| 1:30:00 PM | RUN PRODUCTION CASING BREAK CIRCULATION AND LAND HANGER WITH 120,000 LBS |
| 6:30:00 PM | CIRCULATE & WAIT ON HALCO CEMENTERS |
| 9:30:00 PM | RIG UP HALCO HOLD PREJOB SAFETY MEETING PRESSURE TEST SURFACE LINES TO 4000PSI &PUMP CEMENT |
| 12:00:00 AM | RIG DOWN HALCO LAYDOWN LANDING JOINT CLEANMUD TANKS **RIG RELEASED |
| 6:00:00 AM | NIPPLE DOWN &RIG DOWN PREPARE FOR TRUCKS |

Remarks :

Run 228 jts,(plus 4 marker jts), 17#, LT&C, L80, 5.5" CSG. Run SS float shoe & SS float collar top of frist jt. Land csg at 9491'.
Float Collar Depth = 9448.76
1ST marker = 8105.64
2ND marker = 6729.47
3RD marker = 5362.31
4TH marher = 4432.73
Cement = 1850 sks of 50/50 POZ @ 13.4#, 1.49CU/FT/SK. Displace w/ 3% Clay Fix Water.
Request HCS on loc at 13:00, arrive at .18;30 PUMP 20BL SUPER FLUSH, 1850SX 50/50POZ 2%GEL 3%KCL 75%HALAD-322 2%FWCA3#SK SILICALITE .25#SKFLOCELE GRANULITE

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Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/28/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 28

Spud Date : 9/3/2004 Days From Spud : 25 Depth At 06:00 : 9496

Morning Operations : LAY DOWN DRILL PIPE Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 12:30:00 PM | FINISH SECONDLOG RUN&RIG DOWN HALCO |
| 5:30:00 PM | FUNCTION BLIND RAMS RUN IN HOLE,BREAK CIRCULATION AT 5970,RUN IN TO 9394 |
| 6:00:00 PM | WASH&REAM 102 FEET |
| 11:00:00 PM | CIRCULATE&CONDITION WELL FOR CASING |
| 6:00:00 AM | LAY DOWN DRILL STRING |

Remarks :

DAILY SAFETY MEETING WIRELINE SAFETY DAYS SINCE LOST TIME ACCIDENT488 BOP DRILL ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS WELL SECURED 2MIN I5SEC 12:00 HOURS CALL OUT LAYDOWN MACHINE T&M , INFORM OF WELL STATUS CASERS, HALCO CEMENTERS, WELLHEAD INC., CAROL DANIALS STATE O&G REP, DON STEPHENS BLM REP, DAWN TRUCKING, ORDER MUD MOTOR IN CASE WELL IS DRILLED DEEPER FROM SMITH

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Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/27/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 27

Spud Date : 9/3/2004 Days From Spud : 24 Depth At 06:00 : 9496

Morning Operations : FINAL RUN LOGING Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 8:30:00 AM | DRILLING FROM 9490 TO 9496 |
| 12:30:00 PM | PULL UP HOLE TO 5427& RUN IN HOLE |
| 2:00:00 PM | CIRCULATE CONDITION HOLE FOR LOGS |
| 2:30:00 PM | LUBRICATE DRILLING APARATUS |
| 6:00:00 PM | PULL OUT OF HOLE FOR LOGS |
| 7:00:00 PM | HELD BOP DRILL,HELD SAFETY MEETING WITH HALCO, RIG UP LOGERS |
| 6:00:00 AM | FIRST RUN GAMMA RAY,NETRON DENSITY, INDUCTION, SECOND RUN GAMMA RAY, WAVE SONIC MICRO IMAGER |

Remarks :

DAYS SINCE LOST TIME ACCIDENT487. DAILY SAFETY MEETING TONG DIES. B.O.P. DRILL ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS WELL SECURED IN 2MIN AND 52SEC. CALL HALCO LOGGERS OUT @11:00HOURS CALL TO NOTIFY OF WELL STATUS T&M CASERS, HALCO CEMENTERS WELLHEAD INC. CAROL DANIELS STATE O&G DENNIS INGRAM STATE O&G DON STEPHENS BLM REP. DAWN TRUCKING ,RATHOLE DRILLING K-BAR ROUSTABOUTS

# REGULATORY DRILLING SUMMARY

Bill Barrett Corporation

Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/26/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 26

Spud Date : 9/3/2004 Days From Spud : 23 Depth At 06:00 : 9490

Morning Operations : DRILLING Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 7:30:00 AM | CUT&SLIP DRILLING LINE |
| 11:30:00 AM | RUN IN HOLE WITH BIT#13 |
| 12:00:00 PM | WASH AND REAM FROM 9216 TO9316 |
| 8:00:00 PM | DRILLING FROM 9316 TO 9407 |
| 8:30:00 PM | LUBRICATE DRILLING APARATUS |
| 6:00:00 AM | DRILLING FROM 9407 TO9490 |

Remarks :

DAILY SAFETY MEETING ALL PERSONAL REVIEW PATTERSON SAFETY BOOK. DAYS SINCE LOST TIME ACCIDENT486 . B.O.P. DRILL ALL PERSONAL TO STATIONS FUNCTION ANNULAR WELL SECURED IN 2MIN AND 43 SEC CONTACT AND UPDATE ON CURRENT WELL STATUS DON STEPHENS BLM REP, DENNIS INGRAM STATE O&G REP HALCO LOGERS TM CASERS WELLHEAD INC HALCO CEMENTERS, MUD HOPPER CENTRIFUDGE RAT HOLE DRILLING, K-BAR ROUSTABOUTS

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Well : **Prickly Pear #12-24-12-14** API # : 43-007-30953 Operations Date : 9/25/2004

Surface Location : SWSW-24-12S-14 E 26th PM Area : Nine Mile Canyon Report # : 25

Spud Date : 9/3/2004 Days From Spud : 22 Depth At 06:00 : 9316

Morning Operations : CUT&SLIP Estimated Total Depth : 9700

| Time To | Description |
|---|---|
| 10:30:00 AM | RUN IN HOLE WITH BIT#12 TO 9148 |
| 11:00:00 AM | WASH&REAM FROM 9148 TO 9218 |
| 6:30:00 PM | DRILLING FROM 9218 TO 9282 |
| 7:00:00 PM | LUBRICATE DRILLING APARATUS,BOP DRILL. |
| 10:00:00 PM | DRILLING FROM 9282 TO 9316 |
| 5:30:00 AM | DROP SURVEY, CHECK FLOW ,PUMP SLUG PULL OUT OF HOLE WITH BIT#12 RETRIEVE SURVEY CHANGE BITS CHECK WEAR RING RUN IN HOLE WITH BIT#13 TO SHOE |
| 6:00:00 AM | CUT &SLIP DRILLING LINE |

Remarks :

DAILY SAFETY MEETING SAFETY HARNESS OVERHEAD WORK. DAYS SINCE LOST TIME ACCIDENT485. HELD BOP DRILL ALL PERSONAL TO STATIONS FUNCTION PIPE RAMS WELL SECURED IN 2MIN 35SEC . CALL TO NOTIFY OF PRESENT WELL STATUS DAWN TRUCKING, HALCO LOGERS, T&M CASERS, WELLHEAD INC, HALCO CEMENTERS, STATE O&G REP DENNIS INGRAM, BLM REP DON STEPHENS, CONTACT BRADY OVER NEW LOCATION, BLAST PIT ON SATURDAY, CONTACT RATHOLE DRILLING SCHEDULE SUNDAY CORROSION RING HOURS W.J.=63.5 S.S.=130

FORM 9

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

013

# SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

5. LEASE DESIGNATION AND SERIAL NUMBER: UTU 77513
6. IF INDIAN, ALLOTTEE OR TRIBE NAME: N/A
7. UNIT or CA AGREEMENT NAME: Prickly Pear Unit
1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☑ OTHER
8. WELL NAME and NUMBER: Prickly Pear Unit Fed 12-24 ~~12-14~~
2. NAME OF OPERATOR: Bill Barrett Corporation
9. API NUMBER: 4300730953
3. ADDRESS OF OPERATOR: 1099 18th Street, Suite 2300 CITY Denver STATE CO ZIP 80202
PHONE NUMBER: (303) 312-8168
10. FIELD AND POOL, OR WILDCAT: Prickly Pear Unit/Mesaverde
4. LOCATION OF WELL
FOOTAGES AT SURFACE: 1271' FSL & 483' FWL
COUNTY: Carbon
QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E
STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☑ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☐ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☐ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☑ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☐ OTHER: |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

Attached to this sundry is a copy of a general completion procedure and wellbore diagram to be used in the Nine Mile Canyon area. The exact number of stages and depths will be determined after logs have been run for each well in the Nine Mile area. Upon approval, it is Bill Barrett Corporation's intention to commingle production from the Wasatch, Middle Wasatch, North Horn (part of the lower Wasatch) and Mesaverde formations.

Gas composition is similar across all formations. The pressure profile across the formations is normal and BBC does not anticipate any cross flow.

Production is considered to be from one pool. In the event that allocation by zone or interval is required, BBC would use representative sampling obtained from production logs and allocate on a percentage basis by zone or interval.

A letter and affidavit of notice is being submitted under separate cover.

COPY SENT TO OPERATOR
Date: 10-26-04
Initials: CHD

RECEIVED
OCT 0 5 2004
DIV. OF OIL, GAS & MINING

NAME (PLEASE PRINT) Tracey Fallang TITLE Permit Analyst

SIGNATURE Tracey Fallang DATE 10/4/2004

(This space for State use only)

Accepted by the
Utah Division of
Oil, Gas and Mining
Date: 10/22/04
By: [signature]

Federal Approval Of This
Action Is Necessary

(5/2000) (See Instructions on Reverse Side)

**Nine Mile Canyon Generic Completion Procedure**
Carbon Co., UT

**Generic Multi-stage Completion Procedure**

Current Well Status: New completion with intention of downhole commingling

Objective: Rigless completion. Perf and frac various sands in separate frac stages.
Procedure:

1) Install wellhead isolation tool. Test casing to 3500 psi for 10" and low test to 250 psi for 10".
2) MIRU electric line unit. RIH with 4" casing gun, perforate interval from (to be determined) with 3 jspf, 120 deg phasing. POOH.
3) MIRU Halliburton frac equipment. Test all frac lines to 5000 psi. Frac **Stage 1** per frac rec.

4) RIH with 5-1/2" flow through composite frac plug and 4" casing gun. Set plug # 1 at (to be determined). Perforate 2nd interval from (to be determined) with 3 jspf, 120 deg phasing. POOH.
5) Test all frac lines to 5000 psi. Frac **Stage 2** per rec.

6) RIH with 5-1/2" flow through composite frac plug and 4"casing gun. Set plug # 2 at (to be determined). Perforate 3rd interval from (to be determined)' with 3 jspf, 120 deg phasing. POOH.
7) Test all frac lines to 5000 psi. Frac **Stage 3** per rec.
8) Flow back frac Stages 1 through 3 24-48 hrs to cleanup.

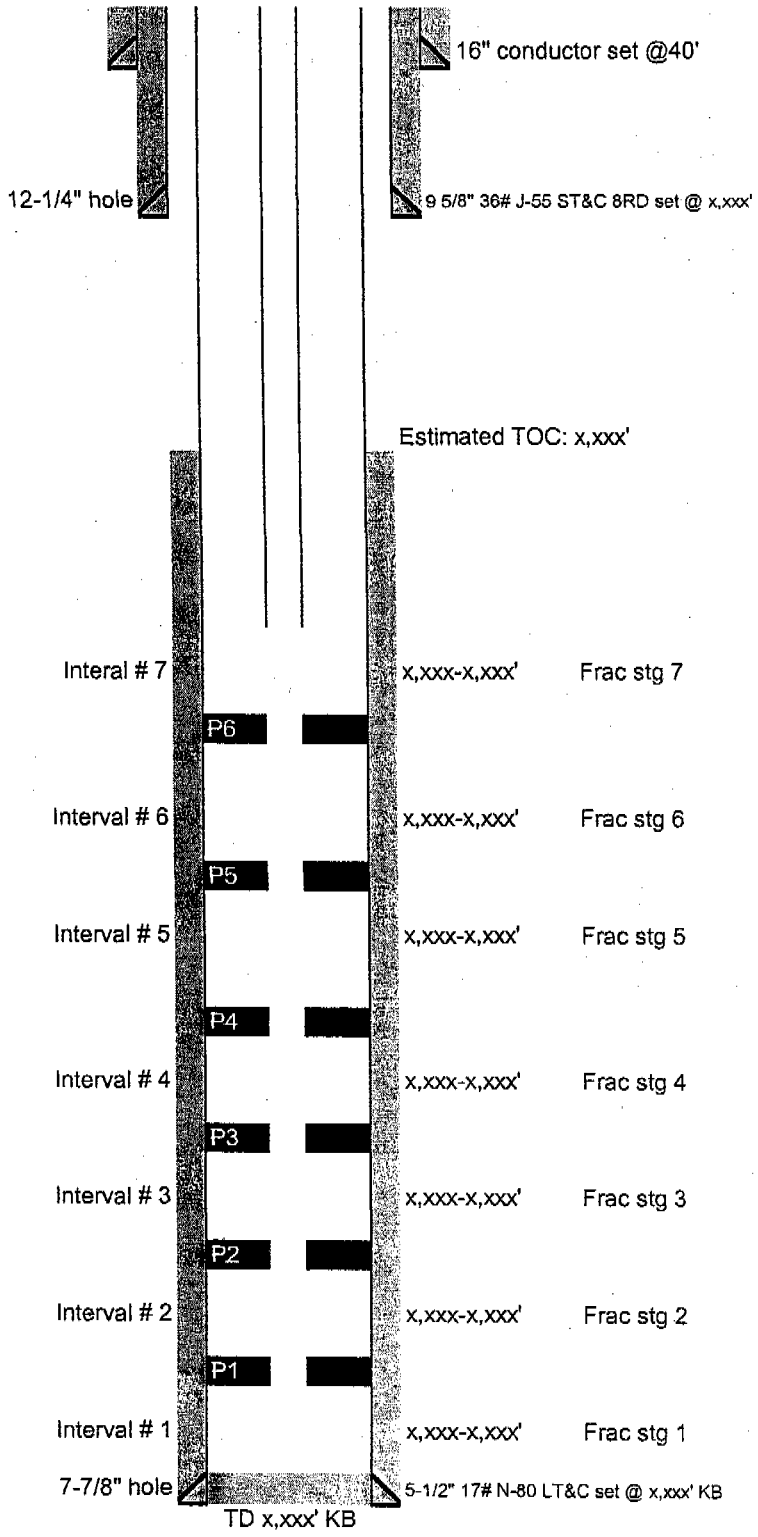
9) RU service unit. RU e-line and RIH with 5-1/2" composite bridge plug and set at (to be determined). Remove well head isolation tool. NU BOP's. Pressure test BOP's to 3000 psi, test hydril to 1500 psi. Run 4-3/4" drag bit with pump off bit sub with dart valve, 1 jt 2-3/8" tubing, 2-3/8" "XN" and "X" profile nipple, rest of 2-3/8" tubing. Drill out all plugs. Clean out to PBTD. Utilize foam unit if necessary to obtain sufficient returns. EOT depth to be determined.
10) Strip BOP's off and NU wellhead.
11) Drop ball, pump off bit and sub. Swab well in and place all intervals on production.
12) RDMO service unit. Turn well to sales.

Note: There may be up to 10 frac stages.

**Bill Barrett Corporation**

**Generic well bore diagram**
Nine Mile Canyon

Carbon Co., UT




**5-1/2" 17# N-80 LT&C specs:**
ID-4.892"
Drift-4.767'
Burst-7740 psi
Collapse-6280 psi

rparham

10/4/2004

**Bill Barrett Corporation**

October 4, 2004

Federal Express

Utah Division of Oil, Gas & Mining
1594 W. North Temple, Suite 1210
Salt Lake City, Utah 84114-5801
Attention: Mr. Dustin Doucet

RE: Sundry Notices
Prickly Pear Unit Federal 10-4
SESE Section 10, Township 12 South, Range 14 East
Prickly Pear Unit Federal 12-24
SWSW Section 24, Township 12 South, Range 14 East
Carbon County, Utah

Dear Mr. Doucet:

In accordance with our recent telephone conversations, Bill Barrett Corporation has submitted Sundry Notices to commingle production from the Wasatch, Middle Wasatch, North Horn and Mesaverde Formations in the captioned wells. We have enclosed herewith copies of the Sundry Notices together with a plat showing the leases and wells in the area, a description of the recompletion procedures and an affidavit confirming notice pursuant to the Utah OGM regulations.

Should you require additional information in this regard, please contact the undersigned at 303-312-8184 or by email at dgundry-white@billbarrettcorp.com. Your earliest attention to this matter is most appreciated.

Sincerely
Bill Barrett Corporation

Doug Gundry-White
Consulting Landman



1099 18TH STREET
SUITE 2300
DENVER, CO 80202
P 303.293.9100
F 303.291.0420

# AFFIDAVIT

Affiant on oath swears that the following statements are true:

My name is Douglas W. G. Gundry-White. I am a Petroleum Landman working for Bill Barrett Corporation (BBC). BBC has submitted Sundry Notices to commingle production from the Wasatch, Middle Wasatch, North Horn and Mesaverde Formations in the Prickly Pear Unit Federal 10-4 well, which is located in the SESE of Section 10, Township 12 South, Range 14 East, and the Prickly Pear Unit Federal 12-24 well, which is located in the SWSW of Section 24, Township 12 South, Range 14 East, Carbon County Utah. In compliance with the Utah OGM regulation R649-3-22, I have provided a copy of the Sundry Notices, by certified mail, to the owners (see listed below) of all contiguous oil and gas leases or drilling units overlying the pool.

EOG Resources, Inc.
600 17th Street, Suite 1100N
Denver, CO 80202
Attention: Mr. Bob Davis

Dominion Exploration & Production, Inc.
14000 Quail Springs Parkway, Suite 600
Oklahoma City, Oklahoma 73134-2600
Attention: Mr. Rusty Waters

Gasco Energy, Inc.(formerly Pannonian Energy).
14 Inverness Drive East, Suite H-236
Englewood, CO 80112
Attention: Mr. Marc Choury

Date: 10/4/04

Affiant

Douglas W. G. Gundry-White

**From:** <Russell_R_Waters@dom.com>
**To:** <dustindoucet@utah.gov>
**Date:** 10/13/2004 11:54:13 AM

Dustin, Dominion Exploration & Production has no objection to Bill Barretts comingling application.

Russell R. Waters
Senior Staff Landman
Onshore/Western U.S.-OKC
(405) 749-5282
(405) 749-6662 fax
86705282 tie line

**CC:** <dgundry-white@billbarrettcorp.com>

**From:** <Bob_Davis@eogresources.com>
**To:** <dustindoucet@utah.gov>
**Date:** 10/11/2004 9:36:22 AM
**Subject:** Commingling Proposal

Dustin: Please allow this e-mail to serve as EOG Resources, Inc. notice of approval of Bill Barrett's application to commingle production from the Wasatch, Middle Wasatch, North Horn and Mesaverde Formations in the Prickly Pear Unit Federal 10-4 and 12-24 Wells. We hereby waive the 15-day response period. Should you require any additional information, in this regard, please do not hesitate to give me a call. RG

Bob Davis, CPL
EOG Resources, Inc.
600 17th Street, Suite 1100N
Denver, CO 80202
303-824-5428
303-824-5401 (fax)
303-638-2526 (cell)

**CC:** <dgundry-white@billbarrettcorp.com>, <Russell_R_Waters@dom.com>, <Roger_Falk@eogresources.com>, <Dan_Frederick@eogresources.com>

**From:** "Robin Dean" <rdean@gascoenergy.com>
**To:** <dustindoucet@utah.gov>
**Date:** 10/8/2004 8:52:15 AM
**Subject:** Bill Barrett Corporation Production Commingling

Mr. Doucet:

Please be advised that Gasco Energy, Inc has no objection to Bill Barrett Corporation commingling production at its Prickly Pear Unit Federal 10-4 well and its Prickly Pear Unit Federal 12-24 well.

Thank you

Robin Dean
Senior Geologist
Gasco Energy, Inc.

014

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 9

# SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

| | |
|---|---|
| 5. LEASE DESIGNATION AND SERIAL NUMBER: | UTU-77513 |
| 6. IF INDIAN, ALLOTTEE OR TRIBE NAME: | n/a |
| 7. UNIT or CA AGREEMENT NAME: | Prickly Pear Unit |
| 1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☑ OTHER | 8. WELL NAME and NUMBER: Prickly Pear Unit Fed 12-24-12-14 |
| 2. NAME OF OPERATOR: BILL BARRETT CORPORATION | 9. API NUMBER: 43-007-30953 |
| 3. ADDRESS OF OPERATOR: 1099 18TH St. Ste2300 CITY Denver STATE CO ZIP 80202 | PHONE NUMBER: (303) 312-8168 |
| | 10. FIELD AND POOL, OR WILDCAT: Prickly Pear Unit/Mesaverde |

4. LOCATION OF WELL

FOOTAGES AT SURFACE: 1271' FSL & 483' FWL — COUNTY: Carbon

QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E — STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☐ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☐ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☑ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☑ OTHER: Weekly Activity Reports |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

COMPLETION ACTIVITY REPORT FOR OCTOBER 7, 2004. WAITING ON FURTHER COMPLETION ACTIVITY.

NAME (PLEASE PRINT) Tracey Fallang — TITLE Permit Analyst

SIGNATURE Tracey Fallang — DATE 10/8/2004

(This space for State use only)

RECEIVED
OCT 12 2004
DIV. OF OIL, GAS & MINING

(5/2000) (See Instructions on Reverse Side)

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/7/2004 Report # : End Time Description

Summary : Set Frac head. & test, MESA Wire Line Bond Log Casing.

FORM 9

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

015

# SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

5. LEASE DESIGNATION AND SERIAL NUMBER: UTU-77513

6. IF INDIAN, ALLOTTEE OR TRIBE NAME: n/a

7. UNIT or CA AGREEMENT NAME: Prickly Pear Unit

1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☑ OTHER

8. WELL NAME and NUMBER: Prickly Pear Unit Fed 12-24~~-12-14~~

2. NAME OF OPERATOR: BILL BARRETT CORPORATION

9. API NUMBER: 43-007-30953

3. ADDRESS OF OPERATOR: 1099 18TH St. Ste2300 CITY Denver STATE CO ZIP 80202

PHONE NUMBER: (303) 312-8168

10. FIELD AND POOL, OR WILDCAT: Prickly Pear Unit/Mesaverde

4. LOCATION OF WELL

FOOTAGES AT SURFACE: 1271' FSL & 483' FWL

COUNTY: Carbon

QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN: SWSW 24 12S 14E

STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☐ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☐ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☑ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☑ OTHER: Weekly Activity Reports |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

WEEKLY COMPLETION ACTIVITY REPORT FROM OCTOBER 12, 2004 THROUGH OCTOBER 15, 2004.
NO ACTIVITY OCCURRED BETWEEN OCTOBER 8TH THROUGH OCTOBER 11TH.

NAME (PLEASE PRINT) Tracey Fallang TITLE Permit Analyst

SIGNATURE Tracey Fallang DATE 10/15/2004

(This space for State use only)

RECEIVED
OCT 18 2004
DIV. OF OIL, GAS & MINING

(5/2000) (See Instructions on Reverse Side)

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/15/2004 Report # : 4

Summary : Rig HES, Frac Blackhawk. Rig Wire line set frac plug perf stage 2

| End Time | Description |
|---|---|
| 8:30:00 AM | rig HES frac, wait on HES Frac Engineer |
| 10:00:00 AM | CO2 Foam Frac Stage 1. Black Hawk. Fluid System: 30# Purgel III Lt. 70Q CO2. Break @ 3724 @ 5 BPM. Avg, foam Rate:14 bpm, Avg. CO2 Rate: Avg. Pressure: 4930 PSI, Max Foam Rate: 33 BPM, Max CO2 Rate: Max Pressure: 5492 PSi. Total Fluid Pumped: 19,000 gal. Totel CO2 Pumped: 110 tons+ 10 tons cooldown, Totel Sand Pumped in formation: 58,000LB, ISIP: 4390 PSI, Frac Gradient: 0.910 psi/ft, flushed with 50Q CO2 foam with 500 gal fluid cap. jo was flushed successfully. |
| 1:30:00 PM | rig Mesa Wire line, Pickup 5.5" frac plug two 4 ft guns RIH Corelate to short joint run to setting depth check depth to casig coller set frac plug #1 @ 8750 pull to perf depth shoot U.Sego ...GUNS DID NOT FIRE. POOH Wire in guns broke off. rewire guns RIH Correlate to short joint run to perf ndepth check depth to casing coller. perforate U. SEGO @ 8695-8699 3spf 120 phasing 23 gram shot. .410 hole. pickup to 8620 perforate @ 8620-8624 3spf 120 phasing 23 gram shot .410 hole. POOH.all shots fired |
| 3:00:00 PM | HES Frac Stage #2 U.SEGO, Fluid System: 30 # Purgel III LT 70 Q CO2. Break @ 5 BPM. Avg.Foam Rate: 14 BPM, Avg. Co2 Rate: BPM, Avg. Pressure: 5180 PSI, Max. Foam Rate: 35 BPM. Max. CO2 Rate: BPM, Max. Pressure: 6453 PSI, Totel Fluid Pumped: 24,000 gal, Totel Co2 Pumped: 110 tons + 10 tons cooldown, Totel Sand pumped in Formation: 58,000 lb, ISIP; 4390 psi, Frac Gradient: 0.950 psi/ft, flushed with 50 Q foam with 500 gal fluid cap. job was flushed successfully. |
| 3:00:00 PM | Flow back stages 1 and 22040 psi, 18/64 ck, 1179 bbls to recover |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/14/2004 Report # : 3

Summary : MI Hes Frac equipment Rig up stopped rigging to let CO2 Vessels se in.MIRU Mesa wire line Perf stage #1

| End Time | Description |
|---|---|
| 12:00:00 PM | MI Rig HES Equipment had to stop rigging to let CO2 Vessels move in #s 5&6 |
| 3:00:00 PM | Move in rig up Mesa Wire Line. Pickup two 4 ft 31/8" perf guns. RIH Correlate to short joint, run to perf depth chech depth to casing coller, perf Blackhawk @ 9275-9279 pickup to 9242 check depth to casing perforate Blackhawk @ 9242-9246 all shots 3SPF 120 phasing 23 grams. .410 holes. POH no pressure change on surface all shots fired. |
| 3:00:00 PM | SIFN . CO2 unloading . H20 unloading, sand on loc. |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/13/2004 Report # : 2

Summary : set sand master &fill, set # 3 FRAC TANK FILL WITH 2% KCL, SPOT 3 C02 VESSELS START FILLING

| End Time | Description |
|---|---|
| | Enter the description here |

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/12/2004 Report # : 1 End Time Description

Summary : MI CO2 Vessels QTY 6, blade off loc.set 3 frac tanks. start filling CO2 and Frac fluid

Enter the description here

Form 3160- 5
(September 2001)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004- 0135
Expires: January 31,2004

016

## SUNDRY NOTICES AND REPORTS ON WELLS

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.***

SUBMIT IN TRIPLICATE - Other instructions on reverse side

5. Lease Serial No.: **UTU 77513**

6. If Indian, Allottee, or Tribe Name: **n/a**

7. If Unit or CA. Agreement Designation: **Prickly Pear Unit**

1. Type of Well: ☐ Oil Well ☒ Gas Well ☐ Other — CONFIDENTIAL

8. Well Name and No.: **Prickly Pear Unit Fed 12-24-12-14**

2. Name of Operator: **BILL BARRETT CORPORATION**

9. API Well No.: **43-007-30953**

3a. Address: **1099 18TH STREET, STE 2300, DENVER, CO 80202**

3b. Phone No. *(include area code)*: **(303) 312-8168**

10. Field and Pool, or Exploratory Area: **Prickly Pear Unit/Mesaverde**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*
**1271' FSL & 483' FWL**
**SWSW 24-12S-14E**

11. County or Parish, State: **Carbon County, UT**

12. CHECK APPROPRIATE BOX(S) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☐ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production ( Start/ Resume) | ☐ Water Shut-off |
| | ☐ Altering Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☒ Subsequent Report | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☒ Other **Weekly Activity Report** |
| | ☐ Change Plans | ☐ Plug and abandon | ☐ Temporarily Abandon | |
| ☐ Final Abandonment Notice | ☐ Convert to Injection | ☐ Plug back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths or pertinent markers and sands. Attach the Bond under which the work will performed or provide the Bond No. on file with the BLM/ BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notice shall be filed only after all requirements, including reclamantion, have been completed, and the operator has determined that the site is ready for final inspection.)

**WEEKLY COMPLETION ACTIVITY REPORT FROM OCTOBER 16, 2004 THROUGH OCTOBER 20, 2004. WAITING ON WEATHER TO CLEAR FOR FURTHER OPERATIONS.**

RECEIVED
OCT 26 2004
DIV. OF OIL, GAS & MINING

14. I hereby certify that the foregoing is true and correct.

Name *(Printed/ Typed)*: Tracey Fallang — Title: Permit Analyst

Signature: Tracey Fallang — Date: 22-Oct-04

THIS SPACE FOR FEDERAL OR STATE OFFICE USE

Approved by — Title — Date

Conditions of approval, if any are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. — Office

Title 18 U.S.C. Section 1001 AND Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make any department or agency of the United States any false, fictitiousor fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on reverse)

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/20/2004 Report # : 9

Summary : Flow back stages 1-4.set frac plug & pref stage#5 Price River,7620-30

| End Time | Description |
|---|---|
| 7:00:00 AM | flow back stages 1-4, FCP 400 psi, 24 ck, 19 hours flow time recover 481 bbls, avg. 25.31 BPH , 432.8 bbls left to recover, heavy mist, light trace sand, |
| 9:30:00 AM | rig Mesa Wire line , pickup 5.5" composite frac plug one 10 ft. perf gun RIH, correlate to short joint, run to setting depth set frac plug @ 7670, pull to perf depth check depth to casing coller. perforate @ 7620-7630, 3SPF 120 phasing. 23 gram shots. .410 hole POOH all shots fired. |
| 11:00:00 AM | Waiting on CO2 trucks stuck in Harmond Canyon. muddy roads |
| 1:30:00 PM | Co2 Foam Frac Price River, Start Pad No break pressure up to max pressure 6500 psi surface,. bleed off pressure try to break formation, pressure up to max pressure. shut down . flow casing to pit on 24 choke 1/2 hour to clean perfs if sand is covering perforations. shut in casing try to break formation pressure up to max pressure. shut down frac, flow casing to pit |
| 2:00:00 PM | shut in casing . try to break formation forth try, presure up to casing to max PSi 6500#. shut down . |
| 4:00:00 PM | Rig Mesa wire line . RIH with 8 ft. perf gun tage sand fill @ 7477 , 143 ft sand fill on perfs. 7620-7630 POOH shut down for day release frac crew. |
| 11:59:00 PM | Flow back stages 1-4 flow sand off Price River perforations. |

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Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/19/2004 Report # : 8

Summary : flow back stages 1-3, Rig Mesa set frac plug & perf Bluecastle,frac ,flow back

| End Time | Description |
|---|---|
| 7:00:00 AM | flowback stages 1-3, FCP 600 psi, 20/64 ck. recovered 243 bbls, 24 hours flowing, avg,10.12 BPH. 411.8 bbls left to recover. |
| 10:00:00 AM | SI Casing. Mesa Wire line, pickup 5K frac plug, two 4ft. perforating guns, RIH correlate to short joint run to setting depth check ndepth to casing coller, set frac plug @ 8420 ft. pull to perf depth Perforate Bluecastle @ 8375-8379 3 SPF. 120 phasing. 12 holes 23 gram shots, .410 hole. pickup to 8327 check depth to casing perforate @ 8327-8331, 3 spf, 120 phasing 12 holes .410 hole, 23 gram shot. POOH all shots fired. |
| 11:30:00 AM | HES CO2 Foam Frac Bluecastle. Fluid system :30# purgel III LT 70Q CO2, Break 4,788 psi, @ 12.4 BPM. Avg. Foam Rate: 35 BPM, Avg. CO2 Rate: 17 BPM, Avg. Pressure: 4050 psi, Max. Foam rate: 36.5BPM, Max. CO2 Rate: 22.5 BPM. Max. Pressure 6,500 psi, totel Fluid Pumped: 12,891 gal, Totel CO2 Pumped: 65 tons + 5 tons cooldown. 70 totel tons, Totel sand in formation 27,000 lb. (20-40 white sand) ISIP NA, Frac Gradient: NA. Screened out frac 270 sacks in wellbore 273 in formation. cut sand during 5# sand stage due to rising pressure, went to flush screened out try to push frac pressured up to Max. pressure.SD Flow back |
| 8:00:00 AM | Flow back frac. 4300 psi 18/64 ck. 502 bbl to recover, |

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/18/2004 Report # : 7

Summary : Flow back stages 1-3

| End Time | Description |
|---|---|
| 7:00:00 AM | blow backstages 1-3. FCP 975 . 24 hours flowing recovered 261 bbls, avg 10.87 BPH , 654 bbl left to recover. CO2 15 %. mid |
| 11:59:00 PM | flow stages 1-3 |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/17/2004 Report # : 6

Summary : Floa Back Stages 1-3

| End Time | Description |
|---|---|
| 7:00:00 AM | flow back stages 1-3..FCP 800 psi.18/64 ck,,recovered 329.25 bbls 16 hours flowing, avg.20.57 BPH,,015 bbl left to recover, CO2 10% |
| 11:59:00 PM | flow back stages 1-3 |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/16/2004 Report # : 5

Summary : Flow back stages 1&2, RU Mesa Wire line set frac plug and perf Bluecastle. Frac Bluecastle, flow back stages 1,2&3

| End Time | Description |
|---|---|
| 7:00:00 AM | Flow back stages 1&2 FCp 750 psi, 18/64 ck, recovered 443.75 bbls in 16 hours 27.73 BPH. 710 bbl left to recover. |
| 11:00:00 AM | Rig Mesa Wire Line pickup 5.5" frac plug 4ft gun =2ft gun=4ft gun, RIH correlate to short joint run to setting depth check depth to casing coller set comp. frac plug @ 8600 ft. pickup to perforate depth shoot lower Bluecastle @ 8568-8572 3spf 120 phasing 23 gram shot .410 hole. pick up to 8502 check depth to casing coller shot didnt go off. POOH to check problem (firing switch shorted out) repair switch run in hole correlate to short joint run to depth perforate @ 8502-8504, pickup to 8460 perforate @8460-8464 3SPF 120 phasing 23 gram shot .410 holes. POOH all shots fired. |
| 12:00:00 PM | Frac Bluecastle formation, Fluid system, 30# Purgel III lt 70Q CO2. Break @ 3800 psi 5 BPM, Avg. Foam Rate: 30 BPM, Avg. CO2 Rate: 18.5 bpm, aVG. pRESSURE: 5,160 PSI, Max Foam Rate:: 40.2 bpm, Max. CO2 Rate: 24.7 BPM, Max. Pressure: 6,471 psi, Toel Fluid Pumped: 14,075 gal, Totel CO2 Pumped: 105 tons + 5 tons cooldown totel 110 tons, totel sand pumped in formation: 45,600 lb (20/40 WHITE SAND) ISIP N/A, Frac Gradient: N/A, ( Cut sand during 5# sand stage due to rising pressure, went to flush. blender dropped off line came back up frac stopped, pressured up. tryed to push frac pressured up to max. shut down flow back frac. Screened out with 250 sacks in wellbore.411 sacks in form |
| 12:00:00 PM | flow back stages 1-2&3 18 /64 ck. 4421 psi, 535 bbls to recover, stage #3 totel bbls in well to recover 1245 bbls. |

Form 3160-5
(August 1999)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB NO. 1004-0135
Expires: November 30, 2000

017

**SUNDRY NOTICES AND REPORTS ON WELLS**

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use form 3160-3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE - Other instructions on reverse side.***

CONFIDENTIAL

| | |
|---|---|
| 1. Type of Well<br>☐ Oil Well ☒ Gas Well ☐ Other | 5. Lease Serial No.<br>UTU 77513 |
| 2. Name of Operator<br>BILL BARRETT CORPORATION<br>Contact: TRACEY FALLANG<br>E-Mail: TFALLANG@BILLBARRETTCORP.COM | 6. If Indian, Allottee or Tribe Name<br>N/A |
| 3a. Address<br>1099 18TH STREET, SUITE 2300<br>DENVER, CO 80202 | 7. If Unit or CA/Agreement, Name and/or No.<br>PRICKLY PEAR |
| 3b. Phone No. (include area code)<br>Ph: 303.312.8168 | 8. Well Name and No.<br>PRICKLY PEAR UNIT FEDERAL 12-24-12 |
| 4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*<br>Sec 24 T12S R14E SWSW 1271FSL 483FWL | 9. API Well No.<br>43-007-30953 |
| | 10. Field and Pool, or Exploratory<br>PRICKLY PEAR UNIT |
| | 11. County or Parish, and State<br>CARBON COUNTY, UT |

12. CHECK APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☐ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production (Start/Resume) | ☐ Water Shut-Off |
| ☒ Subsequent Report | ☐ Alter Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☐ Final Abandonment Notice | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☒ Other |
| | ☐ Change Plans | ☐ Plug and Abandon | ☐ Temporarily Abandon | |
| | ☐ Convert to Injection | ☐ Plug Back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be performed or provide the Bond No. on file with BLM/BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notices shall be filed only after all requirements, including reclamation, have been completed, and the operator has determined that the site is ready for final inspection.)

WEEKLY COMPLETION ACTIVITY REPORT FROM 10/21/04-10/29/04.

RECEIVED
NOV 0 8 2004
DIV. OF OIL, GAS & MINING

14. I hereby certify that the foregoing is true and correct.

**Electronic Submission #50546 verified by the BLM Well Information System**
**For BILL BARRETT CORPORATION, sent to the Moab**
**Committed to AFMSS for processing by MARIE MCGANN on 11/01/2004 ()**

| | |
|---|---|
| Name *(Printed/Typed)* TRACEY FALLANG | Title PERMIT ANALYST |
| Signature (Electronic Submission) | Date 10/29/2004 |

**THIS SPACE FOR FEDERAL OR STATE OFFICE USE**

| | |
|---|---|
| Approved By ACCEPTED | Title Division of Resources<br>Moab Field Office<br>Office<br>Date NOV 1 2004 |

Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

**** OPERATOR-SUBMITTED ** OPERATOR-SUBMITTED ** OPERATOR-SUBMITTED ****

CONFIDENTIAL

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/29/2004 Report # : 18

Summary : Nine Mile Creek running high 3 to 4 ft deep with water crews could not cross creek safely shut down operations. flow well to pit

| End Time | Description |
|---|---|
| 8:00:00 AM | Nine mile creek running high with water crews could'nt. cross safely, shut down operations for day. |
| 11:00:00 AM | flow back well to pit 24/64 ck. 1250 psi. open well |
| 1:00:00 PM | open second flow line 28/64 ck. FCP 500 |
| 11:59:00 PM | FCP 50 psi flowing on 24/64 and 28/64 ck. mid. mist, gas, no sand. |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/28/2004 Report # : 17

Summary : MIRU Mesa Wire Line. Run gauge ring tage fill.@7550 frac valve frozen could not open to full open. wait for hot oil

| End Time | Description |
|---|---|
| 11:00:00 AM | MIRU Mesa wire line, run gauge ring 3.60" to check plug back, frac valve frozen could not open all the way. call for hot oil truck unavailable. put methanol in frac valve.chop on ice with gauge ring. |
| 1:00:00 PM | broke ice block run in hole tage sand fill @ 7550. top perf @ 7620= 70 ft. over perfs. totel of 120 ft from frac plug. POOH close frac valve wait on hot oil truck. |
| 3:00:00 PM | flow well to pit 28/64 ck. 1300 psi. sent Rig crew and wire line crew home hot oil truck can not arrive to loc until 8 or 9pm. |
| 8:00:00 PM | flow well on 24/64 ck and 22/64 ck. two lines try to lift sand to surface. |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/27/2004 Report # : 16

Summary : SICP 1650, flow well 24/64 ck . SI. MI pump and tank. BOPs

| End Time | Description |
|---|---|
| 12:00:00 PM | SICP 1650. flow on 24/64 ck. flow 30 min. started to flow water, no sand dryed to a light to mid mist. |
| 12:00:00 PM | SI Casing |
| 7:00:00 PM | MI set LEED Pump and tank. Weatherford BOPS, power swivel |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/26/2004 Report # : 15

Summary : MI WSU, rig up, Weatherford foam unit.

| End Time | Description |
|---|---|
| 9:00:00 AM | MI Leed well service unit. pull to loc with Cat. roads muddy |
| 11:00:00 AM | Rig up well service unit. well had 750 psi flow well to pit unload water strong flow 24/64 ck. |
| 3:00:00 PM | JD Field service lost truck and trailer off side of hill rolled our truck float with , rig pump and tank and BOPs with Accum. Crane and pole truck to set truck back on wheels. pull BOP and Accum, up hill truck to Vernal for repairs. pump and tank still off road |
| 8:30:00 PM | pull Weatherford foam unit to loc.with Cat spot in |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/25/2004 Report # : 14

Summary : shut in

| End Time | Description |
|---|---|
| | shut in |

CONFIDENTIAL

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/24/2004 Report # : 13

Summary : shut in

| End Time | Description |
|---|---|
| | shut in |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/23/2004 Report # : 12

Summary : SI. snow , mud, rocks clean roads . pull truck to Loc with Cat. unload 300 jts 23/8 N-80

| End Time | Description |
|---|---|
| 7:00:00 PM | Gate Canyon rock slide set grader to clean road to bring tubing in. pull truck to loc with Cat. spot and unload 300 joints 23/8 N-80 on seals. |
| 7:00:00 PM | shut in |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/22/2004 Report # : 11

Summary : Shut in 0 psi.

| End Time | Description |
|---|---|
| | Enter the description here |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/21/2004 Report # : 10

Summary : Flow back stages 1-4. Rig Hes Try to Break Price River formation and frac. Max PSI no break. RIH/wire line. tage sand fill 243 ft over perfs. flow back. well died. no flow Rig down Wire line and part of HES Frac equip. ready for rig to clean out.

| End Time | Description |
|---|---|
| 8:00:00 AM | Flow back stages 1-4. FCP 225 on 26/64 ck, recovered 225 bbl. 16 hours flow time, avg. 14.06 BPH. CO2 test 15%, 207 bbl left to recover. 5PM sand slug came out of well. |
| 8:30:00 AM | Rig HES. Fill hole try to break Price River formation pressured up to 6500 psi had small bleedoff try to hold psi to break. bleed off to 5500 run psi up to max try for break no break. |
| 10:00:00 AM | Rig Mesa Wire RIH with 8ft perf gun to check for sand.243 ft, over perfs. POOH Rig down move to side of loc. |
| 12:00:00 PM | Rig down part of frac equipment move to side of loc. ready well for workover rig. |
| 4:00:00 PM | well flowing on 26/64 and 32/64 |
| 7:00:00 PM | well died no flow. SIFN |

Form 3160- 5
(September 2001)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004- 0135
Expires: January 31,2004

**SUNDRY NOTICES AND REPORTS ON WELLS**

018

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE - Other Instructions on reverse side***

5. Lease Serial No.: **UTU 77513**

6. If Indian, Allottee, or Tribe Name: **n/a**

7. If Unit or CA. Agreement Designation: **Prickly Pear Unit**

1. Type of Well: ☐ Oil Well ☒ Gas Well ☐ Other — CONFIDENTIAL

8. Well Name and No.: **Prickly Pear Unit Fed 12-24-12-14**

2. Name of Operator: **BILL BARRETT CORPORATION**

9. API Well No.: **43-007-30953**

3a. Address: **1099 18TH STREET, STE 2300, DENVER, CO 80202**

3b. Phone No. *(include area code)*: **(303) 312-8168**

10. Field and Pool, or Exploratory Area: **Prickly Pear Unit/Mesaverde**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*
**1271' FSL & 483' FWL**
**SWSW 24-12S-14E**

11. County or Parish, State: **Carbon County, UT**

12. CHECK APPROPRIATE BOX(S) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☐ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production ( Start/ Resume) | ☐ Water Shut-off |
| | ☐ Altering Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☒ Subsequent Report | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☒ Other **Weekly Activity Report** |
| | ☐ Change Plans | ☐ Plug and abandon | ☐ Temporarily Abandon | |
| ☐ Final Abandonment Notice | ☐ Convert to Injection | ☐ Plug back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths or pertinent markers and sands. Attach the Bond under which the work will performed or provide the Bond No. on file with the BLM/ BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notice shall be filed only after all requirements, including reclamantion, have been completed, and the operator has determined that the site is ready for final inspection.)

**WEEKLY COMPLETION ACTIVITY REPORT FROM OCTOBER 30, 2004 THROUGH NOVEMBER 5, 2004.**

RECEIVED
NOV 0 8 2004
DIV. OF OIL, GAS & MINING

14. I hereby certify that the foregoing is true and correct.
Name *(Printed/ Typed)*: Tracey Fallang — Title: Permit Analyst

Signature: Tracey Fallang — Date: 5-Nov-04

THIS SPACE FOR FEDERAL OR STATE OFFICE USE

Approved by — Title — Date

Conditions of approval, if any are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. — Office

Title 18 U.S.C. Section 1001 AND Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make any department or agency of the United States any false, fictitiousor fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on reverse)

# REGULATORY COMPLETION SUMMARY

CONFIDENTIAL

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/5/2004 Report # : 25

Summary : Flow back stages 3-7.

| End Time | Description |
|---|---|
| 7:00:00 AM | Flow back stages 3-7, FCP 650 psi, 22/6 ck, recovered 210 bbls, 16 hours flow time, av. 13.12 bph. 1064 bbl left to recover, CO2 test 10%. |
| 11:59:00 PM | Flow back stages 3-7 22/64 ck 650 psi |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/4/2004 Report # : 24

Summary : Flow back stages 3-6, RIH w?Wire line Perf 6908-16 4SPF. 90deg. POOH RIH W/frfac plug & perf North Horn 6791-99,POOH rig & Frac.North Horn, Wire line RH Perf 6295-6300 4SPF 90 deg phas. Flow back. MO Frac and CO2 Vessels

| End Time | Description |
|---|---|
| 7:00:00 AM | Flow back stages 3-6 FCP 700 psi. 22/64 ck. recovered 144 bbls 17 hours flowing avg.8.47 BPH. 749 bbl left to recover |
| 11:00:00 AM | .Rig Mesa Wire ine. RIH Perforate North Horn @ 6908-6916 4SPF 90 deg. phasing 23 gram shots .410 hole. POOH pickup 8 ft gon with frac plug run in hole correlate to short joint run to plug depth check depth to casing coller set frac plug @ pull up to perf depth perforate North Horn @ 6791-6799 3 spf 120 phasing .410 hole 23 gram shot. POOH all shots fired |
| 1:00:00 PM | Ri Halliburtion to Fac Stage 7 North Horn: Fluid System: 30# Purgel III LT 70Q CO2. Break @ 3613, 10 BPM. Av. Foam Rate: 29 BPM, Avg. CO2 Rate: 16.4 BPM, Avg. Pressure: 4,219 PSI, Max. Foam Rate:32.3 BPM. Max. CO2 Rate: 21.2 BPM. Max Pressure 4731 psi. Totel Fluid Pumped: 16,443 gal. Totel CO2 pumped in Formation: 122 tons (10 tons cooldown) Totel sand pumped in formation: 78,000 lb. (20/40 white sand) ISIP: 3,350 psi Frac Gradient: 0.93 psi/ft pumped 50Q Co2 with 500 fluid cap job was flushed successfully. |
| 2:30:00 PM | Rig Wire line RIH with 8 ft. gun correlate to short joint Perforate North Horn @ 6295-6300 4 SPF 90 deg. phasing.410 hole 23 grams. POOH all shots fired. |
| 2:30:00 PM | start flow back 18/64 ck. 1274 bbl to recover |

CONFIDENTIAL

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/3/2004 Report # : 23

Summary : Rig Halliburtion Frac Stage 5 Price River, Wire line frac plug and perf stage 6 U.Price River7258-66

| End Time | Description |
|---|---|
| 7:00:00 AM | FCP 0 psi, |
| 9:20:00 AM | Rig Halliburtion, Safety Meeting, Fra Stage #5 Price River 7620-30 , Fluid System:30# Purgel III LT 70Q Co2, base fluid 8.48 lb/gal. Break 4,780 psi 4.7 BPM, Avg. Foam Rate: 31.5 BPM, Avg. Co2 Rate: 18.7 BPM, Avg. Pressure: 3,693 psi, Max. Foam Rate: 35.1 BPM. Max. CO2 Rate: 20.9 bpm. Max. Pressure: 4,780 PSI, Totel fluid Pumped: 17,747 gal, Totel Co2 Pumped: 128 tons + 10 ton cooldown. Totel Sand In formation: 80,000lb. (20/40 White Sand) ISIP: 2,900 PSI, frac Gradient: 0.82 psi/ft, flush with 50Q CO2 Foam with 500 gal fluid cap. flush was pumped successfully. |
| 11:00:00 AM | Rig Mesa Wire Line. Pickup 5.5" Composite frac plug 8 ft. perf gun RIH Correlate to short joint run to setting depth check depth to casing coller set frac plug @7305 pull to perf depth perforate U.Price River @ 7258-7266 3SPF 120 phasing 23 gram shot .410 hole. POOH all shots fired. rig down off well. |
| 1:00:00 PM | Rig Frac Equipment to frac U.Price River 7258-66, Fluid System: 30# Purgel III LT 70Q CO2. Base fluid: 8.48 lb/gal. Break:4,259 PSi @ 4.7 bpm. Avg. Foam Rate: 29 BPM. Avg. CO2 rate:17.6BPM, Avg. Pressure: 5,928 PSi. Max. foam Rate: 31.8 BPM. Max. CO2 Rate: 19 BPM. Max. Pressure: 6,484 PSi, Totel Fluid Pumped: 8,008 gal. Totel CO2 Pumped: 75 tons = 10 tons cooldown, 85 totel Totel Sand in Formation: 22,000 Lb. ( 20/40 White sand) ISIP: NA frac Gradient: psi/ft. the job screened out when 5# sand hit the perfs placed 220 sacks in formation and left 230 sacks in well bore. CO2 65 tons down hole. Try to push frac pressured up to 6500 psi shut down & flow back |
| 1:40:00 PM | start flow back 18/64 choke 4200 psi. heavy sand |
| 2:00:00 PM | 1500 psi 18/64 ck no washouts mid to heavy sand |
| 3:00:00 PM | 1100 psi 18/64 ck. no washouts mid. sand recovered 60 bbls |
| 3:30:00 PM | turn over to flow watchers |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/2/2004 Report # : 22

Summary : POOH with tbg. lay down on seals. Bit X,XN nipples. ND/NUfrac head, RDMO WSE. MIRU Mesa Wire Line set CBP@ 8595 and CFP@7665

| End Time | Description |
|---|---|
| 7:00:00 AM | SICP 750 Blow down on 24/64 ck. |
| 11:00:00 AM | change out slip dies. POOH lay down 70 JOINTS X,XN nipples Bit sub and 43/4 bit. |
| 12:00:00 PM | pump top kill 35 bbls. nipple down BOPs. Nipple up 10K Well head INC. frac head. hook up flowback manifold |
| 1:00:00 PM | Rig down well service equipment. |
| 2:00:00 PM | road RIG |
| 8:30:00 PM | MI Rig up Mesa Wire Line . Set composite solid plug @ 8595, POOH pick up 5.5 CFP RIH Set @ 7675 POOH. open well to pit |

# REGULATORY COMPLETION SUMMARY

CONFIDENTIAL

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/1/2004 Report # : 21

Summary : SICP 875, set back swivel pickup tbg tage fill @ 9265, pickup swivel cleanout to 9400 ft. circ hole 1 hour, rig down swivel POOH lay down tbg.230 joints. Rig slips would'nt hold shut down

| End Time | Description |
|---|---|
| 7:00:00 AM | SICP 875 |
| 7:30:00 AM | open well 26/64 ck. rig down power swivel. |
| 8:30:00 AM | pickup tbg. off ground tage fill @ 9265 middle perfs in Blackhawk |
| 11:00:00 AM | rig power swivel drill and clean out to 9400 ft. |
| 12:00:00 PM | circ hole for one hour with foam air. rig down power swivel, rig down Weatherford Foam Unit move out. |
| 4:00:00 PM | POOH lay down 23/8 tbg. on seals 230 joints ( rig slipes started to slip on tbg. no spair on rig had to shut down before droping pipe in hole) |
| 4:00:00 PM | shut in for night |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/31/2004 Report # : 20

Summary : tally Pickup tubing. pickup power swivel, rig Weatherford Foam unit, Break circ. drill Frac plugs #4, #3, #2 and #1plug blow foam air for 1 hour SIFN

| End Time | Description |
|---|---|
| 8:00:00 AM | SICP 500 psi, ( rig crew late to start work) |
| 9:45:00 AM | Tally and pickup 23/8 EUE tubing. tage sand fill @7525 totel of 145 ft. to frac plug. 95 ft. over perfs. |
| 12:00:00 PM | pickup Weatherford power swivel. break circ with foam air. |
| 1:00:00 PM | clean out sand from 7525 to 7670 frac plug #4 drill frac plug . recovered 50 bbls fluid . no pressure change on surface after cleaning out to frac plug and drilling up plug. |
| 3:30:00 PM | pickup singles with swivel 24 joints tage @ 8420 no fill on frac plug #3 recovered 80 bbls fluid.no flow change on surface drilling up plug. |
| 5:30:00 PM | pickup singles 6 joints tage frac plug #2 U.Sego= no fill on plug drill plug no pressure change on surface drilling plug loss circ took 1 hour to start returns on surface. flowing heavy sand with foam air |
| 7:00:00 PM | pickup 5 joints with swivel tage frac plug #1 above the Blackhawk. @8750 drill plug o pressure change on surface, run two joints to make sure plug fail free. blw well with foam air for one hour to clean up for night. drain lines.( 281 joints in well.8800 feet.) |
| 8:30:00 PM | shut in for night |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 10/30/2004 Report # : 19

Summary : Rig Mesa Wire line RIH Tage fill 7550ft. 120 feet sand from frac plug. 70 ft over perfs. ND frac Tree. NU BOPs, Rig floor tally and pick up bit & tbg.

| End Time | Description |
|---|---|
| 8:00:00 AM | flow back 1-3 24/64 & 28/64 ck. FCP 50 psi. recovered 78 bbls . |
| 10:30:00 AM | rig Mesa Wire Line RIH with gauge ring. tage sand fill @ 7550. stuck gauge ring in sand worked free POOH. rig down Mesa Wire And move out. |
| 12:00:00 PM | Hot oil truck pump 50 bbl top kill on casing. nipple down frac head, nipple up BOPs, rig work floor. to pick up tbg. |
| 7:00:00 PM | pickup 43/4 smith cone bit weatherford pumpoff bit sub . one joint XN nipple 1 jt. X nipple tally and pickup 187 joints 5850 ft.. ( thd. protectors cold and hard to get off tubing and wind blowing cross threading pipe slowed pickup time.) |
| 7:00:00 PM | SIFN |

Form 3160- 5
(September 2001)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004- 0135
Expires: January 31,2004

**SUNDRY NOTICES AND REPORTS ON WELLS**

019

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE - Other Instructions on reverse side***

5. Lease Serial No.
**UTU 77513**

6. If Indian, Allottee, or Tribe Name
**n/a**

7. If Unit or CA. Agreement Designation
**Prickly Pear Unit**

1. Type of Well
☐ Oil Well ☒ Gas Well ☐ Other CONFIDENTIAL

8. Well Name and No.
**Prickly Pear Unit Fed 12-24-12-14**

2. Name of Operator
**BILL BARRETT CORPORATION**

9. API Well No.
**43-007-30953**

3a. Address
**1099 18TH STREET, STE 2300, DENVER, CO 80202**

3b. Phone No. *(include area code)*
**(303) 312-8168**

10. Field and Pool, or Exploratory Area
**Prickly Pear Unit/Mesaverde**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*
**1271' FSL & 483' FWL**
**SWSW 24-12S-14E**

11. County or Parish, State
**Carbon County, UT**

12. CHECK APPROPRIATE BOX(S) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☐ Notice of Intent | ☐ Acidize | ☐ Deepen | ☒ Production ( Start/ Resume) | ☐ Water Shut-off |
| | ☐ Altering Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☒ Subsequent Report | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☐ Other |
| | ☐ Change Plans | ☐ Plug and abandon | ☐ Temporarily Abandon | |
| ☐ Final Abandonment Notice | ☐ Convert to Injection | ☐ Plug back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths or pertinent markers and sands. Attach the Bond under which the work will performed or provide the Bond No. on file with the BLM/ BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notice shall be filed only after all requirements, including reclamantion, have been completed, and the operator has determined that the site is ready for final inspection.)

**THIS SUNDRY IS BEING SUBMITTED AS NOTIFICATION OF FIRST SALES ON 11/5/04.**

14. I hereby certify that the foregoing is true and correct.
Name *(Printed/ Typed)*
Tracey Fallang

Title Permit Analyst

Signature Tracey Fallang

Date 8-Nov-04

RECEIVED
NOV 12 2004
DIV. OF OIL, GAS & MINING

**THIS SPACE FOR FEDERAL OR STATE OFFICE USE**

| Approved by | Title | Date |
|---|---|---|
| Conditions of approval, if any are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. | Office | |

Title 18 U.S.C. Section 1001 AND Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make any department or agency of the United States any false, fictitiousor fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on reverse)

Form 3160- 5
(September 2001)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

COPY

FORM APPROVED
OMB No. 1004- 0135
Expires: January 31,2004

## SUNDRY NOTICES AND REPORTS ON WELLS

020

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE - Other Instructions on reverse side***

5. Lease Serial No.: **UTU 77513**

6. If Indian, Allottee, or Tribe Name: **n/a**

7. If Unit or CA. Agreement Designation: **Prickly Pear Unit**

1. Type of Well: ☐ Oil Well ☒ Gas Well ☐ Other — CONFIDENTIAL

8. Well Name and No.: **Prickly Pear Unit Fed 12-24-12-14**

2. Name of Operator: **BILL BARRETT CORPORATION**

9. API Well No.: **43-007-30953**

3a. Address: **1099 18TH STREET, STE 2300, DENVER, CO 80202**

3b. Phone No. *(include area code)*: **(303) 312-8168**

10. Field and Pool, or Exploratory Area: **Prickly Pear Unit/Mesaverde**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*
**1271' FSL & 483' FWL**
**SWSW 24-12S-14E**

11. County or Parish, State: **Carbon County, UT**

12. CHECK APPROPRIATE BOX(S) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☐ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production ( Start/ Resume) | ☐ Water Shut-off |
| | ☐ Altering Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☒ Subsequent Report | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☒ Other **Weekly Activity Report** |
| | ☐ Change Plans | ☐ Plug and abandon | ☐ Temporarily Abandon | |
| ☐ Final Abandonment Notice | ☐ Convert to Injection | ☐ Plug back | ☐ Water Disposal | |

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**WEEKLY COMPLETION ACTIVITY REPORT FROM NOVEMBER 6, 2004 THROUGH NOVEMBER 12, 2004.**

RECEIVED
NOV 15 2004
DIV. OF OIL, GAS & MINING

14. I hereby certify that the foregoing is true and correct.
Name *(Printed/ Typed)*: Tracey Fallang — Title: Permit Analyst

Signature: Tracey Fallang — Date: 12-Nov-04

THIS SPACE FOR FEDERAL OR STATE OFFICE USE

Approved by — Title — Date

Conditions of approval, if any are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. — Office

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(Instructions on reverse)

CONFIDENTIAL

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/12/2004 Report # : 32

Summary : TIH 5 jts Rig swivel drill on plug,POOH, RIH w/ fishen Overshot. and tubing 36 stds. dark shut down drain equipment

| End Time | Description |
|---|---|
| 7:00:00 AM | Open well to pit |
| 8:00:00 AM | Pick up 4 joints, rig up power swivel with joint |
| 10:00:00 AM | drill on frac plug made 10 inch. 2 hours |
| 12:00:00 PM | rig down power swivel POOH lost 9.56 ft. tbg pumpoff bit sub with cone bit. fish top @7663 20.40 ft of bottom joint came out. |
| 3:00:00 PM | wait on fishen tools from Weatherford. flow back kill fluid. casing on sales |
| 6:00:00 PM | sales . pickup 41/8 overshot with 23/8 grapple with cuttright on control, 3 ft extension, X overs to tubing, dart valve.RIH with |
| 8:00:00 PM | flow back kill fluid. put casing to sales for night. |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/11/2004 Report # : 31

Summary : pickup tbg. rig Foam unit & Power swivel, Drill plugs,sales

| End Time | Description |
|---|---|
| 8:30:00 AM | pickup tubing 50 joints tage @ 6240 10 ft. sand fill on kill plug |
| 9:00:00 AM | Rig up Weatherford Power swivel, rig Weatherford foam unit |
| 10:00:00 AM | break circ with foam air. clean out sant to 6250 kill plug drill plug, surface pressure came up to 1150 psi on 32/64 ck. drill and push plug 2 joint set back swivel , |
| 10:45:00 AM | pickup tbg off ground 16 joints tage @6840 no fill on frac plug. rig power swivel |
| 11:00:00 AM | pick up tbg. tage 6840 frac plug #3 no fill on plug, drill frac plug 6840 FCP 750 38/64 ck. |
| 1:00:00 PM | pickup tbg RIH Tage @ 7305 no fill on frac plug #2 drill out no flow or pressure change at surface. |
| 5:30:00 PM | RIH tage at 7665, 10 feet of sand fill on frac plug drill plug had 300 psi increase on surface plug sticking to bit torgue up, could not set weight on plug to drill. [plug would not fall free |
| 6:00:00 PM | set power swivel back POOH 2 stands. bit @ 7500ft. shut down for night |
| 11:59:00 PM | flow casing clean of air and foam . put casing to sales over night. |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/10/2004 Report # : 30

Summary : MIRU Well service Unit.MIRU Wire line, Set kill plug @ 6250, RDMO Wire line , ND Frac Head NU BOPS. PU RIH w/bit &tbg 150 jts.4700 ft.

| End Time | Description |
|---|---|
| 9:30:00 AM | Rig up well service unit |
| 1:30:00 PM | MIRU Mesa Wire Line. Late getting to loc. snow and mud. PU RIH w/ CBP correlate to short joint set composite kill plug @ 6250 sand in setting tools. POOH RD MO Mesa WIRE Line. |
| 3:00:00 PM | blw down casing 250 psi. nipple down Frac head. and flow lines, NU BOPs and flow manifold. rig work floor to run tubing. |
| 5:30:00 PM | Pickup 43/4 Smith cone Bit, Weatherford pumpoff bit sub, 1 jt. XN Nipple 1 jt X nipple 150 joints. 4700 ft. 1500 ft left to pickup. ( pull Weatherford foam unit to Loc with Cat.) |
| 5:30:00 PM | SI for night |

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Bill Barrett Corporation

# REGULATORY COMPLETION SUMMARY

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/9/2004 Report # : 29 End Time Description

Summary : production Enter the description here

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/8/2004 Report # : 28 End Time Description

Summary : production Enter the description here

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/7/2004 Report # : 27 End Time Description

Summary : production Enter the description here

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/6/2004 Report # : 26

Summary : Flow back stages 3-7

| End Time | Description |
|---|---|
| 7:00:00 AM | Flow back stages 3-7, FCP 350 psi, 22/64 ck. recovered 240 bbls 24 hours avg. 10 bph, 824 bbl left to recover, CO2 test 1%. 1009.08 mmcfd |
| 12:00:00 PM | flow back stages 3-7. |
| 12:00:00 PM | shut in well hook up production lines, |
| 3:00:00 PM | purge pipe line put casing to sales |

Form 3160- 5
(September 2001)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004- 0135
Expires: January 31,2004

**SUNDRY NOTICES AND REPORTS ON WELLS**

021

*Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.*

*SUBMIT IN TRIPLICATE--Other Instructions on reverse side*

5. Lease Serial No.
**UTU 77513**

6. If Indian, Allottee, or Tribe Name
**n/a**

7. If Unit or CA. Agreement Designation
**Prickly Pear Unit**

1. Type of Well
☐ Oil Well ☒ Gas Well ☐ Other

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8. Well Name and No.
**Prickly Pear Unit Fed 12-24-12-14**

2. Name of Operator
**BILL BARRETT CORPORATION**

9. API Well No.
**43-007-30953**

3a. Address
**1099 18TH STREET, STE 2300, DENVER, CO 80202**

3b. Phone No. *(include area code)*
**(303) 312-8168**

10. Field and Pool, or Exploratory Area
**Prickly Pear Unit/Mesaverde**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*
**1271' FSL & 483' FWL**
**SWSW 24-12S-14E**

11. County or Parish, State
**Carbon County, UT**

12. CHECK APPROPRIATE BOX(S) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☐ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production ( Start/ Resume) | ☐ Water Shut-off |
| | ☐ Altering Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☒ Subsequent Report | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☒ Other **Weekly Activity Report** |
| | ☐ Change Plans | ☐ Plug and abandon | ☐ Temporarily Abandon | |
| ☐ Final Abandonment Notice | ☐ Convert to Injection | ☐ Plug back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths or pertinent markers and sands. Attach the Bond under which the work will performed or provide the Bond No. on file with the BLM/ BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notice shall be filed only after all requirements, including reclamantion, have been completed, and the operator has determined that the site is ready for final inspection.)

**WEEKLY COMPLETION ACTIVITY REPORT FROM NOVEMBER 13, 2004 THROUGH NOVEMBER 18, 2004**
**FINAL REPORT.**

RECEIVED
NOV 22 2004
DIV. OF OIL, GAS & MINING

14. I hereby certify that the foregoing is true and correct.
Name *(Printed/ Typed)*
Tracey Fallang

Title Permit Analyst

Signature Tracey Fallang

Date 19-Nov-04

THIS SPACE FOR FEDERAL OR STATE OFFICE USE

Approved by

Title

Date

Conditions of approval, if any are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Office

Title 18 U.S.C. Section 1001 AND Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make any department or agency of the United States any false, fictitiousor fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on reverse)

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# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/18/2004 Report # : 38

Summary : flow test, kill tbg. lay down 1 jt. land tub. on hanger, ND/NU tree and flow line. swab in tbg. sales. RDMO Leed Well service, and rental equipmet.

| End Time | Description |
|---|---|
| 7:00:00 AM | FTP 70, SICP 395, Flow 263.47 MCFD, 36/64 ck. recovered 63 BBLs 15 hours, avg. 4.20 BPH, 103 BBL left to recover. |
| 8:00:00 AM | rig down power swivel. |
| 10:00:00 AM | top kill tbg 5 bbls. lay down 1 joint tbg. land tub on hanger, ND BOPs, NU Tree and flow lines |
| 11:00:00 AM | rig swab fluid level 3800 ft. made two runs start well flowing recovered kill fluid |
| 1:00:00 PM | rig down well service unit and equipment |
| 4:00:00 PM | Move Well Service Unit out with Cat. truck pump and flat tank |
| 4:00:00 PM | flow well to pit on 24/64 ck. pipe line shut repairs on compreser.160 FTP 490 SICP |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/17/2004 Report # : 37

Summary : lay down fishen tools, RIH w/ tubing to 7620, swab,

| End Time | Description |
|---|---|
| 7:00:00 AM | 12.5 hours flowing. FCP 50 psi, 213.44 MCFD, recovered 33 BBLs, avg.2.65 BPH 32 ck. |
| 8:00:00 AM | Lay down Fishen tools jars and bumper sub. (fish top 7665 washed and milled from 7659 to 7665 two washover shoes both lost carbide pinched and rolled bottom of shoe in. impression block showed casing pinched in with looks of split tubing pointing up. fish is 9 ft. 23/8 eue N-80 tbg. 33/4 Weatherford Hyd. pumpoff bit sub 2ft. ,smith cone bit 43/4" partly drilled 5 1/2" HES Composite frac plug. was set @7675 ft. |
| 8:00:00 AM | Pump 30 bbl top kill |
| 11:00:00 AM | Trip in hole with 1 joint XN nipple 1 joint X nipple tubing from derrick totel of 243 joints 7618 hanging in BOPS.(see final well report) flow casing to pit tripping in hole |
| 3:00:00 PM | first run fluid @ 3800 ft. gas cutt. made 8 swab runs pulled from 5500ft. recovered45 bbls |
| 4:00:00 PM | flow to flat tank 38/64 ck. mid to light mist. 200 FTP SICP 650 |
| 4:00:00 PM | hook up flow lines to sales , 225 FTP SICP 560 8/64 ck. 800.23 MCFD |

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# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 11/13/2004 Report # : 33

Summary : RIHw/fishen tools.rig swivel, mill on fish, POOH . no fish.

| End Time | Description |
|---|---|
| 9:00:00 AM | TIH with tubing out of derrick, with fishen tools. |
| 11:00:00 AM | Pickup powerswivel (broke HYD line off power swivel. welder to weld line on swivel) |
| 1:30:00 PM | drill and mill on fish, tage fish mill over 1 ft. pull up pulled 10,000 # OVER STRING pulled free. set down tage same place milled torque up tbg pulled 10,000# over string pulled free, try to mill over fish torque up pulled off, 8 to 10 attempted trys to milll over fish torque up could'nt make hole. hard drag for 10 to 12 feet up hole before free pipe no drag. |
| 2:20:00 PM | rig down swivel |
| 4:30:00 PM | POOH with tubing and fishen tools pump 15 bbl top kill. 244 joints with overshot and mule shoe(no fish in overshot. deep scares on out side of overshot,possible split tbg. |
| 5:00:00 PM | flow back kill fluid to light mist flow |
| 6:30:00 PM | put casing to sales separator would'nt open to sales, work on unit |
| 6:32:00 PM | sales 350 psi 40/64 ck |

Form 3160-4
(April 2004)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

BBC CONFIDENTIAL

FORM APPROVED
OMB NO. 1004-0137
Expires: March 31, 2007

022

# WELL COMPLETION OR RECOMPLETION REPORT AND LOG

5. Lease Serial No. **UTU 77513**

1a. Type of Well ☐ Oil Well ☑ Gas Well ☐ Dry ☐ Other
b. Type of Completion: ☑ New Well ☐ Work Over ☐ Deepen ☐ Plug Back ☐ Diff. Resvr,.
Other

6. If Indian, Allottee or Tribe Name

7. Unit or CA Agreement Name and No. **Prickly Pear Unit**

2. Name of Operator **BILL BARRETT CORPORATION** CONFIDENTIAL

8. Lease Name and Well No. **Prickly Pear Unit Fed 12-24**

3. Address **1099 18th Street, Suite 2300, Denver, CO 80202**
3a. Phone No. *(include area code)* **303-312-8168**

9. API Well No. **4300730953**

4. Location of Well *(Report location clearly and in accordance with Federal requirements)**
At surface **SWSW, 1271' FSL, 483' FWL**
At top prod. interval reported below **same**
At total depth **same**

10. Field and Pool, or Exploratory **Prickly Pear**

11. Sec., T., R., M., on Block and Survey or Area **24-T12S-R14E**

12. County or Parish **Carbon** 13. State **UT**

14. Date Spudded **09/03/2004**
15. Date T.D. Reached **09/26/2004**
16. Date Completed **11/18/2004** ☐ D & A ☑ Ready to Prod.
17. Elevations (DF, RKB, RT, GL)* **7795'**

18. Total Depth: MD **9496'** TVD **9946'**
19. Plug Back T.D.: MD **9400'** TVD **9400'**
20. Depth Bridge Plug Set: MD **8595'** TVD **8595'**

21. Type Electric & Other Mechanical Logs Run (Submit copy of each)
TRPL COMBO (GR/DSN/SDL AND HRI) DIPOLE SONIC & CBL/GR/CCL

22. Was well cored? ☑ No ☐ Yes (Submit analysis)
Was DST run? ☑ No ☐ Yes (Submit report)
Directional Survey? ☑ No ☐ Yes (Submit copy)

23. Casing and Liner Record *(Report all strings set in well)*

| Hole Size | Size/Grade | Wt. (#/ft.) | Top (MD) | Bottom (MD) | Stage Cementer Depth | No. of Sks. & Type of Cement | Slurry Vol. (BBL) | Cement Top* | Amount Pulled |
|---|---|---|---|---|---|---|---|---|---|
| 12-1/4" | 95/8 J-55 | 36 | 0 | 1002 | | 225 HLP | 74 | Surf (CIR) | None |
| | | | | | | 190 Premag | 39 | | |
| 7-7/8" | 51/2 L80 | 17 | 0 | 9491 | | 1850 5050Poz | 491 | 740 (CBL) | None |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

24. Tubing Record

| Size | Depth Set (MD) | Packer Depth (MD) | Size | Depth Set (MD) | Packer Depth (MD) | Size | Depth Set (MD) | Packer Depth (MD) |
|---|---|---|---|---|---|---|---|---|
| 2 3/8" | 7594' | | | | | | | |

25. Producing Intervals / 26. Perforation Record

| Formation | Top | Bottom | Perforated Interval | Size | No. Holes | Perf. Status |
|---|---|---|---|---|---|---|
| A) Mesaverde | 7258' | 8572' | 9242' - 9279' | 0.41" | 24 | Closed |
| B) North Horn | 6295' | 6916' | 8620' - 8699' | 0.41" | 24 | Closed |
| C) | | | 8460' - 8572' | 0.41" | 36 | Open |
| D) | | | 8327' - 8379' | 0.41" | 24 | Open |

27. Acid, Fracture, Treatment, Cement Squeeze, etc.

| Depth Interval | Amount and Type of Material |
|---|---|
| 9242' - 9279' | 30# Purgel III LT 70Q CO2 foam frac: 110 tons of CO2, 58,000# 20/40 White Sand, 207 bbls |
| 8620' - 8699' | 30# Purgel III LT 70Q CO2 foam frac: 141 tons of CO2, 102,000# 20/40 White Sand, 321 bbls |
| 8460' - 8572' | 30# Purgel III LT 70Q CO2 foam frac: 105 tons of CO2, 45,600# 20/40 White Sand, 260 bbls |
| 8327' - 8379' | 30# Purgel III LT 70Q CO2 foam frac: 70 tons of CO2, 27,000# 20/40 White Sand, 223 bbls |

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DEC 06 2004
DIV. OF OIL, GAS & MINING

28. Production - Interval A

| Date First Produced | Test Date | Hours Tested | Test Production → | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| 11/05/2004 | 11/21/2004 | 24 | | 0 | 280 | 63 | | | Flowing |
| **Choke Size** | **Tbg. Press. Flwg. SI** | **Csg. Press.** | **24 Hr. Rate →** | **Oil BBL** | **Gas MCF** | **Water BBL** | **Gas/Oil Ratio** | **Well Status** | |
| 32/64 | 75 | 350 | | 0 | 280 | 63 | | Open | |

28a. Production - Interval B

| Date First Produced | Test Date | Hours Tested | Test Production → | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | |
| **Choke Size** | **Tbg. Press. Flwg. SI** | **Csg. Press.** | **24 Hr. Rate →** | **Oil BBL** | **Gas MCF** | **Water BBL** | **Gas/Oil Ratio** | **Well Status** | |
| | | | | | | | | | |

*(See instructions and spaces for additional data on page 2)*

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28b. Production - Interval C

| Date First Produced | Test Date | Hours Tested | Test Production → | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | |
| **Choke Size** | **Tbg. Press. Flwg. SI** | **Csg. Press.** | **24 Hr. Rate →** | **Oil BBL** | **Gas MCF** | **Water BBL** | **Gas/Oil Ratio** | **Well Status** | |
| | | | | | | | | | |

28c. Production - Interval D

| Date First Produced | Test Date | Hours Tested | Test Production → | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | |
| **Choke Size** | **Tbg. Press. Flwg. SI** | **Csg. Press.** | **24 Hr. Rate →** | **Oil BBL** | **Gas MCF** | **Water BBL** | **Gas/Oil Ratio** | **Well Status** | |
| | | | | | | | | | |

29. Disposition of Gas *(Sold, used for fuel, vented, etc.)*

**Sold**

30. Summary of Porous Zones (Include Aquifers):

Show all important zones of porosity and contents thereof: Cored intervals and all drill-stem tests, including depth interval tested, cushion used, time tool open, flowing and shut-in pressures and recoveries.

31. Formation (Log) Markers

| Formation | Top | Bottom | Descriptions, Contents, etc. | Name | Top Meas. Depth |
|---|---|---|---|---|---|
| | | | | **Green River (marker)** | **2102'** |
| | | | | **Base Resisti** | **2409'** |
| | | | | **Uteland Butte** | **2838'** |
| | | | | **Wasatch** | **3060'** |
| | | | | **Middle Wasatch** | **4088'** |
| | | | | **North Horn** | **5168'** |
| | | | | **Price River** | **6984'** |
| | | | | **Base UPR** | **7268'** |
| | | | | **Bluecastle** | **8288'** |
| | | | | **Sego** | **8582'** |
| | | | | **Castlegate** | **8972'** |
| | | | | **Blackhawk** | **9211'** |

32. Additional remarks (include plugging procedure):

**Copies of logs already submitted.**

33. Indicate which itmes have been attached by placing a check in the appropriate boxes:

☐ Electrical/Mechanical Logs (1 full set req'd.) ☐ Geologic Report ☐ DST Report ☐ Directional Survey
☐ Sundry Notice for plugging and cement verification ☐ Core Analysis ☐ Other:

34. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records (see attached instructions)*

Name *(please print)* **Tracey Fallang** Title **Permit Analyst**

Signature **Tracey Fallang** Digitally signed by Tracey Fallang DN: CN = Tracey Fallang, C = US, O = BRC Date: 2004.12.01 16:01:26 -07'00' Date **12/01/2004**

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

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| 27. PERFORATION RECORD (cont.) | | | | |
|---|---|---|---|---|
| INTERVAL (Top/Bot-MD) | | SIZE | NO. HOLES | PERFORATION STATUS |
| 7620' | 7630' | 0.41" | 30 | Open |
| 7258' | 7266' | 0.41" | 24 | Open |
| 6908' | 6916' | 0.41" | 32 | Open (perf only, no frac) |
| 6791' | 6799' | 0.41" | 24 | Open |

| 28. ACID, FRACTURE, TREATMENT, CEMENT SQUEEZE, ETC. (cont.) | |
|---|---|
| DEPTH INTERVAL | AMOUNT AND TYPE OF MATERIAL |
| 7620' – 7630' | 30# Purgel III LT 70Q CO2 foam frac: 138 tons of CO2, 80,000# 20/40 White Sand, 264 bbls |
| 7258' – 7266' | 30# Purgel III LT 70Q CO2 foam frac: 75 tons of CO2, 22,000# 20/40 White Sand, 176 bbls |
| 6791' – 6799' | 30# Purgel III LT 70Q CO2 foam frac: 122 tons of CO2, 78,000# 20/40 White Sand, 271 bbls |

023

STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

FORM 6

# ENTITY ACTION FORM

Operator: Bill Barrett Corp

Operator Account Number: N 2165

Address: 1099 18th St Suite 2300

city Denver

state CO zip 80202

Phone Number: (303) 312-8168

**Well 1**

| API Number | Well Name | QQ | Sec | Twp | Rng | County |
|---|---|---|---|---|---|---|
| 4300730953 | Prickly Pear U Fed 12-24 | SWSW | 24 | 12S | 14E | Carbon |

| Action Code | Current Entity Number | New Entity Number | Spud Date | Entity Assignment Effective Date |
|---|---|---|---|---|
| D | 13605 | 14467 | | 12/22/2004 |

**Comments:** Correction by DOGM as no unit participating area established. nhmvd = 14467 Please amend reports to begining of production.

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**Well 2**

| API Number | Well Name | QQ | Sec | Twp | Rng | County |
|---|---|---|---|---|---|---|
| | | | | | | |

| Action Code | Current Entity Number | New Entity Number | Spud Date | Entity Assignment Effective Date |
|---|---|---|---|---|
| | | | | |

**Comments:**

**Well 3**

| API Number | Well Name | QQ | Sec | Twp | Rng | County |
|---|---|---|---|---|---|---|
| | | | | | | |

| Action Code | Current Entity Number | New Entity Number | Spud Date | Entity Assignment Effective Date |
|---|---|---|---|---|
| | | | | |

**Comments:**

**ACTION CODES:**

- **A** - Establish new entity for new well (single well only)
- **B** - Add new well to existing entity (group or unit well)
- **C** - Re-assign well from one existing entity to another existing entity
- **D** - Re-assign well from one existing entity to a new entity
- **E** - Other (Explain in 'comments' section)

Earlene Russell For DOGM

**Name (Please Print)**

Earlene Russell

**Signature**

Engineering Tech

**Title**

12/22/2004

**Date**

(5/2000)

Form 3160-5
(February 2005)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OM B No. 1004-0137
Expires: March 31, 2007

## SUNDRY NOTICES AND REPORTS ON WELLS

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160 - 3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE- Other instructions on reverse side.***

5. Lease Serial No.
**UTU 77513**

6. If Indian, Allottee or Tribe Name
**n/a**

7. If Unit or CA/Agreement, Name and/or No.
**Prickly Pear Unit**

1. Type of Well
☐ Oil Well ☑ Gas Well ☐ Other CONFIDENTIAL

8. Well Name and No.
**Prickly Pear Unit Fed 12-24-12-14**

2. Name of Operator **BILL BARRETT CORPORATION**

9. API Well No.
**43-007-30953**

3a. Address
**1099 18th Street, Suite 2300, Denver, CO 80202**

3b. Phone No. *(include area code)*
**303-312-8168**

10. Field and Pool, or Exploratory Area
**Prickly Pear Unit/Mesaverde**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*
**1271' FSL, 483' FWL, SWSW, Sec. 24-T12S-R14E**

11. County or Parish, State
**Carbon, UT**

12. CHECK APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☐ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production (Start/Resume) | ☐ Water Shut-Off |
| ☑ Subsequent Report | ☐ Alter Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☐ Final Abandonment Notice | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☑ Other **Weekly Activity Reports** |
| | ☐ Change Plans | ☐ Plug and Abandon | ☐ Temporarily Abandon | |
| | ☐ Convert to Injection | ☐ Plug Back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be performed or provide the Bond No. on file with BLM/BIA. Required subsequent reports must be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 must be filed once testing has been completed. Final Abandonment Notices must be filed only after all requirements, including reclamation, have been completed, and the operator has determined that the site is ready for final inspection.)

**WEEKLY COMPLETION ACTIVITY REPORT FROM 06/11/2005 - 06/12/05.**

RECEIVED
JUN 15 2005
DIV. OF OIL, GAS & MINING

14. I hereby certify that the foregoing is true and correct
Name *(Printed/Typed)* **Matt Barber**

Title **Contract Permit Analyst for the Bill Barrett Corp.**

Signature Matt Barber

Date **06/13/2005**

## THIS SPACE FOR FEDERAL OR STATE OFFICE USE

Approved by

Title

Date

Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Office

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

(Instructions on page 2)

# REGULATORY COMPLETION SUMMARY

Bill Barrett Corporation

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 6/12/2005 Report # : 40

Summary : SITP 500 SICP 700psi. Swab FL 2300 ft.NU/BOP. POOH retrive swab bars, TIH land on hanger, ND/NUtree. swab, sand line parted @ bars scond tme . ND/NU BOPS.

CONFIDENTIAL

| End Time | Description |
|---|---|
| 7:00:00 AM | SITP 500 SICP 700 |
| 7:15:00 AM | open tbg to pit blow down no flow. |
| 8:00:00 AM | rig swab RIH fluid level @ 2300 ft. pulled from 4500 ft. as cutt fluid. (pulling out of hole with swab sand line parted @ sinker bars. dropped bars in tubing. |
| 10:00:00 AM | blow down casing , nipple down Tree. nipple up BOP and stripper head |
| 2:00:00 PM | POOH with tbg. retrive sinker bars from X nipple |
| 3:00:00 PM | land tbg on hanger. nipple down BOPs NU Tree |
| 4:00:00 PM | cutt off 350ft. sand line. pour new rope scoket |
| 5:00:00 PM | rig swab RIH FL 2300 ft. pull from 4800 ft. gas cutt fluid. #2 run half way out with swab sand line parted scond time dropped bars in tbg. |
| 6:00:00 PM | ND Tree NU BOPs strip tbg hanger. ready to pull tbg. |
| 6:00:00 PM | SIFWE |

Well Name : **Prickly Pear #12-24-12-14** API : 43-007-30953 Area : Nine Mile Canyon

Ops Date : 6/11/2005 Report # : 39

Summary : MIRU WSU. top kill tbg. ND/NU BOPs . Strip Tbg. Hanger. lay down 26 joints, land tbg. on hanger. ND/NU Tree. swab tbg.

| End Time | Description |
|---|---|
| 7:00:00 AM | Rig up wel service unit. |
| 8:00:00 AM | blow down tbg pump top kill 10 bbl. |
| 9:00:00 AM | nipple down tree. nipple up BOPS and stripper head.rig work floor |
| 9:40:00 AM | strip tbg hanger. POOH lay down 26 joints 23/8 tbg. |
| 10:30:00 AM | land tbg on hanger ND/NU tree and flow lines |
| 11:00:00 AM | rig swab Fluid level 2700 ft.made 15 swab runs recovered 106 bbls. gas cutt fluid. SICP 375 pulled from X nipple |
| 6:00:00 PM | shut nin for night to build casing PSI. |

UIC.338.2

**Bill Barrett Corporation**

March 21, 2007

Mr. Chris Kierst
State of Utah
Division of Oil, Gas and Mining
PO Box 145801
Salt Lake City, UT 84114-5801

***RE: Prickly Pear Unit Federal 10-4 and Prickly Pear Unit Federal 12-24 Applications for Disposal***

Dear Mr. Kierst:

Bill Barrett Corporation would like to respectfully submit the two enclosed applications for water disposal as per R649-5-2, Requirements for Class II Injections Wells.

A casing test will be performed for each well as noted in the Conversion to Disposal procedures enclosed. These wells are being converted to water disposal wells as they no longer produce gas in commercial quantities.

If you require further information, please call me at 303-312-8134 or e-mail me at tfallang@billbarrettcorp.com.

Sincerely,

***BILL BARRETT CORPORATION***

Tracey Fallang
Environmental/Regulatory Analyst

Enclosures

1099 18TH STREET
SUITE 2300
DENVER, CO 80202
P 303.293.9100
F 303.291.0420

# 2.2 / 2.3

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

UIC FORM 1

# APPLICATION FOR INJECTION WELL

| | | |
|---|---|---|
| Name of Operator: Bill Barrett Corporation | Utah Account Number: N | Well Name and Number: Prickly Pear Unit Federal 12-24 |
| Address of Operator: 1099 18th Street, 2300 CITY Denver STATE CO ZIP 80202 | Phone Number: (303) 312-8134 | API Number: 4300730953 |
| Location of Well<br>Footage : 1271' FSL, 483' FWL County : Carbon<br>QQ, Section, Township, Range: SWSW 24 12S 14E State : UTAH | | Field or Unit Name: Prickly Pear<br>Lease Designation and Number: UTU-77513 |

| | | | |
|---|---|---|---|
| Is this application for expansion of an existing project? | | Yes ☑ | No ☐ |
| Will the proposed well be used for: | Enhanced Recovery? | Yes ☐ | No ☑ |
| | Disposal? | Yes ☑ | No ☐ |
| | Storage? | Yes ☐ | No ☑ |
| Is this application for a new well to be drilled? | | Yes ☐ | No ☑ |
| If this application is for an existing well, has a casing test been performed? | | Yes ☐ | No ☑ |
| Date of test: _____ | | | |

Obsolete
UIC Form 1
-See 4/11/07 revision
for most recent
version

Proposed injection interval: from 6,791 to 7,630

Proposed maximum injection: rate 2,000 bpd pressure 2,000 psig

Proposed injection zone contains oil ☐, gas ☐, and / or fresh water ☐ within ½ mile of the well.

List of attachments: Attachments as required by R649-5-2. As per 2.4 under R649-5.2, logs on file with the Division are as follows: Neutron Density and Resistivity.

**ATTACH ADDITIONAL INFORMATION AS REQUIRED BY CURRENT UTAH OIL AND GAS CONSERVATION GENERAL RULES**

I hereby certify that this report is true and complete to the best of my knowledge.

Name (Please Print) Tracey Fallang Title Environmental/Regulatory Analyst

Signature Tracey Fallang Date 3/21/2007

(5/2002)

## R649-5-2. Requirements for Class II Injection Wells Including Water Disposal, Storage and Enhanced Recovery Wells.

2. The application for an injection well shall include a properly completed UIC Form 1 and the following:

2.1. A plat showing the location of the injection well, all abandoned or active wells within a one-half mile radius of the proposed well, and the surface owner and the operator of any lands or producing leases, respectively, within a one-half mile radius of the proposed injection well. **(SEE ATTACHED MAP)**

2.2. Copies of electrical or radioactive logs, including gamma ray logs, for the proposed well run prior to the installation of casing and indicating resistivity, spontaneous potential, caliper, and porosity. **PRICKLY PEAR 12-24: COPY OF A WAVE SONIC AND A MUD LOG ARE ENCLOSED. ALL OTHER LOGS PREVIOUSLY SUBMITTED. PRICKLY PEAR 10-4: COPY OF A MUD LOG IS ENCLOSED. ALL OTHER LOGS PREVIOUSLY SUBMITTED.**

2.3. A copy of a cement bond or comparable log run for the proposed injection well after casing was set and cemented. **PRICKLY PEAR 12-24: COPY ENCLOSED. PRICKLY PEAR 10-4: COPY ALREADY ON FILE WITH THE DIVISION.**

2.4. Copies of logs already on file with the division should be referenced, but need not be refiled. **(SEE COMMENTS ON UIC FORM 1 PAGE REGARDING LOGS ALREADY SUBMITTED)**

2.5. A description of the casing or proposed casing program of the injection well and of the proposed method for testing the casing before use of the well. **(SEE WELLBORE DIAGRAM AND CONVERSION TO DISPOSAL PROCEDURES ENCLOSED)**

2.6. A statement as to the type of fluid to be used for injection, its source and estimated amounts to be injected daily. **(ENLCOSED)**

2.7. Standard laboratory analyses of: **(ENCLOSED)**

2.7.1. The fluid to be injected,

2.7.2. The fluid in the formation into which the fluid is being injected, and

2.7.3. The compatibility of the fluids.

MIT?

2.8. The proposed average and maximum injection pressures. **(ENCLOSED – SEE DOCUMENT LABELED 2.6)**

2.9. Evidence and data to support a finding that the proposed injection well will not initiate fractures through the overlying strata or a confining interval that could enable the injected fluid or formation fluid to enter any fresh water strata. **(ENCLOSED – SEE DOCUMENT LABELED 2.6)**

2.10. Appropriate geological data on the injection interval with confining beds clearly labeled, **(ENCLOSED – SEE DOCUMENT LABELED 2.10 AND ASSOCIATED MAPS)**

2.10.1. Nearby Underground Sources of Drinking Water, including the geologic formation name,

2.10.2. Lithologic descriptions, thicknesses, depths, water quality, and lateral extent;

2.10.3. Information relative to geologic structure near the proposed well that may effect the conveyance and/or storage of the injected fluids.

2.11. A review of the mechanical condition of each well within a one-half mile radius of the proposed injection well to assure that no conduit exists that could enable fluids to migrate up or down the wellbore and enter improper intervals. **N/A**

2.12. An affidavit certifying that a copy of the application has been provided to all operators, owners, and surface owners within a one-half mile radius of the proposed injection well. **(ENCLOSED)**

**From:** "Tracey Fallang" <tfallang@billbarrettcorp.com>
**To:** <chriskierst@utah.gov>
**Date:** 03/30/2007 2:14:33 PM
**Subject:** revised UIC form - Prickly Pear 12-24

---

From: LEIF FALLANG [mailto:fallang@comcast.net]
Sent: Friday, March 30, 2007 2:12 PM
To: Tracey Fallang
Subject: IMG.pdf - Adobe Reader

**From:** Chris Kierst
**To:** Tracey Fallang
**Subject:** Re: revised UIC form - Prickly Pear 12-24

Tracey,
I talked with one of our managers and he said that whet you have sent and with my hand amending, dating and initialing of the original should suffice to document the correction adequately so no new UIC Form 1 is necessary.

>>> "Tracey Fallang" <tfallang@billbarrettcorp.com> 03/30/2007 2:13 PM >>>

---

From: LEIF FALLANG [mailto:fallang@comcast.net]
Sent: Friday, March 30, 2007 2:12 PM
To: Tracey Fallang
Subject: IMG.pdf - Adobe Reader

Corrected UIC Form 1 — after conversation w/ Tracey Fallang on 3/30/07

See corrected UIC Form 1 (rec'd. on 4/12/07). *New proposed injection interval 6295-7630

DE
DIV

UIC FORM 1

**APPLI**

| | | |
|---|---|---|
| Name of Operator: Bill Barrett Corporation | N | Prickly Pear Unit Federal 12-24 |
| Address of Operator: 1099 18th Street, 2300 CITY Denver STATE CO ZIP 80202 | Phone Number: (303) 312-8134 | API Number: 4300730953 |
| Location of Well: Footage : 1271' FSL, 483' FWL; QQ, Section, Township, Range: SWSW 24 12S 14E; County : Carbon; State : UTAH | | Field or Unit Name: Prickly Pear; Lease Designation and Number: UTU-77513 |

| | | | |
|---|---|---|---|
| Is this application for expansion of an existing project? | | Yes ☑ | No ☐ |
| Will the proposed well be used for: | Enhanced Recovery? | Yes ☐ | No ☑ |
| | Disposal? | Yes ☑ | No ☐ |
| | Storage? | Yes ☐ | No ☑ |
| Is this application for a new well to be drilled? | | Yes ☐ | No ☑ |
| If this application is for an existing well, has a casing test been performed? | | Yes ☐ | No ☑ |
| Date of test: _____ | | | |

Proposed injection interval: from 6,791 to 7,630

Proposed maximum injection: rate 2,000 bpd pressure 2,000 psig

Proposed injection zone contains oil ☐, gas ☐, and / or fresh water ☐ within ½ mile of the well.

List of attachments: Attachments as required by R649-5-2. As per 2.4 under R649-5.2, logs on file with the Division are as follows: Neutron Density and Resistivity.

**ATTACH ADDITIONAL INFORMATION AS REQUIRED BY CURRENT UTAH OIL AND GAS CONSERVATION GENERAL RUL**

I hereby certify that this report is true and complete to the best of my knowledge.

Name (Please Print) Tracey Fallang Title Environmenta

Signature Tracey Fallang Date 3/21/2007

(5/2002)

Corrected UIC Form 1

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

UIC FORM 1

# APPLICATION FOR INJECTION WELL

| Name of Operator | Utah Account Number | Well Name and Number |
|---|---|---|
| Bill Barrett Corporation | N | Prickly Pear Unit Federal 12-24 |
| **Address of Operator** | **Phone Number** | **API Number** |
| 1099 18th Street, 2300 CITY Denver STATE CO ZIP 80202 | (303) 312-8134 | 4300730953 |
| **Location of Well** | | **Field or Unit Name** |
| Footage : 1271' FSL, 483' FWL County : Carbon | | Prickly Pear |
| QQ, Section, Township, Range: SWSW 24 12S 14E State : UTAH | | **Lease Designation and Number** UTU-77513 |

| | | | |
|---|---|---|---|
| Is this application for expansion of an existing project? | | Yes ☑ | No ☐ |
| Will the proposed well be used for: | Enhanced Recovery? | Yes ☐ | No ☑ |
| | Disposal? | Yes ☑ | No ☐ |
| | Storage? | Yes ☐ | No ☑ |
| Is this application for a new well to be drilled? | | Yes ☐ | No ☑ |
| If this application is for an existing well, has a casing test been performed? | | Yes ☐ | No ☑ |
| Date of test: _____ | | | |

Proposed injection interval: from 6,791 to 7,630

Proposed maximum injection: rate 2,000 bpd pressure 2,000 psig

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List of attachments: Attachments as required by R649-5-2. As per 2.4 under R649-5.2, logs on file with the Division are as follows: Neutron Density and Resistivity.

**ATTACH ADDITIONAL INFORMATION AS REQUIRED BY CURRENT UTAH OIL AND GAS CONSERVATION GENERAL RULES**

I hereby certify that this report is true and complete to the best of my knowledge.

Name (Please Print) Tracey Fallang Title Environmental/Regulatory Analyst

Signature Tracey Fallang Date 3/21/2007

(5/2002)

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

UIC FORM 1

# APPLICATION FOR INJECTION WELL

| | | |
|---|---|---|
| Name of Operator: Bill Barrett Corporation | Utah Account Number: N | Well Name and Number: Prickly Pear Unit Federal 12-24 |
| Address of Operator: 1099 18th Street, 2300 CITY Denver STATE CO ZIP 80202 | Phone Number: (303) 312-8134 | API Number: 4300730953 |
| Location of Well<br>Footage : 1271' FSL, 483' FWL<br>QQ, Section, Township, Range: SWSW 24 12S 14E<br>County : Carbon<br>State : UTAH | | Field or Unit Name: Prickly Pear<br>Lease Designation and Number: UTU-77513 |

| | | | |
|---|---|---|---|
| Is this application for expansion of an existing project? | | Yes ☑ | No ☐ |
| Will the proposed well be used for: | Enhanced Recovery? | Yes ☐ | No ☑ |
| | Disposal? | Yes ☑ | No ☐ |
| | Storage? | Yes ☐ | No ☑ |
| Is this application for a new well to be drilled? | | Yes ☐ | No ☑ |
| If this application is for an existing well, has a casing test been performed? | | Yes ☒ | No ☑ |

Date of test: _____

No, not yet as per Tracey Fallang 3/30/07

Proposed injection interval: from 6,791 to 7,630

Proposed maximum injection: rate 2,000 bpd pressure 2,000 psig

Proposed injection zone contains oil ☐, gas ☐, and / or fresh water ☐ within ½ mile of the well.

List of attachments: Attachments as required by R649-5-2. As per 2.4 under R649-5.2, logs on file with the Division are as follows: Neutron Density and Resistivity.

**ATTACH ADDITIONAL INFORMATION AS REQUIRED BY CURRENT UTAH OIL AND GAS CONSERVATION GENERAL RULES**

I hereby certify that this report is true and complete to the best of my knowledge.

Name (Please Print) Tracey Fallang Title Environmental/Regulatory Analyst

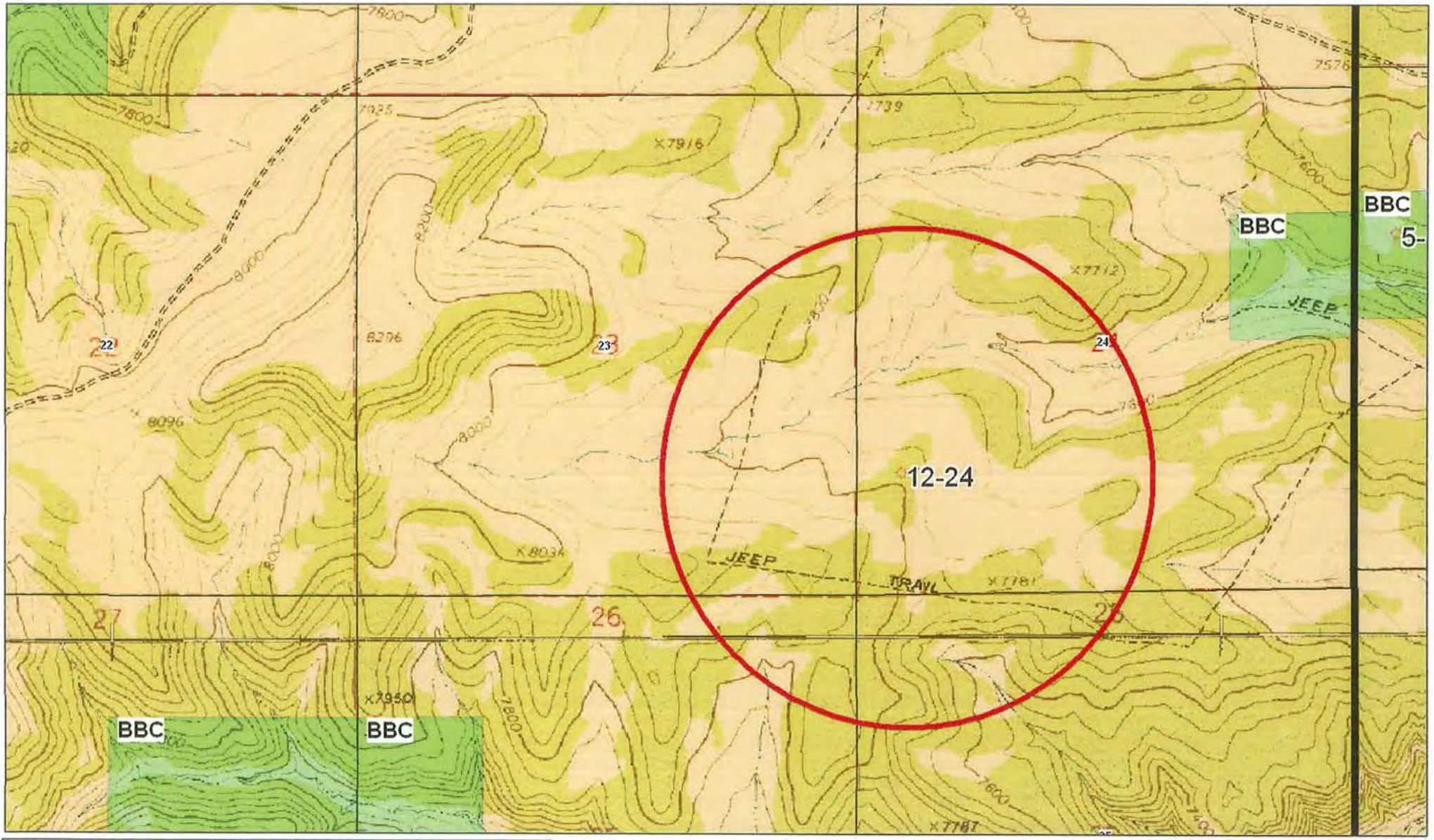
Signature Tracey Fallang Date 3/21/2007

(5/2002)

# 2.1

# Prickly Pear 12-24

Surface Ownership and 1/2 Mile Radius




| FED Surface Owner | STATE Surface Owner | FEE Surface Owner |
|---|---|---|
| Region | Region | Region |

**Bill Barrett Corporation**

Prickly Pear 12-24

API 4300730953

NWSW Sec 24 T12S - R14E

West Tavaputs Field

Carbon County, Utah


**Bill Barrett Corporation**

## Township 12 South, Range 14 East, SLM
## Carbon County, UTAH
## 03/19/2007

**Injection Well 1/2 Mile Buffer**

**UTU-084619 - PENDING**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Petro Canada Resources (USA) Inc*

**UTU-077059**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Bill Barrett Corporation 100%*

**UTU-077513**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Bill Barrett Corporation 100%*

**UTU-077060**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Bill Barrett Corporation 100%*

**UTU-069095**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Bill Barrett Corporation 100%*

**UTU-073666**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator:*
*Surface down to a depth stratigraphic equivalent of forty feet below the base of the "C" Shoal marker found at a subsurface depth of 5,340 feet, as shown on the electric log for the Chandler West River Bend 3-12-10-15 well locate in the NW/4 of Sec. 12, T10S,R15E, SLM, Duchesne County, Utah*

| | |
|---|---|
| *Bill Barrett Corporation* | *52.50%* |
| *Dominion Exploration & Production Inc.* | *25.00%* |
| *EOG Resources Inc.* | *22.50%* |

*From a depth stratigraphic equivalent of forty feet below the base of the "C" Shoal marker found at a subsurface depth of 5,340 feet, as shown on the electric log for the Chandler West River Bend 3-12-10-15 well locate in the NW/4 of Sec. 12, T10S,R15E, SLM, Duchesne County, Utah down to a depth stratigraphic equivalent depth of 9,691 feet as found in the Fasselin 5-19 well located in Sec. 19, T12S, R15E, SLM, Carbon County, Utah*

| | |
|---|---|
| *Bill Barrett Corporation* | *26.25%* |
| *Dominion Exploration & Production Inc.* | *73.75%* |

*Below a depth stratigraphic equivalent of 9,691 feet as found in the Fasselin 5-19 well located in Sec. 19, T12S, R15E, SLM, Carbon County, Utah*

| | |
|---|---|
| *Dominion Exploration & Production Inc.* | *73.75%* |
| *EOG Resources Inc.* | *26.25%* |

# 2.5

**16" Conductor** 40'

CBL TOC: 750'

**9-5/8" 36# J-55 STC Surface Casing**

| | | |
|---|---|---|
| | 9-5/8" Float Collar | 954.46' |
| 23 jts | 9-5/8" 36# J-55 STC | 1,002.00' |
| | 12-1/4" Surface Hole | 1,005' |

**9-5/8" Surface Casing Cementing (09-04-04)**

| | | | | | | |
|---|---|---|---|---|---|---|
| **Lead:** | 225 sxs | 74 bbls | HL Prem | 1.85 ft3/sx | 12.7 ppg | 2% CaCl2 + 0.25 pps Flocele |
| **Tail:** | 190 sxs | 39 bbls | AG-300 | 1.15 ft3/sx | 15.8 ppg | 2% CaCl2 + 0.25 pps Flocele |

**Displace:** Bumped plug. Full returns. Circulated 40 bbls cement to pit. Floats held.

**TUBING DETAIL AS OF 11-17-04**

| | | | |
|---|---|---|---|
| | KB Elevation | 14.00' | |
| 6 | 2-3/8" 8rd Tubing Hanger | 0.80' | 14.00' |
| 5 | 240 jts 2-3/8" 4.7# N-80 8rd EUE Tubing | 7,513.94' | 14.80' |
| 4 | 2-3/8" 8rd "XN" Nipple (ID: 1.875") | 1.15' | 7,528.74' |
| 3 | 1 jt 2-3/8" 4.7# N-80 8rd EUE Tubing | 31.15' | 7,529.89' |
| 2 | 2-3/8" 8rd "X" Nipple (ID: 1.791") | 1.35' | 7,561.04' |
| 1 | 1 jt 2-3/8" 4.7# N-80 8rd EUE Tubing | 31.60' | 7,562.39' |
| | **END OF TUBING** | **7,593.99'** | **7,593.99'** |

| | | | |
|---|---|---|---|
| | TOP OF FISH | 7,665' | |
| | Split 2-38" 4.7# N-80 8rd EUE | 9.56' | 7,665.00' |
| | 3-3/4" Weatherford Hydraulic PO Sub | 1.80' | 7,674.56' |
| | 4-3/4" STC Rock Bit | 0.60' | 7,676.36' |
| | 5-1/2" HEC Composite Frac Plug | 2.42' | 7,676.96' |
| | **BOTTOM OF FISH** | **14.38'** | **7,679.38'** |

| | | | | | | |
|---|---|---|---|---|---|---|
| 3-1/8" guns: 23g; 0.41"; 90°; 4 spf | 20 shots | 5' | 6,295' | 6,300' | **Limited Entry Interval - No Treatment** | |
| 3-1/8" guns: 23g; 0.41"; 120°; 3 spf | 24 shots | 8' | 6,791' | 6,799' | 78,000# 20/40 | 392 bbls<br>FG: 0.93 psi/ft |
| 3-1/8" guns: 23g; 0.41"; 90°; 4 spf | 32 shots | 8' | 6,908' | 6,916' | **Limited Entry Interval - No Treatment** | |
| 3-1/8" guns: 23g; 0.41"; 120°; 3 spf | 24 shots | 8' | 7,258' | 7,266' | 22,000# 20/40 | 183 bbls<br>NA |
| 3-1/8" guns: 23g; 0.41"; 120°; 3 spf | 30 shots | 10' | 7,620' | 7,630' | 80,000# 20/40 | 362 bbls<br>FG: 0.82 psi/ft |
| 3-1/8" guns: 23g; 0.41"; 120°; 3 spf | 12 shots<br>12 shots | 4'<br>4' | 8,327'<br>8,375' | 8,331'<br>8,379' | 27,300# 20/40 | 307 bbls<br>NA |
| 3-1/8" guns: 23g; 0.41"; 120°; 3 spf | 12 shots<br>6 shots<br>12 shots | 4'<br>2'<br>4' | 8,460'<br>8,502'<br>8,568' | 8,464'<br>8,504'<br>8,572' | 41,100# 20/40 | 335 bbls<br>NA |
| 3-1/8" guns: 23g; 0.41"; 120°; 3 spf | 12 shots<br>12 shots | 4'<br>4' | 8,620'<br>8,695' | 8,624'<br>8,699' | 102,000# 20/40 | 434 bbls<br>FG: 0.78 psi/ft |
| 3-1/8" guns: 23g; 0.41"; 120°; 3 spf | 12 shots<br>12 shots | 4'<br>4' | 9,242'<br>9,275' | 9,246'<br>9,279' | 58,000# 20/40 | 326 bbls<br>FG: 0.91 psi/ft |

| | | | | |
|---|---|---|---|---|
| | | | | |
| 132 tons CO2 | ISIP: 3,350 psi | 70Q CO2 Foam Frac North Horn Interval 07. | | |
| CBP: 6,840' | 11/03/04 | | | |
| | | | | |
| 85 tons CO2 | NA | 70Q CO2 Foam Frac U Price River Interval 06. Screaned out at | | |
| CBP: 7,305' | 11/02/04 | 6,484 psi in 5 ppg stage. | | |
| 125 tons CO2 | ISIP: 2,900 psi | 70Q CO2 Foam Frac Price River Interval 05. | | |
| CBP: 7,675' | 11/02/04 | | | |
| 70 tons CO2 | NA | 70Q CO2 Foam Frac Blue Castle Interval 04. Screaned out at 6,500 | | |
| CBP: 8,420' | 10/18/04 | psi in 5 ppg stage. | | |
| 105 tons CO2 | NA | 70Q CO2 Foam Frac Blue Castle Interval 03. Screaned out at 6,217 | | |
| CBP: 8,600' | 10/15/04 | psi in 5 ppg stage. | | |
| 141 tons CO2 | ISIP: 2,980 psi | 70Q CO2 Foam Frac U. Sego Interval 02 | | |
| CBP: 8,750' | 10/15/04 | | | |
| 110 tons CO2 | ISIP: 4,390 psi | 70Q CO2 Foam Frac Blackhawk Interval 01 | | |
| | 10/15/04 | | | |

TOF @7,665'

CIBP @8,595'

PBTD: 9,400'

**5-1/2" 17# L-80 LTC Production Casing**

| | | |
|---|---|---|
| | 5-1/2" Super Seal II FC | 9,448.76' |
| 228 jts | 5-1/2" 17 L-80 LTC | 9,491' |
| | TD 7-7/8" Production Hole | 9,496' MD |

MW: 9.8 ppg

**Cement 5-1/2" Production Casing (09-29-04)**

| | | | | | |
|---|---|---|---|---|---|
| **Lead:** | 1,850 sxs | 491 bbls | 50/50 Poz | 1.49 ft3/sx | water: 7.1 gal/sx |
| | 13.4 ppg | 2% gel + 3% Kcl + 0.75% Halad-322 + 0.2% FWCA | | | |

**Displace:** Bumped plug. Floats held. Good returns.

# Bill Barrett Corporation

| | |
|---|---|
| **WELL:** | **Prickly Pear 12-24-12-14** |
| **LOCATION:** | NWSW 10 12S 14E<br>FSL: 1,271' FWL: 483' GL: 7,793' KB: 7,808' |
| **FORMATION:** | **Blue Castle, Price River & North Horn** |
| **API #:** | **43-007-309530000** |
| **Field:** | **West Tavaputs** |
| **CLASSIFICATION:** | |
| **CURRENT STATUS:** | **Shut-in Gas Well** |

**WI:** 100.00%
**NRI:**

**Spud:** 09/03/04 **Rig:** Patterson #77
**TD:** 09/26/04
**RR:** 09/29/04
**1st Sales:** 11/05/04
**Completed:** 11/18/04

**TUBULAR DATA**

| Type | Size | Weight | Grade | Top | Bottom | Burst | Collapse |
|---|---|---|---|---|---|---|---|
| Surface | 9 5/8" | 36.0 ppf | J-55 | 0 | 1,002' | 3,520 psi | 2,020 psi |
| Production | 5 1/2" | 17.0 ppf | L-80 | 0 | 9,491' | 7,740 psi | 6,290 psi |
| Tubing | 2 3/8" | 4.7 ppf | N-80 | 0 | 7,594' | 11,200 psi | 11,780 psi |

| | | ID | Drift | Length | | Capacity |
|---|---|---|---|---|---|---|
| 5 1/2" | 17.0 ppf L-80 | 4.892" | 4.767" | 9,491' | 0.0232 bpf | 221 bbls |
| 2 3/8" | 4.7 ppf N-80 | 1.995" | 1.901" | 7,594' | 0.0039 bpf | 29 bbls |
| 2 3/8" | 5 1/2" Annulus | | | 7,594' | 0.0178 bpf | 135 bbls |

**DEVIATION SURVEY**

| MD | Angle | Azmuth | TVD | North | East | VS | DLS |
|---|---|---|---|---|---|---|---|
| 432' | 0.50 deg | | | | | | |
| 930' | 0.75 deg | | | | | | |
| 1,993' | 0.50 deg | | | | | | |
| 2,987' | 0.50 deg | | | | | | |
| 4,070' | 0.50 deg | | | | | | |
| 5,030' | 1.25 deg | | | | | | |
| 5,382' | 1.50 deg | | | | | | |
| 6,276' | 1.50 deg | | | | | | |
| 8,322' | 2.25 deg | | | | | | |
| 8,703' | 4.00 deg | | | | | | |
| 9,097' | 5.00 deg | | | | | | |
| 9,236' | 5.75 deg | | | | | | |

**Bill Barrett Corporation**

# Prickly Pear 12-24-12-14

NWSW Sec 24 T12S-R14E, Carbon County, UT

**Surface Casing:** 9-5/8" 36# J-55 STC @ 1,002' Cemented to surface
**Production Liner:** 5-1/2" 17# L-80 LTC @ 9,491 Cemented w/1,850 sx

PBTD: 9,400' (Fish @ 7,665'), KB Elevation: 7,808', GL Elevation: 7,793'

## Conversion to Disposal

1. Note: Water in the context of this procedure will be either clean produced water or 3% KCl water. Any water will require biocide as a precaution.

2. MIRU workover rig. Set tanks and fill with water. Using rig pump kill backside & tubing with water. ND WH & NU BOPE

3. TOOH w/production tubing. PU bit & scraper and TIH to top of fish at 7,665'. TOOH.

4. TIH w/cmt retainer to 7,650'. Establish injection and cement squeeze w/20sx. Sting out of retainer and circulate hole.

5. TOOH w/tubing. PU bit & scraper and TIH to top of retainer at 7,650'. TOOH.

6. PU RBP and Baker Hornet PKR w/bypass valve. TIH and set RBP at +/-7,640' PU and set PKR at +/-7,610'.

7. MIRU Halliburton. Pressure test surface lines to 6,000 psig. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 7,620 – 30' 3 spf 30 shots)

8. Release PKR and PU RBP. PU & set RBP at +/-7,275'. PU & set PKR at +/-7,245'.

9. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 7,258 – 66' 3 spf 24 shots)

10. Release PKR and PU RBP. PU & set RBP at +/-6,930'. PU & set PKR at +/-6,900'.

11. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 6,908 – 16' 4 spf 32 shots)

12. Release PKR and PU RBP. PU & set RBP at +/-6,810'. PU & set PKR at +/-6,780'.

13. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 6,791 – 99' 3 spf 24 shots)

14. Release PKR and PU RBP. PU & set RBP at +/-6,310'. PU & set PKR at +/-6,280'.

15. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 6,295 – 300' 4 spf 20 shots)

16. RDMO Halliburton.

17. Release PKR and PU RBP. TOOH w/tubing, PKR & RBP.

18. Redress PKR & TIH w/WL re-entry guide, tail joint, Hornet packer, 1.78" XN profile nipple, on-off tool, 1.81" X profile nipple and tubing. Set packer at +/- 6,230'.

19. Sting out of on-off tool and circulate annulus w/inhibited water. Sting into on-off tool.

20. Land tubing and ND BOPE & NU WH.

21. Set plug in XN nipple and pressure test tubing to 3,000 psig. Hold pressure for 30 minutes.

22. Retrieve profile plug.

23. Pressure test backside annulus to 500 psig. Record pressure test on Barton chart recorder for 30 minutes at stabilizing. Send chart to Denver: Attn Chuck Maybee. Bleed off backside pressure.

24. RDMO workover rig. Turn well over to production group.

Total Acid: 2,500 gal 7-1/2% HCl double inhibited at 150 deg F

C.A.Maybee
2/20/2007

Attachments: Wellbore Schematic

# 2.6

# Bill Barrett Corporation

West Tavaputs Field SWD Well Application

**Maximum Allowable Surface Pressure Calculations**
**Based on Observed Fracture Gradients**

Water SG = 1.02 Gradient = 0.4417 psi/ft

Prickly Pear Federal 10-4

| Depth (ft) | Observed ISIP (psig) | Calculated Btm Hole (psig) | Resulting Frac Grad (psi/ft) |
|---|---|---|---|
| 4772 | 2220 | 4327.6 | 0.907 |
| 4964 | 2600 | 4792.4 | 0.965 |
| 5450 | 3030 | 5437.0 | 0.998 |
| 6700 | 4120 | 7079.1 | 1.057 |
| 6890 | 4100 | 7143.0 | 1.037 |
| 7180 | 3910 | 7081.1 | 0.986 |
| 7550 | 3910 | 7244.5 | 0.960 |

Requested Max Surface Pressure = 2000 psig

Prickly Pear 12-24-12-14

| Depth (ft) | Observed ISIP (psig) | Calculated Btm Hole (psig) | Resulting Frac Grad (psi/ft) | |
|---|---|---|---|---|
| 6295 | No Treatment | | | |
| 6791 | 3350 | 6349.3 | 0.935 | |
| 6908 | No Treatment | | | |
| 7620 | 2900 | 6265.4 | 0.822 | |
| 8620 | 2980 | 6787.1 | 0.787 | Below |
| 9242 | 4390 | 8471.8 | 0.917 | Fish @ 7665' |

Requested Max Surface Pressure = 2000 psig

ISIP Data collected during initial completion treatments

Calculated Bottom Hole Pressure = ISIP + 0.4417 x De
Resulting Frac Gradient = Calculated Btm Hole Pressu

Requested Max Surface Pressure < 90% x ISIP
Anticipated Avg Surface Pressure = 75% x Max Surfac

Anticipated Avg Disposal Rate = 400 bwpd / well
Requested Maximum Disposal Rate = 2000 bwpd / wel

This info is more appropriate to satisfy 2.9 partly (but not fully). calculated

4-3-06

# Bill Barrett Corporation

## West Tavaputs Field SWD Well Application

**Maximum Allowable Surface Pressure Calculations**
**Based on Observed Fracture Gradients**

Water SG = 1.02 Gradient = 0.4417 psi/ft

Prickly Pear Federal 10-4

| Depth (ft) | Observed ISIP (psig) | Calculated Btm Hole (psig) | Resulting Frac Grad (psi/ft) |
|---|---|---|---|
| 4772 | 2220 | 4327.6 | 0.907 |
| 4964 | 2600 | 4792.4 | 0.965 |
| 5450 | 3030 | 5437.0 | 0.998 |
| 6700 | 4120 | 7079.1 | 1.057 |
| 6890 | 4100 | 7143.0 | 1.037 |
| 7180 | 3910 | 7081.1 | 0.986 |
| 7550 | 3910 | 7244.5 | 0.960 |

Requested Max Surface Pressure = 2000 psig

Prickly Pear 12-24-12-14

| Depth (ft) | Observed ISIP (psig) | Calculated Btm Hole (psig) | Resulting Frac Grad (psi/ft) | |
|---|---|---|---|---|
| 6295 | No Treatment | | | |
| 6791 | 3350 | 6349.3 | 0.935 | |
| 6908 | No Treatment | | | |
| 7620 | 2900 | 6265.4 | 0.822 | |
| 8620 | 2980 | 6787.1 | 0.787 | Below |
| 9242 | 4390 | 8471.8 | 0.917 | Fish @ 7665' |

Requested Max Surface Pressure = 2000 psig

ISIP Data collected during initial completion treatments

Calculated Bottom Hole Pressure = ISIP + 0.4417 x Depth
Resulting Frac Gradient = Calculated Btm Hole Pressure / Depth

Requested Max Surface Pressure < 90% x ISIP
Anticipated Avg Surface Pressure = 75% x Max Surface Pressure

Anticipated Avg Disposal Rate = 400 bwpd / well
Requested Maximum Disposal Rate = 2000 bwpd / well

# 2.7

.46 psi/ft

90,000 lb 2.95 #@ 4772'

2000

195

10%-
15%-
20%-
25%-

1327 psi max pressure

1.065 SG gas

10%
25%

3,895 bhp 10%
3,461 @ 20%

bottomhole pressure

1,700 # Surface pressure

@ 90% @ worst case

90,000 mg/l

Champion Technologies

# Saturation Index Calculations

*Based on Tomson-Oddo Model; $CO_2$ in Brine*

4-Mar-2007

BWPD $_{TOTAL}$ = 315.74

Wasatch - Mesa Verde

## Prickly Pear

| Component | 02-25 | 03-28D | 05-13 | 05-16 | 05-19 | 07-16 | 07-28D | 07-33D | 09-18D | 10-04 (BAD SAMPLE) | 13-04 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| BWPD | 0.01 | 14.86 | 0.01 | 3.09 | 0.01 | 0.01 | 35.43 | 0.01 | 0.01 | 0.01 | 0.01 |
| Calcium, $Ca^{+2}$ mg/l | 3,976 | 4,548 | 3,892 | 3,628 | 1 | 921 | 3,916 | 1 | 1 | 1 | 3,904 |
| Magnesium, $Mg^{+2}$ mg/l | 2,654 | 671 | 1,582 | 826 | | 501 | 1,912 | | | | 2,352 |
| Barium, $Ba^{+2}$ mg/l | 0 | 0 | 0 | 0 | | 0 | 0 | | | | 0 |
| Strontium, $Sr^{+2}$ mg/l | 0 | 0 | 0 | 0 | | 0 | 0 | | | | 0 |
| Iron, $Fe^{+3}$ mg/l | 43 | 1 | 183 | 21 | | 56 | 11 | | | | 92 |
| Manganese, $Mn^{+2}$ mg/l | | | | | | | | | | | |
| Sodium, $Na^{+1}$ mg/l | 12,049 | 17,749 | 18,867 | 11,316 | | 10,907 | 16,701 | | | | 16,576 |
| Chloride, $Cl_2$ mg/l | 32,340 | 35,800 | 39,580 | 24,900 | | 18,760 | 36,760 | | | | 38,120 |
| Carbonate, $CO_3^{-2}$ mg/l | 0 | 0 | 0 | 0 | | 0 | 0 | | | | 0 |
| Bicarbonate, $HCO_3^{-1}$ mg/l | 866 | 1,086 | 976 | 937 | | 874 | 1,052 | | | | 930 |
| Sulfate, $SO_4^{-2}$ mg/l | 693 | 1,273 | 603 | 1,128 | | 868 | 1,200 | | | | 903 |
| Total Dissolved Solids mg/l | 52,621 | 61,128 | 65,683 | 42,756 | | 32,887 | 61,552 | | | | 62,877 |
| pH | 6.79 | 6.80 | 7.00 | 6.96 | | 7.06 | 6.72 | | | | 6.59 |
| $CO_2$ in Brine mg/l | 300 | 300 | 300 | 300 | | 300 | 300 | | | | 300 |
| $H_2S$ in Brine mg/l | 10.0 | 1.0 | | 1.0 | | 1.0 | 2.0 | | | | 3.0 |
| Ionic Strength | 1.16 | 1.21 | 1.31 | 0.88 | | 0.61 | 1.27 | | | | 1.31 |
| Temperature °F | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 |
| Pressure psia | 100 | 100 | 100 | 100 | 100 | 1 | | | | | |

Note: The suspect 12-24 well connate waters are not being tested yet.
Note: we need interpretations & Rw info from this!
Water Analyses

### Tomson-Oddo Saturation Index

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | -0.20 | 0.05 | -0.13 | -0.08 | | -0.5 | | | | | |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | N/A | N/A | N/A | | N/A | | | | | |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | N/A | N/A | N/A | | N/A | | | | | |
| Anhydrite; $CaSO_4$ | N/A | N/A | N/A | N/A | | N/A | | | | | |
| Barite; $BaSO_4$ | N/A | N/A | N/A | N/A | | N/A | | | | | |
| Celestite; $SrSO_4$ | N/A | N/A | N/A | N/A | | N/A | | | | | |

### P(Pounds Per)T(Thousand)B(Barrels)

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | N/A | 34.1 | N/A | N/A | | N/A | | | | | |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | N/A | N/A | N/A | | N/A | | | | | |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | N/A | N/A | N/A | | N/A | | | | | |
| Anhydrite; $CaSO_4$ | N/A | N/A | N/A | N/A | | N/A | | | | | |
| Barite; $BaSO_4$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |
| Celestite; $SrSO_4$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |

Champion Technologies

# Saturation Index Calculations

*Based on Tomson-Oddo Model; $CO_2$ in Brine*

4-Mar-2007

BWPD $_{TOTAL}$ = 315.74

Wasatch - Mesa Verde

## Prickly Pear

| Component | 02-25 | 03-28D | 05-13 | 05-16 | 05-19 | 07-16 | 07-28D | 07-33D | 09-18D | 10-04 (BAD SAMPLE) | 13-04 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| BWPD | 0.01 | 14.86 | 0.01 | 3.09 | 0.01 | 0.01 | 35.43 | 0.01 | 0.01 | 0.01 | 0.01 |
| Calcium, $Ca^{+2}$ mg/l | 3,976 | 4,548 | 3,892 | 3,628 | 1 | 921 | 3,916 | 1 | 1 | 1 | 3,904 |
| Magnesium, $Mg^{+2}$ mg/l | 2,654 | 671 | 1,582 | 826 | | 501 | 1,912 | | | | 2,352 |
| Barium, $Ba^{+2}$ mg/l | 0 | 0 | 0 | 0 | | 0 | 0 | | | | 0 |
| Strontium, $Sr^{+2}$ mg/l | 0 | 0 | 0 | 0 | | 0 | 0 | | | | 0 |
| Iron, $Fe^{+3}$ mg/l | 43 | 1 | 183 | 21 | | 56 | 11 | | | | 92 |
| Manganese, $Mn^{+2}$ mg/l | | | | | | | | | | | |
| Sodium, $Na^{+1}$ mg/l | 12,049 | 17,749 | 18,867 | 11,316 | | 10,907 | 16,701 | | | | 16,576 |
| Chloride, $Cl_2$ mg/l | 32,340 | 35,800 | 39,580 | 24,900 | | 18,760 | 36,760 | | | | 38,120 |
| Carbonate, $CO_3^{-2}$ mg/l | 0 | 0 | 0 | 0 | | 0 | 0 | | | | 0 |
| Bicarbonate, $HCO_3^{-1}$ mg/l | 866 | 1,086 | 976 | 937 | | 874 | 1,052 | | | | 930 |
| Sulfate, $SO_4^{-2}$ mg/l | 693 | 1,273 | 603 | 1,128 | | 868 | 1,200 | | | | 903 |
| Total Dissolved Solids mg/l | 52,621 | 61,128 | 65,683 | 42,756 | | 32,887 | 61,552 | | | | 62,877 |
| pH | 6.79 | 6.80 | 7.00 | 6.96 | | 7.06 | 6.72 | | | | 6.59 |
| $CO_2$ in Brine mg/l | 300 | 300 | 300 | 300 | | 300 | 300 | | | | 300 |
| $H_2S$ in Brine mg/l | 10.0 | 1.0 | | 1.0 | | 1.0 | 2.0 | | | | 3.0 |
| Ionic Strength | 1.16 | 1.21 | 1.31 | 0.88 | | 0.61 | 1.27 | | | | 1.31 |
| Temperature °F | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 |
| Pressure psia | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |

### Tomson-Oddo Saturation Index

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | -0.20 | 0.05 | -0.13 | -0.08 | | -0.57 | -0.06 | | | | -0.17 |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |
| Anhydrite; $CaSO_4$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |
| Barite; $BaSO_4$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |
| Celestite; $SrSO_4$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |

### **P**(Pounds Per)**T**(Thousand)**B**(Barrels)

| | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | N/A | 34.1 | N/A | N/A | | N/A | N/A | | | | N/A |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |
| Anhydrite; $CaSO_4$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |
| Barite; $BaSO_4$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |
| Celestite; $SrSO_4$ | N/A | N/A | N/A | N/A | | N/A | N/A | | | | N/A |

Champion Technologies

4-Mar-2007

| Component | Prickly Pear | | | | | | | Prickly Pear Federal | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| | 13-16 (BAD SAMPLE) | 13-21D | 15-18 | 15-21 | 16-15 | 21-02-12-15 | Unit State 36-06 | 01-20 | 01-27D | 03-22 | 03-26D |
| BWPD | 1.67 | 12.00 | 0.01 | 11.29 | 2.62 | 3.33 | 0.01 | 6.86 | 2.29 | 7.43 | 6.43 |
| Calcium, $Ca^{+2}$ mg/l | 1 | 5,572 | 1 | 1 | 4,700 | 1 | 1,662 | 2,790 | 5,708 | 2,380 | 2,936 |
| Magnesium, $Mg^{+2}$ mg/l | | 62 | | | 153 | | 1,742 | 448 | 2,656 | 727 | 669 |
| Barium, $Ba^{+2}$ mg/l | | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 |
| Strontium, $Sr^{+2}$ mg/l | | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 |
| Iron, $Fe^{+3}$ mg/l | | 3 | | | 46 | | 19 | 63 | 16 | 6 | 176 |
| Manganese, $Mn^{+2}$ mg/l | | | | | | | | | | | |
| Sodium, $Na^{+1}$ mg/l | | 17,802 | | | 18,255 | | 10,199 | 21,806 | 14,990 | 8,783 | 21,382 |
| Chloride, $Cl_2$ mg/l | | 37,360 | | | 35,420 | | 22,760 | 38,080 | 40,040 | 13,800 | 38,380 |
| Carbonate, $CO_3^{-2}$ mg/l | | 0 | | | 0 | | 0 | 0 | 0 | 0 | 0 |
| Bicarbonate, $HCO_3^{-1}$ mg/l | | 1,054 | | | 947 | | 1,232 | 1,281 | 892 | 2,611 | 1,339 |
| Sulfate, $SO_4^{-2}$ mg/l | | 960 | | | 1,273 | | 370 | 1,412 | 543 | 6,175 | 1,298 |
| Total Dissolved Solids mg/l | | 62,813 | | | 60,794 | | 37,984 | 65,880 | 64,845 | 34,482 | 66,180 |
| pH | | 6.65 | | | 6.82 | | 7.08 | 6.80 | 7.03 | 7.20 | 6.55 |
| $CO_2$ in Brine mg/l | | 300 | | | 300 | | 300 | 300 | 300 | 300 | 300 |
| $H_2S$ in Brine mg/l | | 2.0 | | | 0.7 | | 25.0 | | | | |
| Ionic Strength | | 1.24 | | | 1.18 | | 0.79 | 1.23 | 1.41 | 0.71 | 1.25 |
| Temperature °F | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 |
| Pressure psia | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |

| Tomson-Oddo Saturation | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | 0.10 | | | -0.05 | | -0.14 | -0.03 | -0.05 | 0.72 | 0.03 |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |
| Anhydrite; $CaSO_4$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |
| Barite; $BaSO_4$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |
| Celestite; $SrSO_4$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |

| P(Pounds Per)T(Thousan | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | 61.5 | | | N/A | | N/A | N/A | N/A | 699.1 | 24.0 |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |
| Anhydrite; $CaSO_4$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |
| Barite; $BaSO_4$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |
| Celestite; $SrSO_4$ | N/A | | | N/A | | N/A | N/A | N/A | N/A | N/A |

Champion Technologies

4-Mar-2007

## Prickly Pear Federal

| Component | 05-22D | 07-20 | 07-22D | 07-25 | 09-20D | 10-27 | 11-15D | 11-17D | 11-30 | 12-27D | 13-23 |
|---|---|---|---|---|---|---|---|---|---|---|---|
| BWPD | 8.29 | 11.86 | 7.29 | 0.01 | 0.01 | 55.86 | 8.57 | 12.14 | 0.01 | 42.86 | 2.00 |
| Calcium, $Ca^{+2}$ mg/l | 5,932 | 3,320 | 4,264 | 1 | 3,595 | 2,864 | 2,712 | 4,356 | 3,976 | 4,904 | 3,832 |
| Magnesium, $Mg^{+2}$ mg/l | 394 | 484 | 508 | | 356 | 3,149 | 1,409 | 2,313 | 2,654 | 3,667 | 1,494 |
| Barium, $Ba^{+2}$ mg/l | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Strontium, $Sr^{+2}$ mg/l | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Iron, $Fe^{+3}$ mg/l | 24 | 95 | 11 | | 149 | 154 | 46 | 71 | 40 | 470 | 56 |
| Manganese, $Mn^{+2}$ mg/l | | | | | | | | | | | |
| Sodium, $Na^{+1}$ mg/l | 17,781 | 23,508 | 17,221 | | 30,312 | 15,127 | 16,428 | 14,877 | 12,049 | 11,297 | 17,791 |
| Chloride, $Cl_2$ mg/l | 37,460 | 41,160 | 33,960 | | 51,460 | 34,980 | 32,420 | 34,660 | 32,340 | 34,040 | 37,160 |
| Carbonate, $CO_3^{-2}$ mg/l | 0 | 0 | 0 | | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Bicarbonate, $HCO_3^{-1}$ mg/l | 1,071 | 2,074 | 1,068 | | 2,369 | 2,679 | 1,119 | 2,586 | 866 | 3,118 | 749 |
| Sulfate, $SO_4^{-2}$ mg/l | 1,325 | 1,583 | 1,353 | | 1,763 | 1,410 | 1,583 | 1,668 | 693 | 1,273 | 1,320 |
| Total Dissolved Solids mg/l | 63,987 | 72,224 | 58,385 | 1 | 90,004 | 60,363 | 55,717 | 60,531 | 52,618 | 58,769 | 62,402 |
| pH | 6.56 | 6.66 | 6.81 | | 6.63 | 6.73 | 6.73 | 6.96 | 6.79 | 6.58 | 6.82 |
| $CO_2$ in Brine mg/l | 300 | 300 | 300 | | 300 | 300 | 300 | 300 | 300 | 300 | 300 |
| $H_2S$ in Brine mg/l | | | | | | 2.0 | | 1.0 | 10.0 | 2.0 | |
| Ionic Strength | 1.28 | 1.35 | 1.15 | | 1.65 | 1.28 | 1.11 | 1.28 | 1.16 | 1.32 | 1.26 |
| Temperature °F | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 |
| Pressure psia | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |

| Tomson-Oddo Saturation | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | 0.14 | 0.45 | 0.02 | | 0.59 | 0.62 | -0.13 | 0.77 | -0.20 | 0.98 | -0.36 |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Anhydrite; $CaSO_4$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Barite; $BaSO_4$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Celestite; $SrSO_4$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |

| P(Pounds Per)T(Thousan | | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | 86.5 | 423.4 | 14.4 | | 595.3 | 661.2 | N/A | 794.9 | N/A | 1119.3 | N/A |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Anhydrite; $CaSO_4$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Barite; $BaSO_4$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |
| Celestite; $SrSO_4$ | N/A | N/A | N/A | | N/A | N/A | N/A | N/A | N/A | N/A | N/A |

Champion Technologies

4-Mar-2007

| Component | Prickly Pear Federal | | | Prickly Pear State | Hunt Ranch | Stone Cabin Unit | | Stone Cabin Federal | Argyle State | Sharples Gov't Pickrell |
|---|---|---|---|---|---|---|---|---|---|---|
| | 15-17 | 15-22D | 16-27D | 04-36 (BAD SAMPLE) | 03-04 | #1 UT (BAD SAMPLE) | 02B-27 UT | 01-11 UT | 33-36 | #1 |
| BWPD | 13.43 | 6.14 | 39.57 | 0.01 | 0.01 | 0.01 | 0.24 | 0.01 | 0.01 | 0.01 |
| Calcium, $Ca^{+2}$ mg/l | 4,744 | 4,540 | 4,204 | 1 | 2,408 | 1 | 1 | 1 | 1 | 2,965 |
| Magnesium, $Mg^{+2}$ mg/l | 1,157 | 758 | 1,708 | | 2,406 | | | | | 2,644 |
| Barium, $Ba^{+2}$ mg/l | 0 | 0 | 0 | | 0 | | | | | 0 |
| Strontium, $Sr^{+2}$ mg/l | 0 | 0 | 0 | | 0 | | | | | 0 |
| Iron, $Fe^{+3}$ mg/l | 100 | 5 | 300 | | 73 | | | | | 29 |
| Manganese, $Mn^{+2}$ mg/l | | | | | | | | | | |
| Sodium, $Na^{+1}$ mg/l | 19,835 | 16,584 | 18,408 | | 12,169 | | | | | 5,076 |
| Chloride, $Cl_2$ mg/l | 40,340 | 34,500 | 37,320 | | 29,680 | | | | | 19,720 |
| Carbonate, $CO_3^{-2}$ mg/l | 0 | 0 | 0 | | 0 | | | | | 0 |
| Bicarbonate, $HCO_3^{-1}$ mg/l | 1,288 | 1,044 | 4,504 | | 486 | | | | | 1,635 |
| Sulfate, $SO_4^{-2}$ mg/l | 1,713 | 960 | 1,175 | | 108 | | | | | 155 |
| Total Dissolved Solids mg/l | 69,177 | 58,391 | 67,619 | | 47,330 | | | | | 32,224 |
| pH | 6.69 | 6.43 | 6.76 | | 6.65 | | | | | 6.24 |
| $CO_2$ in Brine mg/l | 300 | 300 | 300 | | 300 | | | | | 300 |
| $H_2S$ in Brine mg/l | 1.0 | | 1.0 | | 0.5 | | | | | |
| Ionic Strength | 1.38 | 1.16 | 1.34 | | 1.01 | | | | | 0.77 |
| Temperature °F | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 | 85 |
| Pressure psia | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 | 100 |

## Tomson-Oddo Saturation

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | 0.19 | 0.02 | 1.23 | | -0.88 | | | | | 0.37 |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | N/A | N/A | | N/A | | | | | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | N/A | N/A | | N/A | | | | | N/A |
| Anhydrite; $CaSO_4$ | N/A | N/A | N/A | | N/A | | | | | N/A |
| Barite; $BaSO_4$ | N/A | N/A | N/A | | N/A | | | | | N/A |
| Celestite; $SrSO_4$ | N/A | N/A | N/A | | N/A | | | | | N/A |

## P(Pounds Per)T(Thousan

| | | | | | | | | | | |
|---|---|---|---|---|---|---|---|---|---|---|
| Calcite; $CaCO_3$ | 132.9 | 14.1 | 1723.2 | | N/A | | | | | 286.1 |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A | N/A | N/A | | N/A | | | | | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A | N/A | N/A | | N/A | | | | | N/A |
| Anhydrite; $CaSO_4$ | N/A | N/A | N/A | | N/A | | | | | N/A |
| Barite; $BaSO_4$ | N/A | N/A | N/A | | N/A | | | | | N/A |
| Celestite; $SrSO_4$ | N/A | N/A | N/A | | N/A | | | | | N/A |

Champion Technologies

4-Mar-2007

| Component | Averaged Chemistries based on averaged bwpd |
|---|---|
| BWPD | |
| Calcium, $Ca^{+2}$ mg/l | 3,792 |
| Magnesium, $Mg^{+2}$ mg/l | 1,828 |
| Barium, $Ba^{+2}$ mg/l | 0 |
| Strontium, $Sr^{+2}$ mg/l | 0 |
| Iron, $Fe^{+3}$ mg/l | 149 |
| Manganese, $Mn^{+2}$ mg/l | |
| Sodium, $Na^{+1}$ mg/l | 15,438 |
| Chloride, $Cl_2$ mg/l | 33,635 |
| Carbonate, $CO_3^{-2}$ mg/l | 0 |
| Bicarbonate, $HCO_3^{-1}$ mg/l | 2,152 |
| Sulfate, $SO_4^{-2}$ mg/l | 1,361 |
| Total Dissolved Solids mg/l | 55,659 |
| pH | 6.37 |
| $CO_2$ in Brine mg/l | 284 |
| $H_2S$ in Brine mg/l | 1.2 |
| Ionic Strength | 1.20 |
| Temperature °F | 85 |
| Pressure psia | 100 |

1.04 sg = .450 psi/ft = 8.6538 #/gal

| Tomson-Oddo Saturation | |
|---|---|
| Calcite; $CaCO_3$ | 0.59 |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A |
| Anhydrite; $CaSO_4$ | N/A |
| Barite; $BaSO_4$ | N/A |
| Celestite; $SrSO_4$ | N/A |

| P(Pounds Per)T(Thousan | |
|---|---|
| Calcite; $CaCO_3$ | 550.3 |
| Gypsum; $CaSO_4$-$2H_2O$ | N/A |
| Hemihydrate; $CaSO_4$-$1/2H_2O$ | N/A |
| Anhydrite; $CaSO_4$ | N/A |
| Barite; $BaSO_4$ | N/A |
| Celestite; $SrSO_4$ | N/A |

# 2.10

2.10.1. Nearby Underground Sources of Drinking Water, including the geologic formation name,

The literature discussing aquifers in this particular area is limited. U.S. Geological Survey, Water-Resources Investigations Report 92-4161 does indicate however, in the Uinta basin, north of Carbon County, the Douglas Creek-Renegade aquifer occurs above the Wasatch-Green River confining unit. The Wasatch-Green River confining unit lies below the Green River and above the North Horn (Glover, 1996). It would stand to reason the Wasatch formation in the West Tavaputs Plateau area, would protect any drinking water sources from contamination of higher TDS water, injected in deeper formations. In the area of the proposed injection wells, the top of the Wasatch formation occurs approximately 4750 ft above sea level and 2900 ft below ground level, and the highest injection perf occurs in the Prickly Pear #10-4-12-14 which is 2821 ft above sea level and 4757 ft below ground level.

2.10.2. Lithologic descriptions, thicknesses, depths, water quality, and lateral extent;

The Wasatch formation, in the West Tavaputs Plateau area, underlies the Green River formation and is indicated by a transition zone containing a series of transgressive/regressive parasequences of lucustrine origin. In addition, near-shore lucustrine and alluvial deposits occur within the sequence. The Wasatch is Tertiary in age and is marked by a succession of multi-colored shales and interbedded mudstones, siltstones and sandstones. The formation is typically 70-80% silty shale. The shales are silty to very silty, often containing mica or to a lesser extent pyrite. Shales are predominantly tan to reddish brown to brown-and commonly gradational with shaly sands being light brown to brown. Shales usually are blocky and soft, but vary in amounts of calcium carbonate cement.

In the proposed area the Wasatch is about 1000 ft thick and occurs 2800 ft below ground level and 4700 ft above sea level. The sand bodies within the Wasatch, for the most part, are limited in aerial extent and discontinuous. Only sands found in the upper part of the Wasatch, associated with the lucustrine depositional environment have greater continuity.
The middle Wasatch lies between the Wasatch and the North Horn, and is similar to the discontinuous meandering fluvial depositional environment of the Wasatch. The middle Wasatch can be identified on open-hole logs by the drop in resistivity throughout the formation. The formation is also about 1000 ft thick in the area of study.

The North Horn formation is approximately 1900 ft thick, in the area of study, and its top is 5100 ft below ground level (2625' above sea level). The North Horn is predominately a meandering fluvial depositional environment, with exception of the bottom most beds. These sand bodies are indicative of higher energy fluvial environments and are the transition from the Dark Canyon; a braided fluvial environment to the North Horn formation, a lower energy, meandering fluvial environment, which gradually decreases in energy, moving up section. These deepest beds of the North Horn are generally "cleaner" and have a greater aerial extent than beds higher in the formation.
Similar to the Wasatch, most North Horn lithologies are still redbeds, but have subtle color changes in the silty shales and typically are smoother in texture. In addition, some shales are found in yellow, purple, green, and gray coloration.

The Dark Canyon formation, as indicated earlier, is a high-energy braided stream depositional environment. The sands are larger grained, higher in quarts content, more continuous and aerially most extensive. There are some indications that the lowest most deposits in the formation may be a basal conglomerate in some areas. In most areas in the West Tavaputs Plateau, there is a marked increase in sand content in the Dark Canyon, with the higher sand-content pulses occurring at the top and bottom of the formation. The formation averages about 250 ft in thickness and occurs 7000 ft below ground level, which equates to about 700 ft above sea level, in the area of study.

The Price River formation is comprised of sands and shales which seem to be of a more continuous nature, than the Wasatch and North Horn, but more lenticular than the Dark Canyon. Similarly, it seems that there is a higher percentage of sand content in the Price River formation, than the Wasatch or North Horn, but less than the Dark Canyon. The top of the Price River usually begins with an abrupt increase in gray shale and sands within the Price River contain intergranular shale. Down section carbonaceous shales can be found. The top of the formation occurs roughly 7200 ft below ground level, 400-500 ft above sea level and is about 1000 ft thick.

2.10.3. Information relative to geologic structure near the proposed well that may effect the conveyance and/or storage of the injected fluids.

The proposed injection wells are structurally lower than the producing wells to the east. The anticline in the Prickly Pear Federal Unit's structural closure is centered on section 29 of T12S, R15E and its axis trends approximately N50W. The Prickly Pear #10-4 and #12-24 are situated in a saddle or syncline adjacent to the rest of Prickly Pear Federal Unit. Structural highs vary from 50 feet or more, to a few hundred feet up structure, from the synclinal axis, of the Dark Canyon and Price River.
Formation microimager logs run in the Prickly Pear #1-20-12-15, a nearby well, have indicated very few, if any, naturally occurring fractures and cross-dipole sonic logs have concurred with that conclusion, indicating very little anisotropy. The general consensus, when consulting all the cross-dipole data and a recent microseismic survey done in the Prickly Pear #1-20-12-15, is the principle horizontal stress is N50W and likewise hydraulic fracturing would and did create a fracture pattern in the shape of a 4:1 ellipse, with the long axis oriented N50W, in the Prickly Pear #1-20. That fracture pattern and microseismic events were observed in a 9-stage microseimic survey conducted last year on the aforementioned Prickly Pear well. This fracture pattern and hydraulic conveyance regime would transport and store water in an axis parallel to the productive wells to the east, and prevent interference with gas production in the Prickly Pear Unit, in addition to the structural impediments.

# 2.12

# AFFIDAVIT OF NOTICE

Prickly Pear Unit Federal 12-24
Surface Location: 1,271 FSL & 483' FWL
SW/4, Section 24, T12S, R14E
Carbon County, Utah
API: 4300730953
Lease: UTU-77513

I Doug Gundry-White, Senior Landman for Bill Barrett Corporation hereby certify the following;

A copy of the UIC Form 1 Application for Injection Well with supplemental ownership and topographic information was mailed via mail to all operators, owners and surface owners located within a one-half (1/2) mile radius exposure of the location pursuant to R649-5-2.12 of the Oil and Gas Conservation, General Rules.

Doug Gundry-White
Senior Landman
Bill Barrett Corporation

State of Colorado )
)
County of Denver )

BEFORE ME, the undersigned authority, on this day personally appeared Doug Gundry-White known to me to be the person whose name is subscribed to forgoing instrument and acknowledged to me that he executed the same for the purpose and consideration therein expressed.

GIVEN UNDER MY HAND AND SEAL OF OFFICE THIS 21st DAY OF March, 2007

Notary Public

My commission expires:

ERICA L. EVERLY
NOTARY
PUBLIC
STATE OF COLORADO

My Commission Expires Feb. 15, 2010

**Bill Barrett Corporation**

March 21, 2007

U.S. Bureau of Land Management
P.O. Box 45155
Salt Lake City, Utah

RE: Notice of Application for Injection Well
Bill Barrett Corporation – Prickly Pear Unit Federal 12-24
1,271' FSL, 483' FWL, SW/4, Section 24, T12S, R14E, SLM
Carbon County, Utah

Gentlemen;

In accordance with State of Utah Division of Oil, Gas and Mining (UDOGM) General rules R649-5-2.12,. Please find enclosed a copy Bill Barrett Corporation Application for Injection Well (UIC Form 1) for the referenced well. This form is being mail concurrently to all other operators, owner and surface owners within a one-half mile radius of the proposed injection well in accordance with said rules.

Please feel free to contact my contact me at (303) 312-8129 if you have any questions.

Sincerely,

Bill Barrett Corporation

Doug Gundry-White
Senior Landman

Enclosures

1099 18TH STREET
SUITE 2300
DENVER, CO 80202
P 303.293.9100
F 303.291.0420

# CERTIFICATE OF SERVICE

I hereby certify that I caused a true and correct copy of the forgoing Notice of Application for Injection Well to be mailed, postage prepaid, this 21st day of March, 2007, to the following:

U.S. Bureau of Land Management
P.O. Box 45155
Salt Lake City, Utah 84145-0155

Dominion Exploration & Production, Inc.
Attn: Mr. Rusty Waters
14000 Quail Springs Parkway, #600
Oklahoma City, Ok 73134

EOG Resources, Inc.
Attn:
600 17th Street, Suite 1100 North
Denver, Colorado 80202

Petro Canada Resources (USA) Inc.
1099 18th Street, Suite 400
Denver, Colorado 80202-1904

By: _____
Doug Gundry-White, Senior Landman
Bill Barrett Corporation

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

UIC FORM 1

# APPLICATION FOR INJECTION WELL

| Name of Operator | Utah Account Number | Well Name and Number |
|---|---|---|
| Bill Barrett Corporation | N | Prickly Pear Unit Federal 12-24 |
| **Address of Operator** | **Phone Number** | **API Number** |
| 1099 18th Street, 2300 CITY Denver STATE CO ZIP 80202 | (303) 312-8134 | 4300730953 |
| **Location of Well** | | **Field or Unit Name** |
| Footage : 1271' FSL, 483' FWL County : Carbon | | Prickly Pear |
| QQ, Section, Township, Range: SWSW 24 12S 14E State : UTAH | | **Lease Designation and Number** UTU-77513 |

| | | | |
|---|---|---|---|
| Is this application for expansion of an existing project? | | Yes ☑ | No ☐ |
| Will the proposed well be used for: | Enhanced Recovery? | Yes ☐ | No ☑ |
| | Disposal? | Yes ☑ | No ☐ |
| | Storage? | Yes ☐ | No ☑ |
| Is this application for a new well to be drilled? | | Yes ☐ | No ☑ |
| If this application is for an existing well, has a casing test been performed? | | Yes ☐ | No ☑ |
| Date of test: _____ | | | |

Proposed injection interval: from 6,791 to 7,630

Proposed maximum injection: rate 2,000 bpd pressure 2,000 psig

Proposed injection zone contains oil ☐, gas ☐, and / or fresh water ☐ within ½ mile of the well.

List of attachments: Attachments as required by R649-5-2. As per 2.4 under R649-5.2, logs on file with the Division are as follows: Neutron Density and Resistivity.

**ATTACH ADDITIONAL INFORMATION AS REQUIRED BY CURRENT UTAH OIL AND GAS CONSERVATION GENERAL RULES**

**I hereby certify that this report is true and complete to the best of my knowledge.**

Name (Please Print) Tracey Fallang Title Environmental/Regulatory Analyst

Signature Tracey Fallang Date 3/15/2007

(5/2002)


**Bill Barrett Corporation**

## Township 12 South, Range 14 East, SLM
## Carbon County, UTAH
## 03/19/2007

**Injection Well 1/2 Mile Buffer**

**UTU-084619 - PENDING**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Petro Canada Resources (USA) Inc*

**UTU-077059**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Bill Barrett Corporation 100%*

**UTU-077513**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Bill Barrett Corporation 100%*

**UTU-077060**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Bill Barrett Corporation 100%*

**UTU-069095**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator: Bill Barrett Corporation 100%*

**UTU-073666**

*Minerals: Dept of the Interior (BLM) 100%*
*Operator:*
*Surface down to a depth stratigraphic equivalent of forty feet below the base of the "C" Shoal marker found at a subsurface depth of 5,340 feet, as shown on the electric log for the Chandler West River Bend 3-12-10-15 well locate in the NW/4 of Sec. 12, T10S,R15E, SLM, Duchesne County, Utah*

| | |
|---|---|
| *Bill Barrett Corporation* | *52.50%* |
| *Dominion Exploration & Production Inc.* | *25.00%* |
| *EOG Resources Inc.* | *22.50%* |

*From a depth stratigraphic equivalent of forty feet below the base of the "C" Shoal marker found at a subsurface depth of 5,340 feet, as shown on the electric log for the Chandler West River Bend 3-12-10-15 well locate in the NW/4 of Sec. 12, T10S,R15E, SLM, Duchesne County, Utah down to a depth stratigraphic equivalent depth of 9,691 feet as found in the Fasselin 5-19 well located in Sec. 19, T12S, R15E, SLM, Carbon County, Utah*

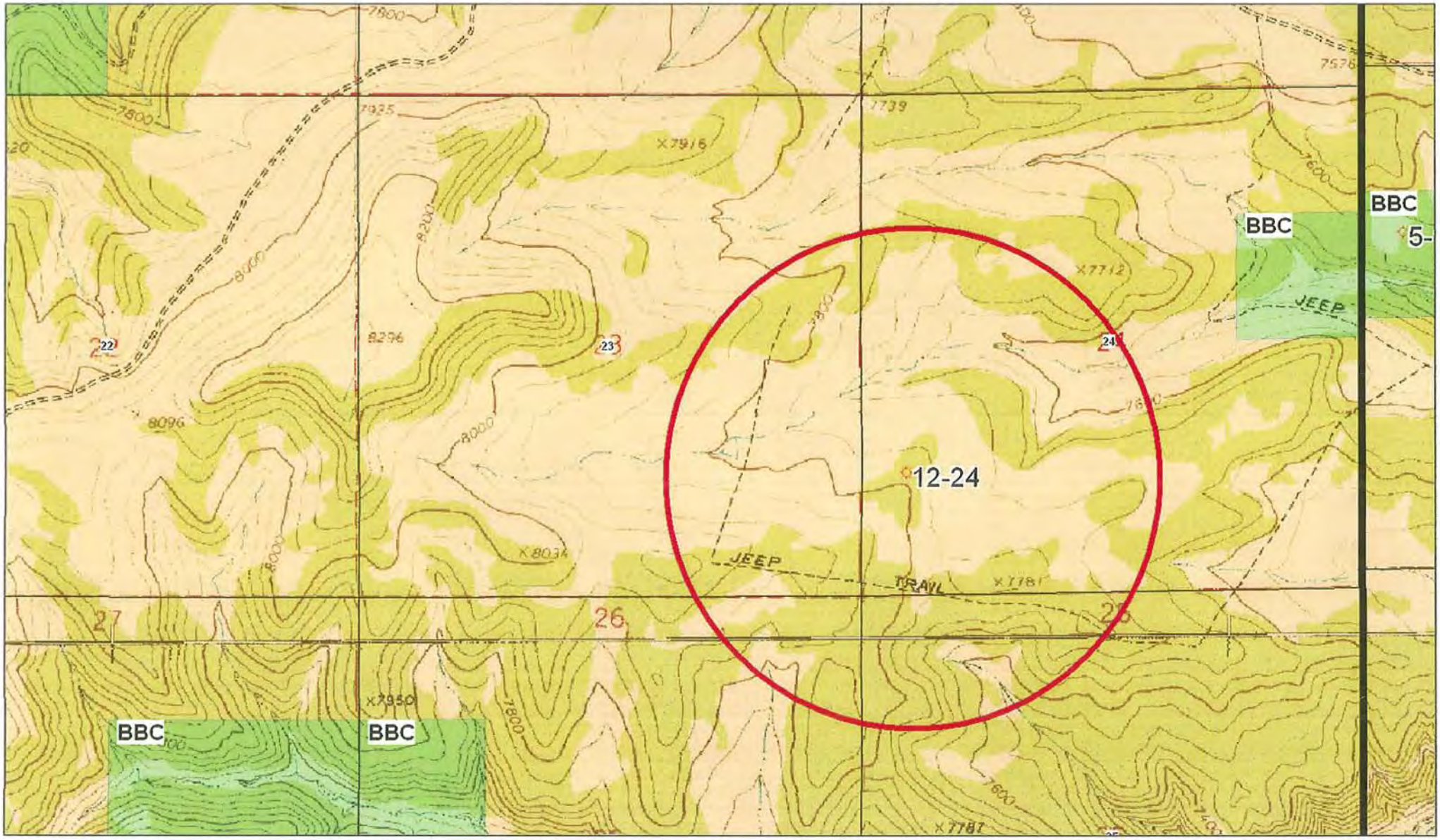
| | |
|---|---|
| *Bill Barrett Corporation* | *26.25%* |
| *Dominion Exploration & Production Inc.* | *73.75%* |

*Below a depth stratigraphic equivalent of 9,691 feet as found in the Fasselin 5-19 well located in Sec. 19, T12S, R15E, SLM, Carbon County, Utah*

| | |
|---|---|
| *Dominion Exploration & Production Inc.* | *73.75%* |
| *EOG Resources Inc.* | *26.25%* |

# Prickly Pear 12-24

Surface Ownership and 1/2 Mile Radius




| FED Surface Owner | STATE Surface Owner | FEE Surface Owner |
|---|---|---|
| Region | Region | Region |

**Bill Barrett Corporation**

Prickly Pear 12-24
API 4300730953
NWSW Sec 24 T12S - R14E
West Tavaputs Field
Carbon County, Utah

**From:** Tracey Fallang <tfallang@billbarrettcorp.com>
**To:** "eric_jones@blm.gov" <eric_jones@blm.gov>, Chris Kierst <chriskierst@uta...
**CC:** John Shepard <jshepard@billbarrettcorp.com>
**Date:** 03/27/2008 3:08 PM
**Subject:** FW: Prickly Pear 12-24 step rate test
**Attachments:** BILL BARRETT==PRICKLY PEAR 12-24.xls

Gentlemen, more information for your review. Please note that there are three tabs in the excel workbook attached. I'll be out of the office after today, back in next Wednesday. If you have any questions, please feel free to call John Shephard, our senior operations engineer, at 303-312-8167.

Thank you.

---

From: John Shepard
Sent: Thursday, March 27, 2008 2:12 PM
To: Tracey Fallang
Subject: FW: Prickly Pear 12-24 step rate test

Charts and data from the step-rate test.

---

From: Donald Kundert [mailto:Donald.Kundert@Halliburton.com]
Sent: Thursday, March 27, 2008 2:00 PM
To: John Shepard
Subject: Prickly Pear 12-24 step rate test

Pat Kundert
Halliburton - Denver
Office 303-312-8188
Cell 303-886-0839
email:donald.kundert@halliburton.com

**From:** Chris Kierst
**To:** Tracey Fallang
**Date:** 03/27/2008 8:36 AM
**Subject:** Re: Injection test for UIC Conversion

Hi Tracey,
A review of the file indicates that BBC currently only has an Approval to Convert letter but no Class II UIC Injection Permit or DOGM permission to inject temporarily (such as to charge the reservoir to get a better Step Rate Test). You say that BBC did conduct a Step Rate Test and that the charts were attached to your post. I do not find these attached.

As regards you request, DOGM would like BBC to run a normal successful witnessed MIT on the well before you do the proposed injectivity test procedure. If the MIT is successful we'll issue BBC a UIC Class II Injection Permit for the well if you wish. In any case, however, BBC can conduct the injectivity test with a verbal approval before we issue the injection permit. If your injectivity test is unsatisfactory it sounds as though it may obviate the need for a UIC Class II Permit, but that would be your decision. If you have any questions please feel free to inquire.

>>> Tracey Fallang <tfallang@billbarrettcorp.com> 03/27/2008 7:51 AM >>>
Chris, here is exactly what we'd like to do on the Prickly Pear 12-24-12-14. Again, per our conversation yesterday, I'd like to confirm that the letter of temporary approval for testing that we have from you covers this test. If at all possible, I'd like to try to get whatever approvals to do this today as I'll be out of the office the rest of the week through next Tuesday. Thanks!

"BBC requests permissions to set two (2) 500 bbl frac tanks on the above referenced location to perform an extended injection test into the North Horn, Dark Canyon and Price River perforations. BBC pumped a step-rate test on the Prickly Pear 12-24-12-14 well on August 30, 2007 and determined the frac extension pressure is approximately 1,900 psi (step-rate charts attached). BBC will haul water from other producing Prickly Pear Unit North Horn/Dark Canyon/Price River wells into the frac tanks. The produced water will be filtered then injected into the Prickly Pear 12-24 well using a hot-oil truck. The maximum allowable surface injection pressure will be kept at or below 1,800 psi. The rate at this maximum pressure is expected to be between 0.5 and 1.0 BPM. In order to determine if the Prickly Pear 12-24 well is suitable for conversion to a water disposal well, BBC would like to run this injection test for up to 7 days to see if the formations will continue to take water or if they pressure up to the maximum allowable pressure after a period of time. "

Tracey Fallang | Direct: 303.312.8134 | Cell: 303.596.4818 |
Fax: 303.291.0420

1099 18th Street, Suite 2300, Denver, CO 80202

tfallang@billbarrettcorp.com

Chris, here is exactly what we'd like to do on the Prickly Pear 12-24-12-14. Again, per our conversation yesterday, I'd like to confirm that the letter of temporary approval for testing that we have from you covers this test. If at all possible, I'd like to try to get whatever approvals to do this today as I'll be out of the office the rest of the week through next Tuesday. Thanks!

"BBC requests permissions to set two (2) 500 bbl frac tanks on the above referenced location to perform an extended injection test into the North Horn, Dark Canyon and Price River perforations. BBC pumped a step-rate test on the Prickly Pear 12-24-12-14 well on August 30, 2007 and determined the frac extension pressure is approximately 1,900 psi (step-rate charts attached). BBC will haul water from other producing Prickly Pear Unit North Horn/Dark Canyon/Price River wells into the frac tanks. The produced water will be filtered then injected into the Prickly Pear 12-24 well using a hot-oil truck. The maximum allowable surface injection pressure will be kept at or below 1,800 psi. The rate at this maximum pressure is expected to be between 0.5 and 1.0 BPM. In order to determine if the Prickly Pear 12-24 well is suitable for conversion to a water disposal well, BBC would like to run this injection test for up to 7 days to see if the formations will continue to take water or if they pressure up to the maximum allowable pressure after a period of time. "

**Tracey Fallang | Direct: 303.312.8134 | Cell: 303.596.4818 | Fax: 303.291.0420**

**1099 18th Street, Suite 2300, Denver, CO 80202**

**tfallang@billbarrettcorp.com**

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DIV. OF OIL, GAS & MINING

**Bill Barrett Corporation**

Uinta Basin

West Tavaputs Plateau

B to B', East/West Cross-section

Prickly Pear SWD #10-4

Horizontal Scale = 300.0
Vertical Scale = 50.0
Vertical Exaggeration = 6.0x

LOG CURVES

| | | |
|---|---|---|
| 0 | 200 | RESD_A (OHM-M) Aliased deep resistivity |
| 0 | 150 | GR_NRM 2 |
| 0.3 | -0.1 | DPHI_NRM DPHI_NRM |
| 0.3 | -0.1 | NPHI_NRM 3 |
| 0 | 2,000 | DSGAS (UNITS) 33 CUTOFF = 0.00 |

TOPS AND MARKERS

- M__WASATCH KMR - T/ Middle Wasatch
- MW_CONFINING_BASE JK - Base of confining interval in M. Wasatch
- NORTH_HORN KMR - T/ Lower Wasatch
- DARK_CANYON JK - T/ Mesaverde (WTP)
- PRICE_RIVER GSH - Base of Dark Canyon
- PRICE_RIVER_6840'_SAND JK - Persistent clean sand in Price River
- PRICE_RIVER_6840'_BASE JK - Base of WTP Payzone
- PRICE_RIVER_CONFINING_BASE JK - Base of confining layer in Price River
- TD GH - Total Depth

Well Name
Well Number
Twn-Rge-Sec
Spot Codes

CORES: SDWL
PERFS: ACTIVE, INACTIVE, SQUEEZED, PROPOSED, BRIDGEPLUG, PLUGGED, LOAD
SHOWS/DST/WLTIP: GAS, OIL, WATER, OTHER
CASING: LINER

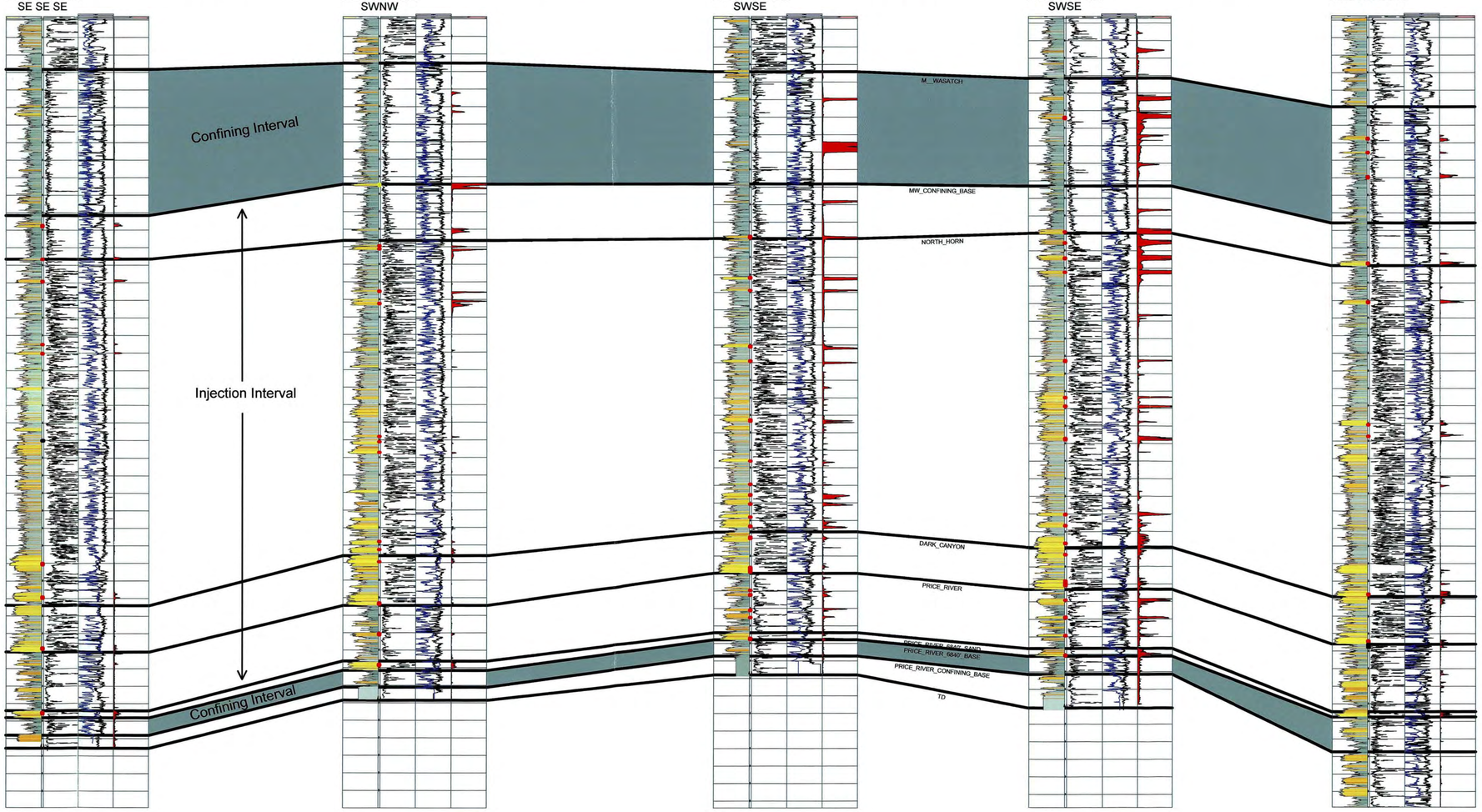
February 28,2007 10:04 AM

PETRA 2/28/2007 10:05:23 AM (SWD 10_4_SW.CSP)

B

B'

| Prickly Pear Federal 10-4 | <1.25MI> | Prickly Pear Federal 5-13 | <1.45MI> | Prickly Pear 15-18 | <1.09MI> | Prickly Pear 15-17 | <1.03MI> | Prickly Pear 7-16 |
|---|---|---|---|---|---|---|---|---|
| T12S R14E S10 SE SE SE | | T12S R14E S13 SWNW | | T12S R15E S18 SWSE | | T12S R15E S17 SWSE | | T12S R15E S16 |



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MAR 2 2 2007
DIV. OF OIL, GAS & MINING

**Bill Barrett Corporation**

Uinta Basin

West Tavaputs Plateau

A to A', North/South Cross-section

Prickly Pear SWD 10-4 and 12-24

Horizontal Scale = 300.0
Vertical Scale = 50.0
Vertical Exaggeration = 6.0x

LOG CURVES

| | | |
|---|---|---|
| 0 | 200 | RESD_A (OHM-M) Aliased deep resistivity |
| 0 | 150 | GR_NRM 2 |
| 0.3 | -0.1 | DPHI_NRM DPHI_NRM |
| 0.3 | -0.1 | NPHI_NRM 3 |
| 0 | 2,000 | DSGAS (UNITS) 33 CUTOFF = 0.00 |

TOPS AND MARKERS

- M__WASATCH KMR - T/ Middle Wasatch
- MW_CONFINING_BASE JK - Base of confining interval in M. Wasatch
- NORTH_HORN KMR - T/ Lower Wasatch
- DARK_CANYON JK - T/ Mesaverde (WTP)
- PRICE_RIVER GSH - Base of Dark Canyon
- PRICE_RIVER_6840'_SAND JK - Persistent clean sand in Price River
- PRICE_RIVER_6840'_BASE JK - Base of WTP Payzone
- PRICE_RIVER_CONFINING_BASE JK - Base of confining layer in Price River
- BLUECASTLE - q
- TD GH - Total Depth

Well Name
Well Number
Twn-Rge-Sec
Spot Codes

CORES: SDWL, CMTHE
PERFS: CMTHE, SCHEDULE, PROPOSED, PLUGGED, JUNK
SHOWSDST/WLTIP: GAS, OIL, WATER, OTHER
CASING: LINER

February 28,2007 8:05 AM

PETRA 2/28/2007 8:05:38 AM (SWD N_S CSP)

A

Argyle State 33-36 — T11S R14E S36 SW NW SE

<2.29MI>

STONE CABIN UNIT 3 — T12S R14E S3 SW SE

<1.21MI>

Prickly Pear Federal 10-4 — T12S R14E S10 SE SE SE

<2.10MI>

Prickly Pear Federal 12-24 — T12S R14E S24 SWSW

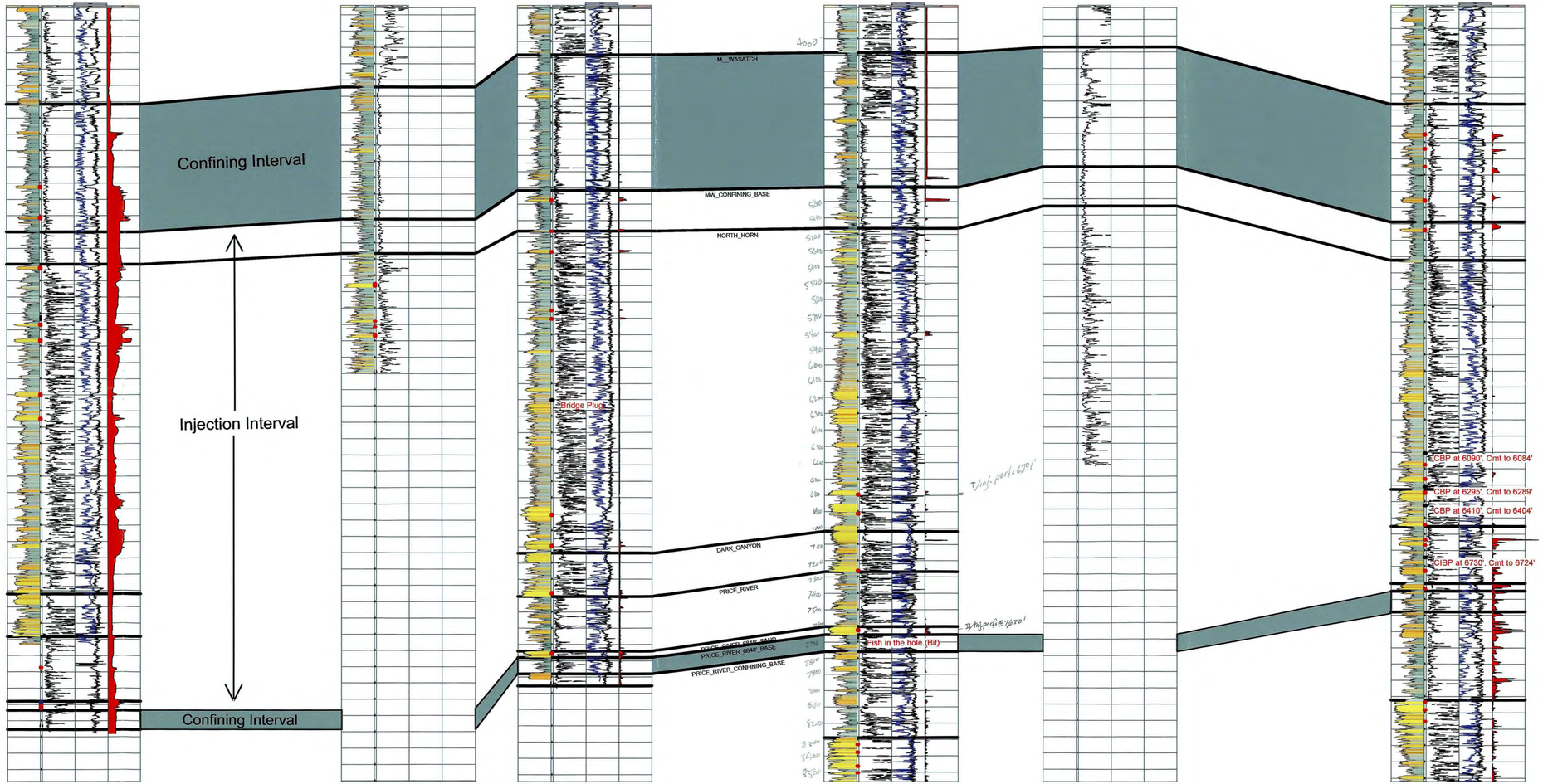
<1.50MI>

CLAYBANK SPRGS UNIT 3 — T12S R15E S30 SESENW

<2.45MI>

Prickly Pear 7-33D — T12S R15E S33 SWNE

A'



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**Bill Barrett Corporation**

Uinta Basin

West Tavaputs Plateau

C to C', East/West Cross-section

Prickly Pear SWD 12-24

Horizontal Scale = 300.0
Vertical Scale = 50.0
Vertical Exaggeration = 6.0x

LOG CURVES

| | | |
|---|---|---|
| 0 | 200 | RESD_A (OHM-M) Aliased deep resistivity |
| 0 | 150 | GR_NRM 2 |
| 0.3 | -0.1 | DPHI_NRM DPHI_NRM |
| 0.3 | -0.1 | NPHI_NRM 3 |
| 0 | 2,000 | DSGAS (UNITS) 33 CUTOFF = 0.00 |

TOPS AND MARKERS

- M__WASATCH KMR - T/ Middle Wasatch
- MW_CONFINING_BASE JK - Base of confining interval in M. Wasatch
- NORTH_HORN KMR - T/ Lower Wasatch
- DARK_CANYON JK - T/ Mesaverde (WTP)
- PRICE_RIVER GSH - Base of Dark Canyon
- PRICE_RIVER_6840'_BASE JK - Base of WTP Payzone
- PRICE_RIVER_CONFINING_BASE JK - Base of confining layer in Price River
- BLUECASTLE - q
- NESLEN JK - Neslen
- TD GH - Total Depth

Well Name
Well Number
Twn-Rge-Sec
Spot Codes

CORES: SDWL
PERFS: ACTIVE, INACTIVE, OPENHOLE, PLUGGED, PROPOSED, SQUEEZED
SHOWS: GAS, OIL, WATER, OTHER
DST/WLTIP
CASING: LINER

February 28,2007 10:22 AM

PETRA 2/28/2007 10:22:55 AM (SWD 12_24_EW.CSP)

C

C'

Prickly Pear Federal 12-24
T12S R14E S24
SWSW

<1.11MI>

Prickly Pear Unit Fass 5-19
T12S R15E S19
SWNW

<1.47MI>

Prickly Pear 7-20
T12S R15E S20
SWNE

<0.64MI>

Prickly Pear 21-2
T12S R15E S21
NE SW NW

<1.91MI>

Prickly Pear 13-23
T12S R15E S23
SWSW

Confining Interval

Injection Interval

Confining Interval

BLUECASTLE

M__WASATCH

MW_CONFINING_BASE

NORTH_HORN

DARK_CANYON

PRICE_RIVER

PRICE_RIVER_6840'_BASE

PRICE_RIVER_CONFINING_BASE

TD

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# Prickly Pear Unit

T12S-R14E

T12S-R15E

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**Bill Barrett Corporation**

## Uinta Basin

### West Tavaputs Plateau

Prickly Pear Fed. Unit

Price River Confining Structure

0 2,500 5,000 7,500
FEET

POSTED WELL DATA

**Well Number**

●

FMTOPS - PRICE_RIVER_6840'_BASE[JK] (SS) (FEET)

By: JK

February 27, 2007

PETRA 2/27/2007 2:21:30 PM

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**Bill Barrett Corporation**

# Uinta Basin

## West Tavaputs Plateau

Prickly Pear Fed. Unit

M. Wasatch Confining Structure

0 2,500 5,000 7,500
FEET

POSTED WELL DATA

Well Number

FMTOPS - M__WASATCH[KMR] (SS) (FT)

By: JK

February 27, 2007



PETRA 2/27/2007 2:59:31 PM

**Bill Barrett Corporation**

April 11, 2007

Mr. Chris Kierst
State of Utah
Division of Oil, Gas and Mining
PO Box 145801
Salt Lake City, UT 84114-5801

***RE: Prickly Pear Unit Federal 10-4 and Prickly Pear Unit Federal 12-24 Revisions to Disposal Applications***

Dear Mr. Kierst:

Bill Barrett Corporation would like to respectfully submit the additional information requested in our conversation on April 10th, 2007.

| **Request by DOGM:** | **BBC Response:** |
|---|---|
| Revise UIC Form 1 injection interval to match conversion to disposal procedures for 12-24 application | Enclosed |
| Under 2.6 of R649-5-2: Provide a "firm statement" as to where water production is coming from | Addition to initial submittal enclosed. |
| Under 2.7 of R649-5-2: Provide water sample for the 12-24 | Well will not produce. Samples provided should be representative. Brad Hill to confirm if any further action necessary. |
| Under 2.9 of R649-5-2: Need to perform a step-rate test | Both wells were frac treated and the tables that were provided (under 2.6) were generated from the frac data. |
| Revise conversion to disposal procedures as need to pressure test casing to 1000 psi. | Enclosed |
| Provide a written argument to show that these applications are for disposal wells and why they should not be classified as enhanced recovery (waterflood) wells. | Enclosed |

If you require further information, please call me at 303-312-8134 or e-mail me at tfallang@billbarrettcorp.com.

Sincerely,

*BILL BARRETT CORPORATION*

Tracey Fallang
Environmental/Regulatory Analyst

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DIV. OF OIL, GAS & MINING

Enclosures

cc: Marie McGann, BLM – Moab Field Office

1099 18TH STREET
SUITE 2300
DENVER, CO 80202
P 303.293.9100
F 303.291.0420

# Prickly Pear 12-24

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

UIC FORM 1

# APPLICATION FOR INJECTION WELL

| | | |
|---|---|---|
| Name of Operator: Bill Barrett Corporation | Utah Account Number: N | Well Name and Number: Prickly Pear Unit Federal 12-24 |
| Address of Operator: 1099 18th Street, 2300 CITY Denver STATE CO ZIP 80202 | Phone Number: (303) 312-8134 | API Number: 4300730953 |
| Location of Well<br>Footage : 1271' FSL, 483' FWL<br>QQ, Section, Township, Range: SWSW 24 12S 14E<br>County : Carbon<br>State : UTAH | | Field or Unit Name: Prickly Pear<br>Lease Designation and Number: UTU-77513 |

| | | | |
|---|---|---|---|
| Is this application for expansion of an existing project? | | Yes ☑ | No ☐ |
| Will the proposed well be used for: | Enhanced Recovery? | Yes ☐ | No ☑ |
| | Disposal? | Yes ☑ | No ☐ |
| | Storage? | Yes ☐ | No ☑ |
| Is this application for a new well to be drilled? | | Yes ☐ | No ☑ |
| If this application is for an existing well, has a casing test been performed? | | Yes ☐ | No ☑ |

Date of test: _____

Proposed injection interval: from 6,295 to 7,630

Proposed maximum injection: rate 2,000 bpd pressure 2,000 psig

Proposed injection zone contains oil ☐, gas ☐, and / or fresh water ☐ within ½ mile of the well.

List of attachments: Attachments as required by R649-5-2. As per 2.4 under R649-5.2, logs on file with the Division are as follows: Neutron Density and Resistivity.

**ATTACH ADDITIONAL INFORMATION AS REQUIRED BY CURRENT UTAH OIL AND GAS CONSERVATION GENERAL RULES**

**I hereby certify that this report is true and complete to the best of my knowledge.**

Name (Please Print) Tracey Fallang Title Environmental/Regulatory Analyst

Signature Tracey Fallang Date 3/21/2007 (revised 4/11/07)

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**APR 12 2007**
**DIV. OF OIL, GAS & MINING**

(5/2002)

# Statement in support of Water Disposal application in opposition to Water Injection application

Disposal Evaluation Request

It is the request of Bill Barrett Corporation that the submitted applications for water disposal in the Prickly Pear field be evaluated based on water disposal and not water injection. This request is based on structural position of the proposed disposal intervals in these proposed water disposal wells, the very discontinuous nature of the proposed disposal intervals and the distance between the proposed disposal wells and the nearest economic gas production.

Structural Position

Based on the supplied structure maps and well log analyses it is evident that the proposed disposal wells, Prickly Pear Federal 10-4 to the north and the Prickly Pear 12-24-12-14 to the south, are significantly down-dip from economic production to the east. Nearest economic gas production from the proposed disposal intervals lies more that 1-1/2 miles from the two proposed disposal wells.

From the shallowest proposed disposal interval in the Middle Wasatch, structural positions indicate a 100' change from the crest of the structure to the Prickly Pear Federal 10-4 and to the Prickly Pear 12-24-12-14 wellbore. This down-dip distance increases as penetration occurs deeper into the section. At the North Horn formation the change between top of structure and wellbore is 150' and 175' for the Pear Federal 10-4 and the Prickly Pear 12-24-12-14 respectively. This trend continues into the Dark Canyon (Upper Price River) with changes of 400'and 300' in the Pear Federal 10-4 and the Prickly Pear 12-24-12-14 respectively. Finally, by the time the Price River is penetrated the structural relief from the localized formation crest is 525'at the Prickly Pear Federal 10-4 and is 400' at the Prickly Pear 12-24-12-14.

The implication of this geologic condition is a proposed gross disposal interval well below the crest of the individual formations and unsuited for water injection support of the gas productive formations in the Prickly Pear field.

Sand Discontinuity

The proposed disposal intervals, from the Middle Wasatch down to the Price River formations, are generally comprised of discontinuous sand bodies. A field study of well logs in the Peters Point area, which is just to the east of the Prickly Pear area, has indicated that producing sand bodies can be shown to be discontinuous even within spacing distances of less than 1,000 ft.

Based on this study it has been found that in the Peters Point area, at most about 50% of the Middle Wasatch sands can be correlated between wells as close as 1,000 ft. The number of correlative sands drops in the North Horn formation to less than 30% at a spacing of +/- 1,500 ft. Sands in the Dark Canyon (Upper Price River) are more correlative within the horizontal spacing of 1,500 ft to 2,000 ft with analysis that indicate these intervals are between 66.7% and 100% continuous. The analysis also observes an 80% correlation between completed Price River sands, but less than a 35% correlation of all Price River Sand, when within a horizontal spacing of 1,500 ft to 2,250 ft.

In total, for the Peters Point area, the wellbore sand correlation between wells ranging from 880 ft of horizontal spacing to a maximum studied distance of 2,360 ft indicates a range of between 41.2% and 47.1% for completed intervals and between

26.8% and 36.6% of all sand bodies found within and between the Middle Wasatch and the Price River.

Proposed Interval Fill-up

A common tool to evaluate the potential for waterflooding success is to calculate the required amount of water before reservoir pressurization could begin to occur. It is usual for this calculation to assume radial displacement and to consider, interval by interval, the porosity corrected vertical thickness (phi*h) for the assumed allocation of injected water.

The following tables summarize for each of the proposed disposal wells, sand interval reservoir properties and resulting fill-up for a ½ mile radius:

| Prickly Pear Federal 10-4 Disposal Interval | | Thickness (ft) | Porosity (%) | Porosity-Feet (phi * ft) | 1/2 mile radius volume (bbl) |
|---|---|---|---|---|---|
| M.Wasatch | 4772-4781 | 9 | 18 | 1.62 | 384,050 |
| | 4964-4968 | 4 | 17 | 0.68 | 161,206 |
| N.Horn | 5090-5095 | 5 | 17 | 0.85 | 201,508 |
| | 5450-5454 | 4 | 12 | 0.48 | 113,793 |
| | 5502-5507 | 5 | 14 | 0.7 | 165,948 |
| Total proposed interval | | 27 | | 4.33 | 1,026,505 |

-- Calculations assume 40% water saturation --

| Prickly Pear 12-24-12-14 Disposal Interval | | Thickness (ft) | Porosity (%) | Porosity-Feet (phi * ft) | 1/2 mile radius volume (bbl) |
|---|---|---|---|---|---|
| N.Horn | 6295-6300 | 5 | 12 | 0.6 | 142,241 |
| | 6791-6799 | 8 | 15 | 1.2 | 284,482 |
| | 6908-6916 | 8 | 14 | 1.12 | 265,516 |
| Dark Canyon | 7258-7266 | 8 | 12 | 0.96 | 227,585 |
| Price River | 7620-7630 | 10 | 13 | 1.3 | 308,189 |
| Total proposed interval | | 39 | | 5.18 | 1,228,013 |

Based on the above calculations over 1 million barrels of water would have to be disposed into the Prickly Pear Federal 10-4 before any reservoir effect would be seen at ½ mile from the wellbore. This volume increases for the Prickly Pear 12-24-12-14 due the increase of proposed interval to over 1.2 million barrels. The amount to effect reservoir pressure increases to over 4.1 million barrels at the Prickly Pear Federal 10-4 location and 4.9 million barrels at the Prickly Pear 12-24-12-14 location if you consider a 1 mile radius around each well. Due to the large volumes required before fill-up can be obtained, water injection for pressure support in this area, for these reservoirs would not be practical.

Summary

Barrett Corporation feels, based on the arguments and calculations provided above, justified to request that the submitted application for water disposal into the Prickly Pear Federal 10-4 and the Prickly Pear 12-24-12-14 be evaluated as such and not on water injection criteria.

# 2.5

(revision to disposal procedure)

**Bill Barrett Corporation**

# Prickly Pear 12-24-12-14

NWSW Sec 24 T12S-R14E, Carbon County, UT

**Surface Casing:** 9-5/8" 36# J-55 STC @ 1,002' Cemented to surface
**Production Liner:** 5-1/2" 17# L-80 LTC @ 9,491 Cemented w/1,850 sx

PBTD: 9,400' (Fish @ 7,665'), KB Elevation: 7,808', GL Elevation: 7,793'

## Conversion to Disposal

1. Note: Water in the context of this procedure will be either clean produced water or 3% KCl water. Any water will require biocide as a precaution.

2. MIRU workover rig. Set tanks and fill with water. Using rig pump kill backside & tubing with water. ND WH & NU BOPE

3. TOOH w/production tubing. PU bit & scraper and TIH to top of fish at 7,665'. TOOH.

4. TIH w/cmt retainer to 7,650'. Establish injection and cement squeeze w/20sx. Sting out of retainer and circulate hole.

5. TOOH w/tubing. PU bit & scraper and TIH to top of retainer at 7,650'. TOOH.

6. PU RBP and Baker Hornet PKR w/bypass valve. TIH and set RBP at +/-7,640' PU and set PKR at +/-7,610'.

7. MIRU Halliburton. Pressure test surface lines to 6,000 psig. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 7,620 – 30' 3 spf 30 shots)

8. Release PKR and PU RBP. PU & set RBP at +/-7,275'. PU & set PKR at +/-7,245'.

9. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 7,258 – 66' 3 spf 24 shots)

10. Release PKR and PU RBP. PU & set RBP at +/-6,930'. PU & set PKR at +/-6,900'.

11. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 6,908 – 16' 4 spf 32 shots)

12. Release PKR and PU RBP. PU & set RBP at +/-6,810'. PU & set PKR at +/-6,780'.

13. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 6,791 – 99' 3 spf 24 shots)

14. Release PKR and PU RBP. PU & set RBP at +/-6,310'. PU & set PKR at +/-6,280'.

15. With bypass valve close pump into interval and establish rate at 500 psig surface pressure. Open bypass and displace 500 gal 7-1/2% HCl to bypass. Close bypass and pump acid into formation displacing with 50 bbl overflush. (Perfs 6,295 – 300' 4 spf 20 shots)

16. RDMO Halliburton.

17. Release PKR and PU RBP. TOOH w/tubing, PKR & RBP.

18. Redress PKR & TIH w/WL re-entry guide, tail joint, Hornet packer, 1.78" XN profile nipple, on-off tool, 1.81" X profile nipple and tubing. Set packer at +/- 6,230'.

19. Sting out of on-off tool and circulate annulus w/inhibited water. Sting into on-off tool.

20. Land tubing and ND BOPE & NU WH.

21. Set plug in XN nipple and pressure test tubing to 3,000 psig. Hold pressure for 30 minutes.

22. Retrieve profile plug.

23. Pressure test backside annulus to 1000 psig. Record pressure test on Barton chart recorder for 30 minutes at stabilizing. Send chart to Denver: Attn Chuck Maybee. Bleed off backside pressure.

24. RDMO workover rig. Turn well over to production group.

Total Acid: 2,500 gal 7-1/2% HCl double inhibited at 150 deg F

C.A.Maybee
2/20/2007
4/10/2007 (rev 1)

Attachments: Wellbore Schematic

# 2.6

(addition to)

**Statement of Water Production:**

All waters proposed for disposal in both the Prickly Pear Federal 10-4 and the Prickly Pear 12-24-12-14 will be from Bill Barrett Corporation field production activities within the Prickly Pear Unit area. No 3rd party or off-unit waters will be accepted for disposal.

~Version I

| ~A DEPT | NPHI | DRHO | DPHI | HDRS | F=0.62/Phixp^2.15 | Rw apparent |
|---|---|---|---|---|---|---|
| 6188.5 | 0.0501 | 0.0016 | -0.0397 | 375.7655 | 50464.32873 | 0.00744616 |
| 6189 | 0.0545 | -0.0058 | -0.0329 | 303.9433 | 10484.08698 | 0.02899092 |
| 6189.5 | 0.0576 | -0.0171 | -0.0197 | 264.5358 | 3129.91021 | 0.08451865 |
| 6190 | 0.0579 | -0.0171 | -0.0147 | 243.1895 | 2362.197059 | 0.10295056 |
| 6190.5 | 0.061 | -0.0107 | -0.0163 | 202.9692 | 2195.052973 | 0.09246665 |
| 6191 | 0.0733 | 0.0006 | -0.0241 | 171.5794 | 1785.998991 | 0.09606915 |
| 6191.5 | 0.0899 | 0.0077 | -0.033 | 107.9348 | 1306.516225 | 0.08261267 |
| 6192 | 0.1009 | -0.0059 | -0.0245 | 69.5222 | 693.3546927 | 0.10026931 |
| 6192.5 | 0.1022 | -0.0209 | -0.0137 | 63.4227 | 505.4499387 | 0.12547771 |
| 6193 | 0.097 | -0.0277 | -0.0082 | 78.2822 | 501.7857268 | 0.15600723 |
| 6193.5 | 0.0916 | -0.0142 | -0.0204 | 97.3737 | 806.8154273 | 0.12068894 |
| 6194 | 0.0965 | -0.0006 | -0.0326 | 91.2948 | 1018.073974 | 0.08967403 |
| 6194.5 | 0.1216 | -0.0016 | -0.0345 | 67.8497 | 523.0788339 | 0.12971219 |
| 6195 | 0.147 | -0.0088 | -0.0237 | 49.2551 | 247.7624948 | 0.19879966 |
| 6195.5 | 0.1434 | -0.0145 | -0.0092 | 39.1247 | 206.5086612 | 0.18945791 |
| 6196 | 0.124 | -0.0146 | -0.0034 | 37.3651 | 259.8420706 | 0.14379927 |
| 6196.5 | 0.1134 | -0.0225 | 0.0018 | 42.5385 | 286.7367445 | 0.14835385 |
| 6197 | 0.105 | -0.0358 | 0.0092 | 51.0777 | 292.1622206 | 0.17482651 |
| 6197.5 | 0.0849 | -0.0347 | 0.0132 | 64.3029 | 405.0585599 | 0.15874964 |
| 6198 | 0.0581 | -0.0216 | 0.0025 | 101.9403 | 1141.011544 | 0.08934204 |
| 6198.5 | 0.0443 | -0.0086 | -0.0121 | 274.1587 | 4443.406603 | 0.06170012 |
| 6199 | 0.0469 | 0.0018 | -0.0235 | 332.2456 | 8826.572377 | 0.03764152 |
| 6199.5 | 0.0503 | 0.0098 | -0.0287 | 310.1913 | 10484.08698 | 0.02958687 |
| 6200 | 0.0576 | 0.0106 | -0.0285 | 182.0799 | 5523.778481 | 0.03296293 |
| 6200.5 | 0.0799 | 0.0185 | -0.0326 | 88.2766 | 1943.814098 | 0.04541412 |
| 6201 | 0.0984 | 0.02 | -0.0288 | 53.664 | 847.2202254 | 0.06334126 |
| 6201.5 | 0.0942 | 0.0127 | -0.0195 | 47.0621 | 727.7243155 | 0.06467023 |
| 6202 | 0.0803 | 0.0007 | -0.0116 | 57.6262 | 871.2628481 | 0.066141 |
| 6202.5 | 0.0669 | 0.0007 | -0.0151 | 91.0884 | 1598.811254 | 0.05697258 |
| 6203 | 0.0546 | 0.0108 | -0.0276 | 161.6457 | 6488.944912 | 0.02491094 |
| 6203.5 | 0.0482 | 0.0222 | -0.0425 | 223.8452 | 183854.9134 | 0.00121751 |
| 6204 | 0.0534 | 0.0235 | -0.0477 | 267.7811 | 183854.9134 | 0.00145648 |
| 6204.5 | 0.0716 | 0.0181 | -0.0455 | 152.3226 | 6979.576784 | 0.02182405 |
| 6205 | 0.0955 | 0.0032 | -0.0336 | 79.2257 | 1090.112413 | 0.07267663 |
| 6205.5 | 0.1128 | -0.0009 | -0.0256 | 53.747 | 521.7899831 | 0.10300504 |
| 6206 | 0.1141 | 0.0023 | -0.0234 | 48.9333 | 479.4579377 | 0.10205963 |
| 6206.5 | 0.1034 | 0.0068 | -0.024 | 54.6481 | 638.251876 | 0.08562153 |
| 6207 | 0.093 | 0.0052 | -0.0207 | 62.9628 | 780.6544524 | 0.08065387 |
| 6207.5 | 0.0867 | -0.0013 | -0.0113 | 70.9927 | 713.2762878 | 0.09953044 |
| 6208 | 0.0803 | -0.0118 | -0.0043 | 92.1518 | 701.2242987 | 0.13141558 |
| 6208.5 | 0.0746 | -0.0164 | -0.0081 | 170.739 | 934.4146585 | 0.18272295 |
| 6209 | 0.0808 | -0.012 | -0.0133 | 244.8607 | 904.9051681 | 0.27059266 |
| 6209.5 | 0.102 | -0.0035 | -0.0158 | 149.1971 | 534.8913302 | 0.27892974 |
| 6210 | 0.1202 | -0.0006 | -0.0176 | 95.6473 | 367.8234 | 0.26003593 |
| 6210.5 | 0.126 | -0.0044 | -0.0196 | 73.2826 | 340.158776 | 0.21543645 |
| 6211 | 0.1297 | -0.0067 | -0.0205 | 68.7064 | 321.6825536 | 0.21358448 |
| 6211.5 | 0.1334 | -0.0074 | -0.0174 | 77.7572 | 282.5019847 | 0.27524479 |
| 6212 | 0.1228 | -0.0055 | -0.0158 | 108.4102 | 336.0710154 | 0.32258123 |
| 6212.5 | 0.1002 | -0.0024 | -0.0168 | 191.0692 | 574.2475769 | 0.33272966 |
| 6213 | 0.1031 | 0.0094 | -0.0208 | 274.1397 | 590.8762506 | 0.46395451 |

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|---|---|---|---|---|---|---|
| 6213.5 | 0.1384 | 0.0175 | 0.0429 | 115.0037 | 108.1560708 | 1.06331248 |
| 6214 | 0.1681 | 0.0429 | 0.194 | 37.146 | 24.44133096 | 1.51980267 |
| 6214.5 | 0.2113 | 0.1118 | 0.3421 | 22.0713 | 9.819107107 | 2.24779094 |
| 6215 | 0.3126 | 0.2106 | 0.3525 | 7.8535 | 6.613010958 | 1.18758309 |
| 6215.5 | 0.407 | 0.2601 | 0.2889 | 6.1291 | 5.999713077 | 1.02156552 |
| 6216 | 0.4117 | 0.243 | 0.2636 | 6.9372 | 6.400120757 | 1.08391705 |
| 6216.5 | 0.3752 | 0.22 | 0.2806 | 8.6163 | 6.816283477 | 1.26407595 |
| 6217 | 0.3546 | 0.241 | 0.2535 | 11.1897 | 8.017886845 | 1.39559216 |
| 6217.5 | 0.3229 | 0.2794 | 0.1546 | 21.1594 | 13.48383477 | 1.56924201 |
| 6218 | 0.2725 | 0.3006 | 0.0531 | 36.8052 | 30.71388319 | 1.19832454 |
| 6218.5 | 0.242 | 0.3214 | -0.0099 | 69.9142 | 63.59231397 | 1.09941274 |
| 6219 | 0.2432 | 0.3199 | -0.0121 | 145.0834 | 64.1854067 | 2.26037985 |
| 6219.5 | 0.2591 | 0.2888 | 0.0235 | 46.8982 | 41.64722235 | 1.1260823 |
| 6220 | 0.2765 | 0.2349 | 0.1066 | 30.9196 | 21.65135363 | 1.42806776 |
| 6220.5 | 0.2846 | 0.197 | 0.1783 | 26.6981 | 14.414804 | 1.85213063 |
| 6221 | 0.2818 | 0.1746 | 0.1912 | 27.8434 | 13.76114996 | 2.02333381 |
| 6221.5 | 0.2745 | 0.1863 | 0.1374 | 32.4771 | 18.52694565 | 1.75296569 |
| 6222 | 0.2733 | 0.2522 | 0.0674 | 29.0455 | 27.86160257 | 1.04249208 |
| 6222.5 | 0.2848 | 0.3143 | 0.0722 | 19.0416 | 25.19819982 | 0.75567303 |
| 6223 | 0.2947 | 0.3076 | 0.1828 | 15.8638 | 13.48383477 | 1.17650507 |
| 6223.5 | 0.2903 | 0.2347 | 0.327 | 18.0724 | 7.763171575 | 2.32796607 |
| 6224 | 0.2645 | 0.1676 | 0.3509 | 25.4378 | 7.814794687 | 3.25508232 |
| 6224.5 | 0.2068 | 0.1176 | 0.2374 | 39.6219 | 15.75115077 | 2.5154924 |
| 6225 | 0.1415 | 0.0699 | 0.1017 | 68.286 | 57.51544753 | 1.18726365 |
| 6225.5 | 0.1 | 0.0225 | 0.0351 | 122.0182 | 203.5622206 | 0.59941476 |
| 6226 | 0.0783 | -0.0061 | 0.0197 | 173.8165 | 405.9477302 | 0.42817458 |
| 6226.5 | 0.065 | -0.0216 | 0.0182 | 251.6499 | 577.2195457 | 0.43596912 |
| 6227 | 0.0551 | -0.0293 | 0.017 | 424.058 | 785.3176549 | 0.53998277 |
| 6227.5 | 0.0493 | -0.0256 | 0.0135 | 634.7236 | 1056.800344 | 0.60060881 |
| 6228 | 0.0581 | -0.0112 | 0.0035 | 391.166 | 1101.558711 | 0.35510227 |
| 6228.5 | 0.0845 | 0.0087 | 0.0047 | 152.7223 | 496.9603538 | 0.30731284 |
| 6229 | 0.1157 | 0.0737 | 0.0084 | 70.1849 | 244.341283 | 0.28724127 |
| 6229.5 | 0.1469 | 0.1609 | 0.0237 | 40.0488 | 123.2682619 | 0.32489141 |
| 6230 | 0.1769 | 0.1919 | 0.0444 | 25.376 | 70.45245646 | 0.36018616 |
| 6230.5 | 0.1837 | 0.1286 | 0.0568 | 22.8166 | 58.91267687 | 0.38729525 |
| 6231 | 0.155 | 0.0408 | 0.0492 | 29.0121 | 83.75029472 | 0.34641192 |
| 6231.5 | 0.1204 | -0.0005 | 0.0258 | 44.717 | 171.7787068 | 0.26031748 |
| 6232 | 0.1057 | -0.0063 | 0.0099 | 64.8996 | 284.6078253 | 0.22803168 |
| 6232.5 | 0.1041 | -0.0044 | 0.0055 | 90.9928 | 319.1636983 | 0.28509759 |
| 6233 | 0.1081 | -0.0065 | 0.0051 | 110.1239 | 297.7394367 | 0.36986669 |
| 6233.5 | 0.1326 | -0.0195 | 0.0087 | 85.8297 | 184.841946 | 0.46434103 |
| 6234 | 0.1873 | -0.0259 | 0.0117 | 51.6909 | 88.52624962 | 0.58390478 |
| 6234.5 | 0.2406 | -0.012 | 0.0138 | 35.1402 | 52.20888282 | 0.67306937 |
| 6235 | 0.2594 | 0.0254 | 0.0212 | 28.5571 | 42.28805365 | 0.67529946 |
| 6235.5 | 0.246 | 0.1019 | 0.0344 | 27.6166 | 42.35292998 | 0.65205878 |
| 6236 | 0.2259 | 0.207 | 0.0788 | 29.5048 | 35.42259744 | 0.83293722 |
| 6236.5 | 0.2284 | 0.2992 | 0.1587 | 26.1373 | 21.17319327 | 1.23445244 |
| 6237 | 0.2491 | 0.3296 | 0.2514 | 21.9877 | 12.18673603 | 1.80423207 |
| 6237.5 | 0.2549 | 0.3305 | 0.2818 | 23.9262 | 10.48777231 | 2.28134243 |
| 6238 | 0.2388 | 0.3109 | 0.2223 | 34.8894 | 14.53605868 | 2.4001967 |
| 6238.5 | 0.2153 | 0.2456 | 0.1127 | 60.5331 | 30.23273353 | 2.00223708 |
| 6239 | 0.1924 | 0.1372 | 0.0287 | 162.1285 | 70.58954517 | 2.2967778 |

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|---|---|---|---|---|---|---|
| 6239.5 | 0.1785 | 0.0576 | 0.0117 | 159.6847 | 97.56714077 | 1.63666475 |
| 6240 | 0.1892 | 0.0849 | 0.0242 | 119.3377 | 76.17951226 | 1.56653274 |
| 6240.5 | 0.2306 | 0.211 | 0.0412 | 49.1459 | 45.28661474 | 1.08521912 |
| 6241 | 0.2799 | 0.3429 | 0.0737 | 30.0732 | 25.72200564 | 1.16916233 |
| 6241.5 | 0.3216 | 0.3657 | 0.1413 | 12.0254 | 14.414804 | 0.83423958 |
| 6242 | 0.3646 | 0.3089 | 0.1943 | 8.2294 | 9.612533017 | 0.85611149 |
| 6242.5 | 0.389 | 0.2437 | 0.2365 | 7.7261 | 7.546011366 | 1.02386541 |
| 6243 | 0.3613 | 0.2157 | 0.2822 | 8.365 | 7.099484168 | 1.17825462 |
| 6243.5 | 0.2948 | 0.2083 | 0.3077 | 11.0834 | 8.178968207 | 1.3551098 |
| 6244 | 0.225 | 0.189 | 0.2485 | 24.9815 | 13.72992662 | 1.81949261 |
| 6244.5 | 0.1687 | 0.1363 | 0.1408 | 43.5433 | 34.25198739 | 1.27126346 |
| 6245 | 0.1281 | 0.0675 | 0.0628 | 126.7542 | 96.79957134 | 1.30945001 |
| 6245.5 | 0.0978 | 0.0254 | 0.0339 | 528.9875 | 215.0288657 | 2.46007669 |
| 6246 | 0.075 | 0.0121 | 0.0276 | 3193.523 | 367.8234 | 8.6822187 |
| 6246.5 | 0.0581 | 0.0102 | 0.0201 | 11787.44 | 659.4952336 | 17.8734308 |
| 6247 | 0.0461 | 0.0092 | 0.013 | 4201.261 | 1204.184676 | 3.48888404 |
| 6247.5 | 0.0404 | 0.0051 | 0.0142 | 1390.487 | 1427.716565 | 0.97392342 |
| 6248 | 0.0399 | -0.0007 | 0.023 | 634.9323 | 1053.191372 | 0.60286508 |
| 6248.5 | 0.0415 | -0.0154 | 0.036 | 354.362 | 672.3687492 | 0.5270352 |
| 6249 | 0.0448 | -0.0302 | 0.041 | 202.0544 | 540.2670871 | 0.37398984 |
| 6249.5 | 0.0546 | -0.0322 | 0.0388 | 110.6552 | 450.1532565 | 0.24581673 |
| 6250 | 0.0765 | -0.0187 | 0.0258 | 64.5988 | 370.1464323 | 0.17452228 |
| 6250.5 | 0.1048 | 0.0019 | 0.0117 | 42.3631 | 279.9016384 | 0.15134995 |
| 6251 | 0.1237 | 0.0098 | 0.0068 | 31.274 | 219.3024987 | 0.14260667 |
| 6251.5 | 0.1262 | 0.0182 | 0.006 | 31.4398 | 213.2841348 | 0.14740806 |
| 6252 | 0.1199 | 0.0247 | 0.0035 | 41.2531 | 247.331019 | 0.16679307 |
| 6252.5 | 0.1129 | 0.0182 | 0.0068 | 56.9675 | 264.0606918 | 0.21573639 |
| 6253 | 0.114 | 0.0049 | 0.0208 | 63.0932 | 204.5374852 | 0.30846766 |
| 6253.5 | 0.1324 | 0.0038 | 0.0365 | 82.1099 | 125.951236 | 0.65191818 |
| 6254 | 0.1629 | 0.0267 | 0.0448 | 57.0979 | 80.74538556 | 0.70713515 |
| 6254.5 | 0.1902 | 0.0601 | 0.042 | 36.3415 | 63.53344678 | 0.5720058 |
| 6255 | 0.2017 | 0.1075 | 0.0211 | 29.8442 | 69.43661311 | 0.42980495 |
| 6255.5 | 0.194 | 0.1348 | 0.0014 | 31.854 | 92.07004968 | 0.3459757 |
| 6256 | 0.1769 | 0.1129 | 0.0036 | 53.3383 | 109.1893264 | 0.48849372 |
| 6256.5 | 0.1642 | 0.0805 | 0.0455 | 87.8327 | 79.09873803 | 1.11041847 |
| 6257 | 0.1673 | 0.1008 | 0.1512 | 98.1782 | 32.20482113 | 3.04855598 |
| 6257.5 | 0.194 | 0.1688 | 0.2869 | 56.9149 | 13.27970445 | 4.28585593 |
| 6258 | 0.238 | 0.2384 | 0.3611 | 33.2586 | 8.27909075 | 4.01718027 |
| 6258.5 | 0.2809 | 0.2946 | 0.3392 | 19.0925 | 7.688001471 | 2.48341524 |
| 6259 | 0.3097 | 0.318 | 0.3151 | 13.5478 | 7.564199688 | 1.79104209 |
| 6259.5 | 0.3222 | 0.3277 | 0.3057 | 10.0823 | 7.484135497 | 1.34715626 |
| 6260 | 0.3233 | 0.3723 | 0.2351 | 9.7888 | 9.631048048 | 1.01637952 |
| 6260.5 | 0.3056 | 0.4144 | 0.1538 | 13.4571 | 14.65195411 | 0.91845087 |
| 6261 | 0.2682 | 0.3824 | 0.1602 | 23.5102 | 17.02667461 | 1.38078636 |
| 6261.5 | 0.2382 | 0.2975 | 0.2127 | 30.7916 | 15.25224154 | 2.01882457 |
| 6262 | 0.224 | 0.2243 | 0.1791 | 32.0074 | 19.40745841 | 1.64923193 |
| 6262.5 | 0.2112 | 0.1506 | 0.0944 | 44.5366 | 35.19868817 | 1.26529147 |
| 6263 | 0.1898 | 0.0726 | 0.0319 | 81.5879 | 70.17944672 | 1.16256117 |
| 6263.5 | 0.1656 | 0.0215 | 0.0086 | 136.7632 | 117.8562603 | 1.16042372 |
| 6264 | 0.1489 | 0.007 | -0.0035 | 105.9856 | 173.8171826 | 0.6097533 |
| 6264.5 | 0.1396 | 0.0043 | -0.0061 | 85.1606 | 208.8437385 | 0.40777186 |
| 6265 | 0.1415 | 0.0012 | -0.0004 | 73.8153 | 185.4057081 | 0.39812852 |

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|---|---|---|---|---|---|---|
| 6265.5 | 0.1536 | 0.0083 | 0.0078 | 62.4962 | 138.8716482 | 0.4500285 |
| 6266 | 0.1661 | 0.0415 | 0.0122 | 52.0721 | 112.1064996 | 0.46448779 |
| 6266.5 | 0.1744 | 0.0856 | 0.0084 | 44.9075 | 106.2569556 | 0.42263116 |
| 6267 | 0.1747 | 0.0922 | -0.0018 | 44.7724 | 119.7696953 | 0.37382077 |
| 6267.5 | 0.1682 | 0.0477 | -0.0061 | 48.3657 | 137.5855101 | 0.35153193 |
| 6268 | 0.1627 | 0.0011 | -0.0037 | 50.415 | 143.417571 | 0.35152596 |
| 6268.5 | 0.1599 | -0.0159 | -0.0029 | 53.4619 | 147.3743584 | 0.36276256 |
| 6269 | 0.1568 | -0.0092 | -0.0093 | 56.4066 | 168.5401346 | 0.33467755 |
| 6269.5 | 0.153 | -0.0034 | -0.0122 | 56.1058 | 186.256086 | 0.30122935 |
| 6270 | 0.1517 | -0.0103 | -0.0063 | 53.8841 | 173.8171826 | 0.31000445 |
| 6270.5 | 0.155 | -0.0213 | -0.0024 | 51.2709 | 156.6620961 | 0.32727061 |
| 6271 | 0.163 | -0.0242 | -0.0008 | 48.1077 | 137.4032018 | 0.35012066 |
| 6271.5 | 0.1695 | -0.0168 | -0.0032 | 45.6163 | 130.2230444 | 0.35029361 |
| 6272 | 0.1664 | -0.006 | -0.0017 | 45.5577 | 132.9581434 | 0.34264693 |
| 6272.5 | 0.1572 | 0.0076 | -0.0079 | 48.083 | 164.201679 | 0.29282892 |
| 6273 | 0.1472 | 0.0197 | -0.0197 | 52.5387 | 230.5468979 | 0.22788726 |
| 6273.5 | 0.1374 | 0.0279 | -0.0301 | 54.0852 | 334.0540781 | 0.16190552 |
| 6274 | 0.1299 | 0.025 | -0.0252 | 52.9881 | 352.1444228 | 0.15047264 |
| 6274.5 | 0.1234 | 0.014 | -0.0141 | 61.0826 | 321.0501166 | 0.19025877 |
| 6275 | 0.1134 | -0.0017 | -0.0071 | 97.8611 | 340.8471457 | 0.2871114 |
| 6275.5 | 0.0975 | -0.0033 | -0.0162 | 178.7721 | 606.6127122 | 0.2947055 |
| 6276 | 0.0802 | 0.002 | -0.027 | 244.6087 | 1509.719174 | 0.16202265 |
| 6276.5 | 0.068 | 0.0007 | -0.0264 | 230.0774 | 2561.860746 | 0.08980871 |
| 6277 | 0.0598 | -0.001 | -0.0208 | 261.5046 | 2943.183059 | 0.08885095 |
| 6277.5 | 0.0509 | -0.0057 | -0.0113 | 345.8781 | 2848.141294 | 0.12143994 |
| 6278 | 0.0412 | -0.0087 | -0.009 | 449.6213 | 4443.406603 | 0.10118842 |
| 6278.5 | 0.0332 | -0.0114 | -0.0064 | 535.2143 | 6593.505503 | 0.08117295 |
| 6279 | 0.028 | -0.0026 | -0.0095 | 556.2235 | 14628.06778 | 0.0380244 |
| 6279.5 | 0.0254 | 0.0041 | -0.0128 | 549.2748 | 33404.84863 | 0.01644297 |
| 6280 | 0.0251 | 0.0041 | -0.0132 | 552.1741 | 37772.88994 | 0.01461826 |
| 6280.5 | 0.0262 | -0.0069 | -0.0011 | 552.3386 | 7591.151851 | 0.07276084 |
| 6281 | 0.0275 | -0.0118 | 0.0031 | 498.2577 | 4957.983912 | 0.10049603 |
| 6281.5 | 0.0281 | -0.0037 | -0.0042 | 387.6425 | 8434.33202 | 0.04596007 |
| 6282 | 0.0274 | 0.0102 | -0.0096 | 288.5096 | 15892.90089 | 0.01815336 |
| 6282.5 | 0.0257 | 0.0205 | -0.0098 | 205.3707 | 20258.27036 | 0.01013762 |
| 6283 | 0.0243 | 0.0156 | -0.0012 | 189.8369 | 9074.870231 | 0.02091897 |
| 6283.5 | 0.0246 | 0.0027 | 0.0068 | 287.5781 | 4690.373601 | 0.06131241 |
| 6284 | 0.0285 | -0.0066 | 0.0083 | 309.6234 | 3334.520333 | 0.09285395 |
| 6284.5 | 0.0358 | -0.01 | 0.0034 | 190.6991 | 2910.992832 | 0.06550999 |
| 6285 | 0.0449 | -0.0004 | -0.0084 | 122.9214 | 3393.724015 | 0.03622021 |
| 6285.5 | 0.0502 | 0.0188 | -0.0215 | 112.3484 | 5690.626765 | 0.01974271 |
| 6286 | 0.0453 | 0.0282 | -0.0268 | 147.9448 | 14628.06778 | 0.01011376 |
| 6286.5 | 0.0337 | 0.0116 | -0.0107 | 310.2599 | 9159.912661 | 0.03387149 |
| 6287 | 0.0238 | -0.0066 | 0.0073 | 560.2132 | 4788.189652 | 0.11699896 |
| 6287.5 | 0.0188 | -0.0115 | 0.0163 | 1598.143 | 3691.44056 | 0.43293212 |
| 6288 | 0.0171 | -0.005 | 0.0158 | 6464.386 | 4242.628447 | 1.52367484 |
| 6288.5 | 0.0161 | 0.0059 | 0.0093 | 20000 | 7399.692786 | 2.70281491 |
| 6289 | 0.0145 | 0.0112 | 0.0036 | 20000 | 15331.9447 | 1.30446596 |
| 6289.5 | 0.0133 | 0.007 | 0.0055 | 20000 | 14130.80178 | 1.41534786 |
| 6290 | 0.0141 | -0.002 | 0.0068 | 18811.13 | 11253.60494 | 1.67156471 |
| 6290.5 | 0.0166 | -0.0082 | 0.0031 | 5227.485 | 12779.20373 | 0.40906186 |
| 6291 | 0.02 | -0.0046 | -0.0052 | 2026.429 | 23634.34072 | 0.08574088 |

| | Nϕ | Δϕ | dϕ | $R_t$ | | | |
|---|---|---|---|---|---|---|---|
| 6291.5 | 0.0239 | 0.004 | -0.0134 | 1063.658 | | 49436.66746 | 0.02151556 |
| 6292 | 0.0268 | 0.0111 | -0.0151 | 728.1864 | | 39174.78101 | 0.01858814 |
| 6292.5 | 0.0268 | 0.0046 | -0.0058 | 625.046 | | 11138.70486 | 0.05611478 |
| 6293 | 0.0243 | -0.006 | 0.0079 | 631.2062 | | 4443.406603 | 0.14205457 |
| 6293.5 | 0.0213 | -0.0046 | 0.0143 | 639.907 | | 3580.871071 | 0.17870149 |
| 6294 | 0.02 | 0.0097 | 0.0141 | 519.2366 | | 3928.115647 | 0.13218465 |
| 6294.5 | 0.0208 | 0.016 | 0.0248 | 400.6442 | | 2102.963662 | 0.19051409 |
| 6295 | 0.0232 | 0.0116 | 0.0461 | 213.2789 | | 855.1252409 | 0.24941247 |
| 6295.5 | 0.0265 | 0.0068 | 0.0605 | 168.9784 | | 524.3723544 | 0.32224887 |
| 6296 | 0.0295 | 0.0062 | 0.0654 | 195.3719 | 7% ϕ | 434.9945577 | 0.44913642 |
| 6296.5 | 0.0309 | 0.0076 | 0.068 | 224.8715 | | 398.046815 | 0.56493732 |
| 6297 | 0.0316 | 0.006 | 0.0712 | 198.5624 | gas | 366.2865601 | 0.54209578 |
| 6297.5 | 0.0323 | 0.0075 | 0.0661 | 145.2917 | | 402.4081042 | 0.3610556 |
| 6298 | 0.0326 | 0.0115 | 0.0586 | 113.908 | | 473.8242434 | 0.24040138 |
| 6298.5 | 0.0323 | 0.0131 | 0.0606 | 112.7065 | | 455.3783667 | 0.24750078 |
| 6299 | 0.0317 | 0.0085 | 0.0703 | 137.1078 | | 372.4910231 | 0.3680835 |
| 6299.5 | 0.031 | 0.0009 | 0.0723 | 180.3271 | | 362.4853749 | 0.49747414 |
| 6300 | 0.0301 | -0.0057 | 0.0596 | 270.937 | | 491.0236696 | 0.55177992 |
| 6300.5 | 0.031 | -0.0043 | 0.0305 | 478.8258 | | 1105.413289 | 0.4331645 |
| 6301 | 0.0382 | -0.0065 | 0.01 | 517.3121 | | 1866.616274 | 0.27713896 |
| 6301.5 | 0.0554 | -0.0054 | -0.0016 | 277.6467 | | 1473.751593 | 0.1883945 |
| 6302 | 0.0808 | -0.008 | 0.0023 | 145.5912 | | 578.7139871 | 0.25157712 |
| 6302.5 | 0.1013 | -0.0128 | 0.0062 | 122.2217 | | 332.7192911 | 0.36734179 |
| 6303 | 0.1068 | -0.021 | 0.0086 | 126.3455 | | 285.6693793 | 0.44227876 |
| 6303.5 | 0.102 | -0.0211 | 0.0072 | 141.0652 | | 321.6825536 | 0.438523 |
| 6304 | 0.0947 | -0.0074 | -0.0031 | 165.7374 | | 469.3868427 | 0.35309341 |
| 6304.5 | 0.0893 | 0.008 | -0.0094 | 208.9633 | | 629.6955217 | 0.33184816 |
| 6305 | 0.0888 | 0.0122 | -0.0096 | 256.4018 | | 641.7221646 | 0.39955266 |
| 6305.5 | 0.092 | 0.002 | -0.0002 | 219.8411 | | 467.1909437 | 0.47055942 |
| 6306 | 0.0968 | -0.0052 | 0.0085 | 151.2526 | | 347.8445331 | 0.43482816 |
| 6306.5 | 0.1025 | -0.0063 | 0.0139 | 109.9032 | | 280.4188943 | 0.39192509 |
| 6307 | 0.1066 | -0.0097 | 0.022 | 94.9567 | | 226.327902 | 0.41955366 |
| 6307.5 | 0.11 | -0.0094 | 0.0242 | 89.233 | | 206.5086612 | 0.43210294 |
| 6308 | 0.1155 | -0.0004 | 0.0216 | 80.7639 | | 197.231216 | 0.40948842 |
| 6308.5 | 0.1196 | 0.011 | 0.0129 | 68.0691 | | 212.2472353 | 0.32070665 |
| 6309 | 0.1186 | 0.0104 | 0.0127 | 63.8507 | | 216.4397477 | 0.2950045 |
| 6309.5 | 0.115 | -0.0029 | 0.0197 | 71.3222 | | 204.8640949 | 0.34814397 |
| 6310 | 0.1101 | -0.0172 | 0.0326 | 78.9533 | | 180.9650212 | 0.43629039 |
| 6310.5 | 0.1003 | -0.0239 | 0.0366 | 71.5086 | | 197.8512355 | 0.3614261 |
| 6311 | 0.088 | -0.0321 | 0.0435 | 57.5934 | | 215.7326169 | 0.26696658 |
| 6311.5 | 0.081 | -0.0312 | 0.0543 | 47.0733 | | 202.9158247 | 0.23198437 |
| 6312 | 0.0818 | -0.0195 | 0.061 | 39.0776 | | 180.6926695 | 0.21626555 |
| 6312.5 | 0.0862 | -0.0014 | 0.0602 | 32.7652 | | 171.2745619 | 0.1913022 |
| 6313 | 0.0921 | 0.0125 | 0.0535 | 28.2956 | | 173.3042543 | 0.16327124 |
| 6313.5 | 0.0998 | 0.012 | 0.0567 | 25.8038 | | 148.3885343 | 0.17389349 |
| 6314 | 0.1068 | 0.0036 | 0.0698 | 24.7635 | 11% ϕ | 114.4395593 | 0.21638933 |
| 6314.5 | 0.1104 | 0.004 | 0.0786 | 24.0493 | | 98.9038736 | 0.24315832 |
| 6315 | 0.1086 | 0.0105 | 0.0798 | 23.4751 | wet | 99.58232196 | 0.23573562 |
| 6315.5 | 0.1033 | 0.0069 | 0.083 | 23.3275 | | 102.0113611 | 0.22867551 |
| 6316 | 0.1009 | -0.0033 | 0.0918 | 23.1632 | ~38,000 PPM | 94.86597916 | 0.24416762 |
| 6316.5 | 0.1013 | -0.008 | 0.0996 | 22.4426 | | 86.73598527 | 0.25874612 |
| 6317 | 0.1011 | -0.0014 | 0.0981 | 21.5215 | | 88.33526412 | 0.2436343 |

0.25 to 0.56

0.16 to 2.2

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|---|---|---|---|---|---|---|
| 6317.5 | 0.1012 | 0.005 | 0.0923 | 20.7967 | 94.02473023 | 0.2211833 |
| 6318 | 0.1011 | -0.0003 | 0.0939 | 20.4193 | 92.47658119 | 0.22080509 |
| 6318.5 | 0.1003 | -0.0066 | 0.0962 | 20.509 | 90.96549509 | 0.22545911 |
| 6319 | 0.0999 | -0.0119 | 0.0987 | 20.9799 | 88.91003992 | 0.23596773 |
| 6319.5 | 0.099 | -0.0207 | 0.1017 | 21.5444 | 86.92192371 | 0.24785922 |
| 6320 | 0.0961 | -0.03 | 0.1071 | 22.0052 | 84.63894033 | 0.25998908 |
| 6320.5 | 0.0927 | -0.0278 | 0.11 | 22.2774 | 85.08845157 | 0.26181461 |
| 6321 | 0.0899 | -0.0101 | 0.1007 | 22.4893 | 97.12744246 | 0.23154424 |
| 6321.5 | 0.0875 | 0.0063 | 0.0899 | 22.9071 | 113.3328752 | 0.20212229 |
| 6322 | 0.0887 | 0.0043 | 0.0893 | 23.5973 | 112.5131219 | 0.20972932 |
| 6322.5 | 0.0926 | -0.011 | 0.096 | 24.6675 | 99.35541692 | 0.24827534 |
| 6323 | 0.0943 | -0.0222 | 0.1039 | 26.4866 | 89.29627288 | 0.29661484 |
| 6323.5 | 0.0942 | -0.0191 | 0.1063 | 29.0671 | 87.10844673 | 0.33368865 |
| 6324 | 0.0942 | -0.0028 | 0.1025 | 31.5131 | 90.76675439 | 0.34718769 |
| 6324.5 | 0.0934 | 0.0168 | 0.0911 | 33.9754 | 104.1631209 | 0.32617494 |
| 6325 | 0.0909 | 0.0217 | 0.0843 | 37.6803 | 116.4147102 | 0.32367301 |
| 6325.5 | 0.0859 | 0.0135 | 0.0845 | 45.1724 | 123.5795361 | 0.36553301 |
| 6326 | 0.0784 | 0.0029 | 0.0866 | 65.9346 | 132.4389412 | 0.49784904 |
| 6326.5 | 0.0718 | -0.0006 | 0.0824 | 116.5987 | 153.1880108 | 0.76114769 |
| 6327 | 0.0745 | 0.0012 | 0.0881 | 119.0232 | 136.6774969 | 0.87083245 |
| 6327.5 | 0.106 | 0.0084 | 0.1551 | 48.772 | 49.3709411 | 0.98786855 |
| 6328 | 0.1873 | 0.0437 | 0.2709 | 32.2162 | 14.73457955 | 2.18643497 |
| 6328.5 | 0.3027 | 0.1072 | 0.3475 | 9.8259 | 6.943128533 | 1.41519777 |
| 6329 | 0.4029 | 0.1551 | 0.3387 | 6.0422 | 5.232886074 | 1.15465919 |
| 6329.5 | 0.4513 | 0.1653 | 0.3031 | 6.0222 | 5.043854718 | 1.19396778 |
| 6330 | 0.4309 | 0.1593 | 0.28 | 7.4992 | 5.730834604 | 1.30857031 |
| 6330.5 | 0.364 | 0.153 | 0.2231 | 10.5432 | 8.647194097 | 1.21926256 |
| 6331 | 0.2979 | 0.1325 | 0.1278 | 19.358 | 17.25970356 | 1.12157199 |
| 6331.5 | 0.2431 | 0.1012 | 0.0501 | 34.2391 | 38.47721706 | 0.88985386 |
| 6332 | 0.1953 | 0.0689 | 0.0178 | 88.7463 | 76.4102751 | 1.16144458 |
| 6332.5 | 0.1567 | 0.0361 | 0.0119 | 317.6869 | 126.4335709 | 2.51267838 |
| 6333 | 0.1253 | 0.0136 | -0.0094 | 1626.356 | 283.0262993 | 5.74630592 |
| 6333.5 | 0.1037 | 0.0082 | -0.0335 | 8430.625 | 831.7281281 | 10.136275 |
| 6334 | 0.0925 | 0.0061 | -0.0411 | 4973.644 | 1625.68154 | 3.0594206 |
| 6334.5 | 0.0894 | -0.0057 | -0.0277 | 1510.068 | 1097.723793 | 1.37563539 |
| 6335 | 0.0937 | -0.0138 | -0.0149 | 617.993 | 648.7461784 | 0.95259598 |
| 6335.5 | 0.0981 | -0.0199 | -0.0069 | 332.5936 | 473.8242434 | 0.70193454 |
| 6336 | 0.0966 | -0.0228 | -0.0067 | 219.9414 | 488.6780621 | 0.45007422 |
| 6336.5 | 0.0942 | -0.0324 | -0.0032 | 164.128 | 476.0660228 | 0.3447589 |
| 6337 | 0.0938 | -0.0363 | -0.0006 | 136.9596 | 452.2327068 | 0.30285204 |
| 6337.5 | 0.0916 | -0.0375 | 0.0031 | 119.2919 | 436.9721166 | 0.2729966 |
| 6338 | 0.0884 | -0.0311 | 0.0044 | 97.5855 | 456.4340458 | 0.21379978 |
| 6338.5 | 0.0898 | -0.017 | -0.0061 | 83.7362 | 569.83149 | 0.14694906 |
| 6339 | 0.0931 | -0.0086 | -0.0166 | 85.5746 | 691.4075133 | 0.12376869 |
| 6339.5 | 0.0918 | -0.0063 | -0.0208 | 105.7239 | 811.7096899 | 0.13024841 |
| 6340 | 0.086 | -0.0039 | -0.019 | 134.8652 | 919.4864939 | 0.14667448 |
| 6340.5 | 0.0788 | 0.0051 | -0.0239 | 160.5803 | 1410.995535 | 0.11380638 |
| 6341 | 0.0732 | 0.0051 | -0.0222 | 180.3293 | 1653.218671 | 0.10907771 |
| 6341.5 | 0.0725 | -0.0055 | -0.015 | 202.0303 | 1277.380594 | 0.15815983 |
| 6342 | 0.0732 | -0.0193 | -0.0049 | 236.5727 | 882.2703153 | 0.26814084 |
| 6342.5 | 0.0722 | -0.0199 | -0.0066 | 306.302 | 962.1946228 | 0.31833684 |
| 6343 | 0.0694 | -0.0087 | -0.0202 | 471.6335 | 1785.998991 | 0.26407266 |

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|---|---|---|---|---|---|---|
| 6343.5 | 0.0658 | -0.0034 | -0.0258 | 842.5502 | 2787.258181 | 0.30228639 |
| 6344 | 0.0653 | -0.0048 | -0.0212 | 1522.244 | 2259.764662 | 0.67362944 |
| 6344.5 | 0.0699 | -0.005 | -0.0124 | 1587.677 | 1277.380594 | 1.24291578 |
| 6345 | 0.0745 | -0.0002 | -0.006 | 1156.305 | 876.7412726 | 1.31886731 |
| 6345.5 | 0.0706 | 0.0015 | -0.0039 | 1025.536 | 928.4010806 | 1.10462603 |
| 6346 | 0.0565 | 0.001 | -0.0017 | 1224.101 | 1416.537185 | 0.86415049 |
| 6346.5 | 0.0413 | 0.0018 | 0.0003 | 1796.069 | 2561.860746 | 0.70107995 |
| 6347 | 0.0331 | 0.0117 | -0.0063 | 2851.373 | 6593.505503 | 0.43245172 |
| 6347.5 | 0.0309 | 0.0137 | -0.0093 | 4306.436 | 10484.08698 | 0.41075923 |
| 6348 | 0.0317 | 0.0038 | -0.0053 | 2966.29 | 6810.166616 | 0.43556787 |
| 6348.5 | 0.039 | -0.0052 | 0.0014 | 911.0222 | 2728.263075 | 0.33392022 |
| 6349 | 0.058 | -0.0084 | -0.0025 | 321.4842 | 1378.40318 | 0.23322944 |
| 6349.5 | 0.0871 | -0.0097 | -0.0094 | 168.7517 | 668.6532961 | 0.25237549 |
| 6350 | 0.1132 | -0.012 | -0.0087 | 81.1776 | 353.5950329 | 0.22957789 |
| 6350.5 | 0.1224 | -0.0059 | -0.0095 | 66.6546 | 299.4430275 | 0.22259526 |
| 6351 | 0.11 | 0.0023 | -0.0119 | 81.381 | 405.0585599 | 0.20091169 |
| 6351.5 | 0.0877 | 0.0061 | -0.0172 | 132.0048 | 824.1373154 | 0.16017331 |
| 6352 | 0.0732 | 0.0119 | -0.0282 | 236.7545 | 2163.711113 | 0.10942057 |
| 6352.5 | 0.0667 | 0.0179 | -0.0372 | 320.4433 | 5364.000947 | 0.05973961 |
| 6353 | 0.0591 | 0.0299 | -0.0457 | 437.2123 | 29263.80968 | 0.01494038 |
| 6353.5 | 0.0501 | 0.0356 | -0.0446 | 436.8311 | 198530.1167 | 0.00220033 |
| 6354 | 0.0426 | 0.0272 | -0.0316 | 413.1139 | 44731.33987 | 0.00923545 |
| 6354.5 | 0.0366 | 0.0163 | -0.0174 | 382.2337 | 13505.4338 | 0.02830222 |
| 6355 | 0.0314 | 0.0101 | -0.0078 | 328.1281 | 8666.532576 | 0.03786152 |
| 6355.5 | 0.0282 | 0.0088 | 0.0003 | 306.2528 | 5776.831913 | 0.05301397 |
| 6356 | 0.0275 | 0.0033 | 0.0101 | 281.2051 | 3183.84791 | 0.0883224 |
| 6356.5 | 0.027 | 0.0059 | 0.0067 | 255.2482 | 4029.042915 | 0.06335207 |
| 6357 | 0.0259 | 0.0069 | -0.0019 | 239.5808 | 8358.955448 | 0.02866157 |
| 6357.5 | 0.0258 | -0.0002 | -0.0009 | 271.9096 | 7722.84972 | 0.03520845 |
| 6358 | 0.0256 | -0.0138 | 0.0157 | 342.9671 | 2602.037607 | 0.13180713 |
| 6358.5 | 0.0239 | -0.0144 | 0.023 | 440.6943 | 1979.632469 | 0.2226142 |
| 6359 | 0.0218 | -0.0073 | 0.0157 | 525.3441 | 3202.129964 | 0.16406083 |
| 6359.5 | 0.0207 | 0.0016 | 0 | 576.7094 | 11488.67483 | 0.05019808 |
| 6360 | 0.0202 | 0.014 | -0.0137 | 664.6039 | 138625.2886 | 0.00479425 |
| 6360.5 | 0.0191 | 0.0185 | -0.0161 | 905.1151 | 730794.8573 | 0.00123854 |
| 6361 | 0.0169 | 0.0093 | -0.0054 | 1396.006 | 40654.23782 | 0.0343385 |
| 6361.5 | 0.0148 | -0.0019 | 0.0082 | 1745.071 | 9159.912661 | 0.19051177 |
| 6362 | 0.014 | -0.0032 | 0.0149 | 1597.095 | 5606.293346 | 0.2848753 |
| 6362.5 | 0.0144 | 0.0037 | 0.0162 | 1478.632 | 4957.983912 | 0.29823245 |
| 6363 | 0.017 | 0.0155 | 0.0086 | 1069.633 | 7275.959194 | 0.14700917 |
| 6363.5 | 0.0274 | 0.0256 | -0.0014 | 434.5024 | 7037.42018 | 0.06174172 |
| 6364 | 0.0502 | 0.0289 | -0.0084 | 187.3832 | 2535.579164 | 0.07390154 |
| 6364.5 | 0.0854 | 0.0163 | 0 | 92.314 | 545.7223721 | 0.16915927 |
| 6365 | 0.1234 | 0.0019 | 0.0158 | 48.6955 | 190.889405 | 0.25509797 |
| 6365.5 | 0.1483 | 0.0043 | 0.017 | 39.3637 | 131.9227042 | 0.29838457 |
| 6366 | 0.1546 | 0.0148 | 0.008 | 39.3465 | 136.6774969 | 0.28787841 |
| 6366.5 | 0.1493 | 0.019 | -0.0012 | 47.1622 | 167.0755134 | 0.28228074 |
| 6367 | 0.1419 | 0.0108 | 0.0022 | 65.3314 | 177.2060812 | 0.36867471 |
| 6367.5 | 0.1368 | 0.0033 | 0.0019 | 94.8599 | 192.3719684 | 0.49310667 |
| 6368 | 0.135 | 0.0063 | -0.0064 | 132.0808 | 226.327902 | 0.5835816 |
| 6368.5 | 0.1354 | 0.0164 | -0.0183 | 165.2617 | 276.827261 | 0.59698492 |
| 6369 | 0.1325 | 0.0126 | -0.0169 | 183.7079 | 284.6078253 | 0.64547733 |

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|---|---|---|---|---|---|---|
| 6369.5 | 0.1263 | 0.0067 | -0.0074 | 177.9257 | 267.8953607 | 0.66416118 |
| 6370 | 0.1237 | 0.0079 | 0.0004 | 136.0084 | 244.341283 | 0.55663291 |
| 6370.5 | 0.1261 | 0.0084 | 0.0043 | 112.9391 | 219.6642382 | 0.51414423 |
| 6371 | 0.1305 | 0.0001 | 0.0046 | 113.6455 | 203.5622206 | 0.55828385 |
| 6371.5 | 0.1364 | -0.0027 | -0.0009 | 127.1306 | 202.2724317 | 0.62851175 |
| 6372 | 0.141 | 0.0034 | -0.0087 | 129.547 | 212.9376786 | 0.60837988 |
| 6372.5 | 0.1406 | 0.005 | -0.0082 | 122.5571 | 212.5920463 | 0.57648958 |
| 6373 | 0.1389 | 0.0006 | -0.0014 | 119.2577 | 195.9996876 | 0.60845862 |
| 6373.5 | 0.1402 | -0.002 | 0.0012 | 112.1176 | 184.5610065 | 0.6074826 |
| 6374 | 0.1435 | 0.0049 | -0.0045 | 95.3734 | 191.4804148 | 0.49808436 |
| 6374.5 | 0.1467 | 0.0118 | -0.0112 | 78.9344 | 202.2724317 | 0.39023805 |
| 6375 | 0.145 | 0.0163 | -0.0108 | 69.2723 | 206.5086612 | 0.33544501 |
| 6375.5 | 0.1404 | 0.0165 | -0.0075 | 67.7954 | 210.8761535 | 0.32149391 |
| 6376 | 0.1372 | 0.0152 | -0.0098 | 73.8038 | 230.936144 | 0.31958531 |
| 6376.5 | 0.1321 | 0.0172 | -0.0201 | 84.8095 | 304.640354 | 0.27839221 |
| 6377 | 0.1269 | 0.011 | -0.0239 | 91.0925 | 364.7591097 | 0.24973331 |
| 6377.5 | 0.1288 | 0.0019 | -0.023 | 84.0002 | 344.3197978 | 0.24395983 |
| 6378 | 0.1383 | -0.0006 | -0.0245 | 68.4051 | 294.3745881 | 0.23237434 |
| 6378.5 | 0.151 | 0.0063 | -0.025 | 55.1907 | 236.4882177 | 0.23337611 |
| 6379 | 0.162 | 0.0024 | -0.0184 | 46.9979 | 178.5353151 | 0.26324148 |
| 6379.5 | 0.1674 | -0.0062 | -0.0105 | 42.8112 | 147.5763795 | 0.2900952 |
| 6380 | 0.1678 | -0.0219 | -0.0016 | 40.6412 | 130.3915621 | 0.31168581 |
| 6380.5 | 0.1667 | -0.0249 | 0.0015 | 39.5582 | 127.0809049 | 0.31128359 |
| 6381 | 0.1643 | -0.0136 | 0.0003 | 41.5228 | 133.1318735 | 0.31189225 |
| 6381.5 | 0.161 | -0.0066 | 0.0053 | 47.9444 | 130.2230444 | 0.3681714 |
| 6382 | 0.1605 | -0.0115 | 0.0108 | 53.2707 | 122.1878012 | 0.43597396 |
| 6382.5 | 0.1636 | -0.0265 | 0.0194 | 50.0589 | 106.0074377 | 0.47222064 |
| 6383 | 0.1674 | -0.0329 | 0.0208 | 43.6378 | 99.80998702 | 0.43720875 |
| 6383.5 | 0.1727 | -0.0271 | 0.0231 | 38.6078 | 91.66613119 | 0.42117846 |
| 6384 | 0.176 | -0.011 | 0.0177 | 35.4555 | 93.81612604 | 0.37792543 |
| 6384.5 | 0.1686 | 0.0018 | 0.0097 | 35.8609 | 112.1064996 | 0.31988243 |
| 6385 | 0.1455 | 0.007 | 0.0016 | 42.6791 | 169.5270223 | 0.25175396 |
| 6385.5 | 0.1158 | 0.0072 | 0.0002 | 60.8725 | 282.5019847 | 0.21547636 |
| 6386 | 0.0995 | 0.008 | -0.0021 | 97.7427 | 411.3432953 | 0.23761831 |
| 6386.5 | 0.0989 | 0.0241 | -0.017 | 141.1684 | 597.0982405 | 0.23642408 |
| 6387 | 0.1035 | 0.0359 | -0.0232 | 127.0914 | 622.9708961 | 0.20400857 |
| 6387.5 | 0.1168 | 0.0273 | -0.013 | 89.9889 | 358.7417068 | 0.25084594 |
| 6388 | 0.1411 | 0.0029 | 0.0105 | 64.8429 | 158.8923168 | 0.40809336 |
| 6388.5 | 0.1607 | -0.0104 | 0.0228 | 49.251 | 105.387386 | 0.46733297 |
| 6389 | 0.1656 | -0.0088 | 0.0219 | 41.4391 | 100.6128486 | 0.41186688 |
| 6389.5 | 0.1667 | -0.0079 | 0.0188 | 39.8236 | 102.9595807 | 0.38678868 |
| 6390 | 0.1686 | 0.0005 | 0.0042 | 41.4306 | 119.9187639 | 0.34548888 |
| 6390.5 | 0.1688 | 0.0075 | -0.01 | 43.4852 | 143.8061996 | 0.30238752 |
| 6391 | 0.1743 | 0.0141 | -0.0164 | 44.8527 | 145.5742632 | 0.30810872 |
| 6391.5 | 0.1841 | 0.0118 | -0.0137 | 44.9904 | 123.5795361 | 0.36406028 |
| 6392 | 0.1895 | 0.0089 | -0.0131 | 42.0054 | 114.7187038 | 0.36615999 |
| 6392.5 | 0.1899 | 0.0017 | -0.0122 | 36.596 | 112.9219087 | 0.32408237 |
| 6393 | 0.1908 | -0.0048 | -0.0088 | 32.2053 | 107.2636808 | 0.30024422 |
| 6393.5 | 0.1941 | -0.0083 | -0.003 | 30.3195 | 96.58189071 | 0.31392531 |
| 6394 | 0.1962 | -0.0026 | -0.0008 | 31.0193 | 92.07004968 | 0.33690978 |
| 6394.5 | 0.1962 | 0.0037 | -0.0013 | 34.6162 | 92.57862496 | 0.37391136 |
| 6395 | 0.1927 | 0.0029 | 0.0013 | 40.9969 | 93.50448893 | 0.43844847 |

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|---|---|---|---|---|---|---|
| 6395.5 | 0.1889 | 0.0005 | 0.0062 | 46.9719 | 92.37470213 | 0.50849311 |
| 6396 | 0.1951 | 0.0008 | 0.0044 | 46.6825 | 88.04991583 | 0.53018222 |
| 6396.5 | 0.2037 | 0.0025 | 0.0004 | 43.7468 | 83.83854257 | 0.52179819 |
| 6397 | 0.2031 | -0.0017 | -0.0021 | 43.7264 | 86.64323451 | 0.50467183 |
| 6397.5 | 0.1976 | -0.0109 | 0.0056 | 47.4159 | 84.63894033 | 0.56021377 |
| 6398 | 0.1917 | -0.0189 | 0.0172 | 54.9708 | 79.75144014 | 0.68927658 |
| 6398.5 | 0.1739 | -0.0297 | 0.0314 | 70.0142 | 82.78848572 | 0.84569973 |
| 6399 | 0.1367 | -0.0292 | 0.03 | 102.6522 | 129.5521547 | 0.79236197 |
| 6399.5 | 0.117 | -0.0173 | 0.0201 | 176.3568 | 197.231216 | 0.89416272 |
| 6400 | 0.1467 | -0.0054 | 0.0106 | 184.6635 | 146.7707206 | 1.25817669 |
| 6400.5 | 0.1856 | 0.0049 | 0.0059 | 181.3336 | 96.14867569 | 1.88597085 |
| 6401 | 0.1927 | 0.0006 | 0.0141 | 90.2589 | 81.5028004 | 1.10743311 |
| 6401.5 | 0.184 | -0.0036 | 0.0245 | 47.2941 | 80.08075383 | 0.5905801 |
| 6402 | 0.1772 | 0.0013 | 0.0323 | 33.3668 | 79.26117779 | 0.4209728 |
| 6402.5 | 0.1702 | 0.0121 | 0.0327 | 29.4888 | 84.90822832 | 0.34730203 |
| 6403 | 0.1596 | 0.0193 | 0.029 | 32.2187 | 99.35541692 | 0.32427724 |
| 6403.5 | 0.1415 | 0.019 | 0.0199 | 44.3555 | 138.8716482 | 0.31939925 |
| 6404 | 0.1212 | 0.0138 | 0.0099 | 73.8882 | 217.1502797 | 0.34026297 |
| 6404.5 | 0.1115 | 0.008 | 0.0044 | 129.9505 | 283.0262993 | 0.45914638 |
| 6405 | 0.1151 | 0.0027 | 0.0038 | 190.5883 | 267.8953607 | 0.71142815 |
| 6405.5 | 0.1241 | -0.0021 | 0.0062 | 220.8316 | 220.0268526 | 1.0036575 |
| 6406 | 0.13 | -0.0023 | -0.0009 | 199.4126 | 224.4474932 | 0.88845991 |
| 6406.5 | 0.1351 | -0.0071 | -0.0042 | 151.6332 | 217.8642343 | 0.69599859 |
| 6407 | 0.1486 | -0.0118 | 0.0022 | 95.5818 | 160.7101461 | 0.59474652 |
| 6407.5 | 0.1671 | -0.0035 | 0.0047 | 61.5712 | 121.4245177 | 0.50707387 |
| 6408 | 0.1788 | 0.0108 | -0.0012 | 48.0064 | 113.0586546 | 0.42461499 |
| 6408.5 | 0.1788 | 0.0114 | -0.0033 | 44.3384 | 115.9872817 | 0.3822695 |
| 6409 | 0.1678 | 0.0039 | -0.0032 | 47.6448 | 133.1318735 | 0.35787673 |
| 6409.5 | 0.1485 | -0.005 | -0.0049 | 60.6125 | 178.5353151 | 0.33949866 |
| 6410 | 0.1272 | -0.0156 | -0.0002 | 84.028 | 232.5027961 | 0.36140641 |
| 6410.5 | 0.1061 | -0.0186 | 0.0052 | 107.0375 | 308.7746064 | 0.34665253 |
| 6411 | 0.0856 | -0.0183 | 0.0066 | 116.0667 | 462.8440658 | 0.25076847 |
| 6411.5 | 0.0702 | -0.0161 | 0.0042 | 132.5771 | 734.0478463 | 0.18061098 |
| 6412 | 0.0603 | -0.013 | 0.0015 | 203.685 | 1093.908404 | 0.18619932 |
| 6412.5 | 0.0552 | -0.0059 | 0.0001 | 367.5911 | 1389.143617 | 0.26461706 |
| 6413 | 0.0541 | 0 | 0.0012 | 850.7952 | 1389.143617 | 0.61246022 |
| 6413.5 | 0.055 | -0.0043 | 0.0038 | 2177.138 | 1217.432606 | 1.7883026 |
| 6414 | 0.0561 | -0.0066 | 0.0011 | 1710.341 | 1291.828074 | 1.32396968 |
| 6414.5 | 0.0602 | 0.0016 | -0.004 | 543.1144 | 1341.754627 | 0.40477923 |
| 6415 | 0.0727 | 0.0157 | -0.0096 | 286.4703 | 1046.027393 | 0.27386501 |
| 6415.5 | 0.0948 | 0.0177 | -0.0058 | 131.1639 | 499.3645011 | 0.26266164 |
| 6416 | 0.1246 | 0.0107 | 0.0002 | 56.8173 | 241.4041999 | 0.23536169 |
| 6416.5 | 0.1563 | -0.0075 | 0.0115 | 34.6167 | 127.7331063 | 0.27100805 |
| 6417 | 0.1764 | -0.0175 | 0.0172 | 27.9783 | 93.92034329 | 0.29789393 |
| 6417.5 | 0.1751 | -0.0185 | 0.0161 | 27.5227 | 96.47331926 | 0.2852882 |
| 6418 | 0.1576 | -0.0005 | 0.001 | 32.8637 | 144.196373 | 0.22790934 |
| 6418.5 | 0.1399 | 0.0211 | -0.0051 | 46.4379 | 204.5374852 | 0.22703858 |
| 6419 | 0.1342 | 0.0527 | 0.0139 | 64.9063 | 167.0755134 | 0.38848482 |
| 6419.5 | 0.1395 | 0.1472 | 0.0402 | 59.7804 | 110.2371088 | 0.54228926 |
| 6420 | 0.1503 | 0.3119 | 0.0423 | 57.4563 | 94.97190998 | 0.60498204 |
| 6420.5 | 0.1682 | 0.4504 | 0.0458 | 28.0859 | 75.72103952 | 0.37091276 |
| 6421 | 0.1849 | 0.4444 | 0.1052 | 17.1389 | 39.36665945 | 0.43536587 |

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|---|---|---|---|---|---|---|
| 6421.5 | 0.1791 | 0.3139 | 0.1752 | 16.9051 | 25.61286749 | 0.66002372 |
| 6422 | 0.146 | 0.1698 | 0.1522 | 31.5472 | 37.10348951 | 0.85024887 |
| 6422.5 | 0.1091 | 0.0709 | 0.0573 | 67.0494 | 130.0548456 | 0.51554711 |
| 6423 | 0.0893 | 0.0221 | -0.0253 | 165.3158 | 1014.656954 | 0.16292778 |
| 6423.5 | 0.083 | 0.0069 | -0.0555 | 584.792 | 6237.935623 | 0.09374768 |
| 6424 | 0.0788 | 0.0002 | -0.0537 | 1413.108 | 7591.151851 | 0.18615197 |
| 6424.5 | 0.0801 | 0.0036 | -0.0517 | 1018.607 | 5820.653531 | 0.17499879 |
| 6425 | 0.0922 | 0.0067 | -0.05 | 604.7735 | 2484.18772 | 0.24344919 |
| 6425.5 | 0.1028 | 0.0044 | -0.0458 | 399.9567 | 1301.593108 | 0.30728244 |
| 6426 | 0.103 | 0.0058 | -0.044 | 281.9664 | 1208.577084 | 0.23330444 |
| 6426.5 | 0.0999 | 0.0132 | -0.0447 | 206.1544 | 1394.559868 | 0.14782757 |
| 6427 | 0.0964 | 0.0182 | -0.0368 | 158.2229 | 1182.569631 | 0.13379584 |
| 6427.5 | 0.0932 | 0.0125 | -0.0198 | 122.1062 | 755.7177996 | 0.16157645 |
| 6428 | 0.1005 | 0.0095 | -0.009 | 94.368 | 470.4904667 | 0.20057367 |
| 6428.5 | 0.1231 | 0.0071 | -0.0051 | 76.105 | 272.3076639 | 0.27948167 |
| 6429 | 0.1496 | 0.0003 | 0.001 | 67.9093 | 161.1693635 | 0.42135365 |
| 6429.5 | 0.1662 | -0.0038 | 0.0071 | 62.8562 | 119.1761278 | 0.52742274 |
| 6430 | 0.1726 | 0.0035 | 0.0071 | 57.6494 | 110.2371088 | 0.5229582 |
| 6430.5 | 0.1772 | 0.016 | 0.0026 | 51.2771 | 110.1053324 | 0.46570951 |
| 6431 | 0.1892 | 0.0178 | 0.0099 | 41.9245 | 88.43068133 | 0.4740945 |
| 6431.5 | 0.2009 | 0.0143 | 0.025 | 33.408 | 67.40409526 | 0.49563754 |
| 6432 | 0.198 | 0.0209 | 0.0402 | 30.6734 | 60.14248968 | 0.51001214 |
| 6432.5 | 0.1862 | 0.0483 | 0.0306 | 35.9538 | 73.63405758 | 0.48827677 |
| 6433 | 0.1693 | 0.0548 | 0.0129 | 54.1137 | 107.0106936 | 0.50568498 |
| 6433.5 | 0.1499 | 0.0331 | -0.003 | 100.6618 | 170.0236437 | 0.59204589 |
| 6434 | 0.1363 | 0.0052 | -0.008 | 224.1992 | 227.4672457 | 0.9856329 |
| 6434.5 | 0.1304 | -0.0049 | -0.0119 | 260.1867 | 269.8433544 | 0.96421385 |
| 6435 | 0.1338 | 0.0003 | -0.0139 | 128.5255 | 263.1145934 | 0.48847728 |
| 6435.5 | 0.1414 | 0.0164 | -0.0194 | 67.6258 | 253.4734898 | 0.26679634 |
| 6436 | 0.1474 | 0.0329 | -0.0234 | 47.7941 | 244.7651357 | 0.19526515 |
| 6436.5 | 0.1508 | 0.0337 | -0.0167 | 44.4376 | 206.8398946 | 0.21484057 |
| 6437 | 0.1473 | 0.0147 | 0.0007 | 52.7178 | 167.3183188 | 0.31507488 |
| 6437.5 | 0.138 | 0.0039 | 0.0036 | 79.2752 | 184.0010009 | 0.43084113 |
| 6438 | 0.1293 | 0.008 | -0.0056 | 110.921 | 246.0431769 | 0.45081925 |
| 6438.5 | 0.1276 | 0.0206 | -0.0132 | 113.1704 | 291.0651622 | 0.38881465 |
| 6439 | 0.1326 | 0.0276 | -0.0119 | 95.9603 | 259.3794407 | 0.36996109 |
| 6439.5 | 0.1371 | 0.023 | -0.0047 | 82.7149 | 212.5920463 | 0.38907806 |
| 6440 | 0.1364 | 0.0189 | 0.0027 | 83.4124 | 191.1845753 | 0.43629252 |
| 6440.5 | 0.1281 | 0.0209 | 0.0067 | 90.9436 | 204.5374852 | 0.44463048 |
| 6441 | 0.1149 | 0.0182 | 0.0091 | 98.5784 | 244.7651357 | 0.4027469 |
| 6441.5 | 0.1123 | 0.0086 | 0.0093 | 103.6418 | 255.269539 | 0.40600927 |
| 6442 | 0.1333 | 0.0061 | 0.0069 | 99.7574 | 187.9740726 | 0.53069766 |
| 6442.5 | 0.1654 | 0.0124 | 0.002 | 72.796 | 128.3902235 | 0.56699021 |
| 6443 | 0.1862 | 0.0114 | 0.0022 | 47.8979 | 99.58232196 | 0.48098798 |
| 6443.5 | 0.1964 | 0.009 | 0.0085 | 37.7045 | 83.1363531 | 0.45352603 |
| 6444 | 0.2084 | 0.0305 | 0.0496 | 35.5829 | 50.6551741 | 0.70245341 |
| 6444.5 | 0.2183 | 0.1321 | 0.0965 | 36.0395 | 33.02414057 | 1.09130773 |
| 6445 | 0.2254 | 0.2617 | 0.1366 | 34.6587 | 24.45584952 | 1.41719469 |
| 6445.5 | 0.2453 | 0.3074 | 0.171 | 28.6667 | 18.10849664 | 1.58305245 |
| 6446 | 0.2696 | 0.246 | 0.2108 | 23.4352 | 13.30943847 | 1.76079555 |
| 6446.5 | 0.2684 | 0.165 | 0.2416 | 21.9503 | 11.70389189 | 1.87547016 |
| 6447 | 0.2431 | 0.1364 | 0.2361 | 22.717 | 13.38119933 | 1.69768041 |

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|---|---|---|---|---|---|---|
| 6447.5 | 0.2228 | 0.1381 | 0.1854 | 24.4708 | 18.88988132 | 1.29544488 |
| 6448 | 0.2162 | 0.1164 | 0.1156 | 28.7419 | 29.49320432 | 0.97452619 |
| 6448.5 | 0.2077 | 0.0617 | 0.0601 | 38.1624 | 46.75342689 | 0.81624819 |
| 6449 | 0.189 | 0.0135 | 0.0368 | 47.1356 | 67.46829177 | 0.69863337 |
| 6449.5 | 0.1747 | -0.0029 | 0.0312 | 44.7568 | 82.27067015 | 0.54401891 |
| 6450 | 0.1745 | -0.0017 | 0.0208 | 43.2361 | 92.17143672 | 0.4690835 |
| 6450.5 | 0.1774 | -0.0049 | 0.0159 | 51.9658 | 94.23401471 | 0.5514548 |
| 6451 | 0.1742 | -0.0139 | 0.0122 | 68.647 | 101.8937341 | 0.67371169 |
| 6451.5 | 0.1618 | -0.0131 | -0.0002 | 80.6914 | 138.5023888 | 0.58259934 |
| 6452 | 0.1475 | 0.0007 | -0.0164 | 79.0097 | 217.1502797 | 0.36384802 |
| 6452.5 | 0.1388 | 0.0114 | -0.0252 | 76.4439 | 295.4899862 | 0.25870217 |
| 6453 | 0.1298 | -0.0005 | -0.0104 | 81.2934 | 265.4892114 | 0.30620227 |
| 6453.5 | 0.1217 | -0.0135 | 0.0061 | 89.7312 | 229.3849099 | 0.39118179 |
| 6454 | 0.1218 | -0.025 | 0.0183 | 87.118 | 188.2626594 | 0.4627471 |
| 6454.5 | 0.1261 | -0.0245 | 0.0211 | 74.6543 | 169.2795082 | 0.44101203 |
| 6455 | 0.1265 | -0.0085 | 0.0121 | 64.2804 | 192.6705047 | 0.33362865 |
| 6455.5 | 0.1214 | 0.0032 | 0.0041 | 64.1398 | 238.518555 | 0.26890906 |
| 6456 | 0.1123 | 0.0014 | -0.001 | 82.8684 | 308.7746064 | 0.26837829 |
| 6456.5 | 0.1038 | -0.0061 | 0.0006 | 124.1806 | 354.323623 | 0.35047226 |
| 6457 | 0.1011 | -0.0072 | 0.0016 | 145.1775 | 367.0538016 | 0.39552104 |
| 6457.5 | 0.103 | -0.0106 | 0.0058 | 130.4209 | 324.2306412 | 0.4022473 |
| 6458 | 0.1068 | -0.0206 | 0.0138 | 116.0134 | 259.8420706 | 0.44647658 |
| 6458.5 | 0.1116 | -0.0262 | 0.0198 | 125.8945 | 216.0857585 | 0.58261359 |
| 6459 | 0.113 | -0.017 | 0.0196 | 159.006 | 211.9032431 | 0.75037077 |
| 6459.5 | 0.1122 | -0.0068 | 0.0134 | 184.4394 | 238.1104498 | 0.77459599 |
| 6460 | 0.1177 | -0.0012 | 0.0021 | 174.0157 | 263.5870207 | 0.66018311 |
| 6460.5 | 0.1354 | 0.0006 | -0.0083 | 112.2322 | 232.1096766 | 0.4835309 |
| 6461 | 0.159 | -0.0027 | -0.009 | 77.466 | 162.5586086 | 0.47654197 |
| 6461.5 | 0.1762 | -0.0107 | -0.0006 | 64.6846 | 115.8453165 | 0.55837044 |
| 6462 | 0.1863 | -0.0168 | 0.0074 | 57.3699 | 93.81612604 | 0.61151427 |
| 6462.5 | 0.1953 | -0.0097 | 0.0079 | 48.6318 | 84.63894033 | 0.5745795 |
| 6463 | 0.2033 | 0.0098 | -0.0043 | 41.4986 | 88.52624962 | 0.46877169 |
| 6463.5 | 0.1997 | 0.0207 | -0.0114 | 39.3746 | 99.69605928 | 0.3949464 |
| 6464 | 0.1803 | 0.0184 | -0.0126 | 43.8915 | 127.8969228 | 0.3431787 |
| 6464.5 | 0.1597 | 0.0116 | -0.0126 | 54.0445 | 169.5270223 | 0.31879578 |
| 6465 | 0.152 | 0.0083 | -0.0143 | 55.8219 | 195.3881445 | 0.28569748 |
| 6465.5 | 0.1576 | 0.0068 | -0.0094 | 45.2419 | 166.8332239 | 0.2711804 |
| 6466 | 0.1681 | -0.0015 | -0.0002 | 37.073 | 127.569597 | 0.29061 |
| 6466.5 | 0.1717 | -0.0172 | 0.0153 | 34.9846 | 101.1921273 | 0.34572452 |
| 6467 | 0.1661 | -0.0189 | 0.0133 | 38.9379 | 110.6338273 | 0.35195293 |
| 6467.5 | 0.1609 | -0.0139 | 0.0058 | 48.2487 | 129.5521547 | 0.37242684 |
| 6468 | 0.1612 | -0.0121 | 0.0027 | 52.9681 | 134.3573502 | 0.39423299 |
| 6468.5 | 0.1687 | -0.0203 | 0.0111 | 46.7393 | 110.1053324 | 0.42449624 |
| 6469 | 0.1819 | -0.0196 | 0.019 | 39.9573 | 86.73598527 | 0.46067731 |
| 6469.5 | 0.1915 | 0.0005 | 0.0269 | 36.2716 | 72.47913757 | 0.50044194 |
| 6470 | 0.1945 | 0.0413 | 0.039 | 33.8559 | 62.77538395 | 0.53931809 |
| 6470.5 | 0.1962 | 0.1049 | 0.051 | 30.7746 | 55.53310765 | 0.55416672 |
| 6471 | 0.2008 | 0.1899 | 0.0602 | 29.8266 | 49.41161961 | 0.60363534 |
| 6471.5 | 0.2016 | 0.249 | 0.0753 | 38.2197 | 43.51227848 | 0.87836586 |
| 6472 | 0.1906 | 0.2344 | 0.0782 | 82.5661 | 46.38026885 | 1.78019882 |
| 6472.5 | 0.1699 | 0.1533 | 0.0582 | 465.0872 | 66.01411674 | 7.04526885 |
| 6473 | 0.1409 | 0.0782 | 0.0164 | 287.1448 | 146.7707206 | 1.95641746 |

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|---|---|---|---|---|---|---|
| 6473.5 | 0.1111 | 0.0376 | -0.0108 | 424.6578 | 386.1972475 | 1.09958785 |
| 6474 | 0.0934 | 0.0196 | -0.0155 | 362.3521 | 664.9678465 | 0.54491672 |
| 6474.5 | 0.0864 | 0.0044 | -0.0096 | 289.1281 | 685.6138105 | 0.42170694 |
| 6475 | 0.0815 | -0.0036 | -0.0082 | 259.7419 | 757.9361733 | 0.34269627 |
| 6475.5 | 0.0744 | -0.0139 | -0.0063 | 254.6433 | 887.850594 | 0.28680873 |
| 6476 | 0.0659 | -0.0177 | -0.0026 | 272.0862 | 1038.934585 | 0.26188964 |
| 6476.5 | 0.0611 | -0.0093 | -0.0018 | 276.9322 | 1195.469745 | 0.23165137 |
| 6477 | 0.0587 | 0.0027 | -0.0095 | 264.532 | 1785.998991 | 0.14811431 |
| 6477.5 | 0.0558 | 0.0049 | -0.0212 | 250.7664 | 3807.084951 | 0.06586835 |
| 6478 | 0.0558 | -0.0049 | -0.0218 | 192.1849 | 3952.997217 | 0.04861751 |
| 6478.5 | 0.0594 | -0.0115 | -0.0185 | 140.4529 | 2657.058204 | 0.0528603 |
| 6479 | 0.0634 | -0.0124 | -0.01 | 122.0218 | 1497.588435 | 0.08147886 |
| 6479.5 | 0.0643 | -0.0097 | -0.0011 | 132.3979 | 1042.472151 | 0.12700378 |
| 6480 | 0.0596 | -0.0095 | 0.007 | 158.0578 | 931.4007589 | 0.16969902 |
| 6480.5 | 0.0548 | -0.0108 | 0.0155 | 161.7042 | 829.1865165 | 0.19501547 |
| 6481 | 0.0565 | -0.003 | 0.014 | 124.3808 | 824.1373154 | 0.15092242 |
| 6481.5 | 0.0626 | 0.0081 | 0.01 | 92.0687 | 773.7353617 | 0.11899249 |
| 6482 | 0.0677 | 0.0108 | 0.0103 | 73.243 | 663.1362734 | 0.11044939 |
| 6482.5 | 0.0713 | -0.0005 | 0.0213 | 62.3444 | 458.5561884 | 0.13595804 |
| 6483 | 0.0753 | -0.021 | 0.0427 | 56.1168 | 272.3076639 | 0.20607867 |
| 6483.5 | 0.0786 | -0.0387 | 0.0604 | 51.2966 | 191.4804148 | 0.26789476 |
| 6484 | 0.0802 | -0.036 | 0.062 | 46.3989 | 182.3358424 | 0.25446944 |
| 6484.5 | 0.0822 | -0.0172 | 0.0533 | 41.5176 | 202.2724317 | 0.20525585 |
| 6485 | 0.0857 | 0.0033 | 0.0438 | 37.6174 | 222.9596008 | 0.16871846 |
| 6485.5 | 0.089 | 0.0153 | 0.0413 | 35.1895 | 220.0268526 | 0.15993275 |
| 6486 | 0.0914 | 0.0075 | 0.0456 | 33.9245 | 197.5408694 | 0.17173408 |
| 6486.5 | 0.0943 | -0.0037 | 0.051 | 33.2192 | 174.0744812 | 0.19083326 |
| 6487 | 0.0966 | -0.0064 | 0.0509 | 32.1457 | 168.5401346 | 0.19073024 |
| 6487.5 | 0.0982 | -0.0039 | 0.0501 | 30.5265 | 166.5914489 | 0.1832417 |
| 6488 | 0.1041 | -0.0014 | 0.055 | 29.1217 | 143.2238336 | 0.20332999 |
| 6488.5 | 0.1113 | 0.0042 | 0.0563 | 28.1438 | 128.0610474 | 0.21976862 |
| 6489 | 0.1116 | 0.0062 | 0.0608 | 27.3482 | 120.5177647 | 0.22692256 |
| 6489.5 | 0.1068 | 0.0048 | 0.0685 | 26.845 | 116.271978 | 0.23088108 |
| 6490 | 0.1026 | -0.002 | 0.078 | 26.5355 | 109.0593805 | 0.2433124 |
| 6490.5 | 0.0996 | -0.0031 | 0.0755 | 25.9909 | 116.5576992 | 0.22298741 |
| 6491 | 0.0999 | 0.0012 | 0.067 | 25.2929 | 129.2186074 | 0.19573729 |
| 6491.5 | 0.1023 | 0.0067 | 0.0616 | 25.2216 | 134.3573502 | 0.18772028 |
| 6492 | 0.1018 | 0.0109 | 0.0606 | 26.2978 | 137.0396455 | 0.19189921 |
| 6492.5 | 0.0994 | 0.0153 | 0.0562 | 27.9858 | 150.2399934 | 0.18627397 |
| 6493 | 0.0986 | 0.02 | 0.0488 | 29.4579 | 168.7860659 | 0.17452803 |
| 6493.5 | 0.0998 | 0.0285 | 0.0339 | 30.954 | 208.1726422 | 0.14869389 |
| 6494 | 0.0991 | 0.0308 | 0.0274 | 33.0569 | 234.4831017 | 0.14097775 |
| 6494.5 | 0.096 | 0.0268 | 0.03 | 34.7563 | 236.4882177 | 0.14696842 |
| 6495 | 0.0964 | 0.0247 | 0.0334 | 35.1226 | 221.8531459 | 0.15831464 |
| 6495.5 | 0.0984 | 0.0252 | 0.0331 | 36.454 | 215.7326169 | 0.16897769 |
| 6496 | 0.0939 | 0.0139 | 0.043 | 41.817 | 197.8512355 | 0.21135577 |
| 6496.5 | 0.085 | -0.0064 | 0.0546 | 53.9348 | 189.715376 | 0.28429325 |
| 6497 | 0.0838 | -0.0215 | 0.0619 | 76.88 | 173.0486214 | 0.4442682 |
| 6497.5 | 0.0932 | -0.0195 | 0.0599 | 111.3493 | 155.5641499 | 0.71577738 |
| 6498 | 0.1145 | 0.0021 | 0.0343 | 116.6142 | 165.3902403 | 0.70508514 |
| 6498.5 | 0.1448 | 0.0131 | 0.01 | 75.7782 | 151.9142885 | 0.49882207 |
| 6499 | 0.1618 | 0.0119 | -0.0039 | 48.0661 | 145.5742632 | 0.33018268 |

~8% ϕ

wet

~16,000ppm

0.14 to 0.72

| | | | | | | |
|---|---|---|---|---|---|---|
| 6499.5 | 0.1575 | 0.0126 | -0.0088 | 38.9264 | 165.6294645 | 0.23502099 |
| 6500 | 0.1409 | 0.0202 | -0.0192 | 43.7205 | 254.8187829 | 0.17157487 |
| 6500.5 | 0.1133 | 0.017 | -0.0258 | 68.2767 | 517.9512269 | 0.13182071 |
| 6501 | 0.0809 | -0.0011 | -0.0236 | 141.0121 | 1286.985764 | 0.10956772 |
| 6501.5 | 0.0576 | -0.0098 | -0.0204 | 262.6033 | 3257.908325 | 0.08060488 |
| 6502 | 0.0465 | -0.0056 | -0.0166 | 507.6927 | 5210.904636 | 0.0974289 |
| 6502.5 | 0.042 | 0.0022 | -0.0121 | 1059.071 | 5210.904636 | 0.20324127 |
| 6503 | 0.0403 | 0.0034 | -0.0097 | 982.9468 | 4957.983912 | 0.19825534 |
| 6503.5 | 0.0404 | -0.0003 | -0.006 | 583.9097 | 3854.832649 | 0.15147472 |
| 6504 | 0.0437 | -0.01 | 0.0045 | 410.8216 | 1866.616274 | 0.22008894 |
| 6504.5 | 0.0511 | -0.0201 | 0.0137 | 370.6375 | 987.9157688 | 0.37517115 |
| 6505 | 0.0587 | -0.0221 | 0.0112 | 396.9242 | 839.4218165 | 0.47285428 |
| 6505.5 | 0.0642 | -0.0119 | 0.0002 | 427.384 | 1001.155564 | 0.4268907 |
| 6506 | 0.0682 | -0.0063 | -0.0061 | 388.9363 | 1082.578106 | 0.35926858 |
| 6506.5 | 0.0708 | -0.0085 | -0.0062 | 308.0783 | 994.5033869 | 0.30978105 |
| 6507 | 0.0758 | -0.0018 | -0.0141 | 230.689 | 1097.723793 | 0.21015214 |
| 6507.5 | 0.0884 | 0.002 | -0.0176 | 166.879 | 816.6475738 | 0.20434641 |
| 6508 | 0.1129 | 0.0019 | -0.0112 | 104.0876 | 374.8574369 | 0.2776725 |
| 6508.5 | 0.1376 | -0.0013 | 0.0022 | 64.9055 | 189.1323251 | 0.34317508 |
| 6509 | 0.1454 | -0.0081 | 0.0135 | 52.9495 | 143.6116927 | 0.36869909 |
| 6509.5 | 0.1416 | -0.0128 | 0.0096 | 55.5756 | 159.7974443 | 0.34778779 |
| 6510 | 0.1338 | -0.0041 | -0.0065 | 65.7618 | 231.3263537 | 0.28428149 |
| 6510.5 | 0.1262 | 0.0094 | -0.0213 | 74.2298 | 350.7025152 | 0.2116603 |
| 6511 | 0.1263 | 0.0142 | -0.023 | 75.7028 | 362.4853749 | 0.20884374 |
| 6511.5 | 0.1354 | 0.0069 | -0.0107 | 73.871 | 241.820606 | 0.30547852 |
| 6512 | 0.1519 | -0.003 | -0.0003 | 67.7165 | 158.8923168 | 0.42617857 |
| 6512.5 | 0.1691 | -0.0079 | 0.0026 | 59.0077 | 121.5766145 | 0.48535403 |
| 6513 | 0.1762 | -0.0082 | 0.0048 | 51.9981 | 108.5418562 | 0.47906035 |
| 6513.5 | 0.1762 | 0.0065 | 0.0082 | 49.105 | 104.2846071 | 0.47087486 |
| 6514 | 0.1777 | 0.0508 | 0.0044 | 50.5891 | 107.1370778 | 0.4721904 |
| 6514.5 | 0.1811 | 0.1139 | -0.0126 | 50.6759 | 126.5949507 | 0.40029954 |
| 6515 | 0.1859 | 0.1562 | -0.0265 | 43.6151 | 142.6449163 | 0.30575993 |
| 6515.5 | 0.185 | 0.166 | -0.0335 | 37.105 | 159.1178931 | 0.23319188 |
| 6516 | 0.1771 | 0.1348 | -0.0246 | 47.2213 | 156.8830472 | 0.30099683 |
| 6516.5 | 0.1703 | 0.0946 | 0.0015 | 87.2137 | 121.4245177 | 0.71825445 |
| 6517 | 0.174 | 0.0862 | 0.092 | 82.3337 | 47.4362841 | 1.73566926 |
| 6517.5 | 0.2119 | 0.1259 | 0.2466 | 42.7947 | 14.71385931 | 2.90846195 |
| 6518 | 0.2672 | 0.1693 | 0.3899 | 22.3662 | 6.787323133 | 3.29529029 |
| 6518.5 | 0.2777 | 0.1959 | 0.4206 | 12.0362 | 5.955466551 | 2.02103394 |
| 6519 | 0.2512 | 0.207 | 0.3514 | 12.3317 | 8.176050333 | 1.50827105 |
| 6519.5 | 0.2332 | 0.2122 | 0.2409 | 20.0755 | 13.69259542 | 1.46615739 |
| 6520 | 0.2224 | 0.1996 | 0.1371 | 29.4284 | 24.82295938 | 1.18553149 |
| 6520.5 | 0.2083 | 0.1513 | 0.0669 | 31.2029 | 44.09222923 | 0.70767345 |
| 6521 | 0.1868 | 0.0791 | 0.0388 | 35.2161 | 67.5969538 | 0.5209717 |
| 6521.5 | 0.1595 | 0.0161 | 0.0374 | 47.3712 | 90.56864921 | 0.52304192 |
| 6522 | 0.1343 | -0.0061 | 0.0318 | 64.6502 | 130.5603995 | 0.49517465 |
| 6522.5 | 0.1133 | -0.0128 | 0.0266 | 81.49 | 188.8417838 | 0.43152526 |
| 6523 | 0.0948 | -0.0122 | 0.0044 | 119.0788 | 395.463208 | 0.30111221 |
| 6523.5 | 0.0753 | -0.0159 | -0.0151 | 201.6249 | 1157.374006 | 0.17420894 |
| 6524 | 0.0543 | -0.0255 | -0.0228 | 433.1435 | 4658.418368 | 0.09298081 |
| 6524.5 | 0.0429 | -0.0313 | -0.0136 | 1122.1 | 5443.030857 | 0.20615356 |
| 6525 | 0.0492 | -0.0252 | -0.0058 | 1548.55 | 2338.854804 | 0.66209771 |

0.08 to 0.17

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|---|---|---|---|---|---|---|
| 6525.5 | 0.062 | -0.0091 | -0.0014 | 746.7178 | 1141.011544 | 0.65443492 |
| 6526 | 0.0678 | 0.0055 | 0.0012 | 385.9659 | 863.1387911 | 0.44716551 |
| 6526.5 | 0.0712 | 0.0098 | 0.0024 | 275.3994 | 751.3094983 | 0.36655919 |
| 6527 | 0.0862 | 0.0165 | -0.0032 | 242.4015 | 580.214104 | 0.4177794 |
| 6527.5 | 0.1228 | 0.0345 | 0.0087 | 366.734 | 215.7326169 | 1.69994693 |
| 6528 | 0.1976 | 0.0934 | 0.0523 | 210.7524 | 54.25112262 | 3.88475648 |
| 6528.5 | 0.2831 | 0.186 | 0.1353 | 89.4436 | 17.91364969 | 4.99304171 |
| 6529 | 0.3174 | 0.2509 | 0.2525 | 67.9832 | 9.218050174 | 7.37500867 |
| 6529.5 | 0.3129 | 0.2322 | 0.3809 | 21.1688 | 6.038825007 | 3.50545015 |
| 6530 | 0.2942 | 0.1702 | 0.4226 | 14.1578 | 5.629897492 | 2.51475271 |
| 6530.5 | 0.2467 | 0.1126 | 0.328 | 15.7028 | 9.053314477 | 1.73448078 |
| 6531 | 0.1837 | 0.0722 | 0.1642 | 25.276 | 26.63662266 | 0.9489191 |
| 6531.5 | 0.1345 | 0.0414 | 0.0539 | 43.2008 | 99.58232196 | 0.43381997 |
| 6532 | 0.1073 | 0.0291 | 0.008 | 57.9663 | 286.2023329 | 0.20253608 |
| 6532.5 | 0.0955 | 0.0168 | -0.0012 | 77.0196 | 440.96695 | 0.17466071 |
| 6533 | 0.0885 | 0.0006 | 0.0021 | 104.1305 | 480.5964463 | 0.21666931 |
| 6533.5 | 0.0831 | -0.0082 | 0.0028 | 119.0076 | 538.9157522 | 0.22082784 |
| 6534 | 0.0885 | -0.006 | -0.0008 | 105.7097 | 515.415001 | 0.20509628 |
| 6534.5 | 0.1066 | 0.0047 | -0.002 | 137.8455 | 352.8686358 | 0.39064254 |
| 6535 | 0.1257 | 0.0252 | 0.0038 | 156.5322 | 222.9596008 | 0.7020653 |
| 6535.5 | 0.1329 | 0.0705 | 0.0077 | 103.3286 | 186.8261829 | 0.55307344 |
| 6536 | 0.1429 | 0.1394 | 0.0269 | 46.3187 | 124.5202992 | 0.3719771 |
| 6536.5 | 0.2024 | 0.1956 | 0.1212 | 23.6802 | 31.12346041 | 0.76084727 |
| 6537 | 0.2791 | 0.2083 | 0.2172 | 13.0589 | 12.40954872 | 1.05232674 |
| 6537.5 | 0.2781 | 0.1818 | 0.2052 | 15.1706 | 13.13832711 | 1.15468277 |
| 6538 | 0.2261 | 0.1979 | 0.0753 | 31.7875 | 36.26170304 | 0.87661354 |
| 6538.5 | 0.2035 | 0.3026 | -0.0284 | 67.1709 | 116.5576992 | 0.57628883 |
| 6539 | 0.208 | 0.4481 | -0.04 | 113.6491 | 127.4063941 | 0.89202038 |
| 6539.5 | 0.22 | 0.4982 | 0.0069 | 78.5584 | 66.76702325 | 1.1766048 |
| 6540 | 0.2367 | 0.415 | 0.0561 | 33.8533 | 38.59031953 | 0.8772485 |
| 6540.5 | 0.2423 | 0.2629 | 0.0605 | 27.605 | 35.90219967 | 0.76889439 |
| 6541 | 0.2152 | 0.1187 | 0.0377 | 39.4483 | 52.87692571 | 0.74603997 |
| 6541.5 | 0.1616 | 0.0234 | 0.0241 | 61.022 | 102.7213189 | 0.5940539 |
| 6542 | 0.1188 | -0.0203 | 0.0235 | 80.9813 | 182.0604639 | 0.44480443 |
| 6542.5 | 0.1035 | -0.0258 | 0.0174 | 84.1164 | 258.4577941 | 0.32545507 |
| 6543 | 0.101 | -0.0105 | 0.006 | 72.8092 | 336.0710154 | 0.21664826 |
| 6543.5 | 0.1003 | 0.0032 | -0.0054 | 66.2661 | 434.9945577 | 0.15233777 |
| 6544 | 0.1014 | -0.0002 | -0.0066 | 68.0121 | 435.9816944 | 0.1559976 |
| 6544.5 | 0.1045 | -0.0174 | -0.0001 | 77.0577 | 354.323623 | 0.2174783 |
| 6545 | 0.1031 | -0.0405 | 0.0207 | 97.0134 | 245.616079 | 0.39497984 |
| 6545.5 | 0.0982 | -0.0517 | 0.0379 | 123.0871 | 200.3600867 | 0.61432944 |
| 6546 | 0.096 | -0.0454 | 0.0338 | 130.9869 | 221.8531459 | 0.59042165 |
| 6546.5 | 0.0957 | -0.0309 | 0.0177 | 122.3881 | 296.6115872 | 0.41262076 |
| 6547 | 0.102 | -0.0133 | 0.0078 | 81.6617 | 317.9150948 | 0.25686638 |
| 6547.5 | 0.1281 | 0.0291 | 0.0186 | 59.9813 | 170.5223996 | 0.35175027 |
| 6548 | 0.1823 | 0.193 | -0.0053 | 54.4424 | 113.8842478 | 0.47805031 |
| 6548.5 | 0.2462 | 0.4642 | -0.0843 | 45.9468 | 137.9511913 | 0.33306563 |
| 6549 | 0.2823 | 0.632 | -0.1084 | 28.2913 | 118.2938261 | 0.23916126 |
| 6549.5 | 0.2887 | 0.5538 | -0.0327 | 16.111 | 51.50984639 | 0.31277515 |
| 6550 | 0.2826 | 0.3395 | 0.0444 | 12.6322 | 30.43186103 | 0.41509785 |
| 6550.5 | 0.2568 | 0.1614 | 0.0354 | 14.0419 | 38.76088864 | 0.36226982 |
| 6551 | 0.2168 | 0.058 | 0.0058 | 21.4842 | 69.57081423 | 0.30881053 |

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|---|---|---|---|---|---|---|
| 6551.5 | 0.1812 | 0.0108 | 0.0003 | 37.16 | 107.8999956 | 0.34439297 |
| 6552 | 0.1572 | 0.0006 | 0.0028 | 53.8115 | 141.497321 | 0.38030049 |
| 6552.5 | 0.1464 | -0.0074 | 0.0107 | 70.6645 | 147.1727423 | 0.48014666 |
| 6553 | 0.1408 | -0.0274 | 0.0236 | 87.1038 | 133.4803331 | 0.65255905 |
| 6553.5 | 0.1342 | -0.0426 | 0.0272 | 100.6497 | 138.8716482 | 0.72476781 |
| 6554 | 0.1386 | -0.0375 | 0.0152 | 95.5616 | 154.0458699 | 0.6203451 |
| 6554.5 | 0.1673 | -0.0154 | -0.0047 | 69.6469 | 136.6774969 | 0.50957108 |
| 6555 | 0.2007 | 0.0022 | -0.0159 | 50.7904 | 103.7999039 | 0.48931067 |
| 6555.5 | 0.2102 | 0.0072 | -0.0154 | 42.3911 | 92.68083379 | 0.45738799 |
| 6556 | 0.2038 | 0.004 | -0.0084 | 38.8779 | 92.07004968 | 0.42226435 |
| 6556.5 | 0.1978 | 0.0045 | -0.0103 | 36.0683 | 100.6128486 | 0.35848602 |
| 6557 | 0.1956 | -0.0018 | -0.0064 | 33.0827 | 98.67922869 | 0.33525495 |
| 6557.5 | 0.1958 | -0.015 | 0.0046 | 30.983 | 87.20192822 | 0.35530178 |
| 6558 | 0.1912 | -0.0277 | 0.0173 | 30.8982 | 80.08075383 | 0.38583803 |
| 6558.5 | 0.1829 | -0.0281 | 0.0251 | 33.1408 | 80.49520486 | 0.41171148 |
| 6559 | 0.1732 | -0.0122 | 0.0188 | 35.4479 | 95.61114925 | 0.37075069 |
| 6559.5 | 0.1603 | 0.0108 | 0.0082 | 35.2725 | 126.5949507 | 0.27862486 |
| 6560 | 0.1465 | 0.024 | -0.0015 | 34.7433 | 174.8497338 | 0.19870376 |
| 6560.5 | 0.1267 | 0.0161 | 0.0094 | 36.4171 | 200.3600867 | 0.18175826 |
| 6561 | 0.0983 | 0.0038 | 0.0233 | 43.0428 | 255.269539 | 0.16861706 |
| 6561.5 | 0.0754 | 0.003 | 0.0237 | 62.5749 | 396.3216734 | 0.15788917 |
| 6562 | 0.0675 | 0.0126 | 0.015 | 134.6553 | 587.8008243 | 0.22908321 |
| 6562.5 | 0.0618 | 0.0159 | 0.0108 | 227.7798 | 773.7353617 | 0.2943898 |
| 6563 | 0.0526 | 0.0133 | 0.0091 | 477.0327 | 1097.723793 | 0.43456533 |
| 6563.5 | 0.0539 | 0.0091 | 0.0108 | 393.4632 | 991.2015597 | 0.39695579 |
| 6564 | 0.0639 | 0.0087 | 0.0039 | 330.037 | 896.3184546 | 0.368214 |
| 6564.5 | 0.0677 | 0.0069 | -0.0047 | 96.9044 | 1049.600427 | 0.09232504 |
| 6565 | 0.072 | 0.0024 | -0.0105 | 56.4565 | 1105.413289 | 0.05107275 |
| 6565.5 | 0.1006 | 0.0032 | -0.0088 | 44.9284 | 467.1909437 | 0.0961671 |
| 6566 | 0.1418 | 0.0021 | -0.0015 | 42.9762 | 187.6861335 | 0.22897909 |
| 6566.5 | 0.1665 | -0.0069 | 0.0055 | 47.9312 | 121.1211594 | 0.39572937 |
| 6567 | 0.1859 | -0.0211 | 0.0092 | 57.4032 | 92.37470213 | 0.62141689 |
| 6567.5 | 0.2019 | -0.0214 | 0.0127 | 62.9667 | 75.26659811 | 0.83658225 |
| 6568 | 0.2024 | 0.0363 | 0.0174 | 71.8845 | 71.49022284 | 1.00551512 |
| 6568.5 | 0.2033 | 0.2227 | -0.0113 | 84.7276 | 95.61114925 | 0.88616862 |
| 6569 | 0.2234 | 0.4437 | -0.0451 | 84.2529 | 112.1064996 | 0.7515434 |
| 6569.5 | 0.2557 | 0.529 | -0.0235 | 29.3414 | 63.53344678 | 0.46182604 |
| 6570 | 0.2688 | 0.4346 | 0.0307 | 16.3336 | 36.75809558 | 0.44435381 |
| 6570.5 | 0.2434 | 0.2687 | 0.0415 | 14.1993 | 40.92770706 | 0.34693612 |
| 6571 | 0.1979 | 0.1271 | 0.0111 | 22.5849 | 79.66942175 | 0.28348267 |
| 6571.5 | 0.1615 | 0.0401 | -0.004 | 82.3152 | 146.3703058 | 0.56237636 |
| 6572 | 0.1413 | -0.0001 | 0.0029 | 100.4887 | 176.9419749 | 0.56791895 |
| 6572.5 | 0.1314 | -0.0155 | 0.0111 | 283.1029 | 181.5115318 | 1.5596965 |
| 6573 | 0.1355 | -0.02 | 0.012 | 344.8927 | 168.5401346 | 2.04635353 |
| 6573.5 | 0.1526 | -0.0095 | 0.0103 | 133.0354 | 136.1368975 | 0.9772178 |
| 6574 | 0.1734 | 0.0361 | 0.0372 | 54.3358 | 78.37376159 | 0.6932907 |
| 6574.5 | 0.1902 | 0.1559 | 0.0688 | 33.4137 | 50.23561084 | 0.66513972 |
| 6575 | 0.1951 | 0.321 | 0.0731 | 16.3362 | 46.60363767 | 0.35053487 |
| 6575.5 | 0.199 | 0.4185 | 0.0717 | 12.2605 | 45.68319081 | 0.26838099 |
| 6576 | 0.2131 | 0.3671 | 0.0761 | 12.323 | 39.6305281 | 0.31094716 |
| 6576.5 | 0.2165 | 0.2156 | 0.0682 | 15.4473 | 40.98954767 | 0.37685949 |
| 6577 | 0.1978 | 0.0848 | 0.031 | 24.5552 | 65.58065303 | 0.3744275 |

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|---|---|---|---|---|---|---|
| 6577.5 | 0.1814 | 0.0235 | 0.0049 | 43.1528 | 102.0113611 | 0.42301955 |
| 6578 | 0.1726 | 0.0035 | 0.0031 | 60.7645 | 115.7036056 | 0.52517378 |
| 6578.5 | 0.1617 | 0.0035 | -0.0023 | 69.7412 | 142.6449163 | 0.48891472 |
| 6579 | 0.1591 | 0.0029 | -0.0056 | 67.046 | 154.6938911 | 0.43341078 |
| 6579.5 | 0.1687 | 0.0034 | -0.0042 | 63.3106 | 133.3059365 | 0.47492709 |
| 6580 | 0.1773 | 0.0133 | -0.0027 | 58.9089 | 117.2765187 | 0.50230771 |
| 6580.5 | 0.1789 | 0.0603 | -0.0019 | 50.9484 | 113.8842478 | 0.44737004 |
| 6581 | 0.1772 | 0.2078 | -0.0412 | 39.9103 | 200.6769664 | 0.19887833 |
| 6581.5 | 0.1861 | 0.4107 | -0.1119 | 29.4913 | 738.3083562 | 0.03994442 |
| 6582 | 0.2099 | 0.5047 | -0.1486 | 22.5215 | 1113.181961 | 0.02023164 |
| 6582.5 | 0.2121 | 0.3722 | -0.0978 | 19.311 | 291.6129356 | 0.06622134 |
| 6583 | 0.1843 | 0.159 | -0.0289 | 21.0634 | 150.6560231 | 0.1398112 |
| 6583.5 | 0.1656 | 0.0225 | 0.0137 | 30.5273 | 110.7665318 | 0.2756004 |
| 6584 | 0.1605 | -0.0248 | 0.0318 | 47.8934 | 95.29074428 | 0.50260285 |
| 6584.5 | 0.1524 | -0.0317 | 0.0343 | 60.9814 | 101.5420429 | 0.60055321 |
| 6585 | 0.1428 | -0.0188 | 0.0221 | 64.1814 | 132.611678 | 0.48398 |
| 6585.5 | 0.1367 | -0.0019 | 0.0489 | 69.6875 | 102.8403487 | 0.677628 |
| 6586 | 0.1361 | 0.0339 | 0.1294 | 88.0767 | 47.62855992 | 1.8492413 |
| 6586.5 | 0.1499 | 0.0828 | 0.2368 | 117.1323 | 21.22030932 | 5.51982057 |
| 6587 | 0.1906 | 0.116 | 0.3011 | 52.9641 | 12.66049635 | 4.18341418 |
| 6587.5 | 0.2365 | 0.1125 | 0.3082 | 22.9401 | 10.15939447 | 2.25801844 |
| 6588 | 0.2516 | 0.0916 | 0.2575 | 17.9525 | 11.74842156 | 1.52807762 |
| 6588.5 | 0.2394 | 0.0713 | 0.1579 | 24.6142 | 20.02171455 | 1.22937523 |
| 6589 | 0.2164 | 0.0433 | 0.0612 | 55.7209 | 43.27671998 | 1.28754906 |
| 6589.5 | 0.1866 | 0.0161 | 0.0077 | 76.7342 | 93.19436615 | 0.8233781 |
| 6590 | 0.1575 | 0.0055 | -0.0067 | 77.7132 | 160.7101461 | 0.48356126 |
| 6590.5 | 0.1355 | 0.0064 | -0.0022 | 83.3543 | 209.5180092 | 0.39783835 |
| 6591 | 0.1251 | 0.0072 | 0.0076 | 61.9055 | 211.5600671 | 0.2926143 |
| 6591.5 | 0.1276 | 0.0056 | 0.0147 | 46.4465 | 182.0604639 | 0.2551158 |
| 6592 | 0.1382 | 0.0109 | 0.0113 | 37.1821 | 163.7297565 | 0.22709433 |
| 6592.5 | 0.1609 | 0.0168 | 0.0162 | 33.1928 | 113.7460368 | 0.291815 |
| 6593 | 0.1913 | 0.0355 | 0.0328 | 31.6187 | 68.57347981 | 0.46109225 |
| 6593.5 | 0.2088 | 0.0712 | 0.0483 | 29.1089 | 51.03718534 | 0.57034689 |
| 6594 | 0.2133 | 0.1318 | 0.0454 | 24.7112 | 50.36094356 | 0.49068183 |
| 6594.5 | 0.2163 | 0.2008 | 0.0499 | 20.5454 | 47.3596921 | 0.43381616 |
| 6595 | 0.2206 | 0.2488 | 0.0785 | 19.2093 | 36.86386714 | 0.52108749 |
| 6595.5 | 0.2203 | 0.2304 | 0.1093 | 21.6573 | 29.91807825 | 0.72388674 |
| 6596 | 0.1899 | 0.1658 | 0.0787 | 29.8057 | 46.45455051 | 0.64160991 |
| 6596.5 | 0.128 | 0.0853 | 0.0331 | 49.5877 | 139.4282474 | 0.35565031 |
| 6597 | 0.0824 | 0.0271 | 0.0087 | 114.9455 | 474.9431952 | 0.24201947 |
| 6597.5 | 0.0741 | -0.0031 | 0.0054 | 213.9799 | 636.5270343 | 0.33616781 |
| 6598 | 0.0768 | -0.0152 | 0.0058 | 257.4765 | 586.2718993 | 0.43917592 |
| 6598.5 | 0.0763 | -0.0219 | 0.0062 | 254.0213 | 587.8008243 | 0.4321554 |
| 6599 | 0.075 | -0.0179 | -0.002 | 216.0308 | 764.6488345 | 0.28252289 |
| 6599.5 | 0.0744 | -0.01 | -0.0161 | 200.7622 | 1239.991726 | 0.16190608 |
| 6600 | 0.076 | -0.0004 | -0.0347 | 185.8503 | 2602.037607 | 0.07142491 |
| 6600.5 | 0.0803 | -0.002 | -0.0363 | 158.62 | 2270.821125 | 0.06985138 |
| 6601 | 0.088 | -0.0052 | -0.0343 | 128.0042 | 1479.658407 | 0.08650929 |
| 6601.5 | 0.099 | -0.007 | -0.0299 | 93.4001 | 860.4554275 | 0.10854728 |
| 6602 | 0.1112 | -0.003 | -0.0205 | 70.1887 | 479.4579377 | 0.14639178 |
| 6602.5 | 0.1224 | 0.042 | -0.023 | 60.533 | 393.7544307 | 0.15373287 |
| 6603 | 0.1353 | 0.1618 | -0.0631 | 55.13 | 782.9809674 | 0.0704104 |

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|---|---|---|---|---|---|---|
| 6603.5 | 0.1514 | 0.302 | -0.11 | 47.0928 | 2588.543376 | 0.01819278 |
| 6604 | 0.1637 | 0.369 | -0.11 | 36.2532 | 1479.658407 | 0.02450106 |
| 6604.5 | 0.169 | 0.3317 | -0.0568 | 29.1162 | 303.4740341 | 0.09594297 |
| 6605 | 0.1705 | 0.2082 | 0.009 | 27.4963 | 110.5013557 | 0.24883224 |
| 6605.5 | 0.1623 | 0.0755 | 0.0424 | 31.7985 | 83.31109036 | 0.38168388 |
| 6606 | 0.1391 | -0.0074 | 0.0408 | 47.5975 | 109.9737866 | 0.43280768 |
| 6606.5 | 0.117 | -0.032 | 0.0271 | 94.5649 | 177.2060812 | 0.53364365 |
| 6607 | 0.1094 | -0.0282 | 0.0183 | 193.3387 | 229.7712839 | 0.84143979 |
| 6607.5 | 0.1104 | -0.0138 | 0.0054 | 212.2233 | 283.5520409 | 0.74844568 |
| 6608 | 0.1125 | -0.0082 | -0.0032 | 175.6594 | 321.0501166 | 0.54714012 |
| 6608.5 | 0.1143 | -0.0095 | -0.004 | 166.3428 | 314.8247219 | 0.52836638 |
| 6609 | 0.1144 | -0.0058 | -0.0031 | 176.9473 | 308.7746064 | 0.57306299 |
| 6609.5 | 0.1145 | 0.0011 | -0.0018 | 168.5947 | 300.5867001 | 0.56088543 |
| 6610 | 0.1239 | -0.0006 | 0.003 | 151.7817 | 232.8968919 | 0.651712 |
| 6610.5 | 0.142 | -0.0033 | 0.0049 | 130.0571 | 170.0236437 | 0.76493538 |
| 6611 | 0.1552 | 0 | 0.0019 | 112.2884 | 147.1727423 | 0.76297009 |
| 6611.5 | 0.1547 | -0.0036 | 0.0047 | 110.0756 | 142.6449163 | 0.77167559 |
| 6612 | 0.1409 | -0.0179 | 0.0195 | 118.5495 | 140.7397573 | 0.84233128 |
| 6612.5 | 0.1213 | -0.0294 | 0.0274 | 118.1204 | 165.6294645 | 0.71316055 |
| 6613 | 0.1037 | -0.0353 | 0.023 | 89.5361 | 233.688025 | 0.38314372 |
| 6613.5 | 0.0938 | -0.0356 | 0.0155 | 55.7187 | 321.0501166 | 0.17355141 |
| 6614 | 0.0943 | -0.0252 | 0.014 | 41.3767 | 327.4575427 | 0.12635745 |
| 6614.5 | 0.0995 | -0.0072 | 0.0135 | 38.0288 | 298.8735807 | 0.12724042 |
| 6615 | 0.0969 | 0.0106 | 0.011 | 42.0929 | 330.073056 | 0.12752601 |
| 6615.5 | 0.0803 | 0.009 | 0.0142 | 61.8378 | 438.9628753 | 0.14087251 |
| 6616 | 0.0601 | 0.0001 | 0.0128 | 208.1518 | 766.9057506 | 0.27141771 |
| 6616.5 | 0.0496 | -0.0031 | 0.0084 | 132.178 | 1253.822312 | 0.10542004 |
| 6617 | 0.057 | -0.0011 | 0.0069 | 190.933 | 1018.073974 | 0.18754335 |
| 6617.5 | 0.0908 | -0.0011 | 0.0087 | 53.5851 | 392.9040962 | 0.13638214 |
| 6618 | 0.143 | -0.004 | 0.0115 | 32.7538 | 152.549202 | 0.21470974 |
| 6618.5 | 0.1831 | 0.0007 | 0.0063 | 28.7204 | 98.45533056 | 0.29170995 |
| 6619 | 0.1918 | 0.0023 | 0.0013 | 31.9987 | 94.44398239 | 0.33881142 |
| 6619.5 | 0.1841 | -0.0017 | 0.0039 | 41.0616 | 100.0384155 | 0.41045832 |
| 6620 | 0.184 | 0.0036 | -0.0013 | 49.4428 | 106.3820374 | 0.46476643 |
| 6620.5 | 0.1917 | 0.0044 | -0.0048 | 49.1892 | 101.3085693 | 0.48553839 |
| 6621 | 0.1932 | 0.0121 | -0.0095 | 46.1335 | 105.1408525 | 0.43877807 |
| 6621.5 | 0.1855 | 0.0127 | -0.0033 | 46.1484 | 107.0106936 | 0.43125036 |
| 6622 | 0.1705 | 0.0096 | 0.0038 | 51.0806 | 117.7109319 | 0.4339495 |
| 6622.5 | 0.1525 | 0 | 0.0063 | 65.5111 | 143.8061996 | 0.45555129 |
| 6623 | 0.1375 | -0.0134 | 0.0088 | 98.8192 | 171.526363 | 0.57611669 |
| 6623.5 | 0.1228 | -0.0187 | 0.0094 | 171.1744 | 213.2841348 | 0.80256509 |
| 6624 | 0.1044 | -0.0097 | 0.0089 | 326.9867 | 297.1747281 | 1.10031799 |
| 6624.5 | 0.0852 | 0.006 | 0.0111 | 860.8163 | 421.5117281 | 2.04221198 |
| 6625 | 0.0726 | 0.014 | 0.0194 | 3095.842 | 465.0100631 | 6.65758022 |
| 6625.5 | 0.0693 | 0.0119 | 0.0222 | 15799.54 | 470.4904667 | 33.5809931 |
| 6626 | 0.0709 | 0.0094 | 0.0186 | 20000 | 493.3858093 | 40.5362287 |
| 6626.5 | 0.0705 | 0.007 | 0.0169 | 20000 | 519.2262015 | 38.5188574 |
| 6627 | 0.065 | 0.0072 | 0.0156 | 20000 | 617.9962507 | 32.3626559 |
| 6627.5 | 0.0534 | 0.0032 | 0.0194 | 2899.577 | 769.1724398 | 3.76973582 |
| 6628 | 0.0402 | 0.0042 | 0.0158 | 442.9239 | 1352.078547 | 0.3275874 |
| 6628.5 | 0.0371 | 0.017 | 0.0039 | 100.8541 | 2643.144389 | 0.03815686 |
| 6629 | 0.045 | 0.0401 | 0.0042 | 33.3872 | 1785.998991 | 0.01869385 |

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|---|---|---|---|---|---|---|
| 6629.5 | 0.0486 | 0.0667 | 0.0768 | 19.7433 | 238.9276858 | 0.08263295 |
| 6630 | 0.0458 | 0.1128 | 0.2225 | 7.7017 | 46.56630023 | 0.16539214 |
| 6630.5 | 0.0853 | 0.1738 | 0.3304 | 6.1634 | 18.16473755 | 0.33930576 |
| 6631 | 0.2227 | 0.2223 | 0.3103 | 6.6556 | 10.64492683 | 0.6252368 |
| 6631.5 | 0.3604 | 0.2533 | 0.2127 | 8.5713 | 9.107743727 | 0.94110026 |
| 6632 | 0.3518 | 0.2669 | 0.1834 | 12.1322 | 10.55107123 | 1.14985481 |
| 6632.5 | 0.2675 | 0.2731 | 0.2367 | 16.0807 | 11.9952712 | 1.34058661 |
| 6633 | 0.2328 | 0.2479 | 0.2812 | 21.8952 | 11.50894393 | 1.90245084 |
| 6633.5 | 0.2341 | 0.2047 | 0.2162 | 43.5394 | 15.29596898 | 2.84646236 |
| 6634 | 0.2237 | 0.138 | 0.1061 | 104.1321 | 29.87908404 | 3.48511687 |
| 6634.5 | 0.1906 | 0.0629 | 0.0352 | 348.5609 | 67.46829177 | 5.16629206 |
| 6635 | 0.1505 | 0.0078 | 0.0125 | 1709.388 | 135.9573937 | 12.5729705 |
| 6635.5 | 0.1266 | -0.0121 | 0.0054 | 11834.5 | 213.9795294 | 55.3067106 |
| 6636 | 0.1194 | -0.0059 | -0.0011 | 20000 | 270.8251418 | 73.8483874 |
| 6636.5 | 0.1122 | 0.0018 | -0.0032 | 8686.427 | 322.9529155 | 26.8968831 |
| 6637 | 0.0948 | 0.0084 | -0.0035 | 3467.336 | 472.7091496 | 7.33503086 |
| 6637.5 | 0.0715 | 0.0103 | 0 | 1915.556 | 799.554718 | 2.39577837 |
| 6638 | 0.0527 | 0.0121 | 0.0003 | 1180.426 | 1521.994421 | 0.77557807 |
| 6638.5 | 0.0431 | 0.0039 | 0.0042 | 583.6514 | 1943.814098 | 0.30026092 |
| 6639 | 0.0451 | -0.0018 | 0.0001 | 248.5352 | 2143.179494 | 0.11596565 |
| 6639.5 | 0.0623 | -0.0001 | -0.0055 | 171.5667 | 1311.466672 | 0.13082048 |
| 6640 | 0.0947 | 0.0086 | -0.0098 | 67.8129 | 552.6556905 | 0.1227037 |
| 6640.5 | 0.1353 | 0.0335 | 0.015 | 44.6954 | 161.8618023 | 0.27613309 |
| 6641 | 0.1749 | 0.1039 | 0.0743 | 38.7892 | 54.5792921 | 0.71069445 |
| 6641.5 | 0.2037 | 0.2299 | 0.1309 | 36.0076 | 28.96512563 | 1.24313633 |
| 6642 | 0.2222 | 0.3476 | 0.1624 | 28.6964 | 21.47020684 | 1.3365684 |
| 6642.5 | 0.2354 | 0.3731 | 0.2172 | 21.9689 | 15.12933706 | 1.45207288 |
| 6643 | 0.2352 | 0.3043 | 0.3026 | 23.3097 | 10.44170609 | 2.23236507 |
| 6643.5 | 0.2183 | 0.2012 | 0.3161 | 44.3702 | 10.58505975 | 4.19177606 |
| 6644 | 0.1842 | 0.1145 | 0.1974 | 126.7542 | 21.83474846 | 5.80515962 |
| 6644.5 | 0.1371 | 0.0454 | 0.0608 | 138.0168 | 89.58756295 | 1.54057991 |
| 6645 | 0.0996 | 0.0077 | -0.0036 | 217.895 | 424.3488496 | 0.51348083 |
| 6645.5 | 0.082 | 0.0004 | -0.0104 | 244.4585 | 797.1557484 | 0.30666341 |
| 6646 | 0.0747 | 0.0102 | -0.0142 | 235.4953 | 1145.070232 | 0.20566014 |
| 6646.5 | 0.0733 | 0.009 | -0.0187 | 214.5555 | 1427.716565 | 0.15027878 |
| 6647 | 0.0751 | -0.0044 | -0.0172 | 203.7988 | 1258.482753 | 0.16194008 |
| 6647.5 | 0.0758 | -0.0172 | -0.0125 | 216.3848 | 1038.934585 | 0.20827567 |
| 6648 | 0.0745 | -0.012 | -0.0136 | 245.3091 | 1128.96116 | 0.21728746 |
| 6648.5 | 0.072 | -0.0003 | -0.0208 | 234.5365 | 1639.365397 | 0.14306542 |
| 6649 | 0.0695 | 0.0002 | -0.0251 | 212.3341 | 2227.064496 | 0.09534259 |
| 6649.5 | 0.0655 | 0.0014 | -0.0313 | 204.7912 | 3903.462865 | 0.05246398 |
| 6650 | 0.0575 | -0.0012 | -0.027 | 234.706 | 4992.999535 | 0.04700701 |
| 6650.5 | 0.0489 | 0.0009 | -0.0023 | 339.2127 | 2007.134423 | 0.16900348 |
| 6651 | 0.0473 | 0.0121 | 0.101 | 467.0004 | 166.5914489 | 2.80326753 |
| 6651.5 | 0.0624 | 0.0441 | 0.3017 | 259.7135 | 24.15359169 | 10.752583 |
| 6652 | 0.1049 | 0.0774 | 0.5204 | 97.9374 | 7.551201485 | 12.9697771 |
| 6652.5 | 0.1732 | 0.0979 | 0.6452 | 57.128 | 4.233797632 | 13.4933232 |
| 6653 | 0.2331 | 0.1194 | 0.6453 | 23.5469 | 3.63636674 | 6.47539197 |
| 6653.5 | 0.2499 | 0.1695 | 0.5423 | 18.7755 | 4.54057944 | 4.13504493 |
| 6654 | 0.2333 | 0.2562 | 0.3419 | 19.8557 | 9.036403057 | 2.19730128 |
| 6654.5 | 0.2123 | 0.29 | 0.1374 | 22.8466 | 26.34271727 | 0.86728335 |
| 6655 | 0.1935 | 0.2259 | 0.0037 | 27.2698 | 90.27267719 | 0.30208254 |

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|---|---|---|---|---|---|---|
| 6655.5 | 0.1642 | 0.1086 | -0.0296 | 41.2339 | 205.1914694 | 0.20095329 |
| 6656 | 0.1273 | 0.0293 | -0.0203 | 67.7747 | 336.0710154 | 0.20166779 |
| 6656.5 | 0.1036 | 0.0092 | -0.015 | 125.6518 | 504.2241913 | 0.24919828 |
| 6657 | 0.0969 | 0.0068 | -0.008 | 318.6799 | 500.5729692 | 0.63663026 |
| 6657.5 | 0.0945 | 0.0003 | 0.0051 | 437.8834 | 392.0564495 | 1.11688865 |
| 6658 | 0.091 | -0.0052 | 0.0102 | 698.8546 | 378.8506863 | 1.84467028 |
| 6658.5 | 0.0837 | -0.001 | 0.0005 | 1266.548 | 562.581159 | 2.25131535 |
| 6659 | 0.0733 | 0.0053 | -0.0093 | 2890.839 | 1014.656954 | 2.84908026 |
| 6659.5 | 0.0647 | 0.011 | -0.013 | 4937.343 | 1605.467478 | 3.07533031 |
| 6660 | 0.0594 | 0.0109 | -0.0133 | 2923.138 | 2054.230583 | 1.42298432 |
| 6660.5 | 0.0552 | 0.0078 | -0.0108 | 1513.404 | 2227.064496 | 0.67955113 |
| 6661 | 0.0504 | 0.0117 | -0.0123 | 1061.28 | 3094.692358 | 0.34293548 |
| 6661.5 | 0.0446 | 0.0195 | -0.0127 | 1015.974 | 4533.735834 | 0.22409202 |
| 6662 | 0.0381 | 0.0199 | -0.0084 | 1158.092 | 5286.640932 | 0.21906001 |
| 6662.5 | 0.0334 | 0.0121 | -0.0048 | 1079.83 | 5733.491975 | 0.18833716 |
| 6663 | 0.0342 | -0.0064 | 0.001 | 710.8771 | 3668.930235 | 0.19375596 |
| 6663.5 | 0.0426 | -0.0289 | 0.0003 | 461.5989 | 2397.855467 | 0.19250489 |
| 6664 | 0.0585 | -0.0365 | -0.0001 | 332.7953 | 1235.431183 | 0.26937583 |
| 6664.5 | 0.0739 | -0.0232 | -0.0066 | 284.6163 | 910.6967613 | 0.31252587 |
| 6665 | 0.0787 | -0.0085 | -0.0069 | 311.7871 | 792.3893413 | 0.39347715 |
| 6665.5 | 0.076 | -0.0032 | -0.0035 | 391.6778 | 776.0317071 | 0.50471881 |
| 6666 | 0.0758 | 0.0037 | -0.007 | 389.1804 | 868.5424271 | 0.4480845 |
| 6666.5 | 0.0776 | 0.0114 | -0.0162 | 301.8447 | 1109.287661 | 0.27210679 |
| 6667 | 0.0772 | 0.0208 | -0.0271 | 233.5157 | 1717.730668 | 0.1359443 |
| 6667.5 | 0.0767 | 0.0213 | -0.0274 | 189.7294 | 1778.219235 | 0.10669629 |
| 6668 | 0.0776 | 0.0092 | -0.014 | 157.1065 | 1028.426791 | 0.15276391 |
| 6668.5 | 0.0805 | -0.007 | -0.001 | 131.4596 | 636.5270343 | 0.20652634 |
| 6669 | 0.085 | -0.0114 | 0.0032 | 118.4741 | 509.1534867 | 0.23268838 |
| 6669.5 | 0.0879 | -0.0051 | -0.0016 | 115.699 | 533.5596382 | 0.21684361 |
| 6670 | 0.0882 | 0.0016 | -0.0061 | 122.3641 | 593.9753093 | 0.20600873 |
| 6670.5 | 0.0854 | 0.0028 | -0.0094 | 140.2386 | 701.2242987 | 0.19999107 |
| 6671 | 0.0802 | -0.002 | -0.007 | 165.8908 | 760.1641007 | 0.21823025 |
| 6671.5 | 0.0768 | -0.006 | -0.0023 | 196.729 | 731.931088 | 0.26878077 |
| 6672 | 0.0761 | -0.0107 | 0.0045 | 233.1619 | 617.9962507 | 0.37728692 |
| 6672.5 | 0.0792 | -0.0139 | 0.0114 | 216.6977 | 480.5964463 | 0.45089326 |
| 6673 | 0.0885 | -0.0145 | 0.0168 | 142.5013 | 347.8445331 | 0.40966951 |
| 6673.5 | 0.0955 | -0.0032 | 0.0107 | 100.1733 | 341.5375582 | 0.29330098 |
| 6674 | 0.0923 | 0.0099 | 0.0008 | 87.5048 | 453.2777131 | 0.19304898 |
| 6674.5 | 0.0842 | 0.0162 | -0.0006 | 90.5446 | 571.2979737 | 0.15848927 |
| 6675 | 0.0751 | 0.0099 | 0.0101 | 101.8255 | 548.4803227 | 0.18565023 |
| 6675.5 | 0.0667 | 0.0057 | 0.0142 | 112.6786 | 613.0795906 | 0.18379115 |
| 6676 | 0.065 | 0.0077 | 0.0086 | 119.0036 | 751.3094983 | 0.15839491 |
| 6676.5 | 0.0702 | 0.0064 | 0.007 | 120.9941 | 677.9988925 | 0.17845767 |
| 6677 | 0.075 | -0.001 | 0.0165 | 109.4403 | 470.4904667 | 0.23260896 |
| 6677.5 | 0.0751 | -0.003 | 0.0216 | 86.3579 | 417.7719343 | 0.20671063 |
| 6678 | 0.0715 | -0.0064 | 0.0261 | 65.8025 | 409.5331598 | 0.16067685 |
| 6678.5 | 0.0661 | -0.0125 | 0.0303 | 54.8591 | 420.5721952 | 0.1304392 |
| 6679 | 0.0626 | -0.013 | 0.0354 | 50.5629 | 405.9477302 | 0.1245552 |
| 6679.5 | 0.0618 | -0.0133 | 0.0442 | 49.56 | 342.924544 | 0.14452159 |
| 6680 | 0.0628 | -0.0075 | 0.0501 | 48.8203 | 299.4430275 | 0.16303702 |
| 6680.5 | 0.0672 | 0.0044 | 0.048 | 46.8957 | 286.7367445 | 0.16354967 |
| 6681 | 0.0716 | 0.0107 | 0.044 | 45.1602 | 284.6078253 | 0.15867519 |

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|---|---|---|---|---|---|---|
| 6681.5 | 0.0734 | 0.0048 | 0.0438 | 43.2532 | 276.3196786 | 0.15653319 |
| 6682 | 0.0739 | 0.0002 | 0.0453 | 39.3947 | 266.4478567 | 0.14785144 |
| 6682.5 | 0.0742 | 0.008 | 0.038 | 37.0585 | 303.4740341 | 0.12211424 |
| 6683 | 0.0757 | 0.0156 | 0.0332 | 40.0794 | 323.5908544 | 0.12385826 |
| 6683.5 | 0.0762 | 0.0097 | 0.0345 | 46.8424 | 312.3840098 | 0.14995134 |
| 6684 | 0.0743 | -0.0073 | 0.0433 | 51.6235 | 274.3029248 | 0.18819887 |
| 6684.5 | 0.0737 | -0.0166 | 0.0448 | 56.364 | 269.8433544 | 0.20887674 |
| 6685 | 0.0758 | -0.0134 | 0.0354 | 69.3653 | 309.3719164 | 0.22421331 |
| 6685.5 | 0.0753 | -0.0037 | 0.0208 | 82.2281 | 423.4000419 | 0.194209 |
| 6686 | 0.0703 | -0.0006 | 0.0073 | 86.8209 | 670.5072521 | 0.1294854 |
| 6686.5 | 0.0657 | -0.01 | -0.0034 | 106.5513 | 1075.119849 | 0.09910644 |
| 6687 | 0.0688 | -0.0349 | -0.0111 | 187.9299 | 1267.88009 | 0.14822372 |
| 6687.5 | 0.0893 | -0.051 | -0.0176 | 253.529 | 794.7673098 | 0.31899777 |
| 6688 | 0.1203 | -0.0483 | -0.0189 | 180.7777 | 377.2459421 | 0.47920383 |
| 6688.5 | 0.1394 | -0.0196 | -0.0116 | 89.5309 | 229.3849099 | 0.39030859 |
| 6689 | 0.1436 | 0.0003 | -0.0037 | 66.9055 | 188.8417838 | 0.35429394 |
| 6689.5 | 0.1441 | 0.0028 | 0.001 | 55.6119 | 174.5907552 | 0.31852717 |
| 6690 | 0.1454 | 0.0019 | -0.0019 | 49.0917 | 178.8029142 | 0.27455761 |
| 6690.5 | 0.1444 | 0.0041 | -0.0097 | 49.2627 | 204.8640949 | 0.24046527 |
| 6691 | 0.1359 | 0.0089 | -0.0153 | 58.4642 | 259.8420706 | 0.22499898 |
| 6691.5 | 0.1202 | 0.015 | -0.0238 | 81.7575 | 420.5721952 | 0.19439588 |
| 6692 | 0.1091 | 0.0157 | -0.0264 | 144.0576 | 584.7487938 | 0.2463581 |
| 6692.5 | 0.1112 | 0.0115 | -0.0208 | 210.0561 | 482.8853777 | 0.43500199 |
| 6693 | 0.1282 | 0.0315 | 0.0041 | 175.5737 | 212.9376786 | 0.82453092 |
| 6693.5 | 0.163 | 0.1013 | 0.0661 | 75.4034 | 65.3961586 | 1.15302491 |
| 6694 | 0.2115 | 0.1819 | 0.1883 | 45.4609 | 19.7535057 | 2.30140921 |
| 6694.5 | 0.2529 | 0.203 | 0.3158 | 17.5559 | 9.259920102 | 1.89590189 |
| 6695 | 0.2642 | 0.1548 | 0.333 | 15.0863 | 8.335825453 | 1.80981477 |
| 6695.5 | 0.2405 | 0.0814 | 0.235 | 24.1279 | 13.60606557 | 1.7733194 |
| 6696 | 0.2004 | 0.0271 | 0.1135 | 81.6993 | 33.2280497 | 2.45874497 |
| 6696.5 | 0.1664 | 0.0051 | 0.0383 | 77.3462 | 83.31109036 | 0.92840221 |
| 6697 | 0.1445 | 0.0047 | 0.0061 | 113.9651 | 161.1693635 | 0.70711392 |
| 6697.5 | 0.1336 | 0.0088 | -0.0039 | 117.5163 | 222.2210686 | 0.5288261 |
| 6698 | 0.1305 | -0.0004 | 0.002 | 90.4179 | 212.2472353 | 0.42600272 |
| 6698.5 | 0.1286 | -0.0198 | 0.0149 | 81.5854 | 178.8029142 | 0.45628675 |
| 6699 | 0.1256 | -0.0154 | 0.01 | 79.216 | 201.9518555 | 0.3922519 |
| 6699.5 | 0.1276 | -0.0009 | -0.0027 | 78.1495 | 240.9888436 | 0.3242868 |
| 6700 | 0.1398 | 0.013 | -0.0143 | 74.2368 | 238.518555 | 0.31124119 |
| 6700.5 | 0.1582 | 0.0073 | -0.0171 | 61.3718 | 185.4057081 | 0.33101354 |
| 6701 | 0.1741 | 0.0002 | -0.0122 | 48.4913 | 137.9511913 | 0.35151056 |
| 6701.5 | 0.1847 | -0.0004 | -0.0095 | 41.1055 | 116.4147102 | 0.35309541 |
| 6702 | 0.189 | 0.0056 | -0.0107 | 37.3049 | 112.1064996 | 0.33276304 |
| 6702.5 | 0.1881 | 0.0132 | -0.0151 | 35.6355 | 119.620898 | 0.29790363 |
| 6703 | 0.1861 | 0.0184 | -0.0194 | 35.8708 | 129.5521547 | 0.27688308 |
| 6703.5 | 0.1864 | 0.0211 | -0.013 | 38.6273 | 119.0284094 | 0.32452169 |
| 6704 | 0.1912 | 0.0307 | 0.0459 | 46.0313 | 60.74399332 | 0.7577918 |
| 6704.5 | 0.1956 | 0.0721 | 0.1735 | 67.3285 | 23.45559656 | 2.87046632 |
| 6705 | 0.2023 | 0.1453 | 0.3237 | 67.7064 | 10.95183344 | 6.18219775 |
| 6705.5 | 0.2237 | 0.2112 | 0.4246 | 47.862 | 6.986951582 | 6.85019775 |
| 6706 | 0.2577 | 0.2536 | 0.4472 | 33.3719 | 5.836225079 | 5.71806254 |
| 6706.5 | 0.2934 | 0.2914 | 0.4131 | 16.3382 | 5.807845074 | 2.813126 |
| 6707 | 0.3252 | 0.3405 | 0.3386 | 13.6183 | 6.640887098 | 2.05067483 |

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|---|---|---|---|---|---|---|
| 6707.5 | 0.3482 | 0.3889 | 0.2482 | 14.7591 | 8.359884271 | 1.76546702 |
| 6708 | 0.367 | 0.4226 | 0.18 | 15.3677 | 10.06777332 | 1.52642491 |
| 6708.5 | 0.3832 | 0.4368 | 0.1482 | 14.2773 | 10.71395573 | 1.33258904 |
| 6709 | 0.3837 | 0.4096 | 0.1658 | 12.1617 | 9.969551752 | 1.21988433 |
| 6709.5 | 0.3685 | 0.3491 | 0.2036 | 11.3199 | 9.1420058 | 1.23822936 |
| 6710 | 0.3424 | 0.3018 | 0.2202 | 13.8261 | 9.477128415 | 1.45889128 |
| 6710.5 | 0.2979 | 0.2801 | 0.1883 | 24.1704 | 12.97041966 | 1.86350177 |
| 6711 | 0.2411 | 0.2335 | 0.1252 | 46.6411 | 23.84277525 | 1.95619426 |
| 6711.5 | 0.195 | 0.1416 | 0.0653 | 74.1761 | 49.69774905 | 1.49254446 |
| 6712 | 0.1721 | 0.056 | 0.029 | 153.7527 | 86.55062899 | 1.7764481 |
| 6712.5 | 0.1643 | 0.0277 | 0.0174 | 186.4613 | 107.6448078 | 1.73219038 |
| 6713 | 0.1643 | 0.0374 | 0.017 | 120.5543 | 108.1560708 | 1.11463276 |
| 6713.5 | 0.1698 | 0.0358 | 0.0192 | 72.8821 | 98.9038736 | 0.73689834 |
| 6714 | 0.1636 | 0.0248 | 0.0192 | 58.3166 | 106.2569556 | 0.54882619 |
| 6714.5 | 0.141 | 0.0174 | 0.0132 | 62.688 | 153.1880108 | 0.40922263 |
| 6715 | 0.1279 | 0.0169 | 0.0053 | 71.9537 | 209.8563412 | 0.34287122 |
| 6715.5 | 0.1304 | 0.0102 | 0.0055 | 78.7688 | 200.9945808 | 0.39189514 |
| 6716 | 0.1326 | -0.0057 | 0.0113 | 85.3189 | 177.7360291 | 0.48003154 |
| 6716.5 | 0.1315 | -0.0187 | 0.0167 | 78.1854 | 166.8332239 | 0.46864406 |
| 6717 | 0.131 | -0.0255 | 0.0184 | 66.3069 | 163.965469 | 0.40439551 |
| 6717.5 | 0.1284 | -0.0224 | 0.0139 | 61.7099 | 182.0604639 | 0.33895278 |
| 6718 | 0.1212 | -0.0134 | 0.0048 | 64.4128 | 236.4882177 | 0.27237213 |
| 6718.5 | 0.1142 | -0.0055 | 0.0012 | 74.2212 | 285.6693793 | 0.25981504 |
| 6719 | 0.1106 | 0.0084 | -0.0017 | 87.508 | 323.5908544 | 0.27042791 |
| 6719.5 | 0.1082 | 0.0235 | -0.0023 | 77.0594 | 343.6211334 | 0.22425687 |
| 6720 | 0.1052 | 0.035 | 0.0024 | 57.0808 | 332.0548262 | 0.17190173 |
| 6720.5 | 0.101 | 0.0362 | 0.0049 | 54.5768 | 343.6211334 | 0.15882842 |
| 6721 | 0.0929 | 0.0303 | 0.0095 | 67.5637 | 369.3697057 | 0.18291619 |
| 6721.5 | 0.0819 | 0.019 | 0.0138 | 84.4333 | 427.2140371 | 0.197637 |
| 6722 | 0.075 | 0.0071 | 0.0172 | 81.359 | 462.8440658 | 0.17578058 |
| 6722.5 | 0.0762 | -0.001 | 0.0233 | 72.5995 | 392.9040962 | 0.18477664 |
| 6723 | 0.0799 | -0.0089 | 0.0383 | 72.3619 | 271.3179991 | 0.26670512 |
| 6723.5 | 0.079 | -0.0187 | 0.0555 | 67.5172 | 205.5196108 | 0.3285195 |
| 6724 | 0.0779 | -0.0214 | 0.0625 | 51.0344 | 187.3988401 | 0.27233039 |
| 6724.5 | 0.0817 | -0.0248 | 0.064 | 39.1691 | 173.0486214 | 0.22634737 |
| 6725 | 0.0849 | -0.0303 | 0.0681 | 34.7397 | 155.7828353 | 0.22300082 |
| 6725.5 | 0.0772 | -0.035 | 0.0711 | 35.6864 | 166.5914489 | 0.21421508 |
| 6726 | 0.0613 | -0.0302 | 0.0639 | 41.6557 | 239.7490379 | 0.1737471 |
| 6726.5 | 0.0545 | -0.0143 | 0.0479 | 52.4773 | 369.3697057 | 0.14207256 |
| 6727 | 0.0582 | -0.0022 | 0.036 | 55.4842 | 441.9740176 | 0.12553724 |
| 6727.5 | 0.0598 | 0.0024 | 0.0297 | 40.4088 | 493.3858093 | 0.08190102 |
| 6728 | 0.0678 | 0.0043 | 0.0232 | 32.3149 | 476.0660228 | 0.06787903 |
| 6728.5 | 0.0891 | 0.0078 | 0.0157 | 34.7524 | 351.4223855 | 0.09889068 |
| 6729 | 0.0982 | 0.0025 | 0.0158 | 43.408 | 293.2653478 | 0.14801612 |
| 6729.5 | 0.088 | -0.0158 | 0.0248 | 54.75 | 300.0140654 | 0.18249144 |
| 6730 | 0.0807 | -0.0333 | 0.0408 | 74.8411 | 255.7214643 | 0.29266648 |
| 6730.5 | 0.0792 | -0.0308 | 0.0419 | 109.3545 | 257.5409376 | 0.42461016 |
| 6731 | 0.0766 | -0.0044 | 0.0242 | 129.0315 | 382.0903208 | 0.33769895 |
| 6731.5 | 0.0729 | 0.0193 | 0.0042 | 103.9114 | 679.890961 | 0.15283539 |
| 6732 | 0.0746 | 0.0235 | -0.0042 | 72.5216 | 826.6562679 | 0.08772885 |
| 6732.5 | 0.0865 | 0.0096 | 0.0083 | 56.0077 | 435.9816944 | 0.12846342 |
| 6733 | 0.1041 | 0.0065 | 0.0166 | 47.2959 | 259.3794407 | 0.18234252 |

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|---|---|---|---|---|---|---|
| 6733.5 | 0.1249 | 0.0104 | 0.016 | 40.5572 | 185.9719929 | 0.2180823 |
| 6734 | 0.1455 | 0.0164 | 0.0033 | 38.1154 | 165.3902403 | 0.23045737 |
| 6734.5 | 0.1594 | 0.0141 | -0.0041 | 39.1453 | 150.8646711 | 0.25947294 |
| 6735 | 0.1692 | 0.0086 | -0.0032 | 40.2817 | 130.7295574 | 0.30813001 |
| 6735.5 | 0.178 | -0.0013 | -0.0001 | 40.6133 | 112.6491429 | 0.36052915 |
| 6736 | 0.1842 | -0.0094 | 0.005 | 39.3326 | 98.67922869 | 0.39859047 |
| 6736.5 | 0.1859 | -0.0136 | 0.0101 | 37.3088 | 91.46514491 | 0.40790183 |
| 6737 | 0.1853 | -0.0073 | 0.0082 | 37.0053 | 94.02473023 | 0.39356986 |
| 6737.5 | 0.1899 | 0.0045 | -0.0024 | 38.5929 | 100.6128486 | 0.38357825 |
| 6738 | 0.1963 | 0.0186 | -0.0146 | 39.8749 | 107.6448078 | 0.37043031 |
| 6738.5 | 0.1961 | 0.0248 | -0.0192 | 39.9562 | 114.0227049 | 0.35042319 |
| 6739 | 0.1928 | 0.0258 | -0.0171 | 40.9332 | 115.7036056 | 0.35377636 |
| 6739.5 | 0.185 | 0.0242 | -0.0154 | 44.9791 | 124.8362192 | 0.36030489 |
| 6740 | 0.1604 | 0.025 | -0.0178 | 51.1489 | 181.2379747 | 0.28221955 |
| 6740.5 | 0.127 | 0.0247 | -0.0161 | 55.7937 | 311.1740383 | 0.17930063 |
| 6741 | 0.1071 | 0.0239 | -0.0098 | 60.797 | 412.2527616 | 0.14747506 |
| 6741.5 | 0.1019 | 0.0229 | -0.0068 | 77.2483 | 433.0300835 | 0.17839015 |
| 6742 | 0.1019 | 0.0212 | -0.011 | 117.8976 | 477.1927439 | 0.24706495 |
| 6742.5 | 0.0992 | 0.0191 | -0.0161 | 156.6915 | 578.7139871 | 0.2707581 |
| 6743 | 0.0886 | 0.0112 | -0.0121 | 200.8854 | 691.4075133 | 0.29054558 |
| 6743.5 | 0.0804 | -0.0017 | -0.0028 | 217.4302 | 670.5072521 | 0.32427718 |
| 6744 | 0.0837 | -0.0112 | 0.0019 | 250.7993 | 542.9846922 | 0.46189019 |
| 6744.5 | 0.0898 | -0.0084 | 0.0084 | 229.9716 | 404.1722401 | 0.56899405 |
| 6745 | 0.098 | 0.0145 | 0.0096 | 128.5194 | 332.0548262 | 0.38704271 |
| 6745.5 | 0.1171 | 0.0321 | 0.0137 | 67.1172 | 218.2225019 | 0.30756315 |
| 6746 | 0.1396 | 0.0346 | 0.0123 | 47.3216 | 158.218392 | 0.29909039 |
| 6746.5 | 0.1498 | 0.0276 | 0.0131 | 44.5056 | 136.1368975 | 0.32691798 |
| 6747 | 0.1456 | 0.02 | 0.0151 | 49.7395 | 140.1754778 | 0.35483739 |
| 6747.5 | 0.1383 | 0.0197 | 0.0074 | 66.796 | 173.0486214 | 0.38599556 |
| 6748 | 0.138 | 0.0237 | -0.0026 | 115.9195 | 202.593754 | 0.57217707 |
| 6748.5 | 0.1424 | 0.0475 | 0.0036 | 165.8979 | 172.285029 | 0.96292696 |
| 6749 | 0.1511 | 0.1196 | 0.0469 | 189.6729 | 89.49031177 | 2.11947971 |
| 6749.5 | 0.1724 | 0.232 | 0.1211 | 96.4995 | 38.39270865 | 2.51348507 |
| 6750 | 0.205 | 0.3129 | 0.2174 | 48.0499 | 17.55091548 | 2.73774323 |
| 6750.5 | 0.2447 | 0.3047 | 0.3243 | 21.6665 | 9.249426538 | 2.34246955 |
| 6751 | 0.2829 | 0.2527 | 0.3684 | 14.0308 | 6.917941132 | 2.02817569 |
| 6751.5 | 0.2941 | 0.1934 | 0.2988 | 16.5991 | 8.466346952 | 1.96059766 |
| 6752 | 0.2674 | 0.1267 | 0.1615 | 33.8811 | 16.98402736 | 1.99488021 |
| 6752.5 | 0.2252 | 0.0556 | 0.0585 | 45.2518 | 41.30081371 | 1.09566364 |
| 6753 | 0.1943 | 0.0182 | 0.0059 | 68.1198 | 87.38933266 | 0.77949789 |
| 6753.5 | 0.1782 | 0.0031 | -0.0059 | 80.6232 | 120.6681998 | 0.66813958 |
| 6754 | 0.1678 | 0.0002 | -0.0087 | 76.7415 | 143.2238336 | 0.53581515 |
| 6754.5 | 0.1583 | -0.0027 | -0.0055 | 71.1485 | 156.2215594 | 0.4554333 |
| 6755 | 0.1477 | -0.0087 | -0.0014 | 83.9988 | 171.526363 | 0.48971364 |
| 6755.5 | 0.1345 | -0.0171 | 0.0062 | 132.6214 | 186.5408154 | 0.71095111 |
| 6756 | 0.1179 | -0.0214 | 0.0143 | 238.5528 | 213.2841348 | 1.11847419 |
| 6756.5 | 0.1011 | -0.0168 | 0.0158 | 571.9095 | 277.8465325 | 2.05836472 |
| 6757 | 0.0877 | -0.0072 | 0.007 | 1930.905 | 436.9721166 | 4.41882817 |
| 6757.5 | 0.0795 | 0.0001 | -0.0026 | 9494.063 | 683.698378 | 13.8863318 |
| 6758 | 0.0765 | 0.0028 | -0.0039 | 20000 | 773.7353617 | 25.8486312 |
| 6758.5 | 0.0814 | 0.013 | -0.0131 | 20000 | 882.2703153 | 22.6687894 |
| 6759 | 0.096 | 0.0181 | -0.019 | 16820.5 | 681.7907756 | 24.6710554 |

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|---|---|---|---|---|---|---|
| 6759.5 | 0.1156 | 0.0154 | -0.007 | 1834.706 | 325.5157869 | 5.63630482 |
| 6760 | 0.1367 | 0.0378 | 0.032 | 301.9165 | 126.2724924 | 2.39099185 |
| 6760.5 | 0.1619 | 0.1409 | 0.0671 | 74.1839 | 65.45757216 | 1.13331273 |
| 6761 | 0.2044 | 0.2634 | 0.1127 | 26.4214 | 32.51129433 | 0.81268373 |
| 6761.5 | 0.2746 | 0.2993 | 0.2233 | 13.7741 | 12.32396933 | 1.1176675 |
| 6762 | 0.354 | 0.257 | 0.3406 | 6.9362 | 6.023881298 | 1.15145031 |
| 6762.5 | 0.4226 | 0.2271 | 0.3287 | 5.8458 | 5.088706398 | 1.14877919 |
| 6763 | 0.4854 | 0.2123 | 0.2253 | 6.5958 | 5.734302534 | 1.15023579 |
| 6763.5 | 0.5236 | 0.1609 | 0.1694 | 9.5266 | 6.053823094 | 1.57365021 |
| 6764 | 0.5117 | 0.1128 | 0.1903 | 11.3192 | 5.888184221 | 1.92235833 |
| 6764.5 | 0.4901 | 0.1063 | 0.2385 | 9.1991 | 5.435687379 | 1.69235266 |
| 6765 | 0.4848 | 0.1284 | 0.2978 | 7.4445 | 4.66117616 | 1.59712908 |
| 6765.5 | 0.4619 | 0.1434 | 0.3718 | 7.3352 | 4.068507369 | 1.80292165 |
| 6766 | 0.4149 | 0.1361 | 0.3926 | 9.4613 | 4.357623843 | 2.17120622 |
| 6766.5 | 0.3577 | 0.107 | 0.3 | 19.7067 | 6.774017592 | 2.90915985 |
| 6767 | 0.2966 | 0.0603 | 0.1505 | 37.2645 | 15.53231323 | 2.3991597 |
| 6767.5 | 0.2429 | 0.0215 | 0.0415 | 106.8791 | 41.08256559 | 2.60156829 |
| 6768 | 0.2068 | -0.0007 | 0.0088 | 310.4878 | 74.51802803 | 4.16661321 |
| 6768.5 | 0.1867 | -0.009 | 0.0093 | 338.0225 | 91.46514491 | 3.69564275 |
| 6769 | 0.1727 | -0.004 | 0.0065 | 239.0765 | 110.8994695 | 2.1557948 |
| 6769.5 | 0.1527 | 0.0001 | 0.0063 | 224.4173 | 143.417571 | 1.56478246 |
| 6770 | 0.1253 | -0.0045 | 0.0079 | 291.3649 | 209.8563412 | 1.3884017 |
| 6770.5 | 0.1026 | -0.0067 | 0.0072 | 400.0544 | 317.9150948 | 1.25836869 |
| 6771 | 0.0894 | -0.0019 | 0.0067 | 326.6252 | 423.4000419 | 0.77143403 |
| 6771.5 | 0.0821 | -0.0033 | 0.0104 | 201.2648 | 459.6226843 | 0.43789135 |
| 6772 | 0.078 | -0.0167 | 0.0227 | 116.5443 | 382.9065703 | 0.30436746 |
| 6772.5 | 0.0742 | -0.0195 | 0.0225 | 84.5458 | 417.7719343 | 0.2023731 |
| 6773 | 0.0703 | -0.009 | 0.0186 | 62.493 | 500.5729692 | 0.12484294 |
| 6773.5 | 0.0671 | -0.0051 | 0.016 | 50.522 | 578.7139871 | 0.08730046 |
| 6774 | 0.0633 | -0.0009 | 0.0103 | 46.0591 | 751.3094983 | 0.06130509 |
| 6774.5 | 0.0588 | 0.0046 | 0.0043 | 44.8305 | 1046.027393 | 0.04285786 |
| 6775 | 0.0582 | 0.0067 | 0.0065 | 44.1671 | 991.2015597 | 0.04455915 |
| 6775.5 | 0.0657 | 0.0035 | 0.0126 | 44.5811 | 657.6856888 | 0.06778481 |
| 6776 | 0.076 | -0.0041 | 0.0192 | 47.7012 | 432.0527176 | 0.11040597 |
| 6776.5 | 0.0813 | -0.0098 | 0.0233 | 50.4668 | 352.8686358 | 0.14301866 |
| 6777 | 0.0835 | -0.0146 | 0.0249 | 50.5943 | 326.8084096 | 0.15481334 |
| 6777.5 | 0.0871 | -0.0165 | 0.0263 | 50.9904 | 296.6115872 | 0.17190967 |
| 6778 | 0.0901 | -0.0198 | 0.0368 | 55.298 | 232.8968919 | 0.23743554 |
| 6778.5 | 0.0911 | -0.0183 | 0.0425 | 62.8737 | 208.5077948 | 0.30154124 |
| 6779 | 0.0916 | -0.0125 | 0.0393 | 64.2663 | 217.8642343 | 0.29498325 |
| 6779.5 | 0.0947 | -0.0084 | 0.0362 | 57.4742 | 217.8642343 | 0.26380741 |
| 6780 | 0.1029 | -0.0067 | 0.0377 | 50.8219 | 186.8261829 | 0.27202772 |
| 6780.5 | 0.1074 | -0.0099 | 0.0437 | 44.6232 | 160.0249064 | 0.27885159 |
| 6781 | 0.1039 | -0.0095 | 0.0475 | 37.2284 | 159.3439389 | 0.23363549 |
| 6781.5 | 0.101 | -0.0037 | 0.0487 | 31.7023 | 163.2598185 | 0.19418311 |
| 6782 | 0.1002 | -0.003 | 0.055 | 30.1653 | 151.0737428 | 0.19967269 |
| 6782.5 | 0.0932 | -0.0024 | 0.0661 | 31.7914 | 142.8375072 | 0.22257039 |
| 6783 | 0.0825 | 0.0067 | 0.0714 | 35.0874 | 153.8307465 | 0.22809094 |
| 6783.5 | 0.0785 | 0.0157 | 0.0711 | 41.7598 | 163.4945401 | 0.25542015 |
| 6784 | 0.0798 | 0.0232 | 0.0704 | 54.8517 | 162.093584 | 0.33839526 |
| 6784.5 | 0.0809 | 0.0371 | 0.0688 | 67.1715 | 163.2598185 | 0.41143927 |
| 6785 | 0.0812 | 0.0519 | 0.0715 | 63.7847 | 156.4416005 | 0.40772211 |

0.043 to 1.26

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|---|---|---|---|---|---|---|
| 6785.5 | 0.0814 | 0.0594 | 0.084 | 52.2793 | 131.7512802 | 0.39680298 |
| 6786 | 0.0794 | 0.0601 | 0.1021 | 47.6943 | 107.8999956 | 0.44202319 |
| 6786.5 | 0.0744 | 0.0604 | 0.1117 | 56.2959 | 102.2472127 | 0.55058616 |
| 6787 | 0.0722 | 0.0648 | 0.1054 | 75.4463 | 113.0586546 | 0.66731999 |
| 6787.5 | 0.0723 | 0.0684 | 0.0902 | 89.6897 | 136.8583957 | 0.65534671 |
| 6788 | 0.0717 | 0.0645 | 0.0839 | 85.2905 | 150.2399934 | 0.56769505 |
| 6788.5 | 0.0704 | 0.0581 | 0.0862 | 72.7293 | 148.1848828 | 0.49080108 |
| 6789 | 0.0689 | 0.0553 | 0.0901 | 64.5162 | 143.417571 | 0.44984864 |
| 6789.5 | 0.0683 | 0.0551 | 0.0886 | 59.1811 | 147.5763795 | 0.40102014 |
| 6790 | 0.0679 | 0.0573 | 0.0816 | 63.2665 | 163.7297565 | 0.38640807 |
| 6790.5 | 0.0679 | 0.0601 | 0.0755 | 92.9528 | 179.0711014 | 0.5190832 |
| 6791 | 0.0712 | 0.0581 | 0.0812 | 85.6523 | 157.1044552 | 0.54519332 |
| 6791.5 | 0.0738 | 0.0492 | 0.091 | 72.3268 | 132.7847451 | 0.54469209 |
| 6792 | 0.072 | 0.0348 | 0.0955 | 48.8762 | 128.2254807 | 0.38117385 |
| 6792.5 | 0.0694 | 0.0223 | 0.092 | 36.1237 | 138.8716482 | 0.26012293 |
| 6793 | 0.0697 | 0.0206 | 0.0958 | 35.4047 | 131.5801824 | 0.26907319 |
| 6793.5 | 0.074 | 0.0268 | 0.1064 | 40.6778 | 109.3194993 | 0.37210013 |
| 6794 | 0.0799 | 0.041 | 0.1077 | 56.0718 | 100.4975761 | 0.55794182 |
| 6794.5 | 0.0895 | 0.0466 | 0.1042 | 71.6508 | 93.81612604 | 0.7637365 |
| 6795 | 0.102 | 0.0492 | 0.1023 | 81.3686 | 83.6621829 | 0.97258519 |
| 6795.5 | 0.107 | 0.0542 | 0.1009 | 81.0442 | 80.57847208 | 1.00577981 |
| 6796 | 0.1049 | 0.0503 | 0.103 | 72.541 | 80.57847208 | 0.90025286 |
| 6796.5 | 0.1044 | 0.0385 | 0.1102 | 61.6929 | 75.26659811 | 0.81965841 |
| 6797 | 0.1051 | 0.0314 | 0.1153 | 57.6448 | 71.07244585 | 0.811071 |
| 6797.5 | 0.1005 | 0.0379 | 0.1125 | 60.0061 | 76.48742367 | 0.78452244 |
| 6798 | 0.0897 | 0.0419 | 0.1091 | 71.1686 | 88.71784071 | 0.8021904 |
| 6798.5 | 0.0809 | 0.0438 | 0.1062 | 105.0379 | 101.0758814 | 1.03919846 |
| 6799 | 0.0785 | 0.0517 | 0.0954 | 125.1091 | 118.2938261 | 1.0576131 |
| 6799.5 | 0.0759 | 0.0554 | 0.0813 | 97.439 | 146.9715301 | 0.66297874 |
| 6800 | 0.0753 | 0.0498 | 0.0677 | 64.5434 | 180.1497649 | 0.35827635 |
| 6800.5 | 0.0991 | 0.0353 | 0.0586 | 30.7839 | 145.9714895 | 0.21088981 |
| 6801 | 0.1461 | 0.0151 | 0.0568 | 19.4787 | 84.90822832 | 0.22940886 |
| 6801.5 | 0.174 | 0.0024 | 0.0515 | 18.0893 | 67.66141966 | 0.26735029 |
| 6802 | 0.1688 | 0.002 | 0.0355 | 21.7977 | 83.6621829 | 0.26054424 |
| 6802.5 | 0.1601 | 0.0158 | 0.0231 | 38.5997 | 105.7587773 | 0.36497869 |
| 6803 | 0.1673 | 0.0688 | 0.0194 | 59.7285 | 101.5420429 | 0.58821448 |
| 6803.5 | 0.1846 | 0.2211 | -0.016 | 52.8797 | 126.4335709 | 0.41824098 |
| 6804 | 0.2067 | 0.4201 | -0.0737 | 25.0405 | 210.5354108 | 0.11893724 |
| 6804.5 | 0.2383 | 0.4845 | -0.0189 | 12.5748 | 71.77074266 | 0.17520788 |
| 6805 | 0.2705 | 0.3787 | 0.1023 | 6.3776 | 22.95794374 | 0.27779491 |
| 6805.5 | 0.2675 | 0.2212 | 0.187 | 7.6047 | 14.99368291 | 0.5071936 |
| 6806 | 0.2584 | 0.1235 | 0.2671 | 18.0037 | 10.97424954 | 1.64054042 |
| 6806.5 | 0.3356 | 0.1003 | 0.415 | 32.0545 | 5.098915044 | 6.28653345 |
| 6807 | 0.4529 | 0.1266 | 0.5403 | 28.5985 | 2.792397572 | 10.2415574 |
| 6807.5 | 0.5101 | 0.1812 | 0.5307 | 19.8655 | 2.525029873 | 7.86743167 |
| 6808 | 0.5272 | 0.2153 | 0.4697 | 7.0354 | 2.770162518 | 2.53970659 |
| 6808.5 | 0.508 | 0.2217 | 0.4348 | 5.2426 | 3.123230926 | 1.67858225 |
| 6809 | 0.4284 | 0.2081 | 0.4124 | 6.7037 | 3.995000782 | 1.6780222 |
| 6809.5 | 0.3371 | 0.1741 | 0.3386 | 14.1545 | 6.391977749 | 2.21441634 |
| 6810 | 0.2646 | 0.1242 | 0.1835 | 26.1586 | 15.45788424 | 1.6922497 |
| 6810.5 | 0.1991 | 0.0637 | 0.0518 | 75.0705 | 53.78730175 | 1.39569187 |
| 6811 | 0.161 | 0.0257 | -0.0055 | 258.6426 | 150.4477976 | 1.71915179 |

| | | | | | | |
|---|---|---|---|---|---|---|
| 6811.5 | 0.165 | 0.0068 | -0.0036 | 357.2288 | 138.8716482 | 2.57236668 |
| 6812 | 0.1819 | -0.0036 | 0.0007 | 203.785 | 106.5073349 | 1.9133424 |
| 6812.5 | 0.1872 | -0.0119 | -0.0009 | 142.2514 | 102.0113611 | 1.39446625 |
| 6813 | 0.1847 | -0.0196 | -0.0007 | 141.4771 | 104.7726336 | 1.35032494 |
| 6813.5 | 0.18 | -0.0123 | 0.0521 | 197.7476 | 63.59231397 | 3.10961479 |
| 6814 | 0.1816 | 0.0087 | 0.2135 | 295.6075 | 20.26217521 | 14.5891296 |
| 6814.5 | 0.2305 | 0.0481 | 0.4347 | 158.9013 | 6.610873744 | 24.0363538 |
| 6815 | 0.3919 | 0.0974 | 0.5792 | 48.6653 | 2.930816844 | 16.6046882 |
| 6815.5 | 0.5836 | 0.1389 | 0.6034 | 126.9363 | 1.903430984 | 66.6881547 |
| 6816 | 0.6218 | 0.1682 | 0.5661 | 9.4102 | 1.900331788 | 4.95187212 |
| 6816.5 | 0.5503 | 0.1963 | 0.4954 | 5.8809 | 2.499659754 | 2.3526802 |
| 6817 | 0.5097 | 0.2173 | 0.3842 | 6.3564 | 3.502151788 | 1.81499843 |
| 6817.5 | 0.4938 | 0.2091 | 0.2589 | 9.0463 | 5.068378742 | 1.78485083 |
| 6818 | 0.468 | 0.1713 | 0.1796 | 13.9305 | 7.003199109 | 1.98916235 |
| 6818.5 | 0.4411 | 0.1768 | 0.1341 | 17.5806 | 9.036403057 | 1.94553075 |
| 6819 | 0.4342 | 0.2633 | 0.0877 | 19.8866 | 11.1376481 | 1.78552957 |
| 6819.5 | 0.4431 | 0.3604 | 0.0563 | 26.5593 | 12.24452165 | 2.16907616 |
| 6820 | 0.4451 | 0.3645 | 0.0978 | 37.8987 | 10.23195262 | 3.70395577 |
| 6820.5 | 0.436 | 0.3023 | 0.1661 | 24.9059 | 8.190654969 | 3.04077026 |
| 6821 | 0.4159 | 0.2403 | 0.2022 | 15.9227 | 7.741584909 | 2.05677522 |
| 6821.5 | 0.4002 | 0.222 | 0.1901 | 14.109 | 8.54672433 | 1.65080789 |
| 6822 | 0.4021 | 0.2354 | 0.1682 | 16.8162 | 9.204155161 | 1.82702266 |
| 6822.5 | 0.3984 | 0.2508 | 0.1529 | 22.2278 | 9.899699143 | 2.24530056 |
| 6823 | 0.3751 | 0.2581 | 0.14 | 25.0397 | 11.45616732 | 2.18569608 |
| 6823.5 | 0.3577 | 0.2546 | 0.1621 | 19.7135 | 11.23461486 | 1.7547108 |
| 6824 | 0.3446 | 0.2515 | 0.2 | 13.6882 | 10.16340567 | 1.34681232 |
| 6824.5 | 0.3001 | 0.2374 | 0.2402 | 11.7253 | 10.33810646 | 1.13418256 |
| 6825 | 0.2355 | 0.2268 | 0.2223 | 14.0511 | 14.76227309 | 0.95182496 |
| 6825.5 | 0.1977 | 0.201 | 0.1623 | 26.4069 | 24.74889445 | 1.06699312 |
| 6826 | 0.1905 | 0.178 | 0.0793 | 39.7763 | 46.01145825 | 0.86448684 |
| 6826.5 | 0.1872 | 0.1953 | 0.0196 | 55.3155 | 81.5028004 | 0.67869447 |
| 6827 | 0.1841 | 0.2667 | 0.0057 | 47.1433 | 98.00976159 | 0.48100617 |
| 6827.5 | 0.1957 | 0.3381 | 0.0431 | 32.7278 | 59.81806866 | 0.54712231 |
| 6828 | 0.2071 | 0.3626 | 0.112 | 21.7974 | 32.07477002 | 0.67958087 |
| 6828.5 | 0.1875 | 0.3015 | 0.194 | 17.9844 | 21.84705562 | 0.8231956 |
| 6829 | 0.161 | 0.2012 | 0.2031 | 20.4465 | 24.15359169 | 0.84652006 |
| 6829.5 | 0.1523 | 0.1032 | 0.1432 | 34.2683 | 37.83620649 | 0.90570126 |
| 6830 | 0.1427 | 0.0435 | 0.0611 | 56.4703 | 84.10410505 | 0.67143334 |
| 6830.5 | 0.1266 | 0.0178 | 0.0161 | 48.5279 | 180.9650212 | 0.26816177 |
| 6831 | 0.1168 | 0.0031 | 0.0122 | 42.2839 | 224.8217391 | 0.18807745 |
| 6831.5 | 0.1207 | -0.0072 | 0.0216 | 42.6339 | 182.0604639 | 0.2341744 |
| 6832 | 0.1287 | -0.0199 | 0.0328 | 46.5418 | 138.6868384 | 0.33558916 |
| 6832.5 | 0.1316 | -0.0224 | 0.0324 | 61.4045 | 134.1812727 | 0.45762347 |
| 6833 | 0.135 | -0.0145 | 0.0317 | 98.2128 | 129.5521547 | 0.75809469 |
| 6833.5 | 0.1339 | 0.0007 | 0.0401 | 204.2581 | 118.1477067 | 1.72883677 |
| 6834 | 0.123 | 0.0251 | 0.0639 | 576.0865 | 101.3085693 | 5.68645381 |
| 6834.5 | 0.1195 | 0.0791 | 0.1021 | 1044.038 | 70.24755365 | 14.8622656 |
| 6835 | 0.1406 | 0.1849 | 0.1458 | 327.9039 | 40.46822918 | 8.10274891 |
| 6835.5 | 0.1914 | 0.3095 | 0.1749 | 91.8768 | 23.84277525 | 3.85344403 |
| 6836 | 0.2635 | 0.376 | 0.193 | 37.9039 | 14.85280568 | 2.55196902 |
| 6836.5 | 0.3296 | 0.3529 | 0.2346 | 21.0745 | 9.419439353 | 2.23734123 |
| 6837 | 0.3907 | 0.2801 | 0.3096 | 10.4677 | 5.918958685 | 1.76850364 |

| | | | | | | |
|---|---|---|---|---|---|---|
| 6837.5 | 0.4674 | 0.2308 | 0.3743 | 6.3295 | 3.985822246 | 1.58800358 |
| 6838 | 0.5157 | 0.2417 | 0.3491 | 5.4259 | 3.760429631 | 1.44289364 |
| 6838.5 | 0.4888 | 0.2601 | 0.2819 | 6.0598 | 4.817288523 | 1.25792756 |
| 6839 | 0.4489 | 0.2401 | 0.2304 | 7.8035 | 6.319368904 | 1.23485432 |
| 6839.5 | 0.4409 | 0.1899 | 0.2177 | 12.4528 | 6.754130824 | 1.84373094 |
| 6840 | 0.4382 | 0.1423 | 0.2269 | 20.6486 | 6.613010958 | 3.12242035 |
| 6840.5 | 0.4523 | 0.108 | 0.2426 | 19.9842 | 6.018291373 | 3.32057701 |
| 6841 | 0.4761 | 0.0904 | 0.2458 | 16.538 | 5.544731752 | 2.98265105 |
| 6841.5 | 0.479 | 0.105 | 0.2227 | 15.6689 | 5.893597948 | 2.65863063 |
| 6842 | 0.4658 | 0.1418 | 0.203 | 15.9025 | 6.534603058 | 2.43358317 |
| 6842.5 | 0.4626 | 0.1688 | 0.2024 | 16.7018 | 6.615149184 | 2.52478055 |
| 6843 | 0.4865 | 0.1634 | 0.2335 | 15.7264 | 5.576238144 | 2.82025258 |
| 6843.5 | 0.5035 | 0.1471 | 0.3176 | 12.5055 | 4.20392218 | 2.97472205 |
| 6844 | 0.502 | 0.1588 | 0.4135 | 9.4178 | 3.326907535 | 2.83079704 |
| 6844.5 | 0.5099 | 0.1954 | 0.4282 | 8.4755 | 3.156970603 | 2.68469399 |
| 6845 | 0.4821 | 0.2124 | 0.3443 | 12.9221 | 4.146169159 | 3.11663598 |
| 6845.5 | 0.3939 | 0.1698 | 0.2686 | 25.538 | 6.668935738 | 3.82939662 |
| 6846 | 0.3056 | 0.1048 | 0.2631 | 62.4101 | 9.259920102 | 6.73980977 |
| 6846.5 | 0.2437 | 0.0963 | 0.2665 | 219.4845 | 11.69403 | 18.768936 |
| 6847 | 0.206 | 0.1582 | 0.2206 | 1129.945 | 17.18151083 | 65.7651478 |
| 6847.5 | 0.186 | 0.2054 | 0.1379 | 4571.424 | 31.06151555 | 147.173237 |
| 6848 | 0.1707 | 0.1773 | 0.0717 | 1142.843 | 57.92433504 | 19.7299201 |
| 6848.5 | 0.1573 | 0.1548 | 0.0634 | 214.5644 | 70.8648976 | 3.02779525 |
| 6849 | 0.153 | 0.2796 | 0.0302 | 58.7464 | 105.7587773 | 0.55547541 |
| 6849.5 | 0.1698 | 0.4728 | -0.018 | 92.4055 | 158.4425675 | 0.58321133 |
| 6850 | 0.2079 | 0.5285 | 0.0154 | 11.5012 | 69.10276508 | 0.16643618 |
| 6850.5 | 0.249 | 0.3811 | 0.1255 | 6.6738 | 22.73446627 | 0.29355429 |
| 6851 | 0.2451 | 0.1833 | 0.165 | 6.8828 | 18.70222064 | 0.36802047 |
| 6851.5 | 0.178 | 0.0678 | 0.094 | 13.258 | 45.21505219 | 0.29322094 |
| 6852 | 0.1056 | 0.0264 | 0.019 | 24.1319 | 242.2380653 | 0.09962059 |
| 6852.5 | 0.068 | -0.0019 | 0.0147 | 50.8833 | 584.7487938 | 0.08701737 |
| 6853 | 0.0552 | -0.0228 | 0.0324 | 76.9652 | 516.680834 | 0.14896082 |
| 6853.5 | 0.0538 | -0.022 | 0.0391 | 69.2387 | 455.3783667 | 0.15204653 |
| 6854 | 0.0564 | -0.0062 | 0.0374 | 51.3828 | 446.0361697 | 0.11519873 |
| 6854.5 | 0.0576 | -0.0003 | 0.0402 | 53.3675 | 407.7346709 | 0.13088781 |
| 6855 | 0.0568 | -0.0042 | 0.0468 | 56.214 | 360.2323457 | 0.15604929 |
| 6855.5 | 0.0566 | -0.0061 | 0.0509 | 54.0458 | 332.7192911 | 0.16243663 |
| 6856 | 0.0603 | -0.0038 | 0.0467 | 49.176 | 336.0710154 | 0.14632622 |
| 6856.5 | 0.0653 | 0.0017 | 0.0363 | 44.0804 | 375.6511374 | 0.11734398 |
| 6857 | 0.0663 | 0.0041 | 0.0317 | 42.7054 | 405.9477302 | 0.10519926 |
| 6857.5 | 0.0639 | 0.0064 | 0.0389 | 47.9475 | 366.2865601 | 0.13090161 |
| 6858 | 0.0591 | 0.0055 | 0.0519 | 59.6018 | 310.571626 | 0.19191 |
| 6858.5 | 0.056 | 0.004 | 0.0604 | 68.6561 | 280.4188943 | 0.24483407 |
| 6859 | 0.0576 | 0.0069 | 0.0588 | 62.2669 | 280.4188943 | 0.22204959 |
| 6859.5 | 0.0611 | 0.0174 | 0.0421 | 51.2455 | 363.2409736 | 0.14107852 |
| 6860 | 0.0634 | 0.0217 | 0.0349 | 43.2149 | 403.2887589 | 0.10715622 |
| 6860.5 | 0.061 | 0.0047 | 0.0502 | 40.3332 | 309.3719164 | 0.13037124 |
| 6861 | 0.0544 | -0.023 | 0.0779 | 44.4015 | 212.9376786 | 0.20851876 |
| 6861.5 | 0.0489 | -0.0299 | 0.0836 | 53.1622 | 212.2472353 | 0.25047299 |
| 6862 | 0.0471 | -0.0228 | 0.07 | 58.3655 | 276.827261 | 0.21083726 |
| 6862.5 | 0.0472 | -0.0065 | 0.0515 | 56.6735 | 399.7829809 | 0.14176066 |
| 6863 | 0.0481 | 0.0014 | 0.0419 | 51.8354 | 487.5114103 | 0.10632654 |

0.078 to 0.53

| | | | | | | |
|---|---|---|---|---|---|---|
| 6863.5 | 0.0492 | 0.001 | 0.0395 | 48.381 | 503.0027941 | 0.09618436 |
| 6864 | 0.0503 | -0.0038 | 0.0387 | 49.2142 | 499.3645011 | 0.09855366 |
| 6864.5 | 0.0514 | -0.0036 | 0.0357 | 55.8148 | 523.0788339 | 0.10670437 |
| 6865 | 0.0507 | -0.0004 | 0.0343 | 67.3989 | 551.2587423 | 0.12226364 |
| 6865.5 | 0.0469 | 0.0028 | 0.0361 | 82.8904 | 580.214104 | 0.14286175 |
| 6866 | 0.0417 | -0.0004 | 0.0483 | 103.0145 | 487.5114103 | 0.21130685 |
| 6866.5 | 0.0387 | -0.0017 | 0.0577 | 120.4167 | 420.5721952 | 0.28631636 |
| 6867 | 0.04 | -0.0012 | 0.0589 | 110.9784 | 398.046815 | 0.27880741 |
| 6867.5 | 0.045 | -0.0002 | 0.0498 | 83.8127 | 435.9816944 | 0.19223903 |
| 6868 | 0.0502 | -0.0045 | 0.0445 | 79.6244 | 436.9721166 | 0.18221849 |
| 6868.5 | 0.0509 | -0.0094 | 0.0408 | 99.1254 | 468.2870074 | 0.2116766 |
| 6869 | 0.048 | -0.0054 | 0.0346 | 107.3022 | 586.2718993 | 0.18302463 |
| 6869.5 | 0.0471 | 0.0114 | 0.0273 | 82.7722 | 734.0478463 | 0.11276131 |
| 6870 | 0.0501 | 0.016 | 0.0326 | 70.1666 | 584.7487938 | 0.11999443 |
| 6870.5 | 0.0518 | 0.0061 | 0.0468 | 78.1485 | 400.6552271 | 0.19505174 |
| 6871 | 0.047 | -0.0095 | 0.0609 | 102.3337 | 330.073056 | 0.31003349 |
| 6871.5 | 0.041 | -0.0092 | 0.0603 | 121.9826 | 378.0470667 | 0.32266511 |
| 6872 | 0.0396 | -0.0145 | 0.0638 | 122.2775 | 361.7320769 | 0.33803333 |
| 6872.5 | 0.042 | -0.0186 | 0.0635 | 119.7683 | 346.4283234 | 0.34572318 |
| 6873 | 0.0465 | -0.0171 | 0.0574 | 123.3634 | 357.9997744 | 0.34459072 |
| 6873.5 | 0.0505 | -0.0106 | 0.0521 | 130.1831 | 367.8234 | 0.35392827 |
| 6874 | 0.0509 | -0.0112 | 0.0525 | 124.8999 | 361.7320769 | 0.3452829 |
| 6874.5 | 0.0494 | -0.019 | 0.0573 | 93.7432 | 338.1058448 | 0.27725992 |
| 6875 | 0.0491 | -0.0176 | 0.0555 | 65.8394 | 352.8686358 | 0.18658332 |
| 6875.5 | 0.0513 | -0.012 | 0.0569 | 58.5154 | 328.1085666 | 0.17834158 |
| 6876 | 0.0563 | -0.0013 | 0.059 | 67.0648 | 286.2023329 | 0.23432653 |
| 6876.5 | 0.06 | 0.0051 | 0.0525 | 91.9653 | 301.7367838 | 0.30478651 |
| 6877 | 0.0567 | 0.0034 | 0.045 | 135.9219 | 374.8574369 | 0.36259625 |
| 6877.5 | 0.0496 | -0.0127 | 0.0517 | 182.0628 | 378.0470667 | 0.48158765 |
| 6878 | 0.047 | -0.0234 | 0.061 | 175.2867 | 329.4163159 | 0.53211299 |
| 6878.5 | 0.0502 | -0.0205 | 0.0614 | 138.388 | 306.9927801 | 0.45078585 |
| 6879 | 0.0581 | -0.0085 | 0.0556 | 119.9062 | 294.9315146 | 0.40655608 |
| 6879.5 | 0.0703 | 0.0055 | 0.0494 | 99.0019 | 264.0606918 | 0.37492101 |
| 6880 | 0.0905 | 0.0219 | 0.037 | 66.9053 | 230.5468979 | 0.29020256 |
| 6880.5 | 0.1148 | 0.0349 | 0.0286 | 39.0351 | 179.0711014 | 0.2179866 |
| 6881 | 0.1262 | 0.0353 | 0.036 | 25.6704 | 137.4032018 | 0.18682534 |
| 6881.5 | 0.1237 | 0.0199 | 0.0561 | 20.7902 | 110.1053324 | 0.18882101 |
| 6882 | 0.1185 | 0.0031 | 0.0774 | 18.924 | 91.56555725 | 0.2066716 |
| 6882.5 | 0.12 | -0.0038 | 0.0879 | 17.4109 | 80.57847208 | 0.21607384 |
| 6883 | 0.1281 | -0.0024 | 0.0922 | 15.8593 | 71.14182653 | 0.22292512 |
| 6883.5 | 0.13 | -0.0056 | 0.0964 | 14.9704 | 67.08445128 | 0.22315752 |
| 6884 | 0.1264 | -0.0144 | 0.1015 | 14.7436 | 66.13873453 | 0.22291929 |
| 6884.5 | 0.1273 | -0.0258 | 0.1092 | 14.8301 | 61.07580759 | 0.24281464 |
| 6885 | 0.1276 | -0.0223 | 0.1098 | 15.1856 | 60.57907585 | 0.25067401 |
| 6885.5 | 0.1202 | -0.0155 | 0.1117 | 15.8152 | 63.71028834 | 0.2482362 |
| 6886 | 0.108 | -0.0101 | 0.1096 | 16.5232 | 73.05325384 | 0.22618021 |
| 6886.5 | 0.1018 | -0.0122 | 0.1078 | 17.0642 | 79.17989688 | 0.21551177 |
| 6887 | 0.1096 | -0.0124 | 0.102 | 17.4354 | 77.57959427 | 0.22474209 |
| 6887.5 | 0.1225 | -0.0081 | 0.0976 | 17.7284 | 71.28088591 | 0.24871184 |
| 6888 | 0.1229 | -0.0075 | 0.1009 | 17.9015 | 68.7712635 | 0.26030495 |
| 6888.5 | 0.1114 | -0.0085 | 0.1028 | 18.1159 | 75.56911344 | 0.23972625 |
| 6889 | 0.1025 | -0.0069 | 0.1035 | 18.6705 | 82.1848291 | 0.22717696 |

| | Nϕ | dρ | dϕ | HDRS | F= 0.62/ϕ^2.15 | Rwa |
|---|---|---|---|---|---|---|
| 6889.5 | 0.0988 | -0.0022 | 0.1005 | 19.3233 | 88.23999767 | 0.21898573 |
| 6890 | 0.0974 | 0.0076 | 0.0914 | 19.5309 | 99.12926858 | 0.19702455 |
| 6890.5 | 0.0987 | 0.0071 | 0.089 | 19.2374 | 100.3824969 | 0.19164098 |
| 6891 | 0.1006 | 0 | 0.0902 | 18.7083 | 96.9086813 | 0.19305082 |
| 6891.5 | 0.103 | -0.0074 | 0.0926 | 18.1922 | 91.86776519 | 0.19802593 |
| 6892 | 0.1053 | -0.0048 | 0.0858 | 18.0895 | 96.58189071 | 0.18729702 |
| 6892.5 | 0.1055 | 0.0076 | 0.0764 | 18.328 | 107.3905032 | 0.17066686 |
| 6893 | 0.1043 | 0.0115 | 0.0736 | 18.3885 | 112.6491429 | 0.16323693 |
| 6893.5 | 0.1019 | 0.003 | 0.0791 | 18.3975 | 108.5418562 | 0.16949682 |
| 6894 | 0.0968 | -0.0103 | 0.0873 | 18.8344 | 104.6503138 | 0.17997462 |
| 6894.5 | 0.0927 | -0.0135 | 0.0917 | 19.5677 | 104.2846071 | 0.18763747 |
| 6895 | 0.0949 | -0.0026 | 0.0865 | 19.687 | 108.027922 | 0.18223992 |
| 6895.5 | 0.1012 | 0.0088 | 0.0771 | 18.6608 | 112.1064996 | 0.166456 |
| 6896 | 0.1078 | 0.0162 | 0.0635 | 17.1725 | 122.1878012 | 0.14054185 |
| 6896.5 | 0.112 | 0.0107 | 0.0615 | 16.323 | 118.8809591 | 0.13730542 |
| 6897 | 0.1104 | 0.0026 | 0.068 | 16.6183 | 111.9714372 | 0.14841553 |
| 6897.5 | 0.1039 | 0.004 | 0.0666 | 17.4697 | 123.4237553 | 0.14154244 |
| 6898 | 0.0998 | 0.0026 | 0.0702 | 17.7249 | 124.2055491 | 0.14270618 |
| 6898.5 | 0.1004 | -0.0047 | 0.0779 | 17.5348 | 112.1064996 | 0.15641198 |
| 6899 | 0.097 | -0.0095 | 0.0814 | 17.8449 | 111.9714372 | 0.15937011 |
| 6899.5 | 0.0872 | -0.0026 | 0.0668 | 18.6586 | 153.616063 | 0.12146256 |
| 6900 | 0.078 | 0.0034 | 0.0515 | 19.5237 | 222.9596008 | 0.08756609 |
| 6900.5 | 0.0743 | 0.0022 | 0.0454 | 20.5121 | 264.0606918 | 0.07767949 |
| 6901 | 0.0767 | 0.0004 | 0.0514 | 21.5148 | 228.2314825 | 0.09426745 |
| 6901.5 | 0.0813 | -0.0068 | 0.0683 | 22.1582 | 163.4945401 | 0.13552868 |
| 6902 | 0.0829 | -0.0157 | 0.0784 | 23.2595 | 139.056819 | 0.16726616 |
| 6902.5 | 0.0883 | -0.0193 | 0.0794 | 26.7485 | 127.8969228 | 0.20914108 |
| 6903 | 0.1096 | -0.0066 | 0.0718 | 33.6802 | 108.027922 | 0.3117731 |
| 6903.5 | 0.1576 | 0.033 | 0.0776 | 37.7519 | 61.80390948 | 0.61083353 |
| 6904 | 0.2333 | 0.0837 | 0.1178 | 25.2598 | 26.11739737 | 0.96716375 |
| 6904.5 | 0.2959 | 0.105 | 0.1695 | 14.9895 | 14.24883854 | 1.05198048 |
| 6905 | 0.2997 | 0.0839 | 0.1944 | 12.2825 | 12.52864906 | 0.9803531 |
| 6905.5 | 0.2521 | 0.0691 | 0.1476 | 13.5731 | 19.76413271 | 0.68675414 |
| 6906 | 0.1879 | 0.0622 | 0.0927 | 19.1053 | 42.28805365 | 0.45178953 |
| 6906.5 | 0.1395 | 0.0412 | 0.0644 | 31.1962 | 84.01544746 | 0.37131505 |
| 6907 | 0.1263 | 0.0104 | 0.0605 | 35.5553 | 101.4252077 | 0.35055684 |
| 6907.5 | 0.1427 | -0.0026 | 0.0592 | 25.4506 | 85.8149778 | 0.29657527 |
| 6908 | 0.1599 | 0.001 | 0.0562 | 20.047 | 74.14782758 | 0.2703653 |
| 6908.5 | 0.1442 | 0.0138 | 0.051 | 22.5022 | 92.27298742 | 0.24386552 |
| 6909 | 0.1021 | 0.0168 | 0.0565 | 34.7564 | 144.196373 | 0.24103519 |
| 6909.5 | 0.0704 | 0.0071 | 0.0737 | 58.6861 | 177.2060812 | 0.3311743 |
| 6910 | 0.0577 | -0.0113 | 0.0939 | 85.2419 | 158.8923168 | 0.53647591 |
| 6910.5 | 0.0546 | -0.0154 | 0.1019 | 89.0253 | 148.3885343 | 0.5999473 |
| 6911 | 0.0553 | -0.007 | 0.0983 | 83.1096 | 154.477441 | 0.53800477 |
| 6911.5 | 0.0548 | 0.0023 | 0.0903 | 81.8614 | 174.5907552 | 0.46887591 |
| 6912 | 0.0534 | 0.0066 | 0.0802 | 84.7982 | 208.5077948 | 0.40669079 |
| 6912.5 | 0.0522 | 0.0078 | 0.0715 | 87.1903 | 246.0431769 | 0.35436992 |
| 6913 | 0.0528 | 0.0069 | 0.0683 | 82.9338 | 257.5409376 | 0.32202181 |
| 6913.5 | 0.0576 | 0.0017 | 0.0764 | 69.2778 | 207.171907 | 0.33439766 |
| 6914 | 0.0637 | 0.0027 | 0.0832 | 56.3739 | 170.0236437 | 0.33156506 |
| 6914.5 | 0.069 | 0.0048 | 0.092 | 50.7695 | 139.6145069 | 0.36364058 |
| 6915 | 0.0723 | 0.004 | 0.0975 | 52.7848 | 124.5202992 | 0.42390518 |

2.15 .62 Archie

46,000 PPM

use deep resistivity curve if > 4 Sapi

$R_o = F R_w$

$R_o$ = deep resistivity

$R_o$

0.32 to 0.66

$R_{wa}$ value at formation temp (correct to 77°F)

| Depth | NΦ | Dρ | Dφ | HDRS | | |
|---|---|---|---|---|---|---|
| 6915.5 | 0.071 | 0.0052 | 0.0937 | 61.9707 | 132.9581434 | 0.4660918 |
| 6916 | 0.0687 | 0.0058 | 0.0841 | 69.4179 | 156.2215594 | 0.44435544 |
| 6916.5 | 0.0685 | 0.0053 | 0.0754 | 70.6766 | 177.7360291 | 0.39764926 |
| 6917 | 0.068 | 0.0004 | 0.0725 | 75.4469 | 187.1121905 | 0.40321745 |
| 6917.5 | 0.0664 | 0.0026 | 0.0749 | 89.1739 | 184.841946 | 0.48243325 |
| 6918 | 0.0668 | 0.0058 | 0.0769 | 99.2974 | 178.2683023 | 0.55701097 |
| 6918.5 | 0.0683 | 0.0015 | 0.0794 | 96.3327 | 168.0498446 | 0.57323885 |
| 6919 | 0.0705 | 0.0001 | 0.0744 | 89.8209 | 175.1092756 | 0.51294199 |
| 6919.5 | 0.0844 | 0.0007 | 0.0685 | 84.435 | 156.0019714 | 0.54124316 |
| 6920 | 0.1078 | -0.0017 | 0.0685 | 75.8151 | 114.8586503 | 0.66007305 |
| 6920.5 | 0.1186 | -0.0032 | 0.067 | 67.578 | 102.8403487 | 0.65711562 |
| 6921 | 0.1137 | -0.0063 | 0.0609 | 65.8488 | 117.2765187 | 0.56148324 |
| 6921.5 | 0.1075 | -0.0046 | 0.0518 | 67.3268 | 142.8375072 | 0.47135239 |
| 6922 | 0.1066 | 0.0041 | 0.0432 | 54.6984 | 163.0255903 | 0.33552033 |
| 6922.5 | 0.11 | 0.0248 | 0.0431 | 29.0727 | 155.5641499 | 0.1868856 |
| 6923 | 0.1274 | 0.0521 | 0.0733 | 19.2657 | 86.92192371 | 0.22164374 |
| 6923.5 | 0.1743 | 0.1072 | 0.1266 | 16.2597 | 36.39137595 | 0.44680091 |
| 6924 | 0.2132 | 0.1594 | 0.1583 | 14.323 | 23.13101665 | 0.61921187 |
| 6924.5 | 0.1878 | 0.1577 | 0.1369 | 13.0615 | 30.89720964 | 0.42274044 |
| 6925 | 0.1335 | 0.1108 | 0.0808 | 14.0815 | 75.49331783 | 0.18652644 |
| 6925.5 | 0.1098 | 0.0666 | 0.0252 | 19.947 | 203.8865504 | 0.09783382 |
| 6926 | 0.1082 | 0.0387 | -0.0084 | 44.8547 | 390.3691746 | 0.11490328 |
| 6926.5 | 0.1061 | 0.0217 | -0.0251 | 65.0332 | 611.4534357 | 0.10635839 |
| 6927 | 0.1036 | 0.0129 | -0.0229 | 94.9393 | 616.3509653 | 0.15403448 |
| 6927.5 | 0.1099 | 0.0169 | -0.0182 | 104.7516 | 468.2870074 | 0.22369102 |
| 6928 | 0.1258 | 0.026 | -0.0143 | 43.752 | 307.5850445 | 0.14224359 |
| 6928.5 | 0.143 | 0.0408 | 0.0003 | 31.2942 | 179.3398783 | 0.17449661 |
| 6929 | 0.16 | 0.0808 | 0.0295 | 25.4336 | 98.34366052 | 0.25861962 |
| 6929.5 | 0.1841 | 0.1263 | 0.0601 | 21.7364 | 57.01025874 | 0.38127173 |
| 6930 | 0.2178 | 0.1169 | 0.0702 | 21.3975 | 39.98640234 | 0.53511941 |
| 6930.5 | 0.2452 | 0.0488 | 0.0632 | 23.044 | 34.5151914 | 0.66764804 |
| 6931 | 0.2462 | -0.0103 | 0.0443 | 22.9545 | 39.25021014 | 0.58482489 |
| 6931.5 | 0.2232 | -0.0316 | 0.0356 | 21.6347 | 50.31911513 | 0.42994993 |
| 6932 | 0.1974 | -0.0346 | 0.0379 | 21.5537 | 61.74745137 | 0.34906218 |
| 6932.5 | 0.1723 | -0.0238 | 0.0352 | 24.0163 | 80.91280609 | 0.29681704 |
| 6933 | 0.1367 | -0.0083 | 0.0243 | 32.4288 | 139.6145069 | 0.23227386 |
| 6933.5 | 0.1027 | 0.0013 | 0.0171 | 55.17 | 263.5870207 | 0.20930469 |
| 6934 | 0.0873 | 0.0007 | 0.0152 | 91.1237 | 368.5953648 | 0.24721879 |
| 6934.5 | 0.0847 | -0.0059 | 0.0146 | 101.973 | 394.6074642 | 0.2584163 |
| 6935 | 0.0839 | -0.0159 | 0.0129 | 92.0503 | 416.8445829 | 0.22082643 |
| 6935.5 | 0.0821 | -0.0221 | 0.0122 | 113.6296 | 440.96695 | 0.2576828 |
| 6936 | 0.0794 | -0.0226 | 0.0114 | 157.5513 | 478.3233762 | 0.3293824 |
| 6936.5 | 0.0774 | -0.0179 | 0.0091 | 160.4055 | 530.9107867 | 0.30213268 |
| 6937 | 0.0898 | -0.0156 | 0.0114 | 113.1135 | 378.8506863 | 0.29857013 |
| 6937.5 | 0.1227 | -0.0164 | 0.0124 | 74.0042 | 203.5622206 | 0.36354585 |
| 6938 | 0.1519 | -0.0189 | 0.0177 | 47.7445 | 124.8362192 | 0.38245711 |
| 6938.5 | 0.1618 | -0.0062 | 0.0418 | 39.0449 | 84.28183194 | 0.46326592 |
| 6939 | 0.1566 | 0.024 | 0.1409 | 77.5517 | 37.29144349 | 2.0796111 |
| 6939.5 | 0.1452 | 0.0738 | 0.3096 | 98.1962 | 14.97242684 | 6.55846918 |
| 6940 | 0.1722 | 0.1276 | 0.4606 | 55.1785 | 7.360092435 | 7.49698465 |
| 6940.5 | 0.2647 | 0.1519 | 0.5522 | 22.3703 | 4.250529686 | 5.26294407 |
| 6941 | 0.322 | 0.1508 | 0.5943 | 11.4925 | 3.320665683 | 3.46090245 |

| | | | | | | |
|---|---|---|---|---|---|---|
| 6941.5 | 0.2814 | 0.1419 | 0.6163 | 5.7793 | 3.470356141 | 1.6653334 |
| 6942 | 0.2365 | 0.1431 | 0.5961 | 6.2062 | 4.080072743 | 1.52110033 |
| 6942.5 | 0.2225 | 0.162 | 0.4756 | 11.6743 | 5.959135471 | 1.95905934 |
| 6943 | 0.1949 | 0.1677 | 0.2664 | 26.2434 | 14.52251229 | 1.80708403 |
| 6943.5 | 0.1573 | 0.1344 | 0.1142 | 57.946 | 45.39427008 | 1.27650472 |
| 6944 | 0.1468 | 0.0876 | 0.1623 | 150.0507 | 34.34735662 | 4.36862439 |
| 6944.5 | 0.1821 | 0.0749 | 0.3699 | 98.8411 | 9.872727795 | 10.0115289 |
| 6945 | 0.248 | 0.106 | 0.538 | 37.1406 | 4.617933836 | 8.04268777 |
| 6945.5 | 0.3243 | 0.1427 | 0.589 | 19.3754 | 3.344161527 | 5.79379909 |
| 6946 | 0.3834 | 0.1675 | 0.5705 | 9.8175 | 3.045615368 | 3.22348649 |
| 6946.5 | 0.4067 | 0.1597 | 0.5367 | 8.578 | 3.118961799 | 2.75027415 |
| 6947 | 0.3977 | 0.1146 | 0.4644 | 9.0815 | 3.785796307 | 2.39883482 |
| 6947.5 | 0.348 | 0.0508 | 0.3583 | 12.1708 | 5.811381503 | 2.09430408 |
| 6948 | 0.2676 | 0.0069 | 0.2298 | 31.3549 | 12.35061976 | 2.5387309 |
| 6948.5 | 0.202 | -0.0071 | 0.1147 | 51.6471 | 32.59964299 | 1.58428422 |
| 6949 | 0.1828 | 0.0068 | 0.0536 | 159.2885 | 61.13136805 | 2.60567537 |
| 6949.5 | 0.1925 | 0.0506 | 0.0909 | 443.0428 | 41.3948689 | 10.7028434 |
| 6950 | 0.207 | 0.1139 | 0.2274 | 196.8725 | 16.52506112 | 11.9135717 |
| 6950.5 | 0.2456 | 0.1542 | 0.4048 | 55.5431 | 6.938539023 | 8.00501371 |
| 6951 | 0.3183 | 0.1543 | 0.5485 | 24.9342 | 3.741799731 | 6.66369175 |
| 6951.5 | 0.404 | 0.1642 | 0.5732 | 11.2152 | 2.891623495 | 3.87851324 |
| 6952 | 0.482 | 0.2077 | 0.4989 | 6.3035 | 2.868223574 | 2.19770176 |
| 6952.5 | 0.53 | 0.2619 | 0.4016 | 5.5502 | 3.204518613 | 1.73199181 |
| 6953 | 0.5331 | 0.29 | 0.3244 | 6.4433 | 3.829594612 | 1.68250184 |
| 6953.5 | 0.4984 | 0.2832 | 0.2622 | 9.1521 | 4.955872102 | 1.84671836 |
| 6954 | 0.4563 | 0.2619 | 0.2256 | 13.8894 | 6.267678276 | 2.21603589 |
| 6954.5 | 0.4215 | 0.2719 | 0.2072 | 14.8543 | 7.463675349 | 1.9902125 |
| 6955 | 0.3737 | 0.3242 | 0.1873 | 14.5612 | 9.535336602 | 1.52707771 |
| 6955.5 | 0.3157 | 0.3965 | 0.1423 | 23.6667 | 14.7484168 | 1.60469428 |
| 6956 | 0.2769 | 0.4132 | 0.1306 | 46.2074 | 18.95971532 | 2.43713575 |
| 6956.5 | 0.2592 | 0.3723 | 0.1122 | 60.0326 | 23.14440906 | 2.5938273 |
| 6957 | 0.24 | 0.2997 | 0.054 | 83.632 | 38.25246441 | 2.18631665 |
| 6957.5 | 0.2081 | 0.2417 | -0.0111 | 144.524 | 90.4698341 | 1.59748276 |
| 6958 | 0.1739 | 0.333 | -0.0908 | 297.3675 | 578.7139871 | 0.51384191 |
| 6958.5 | 0.1612 | 0.5644 | -0.1939 | 305.2735 | #NUM! | #NUM! |
| 6959 | 0.1911 | 0.7176 | -0.2217 | 100.3234 | #NUM! | #NUM! |
| 6959.5 | 0.2577 | 0.6389 | -0.071 | 36.3437 | 101.5420429 | 0.35791775 |
| 6960 | 0.3319 | 0.4461 | 0.1647 | 18.396 | 12.3934364 | 1.48433408 |
| 6960.5 | 0.3864 | 0.3508 | 0.2841 | 9.3081 | 6.499033842 | 1.43222827 |
| 6961 | 0.4008 | 0.3391 | 0.3134 | 8.6644 | 5.674054613 | 1.5270209 |
| 6961.5 | 0.3948 | 0.3265 | 0.3447 | 14.8941 | 5.264887514 | 2.82894933 |
| 6962 | 0.4149 | 0.2754 | 0.421 | 15.5508 | 4.045520264 | 3.84395553 |
| 6962.5 | 0.4566 | 0.2329 | 0.4729 | 17.5866 | 3.220104626 | 5.46149956 |
| 6963 | 0.491 | 0.2313 | 0.4621 | 11.6906 | 3.051114253 | 3.83158382 |
| 6963.5 | 0.5293 | 0.2419 | 0.4393 | 10.9754 | 2.947104809 | 3.72412951 |
| 6964 | 0.571 | 0.2024 | 0.4999 | 11.294 | 2.374903706 | 4.75556123 |
| 6964.5 | 0.6353 | 0.124 | 0.6409 | 11.076 | 1.628849236 | 6.79989268 |
| 6965 | 0.7317 | 0.0597 | 0.7704 | 10.1168 | 1.147370451 | 8.8173789 |
| 6965.5 | 0.7901 | 0.0322 | 0.8297 | 10.3051 | 0.975582905 | 10.5630182 |
| 6966 | 0.753 | 0.0254 | 0.802 | 15.135 | 1.065088841 | 14.2100822 |
| 6966.5 | 0.6344 | 0.0245 | 0.6779 | 28.4503 | 1.534033886 | 18.5460701 |
| 6967 | 0.5141 | 0.0381 | 0.5017 | 68.5743 | 2.660532276 | 25.7746544 |

| | | | | | | |
|---|---|---|---|---|---|---|
| 6967.5 | 0.4287 | 0.0801 | 0.3873 | 195.7768 | 4.260615459 | 45.9503567 |
| 6968 | 0.3689 | 0.1191 | 0.3888 | 243.3021 | 4.996742998 | 48.6921381 |
| 6968.5 | 0.3268 | 0.1051 | 0.4301 | 124.0036 | 5.008104633 | 24.7605849 |
| 6969 | 0.2966 | 0.0571 | 0.3937 | 68.2728 | 6.104846554 | 11.1833769 |
| 6969.5 | 0.2753 | 0.0431 | 0.2706 | 46.4876 | 10.11144043 | 4.59752499 |
| 6970 | 0.2505 | 0.0769 | 0.1269 | 37.0912 | 22.36053056 | 1.65877996 |
| 6970.5 | 0.2165 | 0.0847 | 0.044 | 33.6894 | 49.61575059 | 0.67900615 |
| 6971 | 0.1786 | 0.0382 | 0.0259 | 35.4444 | 83.48636623 | 0.42455315 |
| 6971.5 | 0.1537 | -0.0072 | 0.0277 | 33.6365 | 108.027922 | 0.31136857 |
| 6972 | 0.1444 | -0.0119 | 0.0222 | 32.1627 | 129.7194016 | 0.24794055 |
| 6972.5 | 0.1407 | -0.0025 | 0.0204 | 30.7091 | 139.4282474 | 0.2202502 |
| 6973 | 0.1399 | -0.0098 | 0.0251 | 29.6275 | 132.4389412 | 0.22370686 |
| 6973.5 | 0.1384 | -0.0143 | 0.0265 | 29.8643 | 132.611678 | 0.22520113 |
| 6974 | 0.1325 | -0.0033 | 0.019 | 30.3896 | 159.1178931 | 0.19098795 |
| 6974.5 | 0.1234 | 0.0152 | 0.0069 | 31.0534 | 220.0268526 | 0.14113459 |
| 6975 | 0.115 | 0.0244 | -0.0019 | 32.3618 | 298.305719 | 0.10848535 |
| 6975.5 | 0.1095 | 0.0181 | 0.003 | 34.2704 | 301.7367838 | 0.11357714 |
| 6976 | 0.1037 | 0.0175 | 0.0138 | 35.0652 | 274.8050865 | 0.12760026 |
| 6976.5 | 0.0966 | 0.0247 | 0.0217 | 35.2992 | 270.8251418 | 0.13033945 |
| 6977 | 0.0914 | 0.0304 | 0.0277 | 39.5302 | 266.9290821 | 0.14809252 |
| 6977.5 | 0.0853 | 0.0268 | 0.0346 | 49.0856 | 263.1145934 | 0.18655598 |
| 6978 | 0.0769 | 0.0106 | 0.0475 | 59.074 | 243.0761575 | 0.24302671 |
| 6978.5 | 0.0692 | -0.0018 | 0.0514 | 66.5751 | 259.8420706 | 0.25621371 |
| 6979 | 0.0646 | -0.0003 | 0.042 | 75.6631 | 338.7881334 | 0.22333456 |
| 6979.5 | 0.0659 | 0.0015 | 0.0325 | 84.1441 | 402.4081042 | 0.20910141 |
| 6980 | 0.0716 | 0.0068 | 0.0242 | 85.2477 | 426.2558336 | 0.19999187 |
| 6980.5 | 0.0768 | 0.0147 | 0.0171 | 86.6315 | 445.0155194 | 0.19467074 |
| 6981 | 0.0799 | 0.0118 | 0.0226 | 98.009 | 368.5953648 | 0.26589862 |
| 6981.5 | 0.081 | 0.0104 | 0.0274 | 127.3422 | 326.8084096 | 0.38965399 |
| 6982 | 0.0844 | 0.0109 | 0.0309 | 154.6929 | 286.2023329 | 0.54050188 |
| 6982.5 | 0.0957 | 0.0246 | 0.0241 | 137.6108 | 263.5870207 | 0.52206971 |
| 6983 | 0.1083 | 0.0332 | 0.0284 | 97.3204 | 198.4741149 | 0.49034304 |
| 6983.5 | 0.1116 | 0.0331 | 0.0367 | 63.972 | 166.5914489 | 0.3840053 |
| 6984 | 0.106 | 0.0238 | 0.0435 | 46.7804 | 163.7297565 | 0.28571715 |
| 6984.5 | 0.0973 | 0.0078 | 0.0485 | 39.1467 | 172.7935406 | 0.22655187 |
| 6985 | 0.089 | -0.0105 | 0.0596 | 36.2789 | 165.8691961 | 0.21871994 |
| 6985.5 | 0.0855 | -0.0154 | 0.0687 | 35.854 | 153.1880108 | 0.23405226 |
| 6986 | 0.0872 | -0.0079 | 0.0717 | 36.1579 | 143.6116927 | 0.25177546 |
| 6986.5 | 0.0885 | 0.0044 | 0.0661 | 35.6902 | 152.3371329 | 0.23428431 |
| 6987 | 0.087 | 0.0075 | 0.0621 | 34.4005 | 164.6755971 | 0.20889859 |
| 6987.5 | 0.0858 | 0.0078 | 0.0588 | 33.4556 | 175.8912966 | 0.19020611 |
| 6988 | 0.0879 | 0.0159 | 0.0503 | 33.9212 | 193.871463 | 0.17496747 |
| 6988.5 | 0.0924 | 0.0233 | 0.049 | 35.4605 | 184.5610065 | 0.1921343 |
| 6989 | 0.0958 | 0.0213 | 0.0521 | 37.3927 | 167.5616414 | 0.22315788 |
| 6989.5 | 0.0955 | 0.0116 | 0.0621 | 39.5791 | 146.1706984 | 0.27077315 |
| 6990 | 0.093 | 0.001 | 0.0679 | 40.5148 | 139.8011312 | 0.28980309 |
| 6990.5 | 0.0929 | -0.0024 | 0.0687 | 39.6235 | 138.5023888 | 0.28608532 |
| 6991 | 0.0932 | 0.0003 | 0.0729 | 38.9754 | 130.5603995 | 0.2985239 |
| 6991.5 | 0.0909 | 0.003 | 0.0789 | 38.8307 | 124.5202992 | 0.31184233 |
| 6992 | 0.0895 | 0.0049 | 0.0816 | 37.7899 | 122.4950839 | 0.30850136 |
| 6992.5 | 0.0894 | -0.0033 | 0.0878 | 36.1713 | 113.6080714 | 0.31838671 |
| 6993 | 0.0883 | -0.0132 | 0.0941 | 35.2765 | 106.7585796 | 0.33043246 |

0.14 to 0.57

| | | | | | | |
|---|---|---|---|---|---|---|
| 6993.5 | 0.089 | -0.0097 | 0.0901 | 35.6205 | 111.0326412 | 0.32081107 |
| 6994 | 0.0936 | 0.0008 | 0.0826 | 36.8078 | 114.9988471 | 0.32007103 |
| 6994.5 | 0.0964 | 0.0046 | 0.08 | 38.2067 | 114.7187038 | 0.33304682 |
| 6995 | 0.0955 | 0.0027 | 0.0805 | 40.1528 | 115.2799938 | 0.34830675 |
| 6995.5 | 0.0942 | 0.0016 | 0.0801 | 42.7939 | 117.7109319 | 0.36355077 |
| 6996 | 0.0898 | 0.0057 | 0.0731 | 45.5934 | 136.1368975 | 0.33490847 |
| 6996.5 | 0.0827 | 0.0052 | 0.0691 | 48.9898 | 158.4425675 | 0.30919595 |
| 6997 | 0.0804 | -0.0021 | 0.0717 | 53.0914 | 157.7714329 | 0.33650832 |
| 6997.5 | 0.0834 | -0.0077 | 0.0761 | 55.5714 | 142.4527056 | 0.39010421 |
| 6998 | 0.0844 | -0.0055 | 0.0733 | 55.7423 | 145.9714895 | 0.38187115 |
| 6998.5 | 0.0833 | -0.0016 | 0.0686 | 57.6883 | 158.218392 | 0.36461185 |
| 6999 | 0.0819 | -0.0037 | 0.0696 | 65.5844 | 159.1178931 | 0.41217489 |
| 6999.5 | 0.0757 | -0.0124 | 0.0741 | 81.8508 | 163.0255903 | 0.50207332 |
| 7000 | 0.0645 | -0.0148 | 0.0737 | 105.3215 | 193.871463 | 0.54325427 |
| 7000.5 | 0.0526 | -0.0089 | 0.0685 | 132.0444 | 257.5409376 | 0.51271227 |
| 7001 | 0.0448 | -0.0041 | 0.0649 | 160.3286 | 318.5385002 | 0.50332566 |
| 7001.5 | 0.0425 | -0.0099 | 0.0669 | 175.0978 | 320.4194996 | 0.54646425 |
| 7002 | 0.0448 | -0.0155 | 0.07 | 156.4943 | 288.8890767 | 0.54171069 |
| 7002.5 | 0.0512 | -0.007 | 0.0662 | 113.6534 | 275.3085961 | 0.41282184 |
| 7003 | 0.0603 | 0.0004 | 0.0641 | 79.063 | 243.0761575 | 0.3252602 |
| 7003.5 | 0.0686 | 0.0043 | 0.0621 | 59.5747 | 218.5816333 | 0.27255126 |
| 7004 | 0.073 | 0.0056 | 0.0609 | 51.935 | 207.5047008 | 0.25028349 |
| 7004.5 | 0.0753 | 0.0113 | 0.0612 | 50.6786 | 199.0998715 | 0.25453859 |
| 7005 | 0.0761 | 0.0178 | 0.0624 | 50.1923 | 192.9697203 | 0.26010454 |
| 7005.5 | 0.0773 | 0.0195 | 0.0661 | 47.1166 | 179.0711014 | 0.26311672 |
| 7006 | 0.0805 | 0.0171 | 0.067 | 42.7434 | 168.5401346 | 0.25360962 |
| 7006.5 | 0.0843 | 0.0127 | 0.067 | 39.2946 | 159.5704556 | 0.24625235 |
| 7007 | 0.0874 | 0.0061 | 0.0695 | 38.0672 | 147.5763795 | 0.25794914 |
| 7007.5 | 0.0884 | -0.0042 | 0.0737 | 40.3255 | 137.5855101 | 0.29309409 |
| 7008 | 0.0873 | 0.0011 | 0.0641 | 43.7048 | 159.3439389 | 0.27427965 |
| 7008.5 | 0.0861 | 0.0124 | 0.0489 | 40.9157 | 203.8865504 | 0.20067876 |
| 7009 | 0.0857 | 0.0254 | 0.0396 | 34.9137 | 239.3378457 | 0.14587622 |
| 7009.5 | 0.0873 | 0.0307 | 0.041 | 32.799 | 227.4672457 | 0.14419219 |
| 7010 | 0.0899 | 0.0188 | 0.0495 | 35.286 | 190.301064 | 0.18542198 |
| 7010.5 | 0.0921 | 0.0019 | 0.0629 | 39.1022 | 151.4931616 | 0.25811198 |
| 7011 | 0.094 | -0.0028 | 0.0702 | 39.7427 | 133.8301306 | 0.29696377 |
| 7011.5 | 0.0946 | -0.0013 | 0.0722 | 36.8167 | 129.3852236 | 0.28455104 |
| 7012 | 0.0939 | 0.0019 | 0.0676 | 35.9905 | 138.6868384 | 0.25950912 |
| 7012.5 | 0.0888 | 0.0011 | 0.0652 | 41.9751 | 153.616063 | 0.27324682 |
| 7013 | 0.0802 | 0.0131 | 0.0662 | 54.6387 | 171.2745619 | 0.31901235 |
| 7013.5 | 0.079 | 0.028 | 0.0743 | 51.4688 | 155.1281264 | 0.33178252 |
| 7014 | 0.0881 | 0.0402 | 0.0741 | 40.2816 | 137.4032018 | 0.29316347 |
| 7014.5 | 0.0951 | 0.0365 | 0.0654 | 39.7483 | 140.5512949 | 0.2828028 |
| 7015 | 0.0902 | 0.024 | 0.0533 | 51.571 | 178.8029142 | 0.28842371 |
| 7015.5 | 0.0788 | 0.0111 | 0.0542 | 70.2962 | 210.5354108 | 0.33389253 |
| 7016 | 0.0709 | -0.0006 | 0.0638 | 87.5315 | 204.8640949 | 0.42726618 |
| 7016.5 | 0.0715 | -0.0062 | 0.0706 | 104.9119 | 182.6118317 | 0.57450768 |
| 7017 | 0.0826 | 0.0036 | 0.0603 | 88.3731 | 180.420918 | 0.48981626 |
| 7017.5 | 0.1027 | 0.0175 | 0.0432 | 56.0092 | 172.5390103 | 0.3246176 |
| 7018 | 0.122 | 0.0182 | 0.0407 | 40.0435 | 136.4969481 | 0.29336553 |
| 7018.5 | 0.1321 | 0.0126 | 0.0477 | 32.4142 | 110.1053324 | 0.29439264 |
| 7019 | 0.139 | 0.007 | 0.0542 | 27.3005 | 94.33891296 | 0.28938748 |

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|---|---|---|---|---|---|---|
| 7019.5 | 0.1469 | 0.0001 | 0.0638 | 24.7439 | 78.29381019 | 0.31603903 |
| 7020 | 0.1471 | -0.0115 | 0.0803 | 24.134 | 66.45179099 | 0.36318058 |
| 7020.5 | 0.1367 | -0.0142 | 0.0919 | 25.5371 | 65.70407327 | 0.38866845 |
| 7021 | 0.1221 | 0.005 | 0.0825 | 31.9616 | 83.39866083 | 0.38323877 |
| 7021.5 | 0.1031 | 0.0227 | 0.0689 | 50.9612 | 121.1211594 | 0.42074564 |
| 7022 | 0.0824 | 0.0196 | 0.0692 | 91.8256 | 158.8923168 | 0.57791089 |
| 7022.5 | 0.07 | 0.0076 | 0.078 | 122.0727 | 167.3183188 | 0.72958359 |
| 7023 | 0.0663 | 0.0032 | 0.0828 | 107.4973 | 164.6755971 | 0.65278221 |
| 7023.5 | 0.0653 | 0.0025 | 0.0781 | 89.3046 | 179.0711014 | 0.49871028 |
| 7024 | 0.0624 | -0.0047 | 0.0748 | 78.0184 | 196.9222733 | 0.3961888 |
| 7024.5 | 0.0582 | -0.0156 | 0.0765 | 73.0297 | 204.8640949 | 0.35647877 |
| 7025 | 0.0582 | -0.0183 | 0.0745 | 73.7523 | 211.5600671 | 0.34861163 |
| 7025.5 | 0.0634 | -0.0184 | 0.0735 | 79.0174 | 197.8512355 | 0.39937784 |
| 7026 | 0.0716 | -0.0223 | 0.0725 | 81.6864 | 177.2060812 | 0.46096838 |
| 7026.5 | 0.0828 | -0.0203 | 0.0671 | 71.4056 | 162.7918541 | 0.43863128 |
| 7027 | 0.0943 | -0.0132 | 0.06 | 56.0765 | 152.9746398 | 0.36657383 |
| 7027.5 | 0.0978 | -0.0105 | 0.0575 | 46.9295 | 150.8646711 | 0.31107018 |
| 7028 | 0.0906 | -0.0187 | 0.0664 | 44.127 | 147.3743584 | 0.29942115 |
| 7028.5 | 0.0841 | -0.0263 | 0.0686 | 41.9856 | 156.4416005 | 0.26837874 |
| 7029 | 0.0862 | -0.0194 | 0.0608 | 37.8021 | 169.775067 | 0.2226599 |
| 7029.5 | 0.0902 | 0.0001 | 0.0528 | 33.6863 | 180.1497649 | 0.18699053 |
| 7030 | 0.0928 | 0.0126 | 0.0553 | 30.968 | 167.0755134 | 0.18535331 |
| 7030.5 | 0.0956 | 0.0082 | 0.0651 | 29.4668 | 140.1754778 | 0.21021366 |
| 7031 | 0.0973 | -0.0051 | 0.0772 | 28.2243 | 117.4210617 | 0.24036829 |
| 7031.5 | 0.0977 | -0.0131 | 0.0842 | 26.8284 | 107.3905032 | 0.24982097 |
| 7032 | 0.0968 | -0.0074 | 0.0839 | 25.9332 | 108.929661 | 0.2380729 |
| 7032.5 | 0.0953 | -0.0008 | 0.0792 | 25.9161 | 117.4210617 | 0.22071083 |
| 7033 | 0.0942 | 0.0068 | 0.0737 | 26.5355 | 127.569597 | 0.20800803 |
| 7033.5 | 0.0925 | 0.0098 | 0.0703 | 27.3594 | 136.3167486 | 0.20070461 |
| 7034 | 0.091 | 0.0147 | 0.0593 | 27.7902 | 161.8618023 | 0.17169091 |
| 7034.5 | 0.0934 | 0.0126 | 0.0543 | 27.5634 | 168.0498446 | 0.16401919 |
| 7035 | 0.0983 | 0.0008 | 0.0641 | 27.3755 | 137.0396455 | 0.19976336 |
| 7035.5 | 0.1006 | -0.0027 | 0.0759 | 28.1868 | 114.579007 | 0.24600318 |
| 7036 | 0.0993 | -0.0008 | 0.0821 | 30.0025 | 108.027922 | 0.27772912 |
| 7036.5 | 0.0979 | 0.0028 | 0.0843 | 31.9558 | 107.0106936 | 0.29862249 |
| 7037 | 0.0963 | 0.0022 | 0.0868 | 33.5522 | 105.8830005 | 0.31687995 |
| 7037.5 | 0.0924 | -0.0057 | 0.0903 | 34.5048 | 106.3820374 | 0.32434799 |
| 7038 | 0.09 | -0.0159 | 0.0912 | 34.5748 | 108.2844424 | 0.3192961 |
| 7038.5 | 0.0898 | -0.0232 | 0.0864 | 34.6766 | 114.9988471 | 0.30153868 |
| 7039 | 0.0887 | -0.0163 | 0.0788 | 36.532 | 128.2254807 | 0.28490437 |
| 7039.5 | 0.0861 | -0.0047 | 0.0757 | 42.0447 | 138.1345662 | 0.30437494 |
| 7040 | 0.0817 | -0.0027 | 0.0801 | 51.516 | 138.1345662 | 0.37294069 |
| 7040.5 | 0.0791 | -0.009 | 0.0847 | 55.136 | 134.5337664 | 0.4098302 |
| 7041 | 0.0824 | -0.0178 | 0.0873 | 45.4677 | 124.6781126 | 0.36468069 |
| 7041.5 | 0.0888 | -0.0175 | 0.0869 | 36.4356 | 115.7036056 | 0.31490462 |
| 7042 | 0.0923 | -0.0099 | 0.0889 | 33.2821 | 108.2844424 | 0.3073581 |
| 7042.5 | 0.0911 | -0.005 | 0.0894 | 33.5662 | 109.1893264 | 0.30741283 |
| 7043 | 0.088 | -0.0137 | 0.0945 | 34.5606 | 106.6328489 | 0.32410838 |
| 7043.5 | 0.0847 | -0.0239 | 0.1002 | 34.9903 | 103.6792439 | 0.33748606 |
| 7044 | 0.082 | -0.0246 | 0.1036 | 35.0441 | 102.8403487 | 0.34076217 |
| 7044.5 | 0.0819 | -0.0205 | 0.1012 | 35.3005 | 105.8830005 | 0.33339157 |
| 7045 | 0.0829 | -0.0182 | 0.0958 | 35.5508 | 111.5676775 | 0.31864785 |

0.35 to 0.73

0.15 to 0.41

| | | | | | | |
|---|---|---|---|---|---|---|
| 7045.5 | 0.0845 | -0.0129 | 0.0892 | 35.4699 | 118.5868602 | 0.29910481 |
| 7046 | 0.0872 | -0.0092 | 0.083 | 35.3936 | 123.8919633 | 0.28568116 |
| 7046.5 | 0.089 | -0.0064 | 0.0785 | 36.0992 | 128.2254807 | 0.28152907 |
| 7047 | 0.0882 | -0.0071 | 0.0732 | 37.4073 | 138.8716482 | 0.269366 |
| 7047.5 | 0.085 | -0.0026 | 0.0666 | 38.5223 | 158.8923168 | 0.24244281 |
| 7048 | 0.0836 | -0.0008 | 0.0653 | 38.1394 | 165.1515218 | 0.23093581 |
| 7048.5 | 0.0874 | -0.0037 | 0.0689 | 35.0514 | 148.7970693 | 0.23556512 |
| 7049 | 0.0926 | -0.0131 | 0.0786 | 30.5133 | 122.3413013 | 0.24941128 |
| 7049.5 | 0.0946 | -0.0206 | 0.083 | 26.9674 | 113.0586546 | 0.23852575 |
| 7050 | 0.0939 | -0.0248 | 0.0831 | 25.3473 | 113.8842478 | 0.22257073 |
| 7050.5 | 0.0945 | -0.0262 | 0.0815 | 25.0428 | 115.2799938 | 0.21723457 |
| 7051 | 0.0964 | -0.0298 | 0.0843 | 25.1498 | 108.929661 | 0.2308811 |
| 7051.5 | 0.0952 | -0.0314 | 0.0873 | 25.1097 | 106.6328489 | 0.23547809 |
| 7052 | 0.0935 | -0.025 | 0.0855 | 24.6958 | 111.1660472 | 0.22215236 |
| 7052.5 | 0.0977 | -0.016 | 0.0793 | 24.3198 | 113.8842478 | 0.21354841 |
| 7053 | 0.1055 | -0.0097 | 0.0769 | 24.5519 | 106.7585796 | 0.2299759 |
| 7053.5 | 0.108 | -0.0103 | 0.0787 | 25.6405 | 101.5420429 | 0.25251117 |
| 7054 | 0.1016 | -0.0179 | 0.0814 | 27.3789 | 106.0074377 | 0.25827339 |
| 7054.5 | 0.0932 | -0.0241 | 0.0809 | 28.8837 | 118.0018517 | 0.24477328 |
| 7055 | 0.0891 | -0.0277 | 0.0803 | 29.1435 | 125.1533149 | 0.23286239 |
| 7055.5 | 0.0879 | -0.0266 | 0.0779 | 28.3657 | 131.0688379 | 0.21641834 |
| 7056 | 0.087 | -0.0117 | 0.065 | 27.2939 | 157.9946809 | 0.17275202 |
| 7056.5 | 0.0852 | -0.001 | 0.0582 | 26.1529 | 179.0711014 | 0.14604757 |
| 7057 | 0.0838 | -0.0021 | 0.0662 | 25.2996 | 162.5586086 | 0.15563371 |
| 7057.5 | 0.0862 | -0.0093 | 0.0744 | 25.3234 | 140.3632021 | 0.18041338 |
| 7058 | 0.0912 | -0.0155 | 0.0738 | 25.7102 | 132.4389412 | 0.1941287 |
| 7058.5 | 0.0971 | -0.0177 | 0.0632 | 24.316 | 140.9285901 | 0.17254128 |
| 7059 | 0.1061 | -0.0181 | 0.0573 | 21.1356 | 135.2428356 | 0.15627889 |
| 7059.5 | 0.1127 | -0.0179 | 0.0619 | 19.1547 | 117.2765187 | 0.16332937 |
| 7060 | 0.1085 | -0.0181 | 0.0755 | 19.3588 | 104.7726336 | 0.18476962 |
| 7060.5 | 0.1002 | -0.0174 | 0.0893 | 20.3947 | 98.34366052 | 0.20738195 |
| 7061 | 0.0977 | -0.014 | 0.0922 | 20.6973 | 97.89883101 | 0.21141519 |
| 7061.5 | 0.0973 | -0.0032 | 0.0833 | 19.9615 | 109.0593805 | 0.18303332 |
| 7062 | 0.0955 | 0.0034 | 0.0725 | 18.8579 | 127.4063941 | 0.14801376 |
| 7062.5 | 0.0959 | -0.0034 | 0.074 | 18.1314 | 124.3627783 | 0.14579443 |
| 7063 | 0.099 | -0.0124 | 0.0805 | 17.8437 | 110.5013557 | 0.16147947 |
| 7063.5 | 0.1039 | -0.01 | 0.0826 | 17.7058 | 101.7763056 | 0.1739678 |
| 7064 | 0.1089 | 0.0014 | 0.077 | 17.8565 | 102.4838642 | 0.17423718 |
| 7064.5 | 0.1088 | 0.005 | 0.0725 | 18.4307 | 108.1560708 | 0.17040837 |
| 7065 | 0.1043 | -0.003 | 0.0769 | 19.1102 | 108.2844424 | 0.17648149 |
| 7065.5 | 0.1016 | -0.0099 | 0.0764 | 19.4898 | 112.5131219 | 0.17322246 |
| 7066 | 0.1019 | -0.0092 | 0.0716 | 19.638 | 118.8809591 | 0.16519046 |
| 7066.5 | 0.1033 | -0.0039 | 0.065 | 20.2331 | 126.9186169 | 0.1594179 |
| 7067 | 0.1045 | 0.009 | 0.0559 | 21.7785 | 140.7397573 | 0.15474305 |
| 7067.5 | 0.1053 | 0.0195 | 0.0537 | 24.4183 | 143.417571 | 0.17026017 |
| 7068 | 0.1047 | 0.0206 | 0.0581 | 28.022 | 136.3167486 | 0.20556535 |
| 7068.5 | 0.1001 | 0.009 | 0.0661 | 31.6462 | 130.3915621 | 0.24270129 |
| 7069 | 0.0942 | -0.0063 | 0.0725 | 35.0263 | 129.5521547 | 0.27036447 |
| 7069.5 | 0.0938 | -0.0063 | 0.0672 | 38.8681 | 139.6145069 | 0.27839585 |
| 7070 | 0.0992 | 0.0035 | 0.0561 | 40.8906 | 150.8646711 | 0.27104159 |
| 7070.5 | 0.1082 | 0.0097 | 0.0477 | 38.4472 | 149.6190981 | 0.2569672 |
| 7071 | 0.1173 | 0.0084 | 0.0468 | 34.8678 | 134.0055331 | 0.26019672 |

~23,000ppm

| | | | | | | |
|---|---|---|---|---|---|---|
| 7071.5 | 0.1179 | 0.0042 | 0.0539 | 34.5445 | 121.4245177 | 0.28449361 |
| 7072 | 0.11 | 0.0032 | 0.059 | 36.8337 | 125.7910567 | 0.29281652 |
| 7072.5 | 0.1053 | 0.0038 | 0.057 | 36.5684 | 137.2212473 | 0.26649226 |
| 7073 | 0.1072 | -0.0018 | 0.0624 | 31.2446 | 124.8362192 | 0.25028473 |
| 7073.5 | 0.1125 | -0.0153 | 0.0854 | 26.2775 | 89.58756295 | 0.29331638 |
| 7074 | 0.1174 | -0.0228 | 0.0981 | 23.6799 | 74.592393 | 0.3174573 |
| 7074.5 | 0.1173 | -0.0273 | 0.0992 | 22.5872 | 73.85360405 | 0.30583748 |
| 7075 | 0.1141 | -0.0222 | 0.0865 | 22.3599 | 87.015112 | 0.25696571 |
| 7075.5 | 0.1114 | -0.0114 | 0.0731 | 22.8297 | 104.1631209 | 0.21917258 |
| 7076 | 0.1095 | -0.0029 | 0.0675 | 24.0709 | 113.8842478 | 0.21136286 |
| 7076.5 | 0.1079 | 0.0033 | 0.0615 | 26.6065 | 125.1533149 | 0.21259125 |
| 7077 | 0.1055 | 0.0088 | 0.0522 | 31.1987 | 145.9714895 | 0.21373146 |
| 7077.5 | 0.1027 | 0.0031 | 0.0497 | 38.4363 | 157.1044552 | 0.24465442 |
| 7078 | 0.1037 | -0.0033 | 0.0495 | 47.2067 | 155.345914 | 0.30388118 |
| 7078.5 | 0.108 | 0.0007 | 0.0414 | 54.9365 | 163.965469 | 0.3350492 |
| 7079 | 0.1085 | 0.0036 | 0.0238 | 64.1608 | 212.9376786 | 0.30131257 |
| 7079.5 | 0.1046 | 0.0028 | 0.0118 | 80.1751 | 280.4188943 | 0.2859119 |
| 7080 | 0.1007 | -0.0011 | 0.012 | 90.0292 | 300.5867001 | 0.29951159 |
| 7080.5 | 0.0975 | -0.0019 | 0.0184 | 73.0745 | 283.0262993 | 0.25818979 |
| 7081 | 0.0888 | 0.0002 | 0.0153 | 53.8109 | 356.5226383 | 0.15093263 |
| 7081.5 | 0.0717 | 0.0076 | 0.0035 | 51.0599 | 717.3611003 | 0.0711774 |
| 7082 | 0.0541 | 0.01 | 0.0038 | 70.6529 | 1258.482753 | 0.05614133 |
| 7082.5 | 0.0441 | 0.0024 | 0.0141 | 128.549 | 1244.576978 | 0.1032873 |
| 7083 | 0.0428 | -0.0129 | 0.0271 | 176.8989 | 839.4218165 | 0.21073898 |
| 7083.5 | 0.046 | -0.0175 | 0.0281 | 156.0528 | 740.4522089 | 0.21075337 |
| 7084 | 0.048 | -0.0138 | 0.0237 | 130.7213 | 794.7673098 | 0.16447745 |
| 7084.5 | 0.047 | -0.0118 | 0.0223 | 122.462 | 855.1252409 | 0.14320943 |
| 7085 | 0.0448 | -0.016 | 0.0269 | 109.6777 | 794.7673098 | 0.13799976 |
| 7085.5 | 0.0415 | -0.0195 | 0.0272 | 102.5149 | 871.2628481 | 0.11766243 |
| 7086 | 0.036 | -0.0121 | 0.0167 | 134.5428 | 1540.683237 | 0.08732671 |
| 7086.5 | 0.0315 | -0.0027 | 0.0091 | 274.0695 | 2699.449504 | 0.10152792 |
| 7087 | 0.034 | 0.001 | 0.0081 | 397.199 | 2496.891518 | 0.1590774 |
| 7087.5 | 0.0464 | -0.0075 | 0.0164 | 363.7737 | 1056.800344 | 0.34422178 |
| 7088 | 0.0643 | -0.0174 | 0.0197 | 232.7769 | 565.4649819 | 0.41165573 |
| 7088.5 | 0.0781 | -0.0199 | 0.0184 | 138.9295 | 419.6357274 | 0.33107167 |
| 7089 | 0.0865 | -0.0215 | 0.0175 | 113.9929 | 357.2600878 | 0.31907538 |
| 7089.5 | 0.095 | -0.0206 | 0.0145 | 107.4281 | 319.7906958 | 0.33593254 |
| 7090 | 0.1036 | -0.0127 | 0.0011 | 103.3066 | 352.1444228 | 0.29336429 |
| 7090.5 | 0.1049 | -0.0002 | -0.0132 | 95.902 | 468.2870074 | 0.20479321 |
| 7091 | 0.0971 | 0.0015 | -0.0129 | 89.6227 | 562.581159 | 0.15930626 |
| 7091.5 | 0.0896 | -0.0124 | 0.0026 | 93.9151 | 462.8440658 | 0.20290873 |
| 7092 | 0.0872 | -0.022 | 0.0137 | 106.2824 | 381.276618 | 0.27875405 |
| 7092.5 | 0.0858 | -0.0138 | 0.0128 | 101.9579 | 400.6552271 | 0.2544779 |
| 7093 | 0.0817 | 0.0086 | 0.0096 | 80.5791 | 472.7091496 | 0.17046232 |
| 7093.5 | 0.0752 | 0.0207 | 0.0175 | 66.2033 | 457.4933143 | 0.14470878 |
| 7094 | 0.072 | 0.0277 | 0.0185 | 61.2338 | 481.7389202 | 0.12710993 |
| 7094.5 | 0.0759 | 0.025 | 0.0184 | 63.5008 | 440.96695 | 0.14400354 |
| 7095 | 0.081 | 0.0225 | 0.0225 | 67.6907 | 360.9810702 | 0.1875187 |
| 7095.5 | 0.0797 | 0.0127 | 0.0343 | 65.8084 | 293.2653478 | 0.22439883 |
| 7096 | 0.0769 | 0.01 | 0.0394 | 59.2413 | 280.9375518 | 0.21086999 |
| 7096.5 | 0.0771 | 0.0077 | 0.0365 | 55.0917 | 295.4899862 | 0.18644185 |
| 7097 | 0.0755 | 0.0001 | 0.0364 | 57.9723 | 305.2259781 | 0.18993239 |

0.21 to 0.31

0.13 to 0.28

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|---|---|---|---|---|---|---|
| 7097.5 | 0.0738 | -0.0065 | 0.0402 | 69.9504 | 293.2653478 | 0.23852255 |
| 7098 | 0.083 | -0.0035 | 0.0422 | 70.4665 | 239.7490379 | 0.29391776 |
| 7098.5 | 0.11 | 0.007 | 0.0351 | 40.1374 | 174.5907552 | 0.22989419 |
| 7099 | 0.1514 | 0.0147 | 0.0215 | 23.3081 | 119.7696953 | 0.19460766 |
| 7099.5 | 0.1878 | 0.0183 | 0.0097 | 18.7515 | 89.9781201 | 0.20840066 |
| 7100 | 0.1947 | 0.0212 | -0.0006 | 19.6754 | 93.40094689 | 0.21065525 |
| 7100.5 | 0.1728 | 0.0131 | -0.0046 | 24.2043 | 127.0809049 | 0.19046371 |
| 7101 | 0.1435 | -0.004 | -0.0024 | 33.2638 | 185.4057081 | 0.17941087 |
| 7101.5 | 0.1245 | -0.0133 | 0.0012 | 48.7912 | 237.7033668 | 0.20526087 |
| 7102 | 0.1162 | -0.0072 | -0.0006 | 72.5165 | 284.6078253 | 0.25479447 |
| 7102.5 | 0.1116 | -0.0001 | -0.0069 | 104.7093 | 352.1444228 | 0.2973476 |
| 7103 | 0.1123 | -0.0008 | -0.0105 | 124.8419 | 374.0661911 | 0.33374281 |
| 7103.5 | 0.1202 | -0.01 | -0.0081 | 105.231 | 304.0563747 | 0.34609043 |
| 7104 | 0.129 | -0.0198 | -0.0023 | 76.1634 | 233.688025 | 0.32591914 |
| 7104.5 | 0.1314 | -0.0201 | 0.0013 | 61.8441 | 211.5600671 | 0.29232407 |
| 7105 | 0.1207 | -0.0225 | 0.0145 | 62.0633 | 203.2386461 | 0.30537155 |
| 7105.5 | 0.0967 | -0.0176 | 0.032 | 77.3824 | 225.9499785 | 0.3424758 |
| 7106 | 0.0754 | -0.0049 | 0.0335 | 113.6673 | 323.5908544 | 0.35126858 |
| 7106.5 | 0.0663 | 0.0095 | 0.0227 | 165.1817 | 499.3645011 | 0.33078383 |
| 7107 | 0.0627 | 0.0102 | 0.0166 | 218.8062 | 639.9835741 | 0.34189346 |
| 7107.5 | 0.0605 | 0.0066 | 0.0145 | 221.6911 | 721.4802779 | 0.30727257 |
| 7108 | 0.0641 | 0.0127 | 0.0068 | 191.5564 | 814.1731472 | 0.23527723 |
| 7108.5 | 0.0805 | 0.0265 | -0.0047 | 133.1466 | 705.2082561 | 0.18880465 |
| 7109 | 0.1091 | 0.0284 | -0.0084 | 65.0799 | 382.9065703 | 0.16996287 |
| 7109.5 | 0.1411 | 0.0222 | -0.0099 | 37.8346 | 216.7945872 | 0.17451819 |
| 7110 | 0.1695 | 0.0096 | -0.007 | 29.0038 | 136.8583957 | 0.21192562 |
| 7110.5 | 0.1923 | -0.0049 | 0.0036 | 28.353 | 91.56555725 | 0.309647 |
| 7111 | 0.2059 | -0.0183 | 0.0148 | 30.8941 | 70.8648976 | 0.43595773 |
| 7111.5 | 0.2072 | -0.0212 | 0.0172 | 32.2942 | 68.3765284 | 0.4722995 |
| 7112 | 0.2025 | -0.0161 | 0.0112 | 31.828 | 75.94976904 | 0.41906645 |
| 7112.5 | 0.1883 | -0.0054 | 0.0026 | 32.1712 | 96.79957134 | 0.33234858 |
| 7113 | 0.161 | -0.0027 | 0.0068 | 37.2906 | 127.7331063 | 0.29194154 |
| 7113.5 | 0.1362 | 0.0076 | 0.0485 | 55.8419 | 103.9207698 | 0.53735072 |
| 7114 | 0.1241 | 0.0477 | 0.153 | 94.4567 | 43.44478474 | 2.17417811 |
| 7114.5 | 0.1261 | 0.1234 | 0.2921 | 89.6358 | 17.93207386 | 4.99862987 |
| 7115 | 0.1455 | 0.2099 | 0.3745 | 61.7562 | 11.22532675 | 5.50150578 |
| 7115.5 | 0.1762 | 0.2664 | 0.3936 | 47.1115 | 9.22152873 | 5.10886008 |
| 7116 | 0.2129 | 0.291 | 0.3853 | 21.4155 | 8.305894328 | 2.57834968 |
| 7116.5 | 0.2485 | 0.2864 | 0.378 | 14.7411 | 7.520139003 | 1.96021643 |
| 7117 | 0.2611 | 0.262 | 0.3365 | 13.8862 | 8.32383407 | 1.66824565 |
| 7117.5 | 0.2465 | 0.2167 | 0.2351 | 16.4082 | 13.23824005 | 1.23945479 |
| 7118 | 0.2105 | 0.1398 | 0.1156 | 24.6617 | 30.61272307 | 0.80560295 |
| 7118.5 | 0.1617 | 0.0601 | 0.0397 | 47.5162 | 86.27368091 | 0.55076125 |
| 7119 | 0.1271 | 0.0145 | 0.0144 | 68.5213 | 184.280692 | 0.37183114 |
| 7119.5 | 0.1182 | 0.0112 | 0.0049 | 106.4612 | 248.6287614 | 0.42819342 |
| 7120 | 0.121 | 0.0092 | 0.0039 | 137.1593 | 240.9888436 | 0.56915207 |
| 7120.5 | 0.1253 | 0.0124 | 0.0152 | 118.6428 | 187.1121905 | 0.63407306 |
| 7121 | 0.1319 | 0.039 | 0.0298 | 72.165 | 138.3182983 | 0.5217314 |
| 7121.5 | 0.1437 | 0.0795 | 0.0241 | 40.4943 | 127.7331063 | 0.31702275 |
| 7122 | 0.1527 | 0.0838 | 0.0135 | 31.9581 | 130.3915621 | 0.24509331 |
| 7122.5 | 0.142 | 0.0471 | 0.0046 | 40.8485 | 170.7725817 | 0.23919823 |
| 7123 | 0.1154 | 0.0111 | -0.0057 | 85.7238 | 318.5385002 | 0.26911598 |

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|---|---|---|---|---|---|---|
| 7123.5 | 0.0947 | -0.009 | -0.0126 | 194.0869 | 593.9753093 | 0.32675921 |
| 7124 | 0.0863 | -0.0188 | -0.01 | 313.2617 | 695.3099169 | 0.45053535 |
| 7124.5 | 0.0808 | -0.0164 | -0.0041 | 330.1851 | 687.5371154 | 0.48024331 |
| 7125 | 0.0752 | -0.0064 | -0.0015 | 279.5919 | 749.119464 | 0.37322739 |
| 7125.5 | 0.0758 | 0.0053 | -0.0031 | 217.6305 | 771.4489581 | 0.28210616 |
| 7126 | 0.084 | 0.0083 | -0.0006 | 159.6645 | 574.2475769 | 0.27804123 |
| 7126.5 | 0.0922 | 0.0175 | -0.0062 | 109.8057 | 537.5693635 | 0.20426331 |
| 7127 | 0.0935 | 0.0257 | -0.0143 | 83.2611 | 641.7221646 | 0.12974634 |
| 7127.5 | 0.0897 | 0.0211 | -0.0141 | 73.8997 | 709.2254636 | 0.10419775 |
| 7128 | 0.0832 | 0.005 | -0.0006 | 79.1703 | 586.2718993 | 0.13504024 |
| 7128.5 | 0.073 | -0.0159 | 0.0196 | 104.079 | 458.5561884 | 0.22697109 |
| 7129 | 0.0644 | -0.0278 | 0.0275 | 147.4607 | 466.0986346 | 0.31637231 |
| 7129.5 | 0.0666 | -0.0231 | 0.0231 | 152.3581 | 491.0236696 | 0.31028667 |
| 7130 | 0.0826 | -0.007 | 0.0138 | 103.4562 | 420.5721952 | 0.24598916 |
| 7130.5 | 0.1061 | 0.0026 | 0.0107 | 57.1102 | 278.3582312 | 0.20516799 |
| 7131 | 0.128 | 0.0052 | 0.0096 | 38.9531 | 195.693566 | 0.19905151 |
| 7131.5 | 0.1378 | 0.0101 | 0.0041 | 34.6541 | 183.1656494 | 0.18919541 |
| 7132 | 0.1292 | 0.0227 | -0.0031 | 37.4988 | 236.0851901 | 0.15883588 |
| 7132.5 | 0.114 | 0.0321 | -0.0075 | 47.1121 | 339.4724412 | 0.13878034 |
| 7133 | 0.1031 | 0.0247 | -0.0036 | 65.7472 | 392.9040962 | 0.16733651 |
| 7133.5 | 0.0954 | 0.0146 | -0.005 | 87.7231 | 482.8853777 | 0.18166444 |
| 7134 | 0.0899 | 0.0058 | -0.0055 | 105.7159 | 559.718833 | 0.18887322 |
| 7134.5 | 0.0867 | 0.0017 | -0.0033 | 127.8342 | 574.2475769 | 0.22261165 |
| 7135 | 0.0827 | 0.0076 | -0.0054 | 150.3538 | 676.1145285 | 0.22237919 |
| 7135.5 | 0.075 | 0.0191 | -0.0103 | 168.7613 | 991.2015597 | 0.17025932 |
| 7136 | 0.0662 | 0.0232 | -0.0055 | 188.7524 | 1136.973898 | 0.16601296 |
| 7136.5 | 0.0586 | 0.0173 | 0.0043 | 172.9898 | 1053.191372 | 0.16425296 |
| 7137 | 0.0555 | 0.013 | 0.0116 | 134.2405 | 916.5428247 | 0.14646397 |
| 7137.5 | 0.0605 | 0.0135 | 0.0129 | 107.33 | 755.7177996 | 0.14202391 |
| 7138 | 0.0682 | 0.0168 | 0.0134 | 103.9407 | 601.82793 | 0.17270834 |
| 7138.5 | 0.0708 | 0.0185 | 0.0158 | 111.7964 | 529.5935807 | 0.21109848 |
| 7139 | 0.0682 | 0.0191 | 0.0233 | 115.5147 | 470.4904667 | 0.24551975 |
| 7139.5 | 0.0648 | 0.0167 | 0.0319 | 97.0244 | 417.7719343 | 0.2322425 |
| 7140 | 0.0607 | 0.0117 | 0.0365 | 67.1629 | 413.165177 | 0.16255702 |
| 7140.5 | 0.0565 | 0.0135 | 0.0356 | 49.1167 | 463.9252124 | 0.10587202 |
| 7141 | 0.0559 | 0.0106 | 0.0419 | 42.0249 | 407.7346709 | 0.10306923 |
| 7141.5 | 0.0573 | 0.0049 | 0.0489 | 41.4471 | 341.5375582 | 0.12135444 |
| 7142 | 0.0571 | -0.0091 | 0.0586 | 44.0664 | 284.0792145 | 0.15512011 |
| 7142.5 | 0.0573 | -0.0143 | 0.0566 | 47.4441 | 293.819201 | 0.16147379 |
| 7143 | 0.0613 | -0.0096 | 0.0418 | 50.3806 | 363.9988821 | 0.13840867 |
| 7143.5 | 0.0656 | 0.0013 | 0.0273 | 51.7246 | 455.3783667 | 0.11358598 |
| 7144 | 0.0713 | 0.0099 | 0.0223 | 50.5019 | 448.0877853 | 0.11270537 |
| 7144.5 | 0.0812 | 0.0085 | 0.0262 | 49.0903 | 333.3857059 | 0.14724776 |
| 7145 | 0.0883 | 0.0153 | 0.0213 | 49.5093 | 319.1636983 | 0.15512196 |
| 7145.5 | 0.0907 | 0.0244 | 0.0193 | 49.5142 | 316.6736349 | 0.15635719 |
| 7146 | 0.0902 | 0.0231 | 0.0277 | 47.5323 | 272.8044807 | 0.17423577 |
| 7146.5 | 0.0858 | 0.0141 | 0.0397 | 46.439 | 238.518555 | 0.19469764 |
| 7147 | 0.0803 | 0.0053 | 0.046 | 46.8081 | 235.282148 | 0.19894455 |
| 7147.5 | 0.0777 | 0.0035 | 0.0425 | 45.5026 | 261.7047316 | 0.17386999 |
| 7148 | 0.0779 | 0.0086 | 0.04 | 41.7838 | 272.8044807 | 0.15316391 |
| 7148.5 | 0.0772 | 0.0055 | 0.0462 | 38.2987 | 247.331019 | 0.15484794 |
| 7149 | 0.0739 | 0.0025 | 0.0514 | 36.7372 | 239.3378457 | 0.15349516 |

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|---|---|---|---|---|---|---|
| 7149.5 | 0.0708 | 0.0013 | 0.0472 | 37.4006 | 272.3076639 | 0.13734685 |
| 7150 | 0.07 | 0.0017 | 0.0424 | 38.3088 | 302.3142446 | 0.12671847 |
| 7150.5 | 0.0711 | -0.0066 | 0.0485 | 37.1743 | 264.5356111 | 0.14052664 |
| 7151 | 0.0745 | -0.0029 | 0.0494 | 35.4684 | 245.1900665 | 0.14465676 |
| 7151.5 | 0.0799 | -0.001 | 0.0475 | 36.7696 | 230.936144 | 0.15921977 |
| 7152 | 0.0818 | 0.0016 | 0.0406 | 43.2257 | 251.6958946 | 0.1717378 |
| 7152.5 | 0.0814 | 0.0069 | 0.0347 | 53.2273 | 281.979092 | 0.18876329 |
| 7153 | 0.0872 | 0.0113 | 0.0325 | 57.0116 | 264.0606918 | 0.2159034 |
| 7153.5 | 0.0969 | 0.0093 | 0.0298 | 46.3726 | 233.688025 | 0.19843807 |
| 7154 | 0.1041 | 0.0023 | 0.0282 | 34.0543 | 212.9376786 | 0.15992614 |
| 7154.5 | 0.1041 | -0.0007 | 0.0233 | 30.7946 | 230.936144 | 0.13334682 |
| 7155 | 0.0916 | 0.0095 | 0.0152 | 38.3378 | 337.4255674 | 0.11361854 |
| 7155.5 | 0.0711 | 0.0131 | 0.0131 | 66.8747 | 562.581159 | 0.1188712 |
| 7156 | 0.0569 | 0.0057 | 0.0175 | 159.8692 | 734.0478463 | 0.21779125 |
| 7156.5 | 0.0613 | -0.0014 | 0.0245 | 493.3684 | 540.2670871 | 0.91319351 |
| 7157 | 0.0928 | 0.0033 | 0.0232 | 439.0932 | 282.5019847 | 1.55430129 |
| 7157.5 | 0.1478 | 0.0033 | 0.028 | 113.6596 | 115.5621486 | 0.98353658 |
| 7158 | 0.1946 | -0.0054 | 0.0294 | 45.6363 | 68.639315 | 0.66487115 |
| 7158.5 | 0.2129 | -0.0176 | 0.0317 | 28.5063 | 56.8100023 | 0.50178312 |
| 7159 | 0.2121 | -0.0206 | 0.0243 | 23.2508 | 61.13136805 | 0.38034156 |
| 7159.5 | 0.1999 | -0.0229 | 0.0206 | 21.1213 | 71.00316426 | 0.29746984 |
| 7160 | 0.1821 | -0.0263 | 0.0219 | 20.6616 | 83.92692673 | 0.24618559 |
| 7160.5 | 0.1645 | -0.03 | 0.0249 | 23.2033 | 98.45533056 | 0.23567337 |
| 7161 | 0.1446 | -0.0302 | 0.0241 | 30.9556 | 126.2724924 | 0.2451492 |
| 7161.5 | 0.1217 | -0.0241 | 0.0191 | 45.9815 | 186.256086 | 0.24687247 |
| 7162 | 0.1039 | -0.0158 | 0.014 | 70.0512 | 272.8044807 | 0.25678171 |
| 7162.5 | 0.0922 | -0.0062 | 0.0121 | 111.5948 | 355.0544148 | 0.31430337 |
| 7163 | 0.0828 | 0 | 0.0133 | 198.4538 | 423.4000419 | 0.46871464 |
| 7163.5 | 0.0793 | 0.0056 | 0.0134 | 376.1087 | 457.4933143 | 0.82210753 |
| 7164 | 0.0836 | 0.0105 | 0.0073 | 124.0707 | 477.1927439 | 0.26000123 |
| 7164.5 | 0.1012 | 0.0094 | 0.0079 | 81.9438 | 322.3168176 | 0.25423371 |
| 7165 | 0.1398 | 0.0182 | 0.0152 | 53.5176 | 151.4931616 | 0.35326743 |
| 7165.5 | 0.1919 | 0.0587 | 0.031 | 37.2317 | 69.36965473 | 0.53671451 |
| 7166 | 0.2405 | 0.1173 | 0.0435 | 21.3311 | 41.2070713 | 0.5176563 |
| 7166.5 | 0.2712 | 0.1319 | 0.0474 | 14.7413 | 32.18309235 | 0.45804486 |
| 7167 | 0.2805 | 0.0784 | 0.0486 | 14.4833 | 30.01589056 | 0.48252108 |
| 7167.5 | 0.2726 | 0.0237 | 0.0319 | 18.935 | 35.47263839 | 0.5337917 |
| 7168 | 0.2466 | -0.0009 | 0.0182 | 24.4227 | 47.89967001 | 0.50987199 |
| 7168.5 | 0.1877 | 0.0045 | 0.0066 | 30.336 | 93.19436615 | 0.32551324 |
| 7169 | 0.1149 | 0.0076 | 0.0089 | 46.9028 | 245.616079 | 0.19095981 |
| 7169.5 | 0.0829 | 0.0118 | 0.017 | 82.5554 | 389.5295243 | 0.21193618 |
| 7170 | 0.0858 | 0.0064 | 0.029 | 130.2243 | 288.8890767 | 0.45077613 |
| 7170.5 | 0.0887 | -0.0033 | 0.0356 | 157.5297 | 243.4967974 | 0.64694773 |
| 7171 | 0.0896 | -0.0092 | 0.0415 | 199.7337 | 217.1502797 | 0.91979481 |
| 7171.5 | 0.0956 | -0.0071 | 0.0486 | 185.5934 | 176.9419749 | 1.04889414 |
| 7172 | 0.1196 | 0.0228 | 0.0653 | 86.5407 | 103.6792439 | 0.83469648 |
| 7172.5 | 0.1609 | 0.0916 | 0.1034 | 344.3763 | 48.09470657 | 7.16037844 |
| 7173 | 0.1944 | 0.1624 | 0.152 | 18.191 | 26.88522844 | 0.6766169 |
| 7173.5 | 0.21 | 0.1656 | 0.183 | 9.8765 | 20.49567363 | 0.48188219 |
| 7174 | 0.2289 | 0.1029 | 0.1603 | 10.2166 | 20.92833085 | 0.4881708 |
| 7174.5 | 0.2404 | 0.0411 | 0.1064 | 16.195 | 26.81860225 | 0.60387189 |
| 7175 | 0.2109 | 0.0219 | 0.0626 | 24.5748 | 44.6835757 | 0.54997389 |

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|---|---|---|---|---|---|---|
| 7175.5 | 0.1859 | 0.03 | 0.0514 | 27.553 | 60.63397537 | 0.4544152 |
| 7176 | 0.201 | 0.0617 | 0.0593 | 27.5328 | 49.69774905 | 0.55400497 |
| 7176.5 | 0.2131 | 0.1102 | 0.0555 | 21.9419 | 46.45455051 | 0.47233048 |
| 7177 | 0.208 | 0.1386 | 0.0338 | 17.7342 | 58.23380162 | 0.30453447 |
| 7177.5 | 0.2002 | 0.1158 | 0.0191 | 17.2383 | 71.84112459 | 0.23995031 |
| 7178 | 0.1904 | 0.0861 | 0.0192 | 18.7093 | 79.17989688 | 0.23628851 |
| 7178.5 | 0.1801 | 0.0896 | 0.0239 | 20.4463 | 83.92692673 | 0.24362026 |
| 7179 | 0.1772 | 0.1173 | 0.0214 | 21.055 | 88.91003992 | 0.2368124 |
| 7179.5 | 0.1847 | 0.1494 | 0.012 | 21.0315 | 90.76675439 | 0.23170929 |
| 7180 | 0.1925 | 0.1876 | 0.0109 | 20.691 | 84.46010961 | 0.24497955 |
| 7180.5 | 0.1939 | 0.2219 | 0.0302 | 19.3706 | 68.57347981 | 0.28247947 |
| 7181 | 0.1915 | 0.2188 | 0.0635 | 18.0441 | 51.94512459 | 0.3473685 |
| 7181.5 | 0.1852 | 0.1704 | 0.0719 | 18.091 | 51.03718534 | 0.35446704 |
| 7182 | 0.1727 | 0.0913 | 0.0617 | 20.2803 | 62.25830954 | 0.32574447 |
| 7182.5 | 0.1464 | 0.0281 | 0.0408 | 27.3624 | 100.959831 | 0.27102264 |
| 7183 | 0.1008 | -0.0001 | 0.023 | 49.1604 | 245.616079 | 0.20015139 |
| 7183.5 | 0.0548 | 0.007 | 0.0034 | 114.3839 | 1244.576978 | 0.09190585 |
| 7184 | 0.03 | 0.014 | -0.0041 | 245.9163 | 7095.968638 | 0.03465578 |
| 7184.5 | 0.0205 | 0.0083 | 0.0035 | 262.7549 | 8358.955448 | 0.03143394 |
| 7185 | 0.0153 | -0.0047 | 0.0188 | 210.7146 | 3928.115647 | 0.05364267 |
| 7185.5 | 0.0142 | -0.0123 | 0.0267 | 213.535 | 2657.058204 | 0.08036519 |
| 7186 | 0.0166 | -0.0109 | 0.0224 | 201.5595 | 2943.183059 | 0.06848351 |
| 7186.5 | 0.0204 | -0.0134 | 0.0186 | 172.7523 | 2943.183059 | 0.05869574 |
| 7187 | 0.0245 | -0.0152 | 0.0214 | 140.3676 | 2073.523235 | 0.06769521 |
| 7187.5 | 0.0256 | -0.0078 | 0.0212 | 121.4727 | 1988.73811 | 0.06108029 |
| 7188 | 0.0229 | 0.0145 | 0.007 | 143.9004 | 5210.904636 | 0.02761524 |
| 7188.5 | 0.021 | 0.0322 | 0.0067 | 243.4014 | 6141.503118 | 0.03963222 |
| 7189 | 0.0229 | 0.105 | 0.0031 | 281.9884 | 7037.42018 | 0.04006985 |
| 7189.5 | 0.0329 | 0.3411 | -0.0728 | 152.0403 | #NUM! | #NUM! |
| 7190 | 0.0631 | 0.6368 | -0.181 | 64.4646 | #NUM! | #NUM! |
| 7190.5 | 0.1124 | 0.7082 | -0.1646 | 32.4485 | #NUM! | #NUM! |
| 7191 | 0.1584 | 0.4801 | -0.0237 | 17.3035 | 204.8640949 | 0.08446331 |
| 7191.5 | 0.1766 | 0.2117 | 0.0554 | 19.797 | 63.65126111 | 0.3110229 |
| 7192 | 0.1627 | 0.0683 | 0.0386 | 36.1023 | 86.36585249 | 0.41801591 |
| 7192.5 | 0.1371 | 0.0265 | 0.002 | 53.8956 | 191.1845753 | 0.2819035 |
| 7193 | 0.118 | 0.0058 | 0.0014 | 58.668 | 265.4892114 | 0.22098073 |
| 7193.5 | 0.1056 | -0.0068 | 0.0095 | 66.6432 | 287.2726194 | 0.23198591 |
| 7194 | 0.0974 | -0.0033 | 0.0061 | 87.9886 | 360.9810702 | 0.24374852 |
| 7194.5 | 0.1013 | 0.0047 | 0.0178 | 143.1421 | 266.9290821 | 0.53625517 |
| 7195 | 0.1194 | 0.009 | 0.1135 | 250.7588 | 63.12360301 | 3.97250455 |
| 7195.5 | 0.1415 | 0.017 | 0.327 | 258.4362 | 14.04690193 | 18.3980924 |
| 7196 | 0.1656 | 0.0531 | 0.5413 | 85.7643 | 5.800781668 | 14.7849557 |
| 7196.5 | 0.201 | 0.1032 | 0.6471 | 29.2355 | 3.921434761 | 7.45530699 |
| 7197 | 0.2752 | 0.1552 | 0.6289 | 15.3586 | 3.417753772 | 4.49377018 |
| 7197.5 | 0.3639 | 0.216 | 0.5222 | 6.5277 | 3.56876784 | 1.8291187 |
| 7198 | 0.37 | 0.2869 | 0.3576 | 6.817 | 5.451762096 | 1.2504214 |
| 7198.5 | 0.3032 | 0.3325 | 0.2017 | 13.4417 | 11.95954434 | 1.12393078 |
| 7199 | 0.2588 | 0.3453 | 0.1093 | 23.9502 | 23.59281013 | 1.01514825 |
| 7199.5 | 0.2481 | 0.3327 | 0.0857 | 44.07 | 29.11458243 | 1.51367447 |
| 7200 | 0.2404 | 0.3291 | 0.0837 | 46.6416 | 31.02031928 | 1.5035822 |
| 7200.5 | 0.2333 | 0.327 | 0.0752 | 30.9029 | 34.49114153 | 0.89596629 |
| 7201 | 0.2293 | 0.2851 | 0.0928 | 23.3881 | 31.43591616 | 0.74399295 |

0.03 to 0.20

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|---|---|---|---|---|---|---|
| 7201.5 | 0.2245 | 0.2311 | 0.1252 | 21.9175 | 26.34271727 | 0.83201364 |
| 7202 | 0.2092 | 0.1954 | 0.128 | 24.252 | 28.48707857 | 0.85133335 |
| 7202.5 | 0.178 | 0.1574 | 0.0739 | 34.137 | 53.32926769 | 0.64011755 |
| 7203 | 0.1524 | 0.0941 | 0.0371 | 54.8499 | 98.34366052 | 0.55773702 |
| 7203.5 | 0.1493 | 0.0745 | 0.0699 | 45.2918 | 71.91160768 | 0.629826 |
| 7204 | 0.1609 | 0.1437 | 0.1285 | 27.9602 | 39.57166716 | 0.70657119 |
| 7204.5 | 0.1809 | 0.2095 | 0.17 | 22.8814 | 26.14941265 | 0.87502539 |
| 7205 | 0.2038 | 0.1905 | 0.175 | 23.1047 | 22.18322805 | 1.04153913 |
| 7205.5 | 0.2187 | 0.1279 | 0.1623 | 22.2838 | 21.90874409 | 1.01711901 |
| 7206 | 0.2197 | 0.109 | 0.1447 | 19.8149 | 24.11085928 | 0.82182471 |
| 7206.5 | 0.2089 | 0.1275 | 0.1169 | 18.8669 | 30.67336046 | 0.61509074 |
| 7207 | 0.1969 | 0.1191 | 0.0661 | 20.4598 | 48.60728019 | 0.42092049 |
| 7207.5 | 0.1929 | 0.064 | 0.0397 | 23.857 | 63.29877463 | 0.37689513 |
| 7208 | 0.1951 | 0.036 | 0.0419 | 25.6164 | 60.799112 | 0.42132852 |
| 7208.5 | 0.1979 | 0.0664 | 0.0634 | 21.6105 | 49.28973114 | 0.43843818 |
| 7209 | 0.1943 | 0.1139 | 0.0715 | 16.418 | 47.51305772 | 0.34554711 |
| 7209.5 | 0.1764 | 0.1075 | 0.0649 | 15.3149 | 58.49354439 | 0.26182206 |
| 7210 | 0.1427 | 0.0604 | 0.0395 | 19.1528 | 107.0106936 | 0.17898024 |
| 7210.5 | 0.1037 | 0.0212 | 0.0152 | 29.976 | 267.8953607 | 0.11189443 |
| 7211 | 0.0731 | 0.0095 | 0.0103 | 49.7765 | 574.2475769 | 0.08668125 |
| 7211.5 | 0.055 | 0.002 | 0.0258 | 96.5376 | 614.7120896 | 0.15704523 |
| 7212 | 0.0437 | -0.0065 | 0.042 | 276.007 | 541.6233924 | 0.5095921 |
| 7212.5 | 0.0368 | -0.0113 | 0.0521 | 383.1905 | 500.5729692 | 0.76550378 |
| 7213 | 0.0352 | -0.0105 | 0.0547 | 1263.698 | 488.6780621 | 2.58595218 |
| 7213.5 | 0.037 | -0.0061 | 0.0539 | 5752.613 | 477.1927439 | 12.0551137 |
| 7214 | 0.0396 | -0.0004 | 0.0543 | 20000 | 445.0155194 | 44.9422529 |
| 7214.5 | 0.0416 | -0.0063 | 0.0627 | 20000 | 355.0544148 | 56.3293939 |
| 7215 | 0.0423 | -0.0146 | 0.0641 | 20000 | 340.158776 | 58.7960723 |
| 7215.5 | 0.0418 | -0.0194 | 0.0617 | 20000 | 360.9810702 | 55.4045673 |
| 7216 | 0.0402 | -0.0148 | 0.0562 | 14936.72 | 420.5721952 | 35.5152289 |
| 7216.5 | 0.0382 | -0.0119 | 0.0556 | 1515.39 | 446.0361697 | 3.39745878 |
| 7217 | 0.0371 | -0.0092 | 0.0574 | 232.0387 | 438.9628753 | 0.52860666 |
| 7217.5 | 0.0438 | -0.005 | 0.077 | 53.1883 | 258.9180166 | 0.20542526 |
| 7218 | 0.0783 | 0.0058 | 0.1517 | 17.8203 | 64.84721554 | 0.2748044 |
| 7218.5 | 0.1592 | 0.0232 | 0.3126 | 10.0843 | 13.83651176 | 0.72881808 |
| 7219 | 0.2618 | 0.0361 | 0.4531 | 4.1542 | 5.662116377 | 0.73368326 |
| 7219.5 | 0.2996 | 0.0298 | 0.4359 | 3.5515 | 5.326640962 | 0.66674289 |
| 7220 | 0.2346 | 0.0131 | 0.2667 | 4.1875 | 12.14496074 | 0.34479321 |
| 7220.5 | 0.147 | -0.0098 | 0.1115 | 6.9457 | 50.44475339 | 0.13768924 |
| 7221 | 0.1002 | -0.0171 | 0.0464 | 13.2606 | 170.7725817 | 0.07765064 |
| 7221.5 | 0.082 | -0.0172 | 0.0371 | 32.8204 | 266.9290821 | 0.1229555 |
| 7222 | 0.0728 | -0.0156 | 0.0419 | 114.2876 | 289.4308578 | 0.39487013 |
| 7222.5 | 0.067 | -0.0147 | 0.0447 | 580.459 | 306.402185 | 1.89443492 |
| 7223 | 0.0621 | -0.0099 | 0.0385 | 4415.646 | 383.7253772 | 11.5073064 |
| 7223.5 | 0.0553 | -0.0014 | 0.0302 | 20000 | 544.3510106 | 36.7409991 |
| 7224 | 0.0472 | 0.002 | 0.0309 | 20000 | 661.3120822 | 30.2429073 |
| 7224.5 | 0.0408 | 0.0014 | 0.0331 | 20000 | 744.7673643 | 26.8540231 |
| 7225 | 0.0385 | -0.0075 | 0.0355 | 11107.26 | 742.6051945 | 14.9571559 |
| 7225.5 | 0.0415 | -0.0227 | 0.0475 | 1863.712 | 499.3645011 | 3.73216758 |
| 7226 | 0.0479 | -0.0172 | 0.0743 | 460.1769 | 252.5824011 | 1.82188822 |
| 7226.5 | 0.0528 | 0.0442 | 0.0847 | 161.7439 | 195.9996876 | 0.82522529 |
| 7227 | 0.0534 | 0.1256 | 0.0768 | 83.3936 | 220.3903447 | 0.37839044 |

0.21 to 58.4

0.12 to 36.74

| | | | | | | |
|---|---|---|---|---|---|---|
| 7227.5 | 0.0561 | 0.153 | 0.0615 | 44.6349 | 274.3029248 | 0.1627212 |
| 7228 | 0.0709 | 0.1065 | 0.0483 | 31.6089 | 266.4478567 | 0.11863072 |
| 7228.5 | 0.0946 | 0.0511 | 0.0366 | 25.2829 | 216.7945872 | 0.11662145 |
| 7229 | 0.1065 | 0.0254 | 0.0289 | 21.7976 | 202.593754 | 0.10759266 |
| 7229.5 | 0.0964 | 0.0222 | 0.0312 | 21.3086 | 230.1586122 | 0.09258224 |
| 7230 | 0.0808 | 0.0261 | 0.0338 | 26.8014 | 289.9741288 | 0.09242687 |
| 7230.5 | 0.0716 | 0.0197 | 0.0303 | 49.462 | 373.2773898 | 0.13250736 |
| 7231 | 0.0618 | -0.0007 | 0.0317 | 66.1859 | 449.1187813 | 0.14736836 |
| 7231.5 | 0.0517 | -0.0217 | 0.0324 | 89.7581 | 564.0203701 | 0.15913982 |
| 7232 | 0.051 | -0.0308 | 0.0354 | 98.405 | 532.2327981 | 0.1848909 |
| 7232.5 | 0.0577 | -0.0278 | 0.0354 | 77.3654 | 453.2777131 | 0.17067991 |
| 7233 | 0.0616 | -0.0211 | 0.0409 | 79.866 | 368.5953648 | 0.21667663 |
| 7233.5 | 0.0573 | -0.0104 | 0.048 | 111.9035 | 347.8445331 | 0.3217055 |
| 7234 | 0.0476 | 0 | 0.0522 | 188.6414 | 390.3691746 | 0.48323846 |
| 7234.5 | 0.0386 | 0.0042 | 0.0538 | 273.2146 | 460.6928182 | 0.59305157 |
| 7235 | 0.0334 | -0.0029 | 0.0579 | 290.9095 | 472.7091496 | 0.61540907 |
| 7235.5 | 0.0322 | -0.0026 | 0.0572 | 271.0185 | 494.5731268 | 0.54798469 |
| 7236 | 0.0344 | 0.0142 | 0.0518 | 229.9722 | 534.8913302 | 0.42994191 |
| 7236.5 | 0.0387 | 0.0292 | 0.0498 | 165.7513 | 505.4499387 | 0.32792822 |
| 7237 | 0.0445 | 0.0248 | 0.0527 | 115.2838 | 413.165177 | 0.27902594 |
| 7237.5 | 0.0499 | 0.0037 | 0.0649 | 85.515 | 288.8890767 | 0.29601327 |
| 7238 | 0.051 | -0.0164 | 0.0738 | 85.5529 | 241.4041999 | 0.3543969 |
| 7238.5 | 0.0492 | -0.0201 | 0.0725 | 125.2819 | 254.8187829 | 0.49165096 |
| 7239 | 0.0507 | 0.0021 | 0.0561 | 197.4732 | 337.4255674 | 0.58523485 |
| 7239.5 | 0.0573 | 0.0311 | 0.042 | 136.3907 | 394.6074642 | 0.34563639 |
| 7240 | 0.0663 | 0.046 | 0.045 | 58.3578 | 308.7746064 | 0.18899805 |
| 7240.5 | 0.0746 | 0.0431 | 0.0537 | 37.3583 | 227.4672457 | 0.16423595 |
| 7241 | 0.0762 | 0.0293 | 0.0621 | 36.5021 | 193.5701974 | 0.18857293 |
| 7241.5 | 0.0705 | 0.0233 | 0.0572 | 53.2304 | 229.7712839 | 0.2316669 |
| 7242 | 0.0634 | 0.0169 | 0.0531 | 98.83 | 279.9016384 | 0.35308832 |
| 7242.5 | 0.0597 | 0.0154 | 0.0507 | 146.3261 | 314.2119315 | 0.46569237 |
| 7243 | 0.0608 | 0.0107 | 0.0531 | 111.942 | 293.819201 | 0.3809894 |
| 7243.5 | 0.0651 | 0.0033 | 0.0577 | 79.0282 | 249.9365044 | 0.31619311 |
| 7244 | 0.0677 | -0.0085 | 0.0647 | 68.6148 | 212.5920463 | 0.32275337 |
| 7244.5 | 0.0662 | -0.014 | 0.0689 | 65.4039 | 203.5622206 | 0.32129685 |
| 7245 | 0.0639 | -0.0086 | 0.0655 | 65.6627 | 223.330216 | 0.29401619 |
| 7245.5 | 0.0619 | -0.0026 | 0.0616 | 87.0055 | 246.9006432 | 0.35239074 |
| 7246 | 0.0574 | 0.0094 | 0.0576 | 158.7178 | 287.8099628 | 0.55146736 |
| 7246.5 | 0.0525 | 0.0255 | 0.0557 | 176.1473 | 328.1085666 | 0.53685675 |
| 7247 | 0.0522 | 0.0393 | 0.057 | 180.9464 | 321.6825536 | 0.56249989 |
| 7247.5 | 0.0582 | 0.0374 | 0.0647 | 154.3053 | 249.4994726 | 0.61845942 |
| 7248 | 0.0668 | 0.0233 | 0.0714 | 207.9044 | 193.871463 | 1.07238268 |
| 7248.5 | 0.0738 | 0.0043 | 0.0751 | 413.8044 | 165.1515218 | 2.50560452 |
| 7249 | 0.0854 | 0.0015 | 0.0688 | 1394.482 | 153.1880108 | 9.10307467 |
| 7249.5 | 0.1019 | 0.0217 | 0.067 | 500.037 | 125.951236 | 3.97008411 |
| 7250 | 0.1116 | 0.0562 | 0.0724 | 91.9831 | 104.7726336 | 0.87793059 |
| 7250.5 | 0.1078 | 0.0819 | 0.0822 | 32.2321 | 97.78808427 | 0.32961173 |
| 7251 | 0.0927 | 0.0706 | 0.0873 | 25.0591 | 109.842471 | 0.22813671 |
| 7251.5 | 0.0737 | 0.0379 | 0.0803 | 40.4257 | 153.616063 | 0.26316063 |
| 7252 | 0.0595 | 0.0328 | 0.0821 | 64.7168 | 184.0010009 | 0.35171983 |
| 7252.5 | 0.0562 | 0.1005 | 0.0956 | 78.9959 | 158.4425675 | 0.49857751 |
| 7253 | 0.059 | 0.2023 | 0.1179 | 76.75 | 114.0227049 | 0.67311155 |

0.06 to 9.1

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|---|---|---|---|---|---|---|
| 7253.5 | 0.0661 | 0.2643 | 0.1414 | 42.653 | 80.91280609 | 0.5271477 |
| 7254 | 0.0841 | 0.2623 | 0.1555 | 32.0543 | 59.38948109 | 0.53973026 |
| 7254.5 | 0.1014 | 0.251 | 0.1345 | 34.2467 | 61.4102842 | 0.55767044 |
| 7255 | 0.0965 | 0.2325 | 0.0846 | 44.5565 | 108.4130374 | 0.41098839 |
| 7255.5 | 0.0741 | 0.1865 | 0.0409 | 46.9071 | 287.8099628 | 0.16297942 |
| 7256 | 0.0558 | 0.1309 | 0.0223 | 39.1097 | 661.3120822 | 0.05913955 |
| 7256.5 | 0.0501 | 0.0797 | 0.0239 | 42.435 | 742.6051945 | 0.05714342 |
| 7257 | 0.0497 | 0.0407 | 0.0256 | 83.5133 | 715.3144221 | 0.11675048 |
| 7257.5 | 0.0481 | 0.0244 | 0.0242 | 124.6822 | 780.6544524 | 0.15971497 |
| 7258 | 0.0461 | 0.0308 | 0.0289 | 148.3087 | 721.4802779 | 0.20556168 |
| 7258.5 | 0.0484 | 0.0402 | 0.0406 | 126.6274 | 499.3645011 | 0.2535771 |
| 7259 | 0.0538 | 0.0345 | 0.0585 | 61.489 | 302.8933261 | 0.20300546 |
| 7259.5 | 0.0547 | 0.0163 | 0.0708 | 55.3994 | 238.518555 | 0.23226453 |
| 7260 | 0.0521 | 0.007 | 0.0731 | 70.3882 | 239.7490379 | 0.29359117 |
| 7260.5 | 0.0504 | 0.0102 | 0.0702 | 113.2615 | 259.8420706 | 0.43588592 |
| 7261 | 0.0487 | 0.0166 | 0.0733 | 149.6757 | 253.4734898 | 0.59049844 |
| 7261.5 | 0.0473 | 0.0126 | 0.0867 | 158.4428 | 207.171907 | 0.76478902 |
| 7262 | 0.048 | 0.007 | 0.0934 | 148.3298 | 184.5610065 | 0.80368981 |
| 7262.5 | 0.05 | -0.0045 | 0.099 | 139.9723 | 164.9133079 | 0.84876292 |
| 7263 | 0.0526 | -0.0106 | 0.0987 | 119.6704 | 159.5704556 | 0.74995336 |
| 7263.5 | 0.055 | -0.01 | 0.0934 | 96.2136 | 166.3501869 | 0.57837987 |
| 7264 | 0.0569 | -0.0003 | 0.0819 | 78.8099 | 192.0741093 | 0.41030986 |
| 7264.5 | 0.0607 | 0.0082 | 0.07 | 64.531 | 218.5816333 | 0.29522609 |
| 7265 | 0.0653 | 0.0192 | 0.0586 | 58.1237 | 245.1900665 | 0.23705569 |
| 7265.5 | 0.0689 | 0.029 | 0.0501 | 74.6909 | 267.4115819 | 0.27931064 |
| 7266 | 0.0729 | 0.04 | 0.0462 | 135.4657 | 266.9290821 | 0.50749697 |
| 7266.5 | 0.0829 | 0.0526 | 0.0635 | 134.1729 | 171.2745619 | 0.78337903 |
| 7267 | 0.1107 | 0.082 | 0.1163 | 53.9895 | 66.70380178 | 0.80939165 |
| 7267.5 | 0.1753 | 0.1292 | 0.2295 | 21.3599 | 19.23264861 | 1.11060626 |
| 7268 | 0.28 | 0.179 | 0.3593 | 10.3788 | 7.200142067 | 1.44147156 |
| 7268.5 | 0.3727 | 0.2303 | 0.4074 | 5.811 | 4.693351517 | 1.23813441 |
| 7269 | 0.3978 | 0.3003 | 0.341 | 6.1953 | 5.275618392 | 1.17432679 |
| 7269.5 | 0.3743 | 0.3418 | 0.2833 | 13.93 | 6.776232527 | 2.05571458 |
| 7270 | 0.358 | 0.2895 | 0.3726 | 20.7401 | 5.403745592 | 3.83809705 |
| 7270.5 | 0.3766 | 0.2024 | 0.5241 | 22.7305 | 3.445552172 | 6.59705582 |
| 7271 | 0.4227 | 0.1502 | 0.594 | 15.3938 | 2.655471285 | 5.79701241 |
| 7271.5 | 0.4627 | 0.1284 | 0.5264 | 7.2908 | 2.817343145 | 2.58782819 |
| 7272 | 0.4304 | 0.0829 | 0.3769 | 9.4071 | 4.359945217 | 2.15761885 |
| 7272.5 | 0.3194 | 0.0255 | 0.2188 | 20.5578 | 10.42502822 | 1.97196588 |
| 7273 | 0.248 | -0.0069 | 0.1162 | 43.545 | 24.13933524 | 1.8039022 |
| 7273.5 | 0.2866 | -0.0195 | 0.1882 | 56.3502 | 13.64923003 | 4.12845266 |
| 7274 | 0.3603 | -0.0151 | 0.4088 | 29.4651 | 4.838860877 | 6.08926372 |
| 7274.5 | 0.4111 | 0.0278 | 0.5898 | 14.1066 | 2.746415227 | 5.13636826 |
| 7275 | 0.4671 | 0.1031 | 0.5874 | 8.8956 | 2.455025596 | 3.62342454 |
| 7275.5 | 0.5195 | 0.1686 | 0.4746 | 10.642 | 2.786965044 | 3.81849066 |
| 7276 | 0.5321 | 0.1979 | 0.395 | 13.3602 | 3.238053581 | 4.1259972 |
| 7276.5 | 0.5414 | 0.2258 | 0.3389 | 13.5189 | 3.619513253 | 3.73500497 |
| 7277 | 0.5686 | 0.2662 | 0.2741 | 9.9843 | 3.975660064 | 2.51135656 |
| 7277.5 | 0.5694 | 0.289 | 0.2215 | 8.4261 | 4.556640782 | 1.84919119 |
| 7278 | 0.5542 | 0.2607 | 0.2363 | 8.1341 | 4.56159948 | 1.78316839 |
| 7278.5 | 0.569 | 0.2226 | 0.2924 | 8.562 | 3.792413774 | 2.25766504 |
| 7279 | 0.5911 | 0.1911 | 0.3594 | 9.9647 | 3.069086434 | 3.2467968 |

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|---|---|---|---|---|---|---|
| 7279.5 | 0.5703 | 0.1755 | 0.381 | 9.7144 | 3.063540049 | 3.17097209 |
| 7280 | 0.4794 | 0.1599 | 0.4059 | 7.3785 | 3.575705003 | 2.06350915 |
| 7280.5 | 0.3302 | 0.1498 | 0.4505 | 5.9851 | 4.685599822 | 1.27733913 |
| 7281 | 0.2169 | 0.1186 | 0.4679 | 7.0463 | 6.210750945 | 1.13453269 |
| 7281.5 | 0.1945 | 0.0766 | 0.3435 | 19.1457 | 10.43336227 | 1.83504603 |
| 7282 | 0.2028 | 0.0373 | 0.1581 | 33.032 | 24.61639113 | 1.34187013 |
| 7282.5 | 0.2047 | 0.0142 | 0.0366 | 95.7734 | 58.49354439 | 1.63733282 |
| 7283 | 0.204 | 0.002 | 0.0041 | 175.1793 | 80.41206364 | 2.17852014 |
| 7283.5 | 0.1864 | -0.0038 | 0.0003 | 122.7768 | 101.5420429 | 1.20912281 |
| 7284 | 0.1485 | -0.0052 | 0.0025 | 69.5691 | 160.2528432 | 0.43412085 |
| 7284.5 | 0.1169 | -0.0039 | 0.0096 | 55.7546 | 234.4831017 | 0.23777662 |
| 7285 | 0.1007 | -0.0026 | 0.0175 | 50.6318 | 271.3179991 | 0.18661423 |
| 7285.5 | 0.0829 | -0.0093 | 0.0302 | 51.2214 | 298.305719 | 0.17170774 |
| 7286 | 0.0651 | -0.0096 | 0.0331 | 52.5825 | 404.1722401 | 0.13009924 |
| 7286.5 | 0.0584 | -0.0104 | 0.0313 | 50.337 | 491.0236696 | 0.10251441 |
| 7287 | 0.0598 | -0.0147 | 0.0311 | 54.5924 | 477.1927439 | 0.11440325 |
| 7287.5 | 0.0678 | -0.0153 | 0.0363 | 56.3022 | 356.5226383 | 0.15792041 |
| 7288 | 0.0889 | -0.0021 | 0.0757 | 46.3946 | 133.1318735 | 0.34848604 |
| 7288.5 | 0.1197 | 0.0287 | 0.17 | 29.2087 | 39.48361563 | 0.73976761 |
| 7289 | 0.1559 | 0.0663 | 0.2619 | 16.9198 | 17.96900558 | 0.94161026 |
| 7289.5 | 0.1861 | 0.0796 | 0.2564 | 9.9102 | 15.88154095 | 0.62400746 |
| 7290 | 0.1817 | 0.0568 | 0.1473 | 13.2168 | 30.03550924 | 0.44003915 |
| 7290.5 | 0.1543 | 0.0228 | 0.0464 | 44.7147 | 86.92192371 | 0.51442373 |
| 7291 | 0.1431 | 0.0043 | 0.0077 | 32.5485 | 160.7101461 | 0.20252922 |
| 7291.5 | 0.1479 | 0.0017 | 0.0084 | 36.7138 | 148.7970693 | 0.24673739 |
| 7292 | 0.1549 | 0.0088 | 0.0115 | 23.4158 | 130.0548456 | 0.18004558 |
| 7292.5 | 0.1692 | 0.014 | 0.0121 | 18.5545 | 108.1560708 | 0.17155301 |
| 7293 | 0.1906 | 0.0159 | 0.0096 | 17.8805 | 87.38933266 | 0.20460735 |
| 7293.5 | 0.192 | 0.0172 | 0.0057 | 19.6957 | 89.78253038 | 0.21937118 |
| 7294 | 0.1646 | 0.0162 | -0.0016 | 24.5292 | 135.9573937 | 0.18041829 |
| 7294.5 | 0.1411 | 0.0127 | -0.0138 | 33.3261 | 231.3263537 | 0.1440653 |
| 7295 | 0.1351 | 0.006 | -0.013 | 46.251 | 253.0273708 | 0.1827905 |
| 7295.5 | 0.1316 | 0.004 | 0.0004 | 56.185 | 213.9795294 | 0.26257185 |
| 7296 | 0.1312 | 0.0264 | 0.0209 | 49.404 | 157.7714329 | 0.31313654 |
| 7296.5 | 0.1656 | 0.1096 | 0.0273 | 31.6302 | 94.65463622 | 0.3341643 |
| 7297 | 0.2322 | 0.2248 | 0.0121 | 17.1987 | 56.96009778 | 0.30194295 |
| 7297.5 | 0.2699 | 0.2882 | 0.0043 | 13.2745 | 44.43868117 | 0.29871499 |
| 7298 | 0.2639 | 0.2608 | 0.0249 | 13.6604 | 39.74863544 | 0.34366966 |
| 7298.5 | 0.2507 | 0.1892 | 0.0523 | 15.3552 | 35.85126869 | 0.42830283 |
| 7299 | 0.2434 | 0.1197 | 0.0578 | 15.6709 | 36.31349084 | 0.43154485 |
| 7299.5 | 0.2339 | 0.0842 | 0.069 | 15.1529 | 35.87672094 | 0.42236023 |
| 7300 | 0.2147 | 0.1112 | 0.1208 | 16.7251 | 28.79832659 | 0.58076638 |
| 7300.5 | 0.1932 | 0.1836 | 0.2229 | 24.03 | 18.12721523 | 1.32563109 |
| 7301 | 0.1922 | 0.2505 | 0.3131 | 23.625 | 11.93919894 | 1.97877597 |
| 7301.5 | 0.2265 | 0.2744 | 0.3649 | 15.4145 | 8.512582654 | 1.81079005 |
| 7302 | 0.2865 | 0.265 | 0.3887 | 14.1628 | 6.402158883 | 2.21219127 |
| 7302.5 | 0.3272 | 0.2478 | 0.3919 | 19.0118 | 5.591253839 | 3.40027488 |
| 7303 | 0.308 | 0.2329 | 0.3214 | 40.9676 | 7.445839873 | 5.50207911 |
| 7303.5 | 0.2692 | 0.1988 | 0.2009 | 60.7076 | 13.94431356 | 4.35357393 |
| 7304 | 0.2774 | 0.1382 | 0.1618 | 68.6266 | 16.1392061 | 4.25216703 |
| 7304.5 | 0.3119 | 0.0751 | 0.3147 | 28.9794 | 7.517558918 | 3.85489496 |
| 7305 | 0.3199 | 0.0477 | 0.5607 | 18.7382 | 3.616862641 | 5.1807884 |

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|---|---|---|---|---|---|---|
| 7305.5 | 0.3117 | 0.047 | 0.7437 | 5.932 | 2.45052669 | 2.4207041 |
| 7306 | 0.3349 | 0.0465 | 0.784 | 3.6806 | 2.161249677 | 1.70299621 |
| 7306.5 | 0.3453 | 0.0418 | 0.6583 | 4.0032 | 2.730554046 | 1.46607609 |
| 7307 | 0.2569 | 0.0209 | 0.4173 | 7.2661 | 6.422592556 | 1.13133442 |
| 7307.5 | 0.153 | -0.0078 | 0.1959 | 21.6174 | 26.47275229 | 0.81659057 |
| 7308 | 0.1287 | -0.023 | 0.073 | 37.9601 | 85.99802926 | 0.44140663 |
| 7308.5 | 0.1338 | -0.0152 | 0.0309 | 136.3659 | 132.9581434 | 1.0256303 |
| 7309 | 0.1358 | -0.0002 | 0.0135 | 308.9042 | 164.201679 | 1.88124873 |
| 7309.5 | 0.1557 | 0.0126 | 0.0081 | 176.9752 | 134.5337664 | 1.31547049 |
| 7310 | 0.1818 | 0.0168 | 0.0127 | 94.6136 | 92.98845415 | 1.01747686 |
| 7310.5 | 0.175 | 0.0111 | 0.0253 | 66.9874 | 87.29555676 | 0.76736323 |
| 7311 | 0.1344 | 0.0111 | 0.0269 | 62.2876 | 139.056819 | 0.44792913 |
| 7311.5 | 0.0986 | 0.0176 | 0.0139 | 74.9647 | 301.7367838 | 0.24844402 |
| 7312 | 0.0861 | 0.0205 | -0.0037 | 115.9365 | 589.3355982 | 0.19672407 |
| 7312.5 | 0.0816 | 0.0092 | -0.0022 | 219.9055 | 638.251876 | 0.34454344 |
| 7313 | 0.0745 | -0.008 | 0.0132 | 598.6594 | 515.415001 | 1.16150946 |
| 7313.5 | 0.0824 | -0.0159 | 0.0306 | 544.2744 | 298.8735807 | 1.82108569 |
| 7314 | 0.1277 | -0.0118 | 0.0333 | 283.5112 | 139.6145069 | 2.0306715 |
| 7314.5 | 0.1928 | -0.0013 | 0.0264 | 76.7786 | 71.91160768 | 1.0676802 |
| 7315 | 0.2288 | 0.0036 | 0.0544 | 24.3051 | 41.4577468 | 0.58626196 |
| 7315.5 | 0.2248 | 0.0031 | 0.1388 | 17.1435 | 24.22505936 | 0.70767628 |
| 7316 | 0.2417 | 0.0021 | 0.2602 | 4.9691 | 12.11376682 | 0.41020271 |
| 7316.5 | 0.3033 | 0.0119 | 0.3032 | 3.8227 | 8.063432393 | 0.47407851 |
| 7317 | 0.3254 | -0.023 | 0.3657 | 6.6537 | 6.08966301 | 1.09262204 |
| 7317.5 | 0.2793 | -0.0781 | 0.4158 | 13.0547 | 6.014568977 | 2.17051297 |
| 7318 | 0.2316 | -0.1066 | 0.4135 | 22.7325 | 7.061680105 | 3.21913478 |
| 7318.5 | 0.2147 | -0.0567 | 0.2959 | 22.2447 | 11.67434269 | 1.9054349 |
| 7319 | 0.211 | 0.0207 | 0.1358 | 14.9593 | 26.81860225 | 0.55779566 |
| 7319.5 | 0.1901 | 0.0478 | 0.0376 | 31.99 | 66.26369729 | 0.48276811 |
| 7320 | 0.1559 | 0.0278 | 0.01 | 64.3277 | 130.8990366 | 0.4914299 |
| 7320.5 | 0.1377 | 0.0107 | 0.0071 | 149.2126 | 175.3693823 | 0.8508475 |
| 7321 | 0.145 | 0.0152 | 0.032 | 154.4044 | 113.8842478 | 1.3558012 |
| 7321.5 | 0.1819 | 0.0301 | 0.1585 | 57.5826 | 27.91442232 | 2.06282614 |
| 7322 | 0.2573 | 0.0692 | 0.3473 | 26.5721 | 8.118011703 | 3.2732276 |
| 7322.5 | 0.3515 | 0.1375 | 0.4497 | 11.6983 | 4.431626573 | 2.63973054 |
| 7323 | 0.3991 | 0.2013 | 0.4321 | 9.9371 | 4.0948621 | 2.42672397 |
| 7323.5 | 0.3646 | 0.2388 | 0.3893 | 14.1135 | 5.051049587 | 2.79417174 |
| 7324 | 0.301 | 0.2548 | 0.3737 | 19.1057 | 6.412363795 | 2.97950968 |
| 7324.5 | 0.2651 | 0.2575 | 0.365 | 17.1838 | 7.428066772 | 2.313361 |
| 7325 | 0.2525 | 0.2565 | 0.339 | 16.1088 | 8.509488778 | 1.89303969 |
| 7325.5 | 0.246 | 0.2524 | 0.2959 | 16.4498 | 10.2725912 | 1.60132918 |
| 7326 | 0.2402 | 0.243 | 0.2009 | 19.9971 | 15.99011201 | 1.25059161 |
| 7326.5 | 0.2247 | 0.1984 | 0.0735 | 38.1084 | 37.10348951 | 1.02708399 |
| 7327 | 0.1883 | 0.1171 | -0.0106 | 25.6168 | 112.9219087 | 0.22685412 |
| 7327.5 | 0.1491 | 0.0595 | -0.0375 | 24.0325 | 306.9927801 | 0.0782836 |
| 7328 | 0.1453 | 0.0478 | -0.0277 | 11.8514 | 274.3029248 | 0.04320552 |
| 7328.5 | 0.1865 | 0.0553 | 0.0395 | 8.7641 | 67.33998821 | 0.13014704 |
| 7329 | 0.252 | 0.0891 | 0.1398 | 7.9092 | 20.63087521 | 0.38336716 |
| 7329.5 | 0.3206 | 0.1411 | 0.2232 | 7.7392 | 10.19557898 | 0.75907411 |
| 7330 | 0.3694 | 0.1882 | 0.259 | 8.3228 | 7.47133829 | 1.11396375 |
| 7330.5 | 0.3946 | 0.1971 | 0.3195 | 8.8422 | 5.675763085 | 1.55788744 |
| 7331 | 0.429 | 0.1863 | 0.3769 | 7.3262 | 4.376245682 | 1.67408334 |

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|---|---|---|---|---|---|---|
| 7331.5 | 0.4697 | 0.1703 | 0.394 | 7.2724 | 3.770734053 | 1.92864304 |
| 7332 | 0.4802 | 0.15 | 0.395 | 11.3474 | 3.665012548 | 3.0961422 |
| 7332.5 | 0.4574 | 0.1577 | 0.3391 | 24.4094 | 4.488040351 | 5.43876572 |
| 7333 | 0.4179 | 0.1629 | 0.2112 | 48.5502 | 7.453475994 | 6.5137662 |
| 7333.5 | 0.353 | 0.1279 | 0.0704 | 149.6497 | 17.46191399 | 8.57006283 |
| 7334 | 0.2627 | 0.0595 | 0.0068 | 362.0026 | 46.12164893 | 7.84886509 |
| 7334.5 | 0.2154 | 0.0129 | 0.0085 | 147.707 | 68.70524284 | 2.14986505 |
| 7335 | 0.262 | 0.0095 | 0.0094 | 46.2176 | 45.43023853 | 1.01733122 |
| 7335.5 | 0.353 | 0.0037 | 0.0553 | 20.8086 | 18.87993581 | 1.10215417 |
| 7336 | 0.3978 | 0.0024 | 0.1112 | 9.9743 | 11.75338462 | 0.84863215 |
| 7336.5 | 0.3606 | 0.0192 | 0.1346 | 8.5877 | 12.46889055 | 0.68873008 |
| 7337 | 0.2811 | 0.082 | 0.1239 | 19.2318 | 19.21223456 | 1.00101838 |
| 7337.5 | 0.2266 | 0.2123 | 0.1131 | 31.6017 | 28.03824036 | 1.12709284 |
| 7338 | 0.2295 | 0.3671 | 0.1127 | 46.012 | 27.59968777 | 1.66712031 |
| 7338.5 | 0.2625 | 0.4276 | 0.1449 | 31.2355 | 18.96972247 | 1.64659763 |
| 7339 | 0.2911 | 0.3375 | 0.2251 | 14.9478 | 11.40374453 | 1.31077998 |
| 7339.5 | 0.2922 | 0.1719 | 0.2709 | 10.358 | 9.459045105 | 1.09503654 |
| 7340 | 0.2486 | 0.0516 | 0.2136 | 13.7758 | 14.46178187 | 0.95256588 |
| 7340.5 | 0.1904 | 0.0061 | 0.1218 | 24.7683 | 33.61827674 | 0.73675103 |
| 7341 | 0.157 | -0.0011 | 0.0737 | 25.9542 | 64.42491466 | 0.40285967 |
| 7341.5 | 0.1411 | -0.0046 | 0.0647 | 23.7888 | 82.35664263 | 0.28885102 |
| 7342 | 0.1252 | -0.0071 | 0.0631 | 23.8033 | 99.69605928 | 0.23875868 |
| 7342.5 | 0.1114 | -0.0039 | 0.0569 | 27.4522 | 126.9186169 | 0.21629766 |
| 7343 | 0.1011 | 0.0024 | 0.0491 | 39.0329 | 162.093584 | 0.24080472 |
| 7343.5 | 0.0908 | 0.005 | 0.0369 | 61.1571 | 229.7712839 | 0.26616511 |
| 7344 | 0.084 | 0.0087 | 0.0278 | 77.7067 | 305.8132531 | 0.25409854 |
| 7344.5 | 0.0828 | 0.0117 | 0.0229 | 74.9818 | 345.0205455 | 0.21732561 |
| 7345 | 0.0845 | 0.01 | 0.0279 | 66.2023 | 302.3142446 | 0.21898505 |
| 7345.5 | 0.0913 | 0.0021 | 0.0356 | 57.673 | 232.8968919 | 0.24763319 |
| 7346 | 0.1022 | -0.0087 | 0.0432 | 53.8407 | 173.8171826 | 0.30975476 |
| 7346.5 | 0.1072 | -0.0134 | 0.0452 | 56.2231 | 157.1044552 | 0.35787082 |
| 7347 | 0.1025 | -0.0053 | 0.0414 | 63.7077 | 177.7360291 | 0.35843999 |
| 7347.5 | 0.0919 | 0.0049 | 0.0319 | 76.6626 | 245.616079 | 0.3121237 |
| 7348 | 0.0782 | 0.0051 | 0.0274 | 103.162 | 345.7233846 | 0.29839463 |
| 7348.5 | 0.0633 | -0.009 | 0.0317 | 162.4 | 434.0106922 | 0.37418433 |
| 7349 | 0.0534 | -0.0163 | 0.0323 | 291.8392 | 541.6233924 | 0.53882311 |
| 7349.5 | 0.0527 | -0.0167 | 0.0294 | 202.6758 | 593.9753093 | 0.34121923 |
| 7350 | 0.0578 | -0.0214 | 0.034 | 110.0311 | 467.1909437 | 0.23551634 |
| 7350.5 | 0.0673 | -0.03 | 0.049 | 67.1039 | 280.9375518 | 0.238857 |
| 7351 | 0.0811 | -0.0334 | 0.0628 | 55.4214 | 177.7360291 | 0.3118186 |
| 7351.5 | 0.0982 | -0.0257 | 0.0672 | 53.9893 | 131.7512802 | 0.40978198 |
| 7352 | 0.1132 | -0.0208 | 0.0682 | 55.6629 | 108.027922 | 0.51526401 |
| 7352.5 | 0.1195 | -0.0125 | 0.0577 | 52.5509 | 113.6080714 | 0.46256309 |
| 7353 | 0.1193 | -0.0037 | 0.0441 | 42.6388 | 135.2428356 | 0.31527585 |
| 7353.5 | 0.1236 | 0.0009 | 0.0307 | 33.6498 | 152.9746398 | 0.21996979 |
| 7354 | 0.1506 | -0.0022 | 0.0308 | 33.5982 | 108.027922 | 0.31101404 |
| 7354.5 | 0.207 | 0.0084 | 0.0419 | 42.4588 | 54.72082702 | 0.77591664 |
| 7355 | 0.2638 | 0.0822 | 0.0439 | 45.9682 | 34.68423046 | 1.32533429 |
| 7355.5 | 0.2936 | 0.1926 | 0.048 | 27.9005 | 27.70401903 | 1.00709215 |
| 7356 | 0.3023 | 0.2372 | 0.0605 | 16.0354 | 24.34005368 | 0.65880709 |
| 7356.5 | 0.3075 | 0.1529 | 0.0764 | 14.2987 | 21.55446457 | 0.66337533 |
| 7357 | 0.3025 | 0.0476 | 0.0644 | 19.2496 | 23.7590242 | 0.81020162 |

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|---|---|---|---|---|---|---|
| 7357.5 | 0.2648 | 0.0023 | 0.0398 | 24.4493 | 35.44760498 | 0.68973066 |
| 7358 | 0.2291 | -0.0038 | 0.0297 | 23.0037 | 50.31911513 | 0.45715629 |
| 7358.5 | 0.2348 | -0.0012 | 0.0239 | 20.7921 | 50.36094356 | 0.41286161 |
| 7359 | 0.2468 | -0.0011 | 0.0205 | 19.0222 | 46.94165733 | 0.40523069 |
| 7359.5 | 0.2418 | 0.002 | 0.0185 | 17.5909 | 49.69774905 | 0.35395768 |
| 7360 | 0.2339 | 0.0018 | 0.0196 | 18.1289 | 52.60821402 | 0.34460208 |
| 7360.5 | 0.2212 | -0.0063 | 0.025 | 21.549 | 56.01919655 | 0.38467171 |
| 7361 | 0.194 | -0.0189 | 0.0316 | 26.9707 | 67.5969538 | 0.39899283 |
| 7361.5 | 0.1721 | -0.0263 | 0.036 | 31.5004 | 80.41206364 | 0.39173724 |
| 7362 | 0.1785 | -0.0245 | 0.0311 | 32.7203 | 79.17989688 | 0.41323999 |
| 7362.5 | 0.1901 | -0.0233 | 0.0322 | 31.7825 | 69.77282951 | 0.45551399 |
| 7363 | 0.1824 | -0.0264 | 0.044 | 31.4648 | 67.08445128 | 0.46903268 |
| 7363.5 | 0.1666 | -0.0298 | 0.0499 | 36.1899 | 73.85360405 | 0.49002213 |
| 7364 | 0.1513 | -0.0247 | 0.0394 | 50.1744 | 97.01797154 | 0.51716604 |
| 7364.5 | 0.1377 | -0.0212 | 0.0285 | 67.2089 | 130.3915621 | 0.51543903 |
| 7365 | 0.1286 | -0.0213 | 0.0266 | 70.8837 | 151.0737428 | 0.46919934 |
| 7365.5 | 0.1224 | -0.016 | 0.0301 | 63.6912 | 156.8830472 | 0.40597886 |
| 7366 | 0.1208 | -0.0091 | 0.0334 | 52.3836 | 153.1880108 | 0.34195626 |
| 7366.5 | 0.1267 | -0.0025 | 0.031 | 43.4472 | 145.9714895 | 0.29764168 |
| 7367 | 0.1321 | 0.0021 | 0.0218 | 39.2897 | 153.8307465 | 0.25540863 |
| 7367.5 | 0.13 | 0.0087 | 0.0138 | 39.8686 | 178.0018742 | 0.22397854 |
| 7368 | 0.1299 | 0.005 | 0.0187 | 42.4215 | 165.8691961 | 0.25575273 |
| 7368.5 | 0.1325 | -0.0041 | 0.0294 | 43.1993 | 137.9511913 | 0.31314916 |
| 7369 | 0.1307 | -0.0105 | 0.0344 | 40.9298 | 132.2665338 | 0.3094494 |
| 7369.5 | 0.1326 | -0.0102 | 0.0338 | 37.73 | 130.0548456 | 0.29010838 |
| 7370 | 0.1353 | -0.0061 | 0.0293 | 37.0785 | 133.1318735 | 0.27850956 |
| 7370.5 | 0.131 | -0.0093 | 0.0299 | 40.5946 | 139.8011312 | 0.2903739 |
| 7371 | 0.1334 | -0.0219 | 0.0413 | 44.6049 | 117.1322362 | 0.38080806 |
| 7371.5 | 0.1403 | -0.0265 | 0.0531 | 40.1365 | 94.12928725 | 0.42639758 |
| 7372 | 0.1404 | -0.0179 | 0.0585 | 33.043 | 88.62196931 | 0.37285337 |
| 7372.5 | 0.1392 | -0.0044 | 0.0554 | 29.743 | 92.88574803 | 0.32021059 |
| 7373 | 0.142 | 0.0014 | 0.0543 | 29.9754 | 91.16487399 | 0.32880427 |
| 7373.5 | 0.1446 | 0.0007 | 0.0553 | 32.9168 | 87.67154758 | 0.3754559 |
| 7374 | 0.1481 | -0.0067 | 0.0579 | 39.5202 | 82.1848291 | 0.48086977 |
| 7374.5 | 0.165 | 0.0035 | 0.0603 | 54.8353 | 67.79062188 | 0.80889212 |
| 7375 | 0.185 | 0.1023 | 0.0368 | 70.2415 | 70.11143648 | 1.0018551 |
| 7375.5 | 0.1924 | 0.3563 | -0.0582 | 55.4459 | 206.5086612 | 0.26849189 |
| 7376 | 0.2111 | 0.6128 | -0.1598 | 19.058 | 1632.502463 | 0.0116741 |
| 7376.5 | 0.2501 | 0.6284 | -0.1532 | 11.5848 | 415.9202443 | 0.02785342 |
| 7377 | 0.2859 | 0.3747 | 0.0031 | 14.5895 | 39.68951741 | 0.36759076 |
| 7377.5 | 0.3059 | 0.1473 | 0.1396 | 24.013 | 15.65249621 | 1.5341323 |
| 7378 | 0.3049 | 0.1122 | 0.1948 | 20.6943 | 12.22872219 | 1.69227002 |
| 7378.5 | 0.2976 | 0.2245 | 0.1739 | 16.1832 | 13.85544668 | 1.16800276 |
| 7379 | 0.3003 | 0.3569 | 0.1389 | 13.6449 | 16.1392061 | 0.84545051 |
| 7379.5 | 0.3034 | 0.3989 | 0.176 | 10.7255 | 13.36919988 | 0.80225444 |
| 7380 | 0.2811 | 0.3379 | 0.2636 | 10.302 | 10.15939447 | 1.01403681 |
| 7380.5 | 0.2384 | 0.2434 | 0.2938 | 14.1009 | 10.67935957 | 1.32038817 |
| 7381 | 0.2184 | 0.1763 | 0.1989 | 43.4871 | 18.01532715 | 2.41389455 |
| 7381.5 | 0.2208 | 0.1284 | 0.1047 | 53.6931 | 30.73417398 | 1.74701621 |
| 7382 | 0.2249 | 0.0962 | 0.1171 | 59.2335 | 27.6344008 | 2.14346967 |
| 7382.5 | 0.2501 | 0.0744 | 0.256 | 41.2826 | 11.89866 | 3.46951673 |
| 7383 | 0.3117 | 0.0674 | 0.4375 | 19.9995 | 5.119422554 | 3.90659294 |

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| 7383.5 | 0.3983 | 0.0747 | 0.5889 | 9.824 | 2.829014118 | 3.47258783 |
| 7384 | 0.4707 | 0.1237 | 0.6063 | 6.967 | 2.346077844 | 2.96963718 |
| 7384.5 | 0.4838 | 0.1843 | 0.5386 | 7.7729 | 2.62374348 | 2.96252285 |
| 7385 | 0.4546 | 0.2008 | 0.4972 | 10.5048 | 3.060081013 | 3.43285029 |
| 7385.5 | 0.4303 | 0.1757 | 0.4844 | 13.6353 | 3.333166591 | 4.09079463 |
| 7386 | 0.4193 | 0.1512 | 0.4366 | 19.7909 | 3.845002916 | 5.14717425 |
| 7386.5 | 0.3913 | 0.1603 | 0.363 | 20.055 | 5.04529249 | 3.97499254 |
| 7387 | 0.3569 | 0.1872 | 0.3255 | 17.4279 | 6.257808821 | 2.78498441 |
| 7387.5 | 0.3572 | 0.2062 | 0.3184 | 7.6857 | 6.394012077 | 1.20201525 |
| 7388 | 0.3456 | 0.2179 | 0.3006 | 7.5803 | 7.035860656 | 1.07738063 |
| 7388.5 | 0.2956 | 0.2304 | 0.2855 | 12.6881 | 8.840295821 | 1.4352574 |
| 7389 | 0.2663 | 0.2662 | 0.2473 | 26.1735 | 11.52822377 | 2.27038445 |
| 7389.5 | 0.2635 | 0.307 | 0.1863 | 61.8348 | 15.33254897 | 4.03291065 |
| 7390 | 0.2635 | 0.29 | 0.1986 | 177.0901 | 14.4685113 | 12.2396905 |
| 7390.5 | 0.272 | 0.2454 | 0.2832 | 150.6 | 9.750790974 | 15.4449009 |
| 7391 | 0.3129 | 0.2301 | 0.3572 | 51.0008 | 6.507377504 | 7.83738149 |
| 7391.5 | 0.3808 | 0.2516 | 0.3689 | 34.3107 | 5.112084594 | 6.71168471 |
| 7392 | 0.4269 | 0.2645 | 0.3735 | 11.6215 | 4.441155282 | 2.61677407 |
| 7392.5 | 0.4602 | 0.2329 | 0.4144 | 6.6372 | 3.670420427 | 1.80829421 |
| 7393 | 0.4929 | 0.1711 | 0.4538 | 5.4566 | 3.095633725 | 1.76267624 |
| 7393.5 | 0.4661 | 0.0962 | 0.4318 | 6.6012 | 3.468694417 | 1.90307914 |
| 7394 | 0.3773 | 0.0287 | 0.3217 | 11.3204 | 5.942651363 | 1.90494096 |
| 7394.5 | 0.3029 | -0.0207 | 0.2054 | 20.6806 | 11.78821218 | 1.75434576 |
| 7395 | 0.2823 | -0.0126 | 0.1342 | 37.3955 | 18.08980635 | 2.06721395 |
| 7395.5 | 0.2955 | 0.028 | 0.1929 | 31.6642 | 12.84513051 | 2.46507421 |
| 7396 | 0.3375 | 0.0926 | 0.3034 | 21.7644 | 7.161551119 | 3.0390623 |
| 7396.5 | 0.4105 | 0.1636 | 0.3476 | 8.3362 | 4.991076338 | 1.6702209 |
| 7397 | 0.466 | 0.2065 | 0.3387 | 7.5273 | 4.390288674 | 1.71453418 |
| 7397.5 | 0.4864 | 0.2184 | 0.3334 | 9.5381 | 4.218267968 | 2.26114132 |
| 7398 | 0.501 | 0.2067 | 0.3572 | 11.2712 | 3.822881915 | 2.9483516 |
| 7398.5 | 0.509 | 0.2047 | 0.3604 | 10.4979 | 3.717782365 | 2.82369944 |
| 7399 | 0.5 | 0.2115 | 0.3588 | 9.3755 | 3.817141886 | 2.45615706 |
| 7399.5 | 0.4737 | 0.2278 | 0.3487 | 8.9732 | 4.18964776 | 2.14175523 |
| 7400 | 0.4081 | 0.2304 | 0.3247 | 9.6744 | 5.368926268 | 1.80192454 |
| 7400.5 | 0.3172 | 0.2327 | 0.2477 | 13.3995 | 9.394362072 | 1.42633421 |
| 7401 | 0.2741 | 0.2429 | 0.1738 | 19.1306 | 15.47272818 | 1.23640768 |
| 7401.5 | 0.2762 | 0.2745 | 0.1514 | 17.4791 | 17.09523726 | 1.02245437 |
| 7402 | 0.2733 | 0.2759 | 0.2294 | 13.7819 | 12.0723572 | 1.14160804 |
| 7402.5 | 0.264 | 0.2196 | 0.3093 | 14.8324 | 9.100913893 | 1.62977039 |
| 7403 | 0.2491 | 0.1349 | 0.2709 | 18.7527 | 11.22532675 | 1.67057053 |
| 7403.5 | 0.2238 | 0.0626 | 0.1488 | 26.633 | 22.98444659 | 1.1587401 |
| 7404 | 0.2052 | 0.0226 | 0.0593 | 39.2984 | 48.01655258 | 0.81843443 |
| 7404.5 | 0.204 | 0.0149 | 0.0447 | 50.7024 | 54.81548258 | 0.92496495 |
| 7405 | 0.2072 | 0.0315 | 0.0493 | 65.6503 | 51.29420886 | 1.27987743 |
| 7405.5 | 0.2001 | 0.0372 | 0.0499 | 94.5445 | 54.20447739 | 1.74421938 |
| 7406 | 0.1745 | 0.0248 | 0.0454 | 136.7258 | 71.4203439 | 1.91438171 |
| 7406.5 | 0.1465 | 0.0037 | 0.0404 | 183.4426 | 101.3085693 | 1.81073133 |
| 7407 | 0.1405 | -0.0149 | 0.0416 | 156.05 | 107.1370778 | 1.45654523 |
| 7407.5 | 0.1432 | -0.003 | 0.0495 | 216.2588 | 94.86597916 | 2.27962439 |
| 7408 | 0.1398 | 0.0625 | 0.0756 | 88.877 | 74.66686675 | 1.19031377 |
| 7408.5 | 0.1657 | 0.1723 | 0.126 | 31.4147 | 38.90387468 | 0.8074954 |
| 7409 | 0.2815 | 0.2503 | 0.2252 | 20.2726 | 11.868388 | 1.70811739 |

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|---|---|---|---|---|---|---|
| 7409.5 | 0.3815 | 0.2528 | 0.3476 | 7.1514 | 5.42767605 | 1.31758048 |
| 7410 | 0.3313 | 0.2062 | 0.4233 | 5.826 | 5.040980974 | 1.15572743 |
| 7410.5 | 0.2604 | 0.1511 | 0.4113 | 8.4802 | 6.474096691 | 1.30986613 |
| 7411 | 0.2607 | 0.135 | 0.325 | 29.8816 | 8.691694408 | 3.43794876 |
| 7411.5 | 0.2689 | 0.1672 | 0.2511 | 30.2074 | 11.22532675 | 2.69100407 |
| 7412 | 0.2565 | 0.2012 | 0.2096 | 60.7184 | 14.2028699 | 4.27507964 |
| 7412.5 | 0.2204 | 0.1683 | 0.1761 | 37.5693 | 20.10866866 | 1.86831364 |
| 7413 | 0.1756 | 0.0984 | 0.1176 | 46.3918 | 38.47721706 | 1.20569531 |
| 7413.5 | 0.1518 | 0.0443 | 0.0641 | 55.2426 | 74.29558372 | 0.7435516 |
| 7414 | 0.1518 | 0.0162 | 0.0341 | 73.1764 | 102.4838642 | 0.7140285 |
| 7414.5 | 0.1521 | -0.0017 | 0.0232 | 141.1355 | 116.271978 | 1.21383933 |
| 7415 | 0.1508 | -0.0124 | 0.0206 | 175.6493 | 122.0345832 | 1.43934035 |
| 7415.5 | 0.1755 | -0.0202 | 0.0527 | 85.2788 | 65.95193681 | 1.29304466 |
| 7416 | 0.2271 | -0.0262 | 0.1491 | 37.9441 | 22.5141616 | 1.68534368 |
| 7416.5 | 0.2833 | -0.0055 | 0.2584 | 20.3441 | 10.28074728 | 1.97885421 |
| 7417 | 0.3326 | 0.0866 | 0.2562 | 16.2661 | 8.593605388 | 1.8928144 |
| 7417.5 | 0.3322 | 0.214 | 0.2085 | 16.3364 | 10.32167037 | 1.58272832 |
| 7418 | 0.2727 | 0.3232 | 0.1722 | 14.3134 | 15.69791625 | 0.91180255 |
| 7418.5 | 0.2157 | 0.3431 | 0.1953 | 12.0998 | 18.61428089 | 0.6500278 |
| 7419 | 0.1798 | 0.2889 | 0.1823 | 16.6898 | 24.44133096 | 0.68285152 |
| 7419.5 | 0.1585 | 0.1968 | 0.1416 | 23.6458 | 36.60027007 | 0.64605534 |
| 7420 | 0.1526 | 0.1009 | 0.1985 | 30.5571 | 26.11739737 | 1.16999024 |
| 7420.5 | 0.1584 | 0.0775 | 0.3507 | 25.1758 | 11.74842156 | 2.14290915 |
| 7421 | 0.2076 | 0.1358 | 0.4588 | 19.628 | 6.585305923 | 2.98057527 |
| 7421.5 | 0.3482 | 0.2133 | 0.4636 | 8.8926 | 4.308149138 | 2.06413467 |
| 7422 | 0.5028 | 0.2568 | 0.4355 | 6.3613 | 3.155524018 | 2.01592508 |
| 7422.5 | 0.5459 | 0.2652 | 0.4319 | 5.7424 | 2.887809956 | 1.9884965 |
| 7423 | 0.5258 | 0.2574 | 0.4445 | 7.0152 | 2.936014612 | 2.38936141 |
| 7423.5 | 0.5007 | 0.2202 | 0.4682 | 14.021 | 2.94514326 | 4.76071918 |
| 7424 | 0.458 | 0.1398 | 0.4707 | 27.157 | 3.226071379 | 8.41797865 |
| 7424.5 | 0.4233 | 0.0666 | 0.3726 | 77.7823 | 4.49531775 | 17.3029593 |
| 7425 | 0.3929 | 0.029 | 0.3009 | 247.7804 | 6.038825007 | 41.0312271 |
| 7425.5 | 0.3668 | 0.0377 | 0.281 | 290.0519 | 6.998551315 | 41.4445629 |
| 7426 | 0.3591 | 0.048 | 0.2468 | 160.5167 | 8.080609734 | 19.8644292 |
| 7426.5 | 0.3344 | 0.0491 | 0.1196 | 79.0764 | 15.02920805 | 5.26151476 |
| 7427 | 0.3104 | 0.0412 | 0.0173 | 34.6982 | 30.29227084 | 1.1454473 |
| 7427.5 | 0.3417 | 0.041 | 0.0257 | 19.9949 | 23.68956049 | 0.84403845 |
| 7428 | 0.399 | 0.0627 | 0.1446 | 8.9952 | 10.20364562 | 0.88156727 |
| 7428.5 | 0.4509 | 0.1138 | 0.3011 | 6.2063 | 5.078527669 | 1.22206679 |
| 7429 | 0.4804 | 0.1868 | 0.3628 | 5.8344 | 3.970593203 | 1.46940261 |
| 7429.5 | 0.4573 | 0.26 | 0.2904 | 7.6106 | 5.141529261 | 1.48022108 |
| 7430 | 0.4125 | 0.3036 | 0.2079 | 12.5546 | 7.680010849 | 1.63471123 |
| 7430.5 | 0.3979 | 0.339 | 0.1774 | 14.5021 | 9.033026327 | 1.60545309 |
| 7431 | 0.4264 | 0.3466 | 0.2134 | 12.0481 | 7.188049734 | 1.67612919 |
| 7431.5 | 0.4673 | 0.3026 | 0.302 | 7.6969 | 4.836156601 | 1.59153242 |
| 7432 | 0.4791 | 0.2271 | 0.375 | 5.6876 | 3.862446066 | 1.47253836 |
| 7432.5 | 0.4545 | 0.1528 | 0.3582 | 5.6333 | 4.297898172 | 1.31071044 |
| 7433 | 0.387 | 0.0884 | 0.2474 | 6.9046 | 7.320240597 | 0.94322036 |
| 7433.5 | 0.296 | 0.0395 | 0.1226 | 12.0698 | 17.89525324 | 0.67446936 |
| 7434 | 0.2317 | 0.0214 | 0.0372 | 55.2968 | 46.34319326 | 1.1932022 |
| 7434.5 | 0.2051 | 0.0169 | 0.0076 | 56.8063 | 76.71955531 | 0.74044094 |
| 7435 | 0.1949 | 0.0135 | 0.0037 | 201.4645 | 88.91003992 | 2.26593645 |

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|---|---|---|---|---|---|---|
| 7435.5 | 0.1787 | 0.0051 | 0.0062 | 994.4578 | 103.6792439 | 9.59167682 |
| 7436 | 0.1503 | -0.0051 | 0.0145 | 2494.994 | 132.7847451 | 18.7897631 |
| 7436.5 | 0.1248 | -0.0099 | 0.0167 | 832.6983 | 184.280692 | 4.51864105 |
| 7437 | 0.1156 | -0.0116 | 0.0124 | 275.3521 | 228.6150123 | 1.20443578 |
| 7437.5 | 0.1229 | -0.0114 | 0.0055 | 122.4541 | 227.0865326 | 0.53923982 |
| 7438 | 0.1435 | -0.0187 | 0.0184 | 69.5854 | 137.9511913 | 0.50442044 |
| 7438.5 | 0.1629 | -0.0249 | 0.0434 | 44.4014 | 81.92809185 | 0.54195574 |
| 7439 | 0.1604 | -0.0183 | 0.0497 | 36.9106 | 78.77531845 | 0.46855539 |
| 7439.5 | 0.1378 | -0.0135 | 0.0449 | 40.4854 | 106.3820374 | 0.38056613 |
| 7440 | 0.1149 | -0.0059 | 0.0384 | 48.1807 | 155.1281264 | 0.31058649 |
| 7440.5 | 0.1077 | -0.0032 | 0.0324 | 46.9084 | 188.2626594 | 0.24916465 |
| 7441 | 0.1171 | 0.0015 | 0.0274 | 47.6509 | 176.1531075 | 0.27050843 |
| 7441.5 | 0.1323 | 0.0056 | 0.033 | 65.7334 | 131.9227042 | 0.49827208 |
| 7442 | 0.1537 | 0.0302 | 0.0638 | 104.7356 | 73.12548649 | 1.43227218 |
| 7442.5 | 0.1878 | 0.0733 | 0.1211 | 37.7598 | 34.39518719 | 1.0978222 |
| 7443 | 0.2206 | 0.0893 | 0.1699 | 16.0652 | 20.77882321 | 0.77315254 |
| 7443.5 | 0.2193 | 0.0548 | 0.1735 | 15.5301 | 20.51811691 | 0.75689694 |
| 7444 | 0.1716 | 0.0123 | 0.1158 | 40.0434 | 40.16609749 | 0.99694525 |
| 7444.5 | 0.1154 | -0.0115 | 0.0594 | 74.0738 | 116.9882136 | 0.63317319 |
| 7445 | 0.0862 | -0.0228 | 0.0336 | 188.7592 | 263.5870207 | 0.7161172 |
| 7445.5 | 0.0809 | -0.0248 | 0.028 | 214.1864 | 323.5908544 | 0.66190499 |
| 7446 | 0.0932 | -0.0071 | 0.0388 | 98.9445 | 213.9795294 | 0.46240171 |
| 7446.5 | 0.1249 | 0.0463 | 0.0718 | 47.9773 | 90.76675439 | 0.5285779 |
| 7447 | 0.1697 | 0.1052 | 0.147 | 25.2929 | 32.59964299 | 0.77586432 |
| 7447.5 | 0.213 | 0.1087 | 0.224 | 33.7813 | 16.31439942 | 2.07064319 |
| 7448 | 0.2364 | 0.0468 | 0.2417 | 123.2865 | 13.4474792 | 9.16800079 |
| 7448.5 | 0.217 | -0.0197 | 0.1781 | 285.4849 | 20.26217521 | 14.0895485 |
| 7449 | 0.1653 | -0.0419 | 0.0809 | 175.0564 | 56.01919655 | 3.12493593 |
| 7449.5 | 0.1199 | -0.0378 | 0.0281 | 113.6021 | 167.3183188 | 0.67895793 |
| 7450 | 0.0952 | -0.0241 | 0.0122 | 95.1078 | 333.3857059 | 0.28527858 |
| 7450.5 | 0.0904 | -0.0162 | 0.0137 | 80.7861 | 356.5226383 | 0.22659459 |
| 7451 | 0.0977 | -0.009 | 0.0196 | 55.8685 | 275.8134586 | 0.20255901 |
| 7451.5 | 0.1073 | -0.0041 | 0.0258 | 35.757 | 210.1954742 | 0.17011308 |
| 7452 | 0.1251 | 0.0048 | 0.0255 | 25.3429 | 161.1693635 | 0.1572439 |
| 7452.5 | 0.159 | 0.01 | 0.034 | 21.4575 | 94.54922335 | 0.22694528 |
| 7453 | 0.1804 | 0.0233 | 0.0425 | 23.5933 | 69.36965473 | 0.34010981 |
| 7453.5 | 0.1603 | 0.0416 | 0.034 | 34.2601 | 93.19436615 | 0.36761986 |
| 7454 | 0.128 | 0.0544 | 0.0167 | 51.6949 | 175.6300554 | 0.29433971 |
| 7454.5 | 0.1146 | 0.0483 | 0.0123 | 57.9605 | 232.8968919 | 0.24886764 |
| 7455 | 0.1126 | 0.0272 | 0.0231 | 52.6762 | 201.6320231 | 0.26124918 |
| 7455.5 | 0.1107 | 0.0029 | 0.0346 | 47.2794 | 174.0744812 | 0.27160443 |
| 7456 | 0.1066 | -0.0105 | 0.0409 | 42.0639 | 168.5401346 | 0.24957794 |
| 7456.5 | 0.1054 | -0.0138 | 0.0445 | 37.0431 | 162.7918541 | 0.22754885 |
| 7457 | 0.1097 | -0.0178 | 0.0514 | 34.376 | 139.4282474 | 0.24654975 |
| 7457.5 | 0.1111 | -0.0185 | 0.0535 | 33.5875 | 133.1318735 | 0.25228744 |
| 7458 | 0.1018 | -0.0102 | 0.0505 | 33.6557 | 157.3263214 | 0.21392288 |
| 7458.5 | 0.0875 | -0.0002 | 0.0473 | 34.6421 | 204.5374852 | 0.16936798 |
| 7459 | 0.0803 | 0.0053 | 0.0469 | 38.624 | 231.7175302 | 0.16668571 |
| 7459.5 | 0.0795 | -0.0012 | 0.0498 | 47.5073 | 223.7017346 | 0.21236894 |
| 7460 | 0.0786 | -0.005 | 0.0416 | 66.0506 | 261.7047316 | 0.25238596 |
| 7460.5 | 0.0802 | -0.0067 | 0.0333 | 108.6691 | 296.0500085 | 0.36706332 |
| 7461 | 0.0836 | -0.0156 | 0.0355 | 154.846 | 266.9290821 | 0.58010165 |

0.17 to 0.83

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|---|---|---|---|---|---|---|
| 7461.5 | 0.0857 | -0.0335 | 0.0566 | 142.4622 | 182.0604639 | 0.78249938 |
| 7462 | 0.0878 | -0.0437 | 0.0748 | 113.9385 | 136.6774969 | 0.83363028 |
| 7462.5 | 0.091 | -0.0326 | 0.0762 | 74.985 | 128.7206408 | 0.58254061 |
| 7463 | 0.0949 | -0.0104 | 0.0654 | 55.0837 | 140.9285901 | 0.39086249 |
| 7463.5 | 0.0987 | -0.0026 | 0.0589 | 48.2857 | 146.1706984 | 0.33033775 |
| 7464 | 0.1016 | -0.0058 | 0.0585 | 46.1679 | 141.307371 | 0.32671969 |
| 7464.5 | 0.1045 | -0.0059 | 0.0559 | 45.1383 | 140.7397573 | 0.32072174 |
| 7465 | 0.1106 | 0.0015 | 0.0484 | 42.5054 | 143.417571 | 0.29637512 |
| 7465.5 | 0.1217 | 0.0143 | 0.0395 | 38.811 | 139.2423517 | 0.27872985 |
| 7466 | 0.1341 | 0.0142 | 0.0416 | 37.0429 | 115.7036056 | 0.32015338 |
| 7466.5 | 0.1385 | 0.0054 | 0.0496 | 37.3784 | 99.92410562 | 0.3740679 |
| 7467 | 0.1307 | -0.0088 | 0.0584 | 40.1061 | 98.79145759 | 0.40596729 |
| 7467.5 | 0.1209 | -0.0171 | 0.0571 | 46.6919 | 112.5131219 | 0.41499071 |
| 7468 | 0.1193 | -0.0135 | 0.0437 | 47.8673 | 135.9573937 | 0.35207574 |
| 7468.5 | 0.1282 | -0.0057 | 0.0322 | 38.607 | 140.7397573 | 0.27431481 |
| 7469 | 0.1414 | 0.002 | 0.0296 | 35.1148 | 122.64915 | 0.28630284 |
| 7469.5 | 0.1436 | 0.002 | 0.0391 | 39.4305 | 106.3820374 | 0.37064998 |
| 7470 | 0.1343 | -0.0004 | 0.0506 | 48.5362 | 103.6792439 | 0.46813806 |
| 7470.5 | 0.1287 | 0.0005 | 0.0547 | 51.4971 | 105.5109705 | 0.48807342 |
| 7471 | 0.1335 | 0.0065 | 0.0544 | 43.2781 | 100.152917 | 0.43212021 |
| 7471.5 | 0.1436 | 0.0145 | 0.054 | 34.618 | 89.88024729 | 0.38515693 |
| 7472 | 0.1509 | 0.0177 | 0.0552 | 29.388 | 82.09911921 | 0.35795756 |
| 7472.5 | 0.1493 | 0.0168 | 0.0557 | 26.7001 | 83.04918577 | 0.32149743 |
| 7473 | 0.1391 | 0.0163 | 0.058 | 26.1552 | 90.37117687 | 0.28941971 |
| 7473.5 | 0.127 | 0.0135 | 0.0623 | 28.538 | 98.56718648 | 0.2895284 |
| 7474 | 0.1181 | -0.0001 | 0.0677 | 34.5539 | 102.6024909 | 0.33677447 |
| 7474.5 | 0.114 | -0.0188 | 0.0756 | 43.7862 | 98.23217594 | 0.44574193 |
| 7475 | 0.1146 | -0.0254 | 0.0796 | 50.3569 | 93.29757275 | 0.53974502 |
| 7475.5 | 0.1242 | -0.0112 | 0.0725 | 44.0448 | 90.76675439 | 0.48525256 |
| 7476 | 0.1482 | 0.0088 | 0.0585 | 30.2253 | 81.58759951 | 0.37046439 |
| 7476.5 | 0.172 | 0.0161 | 0.0536 | 22.5054 | 67.5969538 | 0.33293512 |
| 7477 | 0.1711 | 0.0064 | 0.0601 | 21.3554 | 64.12573356 | 0.33302387 |
| 7477.5 | 0.1435 | -0.0087 | 0.0726 | 24.2024 | 74.14782758 | 0.32640741 |
| 7478 | 0.1127 | -0.0163 | 0.0761 | 24.6629 | 99.12926858 | 0.24879534 |
| 7478.5 | 0.1002 | -0.016 | 0.0748 | 21.1997 | 116.7009457 | 0.18165834 |
| 7479 | 0.1051 | -0.0145 | 0.0757 | 17.9381 | 108.8001675 | 0.16487199 |
| 7479.5 | 0.1151 | -0.01 | 0.0781 | 15.8687 | 94.33891296 | 0.16820949 |
| 7480 | 0.1207 | 0.0022 | 0.0824 | 14.6317 | 84.72856379 | 0.17268911 |
| 7480.5 | 0.1211 | 0.0142 | 0.082 | 13.9651 | 84.72856379 | 0.16482163 |
| 7481 | 0.1212 | 0.019 | 0.0821 | 13.6375 | 84.5494557 | 0.16129613 |
| 7481.5 | 0.1215 | 0.0166 | 0.0819 | 13.3493 | 84.46010961 | 0.1580545 |
| 7482 | 0.1327 | 0.0131 | 0.0838 | 13.169 | 73.85360405 | 0.17831222 |
| 7482.5 | 0.1605 | 0.0109 | 0.0813 | 13.4459 | 58.23380162 | 0.23089511 |
| 7483 | 0.1827 | 0.0195 | 0.0689 | 14.1786 | 53.46607597 | 0.26518872 |
| 7483.5 | 0.1885 | 0.0259 | 0.0554 | 14.7881 | 57.16113051 | 0.25870902 |
| 7484 | 0.1787 | 0.0222 | 0.0558 | 14.9184 | 62.20124236 | 0.23984087 |
| 7484.5 | 0.1538 | 0.0059 | 0.0726 | 14.5972 | 67.08445128 | 0.21759439 |
| 7485 | 0.1315 | -0.0087 | 0.0921 | 13.8835 | 68.90358395 | 0.2014917 |
| 7485.5 | 0.1243 | -0.0043 | 0.0939 | 13.0042 | 72.62204525 | 0.17906684 |
| 7486 | 0.1269 | 0.0067 | 0.0885 | 12.4456 | 74.66686675 | 0.166681 |
| 7486.5 | 0.1291 | 0.0066 | 0.0876 | 12.4477 | 73.70713336 | 0.16888053 |
| 7487 | 0.1261 | -0.0014 | 0.091 | 12.9401 | 73.41546599 | 0.1762585 |

~19,000 ppm

0.17 to 0.57

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|---|---|---|---|---|---|---|
| 7487.5 | 0.1214 | -0.0101 | 0.09 | 13.7929 | 77.73748156 | 0.17742921 |
| 7488 | 0.1221 | -0.0078 | 0.0821 | 14.9093 | 83.75029472 | 0.17802087 |
| 7488.5 | 0.1266 | -0.0037 | 0.0776 | 16.246 | 83.75029472 | 0.19398141 |
| 7489 | 0.1245 | 0.0003 | 0.0812 | 17.7235 | 82.4427468 | 0.21497949 |
| 7489.5 | 0.1171 | 0.0099 | 0.0858 | 18.8542 | 84.90822832 | 0.22205386 |
| 7490 | 0.1122 | 0.0181 | 0.0867 | 18.8881 | 88.62196931 | 0.21313112 |
| 7490.5 | 0.1113 | 0.0161 | 0.0868 | 18.3793 | 89.39321519 | 0.20560061 |
| 7491 | 0.1155 | 0.0062 | 0.0889 | 18.5257 | 83.57420682 | 0.22166767 |
| 7491.5 | 0.1206 | -0.0051 | 0.0919 | 19.0641 | 76.87488361 | 0.24798867 |
| 7492 | 0.1248 | -0.0126 | 0.0949 | 19.5604 | 71.560202 | 0.27334188 |
| 7492.5 | 0.1313 | -0.0168 | 0.0946 | 19.915 | 67.40409526 | 0.29545683 |
| 7493 | 0.1393 | -0.0128 | 0.0914 | 19.9214 | 64.42491466 | 0.30921888 |
| 7493.5 | 0.1528 | -0.0064 | 0.0894 | 19.566 | 58.02722228 | 0.33718657 |
| 7494 | 0.1695 | 0.0007 | 0.0935 | 19.3005 | 48.60728019 | 0.39707015 |
| 7494.5 | 0.1763 | 0.0076 | 0.1094 | 19.7542 | 40.6817066 | 0.48557943 |
| 7495 | 0.1775 | 0.0267 | 0.1188 | 21.6002 | 37.61691099 | 0.57421514 |
| 7495.5 | 0.1886 | 0.0656 | 0.1154 | 24.0109 | 35.59819481 | 0.67449769 |
| 7496 | 0.206 | 0.1357 | 0.0859 | 23.3277 | 38.84658768 | 0.60050834 |
| 7496.5 | 0.2244 | 0.1927 | 0.0617 | 21.4817 | 40.55951806 | 0.52963401 |
| 7497 | 0.251 | 0.1839 | 0.0947 | 14.7689 | 27.00240919 | 0.54694749 |
| 7497.5 | 0.2791 | 0.1305 | 0.1738 | 9.8013 | 15.10779874 | 0.64875765 |
| 7498 | 0.2889 | 0.0926 | 0.204 | 7.9376 | 12.59431992 | 0.63025237 |
| 7498.5 | 0.2586 | 0.0855 | 0.1208 | 8.6272 | 22.10787132 | 0.39023205 |
| 7499 | 0.2056 | 0.0611 | 0.0447 | 14.5266 | 54.06489371 | 0.26868822 |
| 7499.5 | 0.173 | 0.0381 | 0.0234 | 27.0558 | 91.0651046 | 0.29710392 |
| 7500 | 0.163 | 0.0254 | 0.0334 | 28.0984 | 91.0651046 | 0.30855288 |
| 7500.5 | 0.1594 | 0.0158 | 0.0412 | 24.2622 | 87.015112 | 0.27882743 |
| 7501 | 0.1586 | 0.0013 | 0.0559 | 28.0661 | 75.34206038 | 0.3725157 |
| 7501.5 | 0.1676 | -0.0031 | 0.1023 | 38.2914 | 45.97481373 | 0.83287776 |
| 7502 | 0.1982 | 0.0199 | 0.2096 | 46.6759 | 18.92974022 | 2.46574435 |
| 7502.5 | 0.255 | 0.0784 | 0.3529 | 41.1027 | 8.023559396 | 5.12275138 |
| 7503 | 0.3211 | 0.1279 | 0.4822 | 43.2372 | 4.406755764 | 9.81157167 |
| 7503.5 | 0.3757 | 0.1181 | 0.5426 | 19.0898 | 3.305135919 | 5.77579878 |
| 7504 | 0.3952 | 0.0606 | 0.4712 | 15.2592 | 3.745514877 | 4.07399263 |
| 7504.5 | 0.3408 | 0.0088 | 0.2902 | 20.4136 | 7.405306832 | 2.75661772 |
| 7505 | 0.2507 | 0.0011 | 0.1244 | 32.7351 | 22.65635246 | 1.44485305 |
| 7505.5 | 0.2082 | 0.0447 | 0.0612 | 58.5452 | 46.15846508 | 1.2683524 |
| 7506 | 0.2131 | 0.0926 | 0.0587 | 45.6776 | 45.28661474 | 1.00863357 |
| 7506.5 | 0.2269 | 0.0925 | 0.056 | 35.0452 | 41.55232634 | 0.84339923 |
| 7507 | 0.2321 | 0.0657 | 0.0553 | 22.9105 | 40.16609749 | 0.57039397 |
| 7507.5 | 0.2263 | 0.0863 | 0.0757 | 14.6939 | 36.10698727 | 0.40695447 |
| 7508 | 0.228 | 0.1411 | 0.0972 | 15.7344 | 30.79516432 | 0.51093736 |
| 7508.5 | 0.2383 | 0.1482 | 0.0891 | 26.8867 | 30.3519801 | 0.88583018 |
| 7509 | 0.2311 | 0.0864 | 0.0568 | 54.2839 | 40.01626963 | 1.35654574 |
| 7509.5 | 0.2106 | 0.0268 | 0.0258 | 68.8483 | 61.13136805 | 1.12623522 |
| 7510 | 0.1955 | 0.0063 | 0.0134 | 76.726 | 79.75144014 | 0.96206413 |
| 7510.5 | 0.1912 | 0.0029 | 0.0121 | 95.0396 | 84.5494557 | 1.1240711 |
| 7511 | 0.1918 | 0.0053 | 0.0094 | 133.7912 | 86.45816842 | 1.54746743 |
| 7511.5 | 0.1856 | 0.0041 | 0.013 | 234.3887 | 88.91003992 | 2.63624558 |
| 7512 | 0.1839 | -0.0009 | 0.0286 | 378.7459 | 76.87488361 | 4.92678339 |
| 7512.5 | 0.1996 | -0.0022 | 0.0755 | 171.0601 | 44.12669601 | 3.87656715 |
| 7513 | 0.2112 | 0.0198 | 0.1683 | 49.4288 | 22.09534834 | 2.23706815 |

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|---|---|---|---|---|---|---|
| 7513.5 | 0.2091 | 0.0792 | 0.2832 | 37.9414 | 12.62734462 | 3.0047014 |
| 7514 | 0.2437 | 0.16 | 0.3507 | 10.1243 | 8.420478253 | 1.20234263 |
| 7514.5 | 0.3645 | 0.2209 | 0.3476 | 5.7738 | 5.710091411 | 1.01115719 |
| 7515 | 0.4772 | 0.2223 | 0.348 | 3.8625 | 4.159143058 | 0.92867688 |
| 7515.5 | 0.4528 | 0.1824 | 0.3447 | 2.8321 | 4.475949655 | 0.63273723 |
| 7516 | 0.3524 | 0.1118 | 0.3206 | 3.9769 | 6.44723933 | 0.61683766 |
| 7516.5 | 0.2981 | 0.06 | 0.2684 | 8.6835 | 9.33740862 | 0.92996894 |
| 7517 | 0.2981 | 0.0431 | 0.2127 | 15.0815 | 11.66451725 | 1.29293821 |
| 7517.5 | 0.2866 | 0.0455 | 0.1307 | 15.2205 | 18.01532715 | 0.84486392 |
| 7518 | 0.2347 | 0.0282 | 0.067 | 8.7813 | 36.184224 | 0.24268311 |
| 7518.5 | 0.1889 | 0.0002 | 0.047 | 9.3361 | 61.4102842 | 0.15202828 |
| 7519 | 0.1817 | -0.0136 | 0.0485 | 19.1767 | 64.72614528 | 0.2962744 |
| 7519.5 | 0.1885 | -0.0097 | 0.0382 | 38.867 | 66.89372984 | 0.58102606 |
| 7520 | 0.1891 | -0.0013 | 0.0249 | 62.996 | 75.72103952 | 0.83194843 |
| 7520.5 | 0.1871 | 0.002 | 0.0205 | 39.94 | 80.82903231 | 0.49412938 |
| 7521 | 0.1845 | -0.0018 | 0.0326 | 40.3475 | 73.41546599 | 0.54957766 |
| 7521.5 | 0.1823 | -0.002 | 0.0403 | 44.3605 | 69.57081423 | 0.63763089 |
| 7522 | 0.1828 | 0.003 | 0.0425 | 32.6013 | 67.79062188 | 0.48091165 |
| 7522.5 | 0.1862 | 0.0144 | 0.0396 | 23.9726 | 67.46829177 | 0.35531654 |
| 7523 | 0.1814 | 0.0215 | 0.0349 | 21.0459 | 74.00050157 | 0.28440213 |
| 7523.5 | 0.1604 | 0.0099 | 0.0327 | 22.2543 | 94.44398239 | 0.23563492 |
| 7524 | 0.1426 | -0.017 | 0.0371 | 26.118 | 110.2371088 | 0.23692566 |
| 7524.5 | 0.1408 | -0.0339 | 0.0456 | 28.0777 | 101.8937341 | 0.27555865 |
| 7525 | 0.1406 | -0.0321 | 0.0579 | 25.5488 | 89.00636836 | 0.28704463 |
| 7525.5 | 0.1365 | -0.0233 | 0.0669 | 22.8424 | 84.46010961 | 0.27045193 |
| 7526 | 0.1335 | -0.008 | 0.0637 | 21.8943 | 90.27267719 | 0.24253518 |
| 7526.5 | 0.1329 | 0.001 | 0.0612 | 22.0565 | 93.40094689 | 0.23614857 |
| 7527 | 0.1279 | 0.0073 | 0.053 | 22.7256 | 108.6708994 | 0.20912314 |
| 7527.5 | 0.1118 | 0.0035 | 0.047 | 24.7864 | 143.8061996 | 0.17235975 |
| 7528 | 0.0976 | 0.0027 | 0.0358 | 29.2322 | 209.1804758 | 0.13974631 |
| 7528.5 | 0.0982 | 0.001 | 0.0275 | 31.3447 | 237.7033668 | 0.13186477 |
| 7529 | 0.1082 | -0.0009 | 0.0287 | 28.3027 | 197.8512355 | 0.14305041 |
| 7529.5 | 0.1167 | 0.0038 | 0.0391 | 26.0733 | 149.8256448 | 0.17402428 |
| 7530 | 0.1203 | 0.01 | 0.0479 | 25.8565 | 127.0809049 | 0.20346487 |
| 7530.5 | 0.1216 | 0.0135 | 0.0559 | 27.652 | 113.1956433 | 0.24428502 |
| 7531 | 0.1235 | 0.0045 | 0.0656 | 32.2757 | 98.79145759 | 0.32670537 |
| 7531.5 | 0.1314 | -0.0039 | 0.0696 | 44.3253 | 86.64323451 | 0.51158409 |
| 7532 | 0.1696 | -0.0064 | 0.0684 | 79.1375 | 60.25120298 | 1.31345925 |
| 7532.5 | 0.2457 | -0.0119 | 0.0788 | 34.0213 | 30.93816653 | 1.09965469 |
| 7533 | 0.3042 | -0.015 | 0.1099 | 17.1528 | 18.31597047 | 0.93649419 |
| 7533.5 | 0.3106 | 0.001 | 0.1638 | 11.6235 | 13.67398557 | 0.85004478 |
| 7534 | 0.2893 | 0.0454 | 0.1894 | 14.0343 | 13.41126707 | 1.04645593 |
| 7534.5 | 0.2497 | 0.0857 | 0.1485 | 36.8743 | 19.92454811 | 1.85069693 |
| 7535 | 0.193 | 0.0781 | 0.1606 | 52.0642 | 25.72200564 | 2.02411121 |
| 7535.5 | 0.1753 | 0.0691 | 0.2672 | 56.7678 | 15.88154095 | 3.57445163 |
| 7536 | 0.2663 | 0.0832 | 0.3941 | 25.4992 | 6.714613067 | 3.79756804 |
| 7536.5 | 0.381 | 0.1003 | 0.4762 | 16.3269 | 3.83247677 | 4.26014324 |
| 7537 | 0.3826 | 0.087 | 0.5096 | 5.2274 | 3.516514476 | 1.48652879 |
| 7537.5 | 0.3246 | 0.0556 | 0.458 | 5.5721 | 4.66117616 | 1.19542789 |
| 7538 | 0.2934 | 0.0356 | 0.2921 | 14.1126 | 8.698078973 | 1.62249619 |
| 7538.5 | 0.2791 | 0.0318 | 0.1456 | 18.52 | 17.34719734 | 1.06760762 |
| 7539 | 0.2652 | 0.0339 | 0.098 | 25.6712 | 24.28245678 | 1.05719122 |

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|---|---|---|---|---|---|---|
| 7539.5 | 0.2364 | 0.0299 | 0.0955 | 19.954 | 29.47410236 | 0.67700111 |
| 7540 | 0.1976 | 0.0217 | 0.0674 | 25.6969 | 47.82197975 | 0.53734496 |
| 7540.5 | 0.1802 | 0.0124 | 0.0432 | 38.5411 | 69.03627774 | 0.55827315 |
| 7541 | 0.1849 | 0.0136 | 0.0362 | 35.8157 | 70.58954517 | 0.50737967 |
| 7541.5 | 0.1866 | 0.0165 | 0.0395 | 35.4994 | 67.27597045 | 0.52766835 |
| 7542 | 0.1809 | 0.0242 | 0.0369 | 38.878 | 72.9091018 | 0.53323932 |
| 7542.5 | 0.1749 | 0.0278 | 0.0452 | 47.5559 | 71.28088591 | 0.66716202 |
| 7543 | 0.1714 | 0.0141 | 0.1553 | 69.4601 | 30.49197402 | 2.27797977 |
| 7543.5 | 0.1678 | -0.0056 | 0.394 | 117.3405 | 9.506167234 | 12.3436183 |
| 7544 | 0.1581 | -0.0102 | 0.6554 | 123.0982 | 4.288816174 | 28.7021395 |
| 7544.5 | 0.1696 | -0.0012 | 0.7998 | 43.5713 | 2.941878261 | 14.810708 |
| 7545 | 0.3028 | 0.0065 | 0.832 | 15.0637 | 2.096667807 | 7.18459069 |
| 7545.5 | 0.4665 | 0.0058 | 0.8375 | 8.1857 | 1.555103714 | 5.26376468 |
| 7546 | 0.4274 | 0.008 | 0.8379 | 3.5009 | 1.65916714 | 2.11003456 |
| 7546.5 | 0.2972 | 0.0108 | 0.7877 | 3.045 | 2.309501802 | 1.31846617 |
| 7547 | 0.2559 | 0.0137 | 0.6136 | 4.8708 | 3.716863136 | 1.31045988 |
| 7547.5 | 0.2385 | 0.0147 | 0.3338 | 21.5739 | 9.135138296 | 2.36163912 |
| 7548 | 0.1952 | 0.0159 | 0.1244 | 24.3627 | 31.96698103 | 0.76212076 |
| 7548.5 | 0.1679 | 0.0266 | 0.0615 | 70.4851 | 65.21242361 | 1.08085386 |
| 7549 | 0.1808 | 0.0266 | 0.0834 | 102.5915 | 48.13385348 | 2.13137932 |
| 7549.5 | 0.2048 | 0.0123 | 0.088 | 67.0077 | 38.59031953 | 1.73638624 |
| 7550 | 0.2108 | 0.0057 | 0.0592 | 52.6158 | 45.93821196 | 1.14536021 |
| 7550.5 | 0.2093 | 0.024 | 0.0278 | 50.6888 | 60.74399332 | 0.83446605 |
| 7551 | 0.2094 | 0.0491 | 0.0064 | 53.6864 | 74.3696236 | 0.72188613 |
| 7551.5 | 0.2025 | 0.044 | -0.0002 | 65.178 | 85.45058342 | 0.76275664 |
| 7552 | 0.202 | 0.022 | 0.0024 | 86.5404 | 83.57420682 | 1.03549173 |
| 7552.5 | 0.2239 | 0.0121 | 0.0057 | 88.4478 | 65.0903535 | 1.35884651 |
| 7553 | 0.2516 | 0.0207 | 0.0022 | 55.629 | 52.47460788 | 1.06011273 |
| 7553.5 | 0.2664 | 0.0333 | -0.0021 | 52.2593 | 48.09470657 | 1.08659151 |
| 7554 | 0.2713 | 0.0334 | 0.0391 | 35.1013 | 34.03882014 | 1.03121377 |
| 7554.5 | 0.2733 | 0.0451 | 0.0946 | 23.6924 | 23.62039393 | 1.00304847 |
| 7555 | 0.2675 | 0.0741 | 0.1144 | 19.2522 | 21.79788789 | 0.88321401 |
| 7555.5 | 0.2508 | 0.1154 | 0.0814 | 28.6974 | 29.41690512 | 0.9755411 |
| 7556 | 0.237 | 0.1577 | 0.0848 | 44.8801 | 31.49895853 | 1.42481219 |
| 7556.5 | 0.2399 | 0.2201 | 0.1425 | 42.6757 | 21.7366559 | 1.96330568 |
| 7557 | 0.2727 | 0.299 | 0.1893 | 24.331 | 14.47524532 | 1.68086961 |
| 7557.5 | 0.3385 | 0.3332 | 0.2153 | 14.5176 | 9.803865278 | 1.4808037 |
| 7558 | 0.4017 | 0.3082 | 0.2543 | 7.7384 | 6.81181627 | 1.13602594 |
| 7558.5 | 0.4264 | 0.2484 | 0.3186 | 6.6949 | 5.181675282 | 1.29203388 |
| 7559 | 0.4034 | 0.1905 | 0.3247 | 8.5364 | 5.443716044 | 1.56812 |
| 7559.5 | 0.3454 | 0.1559 | 0.2421 | 13.8637 | 8.634541032 | 1.60560937 |
| 7560 | 0.2873 | 0.1378 | 0.2233 | 25.213 | 11.67434269 | 2.15969333 |
| 7560.5 | 0.2524 | 0.1415 | 0.3327 | 33.265 | 8.710868733 | 3.81879248 |
| 7561 | 0.2526 | 0.1595 | 0.4743 | 32.8217 | 5.463055872 | 6.00793782 |
| 7561.5 | 0.2936 | 0.1691 | 0.5525 | 20.8812 | 3.941391138 | 5.29792636 |
| 7562 | 0.3754 | 0.1611 | 0.5888 | 15.4954 | 2.976095456 | 5.20662063 |
| 7562.5 | 0.4536 | 0.1505 | 0.6104 | 23.5601 | 2.408139715 | 9.78352703 |
| 7563 | 0.4569 | 0.1371 | 0.6263 | 41.3998 | 2.317301698 | 17.8655201 |
| 7563.5 | 0.3878 | 0.1263 | 0.5636 | 108.2246 | 3.062847784 | 35.3346322 |
| 7564 | 0.2906 | 0.1073 | 0.3968 | 410.9477 | 6.160354371 | 66.7084514 |
| 7564.5 | 0.213 | 0.0752 | 0.2457 | 789.6108 | 14.70006953 | 53.7147663 |
| 7565 | 0.1968 | 0.0313 | 0.3122 | 184.8658 | 11.75338462 | 15.7287289 |

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|---|---|---|---|---|---|---|
| 7565.5 | 0.2439 | 0.0196 | 0.5262 | 45.6465 | 4.825361612 | 9.45970555 |
| 7566 | 0.3239 | 0.0451 | 0.6792 | 16.2344 | 2.733481159 | 5.93909343 |
| 7566.5 | 0.4121 | 0.0692 | 0.7162 | 8.3815 | 2.122722952 | 3.94846628 |
| 7567 | 0.4748 | 0.081 | 0.6531 | 4.3637 | 2.124341813 | 2.05414212 |
| 7567.5 | 0.4655 | 0.0908 | 0.4847 | 3.691 | 3.071170122 | 1.20182206 |
| 7568 | 0.3899 | 0.0881 | 0.2586 | 3.7079 | 6.982319576 | 0.53104129 |
| 7568.5 | 0.297 | 0.0651 | 0.09 | 4.2732 | 21.18495791 | 0.20170916 |
| 7569 | 0.2285 | 0.0278 | 0.0253 | 7.2612 | 52.47460788 | 0.1383755 |
| 7569.5 | 0.186 | 0.0018 | 0.0159 | 14.0854 | 85.8149778 | 0.16413685 |
| 7570 | 0.1544 | -0.0148 | 0.0193 | 30.8229 | 118.5868602 | 0.25991834 |
| 7570.5 | 0.1313 | -0.0284 | 0.0245 | 39.3641 | 149.8256448 | 0.26273273 |
| 7571 | 0.1115 | -0.0286 | 0.0182 | 23.1516 | 222.2210686 | 0.10418274 |
| 7571.5 | 0.1042 | -0.0146 | 0.0427 | 11.5274 | 170.0236437 | 0.06779881 |
| 7572 | 0.1334 | 0.0087 | 0.1625 | 8.9358 | 37.72632529 | 0.23685848 |
| 7572.5 | 0.21 | 0.0354 | 0.3774 | 8.2256 | 8.637701754 | 0.95229035 |
| 7573 | 0.32 | 0.0642 | 0.5714 | 7.7338 | 3.523303264 | 2.19504238 |
| 7573.5 | 0.4204 | 0.0942 | 0.6158 | 7.2522 | 2.549191526 | 2.84490197 |
| 7574 | 0.4564 | 0.1066 | 0.5199 | 7.3634 | 2.897357652 | 2.54141907 |
| 7574.5 | 0.4206 | 0.0982 | 0.37 | 9.8298 | 4.560359065 | 2.15548817 |
| 7575 | 0.36 | 0.0918 | 0.2651 | 23.7495 | 7.556396837 | 3.14296622 |
| 7575.5 | 0.3015 | 0.0978 | 0.2029 | 41.7326 | 11.98504759 | 3.48205543 |
| 7576 | 0.2487 | 0.0899 | 0.1411 | 130.5751 | 20.85913214 | 6.25985296 |
| 7576.5 | 0.2049 | 0.0592 | 0.0873 | 572.8787 | 38.76088864 | 14.7798134 |
| 7577 | 0.173 | 0.0377 | 0.0559 | 1649.177 | 65.51907025 | 25.1709478 |
| 7577.5 | 0.1564 | 0.0229 | 0.0494 | 791.0634 | 82.35664263 | 9.60533813 |
| 7578 | 0.1498 | 0.0032 | 0.05 | 330.8206 | 87.76591599 | 3.76935165 |
| 7578.5 | 0.1512 | -0.0101 | 0.0493 | 178.8336 | 87.10844673 | 2.05299953 |
| 7579 | 0.161 | -0.0086 | 0.0414 | 116.836 | 85.35983907 | 1.36874672 |
| 7579.5 | 0.1685 | -0.0005 | 0.0359 | 85.6506 | 83.57420682 | 1.0248449 |
| 7580 | 0.1589 | 0.0041 | 0.0284 | 66.1764 | 100.8439756 | 0.65622562 |
| 7580.5 | 0.1353 | 0.0074 | 0.0201 | 53.3244 | 150.6560231 | 0.35394801 |
| 7581 | 0.1128 | 0.008 | 0.009 | 49.3712 | 254.3691919 | 0.19409269 |
| 7581.5 | 0.0992 | -0.0001 | 0.006 | 46.8451 | 348.5558207 | 0.1343977 |
| 7582 | 0.0952 | -0.0072 | 0.0107 | 37.0012 | 343.6211334 | 0.10768022 |
| 7582.5 | 0.1015 | -0.0072 | 0.0222 | 28.2369 | 246.0431769 | 0.114764 |
| 7583 | 0.1146 | -0.0031 | 0.0314 | 24.7172 | 172.285029 | 0.14346691 |
| 7583.5 | 0.1234 | 0.0046 | 0.0278 | 24.1562 | 159.7974443 | 0.15116762 |
| 7584 | 0.1258 | -0.0003 | 0.0321 | 24.797 | 145.5742632 | 0.17033918 |
| 7584.5 | 0.1286 | -0.0032 | 0.0429 | 25.812 | 121.8816466 | 0.21177922 |
| 7585 | 0.132 | 0.0021 | 0.0508 | 26.8745 | 106.2569556 | 0.25291991 |
| 7585.5 | 0.1353 | 0.0123 | 0.0528 | 27.9069 | 99.92410562 | 0.27928096 |
| 7586 | 0.138 | 0.0187 | 0.0464 | 28.3031 | 104.2846071 | 0.27140247 |
| 7586.5 | 0.1397 | 0.0156 | 0.0447 | 28.4374 | 104.2846071 | 0.27269029 |
| 7587 | 0.1418 | 0.0077 | 0.046 | 30.2996 | 100.2676107 | 0.30218731 |
| 7587.5 | 0.1415 | 0.0009 | 0.051 | 33.3796 | 95.07801419 | 0.35107591 |
| 7588 | 0.1398 | -0.0025 | 0.0551 | 35.4895 | 92.57862496 | 0.38334443 |
| 7588.5 | 0.1398 | 0.0032 | 0.0528 | 36.4099 | 94.97190998 | 0.38337546 |
| 7589 | 0.1392 | 0.0059 | 0.055 | 37.0803 | 93.29757275 | 0.39744121 |
| 7589.5 | 0.1374 | 0.0034 | 0.06 | 37.745 | 90.07614913 | 0.41903434 |
| 7590 | 0.1375 | -0.0002 | 0.0638 | 38.6779 | 86.36585249 | 0.44783788 |
| 7590.5 | 0.1421 | 0.0014 | 0.0592 | 40.7808 | 86.36585249 | 0.47218662 |
| 7591 | 0.1481 | 0.0026 | 0.0568 | 43.4428 | 83.1363531 | 0.52254878 |

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|---|---|---|---|---|---|---|
| 7591.5 | 0.1501 | -0.0037 | 0.0611 | 40.5435 | 77.89584008 | 0.52048351 |
| 7592 | 0.1501 | -0.0099 | 0.0658 | 30.6438 | 74.29558372 | 0.41245789 |
| 7592.5 | 0.1516 | -0.0008 | 0.0563 | 22.0474 | 80.57847208 | 0.27361402 |
| 7593 | 0.1539 | 0.0067 | 0.053 | 17.9055 | 81.41813036 | 0.2199203 |
| 7593.5 | 0.1519 | 0.0065 | 0.0642 | 16.8163 | 74.14782758 | 0.22679424 |
| 7594 | 0.1414 | 0.0059 | 0.078 | 17.7219 | 71.77074266 | 0.24692374 |
| 7594.5 | 0.1315 | 0.0001 | 0.088 | 19.1123 | 71.70046172 | 0.26655756 |
| 7595 | 0.1299 | -0.0051 | 0.0904 | 19.6311 | 71.14182653 | 0.27594315 |
| 7595.5 | 0.1307 | -0.0068 | 0.0927 | 19.9502 | 69.03627774 | 0.2889814 |
| 7596 | 0.1302 | 0.0016 | 0.0884 | 20.7744 | 72.33664153 | 0.28719055 |
| 7596.5 | 0.1307 | 0.0092 | 0.0859 | 21.4167 | 73.78031545 | 0.29027661 |
| 7597 | 0.1318 | 0.011 | 0.0826 | 21.329 | 75.41763354 | 0.28281184 |
| 7597.5 | 0.1321 | 0.0021 | 0.0861 | 21.0262 | 72.62204525 | 0.28952916 |
| 7598 | 0.131 | -0.0124 | 0.0921 | 21.4791 | 69.23602149 | 0.31023013 |
| 7598.5 | 0.1274 | -0.0202 | 0.0956 | 23.694 | 69.30279092 | 0.34189099 |
| 7599 | 0.1221 | -0.0114 | 0.0904 | 27.4471 | 76.87488361 | 0.35703599 |
| 7599.5 | 0.1207 | -0.0001 | 0.0842 | 30.5958 | 83.1363531 | 0.36801951 |
| 7600 | 0.1327 | 0.0021 | 0.0723 | 30.8856 | 83.04918577 | 0.37189528 |
| 7600.5 | 0.1582 | -0.0085 | 0.0663 | 29.4371 | 68.31106208 | 0.43092728 |
| 7601 | 0.1848 | -0.0144 | 0.0604 | 27.895 | 56.5115447 | 0.49361595 |
| 7601.5 | 0.193 | -0.0053 | 0.0542 | 27.1046 | 55.53310765 | 0.48808001 |
| 7602 | 0.1728 | 0.0051 | 0.0457 | 28.8555 | 72.40783819 | 0.39851349 |
| 7602.5 | 0.1373 | 0.0033 | 0.0356 | 36.4232 | 119.7696953 | 0.30411032 |
| 7603 | 0.1038 | -0.0095 | 0.0295 | 54.9823 | 209.5180092 | 0.26242279 |
| 7603.5 | 0.081 | -0.0163 | 0.0275 | 85.5914 | 326.16116 | 0.26242058 |
| 7604 | 0.0694 | -0.0147 | 0.0271 | 103.5321 | 419.6357274 | 0.24671898 |
| 7604.5 | 0.0639 | -0.012 | 0.0352 | 103.5178 | 396.3216734 | 0.26119641 |
| 7605 | 0.0589 | -0.0129 | 0.0483 | 104.6732 | 334.7244153 | 0.31271457 |
| 7605.5 | 0.0543 | -0.0154 | 0.0598 | 107.6243 | 292.7130228 | 0.36767855 |
| 7606 | 0.0542 | -0.0063 | 0.0596 | 102.3953 | 294.3745881 | 0.34784015 |
| 7606.5 | 0.0595 | 0.0051 | 0.0512 | 86.0853 | 312.3840098 | 0.27557524 |
| 7607 | 0.0655 | 0.0048 | 0.0496 | 74.0638 | 287.2726194 | 0.25781712 |
| 7607.5 | 0.0669 | -0.0126 | 0.0633 | 74.8441 | 220.3903447 | 0.33959791 |
| 7608 | 0.0627 | -0.0228 | 0.0737 | 82.9792 | 199.4138342 | 0.41611556 |
| 7608.5 | 0.0575 | -0.019 | 0.0752 | 83.7747 | 211.5600671 | 0.39598541 |
| 7609 | 0.0553 | -0.0139 | 0.0743 | 76.5309 | 222.5898859 | 0.3438202 |
| 7609.5 | 0.0541 | -0.0183 | 0.075 | 69.4428 | 224.4474932 | 0.30939441 |
| 7610 | 0.0541 | -0.0241 | 0.0743 | 65.4279 | 227.0865326 | 0.2881188 |
| 7610.5 | 0.057 | -0.0305 | 0.0764 | 63.7426 | 209.1804758 | 0.30472538 |
| 7611 | 0.0598 | -0.0308 | 0.08 | 60.3639 | 189.1323251 | 0.31916226 |
| 7611.5 | 0.0602 | -0.0209 | 0.0806 | 52.802 | 186.256086 | 0.28349141 |
| 7612 | 0.0585 | -0.0096 | 0.0815 | 44.9862 | 188.5518958 | 0.2385879 |
| 7612.5 | 0.0574 | -0.0002 | 0.0798 | 41.2986 | 196.9222733 | 0.20972031 |
| 7613 | 0.0579 | -0.0045 | 0.085 | 41.8058 | 180.420918 | 0.2317126 |
| 7613.5 | 0.0585 | -0.0084 | 0.083 | 45.4446 | 184.280692 | 0.24660533 |
| 7614 | 0.0598 | -0.0031 | 0.0763 | 50.11 | 200.3600867 | 0.25009971 |
| 7614.5 | 0.0612 | 0.0052 | 0.0676 | 54.3921 | 225.5729788 | 0.24112862 |
| 7615 | 0.0592 | 0.0076 | 0.0703 | 61.4346 | 222.9596008 | 0.2755414 |
| 7615.5 | 0.055 | -0.0009 | 0.0836 | 73.0001 | 192.6705047 | 0.3788857 |
| 7616 | 0.0514 | -0.0026 | 0.0917 | 83.175 | 179.8792084 | 0.46239363 |
| 7616.5 | 0.0496 | 0.003 | 0.0908 | 80.6338 | 187.3988401 | 0.43027908 |
| 7617 | 0.0516 | 0.003 | 0.0925 | 69.5678 | 177.2060812 | 0.39258134 |

0.25 to 0.36

0.21 to 0.14

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|---|---|---|---|---|---|---|
| 7617.5 | 0.0561 | -0.0039 | 0.094 | 58.1962 | 162.3258523 | 0.35851467 |
| 7618 | 0.0609 | -0.0091 | 0.0951 | 49.0007 | 149.4129683 | 0.3279548 |
| 7618.5 | 0.0654 | -0.0156 | 0.1057 | 44.006 | 122.4950839 | 0.35924707 |
| 7619 | 0.067 | -0.0152 | 0.1139 | 45.385 | 108.6708994 | 0.41763711 |
| 7619.5 | 0.0645 | -0.0145 | 0.1179 | 53.2495 | 106.7585796 | 0.49878427 |
| 7620 | 0.0606 | -0.0072 | 0.1103 | 64.8433 | 122.8035002 | 0.52802485 |
| 7620.5 | 0.0578 | -0.0098 | 0.1108 | 75.7102 | 126.4335709 | 0.59881406 |
| 7621 | 0.0562 | -0.0193 | 0.116 | 82.7669 | 120.8189102 | 0.68504922 |
| 7621.5 | 0.0559 | -0.0285 | 0.1199 | 85.3147 | 115.5621486 | 0.73825817 |
| 7622 | 0.0567 | -0.0265 | 0.1143 | 84.4675 | 122.64915 | 0.68869209 |
| 7622.5 | 0.0573 | -0.0101 | 0.1017 | 80.1305 | 143.417571 | 0.55872164 |
| 7623 | 0.056 | 0.0082 | 0.0849 | 76.0178 | 185.9719929 | 0.4087594 |
| 7623.5 | 0.052 | 0.0164 | 0.077 | 80.2529 | 224.8217391 | 0.35696237 |
| 7624 | 0.047 | 0.0128 | 0.0761 | 96.3649 | 248.6287614 | 0.38758549 |
| 7624.5 | 0.0434 | -0.0029 | 0.0885 | 113.1381 | 214.328473 | 0.52787247 |
| 7625 | 0.0422 | -0.0123 | 0.0959 | 117.2336 | 194.1734161 | 0.60375721 |
| 7625.5 | 0.0428 | -0.0109 | 0.0948 | 114.9611 | 195.693566 | 0.58745467 |
| 7626 | 0.0446 | 0.0002 | 0.0902 | 103.5179 | 204.5374852 | 0.50610723 |
| 7626.5 | 0.048 | 0.0152 | 0.083 | 77.5083 | 217.5068278 | 0.35634881 |
| 7627 | 0.0526 | 0.0205 | 0.0821 | 58.6595 | 204.8640949 | 0.28633373 |
| 7627.5 | 0.0587 | 0.01 | 0.0889 | 55.8243 | 168.294728 | 0.33170558 |
| 7628 | 0.0705 | -0.0014 | 0.1034 | 64.1159 | 118.2938261 | 0.54200546 |
| 7628.5 | 0.0859 | -0.0044 | 0.1161 | 61.3067 | 85.72366607 | 0.71516657 |
| 7629 | 0.0933 | -0.0075 | 0.1197 | 46.2673 | 76.48742367 | 0.60490075 |
| 7629.5 | 0.0853 | -0.0123 | 0.1145 | 40.3888 | 87.76591599 | 0.46018776 |
| 7630 | 0.0698 | -0.0157 | 0.1054 | 44.9994 | 116.4147102 | 0.38654393 |
| 7630.5 | 0.0579 | -0.0173 | 0.1036 | 56.3605 | 138.6868384 | 0.4063868 |
| 7631 | 0.0505 | -0.0143 | 0.1052 | 69.3292 | 150.0326096 | 0.46209421 |
| 7631.5 | 0.0466 | -0.0156 | 0.1084 | 84.9132 | 151.4931616 | 0.56050847 |
| 7632 | 0.0461 | -0.01 | 0.0993 | 107.8512 | 173.8171826 | 0.62048641 |
| 7632.5 | 0.0488 | -0.0102 | 0.0887 | 122.2274 | 195.9996876 | 0.62361018 |
| 7633 | 0.0539 | -0.0175 | 0.0834 | 104.0839 | 196.6140391 | 0.52938183 |
| 7633.5 | 0.0587 | -0.0185 | 0.0829 | 70.1954 | 184.0010009 | 0.38149466 |
| 7634 | 0.0615 | -0.0086 | 0.0837 | 47.719 | 174.3323382 | 0.27372432 |
| 7634.5 | 0.064 | 0.0059 | 0.0877 | 38.239 | 158.6672086 | 0.24100128 |
| 7635 | 0.0679 | 0.0118 | 0.0943 | 35.0081 | 137.4032018 | 0.25478373 |
| 7635.5 | 0.072 | 0.0049 | 0.108 | 34.0127 | 109.842471 | 0.30964981 |
| 7636 | 0.0734 | -0.0055 | 0.1161 | 33.6499 | 98.34366052 | 0.34216644 |
| 7636.5 | 0.0703 | -0.0076 | 0.115 | 33.855 | 103.198653 | 0.32805661 |
| 7637 | 0.0656 | 0.0023 | 0.1066 | 35.2401 | 120.8189102 | 0.29167702 |
| 7637.5 | 0.063 | 0.0069 | 0.1058 | 36.8933 | 126.1117143 | 0.29254459 |
| 7638 | 0.0619 | 0.0044 | 0.1093 | 37.1862 | 122.3413013 | 0.30395459 |
| 7638.5 | 0.0622 | 0.0035 | 0.1089 | 36.5765 | 122.4950839 | 0.29859566 |
| 7639 | 0.0634 | 0.0044 | 0.1041 | 36.9394 | 128.2254807 | 0.28808159 |
| 7639.5 | 0.0647 | -0.0029 | 0.1056 | 39.5769 | 123.7356053 | 0.31985054 |
| 7640 | 0.0667 | -0.0059 | 0.1026 | 43.5544 | 125.3123055 | 0.34756682 |
| 7640.5 | 0.0708 | -0.0042 | 0.0999 | 46.7036 | 123.1130554 | 0.37935538 |
| 7641 | 0.0785 | -0.0015 | 0.0961 | 47.5139 | 117.2765187 | 0.40514419 |
| 7641.5 | 0.0892 | 0.0003 | 0.0936 | 42.6457 | 106.2569556 | 0.40134502 |
| 7642 | 0.1017 | 0.0142 | 0.0892 | 33.3009 | 96.79957134 | 0.34401909 |
| 7642.5 | 0.1132 | 0.0237 | 0.0946 | 27.0377 | 80.66186557 | 0.33519805 |
| 7643 | 0.1149 | 0.0187 | 0.1046 | 25.923 | 71.70046172 | 0.36154579 |

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|---|---|---|---|---|---|---|
| 7643.5 | 0.1046 | 0.0108 | 0.1075 | 28.0008 | 77.18692556 | 0.3627661 |
| 7644 | 0.0938 | 0.0077 | 0.1094 | 28.5102 | 84.63894033 | 0.33684495 |
| 7644.5 | 0.0919 | 0.0113 | 0.1109 | 26.2307 | 84.99826996 | 0.30860275 |
| 7645 | 0.096 | 0.0109 | 0.1107 | 24.1262 | 81.58759951 | 0.29570915 |
| 7645.5 | 0.0993 | 0.0072 | 0.1102 | 23.3242 | 79.26117779 | 0.29427017 |
| 7646 | 0.1 | 0.0049 | 0.107 | 23.3789 | 81.33358912 | 0.28744459 |
| 7646.5 | 0.0978 | 0 | 0.1089 | 23.6357 | 81.58759951 | 0.28969721 |
| 7647 | 0.0934 | -0.0101 | 0.1106 | 24.0032 | 83.92692673 | 0.28600118 |
| 7647.5 | 0.0888 | -0.0172 | 0.108 | 24.5172 | 90.66762253 | 0.27040744 |
| 7648 | 0.0847 | -0.0103 | 0.1029 | 25.2731 | 100.4975761 | 0.2514797 |
| 7648.5 | 0.0829 | 0.0057 | 0.0992 | 26.4847 | 107.1370778 | 0.24720387 |
| 7649 | 0.0841 | 0.0183 | 0.0946 | 27.9854 | 111.5676775 | 0.25083788 |
| 7649.5 | 0.0884 | 0.0221 | 0.0918 | 29.1516 | 109.580528 | 0.26602902 |
| 7650 | 0.0952 | 0.0163 | 0.0925 | 29.177 | 100.3824969 | 0.29065824 |
| 7650.5 | 0.0999 | 0.0115 | 0.0955 | 28.5557 | 92.07004968 | 0.31015189 |
| 7651 | 0.099 | 0.0081 | 0.0946 | 28.9677 | 93.92034329 | 0.30842839 |
| 7651.5 | 0.094 | -0.0029 | 0.0996 | 30.7157 | 93.92034329 | 0.3270399 |
| 7652 | 0.0864 | -0.008 | 0.1058 | 33.2652 | 95.39737091 | 0.34870143 |
| 7652.5 | 0.0767 | -0.0064 | 0.111 | 36.1071 | 100.3824969 | 0.35969518 |
| 7653 | 0.0676 | 0.0016 | 0.1077 | 39.7354 | 116.271978 | 0.34174528 |
| 7653.5 | 0.0627 | 0.0075 | 0.0938 | 46.0889 | 148.3885343 | 0.3105961 |
| 7654 | 0.0675 | 0.0122 | 0.0722 | 59.2169 | 189.4235219 | 0.3126164 |
| 7654.5 | 0.092 | 0.009 | 0.0504 | 76.4214 | 181.7856943 | 0.42039282 |
| 7655 | 0.1504 | 0.0126 | 0.0347 | 58.7009 | 103.4385395 | 0.56749545 |
| 7655.5 | 0.2338 | 0.0447 | 0.0505 | 58.658 | 41.11364029 | 1.42672844 |
| 7656 | 0.2992 | 0.0983 | 0.0977 | 24.065 | 20.06512259 | 1.19934478 |
| 7656.5 | 0.3243 | 0.1273 | 0.1296 | 13.1497 | 15.03632788 | 0.87452868 |
| 7657 | 0.3291 | 0.0942 | 0.1143 | 13.9244 | 15.8123147 | 0.88060479 |
| 7657.5 | 0.3325 | 0.0523 | 0.057 | 27.5129 | 20.89368952 | 1.31680429 |
| 7658 | 0.3116 | 0.0324 | 0.0162 | 130.7787 | 30.272406 | 4.32006296 |
| 7658.5 | 0.2573 | 0.0205 | 0.0075 | 70.025 | 47.89967001 | 1.46190986 |
| 7659 | 0.2193 | 0.0053 | 0.0098 | 50.8659 | 65.3961586 | 0.77781174 |
| 7659.5 | 0.2173 | -0.0059 | 0.0103 | 41.8312 | 66.32630842 | 0.6306879 |
| 7660 | 0.2188 | -0.0037 | 0.0134 | 44.6285 | 63.53344678 | 0.70244103 |
| 7660.5 | 0.2125 | 0.0089 | 0.0157 | 42.0116 | 65.95193681 | 0.63700328 |
| 7661 | 0.21 | 0.0202 | 0.017 | 36.812 | 66.70380178 | 0.55187259 |
| 7661.5 | 0.2104 | 0.0182 | 0.0149 | 46.117 | 67.79062188 | 0.68028584 |
| 7662 | 0.2022 | 0.0096 | 0.0156 | 52.7925 | 72.9091018 | 0.72408655 |
| 7662.5 | 0.1915 | -0.0007 | 0.0213 | 37.5028 | 76.64206355 | 0.48932399 |
| 7663 | 0.1756 | -0.0086 | 0.0271 | 23.8089 | 85.08845157 | 0.27981353 |
| 7663.5 | 0.1418 | -0.0155 | 0.0332 | 24.2295 | 116.7009457 | 0.20762043 |
| 7664 | 0.1165 | -0.0164 | 0.0423 | 38.522 | 143.8061996 | 0.2678744 |
| 7664.5 | 0.1124 | -0.0133 | 0.0438 | 73.9746 | 149.001955 | 0.49646731 |
| 7665 | 0.1117 | -0.012 | 0.0389 | 92.7915 | 161.1693635 | 0.57573907 |
| 7665.5 | 0.1139 | -0.0105 | 0.0279 | 144.897 | 183.4434814 | 0.78987271 |
| 7666 | 0.132 | -0.0084 | 0.0341 | 107.1586 | 130.5603995 | 0.82075882 |
| 7666.5 | 0.1772 | 0.0036 | 0.0941 | 42.8174 | 45.46624874 | 0.94174033 |
| 7667 | 0.234 | 0.0198 | 0.2115 | 23.0023 | 15.65249621 | 1.46956113 |
| 7667.5 | 0.2799 | 0.0306 | 0.2821 | 9.4396 | 9.498895321 | 0.99375766 |
| 7668 | 0.2946 | 0.0258 | 0.2243 | 8.5446 | 11.27655099 | 0.75773169 |
| 7668.5 | 0.2548 | 0.0093 | 0.1133 | 20.5158 | 23.59281013 | 0.86957848 |
| 7669 | 0.1875 | 0.0017 | 0.0372 | 37.0315 | 68.18040466 | 0.54313993 |

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|---|---|---|---|---|---|---|
| 7669.5 | 0.142 | -0.0003 | 0.0124 | 91.9453 | 152.7617039 | 0.60188711 |
| 7670 | 0.1303 | 0.0023 | 0 | 140.7641 | 220.0268526 | 0.63975873 |
| 7670.5 | 0.1358 | -0.0072 | 0.0064 | 100.289 | 182.3358424 | 0.55002351 |
| 7671 | 0.1433 | -0.0118 | 0.0177 | 55.5796 | 139.6145069 | 0.3980933 |
| 7671.5 | 0.1476 | -0.0113 | 0.0229 | 51.654 | 123.4237553 | 0.41850939 |
| 7672 | 0.1448 | -0.0109 | 0.0214 | 58.0532 | 130.3915621 | 0.44522206 |
| 7672.5 | 0.1387 | -0.009 | 0.0161 | 72.2057 | 151.9142885 | 0.47530552 |
| 7673 | 0.1423 | -0.0048 | 0.0122 | 96.7581 | 152.549202 | 0.6342747 |
| 7673.5 | 0.1599 | 0.0054 | 0.007 | 111.6269 | 129.2186074 | 0.86386088 |
| 7674 | 0.1797 | 0.0158 | 0.0028 | 58.8989 | 106.6328489 | 0.55235231 |
| 7674.5 | 0.1942 | 0.0296 | 0.0102 | 33.7902 | 83.57420682 | 0.40431374 |
| 7675 | 0.2068 | 0.0205 | 0.0367 | 21.2211 | 57.36320447 | 0.36994272 |
| 7675.5 | 0.2125 | 0.0162 | 0.053 | 20.3961 | 47.62855992 | 0.42823256 |
| 7676 | 0.1959 | 0.0308 | 0.052 | 24.7674 | 55.19651367 | 0.44871312 |
| 7676.5 | 0.1585 | 0.0713 | 0.0342 | 28.4387 | 94.86597916 | 0.29977765 |
| 7677 | 0.1273 | 0.1114 | 0.0142 | 33.944 | 184.280692 | 0.18419727 |
| 7677.5 | 0.1184 | 0.1253 | -0.0033 | 62.0789 | 287.2726194 | 0.21609752 |
| 7678 | 0.1222 | 0.1037 | 0.0074 | 112.1908 | 222.5898859 | 0.5040247 |
| 7678.5 | 0.1331 | 0.0791 | 0.0743 | 224.5474 | 80.99670713 | 2.77230283 |
| 7679 | 0.1637 | 0.0795 | 0.2059 | 264.8932 | 23.38742785 | 11.3263075 |
| 7679.5 | 0.2309 | 0.0971 | 0.3671 | 147.6399 | 8.311867942 | 17.7625416 |
| 7680 | 0.3355 | 0.1163 | 0.4684 | 59.0586 | 4.399687378 | 13.4233628 |
| 7680.5 | 0.4469 | 0.1174 | 0.5169 | 45.0672 | 2.978751664 | 15.1295593 |
| 7681 | 0.5057 | 0.109 | 0.5443 | 12.9171 | 2.477702661 | 5.21333742 |
| 7681.5 | 0.499 | 0.1144 | 0.4987 | 7.3552 | 2.765389057 | 2.65973425 |
| 7682 | 0.4923 | 0.1188 | 0.3373 | 8.4304 | 4.111860591 | 2.05026406 |
| 7682.5 | 0.4672 | 0.1127 | 0.1375 | 34.5845 | 8.115125633 | 4.26173316 |
| 7683 | 0.3747 | 0.1246 | 0.025 | 38.9177 | 19.76413271 | 1.9691074 |
| 7683.5 | 0.2905 | 0.2161 | -0.0164 | 66.5898 | 44.47354553 | 1.49729011 |
| 7684 | 0.2307 | 0.3307 | -0.0248 | 43.6521 | 82.27067015 | 0.53059128 |
| 7684.5 | 0.1708 | 0.3494 | 0.0256 | 22.3813 | 91.0651046 | 0.24577252 |
| 7685 | 0.1529 | 0.2577 | 0.096 | 11.9223 | 54.72082702 | 0.217875 |
| 7685.5 | 0.1623 | 0.1257 | 0.1153 | 14.9803 | 43.27671998 | 0.34615146 |
| 7686 | 0.1573 | 0.0386 | 0.0823 | 36.4607 | 59.38948109 | 0.61392522 |
| 7686.5 | 0.1351 | 0.0114 | 0.049 | 187.1631 | 104.6503138 | 1.78846191 |
| 7687 | 0.1172 | 0.0223 | 0.0278 | 82.4157 | 174.8497338 | 0.47135159 |
| 7687.5 | 0.1169 | 0.024 | 0.02 | 45.7483 | 197.8512355 | 0.23122575 |
| 7688 | 0.1234 | 0.0081 | 0.0224 | 44.6497 | 172.7935406 | 0.25839913 |
| 7688.5 | 0.1244 | -0.0088 | 0.0296 | 55.2079 | 153.616063 | 0.35938885 |
| 7689 | 0.1222 | -0.0083 | 0.0273 | 66.0922 | 163.7297565 | 0.40366639 |
| 7689.5 | 0.1336 | 0.0035 | 0.0112 | 70.8856 | 175.3693823 | 0.40420739 |
| 7690 | 0.1589 | 0.0095 | -0.0021 | 67.6257 | 147.7788065 | 0.45761433 |
| 7690.5 | 0.178 | 0.0016 | 0.0052 | 57.8095 | 105.7587773 | 0.54661657 |
| 7691 | 0.1796 | -0.0046 | 0.0171 | 50.9262 | 90.76675439 | 0.56106666 |
| 7691.5 | 0.1691 | -0.0065 | 0.0236 | 56.0637 | 94.86597916 | 0.59097793 |
| 7692 | 0.1578 | -0.004 | 0.0224 | 81.3672 | 109.580528 | 0.74253338 |
| 7692.5 | 0.1603 | -0.0048 | 0.0204 | 99.3908 | 108.929661 | 0.912431 |
| 7693 | 0.1844 | -0.0077 | 0.0228 | 65.1197 | 81.16489205 | 0.80231364 |
| 7693.5 | 0.2084 | -0.0126 | 0.0307 | 43.6599 | 59.65681889 | 0.73185096 |
| 7694 | 0.2064 | -0.0146 | 0.0384 | 37.2374 | 56.71026037 | 0.65662545 |
| 7694.5 | 0.1835 | -0.0133 | 0.0394 | 42.5257 | 69.36965473 | 0.6130303 |
| 7695 | 0.1607 | -0.0064 | 0.0285 | 63.3809 | 98.67922869 | 0.64229221 |

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|---|---|---|---|---|---|---|
| 7695.5 | 0.1545 | -0.0085 | 0.0198 | 96.9424 | 117.7109319 | 0.82356327 |
| 7696 | 0.1696 | -0.0241 | 0.0254 | 89.5797 | 92.47658119 | 0.96867443 |
| 7696.5 | 0.2006 | -0.0414 | 0.041 | 58.4667 | 58.33749555 | 1.00221478 |
| 7697 | 0.2221 | -0.0436 | 0.0437 | 43.5685 | 47.51305772 | 0.9169795 |
| 7697.5 | 0.218 | -0.0271 | 0.0246 | 42.0493 | 57.82171485 | 0.72722333 |
| 7698 | 0.214 | -0.0205 | 0.0152 | 50.8614 | 65.33482943 | 0.77847299 |
| 7698.5 | 0.2243 | -0.0234 | 0.0252 | 62.8565 | 54.43829288 | 1.1546376 |
| 7699 | 0.2458 | -0.0298 | 0.0711 | 66.1156 | 32.55542475 | 2.03086277 |
| 7699.5 | 0.282 | -0.0218 | 0.128 | 64.1222 | 18.71202927 | 3.42679028 |
| 7700 | 0.3127 | -0.0104 | 0.161 | 62.2745 | 13.71746633 | 4.53979609 |

**From:** Chris Kierst
**To:** Tracey Fallang
**Subject:** Re: SWD Applications

Thank you for sending the supplemental information. I now have sufficient information to have the wells noticed. I will start the Noticing process by ordering the drafting of the initial Noticing paperwork today. I am going to try to generate an Rweq to attempt to corroborate the water analysis information from the surrounding non UIC wells with the information in the permit subject well logs. After the Noticing period is over we will issue a Letter of Approval to Convert the well to a Class II UIC well. However, we will require an acceptable Step Rate Test before we will issue a final Permit to Inject. As always, please feel free to contact me if you have any questions.

>>> "Tracey Fallang" <tfallang@billbarrettcorp.com> 04/18/2007 3:46 PM >>>
Chris, just following up on your request for information and our response. At this time, do you need anything further from us and can you advise if/when the public comment period will begin?

Thank you.

Tracey Fallang

Bill Barrett Corporation

1099 18th Street, Suite 2300

Denver, CO 80202

Phone: 303-312-8134

Cell: 303-596-4818

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**To:** Tracey Fallang
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Tracey Fallang

Bill Barrett Corporation

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Denver, CO 80202

Phone: 303-312-8134

Cell: 303-596-4818

# UIC INJECTION PERMIT APPLICATION ANALYSIS FORM
WELL NAME: Prickly Pear Unit Federal 12-24
API #: 4300730953

| R649-5-2. Requirements For Class II Injection Wells Including Water Disposal, Storage And Enhanced Recovery Wells. | **Completed Items, Needed Items, & Comments** |
|---|---|
| 1. Injection wells shall be completed, equipped, operated, and maintained in a manner that will prevent pollution and damage to any USDW, or other resources and will confine injected fluids to the interval approved. | 1. O.K. |
| 2. The application for an injection well shall include a properly completed UIC Form 1 and the following: | 2. Original form not correct. After consultation with Dan Jarvis I hand corrected, dated and initialled the original and received a revised signed and backdated Adobe Acrobat .pdf document (submitted on 3/30/07) from Tracey Fallang of Bill Barrett Corp. Form also was corrected in letter dated 4/11/07 to reflect the same injection interval cited for treatment in the disposal conversion procedure (tendered under 2.5) |
| 2.1. A plat showing the location of the injection well, all abandoned or active wells within a one-half mile radius of the proposed well, and the surface owner and the operator of any lands or producing leases, respectively, within a one-half mile radius of the proposed injection well. | 2.1 O.K. |
| 2.2. Copies of electrical or radioactive logs, including gamma ray logs, for the proposed well run prior to the installation of casing and indicating resistivity, spontaneous potential, caliper, and porosity. | 2.2 O.K. (on file in PIC Room) |
| 2.3. A copy of a cement bond or comparable log run for the proposed injection well after casing was set and cemented. | 2.3 O.K. |
| 2.4. Copies of logs already on file with the division should be referenced, but need not be refiled. | 2.4 O.K. |
| 2.5. A description of the casing or proposed casing program of the injection well and of the proposed method for testing the casing before use of the well. | 2.5 O.K. (Corrected 4/11/07 letter) |
| 2.6. A statement as to the type of fluid to be used for injection, its source and estimated amounts to be injected daily. | 2.6 O.K. (Corrected 4/11/07 letter) |
| 2.7. Standard laboratory analyses of (1) the fluid to be injected, (2) the fluid in the formation into which the fluid is being injected, and (3) the compatibility of the fluids. | 2.7 Operator suggests no sample of connate water can be gathered and Gil requests a log generated Rwa for the injection zone sands. I have requested some log analysis books from Halliburton to analyze their logs but have not been granted access to either their online books or hardcopies. |
| 2.8. The proposed average and maximum injection pressures. | 2.8 O.K but no proposed average injection pressure has been tendered as yet. |
| 2.9. Evidence and data to support a finding that the proposed injection well will not initiate fractures through the overlying strata or a confining interval that could enable the injected fluid or formation fluid to enter the fresh water strata. | 2.9 DOGM Management waived need for SRT in favour of accepting observed frac information provided by BBC in lieu of typical SRT information. |
| 2.10. Appropriate geological data on the injection interval and confining beds, and nearby Underground Sources of Drinking Water, including the geologic name, lithologic description, thickness, depth, water quality, and lateral extent; also information relative to geologic structure near the proposed well which may effect the conveyance and/or storage of the injected fluids. | 2.10 O.K. |
| 2.11. A review of the mechanical condition of each well within a one-half mile radius of the proposed injection well to assure that no conduit exists that could enable fluids to migrate up or down the wellbore and enter improper intervals. | 2.11 OK |
| 2.12. An affidavit certifying that a copy of the application has been provided to all operators, owners and surface owners within a one-half mile radius of the proposed injection well. | 2.12 OK |
| 2.13. Any other additional information that the board or division may determine is necessary to adequately review the application. | 2.13 O.K. |

OTHER COMMENTS AND OBSERVATIONS: It was possible that this application could have been construed as more appropriate for an injection well rather than a disposal well because the Operator proposes to inject into the same overall zone that is being produced in the field. In a letter included in the mailing dated 4/11/07 the operators staff argued convincingly that though the zone was the same, the well failed to rise to the geologic and engineering standards necessary for an injection well and was more appropriately a disposal well. See the letter for the arguments.

Reviewed by: Christopher J. Kierst Date: 4/18/07

# UIC INJECTION PERMIT APPLICATION ANALYSIS FORM
## WELL NAME: Prickly Pear Unit Federal 12-24
## API #: 4300730953

| R64[illegible] Requirements For Class II Injection Wells Including Wa[illegible]isposal, Storage And Enhanced Recovery Wells. | **Completed Items, Needed Items, & Comments** |
|---|---|
| 1. Injection wells shall be completed, equipped, operated, and maintained in a manner that will prevent pollution and damage to any USDW, or other resources and will confine injected fluids to the interval approved. | 1. O.K. |
| 2. The application for an injection well shall include a properly completed UIC Form 1 and the following: | 2. Original form not correct. After consultation with Dan Jarvis I hand corrected, dated and initialled the original and received a revised signed and backdated Adobe Acrobat .pdf document (submitted on 3/30/07) from Tracey Fallang of Bill Barrett Corp Form also was corrected in letter dated 4/11/07 to reflect the same injection interval cited for treatment in the disposal conversion procedure (tendered under 2.5) |
| 2.1. A plat showing the location of the injection well, all abandoned or active wells within a one-half mile radius of the proposed well, and the surface owner and the operator of any lands or producing leases, respectively, within a one-half mile radius of the proposed injection well. | 2.1 O.K. |
| 2.2. Copies of electrical or radioactive logs, including gamma ray logs, for the proposed well run prior to the installation of casing and indicating resistivity, spontaneous potential, caliper, and porosity. | 2.2 O.K. (on file in PIC Room) |
| 2.3. A copy of a cement bond or comparable log run for the proposed injection well after casing was set and cemented. | 2.3 O.K. |
| 2.4. Copies of logs already on file with the division should be referenced, but need not be refiled. | 2.4 O.K. |
| 2.5. A description of the casing or proposed casing program of the injection well and of the proposed method for testing the casing before use of the well. | 2.5 O.K. (Corrected 4/11/07 letter) |
| 2.6. A statement as to the type of fluid to be used for injection, its source and estimated amounts to be injected daily. | 2.6 O.K. (Corrected 4/11/07 letter) |
| 2.7. Standard laboratory analyses of (1) the fluid to be injected, (2) the fluid in the formation into which the fluid is being injected, and (3) the compatibility of the fluids. | 2.7 Operator suggests no sample of connate water can be gathered and Gil requests a log generated Rwa for the injection zone sands. I have requested some log analysis books from Halliburton to analyze their logs but have not been granted access to either their online books or hardcopies. |
| 2.8. The proposed average and maximum injection pressures. | 2.8 O.K but no proposed average injection pressure has been tendered as yet. |
| 2.9. Evidence and data to support a finding that the proposed injection well will not initiate fractures through the overlying strata or a confining interval that could enable the injected fluid or formation fluid to enter the fresh water strata. | 2.9 A step rate test (SRT) on the injection interval will be needed to validate the calculated fracture gradient data provided for this well. This will be done after Noticing, Statement of Basis and Approval to Convert letter sent but prior to issuance of a Permit document. |
| 2.10. Appropriate geological data on the injection interval and confining beds, and nearby Underground Sources of Drinking Water, including the geologic name, lithologic description, thickness, depth, water quality, and lateral extent; also information relative to geologic structure near the proposed well which may effect the conveyance and/or storage of the injected fluids. | 2.10 O.K. |
| 2.11. A review of the mechanical condition of each well within a one-half mile radius of the proposed injection well to assure that no conduit exists that could enable fluids to migrate up or down the wellbore and enter improper intervals. | 2.11 OK |
| 2.12. An affidavit certifying that a copy of the application has been provided to all operators, owners and surface owners within a one-half mile radius of the proposed injection well. | 2.12 OK |
| 2.13. Any other additional information that the board or division may determine is necessary to adequately review the application. | 2.13 O.K. |

OTHER COMMENTS AND OBSERVATIONS: It was possible that this application could have been construed as more appropriate for an injection well rather than a disposal well because the Operator proposes to inject into the same overall zone that is being produced in the field. In a letter included in the mailing dated 4/11/07 the operators staff argued convincingly that though the zone was the same, the well failed to rise to the geologic and engineering standards necessary for an injection well and was more appropriately a disposal well. See the letter for the arguments.

Reviewed by: Christopher J. Kierst Date: 4/18/07

# UIC INJECTION PERMIT APPLICATION ANALYSIS FORM
WELL NAME: Prickly Pear Unit Federal 12-24
API #: 4300730953

| R649-5-2. Requirements For Class II Injection Wells Including Water Disposal, Storage And Enhanced Recovery Wells. | **Completed Items, Needed Items, & Comments** |
|---|---|
| 1. Injection wells shall be completed, equipped, operated, and maintained in a manner that will prevent pollution and damage to any USDW, or other resources and will confine injected fluids to the interval approved. | 1. O.K. |
| 2. The application for an injection well shall include a properly completed UIC Form 1 and the following: | 2. Original form not correct. After consultation with Dan Jarvis I hand corrected, dated and initialled the original and received a revised signed and backdated Adobe Acrobat .pdf document (submitted on 3/30/07) from Tracey Fallang of Bill Barrett Corp. |
| 2.1. A plat showing the location of the injection well, all abandoned or active wells within a one-half mile radius of the proposed well, and the surface owner and the operator of any lands or producing leases, respectively, within a one-half mile radius of the proposed injection well. | 2.1 O.K. |
| 2.2. Copies of electrical or radioactive logs, including gamma ray logs, for the proposed well run prior to the installation of casing and indicating resistivity, spontaneous potential, caliper, and porosity. | 2.2 O.K. (on file in PIC Room) |
| 2.3. A copy of a cement bond or comparable log run for the proposed injection well after casing was set and cemented. | 2.3 O.K. |
| 2.4. Copies of logs already on file with the division should be referenced, but need not be refiled. | 2.4 O.K. |
| 2.5. A description of the casing or proposed casing program of the injection well and of the proposed method for testing the casing before use of the well. | 2.5 OK but the program is currently attempting to treat a set of perfs above those included in the UIC Form 1. MIT needs 1000 psi NOT 500 psi! |
| 2.6. A statement as to the type of fluid to be used for injection, its source and estimated amounts to be injected daily. | 2.6 The information submitted doesn't address the informational request. |
| 2.7. Standard laboratory analyses of (1) the fluid to be injected, (2) the fluid in the formation into which the fluid is being injected, and (3) the compatibility of the fluids. | 2.7 An analysed sample of the injection zone connate water in the subject well is needed to satisfy (2) and (3). This will be done after Noticing, Statement of Basis and Approval to Convert letter sent but prior to issuance of a Permit document. |
| 2.8. The proposed average and maximum injection pressures. | 2.8 O.K but no proposed average injection pressure has been tendered as yet. |
| 2.9. Evidence and data to support a finding that the proposed injection well will not initiate fractures through the overlying strata or a confining interval that could enable the injected fluid or formation fluid to enter the fresh water strata. | 2.9 A step rate test (SRT) on the injection interval will be needed to validate the calculated fracture gradient data provided for this well. This will be done after Noticing, Statement of Basis and Approval to Convert letter sent but prior to issuance of a Permit document. |
| 2.10. Appropriate geological data on the injection interval and confining beds, and nearby Underground Sources of Drinking Water, including the geologic name, lithologic description, thickness, depth, water quality, and lateral extent; also information relative to geologic structure near the proposed well which may effect the conveyance and/or storage of the injected fluids. | 2.10 OK but injection zone is in the same zone as production so they will probably get permission from the Board to do this as a water flood. |
| 2.11. A review of the mechanical condition of each well within a one-half mile radius of the proposed injection well to assure that no conduit exists that could enable fluids to migrate up or down the wellbore and enter improper intervals. | 2.11 OK |
| 2.12. An affidavit certifying that a copy of the application has been provided to all operators, owners and surface owners within a one-half mile radius of the proposed injection well. | 2.12 OK |
| 2.13. Any other additional information that the board or division may determine is necessary to adequately review the application. | 2.13 O.K. |

OTHER COMMENTS AND OBSERVATIONS: It is possible that this application may become a Board matter because the Operator proposes to inject into the same zone that is being produced in the field and this is more likely to be construed as a water flood not a salt water disposal operation and the well would be an injection well rather than a salt water disposal well.

Reviewed by: Christopher J. Kierst Date: 4/4/07

**From:** Chris Kierst
**To:** Tracey Fallang
**Subject:** RE: SWD Applications

Among other things, we discussed SRTs and the need for connate water samples from the injection interval. With respect to the connate water samples we said we would see if we could find alternate means to validate the samples and analyses as reasonably representative substitutes for the subject permit wells. We never agreed to accept the frac data as a substitute for a SRT for the purpose of issuance of a final permit to inject. We considered it sufficient to approve the conversion of the wells to Class II UIC wells but, in consultation with higher management, the frac data was deemed insufficient for a final permit, the SRT standards being rigorously defined by USEPA.

>>> "Tracey Fallang" <tfallang@billbarrettcorp.com> 04/19/2007 3:28 PM >>>
Chris, I thought we sufficiently addressed the step-rate test with the table provided in section 2.6? Can you clarify?

-----Original Message-----
From: Chris Kierst [mailto:chriskierst@utah.gov]
Sent: Thursday, April 19, 2007 3:25 PM
To: Tracey Fallang
Subject: Re: SWD Applications

Thank you for sending the supplemental information. I now have sufficient information to have the wells Noticed. I will start the Noticing process by ordering the drafting of the initial Noticing paperwork today. I am going to try to generate an Rweq to attempt to corroborate the water analysis information from the surrounding non UIC wells with the information in the permit subject well logs. After the Noticing period is over we will issue a Letter of Approval to Convert the well to a Class II UIC well. However, we will require an acceptable Step Rate Test before we will issue a final Permit to Inject. As always, please feel free to contact me if you have any questions.

>>> "Tracey Fallang" <tfallang@billbarrettcorp.com> 04/18/2007 3:46 PM >>>
Chris, just following up on your request for information and our response. At this time, do you need anything further from us and can you advise if/when the public comment period will begin?

Thank you.

Tracey Fallang

Bill Barrett Corporation

1099 18th Street, Suite 2300

Denver, CO 80202

Phone: 303-312-8134

Cell: 303-596-4818

BEFORE THE DIVISION OF OIL, GAS AND MINING
DEPARTMENT OF NATURAL RESOURCES
STATE OF UTAH

| | | |
|---|---|---|
| IN THE MATTER OF THE APPLICATION OF BILL BARRETT CORPORATION FOR ADMINISTRATIVE APPROVAL OF THE PRICKLY PEAR U FED 10-4 AND PRICKLY PEAR U FED 12-24 WELLS LOCATED IN SECTIONS 10 AND 24, TOWNSHIP 12 SOUTH, RANGE 14 EAST, CARBON COUNTY, UTAH, AS CLASS II INJECTION WELLS | : | NOTICE OF AGENCY ACTION<br><br>CAUSE NO. UIC 338 |

THE STATE OF UTAH TO ALL PERSONS INTERESTED IN THE ABOVE ENTITLED MATTER.

Notice is hereby given that the Division of Oil, Gas and Mining (the "Division") is commencing an informal adjudicative proceeding to consider the application of Bill Barrett Corporation for administrative approval of the Prickly Pear U Fed 10-4 and the Prickly Pear U Fed 12-24 wells, located in SE/4 SE/4 Section 10 and SW/4 SW/4 Section 24, Township 12 South, Range 14 East, Carbon County, Utah, for conversion to Class II injection wells. These wells are located in the Prickly Pear Unit. The adjudicative proceeding will be conducted informally according to Utah Admin.Rule R649-10, Administrative Procedures.

Selective zones in the North Horn, Wasatch and Upper Price River Formations will be used for water injection. The maximum requested injection pressure and rate will be determined based on fracture gradient information submitted by Bill Barrett Corporation.

Any person desiring to object to the proposed application or otherwise intervene in the proceeding, must file a written protest or notice of intervention with the Division within fifteen days following publication of this notice. The Division's Presiding Officer for this proceeding is Gil Hunt, Associate Director at PO Box 145801, Salt Lake City, Utah 84114-5801, phone number (801) 538-5340. If such a protest or notice of intervention is received, a hearing will be scheduled in accordance with the aforementioned administrative procedure rule. Protestants and/or interveners should be prepared to demonstrate at the hearing how this matter affects their interests.

Dated this 23rd day of April, 2007.

STATE OF UTAH
DIVISION OF OIL, GAS & MINING

Gil Hunt
Associate Director

**Bill Barrett Corporation**
**Prickly Pear U Fed 12-24**
**Cause No. UIC 338**

Publication Notices were sent to the following:

Bill Barrett Corporation
1099 18th St, Suite 2300
Denver, CO 80202

Sun Advocate
845 E Main St
Price, UT 84501-2708

Salt Lake Tribune
PO Box 45838
Salt Lake City, UT 84145

Moab Office
Bureau of Land Management
82 E Dogwood
Moab, UT 84532

Carbon County Planning
120 E Main
Price, UT 84501

Petro-Canada Resources
1099 18th St, Suite 400
Denver, CO 80202

Dan Jackson
US EPA Region VIII, MS 8P-W-GW
1595 Wynkoop St
Denver, CO 80202-1129

Earlene Russell
Engineering Technician
April 24, 2007

**Earlene Russell - RE: UIC 338 Legal Notice**

**From:** "NAC Legal"
**To:** "'Earlene Russell'"
**Date:** 4/24/2007 4:24 PM
**Subject:** RE: UIC 338 Legal Notice

Please check the ad in the paper on April 28.

Cost is $147.50. Ad # 82037PVA.

Thank you.

Lynn

237-2720

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**From:** Earlene Russell [mailto:earlenerussell@utah.gov]
**Sent:** Tuesday, April 24, 2007 3:46 PM
**To:** SL Tribune
**Subject:** UIC 338 Legal Notice

Please let me know when this will be published.

Thanks.

Earlene Russell
Division of Oil, Gas & Mining
PO Box 145801
Salt Lake City, UT 84114-5801
or
1594 W North Temple, Suite 1210
Salt Lake City, UT 84116
Phone (801) 538-5336
Fax (801) 359-3940
e-mail earlenerussell@utah.gov

JON M. HUNTSMAN, JR.
*Governor*
GARY R. HERBERT
*Lieutenant Governor*

# State of Utah
**DEPARTMENT OF NATURAL RESOURCES**
MICHAEL R. STYLER
*Executive Director*
**Division of Oil, Gas and Mining**
JOHN R. BAZA
*Division Director*

April 24, 2007

SENT VIA E-MAIL AND FAX (801) 237-2577

Salt Lake Tribune
PO Box 45838
Salt Lake City, UT 84145

Re: Notice of Agency Action - Cause No. UIC 338

Gentlemen:

Enclosed is a copy of the referenced Notice of Agency Action. Please publish the Notice, once only, as soon as possible. Please send proof of publication and billing to the Division of Oil, Gas and Mining, Suite 1210, PO Box 145801, Salt Lake City, Utah 84114-5801.

Sincerely,

Earlene Russell

Earlene Russell
Engineering Technician

encl.

P.01

TRANSACTION REPORT

APR-24-2007 TUE 03:40 PM

FOR: OIL, GAS & MINING 801 359 3940

| DATE | START | RECEIVER | TX TIME | PAGES | TYPE | NOTE | M# | DP |
|---|---|---|---|---|---|---|---|---|
| APR-24 | 03:39 PM | 2372577 | 1'27" | 2 | SEND | OK | 459 | |

TOTAL : 1M 27S PAGES: 2

JON M. HUNTSMAN, JR.
*Governor*

GARY R. HERBERT
*Lieutenant Governor*

# State of Utah

**DEPARTMENT OF NATURAL RESOURCES**

MICHAEL R. STYLER
*Executive Director*

**Division of Oil, Gas and Mining**

JOHN R. BAZA
*Division Director*

April 24, 2007

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Sincerely,

**From:** Sun Advocate Legals <legals@sunad.com>
**To:** Earlene Russell <earlenerussell@utah.gov>
**Date:** 4/24/2007 4:32 PM
**Subject:** Re: UIC 338 - LEGAL NOTICE

If I had read the entire attachment I would have seen the publish only once request. The notice will appear in the April 26, 2007 Sun Advocate. Affidavit and invoice will be sent at the end of the month.

Please let me know if I can be of further assistance.

Kelly Wilkinson
Production Manager
Sun Advocate
Emery County Progress
435.637.0732 x30

Earlene Russell wrote:
> Please let me know when this legal notice will be published.
>
> Thanks.
>
>
>
> Earlene Russell
> Division of Oil, Gas & Mining
> PO Box 145801
> Salt Lake City, UT 84114-5801
> or
> 1594 W North Temple, Suite 1210
> Salt Lake City, UT 84116
> Phone (801) 538-5336
> Fax (801) 359-3940
> e-mail earlenerussell@utah.gov

JON M. HUNTSMAN, JR.
*Governor*
GARY R. HERBERT
*Lieutenant Governor*

# State of Utah
**DEPARTMENT OF NATURAL RESOURCES**
MICHAEL R. STYLER
*Executive Director*
**Division of Oil, Gas and Mining**
JOHN R. BAZA
*Division Director*

April 24, 2007

SENT VIA E-MAIL AND FAX(435) 637-2716

Sun Advocate
845 E Main St
Price, UT 84501-2708

Re: Notice of Agency Action - Cause No. UIC 338

Gentlemen:

Enclosed is a copy of the referenced Notice of Agency Action. Please publish the Notice, once only, as soon as possible. Please send proof of publication and billing to the Division of Oil, Gas and Mining, Suite 1210, PO Box 145801, Salt Lake City, Utah 84114-5801.

Sincerely,

Earlene Russell
Engineering Technician

encl.

P. 01

TRANSACTION REPORT

APR-24-2007 TUE 03:38 PM

FOR: OIL, GAS & MINING 801 359 3940

| DATE START | RECEIVER | TX TIME | PAGES | TYPE | NOTE | M# | DP |
|---|---|---|---|---|---|---|---|
| APR-24 03:37 PM | 14356372716 | 44″ | 2 | SEND | OK | 458 | |

TOTAL : 44S PAGES: 2

JON M. HUNTSMAN, JR.
*Governor*

GARY R. HERBERT
*Lieutenant Governor*

# State of Utah

**DEPARTMENT OF NATURAL RESOURCES**

MICHAEL R. STYLER
*Executive Director*

**Division of Oil, Gas and Mining**

JOHN R. BAZA
*Division Director*

April 24, 2007

SENT VIA E-MAIL AND FAX(435) 637-2716

Sun Advocate
845 E Main St
Price, UT 84501-2708

Re: Notice of Agency Action - Cause No. UIC 338

Gentlemen:

Enclosed is a copy of the referenced Notice of Agency Action. Please publish the Notice, once only, as soon as possible. Please send proof of publication and billing to the Division of Oil, Gas and Mining, Suite 1210, PO Box 145801, Salt Lake City, Utah 84114-5801.

Sincerely,

Earlene Russell

**From:** Chris Kierst
**To:** Earlene Russell
**Date:** 4/19/2007 11:39 AM
**Subject:** 2 UIC Apps for Noticing

The subject wells for noticing are as follows:

UIC #

Bill Barrett Corporation Prickly Pear Federal Unit 10-4
4300730823
S. 10, T. 12 S., R. 14 E.
Carbon County, Utah
338.1

Bill Barrett Corporation Prickly Pear Federal Unit 12-24
4300730953
S. 24, T. 12 S., R. 14 E.
Carbon County, Utah
338.2

FYI the operator proposes to inject into the North Horn Formation, the Dark Canyon Conglomerate beds of the Wasatch Formation and the upper Price River Formation.

Please inform me if you need additional information that I may be able to provide.

1099 18th St # 2300
Denco 80202

**From:** Chris Kierst
**To:** Tracey Fallang
**Date:** 04/24/2007 8:27:54 AM
**Subject:** RE: SWD Applications

Among other things, we discussed SRTs and the need for connate water samples from the injection interval. With respect to the connate water samples we said we would see if we could find alternate means to validate the samples and analyses as reasonably representative substitutes for the subject permit wells. We never agreed to accept the frac data as a substitute for a SRT for the purpose of issuance of a final permit to inject. We consider it sufficient to approve the conversion of the wells to Class II UIC wells but, in consultation with higher management, the frac data was deemed insufficient for a final permit, the SRT standards being rigorously defined by USEPA.

>>> "Tracey Fallang" <tfallang@billbarrettcorp.com> 04/19/2007 3:28 PM >>>
Chris, I thought we sufficiently addressed the step-rate test with the table provided in section 2.6? Can you clarify?

-----Original Message-----
From: Chris Kierst [mailto:chriskierst@utah.gov]
Sent: Thursday, April 19, 2007 3:25 PM
To: Tracey Fallang
Subject: Re: SWD Applications

Thank you for sending the supplemental information. I now have sufficient information to have the wells Noticed. I will start the Noticing process by ordering the drafting of the initial Noticing paperwork today. I am going to try to generate an Rweq to attempt to corroborate the water analysis information from the surrounding non UIC wells with the information in the permit subject well logs. After the Noticing period is over we will issue a Letter of Approval to Convert the well to a Class II UIC well. However, we will require an acceptable Step Rate Test before we will issue a final Permit to Inject. As always, please feel free to contact me if you have any questions.

>>> "Tracey Fallang" <tfallang@billbarrettcorp.com> 04/18/2007 3:46 PM >>>
Chris, just following up on your request for information and our response. At this time, do you need anything further from us and can you advise if/when the public comment period will begin?

Thank you.

Tracey Fallang

Bill Barrett Corporation

1099 18th Street, Suite 2300

Denver, CO 80202

Phone: 303-312-8134

Cell: 303-596-4818

**From:** "Jim Kinser" <jkinser@billbarrettcorp.com>
**To:** "Chris Kierst" <chriskierst@utah.gov>
**Date:** 05/02/2007 1:07:00 PM
**Subject:** BBC SWD wells in Prickly Pear

Dear Chris,

I am writing to try to address your concerns relating to a step-rate test request, you sent to Tracey Fallang, yesterday, May 1st. Attached is a document you may have seen before. I think it was included in our application for converting the Prickly Pear #10-4 and #12-24, into SWD wells. The attached document addresses the concepts behind your request to see a pressure "breakover" or fracture extension pressure in an SRT. As you probably know, a pressure "breakover" in an SRT indicates fracture extension pressure at that inflection point and is the pressure we want to stay below, when injecting water into the well for disposal purposes. The attached file lists ISIP's for the different formations into which we propose to inject. With the observed ISIP's, and the fluid pressure gradient of .4417 psi/ft, we can calculate the BHTP's, which are the extension pressures you are looking for. You mention in your letter that "A frac simulation does not provide the requisite degree of procedural rigor to demonstrate a pressure breakover....". These data are not simulations; they are observed pressures and demonstrate fracture extension pressure by way of ISIP, which is equivalent to the "pressure break over" inflection point you mentioned. If you meant frac stimulations, I believe they do demonstrate fracture extension pressures. Also, we are requesting a maximum surface pressure 200 psi lower or 90% than the lowest observed ISIP or extension pressure and an average surface pressure 500psi lower or 75% of observed fracture extension pressure. If there is any error in equating ISIP to fracture extension pressure, it is on the low side or conservative side and ISIP's would tend to be approaching closure pressure and provide us with even more of a safety factor. Lastly, if multiple zones are open, which they are, it may be difficult to achieve fracture extension pressure during a SRT, due to formation leakoff, unless a fairly high injection rate is used. I will give you a call shortly to try to address any additional questions you may have and get your feedback. Thank you for your consideration in this matter.

Sincerely,

Jim Kinser
Development Geologist
Bill Barrett Corporation
Office 303.312.8163
Cell 303.886.4954
Fax 303.291.0420
Home 303.283-6797
jkinser@billbarrettcorp.com

**CC:** "Tracey Fallang" <tfallang@billbarrettcorp.com>

# Bill Barrett Corporation

West Tavaputs Field SWD Well Application

**Maximum Allowable Surface Pressure Calculations**
**Based on Observed Fracture Gradients**

Water SG = 1.02 Gradient = 0.4417 psi/ft

Prickly Pear Federal 10-4

| Depth (ft) | Observed ISIP (psig) | Calculated Btm Hole (psig) | Resulting Frac Grad (psi/ft) |
|---|---|---|---|
| 4772 | 2220 | 4327.6 | 0.907 |
| 4964 | 2600 | 4792.4 | 0.965 |
| 5450 | 3030 | 5437.0 | 0.998 |
| 6700 | 4120 | 7079.1 | 1.057 |
| 6890 | 4100 | 7143.0 | 1.037 |
| 7180 | 3910 | 7081.1 | 0.986 |
| 7550 | 3910 | 7244.5 | 0.960 |

Requested Max Surface Pressure = 2000 psig

Prickly Pear 12-24-12-14

| Depth (ft) | Observed ISIP (psig) | Calculated Btm Hole (psig) | Resulting Frac Grad (psi/ft) | |
|---|---|---|---|---|
| 6295 | No Treatment | | | |
| 6791 | 3350 | 6349.3 | 0.935 | |
| 6908 | No Treatment | | | |
| 7620 | 2900 | 6265.4 | 0.822 | |
| 8620 | 2980 | 6787.1 | 0.787 | Below |
| 9242 | 4390 | 8471.8 | 0.917 | Fish @ 7665' |

Requested Max Surface Pressure = 2000 psig

ISIP Data collected during initial completion treatments

Calculated Bottom Hole Pressure = ISIP + 0.4417 x Depth
Resulting Frac Gradient = Calculated Btm Hole Pressure / Depth

Requested Max Surface Pressure < 90% x ISIP
Anticipated Avg Surface Pressure = 75% x Max Surface Pressure

Anticipated Avg Disposal Rate = 400 bwpd / well
Requested Maximum Disposal Rate = 2000 bwpd / well

**From:** Tracey Fallang <tfallang@billbarrettcorp.com>
**To:** John Shepard <jshepard@billbarrettcorp.com>
**CC:** "eric_jones@blm.gov" <eric_jones@blm.gov>, Chris Kierst <chriskierst@uta...
**Date:** 05/07/2008 4:13 PM
**Subject:** Prickly Pear 12-24 Injection Test

John, based on the results of the MIT conducted today (and witnessed by DOGM), we now have a green light from DOGM and BLM to move forward with the injection test. Please forward a copy of the MIT results to me so that I can provide to Eric and Chris (and we will NOT be required to do another MIT after the test). In addition, once the injection test is complete, we'll need to provide test results within 30 days.

Tracey Fallang I Direct: 303.312.8134 I Cell: 303.596.4818 I Fax: 303.291.0420
1099 18th Street, Suite 2300, Denver, CO 80202
tfallang@billbarrettcorp.com<mailto:tfallang@billbarrettcorp.com>

**From:** Chris Kierst
**To:** Jim Kinser
**Date:** 05/08/2007 10:23 AM
**Subject:** Re: BBC SWD wells in Prickly Pear

Hi Jim,
In response to your request that the Division entertain your suggested use of frac information as an alternative to the customary SRT, I batted it around with several managers/engineers. We'll give you half a loaf on this. If everything else in the permit application is acceptable, we'll let you have a permit without a SRT but, instead, based on the frac information you provide. You will not, however, be permitted to inject at 2000# surface pressure but at 1700# surface pressure. This should provide an acceptable margin of error from injecting the worst case heaviest field brine that you sampled. Please send me the documentation of the source of the 0.4417 pis/ft frac gradient and the nature of the frac fluid you used in your proposal. If this is acceptable to you please inform me.

>>> "Jim Kinser" <jkinser@billbarrettcorp.com> 05/02/2007 1:06 PM >>>
Dear Chris,

I am writing to try to address your concerns relating to a step-rate test request, you sent to Tracey Fallang, yesterday, May 1st. Attached is a document you may have seen before. I think it was included in our application for converting the Prickly Pear #10-4 and #12-24, into SWD wells. The attached document addresses the concepts behind your request to see a pressure "breakover" or fracture extension pressure in an SRT. As you probably know, a pressure "breakover" in an SRT indicates fracture extension pressure at that inflection point and is the pressure we want to stay below, when injecting water into the well for disposal purposes. The attached file lists ISIP's for the different formations into which we propose to inject. With the observed ISIP's, and the fluid pressure gradient of .4417 psi/ft, we can calculate the BHTP's, which are the extension pressures you are looking for. You mention in your letter that "A frac simulation does not provide the requisite degree of procedural rigor to demonstrate a pressure breakover....". These data are not simulations; they are observed pressures and demonstrate fracture extension pressure by way of ISIP, which is equivalent to the "pressure break over" inflection point you mentioned. If you meant frac stimulations, I believe they do demonstrate fracture extension pressures. Also, we are requesting a maximum surface pressure 200 psi lower or 90% than the lowest observed ISIP or extension pressure and an average surface pressure 500psi lower or 75% of observed fracture extension pressure. If there is any error in equating ISIP to fracture extension pressure, it is on the low side or conservative side and ISIP's would tend to be approaching closure pressure and provide us with even more of a safety factor. Lastly, if multiple zones are open, which they are, it may be difficult to achieve fracture extension pressure during a SRT, due to formation leakoff, unless a fairly high injection rate is used. I will give you a call shortly to try to address any additional questions you may have and get your feedback. Thank you for your consideration in this matter.

Sincerely,

Jim Kinser
Development Geologist
Bill Barrett Corporation
Office 303.312.8163
Cell 303.886.4954
Fax 303.291.0420
Home 303.283-6797
jkinser@billbarrettcorp.com

**From:** Chris Kierst
**To:** Jim Kinser
**Subject:** Re: BBC SWD wells in Prickly Pear

Hi Jim,
In response to your request that the Division entertain your suggested use of frac information as an alternative to the customary SRT, I batted it around with several managers/engineers. We'll give you half a loaf on this. If everything else in the permit application is acceptable, we'll let you have a permit without a SRT but, instead, based on the frac information you provide. You will not, however, be permitted to inject at 2000# surface pressure but at 1700# surface pressure. This should provide an acceptable margin of error from injecting the worst case heaviest field brine that you sampled. Please send me the documentation of the source of the 0.4417 pis/ft frac gradient and the nature of the frac fluid you used in your proposal. If this is acceptable to you please inform me.

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I am writing to try to address your concerns relating to a step-rate test request, you sent to Tracey Fallang, yesterday, May 1st. Attached is a document you may have seen before. I think it was included in our application for converting the Prickly Pear #10-4 and #12-24, into SWD wells. The attached document addresses the concepts behind your request to see a pressure "breakover" or fracture extension pressure in an SRT. As you probably know, a pressure "breakover" in an SRT indicates fracture extension pressure at that inflection point and is the pressure we want to stay below, when injecting water into the well for disposal purposes. The attached file lists ISIP's for the different formations into which we propose to inject. With the observed ISIP's, and the fluid pressure gradient of .4417 psi/ft, we can calculate the BHTP's, which are the extension pressures you are looking for. You mention in your letter that "A frac simulation does not provide the requisite degree of procedural rigor to demonstrate a pressure breakover....". These data are not simulations; they are observed pressures and demonstrate fracture extension pressure by way of ISIP, which is equivalent to the "pressure break over" inflection point you mentioned. If you meant frac stimulations, I believe they do demonstrate fracture extension pressures. Also, we are requesting a maximum surface pressure 200 psi lower or 90% than the lowest observed ISIP or extension pressure and an average surface pressure 500psi lower or 75% of observed fracture extension pressure. If there is any error in equating ISIP to fracture extension pressure, it is on the low side or conservative side and ISIP's would tend to be approaching closure pressure and provide us with even more of a safety factor. Lastly, if multiple zones are open, which they are, it may be difficult to achieve fracture extension pressure during a SRT, due to formation leakoff, unless a fairly high injection rate is used. I will give you a call shortly to try to address any additional questions you may have and get your feedback. Thank you for your consideration in this matter.

Sincerely,

Jim Kinser
Development Geologist
Bill Barrett Corporation
Office 303.312.8163

INSPECTION FORM 6

STATE OF UTAH
DIVISION OF OIL GAS AND MINING

## INJECTION WELL - PRESSURE TEST

Well Name: UTE TRIBAL 12-24 API Number: 43-007-30953
Qtr/Qtr: SW/SW Section: 24 Township: 12S Range: 14E
Company Name: BILL BARRETT CORP
Lease: State Surface Fee Federal 14-20-H62-7513 Indian
Inspector: Dennis Ingram Date: 5-7-08

Initial Conditions:

Tubing - Rate: _____ Pressure: 0 psi

Casing/Tubing Annulus - Pressure: 1550 psi

Conditions During Test:

| Time (Minutes) | Annulus Pressure | Tubing Pressure |
|---|---|---|
| 0 | 1550 | OPEN |
| 5 | 1560 | |
| 10 | 1550 | |
| 15 | 1550 | |
| 20 | 1550 | |
| 25 | 1550 | |
| 30 | 1550 | 0 |

Results: Pass/Fail

Conditions After Test:

Tubing Pressure: 0 psi

Casing/Tubing Annulus Pressure: _____ psi

COMMENTS: Test @ 12:35 PM

Lloyd Towns
Operator Representative

TO BRAD HILL

RECEIVED
MAY 12 2008
DIV. OF OIL, GAS & MINING

**From:** "Tracey Fallang" <tfallang@billbarrettcorp.com>
**To:** "Chris Kierst" <chriskierst@utah.gov>
**Date:** 06/11/2007 1:32 PM
**Subject:** SWD Application Approvals

Hi Chris, just checking in on the status of these applications (the Prickly Pear 10-24 and 12-24). Thank you.

Tracey Fallang

Bill Barrett Corporation

1099 18th Street, Suite 2300

Denver, CO 80202

Phone: 303-312-8134

Cell: 303-596-4818

**From:** Tracey Fallang <tfallang@billbarrettcorp.com>
**To:** Chris Kierst <chriskierst@utah.gov>
**Date:** 07/07/2008 10:56 AM
**Subject:** FW: Prickly Pear 12-24 Injection Well-Additional Wasatch perforations.
**Attachments:** PrPr 12-24 Wasatch Perforations.xls; PrPr 12-24 Conversion Procedure (2) 06 -23-08.doc

Chris, as a refresher on this, we had submitted the initial UIC application in April 2007. We received administrative approval in July 2007, conducted the step-rate test & MIT and then conducted an initial injection test in May 2008. The initial rate was approximately 500 BWPD @ 1200 psi, then dropped to 375 BWPD @ 1750 psi and finally ended up at 230 BWPD @ 1750 psi. These results are not sufficient to maintain a viable disposal facility. We have taken another look at the logs on this well and have found a number of intervals in the Wasatch that may have water injection potential (BBC does currently produce hydrocarbons out of the Wasatch in both Prickly Pear and Peter's Point).

My question to you is - what additional information needs to be provided for approval of these additional perfs and to also move forward with testing of this interval? I've attached the procedure and Wasatch perf information.

Thank you.

**Bill Barrett Corporation**

**PRICKLY PEAR 12-24**
Surface Location: SWSW 24-T12S-R15E 1,271' FSL & 483' FWL
Bottom Hole Location:
API No. 43-007-30953

**TOC @ 780'**

| STAGE | FORMATION | TOP PEFORATION | BOTTOM PERFORATION | GUN LENGTH | SHOT DENSITY |
|---|---|---|---|---|---|
| 1 | Middle Wasatch | 4500 ' | 4518 ' | 18 ' | 6 JSPF @ 60° |
| 2 | Middle Wasatch | 4260 ' | 4290 ' | 30 ' | 6 JSPF @ 60° |
| 3 | Middle Wasatch | 4058 ' | 4068 ' | 10 ' | 6 JSPF @ 60° |
| | | 4038 ' | 4048 ' | 10 ' | 6 JSPF @ 60° |
| | | 4018 ' | 4028 ' | 10 ' | 6 JSPF @ 60° |
| | | 3976 ' | 3996 ' | 20 ' | 6 JSPF @ 60° |
| | | 3946 ' | 3964 ' | 18 ' | 6 JSPF @ 60° |
| 4 | Middle Wasatch | 3875 ' | 3890 ' | 15 ' | 6 JSPF @ 60° |
| | | 3838 ' | 3858 ' | 20 ' | 6 JSPF @ 60° |
| 5 | Middle Wasatch | 3798 ' | 3804 ' | 6 ' | 6 JSPF @ 60° |
| | | 3768 ' | 3776 ' | 8 ' | 6 JSPF @ 60° |
| | | 3750 ' | 3755 ' | 5 ' | 6 JSPF @ 60° |
| 6 | Middle Wasatch | 3644 ' | 3662 ' | 18 ' | 6 JSPF @ 60° |
| | | 3616 ' | 3620 ' | 4 ' | 6 JSPF @ 60° |
| | | 3606 ' | 3610 ' | 4 ' | 6 JSPF @ 60° |
| | | 3596 ' | 3600 ' | 4 ' | 6 JSPF @ 60° |
| | | 3586 ' | 3590 ' | 4 ' | 6 JSPF @ 60° |
| | | 3554 ' | 3558 ' | 4 ' | 6 JSPF @ 60° |
| | | 3544 ' | 3548 ' | 4 ' | 6 JSPF @ 60° |
| | | 3501 ' | 3505 ' | 4 ' | 6 JSPF @ 60° |
| | | 3492 ' | 3496 ' | 4 ' | 6 JSPF @ 60° |
| | | 3482 ' | 3486 ' | 4 ' | 6 JSPF @ 60° |
| | | | | | |

**** Correlated to Halliburton Dual-Spaced Neutron/Spectral Density log dated 09/26/04.**

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

**June 23, 2008**

**AFE #** **W.I. 100.0000%**

Surface Casing: 9.625", 36.00#, J-55, ST&C Set @ 1,002'

Production Casing: 5.50", 17.00#, L-80, LT&C Set @9,491'
Float collar @ 9,447'.
Cemented with 1850 sks 50/50 POZ
**Drift I.D. = 4.767". Collapse = 6,290 psi. Burst = 7,740 psi.**
**Capacity = 0.0232 BBL/Linear Ft.**

TOC: 820'

CBP @ 8,595'. CFP @ 7,675".

Bit, bit sub and partial joint of tubing twisted off while drilling up CFP.
**Top of fish @ 7,665'**

CIBP @ 7,655' with 2 sx cement on top. PBTD @ 7,648'.

| Perforations: | | | |
|---|---|---|---|
| | Price River | 7,620-7,630' | 3 JSPF |
| | Dark Canyon | 7,258-7,266' | 3 JSPF |
| | North Horn | 6,908-6,916' | 4 JSPF |
| | | 6,791-6,799' | 3 JSPF |
| | | 6,295-6,300' | 3 JSPF |

Packer: Halliburton "PLS" @ 6215'
2 3/8", 4.7#, N-80, EUE 8RD to 6,215'

Bill Barrett Corporation

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

## Workover Procedure

01 MIRU workover tools.
02 Blow down well and kill with filtered production water if needed.
03 ND tree and NU BOPs.
04 Release packer and TOOH with tubing.
05 RU E-Line and set CBP @ +/- 4,700'. Perforate interval #1 on attached table with 3 3/8" expendable guns loaded with OWEN "HERO" charges 6 JSPF @ 60° phasing. Frac interval with small frac as per Halliburton recommendation.
06 Set CFP and continue to perf and frac intervals on attached sheet.
07 Flow well to clean up.
08 PU bit and TIH with tubing. Drill out CFPs and clean out to PBTD @ 7,648'.
09 TOOH and LD bit.
10 PU Halliburton "PLS packer and TIH. Circulate annulus with packer fluid and space out tubing. Set packer @ +/- 4,400'.
11 ND BOPs and NU tree.
12 Perform MIT on casing, tubing and packer by pressure testing to 1,500 psi with DOGM witness* present.
13 RDMO workover tools.
14 RU injection pump and begin injecting filtered production water into well. Maintain surface injection pressure below 1,800 psi. Monitor rate and pressure and continue injecting into well for 7 to 10 days until a stabilized rate and pressure is obtained.

Form 3160-5
(April 2004)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

COPY

FORM APPROVED
OM B No. 1004-0137
Expires: March 31, 2007

## SUNDRY NOTICES AND REPORTS ON WELLS

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160 - 3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE- Other instructions on reverse side.***

5. Lease Serial No.
**UTU-77513**

6. If Indian, Allottee or Tribe Name
**n/a**

7. If Unit or CA/Agreement, Name and/or No.
**Prickly Pear / UTU-79487**

1. Type of Well
☐ Oil Well ☐ ☑ Gas Well ☐☐ ☐ Other

8. Well Name and No.
**Prickly Pear Unit Fed 12-24**

2. Name of Operator **BILL BARRETT CORPORATION**

9. API Well No.
**43-007-30953**

3a. Address
**1099 18th Street Suite 2300 Denver CO 80202**

3b. Phone No. *(include area code)*
**303 312-8134**

10. Field and Pool, or Exploratory Area

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*
**SWSW, 1271' FSL, 483' FWL, Section 24-T12S-R14E S.L.B.&M.**

11. County or Parish, State
**Carbon County, Utah**

12. CHECK APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☑ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production (Start/Resume) | ☐ Water Shut-Off |
| ☐ Subsequent Report | ☐ Alter Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☐ Final Abandonment Notice | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☑ Other **Request to Perf the Wasatch** |
| | ☐ Change Plans | ☐ Plug and Abandon | ☐ Temporarily Abandon | |
| | ☐ Convert to Injection | ☐ Plug Back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be performed or provide the Bond No. on file with BLM/BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notices shall be filed only after all requirements, including reclamation, have been completed, and the operator has determined that the site is ready for final inspection.)

**Conditional approvals have been received from the BLM and the State of Utah, Division of Oil, Gas and Mining to convert this well to a water disposal well . Upon intial testing of the existing perf'd intervals (with poor disposal results) and after further review of the logs for this well, we would like to request to perf the Middle Wasatch following the attached procedure to conduct further disposal testing. Upon completion of the new perfs, BBC would conduct a step-rate test and file for an amended UIC permit.**

**If you should have any questions or need additional information, please contact me at 303-312-8134.**

COPY SENT TO OPERATOR
Date: 8·4·2008
Initials: KS

RECEIVED
JUL 18 2008
DIV. OF OIL, GAS & MINING

14. I hereby certify that the foregoing is true and correct
Name *(Printed/Typed)* **Tracey Fallang** Title **Environmental/Regulatory Analyst**

Signature Tracey Fallang Date **07/16/2008**

**THIS SPACE FOR FEDERAL OR STATE OFFICE USE**

Approved by BRADLEY G. HILL Title ENVIRONMENTAL MANAGER Date 08-04-08

Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. Office

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

*(Instructions on page 2)*

Bill Barrett Corporation

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

**June 23, 2008**

| | | |
|---|---|---|
| **AFE #** | **W.I. 100.0000%** | |
| Surface Casing: | 9.625", 36.00#, J-55, ST&C | Set @ 1,002' |
| Production Casing: | 5.50", 17.00#, L-80, LT&C<br>Float collar @ 9,447'.<br>Cemented with 1850 sks 50/50 POZ<br>**Drift I.D. = 4.767". Collapse = 6,290 psi. Burst = 7,740 psi.**<br>**Capacity = 0.0232 BBL/Linear Ft.** | Set @9,491' |
| TOC: | 820' | |

CBP @ 8,595'. CFP @ 7,675".

Bit, bit sub and partial joint of tubing twisted off while drilling up CFP.
**Top of fish @ 7,665'**

CIBP @ 7,655' with 2 sx cement on top. PBTD @ 7,648'.

| | | | |
|---|---|---|---|
| Perforations: | Price River | 7,620-7,630' | 3 JSPF |
| | Dark Canyon | 7,258-7,266' | 3 JSPF |
| | North Horn | 6,908-6,916' | 4 JSPF |
| | | 6,791-6,799' | 3 JSPF |
| | | 6,295-6,300' | 3 JSPF |

Packer: Halliburton "PLS" @ 6215'
2 3/8", 4.7#, N-80, EUE 8RD to 6,215'

Bill Barrett Corporation

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**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

## Workover Procedure

01 MIRU workover tools.
02 Blow down well and kill with filtered production water if needed.
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06 Set CFP and continue to perf and frac intervals on attached sheet.
07 Flow well to clean up.
08 PU bit and TIH with tubing. Drill out CFPs and clean out to PBTD @ 7,648'.
09 TOOH and LD bit.
10 PU Halliburton "PLS packer and TIH. Circulate annulus with packer fluid and space out tubing. Set packer @ +/- 3,400'.
11 ND BOPs and NU tree.
12 Perform MIT on casing, tubing and packer by pressure testing to 1,500 psi with DOGM witness* present.
13 RDMO workover tools.
14 Conduct step-rate test and forward information with modified UIC permit to Division Oil, Gas, and Mining and BLM.

**Bill Barrett Corporation**

**PRICKLY PEAR 12-24**
Surface Location: SWSW 24-T12S-R15E 1,271' FSL & 483' FWL
Bottom Hole Location:
API No. 43-007-30953

**TOC @ 780'**

| STAGE | FORMATION | TOP PEFORATION | BOTTOM PERFORATION | GUN LENGTH | SHOT DENSITY |
|---|---|---|---|---|---|
| 1 | Middle Wasatch | 4500 ' | 4518 ' | 18 ' | 6 JSPF @ 60° |
| 2 | Middle Wasatch | 4260 ' | 4290 ' | 30 ' | 6 JSPF @ 60° |
| 3 | Middle Wasatch | 4058 ' | 4068 ' | 10 ' | 6 JSPF @ 60° |
| | | 4038 ' | 4048 ' | 10 ' | 6 JSPF @ 60° |
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| 4 | Middle Wasatch | 3875 ' | 3890 ' | 15 ' | 6 JSPF @ 60° |
| | | 3838 ' | 3858 ' | 20 ' | 6 JSPF @ 60° |
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| | | 3768 ' | 3776 ' | 8 ' | 6 JSPF @ 60° |
| | | 3750 ' | 3755 ' | 5 ' | 6 JSPF @ 60° |
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| | | 3616 ' | 3620 ' | 4 ' | 6 JSPF @ 60° |
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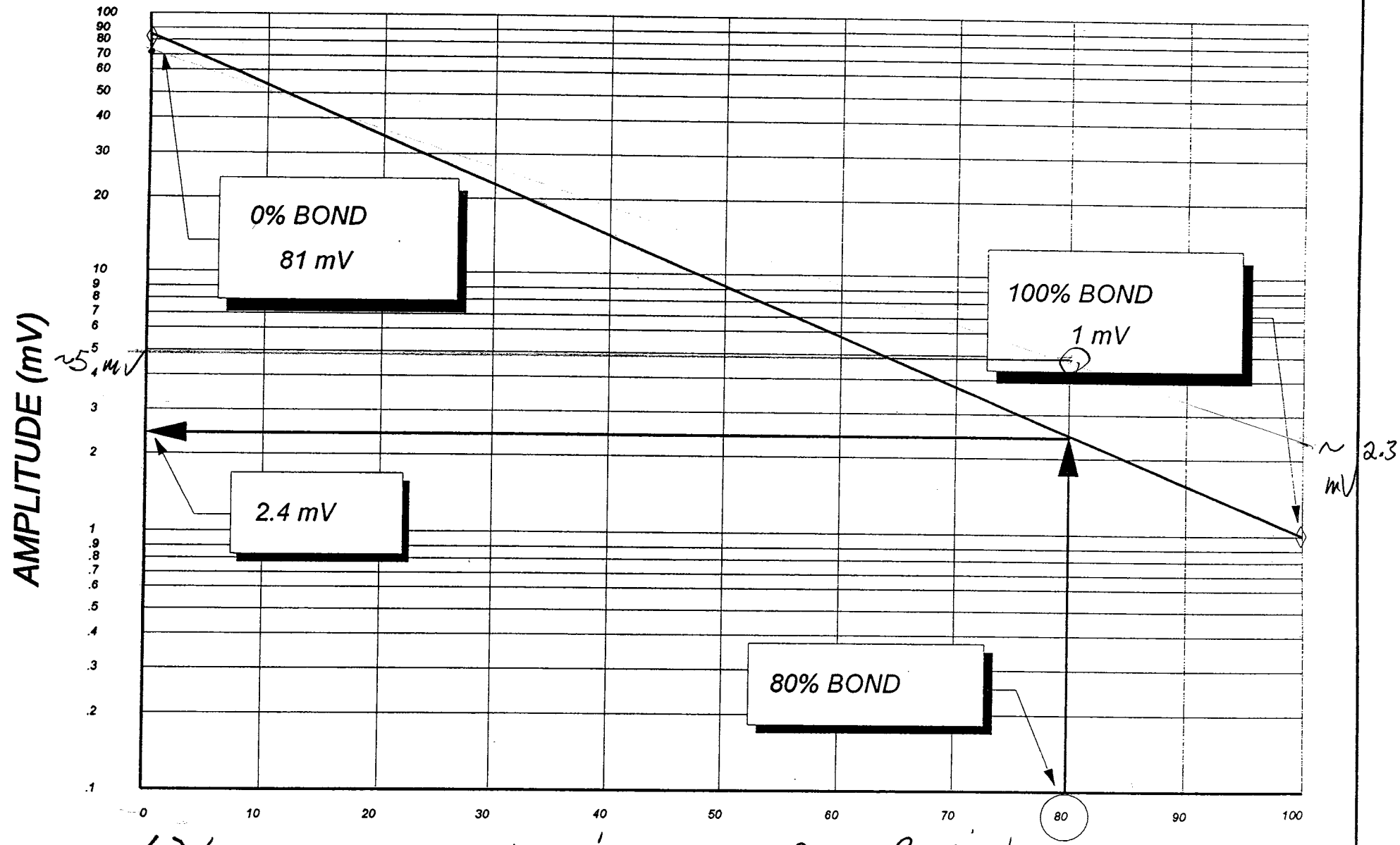
| | | 3554 ' | 3558 ' | 4 ' | 6 JSPF @ 60° |
| | | 3544 ' | 3548 ' | 4 ' | 6 JSPF @ 60° |
| | | 3501 ' | 3505 ' | 4 ' | 6 JSPF @ 60° |
| | | 3492 ' | 3496 ' | 4 ' | 6 JSPF @ 60° |
| | | 3482 ' | 3486 ' | 4 ' | 6 JSPF @ 60° |
| | | | | | |

**** Correlated to Halliburton Dual-Spaced Neutron/Spectral Density log dated 09/26/04.**




~ 60' > 80% bond with 2300' % BOND of top of revised proposed injection perfs. CK

Bill Barrett Corp. Prickly Pear Unit Federal 12-24 4300730953

DIVISION OF OIL, GAS AND MINING

UNDERGROUND INJECTION CONTROL PROGRAM

# PERMIT STATEMENT OF BASIS

**Applicant:** Bill Barrett Corp. **Well:** Prickly Pear Unit Federal 12-24

**Location:** S 24 T12S, R14E, Carbon Co., UT **API:** 43-007-30953

**Ownership Issues:**

The well is located on federal lands administered by the Bureau of Land Management. An affidavit of notification of operators, mineral owners, and surface owners located within a one-half (1/2) mile radius has been provided.

**Well Integrity:**

Description of the Casings and Cement:

CASING PROGRAM

| String Type | Hole Size | Depth | Feet | Casing Diameter | Weight | Grade | Connection Type |
|---|---|---|---|---|---|---|---|
| Conductor | | 40' | | 16" | | | |
| Surface | 12 ¼" | 1005' | 1002' | 9-5/8" | 36# | J-55 | ST&C |
| Production | 7 7/8" | 9496' | 9491' | 5 ½ " | 17# | L-80 | LT&C |

CEMENT PROGRAM

| String Type | DV Depth | Stage Lead/Tail | Cement Bottom | Cement Top | Number Sacks | Cement Type | Cement Yield | Cement Weight |
|---|---|---|---|---|---|---|---|---|
| Conductor | | | 40' | | | | | |
| Surface | | Lead | 1005' | Surface | 225 | HL Premium+adds | 1.85 | 12.7 |
| | | Tail | | | 190 | AG300+adds | 1.15 | 15.8 |
| Production | | Lead | 9496' | 740' (CBL) | 1850 | 50/50 POZ+adds | 1.49 | 13.4 |

Bill Barrett Corporation proposes to inject produced waters from the Prickly Pear Unit area (from the middle Wasatch Formation, including the Dark Canyon Conglomerate beds, the North Horn Formation and the upper part of the Price River Formation) and inject into an interval that includes the middle Wasatch Formation, including the Dark Canyon Conglomerate beds, the North Horn Formation and the upper part of the Price River Formation. The conversion procedure specifies isolating the junked portion of this hole below 7,665′ TD with 20 sacks of cement, acidizing the existing perfs within the proposed permitted injection interval and landing 2 3/8″ injection tubing with subsequent pressure testing of the tubing and casing. They propose to inject 2,000 barrels of field-produced water per day at an injection pressure of 2,000 psig.

The Operator had the well logged to obtain a Cement Bond Log (CBL) on 10/7/2004. An examination of the CBL reveals that sufficient cement with a bond index of 80% or greater is indicated to permit the well.

**Ground Water Protection:**

High quality water, water with Total Dissolved Solids (TDS) concentrations less than 800 milligrams / liter (mg/l), issues from springs and streams that arise from within Tertiary and upper Cretaceous strata along the Tavaputs Plateau. Determinations of the base of moderately saline ground water in nearby drilled wells indicates that it is estimated to be encountered at an elevation of about 3,000 feet (about 4,800 feet Total Depth) in the subject well. The proposed injection zone in the subject well is about 1,500 feet below the base of moderately saline ground water and is therefore unlikely to contaminate any quality fresh water resource. The 5½″ production casing was cemented to within about 800 feet of the surface. This should be adequate to protect superjacent aquifers containing quality water resources.

TDS values of water samples obtained from likely contributor produced water

source wells in the area ranged from 32,224 to 90,004 mg/l. Champion Technologies tested the samples and a report was issued on March 4, 2007. The samples generally grouped around 65,000 mg/l.

The proposed injection interval (middle Wasatch Formation, including the Dark Canyon Conglomerate beds, the North Horn Formation and the upper part of the Price River Formation) is primarily in the Wasatch – Green River Confining Unit, however it does contain a Utah component of the recognized Mesaverde Aquifer, that being the upper part of the Price River Formation. The Price River injection perforations are at about 7,600′ TD, are about 2,800′ below the Base of Moderately Saline Ground Water and are unlikely to meet the standard for classification as an Underground Source of Drinking Water (USDW). This opinion is supported by resistivity values, NaCl calculations and Total Dissolved Solids (TDS) estimations published in two industry water chemistry publications, one of which is Circular 87 produced by the Utah Geological Survey. For the Mesaverde Group calculated NaCl ranged from about 10,500 ppm to about 19,100 ppm and estimated TDS ranged from about 12,900 to about 23,000 mg/l. Additional support was garnered from subject well′s wireline log calculated Rws for the sandstones of the perforated interval, which provided that there were no calculated NaCl concentrations fresher than about 13,000 ppm using the conservative Humble Relationship ( a = 0.62 and m = 2.15) in the Archie Equation. Rw was determined using the relationship Rw = F / Ro. Ro was assumed equivalent to Rt in clean sands (API gamma radioactivity < 45) with obvious permeability, minimal neutron methane crossover and likely high water saturation. Porosity was determined by crossplot from the Neutron Density log. As discussed above, produced water from offset field wells, which largely produce from other sands within the same overall interval, but higher on the structure, could provide no ground water less saline than about 32,000 mg/l, a value in excess of the maximum 10,000 mg/L TDS standard for designation as a USDW.

A step rate test (SRT) is not planned for this well. Instead, Division management has elected to accept calculated Maximum Allowable Surface Pressures and fracture gradients based on observations from well production stimulation fracture data (Initial Shut In Pressures and the fluid pressure gradient of 0.4417 psi/ft).

The North Horn Aquifer is included within the greater Mesaverde Aquifer. Both aquifers are below the Green River / Wasatch Confining Unit, which is the first recognized, contiguous confining unit above the injection interval, although there are probably several unrecognized intervals capable of serving as confinement in the intervening column. In the subject application the Operator proposes such a status for a zone that is in the upper Price River but below their Price River proposed injection perforations (a lower confining interval). The upper Green River Formation also contains a recognized aquifer and water is produced from a shallow upper Green River Formation aquifer in the area.

The subject well appears to be situated on the north flank of the WNW trending trace of the Garmesa Fault, which is expressed at the surface as a system of joints, faults and grabens. This system is about 1½ miles SSW of the proposed salt-water disposal well and extends for about 5 miles to the northwest and 17 miles to the southeast from the nearest point of the system to the subject well. Surface mapping reveals that the system is known to extend to depth at least to the top of the Colton (Wasatch) Formation. In this area the Colton/Wasatch Formation is the basal stratigraphic unit of the Wasatch-Green River Confining Unit as well as being the stratigraphic unit at the floor of the relatively nearby wild and scenic Desolation Canyon section of the Green River. There is about 3,050′ of vertical separation between the injection zone and the Colton Formation in the floor of Desolation Canyon. It is not known with complete certainty if the fractures/faults penetrate into the upper Colton/Wasatch Formation. If the fracture/fault system was accessed, it

could potentially present a conduit for the movement of injectate toward the Green River. I consider this to be an unlikely scenario owing to the great vertical separation and the greater likelihood that the preponderant shales of the Colton/Wasatch, the North Horn and the Price River Formations will serve for confinement and the cement and casing will prevent the vertical migration of injectate. I do not consider the foregoing discussion to pose a significant impediment to granting an injection permit for this well but it is presented merely to confirm consideration.

After reviewing the application and documentation submitted by Bill Barrett Corporation, I find that the injection of the Unit produced waters into the proposed injection interval in the Prickly Pear Unit Federal12-24 well, will cause no diminution of the quality of the already poor quality water in the injection zone. After injection ceases, increased pressure about the wellbore will abate over time. It is therefore to be concluded that no long term negative surficial or ground water impacts are anticipated resultant of the proposed injection operation.

**Oil/Gas & Other Mineral Resources Protection:**

A review of production records of the fields in the area reveals that most of the production is coming from the Wasatch and North Horn Formations and the Mesaverde Group. Some minor production has also come from the Mancos Shale, the Dakota Sandstone and perhaps even from the lower Mesaverde Group. The productive sands are of fluvial origin and, while giving the appearance of being correlative, are typically discontinuous and therefore not contiguous reservoirs and unlikely to interfere with the pressures in the productive reservoirs higher on the structure. No other known potentially producible mineral or hydrocarbon zones are reported in the area.

The well records of the Division document that there are no other wells within the half (1/2) mile area of review (AOR).

**Bonding:**

Bill Barrett Corporation has a $120,000 blanket surety bond in place, which ensures plugging of this well. Bond No. LPM4138148, issued by Fidelity and Deposit Company of Maryland.

**Actions Taken and Further Approvals Needed:**

Notice of this application was published in the Salt Lake Tribune and the Carbon County Sun Advocate. In addition, copies of the notice were provided to the Environmental Protection Agency (EPA), Region VIII, Bureau of Land Management (BLM) Moab, Carbon County Planning, Petro-Canada Resources and the Operator.

A properly designed and constructed water disposal well, combined with periodic mechanical integrity tests, poses no threat to fresh or useable groundwater supplies.

The Division staff recommends approval of this application contingent upon no additional or unforeseen information being presented that is relevant to this analysis or modifies the data presented herein.

Reviewer(s): Christopher J. Kierst Date: 7/27/07

JON M. HUNTSMAN, JR.
*Governor*

GARY R. HERBERT
*Lieutenant Governor*

# State of Utah
**DEPARTMENT OF NATURAL RESOURCES**

MICHAEL R. STYLER
*Executive Director*

**Division of Oil Gas and Mining**

JOHN R. BAZA
*Division Director*

July 31, 2007

Bill Barrett Corporation
1099 18th Street, Suite 2300
Denver, Colorado 80202

Re: Application for Class II Injection Permit, Prickly Pear Unit Federal 12-24 Well, Section 24, Township 12 South, Range 14 East, Carbon County, Utah, API 43-007-30953

Dear Sir:

Pursuant to Utah Admin. Code R649-5-3-3, the Division of Oil, Gas and Mining (the "Division") issues its administrative approval for conversion of the referenced well to a Class II injection well. Accordingly, the following stipulations shall apply for full compliance with this approval and a permit may be issued upon compliance with the stipulations.

1. Conformance with all conditions and requirements of the complete application submitted by Bill Barrett Corporation.

2. Compliance with all applicable requirements for the operation, maintenance and reporting for Underground Injection Control ("UIC") Class II injection wells pursuant to Utah Admin. Code R649-1 et seq.

3. A casing/tubing pressure test shall be conducted prior to commencing injection.

Note that this letter does not constitute final approval to commence injection operations. This approval is only temporary and allows Bill Barrett Corporation to perform activities and gather information necessary for the Division to issue a Class II Underground Injection Control permit.

If you have any questions regarding this approval or the necessary requirements, please contact Christopher Kierst at (801) 538-5337.

Sincerely,

Gil Hunt
Associate Director

CJK:er
cc: EPA, Dan Jackson
Carbon County Commission

**From:** Tracey Fallang <tfallang@billbarrettcorp.com>
**To:** Chris Kierst <chriskierst@utah.gov>
**Date:** 07/10/2008 10:21 AM
**Subject:** RE: FW: Prickly Pear 12-24 Injection Well-Additional Wasatch perforations.

Thanks Chris. And just to reconfirm, our current max injection pressure will be 2000 psi as per the application.

-----Original Message-----
From: Chris Kierst [mailto:chriskierst@utah.gov]
Sent: Thursday, July 10, 2008 10:04 AM
To: Tracey Fallang
Subject: Re: FW: Prickly Pear 12-24 Injection Well-Additional Wasatch perforations.

Please continue to use the current zone within the context of the permission to proceed that we have already granted for the zone. We will inform you if we reach a point where the Division feels the need to write a permanent permit for the zone.

As regards the request to open up new perforations in the Wasatch Formation, this constitutes a permit modification and we need to have this Noticed (15 days during standard 5 day work weeks) and a Sundry submitted informing us of the proposed activities in the well and a new UIC Form 1 to initiate the permit modification process. In addition, we need a map informing us of the proximity of Wasatch Formation production to the subject well and a geologic defense of the selection of the proposed productive zone for injection of produced water.

Please feel free to contact me if you need additional information or guidance in this matter.

(801) 538-5337

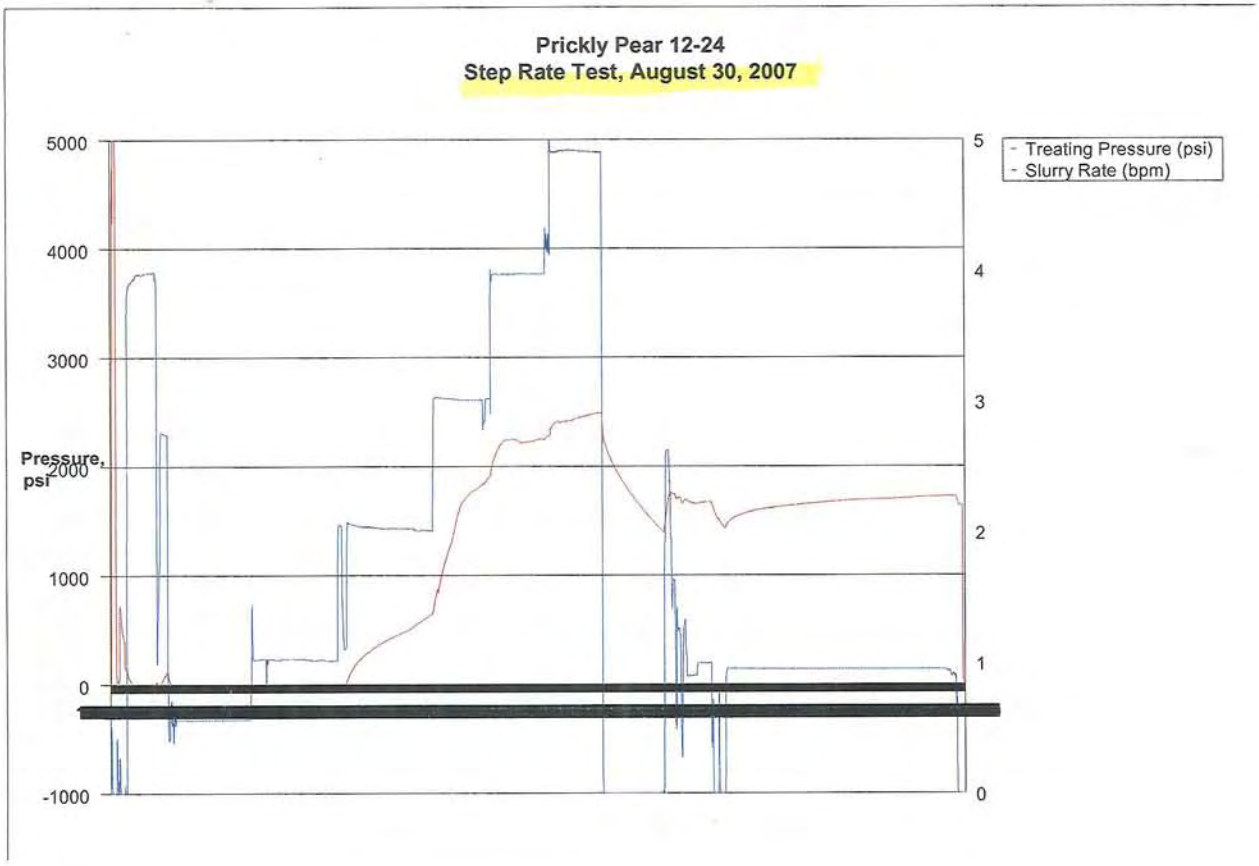
8/30/07

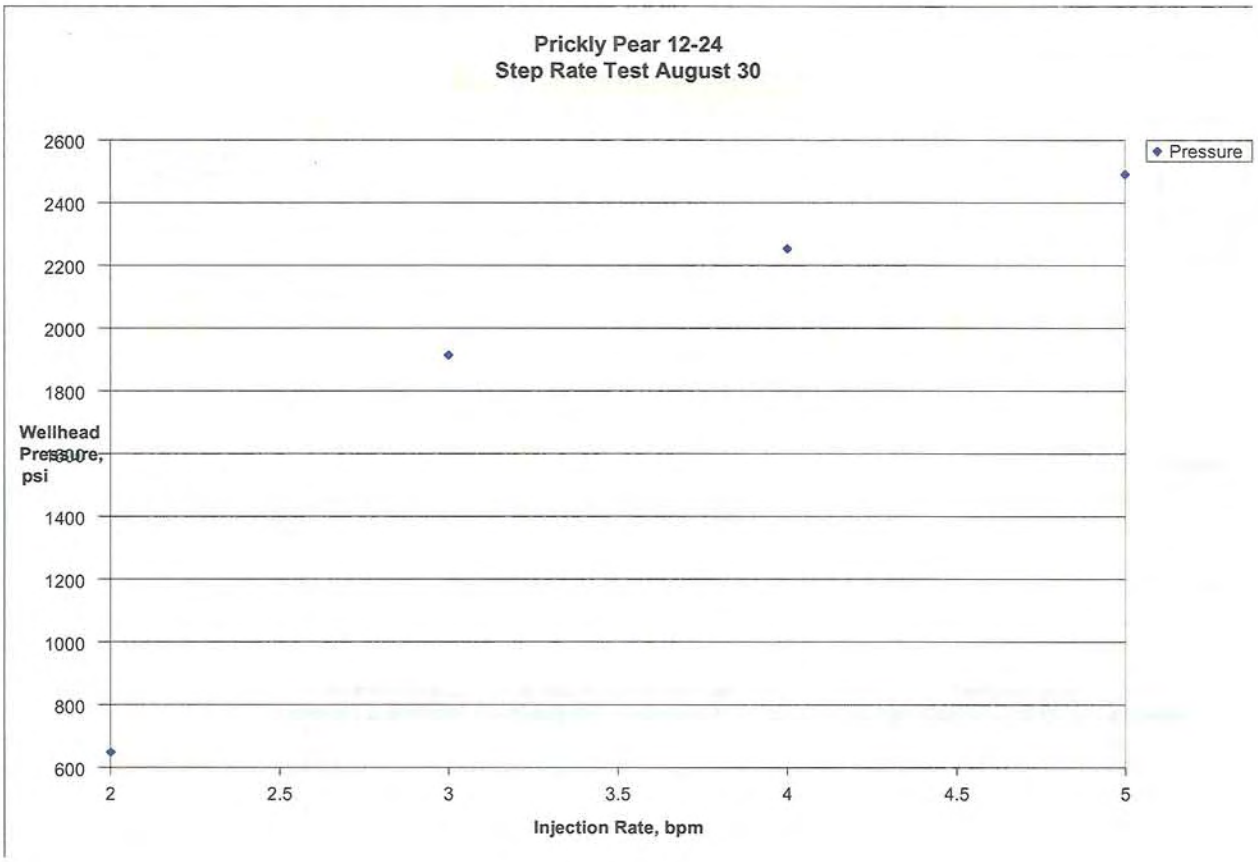
>>> Tracey Fallang <tfallang@billbarrettcorp.com> 07/07/2008 10:56 AM >>>
Chris, as a refresher on this, we had submitted the initial UIC application in April 2007. We received administrative approval in July 2007, conducted the step-rate test & MIT and then conducted an initial injection test in May 2008. The initial rate was approximately 500 BWPD @ 1200 psi, then dropped to 375 BWPD @ 1750 psi and finally ended up at 230 BWPD @ 1750 psi. These results are not sufficient to maintain a viable disposal facility. We have taken another look at the logs on this well and have found a number of intervals in the Wasatch that may have water injection potential (BBC does currently produce hydrocarbons out of the Wasatch in both Prickly Pear and Peter's Point).

North Horsetail

My question to you is - what additional information needs to be provided for approval of these additional perfs and to also move forward with testing of this interval? I've attached the procedure and Wasatch perf information.

Thank you.


Prickly Pear 12-24
Step Rate Test, August 30, 2007
5000
4000
3000
2000
1000
0
-1000
Pressure, psi
5
4
3
2
1
0
Treating Pressure (psi)
Slurry Rate (bpm)


Prickly Pear 12-24
Step Rate Test August 30
Pressure
2600
2400
2200
2000
1800
1600
1400
1200
1000
800
600
Wellhead Pressure, psi
2
2.5
3
3.5
4
4.5
5
Injection Rate, bpm

Bill Barrett Corp
Prickly Pear 12-24
Step Rate Test

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:05:42 | 9 | 0.0 | 0.18 |
| 12:05:43 | 9 | 0.0 | 0.18 |
| 12:05:44 | 10 | 0.0 | 0.18 |
| 12:05:45 | 11 | 0.0 | 0.18 |
| 12:05:46 | 12 | 0.0 | 0.18 |
| 12:05:47 | 14 | 0.0 | 0.18 |
| 12:05:48 | 15 | 0.2 | 0.19 |
| 12:05:49 | 17 | 0.3 | 0.19 |
| 12:05:50 | 19 | 0.4 | 0.20 |
| 12:05:51 | 21 | 0.4 | 0.20 |
| 12:05:52 | 24 | 0.4 | 0.21 |
| 12:05:53 | 28 | 0.5 | 0.22 |
| 12:05:54 | 33 | 0.5 | 0.23 |
| 12:05:55 | 39 | 0.5 | 0.24 |
| 12:05:56 | 57 | 0.5 | 0.25 |
| 12:05:57 | 105 | 0.5 | 0.25 |
| 12:05:58 | 178 | 0.5 | 0.26 |
| 12:05:59 | 278 | 0.4 | 0.27 |
| 12:06:00 | 505 | 0.4 | 0.27 |
| 12:06:01 | 1040 | 0.3 | 0.28 |
| 12:06:02 | 2139 | 0.2 | 0.28 |
| 12:06:03 | 2722 | 0.2 | 0.29 |
| 12:06:04 | 2864 | 0.1 | 0.29 |
| 12:06:05 | 2941 | 0.1 | 0.29 |
| 12:06:06 | 2950 | 0.1 | 0.29 |
| 12:06:07 | 2956 | 0.0 | 0.29 |
| 12:06:08 | 2960 | 0.0 | 0.29 |
| 12:06:09 | 2962 | 0.0 | 0.29 |
| 12:06:10 | 2962 | 0.0 | 0.29 |
| 12:06:11 | 2961 | 0.0 | 0.29 |
| 12:06:12 | 3031 | 0.0 | 0.29 |
| 12:06:13 | 3591 | 0.0 | 0.29 |
| 12:06:14 | 4129 | 0.0 | 0.29 |
| 12:06:15 | 4429 | 0.0 | 0.29 |
| 12:06:16 | 4682 | 0.0 | 0.29 |
| 12:06:17 | 4729 | 0.0 | 0.29 |
| 12:06:18 | 4620 | 0.0 | 0.29 |
| 12:06:19 | 4491 | 0.0 | 0.29 |
| 12:06:20 | 4407 | 0.0 | 0.29 |
| 12:06:21 | 4342 | 0.0 | 0.29 |
| 12:06:22 | 4310 | 0.0 | 0.29 |
| 12:06:23 | 4296 | 0.0 | 0.29 |

| Ave Rate | Wellhead Pressure |
|---|---|
| 2 | 650 |
| 3 | 1915 |
| 4 | 2254 |
| 5 | 2492 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:06:24 | 4286 | 0.0 | 0.29 |
| 12:06:25 | 4276 | 0.0 | 0.29 |
| 12:06:26 | 4267 | 0.0 | 0.29 |
| 12:06:27 | 4259 | 0.0 | 0.29 |
| 12:06:28 | 4251 | 0.0 | 0.29 |
| 12:06:29 | 4244 | 0.0 | 0.29 |
| 12:06:30 | 4237 | 0.0 | 0.29 |
| 12:06:31 | 4233 | 0.0 | 0.29 |
| 12:06:32 | 4698 | 0.0 | 0.29 |
| 12:06:33 | 4898 | 0.0 | 0.29 |
| 12:06:34 | 4962 | 0.0 | 0.29 |
| 12:06:35 | 4972 | 0.0 | 0.29 |
| 12:06:36 | 4980 | 0.0 | 0.29 |
| 12:06:37 | 4986 | 0.0 | 0.29 |
| 12:06:38 | 4991 | 0.0 | 0.29 |
| 12:06:39 | 4995 | 0.0 | 0.29 |
| 12:06:40 | 4998 | 0.0 | 0.29 |
| 12:06:41 | 5000 | 0.0 | 0.29 |
| 12:06:42 | 5001 | 0.0 | 0.29 |
| 12:06:43 | 5002 | 0.0 | 0.29 |
| 12:06:44 | 5003 | 0.0 | 0.29 |
| 12:06:45 | 5003 | 0.0 | 0.29 |
| 12:06:46 | 5002 | 0.0 | 0.29 |
| 12:06:47 | 5001 | 0.0 | 0.29 |
| 12:06:48 | 5001 | 0.0 | 0.29 |
| 12:06:49 | 5000 | 0.0 | 0.29 |
| 12:06:50 | 4998 | 0.0 | 0.29 |
| 12:06:51 | 4997 | 0.0 | 0.29 |
| 12:06:52 | 4996 | 0.0 | 0.29 |
| 12:06:53 | 4994 | 0.0 | 0.29 |
| 12:06:54 | 4993 | 0.0 | 0.29 |
| 12:06:55 | 4992 | 0.0 | 0.29 |
| 12:06:56 | 4990 | 0.0 | 0.29 |
| 12:06:57 | 4989 | 0.0 | 0.29 |
| 12:06:58 | 4987 | 0.0 | 0.29 |
| 12:06:59 | 4986 | 0.0 | 0.29 |
| 12:07:00 | 4984 | 0.0 | 0.29 |
| 12:07:01 | 4983 | 0.0 | 0.29 |
| 12:07:02 | 4982 | 0.0 | 0.29 |
| 12:07:03 | 4980 | 0.0 | 0.29 |
| 12:07:04 | 4979 | 0.0 | 0.29 |
| 12:07:05 | 4978 | 0.0 | 0.29 |
| 12:07:06 | 4976 | 0.0 | 0.29 |
| 12:07:07 | 4975 | 0.0 | 0.29 |
| 12:07:08 | 4974 | 0.0 | 0.29 |
| 12:07:09 | 4973 | 0.0 | 0.29 |
| 12:07:10 | 4971 | 0.0 | 0.29 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:07:11 | 4968 | 0.0 | 0.29 |
| 12:07:12 | 4965 | 0.0 | 0.29 |
| 12:07:13 | 4960 | 0.0 | 0.29 |
| 12:07:14 | 4953 | 0.0 | 0.29 |
| 12:07:15 | 4926 | 0.0 | 0.29 |
| 12:07:16 | 4911 | 0.0 | 0.29 |
| 12:07:17 | 4828 | 0.0 | 0.29 |
| 12:07:18 | 4445 | 0.0 | 0.29 |
| 12:07:19 | 2982 | 0.0 | 0.29 |
| 12:07:20 | 1633 | 0.0 | 0.29 |
| 12:07:21 | 813 | 0.0 | 0.29 |
| 12:07:22 | 489 | 0.0 | 0.29 |
| 12:07:23 | 324 | 0.1 | 0.30 |
| 12:07:24 | 242 | 0.2 | 0.30 |
| 12:07:25 | 173 | 0.2 | 0.30 |
| 12:07:26 | 127 | 0.4 | 0.31 |
| 12:07:27 | 116 | 0.4 | 0.31 |
| 12:07:28 | 106 | 0.4 | 0.32 |
| 12:07:29 | 96 | 0.4 | 0.33 |
| 12:07:30 | 86 | 0.4 | 0.34 |
| 12:07:31 | 77 | 0.4 | 0.34 |
| 12:07:32 | 69 | 0.4 | 0.35 |
| 12:07:33 | 61 | 0.4 | 0.35 |
| 12:07:34 | 55 | 0.4 | 0.36 |
| 12:07:35 | 49 | 0.3 | 0.37 |
| 12:07:36 | 44 | 0.3 | 0.37 |
| 12:07:37 | 39 | 0.2 | 0.37 |
| 12:07:38 | 36 | 0.1 | 0.38 |
| 12:07:39 | 33 | 0.1 | 0.38 |
| 12:07:40 | 30 | 0.1 | 0.38 |
| 12:07:41 | 28 | 0.1 | 0.38 |
| 12:07:42 | 26 | 0.0 | 0.38 |
| 12:07:43 | 25 | 0.0 | 0.38 |
| 12:07:44 | 23 | 0.0 | 0.38 |
| 12:07:45 | 22 | 0.0 | 0.38 |
| 12:07:46 | 21 | 0.0 | 0.38 |
| 12:07:47 | 20 | 0.0 | 0.38 |
| 12:07:48 | 20 | 0.0 | 0.38 |
| 12:07:49 | 19 | 0.0 | 0.38 |
| 12:07:50 | 19 | 0.0 | 0.38 |
| 12:07:51 | 19 | 0.0 | 0.38 |
| 12:07:52 | 18 | 0.0 | 0.38 |
| 12:07:53 | 18 | 0.0 | 0.38 |
| 12:07:54 | 18 | 0.0 | 0.38 |
| 12:07:55 | 18 | 0.0 | 0.38 |
| 12:07:56 | 18 | 0.0 | 0.38 |
| 12:07:57 | 18 | 0.0 | 0.38 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:07:58 | 18 | 0.1 | 0.38 |
| 12:07:59 | 18 | 0.1 | 0.38 |
| 12:08:00 | 18 | 0.1 | 0.39 |
| 12:08:01 | 19 | 0.1 | 0.39 |
| 12:08:02 | 19 | 0.1 | 0.39 |
| 12:08:03 | 20 | 0.1 | 0.39 |
| 12:08:04 | 21 | 0.0 | 0.39 |
| 12:08:05 | 22 | 0.0 | 0.39 |
| 12:08:06 | 23 | 0.0 | 0.39 |
| 12:08:07 | 24 | 0.0 | 0.39 |
| 12:08:08 | 26 | 0.0 | 0.39 |
| 12:08:09 | 28 | 0.1 | 0.39 |
| 12:08:10 | 30 | 0.2 | 0.40 |
| 12:08:11 | 32 | 0.2 | 0.40 |
| 12:08:12 | 35 | 0.2 | 0.40 |
| 12:08:13 | 38 | 0.2 | 0.41 |
| 12:08:14 | 42 | 0.2 | 0.41 |
| 12:08:15 | 46 | 0.2 | 0.42 |
| 12:08:16 | 52 | 0.3 | 0.42 |
| 12:08:17 | 59 | 0.3 | 0.42 |
| 12:08:18 | 67 | 0.3 | 0.43 |
| 12:08:19 | 103 | 0.3 | 0.43 |
| 12:08:20 | 154 | 0.3 | 0.44 |
| 12:08:21 | 226 | 0.3 | 0.44 |
| 12:08:22 | 454 | 0.3 | 0.45 |
| 12:08:23 | 656 | 0.2 | 0.45 |
| 12:08:24 | 702 | 0.2 | 0.45 |
| 12:08:25 | 709 | 0.2 | 0.46 |
| 12:08:26 | 714 | 0.1 | 0.46 |
| 12:08:27 | 717 | 0.1 | 0.46 |
| 12:08:28 | 718 | 0.1 | 0.46 |
| 12:08:29 | 718 | 0.1 | 0.46 |
| 12:08:30 | 717 | 0.0 | 0.46 |
| 12:08:31 | 716 | 0.0 | 0.46 |
| 12:08:32 | 714 | 0.0 | 0.46 |
| 12:08:33 | 712 | 0.0 | 0.46 |
| 12:08:34 | 709 | 0.0 | 0.46 |
| 12:08:35 | 706 | 0.0 | 0.47 |
| 12:08:36 | 702 | 0.0 | 0.47 |
| 12:08:37 | 698 | 0.0 | 0.47 |
| 12:08:38 | 693 | 0.0 | 0.47 |
| 12:08:39 | 686 | 0.0 | 0.47 |
| 12:08:40 | 677 | 0.0 | 0.47 |
| 12:08:41 | 667 | 0.0 | 0.47 |
| 12:08:42 | 653 | 0.0 | 0.47 |
| 12:08:43 | 643 | 0.0 | 0.47 |
| 12:08:44 | 633 | 0.0 | 0.47 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:08:45 | 625 | 0.0 | 0.47 |
| 12:08:46 | 616 | 0.0 | 0.47 |
| 12:08:47 | 608 | 0.0 | 0.47 |
| 12:08:48 | 600 | 0.0 | 0.47 |
| 12:08:49 | 593 | 0.0 | 0.47 |
| 12:08:50 | 585 | 0.0 | 0.47 |
| 12:08:51 | 577 | 0.0 | 0.47 |
| 12:08:52 | 570 | 0.0 | 0.47 |
| 12:08:53 | 564 | 0.0 | 0.47 |
| 12:08:54 | 558 | 0.0 | 0.47 |
| 12:08:55 | 553 | 0.0 | 0.47 |
| 12:08:56 | 547 | 0.0 | 0.47 |
| 12:08:57 | 542 | 0.0 | 0.47 |
| 12:08:58 | 537 | 0.0 | 0.47 |
| 12:08:59 | 532 | 0.0 | 0.47 |
| 12:09:00 | 528 | 0.0 | 0.47 |
| 12:09:01 | 523 | 0.0 | 0.47 |
| 12:09:02 | 519 | 0.0 | 0.47 |
| 12:09:03 | 515 | 0.0 | 0.47 |
| 12:09:04 | 510 | 0.0 | 0.47 |
| 12:09:05 | 506 | 0.0 | 0.47 |
| 12:09:06 | 502 | 0.0 | 0.47 |
| 12:09:07 | 499 | 0.0 | 0.47 |
| 12:09:08 | 495 | 0.0 | 0.47 |
| 12:09:09 | 491 | 0.0 | 0.47 |
| 12:09:10 | 488 | 0.0 | 0.47 |
| 12:09:11 | 483 | 0.0 | 0.47 |
| 12:09:12 | 480 | 0.0 | 0.47 |
| 12:09:13 | 477 | 0.0 | 0.47 |
| 12:09:14 | 473 | 0.0 | 0.47 |
| 12:09:15 | 470 | 0.0 | 0.47 |
| 12:09:16 | 467 | 0.0 | 0.47 |
| 12:09:17 | 464 | 0.0 | 0.47 |
| 12:09:18 | 462 | 0.0 | 0.47 |
| 12:09:19 | 459 | 0.0 | 0.47 |
| 12:09:20 | 456 | 0.0 | 0.47 |
| 12:09:21 | 453 | 0.0 | 0.47 |
| 12:09:22 | 450 | 0.0 | 0.47 |
| 12:09:23 | 448 | 0.0 | 0.47 |
| 12:09:24 | 445 | 0.0 | 0.47 |
| 12:09:25 | 443 | 0.0 | 0.47 |
| 12:09:26 | 440 | 0.0 | 0.47 |
| 12:09:27 | 437 | 0.0 | 0.47 |
| 12:09:28 | 435 | 0.0 | 0.47 |
| 12:09:29 | 433 | 0.0 | 0.47 |
| 12:09:30 | 432 | 0.0 | 0.47 |
| 12:09:31 | 431 | 0.0 | 0.47 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:09:32 | 429 | 0.0 | 0.47 |
| 12:09:33 | 428 | 0.0 | 0.47 |
| 12:09:34 | 428 | 0.0 | 0.47 |
| 12:09:35 | 427 | 0.0 | 0.47 |
| 12:09:36 | 426 | 0.0 | 0.47 |
| 12:09:37 | 426 | 0.0 | 0.47 |
| 12:09:38 | 426 | 0.0 | 0.47 |
| 12:09:39 | 425 | 0.0 | 0.47 |
| 12:09:40 | 420 | 0.0 | 0.47 |
| 12:09:41 | 414 | 0.0 | 0.47 |
| 12:09:42 | 409 | 0.0 | 0.47 |
| 12:09:43 | 404 | 0.0 | 0.47 |
| 12:09:44 | 400 | 0.0 | 0.47 |
| 12:09:45 | 396 | 0.0 | 0.47 |
| 12:09:46 | 393 | 0.0 | 0.47 |
| 12:09:47 | 391 | 0.0 | 0.47 |
| 12:09:48 | 388 | 0.0 | 0.47 |
| 12:09:49 | 371 | 0.0 | 0.47 |
| 12:09:50 | 287 | 0.1 | 0.47 |
| 12:09:51 | 219 | 0.1 | 0.47 |
| 12:09:52 | 200 | 0.0 | 0.47 |
| 12:09:53 | 192 | 0.0 | 0.47 |
| 12:09:54 | 182 | 0.0 | 0.47 |
| 12:09:55 | 176 | 0.0 | 0.47 |
| 12:09:56 | 170 | 0.0 | 0.47 |
| 12:09:57 | 166 | 0.0 | 0.47 |
| 12:09:58 | 162 | 0.0 | 0.47 |
| 12:09:59 | 158 | 0.0 | 0.47 |
| 12:10:00 | 155 | 0.0 | 0.47 |
| 12:10:01 | 153 | 0.0 | 0.47 |
| 12:10:02 | 150 | 0.0 | 0.47 |
| 12:10:03 | 149 | 0.0 | 0.47 |
| 12:10:04 | 147 | 0.0 | 0.47 |
| 12:10:05 | 146 | 0.0 | 0.47 |
| 12:10:06 | 144 | 0.0 | 0.47 |
| 12:10:07 | 143 | 0.0 | 0.47 |
| 12:10:08 | 143 | 0.0 | 0.00 |
| 12:10:09 | 142 | 0.0 | 0.00 |
| 12:10:10 | 141 | 0.0 | 0.00 |
| 12:10:11 | 141 | 0.0 | 0.00 |
| 12:10:12 | 140 | 0.0 | 0.00 |
| 12:10:13 | 140 | 0.0 | 0.00 |
| 12:10:14 | 139 | 0.0 | 0.00 |
| 12:10:15 | 139 | 0.0 | 0.00 |
| 12:10:16 | 139 | 0.0 | 0.00 |
| 12:10:17 | 138 | 0.0 | 0.00 |
| 12:10:18 | 138 | 0.0 | 0.00 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:10:19 | 138 | 0.0 | 0.00 |
| 12:10:20 | 138 | 0.0 | 0.00 |
| 12:10:21 | 138 | 0.0 | 0.00 |
| 12:10:22 | 138 | 0.0 | 0.00 |
| 12:10:23 | 138 | 0.3 | 0.00 |
| 12:10:24 | 138 | 0.6 | 0.02 |
| 12:10:25 | 138 | 1.0 | 0.03 |
| 12:10:26 | 138 | 1.4 | 0.06 |
| 12:10:27 | 139 | 1.9 | 0.09 |
| 12:10:28 | 139 | 2.6 | 0.13 |
| 12:10:29 | 139 | 3.0 | 0.18 |
| 12:10:30 | 139 | 3.3 | 0.23 |
| 12:10:31 | 137 | 3.5 | 0.29 |
| 12:10:32 | 136 | 3.7 | 0.35 |
| 12:10:33 | 133 | 3.7 | 0.42 |
| 12:10:34 | 130 | 3.7 | 0.48 |
| 12:10:35 | 127 | 3.7 | 0.54 |
| 12:10:36 | 123 | 3.7 | 0.60 |
| 12:10:37 | 118 | 3.8 | 0.67 |
| 12:10:38 | 115 | 3.8 | 0.73 |
| 12:10:39 | 111 | 3.8 | 0.79 |
| 12:10:40 | 108 | 3.8 | 0.85 |
| 12:10:41 | 105 | 3.8 | 0.92 |
| 12:10:42 | 101 | 3.8 | 0.98 |
| 12:10:43 | 98 | 3.8 | 1.05 |
| 12:10:44 | 95 | 3.8 | 1.11 |
| 12:10:45 | 93 | 3.8 | 1.17 |
| 12:10:46 | 90 | 3.8 | 1.24 |
| 12:10:47 | 88 | 3.9 | 1.30 |
| 12:10:48 | 85 | 3.9 | 1.37 |
| 12:10:49 | 83 | 3.9 | 1.43 |
| 12:10:50 | 81 | 3.9 | 1.50 |
| 12:10:51 | 79 | 3.9 | 1.56 |
| 12:10:52 | 78 | 3.9 | 1.62 |
| 12:10:53 | 76 | 3.9 | 1.69 |
| 12:10:54 | 74 | 3.9 | 1.75 |
| 12:10:55 | 73 | 3.9 | 1.82 |
| 12:10:56 | 72 | 3.9 | 1.88 |
| 12:10:57 | 70 | 3.9 | 1.95 |
| 12:10:58 | 69 | 3.9 | 2.01 |
| 12:10:59 | 68 | 3.9 | 2.08 |
| 12:11:00 | 67 | 3.9 | 2.14 |
| 12:11:01 | 65 | 3.9 | 2.20 |
| 12:11:02 | 64 | 3.9 | 2.27 |
| 12:11:03 | 63 | 3.9 | 2.33 |
| 12:11:04 | 62 | 3.9 | 2.40 |
| 12:11:05 | 62 | 3.9 | 2.46 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:11:06 | 61 | 3.9 | 2.53 |
| 12:11:07 | 60 | 3.9 | 2.59 |
| 12:11:08 | 59 | 3.9 | 2.66 |
| 12:11:09 | 58 | 3.9 | 2.72 |
| 12:11:10 | 57 | 3.9 | 2.79 |
| 12:11:11 | 56 | 3.9 | 2.85 |
| 12:11:12 | 55 | 3.9 | 2.92 |
| 12:11:13 | 54 | 3.9 | 2.98 |
| 12:11:14 | 53 | 3.9 | 3.05 |
| 12:11:15 | 52 | 3.9 | 3.11 |
| 12:11:16 | 51 | 3.9 | 3.18 |
| 12:11:17 | 50 | 3.9 | 3.25 |
| 12:11:18 | 49 | 3.9 | 3.32 |
| 12:11:19 | 48 | 3.9 | 3.38 |
| 12:11:20 | 47 | 3.9 | 3.45 |
| 12:11:21 | 46 | 3.9 | 3.51 |
| 12:11:22 | 46 | 3.9 | 3.58 |
| 12:11:23 | 45 | 3.9 | 3.64 |
| 12:11:24 | 44 | 3.9 | 3.71 |
| 12:11:25 | 43 | 3.9 | 3.77 |
| 12:11:26 | 42 | 3.9 | 3.84 |
| 12:11:27 | 41 | 3.9 | 3.90 |
| 12:11:28 | 40 | 3.9 | 3.97 |
| 12:11:29 | 39 | 3.9 | 4.03 |
| 12:11:30 | 38 | 3.9 | 4.10 |
| 12:11:31 | 37 | 3.9 | 4.16 |
| 12:11:32 | 37 | 3.9 | 4.23 |
| 12:11:33 | 36 | 3.9 | 4.29 |
| 12:11:34 | 35 | 3.9 | 4.36 |
| 12:11:35 | 34 | 3.9 | 4.42 |
| 12:11:36 | 33 | 3.9 | 4.49 |
| 12:11:37 | 32 | 3.9 | 4.55 |
| 12:11:38 | 31 | 3.9 | 4.62 |
| 12:11:39 | 30 | 3.9 | 4.68 |
| 12:11:40 | 29 | 3.9 | 4.75 |
| 12:11:41 | 28 | 3.9 | 4.81 |
| 12:11:42 | 27 | 3.9 | 4.88 |
| 12:11:43 | 26 | 3.9 | 4.94 |
| 12:11:44 | 25 | 3.9 | 5.01 |
| 12:11:45 | 24 | 3.9 | 5.07 |
| 12:11:46 | 24 | 3.9 | 5.14 |
| 12:11:47 | 23 | 3.9 | 5.20 |
| 12:11:48 | 22 | 3.9 | 5.27 |
| 12:11:49 | 21 | 3.9 | 5.33 |
| 12:11:50 | 20 | 3.9 | 5.40 |
| 12:11:51 | 19 | 3.9 | 5.46 |
| 12:11:52 | 18 | 3.9 | 5.53 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:11:53 | 17 | 3.9 | 5.59 |
| 12:11:54 | 16 | 3.9 | 5.66 |
| 12:11:55 | 15 | 3.9 | 5.72 |
| 12:11:56 | 14 | 3.9 | 5.79 |
| 12:11:57 | 13 | 3.9 | 5.85 |
| 12:11:58 | 12 | 3.9 | 5.92 |
| 12:11:59 | 11 | 3.9 | 5.99 |
| 12:12:00 | 10 | 3.9 | 6.05 |
| 12:12:01 | 9 | 3.9 | 6.12 |
| 12:12:02 | 8 | 3.9 | 6.18 |
| 12:12:03 | 8 | 3.9 | 6.25 |
| 12:12:04 | 7 | 3.9 | 6.31 |
| 12:12:05 | 6 | 3.9 | 6.38 |
| 12:12:06 | 5 | 3.9 | 6.44 |
| 12:12:07 | 4 | 3.9 | 6.51 |
| 12:12:08 | 3 | 3.9 | 6.57 |
| 12:12:09 | 2 | 3.9 | 6.64 |
| 12:12:10 | 1 | 3.9 | 6.70 |
| 12:12:11 | 0 | 3.9 | 6.77 |
| 12:12:12 | -1 | 3.9 | 6.83 |
| 12:12:13 | -2 | 3.9 | 6.90 |
| 12:12:14 | -3 | 3.9 | 6.96 |
| 12:12:15 | -4 | 3.9 | 7.03 |
| 12:12:16 | -4 | 3.9 | 7.09 |
| 12:12:17 | -5 | 3.9 | 7.16 |
| 12:12:18 | -7 | 3.9 | 7.23 |
| 12:12:19 | -7 | 3.9 | 7.29 |
| 12:12:20 | -8 | 3.9 | 7.36 |
| 12:12:21 | -9 | 3.9 | 7.42 |
| 12:12:22 | -10 | 3.9 | 7.49 |
| 12:12:23 | -11 | 3.9 | 7.55 |
| 12:12:24 | -12 | 3.9 | 7.62 |
| 12:12:25 | -13 | 3.9 | 7.68 |
| 12:12:26 | -14 | 3.9 | 7.75 |
| 12:12:27 | -15 | 3.9 | 7.82 |
| 12:12:28 | -15 | 3.9 | 7.88 |
| 12:12:29 | -16 | 3.9 | 7.95 |
| 12:12:30 | -17 | 3.9 | 8.01 |
| 12:12:31 | -18 | 3.9 | 8.08 |
| 12:12:32 | -19 | 3.9 | 8.14 |
| 12:12:33 | -20 | 3.9 | 8.22 |
| 12:12:34 | -20 | 3.9 | 8.28 |
| 12:12:35 | -21 | 3.9 | 8.35 |
| 12:12:36 | -22 | 3.9 | 8.41 |
| 12:12:37 | -23 | 3.9 | 8.48 |
| 12:12:38 | -23 | 3.9 | 8.54 |
| 12:12:39 | -24 | 3.9 | 8.61 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:12:40 | -24 | 3.9 | 8.68 |
| 12:12:41 | -24 | 3.9 | 8.74 |
| 12:12:42 | -25 | 3.9 | 8.81 |
| 12:12:43 | -25 | 3.9 | 8.87 |
| 12:12:44 | -25 | 3.9 | 8.94 |
| 12:12:45 | -25 | 3.9 | 9.00 |
| 12:12:46 | -26 | 3.9 | 9.07 |
| 12:12:47 | -26 | 3.9 | 9.13 |
| 12:12:48 | -26 | 3.9 | 9.20 |
| 12:12:49 | -26 | 3.9 | 9.27 |
| 12:12:50 | -26 | 3.9 | 9.33 |
| 12:12:51 | -26 | 3.9 | 9.40 |
| 12:12:52 | -26 | 3.9 | 9.46 |
| 12:12:53 | -26 | 3.9 | 9.53 |
| 12:12:54 | -26 | 3.9 | 9.59 |
| 12:12:55 | -26 | 3.9 | 9.66 |
| 12:12:56 | -26 | 3.9 | 9.73 |
| 12:12:57 | -26 | 3.9 | 9.79 |
| 12:12:58 | -27 | 3.9 | 9.86 |
| 12:12:59 | -27 | 3.9 | 9.92 |
| 12:13:00 | -27 | 4.0 | 9.99 |
| 12:13:01 | -27 | 4.0 | 10.05 |
| 12:13:02 | -27 | 4.0 | 10.12 |
| 12:13:03 | -27 | 4.0 | 10.19 |
| 12:13:04 | -27 | 4.0 | 10.25 |
| 12:13:05 | -27 | 4.0 | 10.32 |
| 12:13:06 | -27 | 4.0 | 10.39 |
| 12:13:07 | -27 | 4.0 | 10.45 |
| 12:13:08 | -27 | 4.0 | 10.52 |
| 12:13:09 | -27 | 4.0 | 10.58 |
| 12:13:10 | -27 | 4.0 | 10.65 |
| 12:13:11 | -27 | 4.0 | 10.72 |
| 12:13:12 | -27 | 4.0 | 10.78 |
| 12:13:13 | -27 | 4.0 | 10.85 |
| 12:13:14 | -27 | 4.0 | 10.91 |
| 12:13:15 | -28 | 4.0 | 10.98 |
| 12:13:16 | -28 | 4.0 | 11.05 |
| 12:13:17 | -28 | 4.0 | 11.11 |
| 12:13:18 | -28 | 4.0 | 11.18 |
| 12:13:19 | -28 | 4.0 | 11.24 |
| 12:13:20 | -28 | 4.0 | 11.31 |
| 12:13:21 | -28 | 4.0 | 11.38 |
| 12:13:22 | -28 | 4.0 | 11.44 |
| 12:13:23 | -28 | 4.0 | 11.51 |
| 12:13:24 | -28 | 4.0 | 11.58 |
| 12:13:25 | -28 | 4.0 | 11.64 |
| 12:13:26 | -28 | 4.0 | 11.71 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:13:27 | -28 | 4.0 | 11.77 |
| 12:13:28 | -28 | 4.0 | 11.84 |
| 12:13:29 | -28 | 4.0 | 11.91 |
| 12:13:30 | -28 | 4.0 | 11.97 |
| 12:13:31 | -28 | 4.0 | 12.04 |
| 12:13:32 | -28 | 4.0 | 12.10 |
| 12:13:33 | -28 | 4.0 | 12.17 |
| 12:13:34 | -28 | 4.0 | 12.24 |
| 12:13:35 | -28 | 4.0 | 12.30 |
| 12:13:36 | -28 | 4.0 | 12.37 |
| 12:13:37 | -28 | 4.0 | 12.43 |
| 12:13:38 | -28 | 4.0 | 12.50 |
| 12:13:39 | -28 | 4.0 | 12.57 |
| 12:13:40 | -28 | 4.0 | 12.63 |
| 12:13:41 | -28 | 4.0 | 12.70 |
| 12:13:42 | -28 | 4.0 | 12.77 |
| 12:13:43 | -28 | 4.0 | 12.83 |
| 12:13:44 | -28 | 4.0 | 12.90 |
| 12:13:45 | -28 | 4.0 | 12.96 |
| 12:13:46 | -28 | 4.0 | 13.03 |
| 12:13:47 | -28 | 4.0 | 13.10 |
| 12:13:48 | -28 | 4.0 | 13.16 |
| 12:13:49 | -28 | 4.0 | 13.23 |
| 12:13:50 | -28 | 4.0 | 13.29 |
| 12:13:51 | -28 | 4.0 | 13.36 |
| 12:13:52 | -28 | 4.0 | 13.43 |
| 12:13:53 | -28 | 4.0 | 13.49 |
| 12:13:54 | -28 | 4.0 | 13.56 |
| 12:13:55 | -28 | 4.0 | 13.63 |
| 12:13:56 | -28 | 4.0 | 13.69 |
| 12:13:57 | -28 | 4.0 | 13.76 |
| 12:13:58 | -28 | 4.0 | 13.82 |
| 12:13:59 | -28 | 4.0 | 13.89 |
| 12:14:00 | -28 | 4.0 | 13.96 |
| 12:14:01 | -28 | 4.0 | 14.02 |
| 12:14:02 | -28 | 4.0 | 14.09 |
| 12:14:03 | -28 | 4.0 | 14.15 |
| 12:14:04 | -28 | 4.0 | 14.22 |
| 12:14:05 | -28 | 4.0 | 14.29 |
| 12:14:06 | -27 | 4.0 | 14.35 |
| 12:14:07 | -27 | 4.0 | 14.42 |
| 12:14:08 | -27 | 4.0 | 14.49 |
| 12:14:09 | -27 | 4.0 | 14.55 |
| 12:14:10 | -27 | 4.0 | 14.62 |
| 12:14:11 | -27 | 4.0 | 14.68 |
| 12:14:12 | -27 | 4.0 | 14.75 |
| 12:14:13 | -27 | 4.0 | 14.82 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:14:14 | -27 | 4.0 | 14.88 |
| 12:14:15 | -27 | 4.0 | 14.95 |
| 12:14:16 | -27 | 4.0 | 15.01 |
| 12:14:17 | -27 | 4.0 | 15.08 |
| 12:14:18 | -27 | 4.0 | 15.15 |
| 12:14:19 | -27 | 4.0 | 15.21 |
| 12:14:20 | -27 | 4.0 | 15.28 |
| 12:14:21 | -27 | 4.0 | 15.35 |
| 12:14:22 | -27 | 4.0 | 15.41 |
| 12:14:23 | -27 | 4.0 | 15.48 |
| 12:14:24 | -27 | 4.0 | 15.54 |
| 12:14:25 | -26 | 4.0 | 15.61 |
| 12:14:26 | -26 | 4.0 | 15.68 |
| 12:14:27 | -26 | 4.0 | 15.74 |
| 12:14:28 | -26 | 4.0 | 15.81 |
| 12:14:29 | -26 | 4.0 | 15.88 |
| 12:14:30 | -26 | 4.0 | 15.94 |
| 12:14:31 | -26 | 4.0 | 16.01 |
| 12:14:32 | -26 | 4.0 | 16.07 |
| 12:14:33 | -26 | 4.0 | 16.14 |
| 12:14:34 | -26 | 4.0 | 16.21 |
| 12:14:35 | -26 | 4.0 | 16.27 |
| 12:14:36 | -26 | 4.0 | 16.34 |
| 12:14:37 | -26 | 4.0 | 16.40 |
| 12:14:38 | -26 | 4.0 | 16.47 |
| 12:14:39 | -26 | 4.0 | 16.54 |
| 12:14:40 | -26 | 4.0 | 16.60 |
| 12:14:41 | -26 | 4.0 | 16.67 |
| 12:14:42 | -26 | 4.0 | 16.73 |
| 12:14:43 | -26 | 4.0 | 16.80 |
| 12:14:44 | -26 | 4.0 | 16.87 |
| 12:14:45 | -26 | 4.0 | 16.93 |
| 12:14:46 | -26 | 4.0 | 17.00 |
| 12:14:47 | -26 | 4.0 | 17.06 |
| 12:14:48 | -26 | 4.0 | 17.13 |
| 12:14:49 | -26 | 4.0 | 17.20 |
| 12:14:50 | -26 | 4.0 | 17.26 |
| 12:14:51 | -26 | 4.0 | 17.33 |
| 12:14:52 | -26 | 4.0 | 17.39 |
| 12:14:53 | -26 | 4.0 | 17.46 |
| 12:14:54 | -26 | 4.0 | 17.53 |
| 12:14:55 | -26 | 4.0 | 17.59 |
| 12:14:56 | -26 | 4.0 | 17.66 |
| 12:14:57 | -26 | 4.0 | 17.72 |
| 12:14:58 | -26 | 4.0 | 17.79 |
| 12:14:59 | -26 | 4.0 | 17.86 |
| 12:15:00 | -26 | 4.0 | 17.92 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:15:01 | -26 | 4.0 | 17.99 |
| 12:15:02 | -26 | 4.0 | 18.05 |
| 12:15:03 | -26 | 4.0 | 18.12 |
| 12:15:04 | -26 | 4.0 | 18.19 |
| 12:15:05 | -26 | 4.0 | 18.25 |
| 12:15:06 | -26 | 4.0 | 18.32 |
| 12:15:07 | -26 | 4.0 | 18.39 |
| 12:15:08 | -25 | 4.0 | 18.45 |
| 12:15:09 | -25 | 4.0 | 18.52 |
| 12:15:10 | -25 | 4.0 | 18.58 |
| 12:15:11 | -25 | 4.0 | 18.65 |
| 12:15:12 | -25 | 4.0 | 18.72 |
| 12:15:13 | -25 | 4.0 | 18.78 |
| 12:15:14 | -25 | 4.0 | 18.85 |
| 12:15:15 | -25 | 4.0 | 18.91 |
| 12:15:16 | -25 | 4.0 | 18.98 |
| 12:15:17 | -25 | 4.0 | 19.05 |
| 12:15:18 | -25 | 4.0 | 19.11 |
| 12:15:19 | -25 | 4.0 | 19.18 |
| 12:15:20 | -25 | 4.0 | 19.25 |
| 12:15:21 | -25 | 4.0 | 19.31 |
| 12:15:22 | -25 | 4.0 | 19.38 |
| 12:15:23 | -25 | 4.0 | 19.44 |
| 12:15:24 | -25 | 4.0 | 19.51 |
| 12:15:25 | -25 | 4.0 | 19.58 |
| 12:15:26 | -24 | 4.0 | 19.64 |
| 12:15:27 | -24 | 4.0 | 19.71 |
| 12:15:28 | -24 | 4.0 | 19.78 |
| 12:15:29 | -24 | 4.0 | 19.84 |
| 12:15:30 | -24 | 4.0 | 19.91 |
| 12:15:31 | -24 | 4.0 | 19.97 |
| 12:15:32 | -24 | 4.0 | 20.04 |
| 12:15:33 | -24 | 4.0 | 20.11 |
| 12:15:34 | -24 | 4.0 | 20.17 |
| 12:15:35 | -24 | 4.0 | 20.24 |
| 12:15:36 | -24 | 4.0 | 20.31 |
| 12:15:37 | -24 | 4.0 | 20.37 |
| 12:15:38 | -24 | 4.0 | 20.44 |
| 12:15:39 | -24 | 4.0 | 20.50 |
| 12:15:40 | -24 | 4.0 | 20.57 |
| 12:15:41 | -24 | 4.0 | 20.64 |
| 12:15:42 | -24 | 4.0 | 20.70 |
| 12:15:43 | -24 | 4.0 | 20.77 |
| 12:15:44 | -24 | 4.0 | 20.84 |
| 12:15:45 | -24 | 4.0 | 20.90 |
| 12:15:46 | -24 | 4.0 | 20.97 |
| 12:15:47 | -24 | 4.0 | 21.03 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:15:48 | -24 | 4.0 | 21.10 |
| 12:15:49 | -24 | 4.0 | 21.17 |
| 12:15:50 | -23 | 4.0 | 21.23 |
| 12:15:51 | -23 | 4.0 | 21.30 |
| 12:15:52 | -23 | 4.0 | 21.37 |
| 12:15:53 | -23 | 4.0 | 21.43 |
| 12:15:54 | -23 | 4.0 | 21.50 |
| 12:15:55 | -23 | 4.0 | 21.56 |
| 12:15:56 | -23 | 4.0 | 21.63 |
| 12:15:57 | -23 | 4.0 | 21.70 |
| 12:15:58 | -23 | 4.0 | 21.76 |
| 12:15:59 | -23 | 4.0 | 21.83 |
| 12:16:00 | -23 | 4.0 | 21.90 |
| 12:16:01 | -23 | 4.0 | 21.96 |
| 12:16:02 | -23 | 4.0 | 22.03 |
| 12:16:03 | -23 | 4.0 | 22.09 |
| 12:16:04 | -23 | 4.0 | 22.16 |
| 12:16:05 | -23 | 4.0 | 22.23 |
| 12:16:06 | -23 | 4.0 | 22.31 |
| 12:16:07 | -23 | 4.0 | 22.31 |
| 12:16:08 | -23 | 4.0 | 22.37 |
| 12:16:09 | -23 | 4.0 | 22.44 |
| 12:16:10 | -23 | 4.0 | 22.51 |
| 12:16:11 | -23 | 4.0 | 22.57 |
| 12:16:12 | -22 | 4.0 | 22.64 |
| 12:16:13 | -22 | 4.0 | 22.71 |
| 12:16:14 | -22 | 4.0 | 22.77 |
| 12:16:15 | -22 | 4.0 | 22.84 |
| 12:16:16 | -22 | 4.0 | 22.91 |
| 12:16:17 | -22 | 4.0 | 22.97 |
| 12:16:18 | -22 | 4.0 | 23.04 |
| 12:16:19 | -22 | 4.0 | 23.10 |
| 12:16:20 | -22 | 4.0 | 23.17 |
| 12:16:21 | -22 | 4.0 | 23.24 |
| 12:16:22 | -22 | 4.0 | 23.30 |
| 12:16:23 | -22 | 4.0 | 23.37 |
| 12:16:24 | -22 | 4.0 | 23.44 |
| 12:16:25 | -22 | 4.0 | 23.50 |
| 12:16:26 | -22 | 4.0 | 23.57 |
| 12:16:27 | -22 | 4.0 | 23.63 |
| 12:16:28 | -22 | 4.0 | 23.70 |
| 12:16:29 | -22 | 4.0 | 23.77 |
| 12:16:30 | -22 | 4.0 | 23.83 |
| 12:16:31 | -22 | 4.0 | 23.90 |
| 12:16:32 | -21 | 4.0 | 23.97 |
| 12:16:33 | -21 | 4.0 | 24.03 |
| 12:16:34 | -21 | 4.0 | 24.10 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:16:35 | -21 | 4.0 | 24.17 |
| 12:16:36 | -21 | 4.0 | 24.23 |
| 12:16:37 | -21 | 4.0 | 24.30 |
| 12:16:38 | -21 | 4.0 | 24.36 |
| 12:16:39 | -21 | 4.0 | 24.43 |
| 12:16:40 | -21 | 4.0 | 24.50 |
| 12:16:41 | -21 | 4.0 | 24.56 |
| 12:16:42 | -21 | 4.0 | 24.63 |
| 12:16:43 | -21 | 4.0 | 24.70 |
| 12:16:44 | -21 | 4.0 | 24.76 |
| 12:16:45 | -21 | 4.0 | 24.83 |
| 12:16:46 | -21 | 4.0 | 24.90 |
| 12:16:47 | -21 | 4.0 | 24.96 |
| 12:16:48 | -21 | 4.0 | 25.03 |
| 12:16:49 | -21 | 4.0 | 25.09 |
| 12:16:50 | -21 | 4.0 | 25.16 |
| 12:16:51 | -21 | 4.0 | 25.23 |
| 12:16:52 | -21 | 4.0 | 25.29 |
| 12:16:53 | -21 | 4.0 | 25.36 |
| 12:16:54 | -21 | 4.0 | 25.43 |
| 12:16:55 | -21 | 4.0 | 25.49 |
| 12:16:56 | -21 | 4.0 | 25.56 |
| 12:16:57 | -21 | 4.0 | 25.63 |
| 12:16:58 | -21 | 4.0 | 25.69 |
| 12:16:59 | -21 | 4.0 | 25.76 |
| 12:17:00 | -21 | 4.0 | 25.82 |
| 12:17:01 | -21 | 4.0 | 25.89 |
| 12:17:02 | -21 | 4.0 | 25.96 |
| 12:17:03 | -21 | 4.0 | 26.02 |
| 12:17:04 | -21 | 4.0 | 26.09 |
| 12:17:05 | -21 | 4.0 | 26.16 |
| 12:17:06 | -21 | 4.0 | 26.22 |
| 12:17:07 | -21 | 4.0 | 26.29 |
| 12:17:08 | -21 | 4.0 | 26.36 |
| 12:17:09 | -21 | 4.0 | 26.42 |
| 12:17:10 | -21 | 4.0 | 26.49 |
| 12:17:11 | -21 | 4.0 | 26.55 |
| 12:17:12 | -21 | 4.0 | 26.62 |
| 12:17:13 | -21 | 4.0 | 26.69 |
| 12:17:14 | -21 | 4.0 | 26.75 |
| 12:17:15 | -21 | 4.0 | 26.82 |
| 12:17:16 | -20 | 4.0 | 26.89 |
| 12:17:17 | -20 | 4.0 | 26.95 |
| 12:17:18 | -20 | 4.0 | 27.02 |
| 12:17:19 | -20 | 4.0 | 27.08 |
| 12:17:20 | -20 | 4.0 | 27.15 |
| 12:17:21 | -20 | 4.0 | 27.22 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:17:22 | -20 | 4.0 | 27.28 |
| 12:17:23 | -20 | 4.0 | 27.35 |
| 12:17:24 | -20 | 4.0 | 27.42 |
| 12:17:25 | -20 | 4.0 | 27.48 |
| 12:17:26 | -20 | 4.0 | 27.55 |
| 12:17:27 | -20 | 4.0 | 27.62 |
| 12:17:28 | -20 | 4.0 | 27.68 |
| 12:17:29 | -20 | 4.0 | 27.75 |
| 12:17:30 | -20 | 4.0 | 27.81 |
| 12:17:31 | -20 | 4.0 | 27.88 |
| 12:17:32 | -20 | 4.0 | 27.95 |
| 12:17:33 | -20 | 4.0 | 28.01 |
| 12:17:34 | -20 | 4.0 | 28.08 |
| 12:17:35 | -20 | 4.0 | 28.15 |
| 12:17:36 | -20 | 4.0 | 28.21 |
| 12:17:37 | -20 | 4.0 | 28.28 |
| 12:17:38 | -20 | 4.0 | 28.35 |
| 12:17:39 | -20 | 4.0 | 28.41 |
| 12:17:40 | -20 | 4.0 | 28.48 |
| 12:17:41 | -19 | 4.0 | 28.54 |
| 12:17:42 | -19 | 4.0 | 28.61 |
| 12:17:43 | -19 | 4.0 | 28.68 |
| 12:17:44 | -19 | 4.0 | 28.74 |
| 12:17:45 | -19 | 4.0 | 28.81 |
| 12:17:46 | -19 | 4.0 | 28.88 |
| 12:17:47 | -19 | 4.0 | 28.94 |
| 12:17:48 | -19 | 4.0 | 29.01 |
| 12:17:49 | -19 | 4.0 | 29.07 |
| 12:17:50 | -19 | 4.0 | 29.14 |
| 12:17:51 | -19 | 4.0 | 29.21 |
| 12:17:52 | -19 | 4.0 | 29.27 |
| 12:17:53 | -19 | 4.0 | 29.34 |
| 12:17:54 | -19 | 4.0 | 29.41 |
| 12:17:55 | -19 | 4.0 | 29.47 |
| 12:17:56 | -19 | 4.0 | 29.54 |
| 12:17:57 | -19 | 4.0 | 29.61 |
| 12:17:58 | -19 | 4.0 | 29.67 |
| 12:17:59 | -19 | 4.0 | 29.74 |
| 12:18:00 | -19 | 4.0 | 29.80 |
| 12:18:01 | -19 | 4.0 | 29.87 |
| 12:18:02 | -19 | 4.0 | 29.94 |
| 12:18:03 | -19 | 4.0 | 30.00 |
| 12:18:04 | -19 | 4.0 | 30.07 |
| 12:18:05 | -19 | 4.0 | 30.14 |
| 12:18:06 | -19 | 4.0 | 30.20 |
| 12:18:07 | -19 | 4.0 | 30.27 |
| 12:18:08 | -19 | 4.0 | 30.34 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:18:09 | -19 | 4.0 | 30.40 |
| 12:18:10 | -19 | 4.0 | 30.47 |
| 12:18:11 | -19 | 4.0 | 30.54 |
| 12:18:12 | -19 | 4.0 | 30.60 |
| 12:18:13 | -19 | 4.0 | 30.67 |
| 12:18:14 | -19 | 4.0 | 30.74 |
| 12:18:15 | -19 | 4.0 | 30.80 |
| 12:18:16 | -18 | 4.0 | 30.87 |
| 12:18:17 | -18 | 4.0 | 30.93 |
| 12:18:18 | -18 | 4.0 | 31.00 |
| 12:18:19 | -18 | 4.0 | 31.07 |
| 12:18:20 | -18 | 4.0 | 31.13 |
| 12:18:21 | -18 | 4.0 | 31.20 |
| 12:18:22 | -18 | 4.0 | 31.27 |
| 12:18:23 | -18 | 4.0 | 31.33 |
| 12:18:24 | -18 | 4.0 | 31.40 |
| 12:18:25 | -18 | 4.0 | 31.47 |
| 12:18:26 | -18 | 4.0 | 31.53 |
| 12:18:27 | -18 | 4.0 | 31.60 |
| 12:18:28 | -18 | 4.0 | 31.67 |
| 12:18:29 | -18 | 4.0 | 31.73 |
| 12:18:30 | -18 | 4.0 | 31.80 |
| 12:18:31 | -18 | 4.0 | 31.86 |
| 12:18:32 | -18 | 4.0 | 31.93 |
| 12:18:33 | -18 | 4.0 | 32.00 |
| 12:18:34 | -18 | 4.0 | 32.06 |
| 12:18:35 | -18 | 4.0 | 32.13 |
| 12:18:36 | -18 | 4.0 | 32.20 |
| 12:18:37 | -17 | 4.0 | 32.26 |
| 12:18:38 | -15 | 3.9 | 32.33 |
| 12:18:39 | -13 | 3.9 | 32.39 |
| 12:18:40 | -12 | 4.0 | 32.46 |
| 12:18:41 | -11 | 4.0 | 32.53 |
| 12:18:42 | -10 | 3.9 | 32.59 |
| 12:18:43 | -8 | 3.9 | 32.66 |
| 12:18:44 | -6 | 3.9 | 32.72 |
| 12:18:45 | -4 | 3.9 | 32.79 |
| 12:18:46 | -2 | 3.9 | 32.86 |
| 12:18:47 | -0 | 3.9 | 32.92 |
| 12:18:48 | 2 | 3.9 | 32.99 |
| 12:18:49 | 4 | 3.9 | 33.05 |
| 12:18:50 | 6 | 3.9 | 33.12 |
| 12:18:51 | 9 | 3.9 | 33.18 |
| 12:18:52 | 11 | 3.9 | 33.25 |
| 12:18:53 | 13 | 3.9 | 33.32 |
| 12:18:54 | 15 | 3.9 | 33.38 |
| 12:18:55 | 17 | 3.9 | 33.45 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:18:56 | 19 | 3.9 | 33.51 |
| 12:18:57 | 21 | 3.9 | 33.58 |
| 12:18:58 | 23 | 3.9 | 33.64 |
| 12:18:59 | 25 | 3.9 | 33.71 |
| 12:19:00 | 27 | 3.9 | 33.78 |
| 12:19:01 | 28 | 3.9 | 33.84 |
| 12:19:02 | 29 | 3.9 | 33.91 |
| 12:19:03 | 27 | 3.5 | 33.96 |
| 12:19:04 | 24 | 2.5 | 34.01 |
| 12:19:05 | 22 | 2.1 | 34.04 |
| 12:19:06 | 21 | 1.8 | 34.07 |
| 12:19:07 | 20 | 1.8 | 34.10 |
| 12:19:08 | 17 | 1.7 | 34.13 |
| 12:19:09 | 14 | 1.6 | 34.16 |
| 12:19:10 | 11 | 1.3 | 34.18 |
| 12:19:11 | 9 | 1.2 | 34.20 |
| 12:19:12 | 6 | 1.1 | 34.22 |
| 12:19:13 | 3 | 1.0 | 34.23 |
| 12:19:14 | 1 | 1.0 | 34.25 |
| 12:19:15 | -1 | 1.0 | 34.27 |
| 12:19:16 | -3 | 1.1 | 34.28 |
| 12:19:17 | -4 | 1.1 | 34.30 |
| 12:19:18 | -6 | 1.2 | 34.32 |
| 12:19:19 | -7 | 1.2 | 34.34 |
| 12:19:20 | -8 | 1.3 | 34.36 |
| 12:19:21 | -9 | 1.3 | 34.39 |
| 12:19:22 | -10 | 1.3 | 34.41 |
| 12:19:23 | -10 | 1.3 | 34.43 |
| 12:19:24 | -11 | 1.3 | 34.45 |
| 12:19:25 | -11 | 1.3 | 34.47 |
| 12:19:26 | -11 | 1.3 | 34.50 |
| 12:19:27 | -11 | 1.3 | 34.52 |
| 12:19:28 | -12 | 1.3 | 34.54 |
| 12:19:29 | -12 | 1.3 | 34.56 |
| 12:19:30 | -12 | 1.3 | 34.58 |
| 12:19:31 | -12 | 1.3 | 34.61 |
| 12:19:32 | -12 | 1.4 | 34.63 |
| 12:19:33 | -12 | 1.4 | 34.65 |
| 12:19:34 | -13 | 1.4 | 34.68 |
| 12:19:35 | -13 | 1.4 | 34.70 |
| 12:19:36 | -13 | 1.4 | 34.72 |
| 12:19:37 | -13 | 1.5 | 34.75 |
| 12:19:38 | -14 | 1.5 | 34.77 |
| 12:19:39 | -14 | 1.5 | 34.80 |
| 12:19:40 | -14 | 1.5 | 34.82 |
| 12:19:41 | -14 | 1.6 | 34.85 |
| 12:19:42 | -14 | 1.6 | 34.88 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:19:43 | -15 | 1.6 | 34.90 |
| 12:19:44 | -15 | 1.6 | 34.93 |
| 12:19:45 | -15 | 1.7 | 34.96 |
| 12:19:46 | -15 | 1.7 | 34.99 |
| 12:19:47 | -16 | 1.7 | 35.01 |
| 12:19:48 | -16 | 1.7 | 35.04 |
| 12:19:49 | -16 | 1.7 | 35.07 |
| 12:19:50 | -16 | 1.7 | 35.10 |
| 12:19:51 | -16 | 1.7 | 35.13 |
| 12:19:52 | -16 | 1.7 | 35.16 |
| 12:19:53 | -16 | 1.7 | 35.19 |
| 12:19:54 | -16 | 1.7 | 35.21 |
| 12:19:55 | -17 | 1.7 | 35.24 |
| 12:19:56 | -17 | 1.7 | 35.27 |
| 12:19:57 | -17 | 1.7 | 35.30 |
| 12:19:58 | -17 | 1.7 | 35.33 |
| 12:19:59 | -17 | 1.8 | 35.36 |
| 12:20:00 | -17 | 1.8 | 35.39 |
| 12:20:01 | -16 | 1.8 | 35.42 |
| 12:20:02 | -15 | 1.9 | 35.45 |
| 12:20:03 | -14 | 2.0 | 35.48 |
| 12:20:04 | -12 | 2.2 | 35.52 |
| 12:20:05 | -11 | 2.3 | 35.56 |
| 12:20:06 | -10 | 2.4 | 35.60 |
| 12:20:07 | -9 | 2.5 | 35.64 |
| 12:20:08 | -7 | 2.5 | 35.68 |
| 12:20:09 | -6 | 2.5 | 35.73 |
| 12:20:10 | -5 | 2.6 | 35.77 |
| 12:20:11 | -3 | 2.6 | 35.81 |
| 12:20:12 | -1 | 2.7 | 35.86 |
| 12:20:13 | -0 | 2.7 | 35.90 |
| 12:20:14 | 1 | 2.7 | 35.95 |
| 12:20:15 | 3 | 2.7 | 35.99 |
| 12:20:16 | 4 | 2.7 | 36.04 |
| 12:20:17 | 5 | 2.7 | 36.08 |
| 12:20:18 | 6 | 2.7 | 36.13 |
| 12:20:19 | 7 | 2.8 | 36.18 |
| 12:20:20 | 9 | 2.8 | 36.22 |
| 12:20:21 | 10 | 2.8 | 36.27 |
| 12:20:22 | 10 | 2.8 | 36.31 |
| 12:20:23 | 11 | 2.8 | 36.36 |
| 12:20:24 | 12 | 2.8 | 36.41 |
| 12:20:25 | 14 | 2.8 | 36.45 |
| 12:20:26 | 15 | 2.8 | 36.50 |
| 12:20:27 | 16 | 2.8 | 36.54 |
| 12:20:28 | 17 | 2.8 | 36.59 |
| 12:20:29 | 18 | 2.8 | 36.64 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:20:30 | 19 | 2.8 | 36.68 |
| 12:20:31 | 20 | 2.8 | 36.73 |
| 12:20:32 | 22 | 2.8 | 36.77 |
| 12:20:33 | 23 | 2.8 | 36.82 |
| 12:20:34 | 24 | 2.8 | 36.87 |
| 12:20:35 | 25 | 2.8 | 36.91 |
| 12:20:36 | 26 | 2.8 | 36.96 |
| 12:20:37 | 27 | 2.8 | 37.00 |
| 12:20:38 | 28 | 2.8 | 37.05 |
| 12:20:39 | 29 | 2.8 | 37.10 |
| 12:20:40 | 30 | 2.8 | 37.14 |
| 12:20:41 | 31 | 2.8 | 37.19 |
| 12:20:42 | 32 | 2.8 | 37.23 |
| 12:20:43 | 33 | 2.8 | 37.28 |
| 12:20:44 | 34 | 2.8 | 37.33 |
| 12:20:45 | 35 | 2.8 | 37.37 |
| 12:20:46 | 37 | 2.8 | 37.42 |
| 12:20:47 | 38 | 2.8 | 37.46 |
| 12:20:48 | 39 | 2.8 | 37.51 |
| 12:20:49 | 40 | 2.8 | 37.56 |
| 12:20:50 | 41 | 2.8 | 37.60 |
| 12:20:51 | 42 | 2.8 | 37.65 |
| 12:20:52 | 43 | 2.8 | 37.69 |
| 12:20:53 | 44 | 2.8 | 37.74 |
| 12:20:54 | 45 | 2.8 | 37.78 |
| 12:20:55 | 46 | 2.8 | 37.83 |
| 12:20:56 | 47 | 2.8 | 37.88 |
| 12:20:57 | 48 | 2.8 | 37.92 |
| 12:20:58 | 49 | 2.8 | 37.97 |
| 12:20:59 | 50 | 2.8 | 38.01 |
| 12:21:00 | 51 | 2.8 | 38.06 |
| 12:21:01 | 52 | 2.8 | 38.11 |
| 12:21:02 | 53 | 2.8 | 38.15 |
| 12:21:03 | 54 | 2.8 | 38.20 |
| 12:21:04 | 55 | 2.8 | 38.24 |
| 12:21:05 | 56 | 2.8 | 38.29 |
| 12:21:06 | 57 | 2.8 | 38.34 |
| 12:21:07 | 58 | 2.8 | 38.38 |
| 12:21:08 | 59 | 2.8 | 38.43 |
| 12:21:09 | 60 | 2.8 | 38.47 |
| 12:21:10 | 61 | 2.8 | 38.52 |
| 12:21:11 | 62 | 2.7 | 38.56 |
| 12:21:12 | 63 | 2.7 | 38.61 |
| 12:21:13 | 64 | 2.8 | 38.66 |
| 12:21:14 | 65 | 2.7 | 38.70 |
| 12:21:15 | 66 | 2.7 | 38.75 |
| 12:21:16 | 67 | 2.7 | 38.79 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:21:17 | 68 | 2.7 | 38.84 |
| 12:21:18 | 69 | 2.8 | 38.89 |
| 12:21:19 | 69 | 2.7 | 38.93 |
| 12:21:20 | 70 | 2.7 | 38.98 |
| 12:21:21 | 72 | 2.7 | 39.02 |
| 12:21:22 | 73 | 2.7 | 39.07 |
| 12:21:23 | 73 | 2.7 | 39.11 |
| 12:21:24 | 74 | 2.7 | 39.16 |
| 12:21:25 | 75 | 2.7 | 39.21 |
| 12:21:26 | 76 | 2.7 | 39.25 |
| 12:21:27 | 77 | 2.7 | 39.30 |
| 12:21:28 | 78 | 2.7 | 39.34 |
| 12:21:29 | 79 | 2.7 | 39.39 |
| 12:21:30 | 80 | 2.7 | 39.43 |
| 12:21:31 | 81 | 2.7 | 39.48 |
| 12:21:32 | 82 | 2.7 | 39.53 |
| 12:21:33 | 83 | 2.7 | 39.57 |
| 12:21:34 | 84 | 2.7 | 39.62 |
| 12:21:35 | 85 | 2.7 | 39.66 |
| 12:21:36 | 86 | 2.7 | 39.71 |
| 12:21:37 | 87 | 2.7 | 39.76 |
| 12:21:38 | 88 | 2.7 | 39.80 |
| 12:21:39 | 89 | 2.7 | 39.85 |
| 12:21:40 | 89 | 2.7 | 39.89 |
| 12:21:41 | 91 | 2.7 | 39.94 |
| 12:21:42 | 92 | 2.7 | 39.98 |
| 12:21:43 | 93 | 2.7 | 40.03 |
| 12:21:44 | 93 | 2.7 | 40.08 |
| 12:21:45 | 94 | 2.7 | 40.12 |
| 12:21:46 | 95 | 2.7 | 40.17 |
| 12:21:47 | 96 | 2.7 | 40.21 |
| 12:21:48 | 97 | 2.7 | 40.26 |
| 12:21:49 | 98 | 2.7 | 40.31 |
| 12:21:50 | 99 | 2.7 | 40.35 |
| 12:21:51 | 100 | 2.7 | 40.40 |
| 12:21:52 | 101 | 2.7 | 40.44 |
| 12:21:53 | 102 | 2.7 | 40.49 |
| 12:21:54 | 103 | 2.7 | 40.53 |
| 12:21:55 | 104 | 2.7 | 40.58 |
| 12:21:56 | 105 | 2.7 | 40.63 |
| 12:21:57 | 105 | 2.7 | 40.67 |
| 12:21:58 | 106 | 2.7 | 40.72 |
| 12:21:59 | 107 | 2.7 | 40.76 |
| 12:22:00 | 108 | 2.7 | 40.81 |
| 12:22:01 | 110 | 2.7 | 40.85 |
| 12:22:02 | 111 | 2.7 | 40.90 |
| 12:22:03 | 111 | 2.7 | 40.95 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:22:04 | 112 | 2.7 | 40.99 |
| 12:22:05 | 113 | 2.7 | 41.04 |
| 12:22:06 | 114 | 2.7 | 41.08 |
| 12:22:07 | 115 | 2.7 | 41.13 |
| 12:22:08 | 116 | 2.7 | 41.17 |
| 12:22:09 | 117 | 2.7 | 41.22 |
| 12:22:10 | 118 | 2.7 | 41.27 |
| 12:22:11 | 119 | 2.7 | 41.31 |
| 12:22:12 | 119 | 2.7 | 41.36 |
| 12:22:13 | 117 | 2.6 | 41.40 |
| 12:22:14 | 111 | 1.7 | 41.43 |
| 12:22:15 | 110 | 1.2 | 41.45 |
| 12:22:16 | 109 | 1.2 | 41.47 |
| 12:22:17 | 104 | 1.1 | 41.49 |
| 12:22:18 | 102 | 0.9 | 41.50 |
| 12:22:19 | 100 | 0.9 | 41.52 |
| 12:22:20 | 95 | 0.9 | 41.53 |
| 12:22:21 | 92 | 0.8 | 41.55 |
| 12:22:22 | 89 | 0.8 | 41.56 |
| 12:22:23 | 85 | 0.8 | 41.57 |
| 12:22:24 | 82 | 0.7 | 41.59 |
| 12:22:25 | 79 | 0.6 | 41.60 |
| 12:22:26 | 77 | 0.6 | 41.61 |
| 12:22:27 | 75 | 0.5 | 41.62 |
| 12:22:28 | 72 | 0.5 | 41.62 |
| 12:22:29 | 70 | 0.5 | 41.63 |
| 12:22:30 | 68 | 0.4 | 41.64 |
| 12:22:31 | 66 | 0.4 | 41.65 |
| 12:22:32 | 65 | 0.4 | 41.65 |
| 12:22:33 | 63 | 0.4 | 41.66 |
| 12:22:34 | 61 | 0.4 | 41.67 |
| 12:22:35 | 60 | 0.4 | 41.67 |
| 12:22:36 | 58 | 0.4 | 41.68 |
| 12:22:37 | 56 | 0.4 | 41.69 |
| 12:22:38 | 55 | 0.4 | 41.69 |
| 12:22:39 | 53 | 0.4 | 41.70 |
| 12:22:40 | 51 | 0.4 | 41.71 |
| 12:22:41 | 49 | 0.4 | 41.71 |
| 12:22:42 | 48 | 0.4 | 41.72 |
| 12:22:43 | 46 | 0.4 | 41.73 |
| 12:22:44 | 44 | 0.4 | 41.73 |
| 12:22:45 | 43 | 0.4 | 41.74 |
| 12:22:46 | 41 | 0.4 | 41.75 |
| 12:22:47 | 39 | 0.4 | 41.75 |
| 12:22:48 | 38 | 0.4 | 41.76 |
| 12:22:49 | 36 | 0.4 | 41.77 |
| 12:22:50 | 35 | 0.4 | 41.78 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:22:51 | 33 | 0.4 | 41.78 |
| 12:22:52 | 31 | 0.4 | 41.79 |
| 12:22:53 | 30 | 0.4 | 41.80 |
| 12:22:54 | 29 | 0.5 | 41.80 |
| 12:22:55 | 27 | 0.5 | 41.81 |
| 12:22:56 | 26 | 0.5 | 41.82 |
| 12:22:57 | 25 | 0.5 | 41.83 |
| 12:22:58 | 24 | 0.5 | 41.84 |
| 12:22:59 | 23 | 0.6 | 41.85 |
| 12:23:00 | 21 | 0.6 | 41.86 |
| 12:23:01 | 20 | 0.6 | 41.87 |
| 12:23:02 | 19 | 0.6 | 41.88 |
| 12:23:03 | 18 | 0.6 | 41.89 |
| 12:23:04 | 17 | 0.6 | 41.90 |
| 12:23:05 | 16 | 0.6 | 41.91 |
| 12:23:06 | 15 | 0.6 | 41.92 |
| 12:23:07 | 14 | 0.7 | 41.93 |
| 12:23:08 | 13 | 0.7 | 41.94 |
| 12:23:09 | 12 | 0.7 | 41.95 |
| 12:23:10 | 11 | 0.7 | 41.96 |
| 12:23:11 | 10 | 0.7 | 41.98 |
| 12:23:12 | 9 | 0.7 | 41.99 |
| 12:23:13 | 8 | 0.7 | 42.00 |
| 12:23:14 | 7 | 0.7 | 42.01 |
| 12:23:15 | 6 | 0.7 | 42.02 |
| 12:23:16 | 6 | 0.7 | 42.03 |
| 12:23:17 | 5 | 0.7 | 42.04 |
| 12:23:18 | 4 | 0.7 | 42.06 |
| 12:23:19 | 3 | 0.7 | 42.07 |
| 12:23:20 | 2 | 0.7 | 42.08 |
| 12:23:21 | 1 | 0.7 | 42.09 |
| 12:23:22 | 0 | 0.7 | 42.10 |
| 12:23:23 | -1 | 0.7 | 42.11 |
| 12:23:24 | -2 | 0.7 | 42.13 |
| 12:23:25 | -3 | 0.6 | 42.14 |
| 12:23:26 | -4 | 0.6 | 42.15 |
| 12:23:27 | -5 | 0.6 | 42.16 |
| 12:23:28 | -6 | 0.6 | 42.17 |
| 12:23:29 | -7 | 0.6 | 42.18 |
| 12:23:30 | -8 | 0.6 | 42.19 |
| 12:23:31 | -9 | 0.6 | 42.19 |
| 12:23:32 | -10 | 0.6 | 42.20 |
| 12:23:33 | -10 | 0.6 | 42.21 |
| 12:23:34 | -11 | 0.6 | 42.22 |
| 12:23:35 | -12 | 0.5 | 42.23 |
| 12:23:36 | -13 | 0.5 | 42.24 |
| 12:23:37 | -13 | 0.5 | 42.25 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:23:38 | -14 | 0.5 | 42.26 |
| 12:23:39 | -14 | 0.5 | 42.27 |
| 12:23:40 | -15 | 0.5 | 42.28 |
| 12:23:41 | -15 | 0.5 | 42.28 |
| 12:23:42 | -15 | 0.5 | 42.29 |
| 12:23:43 | -15 | 0.5 | 42.30 |
| 12:23:44 | -15 | 0.5 | 42.31 |
| 12:23:45 | -15 | 0.5 | 42.32 |
| 12:23:46 | -15 | 0.5 | 42.33 |
| 12:23:47 | -15 | 0.5 | 42.34 |
| 12:23:48 | -15 | 0.5 | 42.35 |
| 12:23:49 | -15 | 0.5 | 42.36 |
| 12:23:50 | -15 | 0.5 | 42.36 |
| 12:23:51 | -15 | 0.4 | 42.37 |
| 12:23:52 | -15 | 0.4 | 42.38 |
| 12:23:53 | -14 | 0.4 | 42.38 |
| 12:23:54 | -14 | 0.4 | 42.39 |
| 12:23:55 | -14 | 0.4 | 42.40 |
| 12:23:56 | -14 | 0.4 | 42.40 |
| 12:23:57 | -14 | 0.4 | 42.41 |
| 12:23:58 | -14 | 0.4 | 42.42 |
| 12:23:59 | -14 | 0.5 | 42.43 |
| 12:24:00 | -14 | 0.5 | 42.43 |
| 12:24:01 | -14 | 0.5 | 42.44 |
| 12:24:02 | -14 | 0.5 | 42.45 |
| 12:24:03 | -14 | 0.5 | 42.46 |
| 12:24:04 | -14 | 0.5 | 42.47 |
| 12:24:05 | -15 | 0.6 | 42.48 |
| 12:24:06 | -15 | 0.6 | 42.49 |
| 12:24:07 | -15 | 0.6 | 42.50 |
| 12:24:08 | -15 | 0.6 | 42.51 |
| 12:24:09 | -15 | 0.6 | 42.52 |
| 12:24:10 | -15 | 0.6 | 42.53 |
| 12:24:11 | -15 | 0.6 | 42.54 |
| 12:24:12 | -15 | 0.6 | 42.54 |
| 12:24:13 | -15 | 0.6 | 42.55 |
| 12:24:14 | -15 | 0.6 | 42.56 |
| 12:24:15 | -15 | 0.6 | 42.57 |
| 12:24:16 | -15 | 0.6 | 42.58 |
| 12:24:17 | -15 | 0.6 | 42.59 |
| 12:24:18 | -14 | 0.6 | 42.60 |
| 12:24:19 | -14 | 0.6 | 42.61 |
| 12:24:20 | -14 | 0.6 | 42.62 |
| 12:24:21 | -14 | 0.6 | 42.63 |
| 12:24:22 | -14 | 0.6 | 42.64 |
| 12:24:23 | -14 | 0.6 | 42.65 |
| 12:24:24 | -14 | 0.6 | 42.66 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:24:25 | -14 | 0.6 | 42.67 |
| 12:24:26 | -14 | 0.6 | 42.68 |
| 12:24:27 | -13 | 0.6 | 42.69 |
| 12:24:28 | -13 | 0.6 | 42.70 |
| 12:24:29 | -13 | 0.5 | 42.71 |
| 12:24:30 | -13 | 0.5 | 42.71 |
| 12:24:31 | -13 | 0.5 | 42.72 |
| 12:24:32 | -13 | 0.5 | 42.73 |
| 12:24:33 | -12 | 0.5 | 42.74 |
| 12:24:34 | -12 | 0.5 | 42.75 |
| 12:24:35 | -12 | 0.5 | 42.76 |
| 12:24:36 | -12 | 0.5 | 42.77 |
| 12:24:37 | -12 | 0.6 | 42.78 |
| 12:24:38 | -12 | 0.6 | 42.79 |
| 12:24:39 | -12 | 0.6 | 42.80 |
| 12:24:40 | -12 | 0.6 | 42.81 |
| 12:24:41 | -12 | 0.6 | 42.82 |
| 12:24:42 | -12 | 0.6 | 42.83 |
| 12:24:43 | -11 | 0.6 | 42.83 |
| 12:24:44 | -11 | 0.6 | 42.84 |
| 12:24:45 | -11 | 0.6 | 42.85 |
| 12:24:46 | -11 | 0.6 | 42.86 |
| 12:24:47 | -11 | 0.6 | 42.87 |
| 12:24:48 | -11 | 0.6 | 42.88 |
| 12:24:49 | -11 | 0.6 | 42.89 |
| 12:24:50 | -11 | 0.6 | 42.90 |
| 12:24:51 | -10 | 0.6 | 42.91 |
| 12:24:52 | -10 | 0.6 | 42.92 |
| 12:24:53 | -10 | 0.6 | 42.93 |
| 12:24:54 | -10 | 0.6 | 42.94 |
| 12:24:55 | -10 | 0.6 | 42.95 |
| 12:24:56 | -10 | 0.6 | 42.96 |
| 12:24:57 | -10 | 0.6 | 42.97 |
| 12:24:58 | -10 | 0.6 | 42.97 |
| 12:24:59 | -10 | 0.6 | 42.99 |
| 12:25:00 | -10 | 0.6 | 42.99 |
| 12:25:01 | -10 | 0.6 | 43.00 |
| 12:25:02 | -10 | 0.6 | 43.01 |
| 12:25:03 | -10 | 0.6 | 43.02 |
| 12:25:04 | -10 | 0.6 | 43.03 |
| 12:25:05 | -10 | 0.6 | 43.04 |
| 12:25:06 | -10 | 0.6 | 43.05 |
| 12:25:07 | -9 | 0.6 | 43.06 |
| 12:25:08 | -9 | 0.6 | 43.07 |
| 12:25:09 | -9 | 0.6 | 43.08 |
| 12:25:10 | -9 | 0.6 | 43.09 |
| 12:25:11 | -9 | 0.6 | 43.10 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:25:12 | -9 | 0.6 | 43.11 |
| 12:25:13 | -9 | 0.6 | 43.12 |
| 12:25:14 | -9 | 0.6 | 43.13 |
| 12:25:15 | -9 | 0.6 | 43.13 |
| 12:25:16 | -9 | 0.6 | 43.14 |
| 12:25:17 | -9 | 0.6 | 43.15 |
| 12:25:18 | -9 | 0.6 | 43.16 |
| 12:25:19 | -9 | 0.6 | 43.17 |
| 12:25:20 | -9 | 0.6 | 43.18 |
| 12:25:21 | -9 | 0.6 | 43.19 |
| 12:25:22 | -9 | 0.6 | 43.20 |
| 12:25:23 | -9 | 0.6 | 43.21 |
| 12:25:24 | -9 | 0.6 | 43.22 |
| 12:25:25 | -9 | 0.6 | 43.23 |
| 12:25:26 | -9 | 0.6 | 43.24 |
| 12:25:27 | -9 | 0.6 | 43.25 |
| 12:25:28 | -9 | 0.6 | 43.26 |
| 12:25:29 | -9 | 0.6 | 43.27 |
| 12:25:30 | -9 | 0.6 | 43.28 |
| 12:25:31 | -9 | 0.6 | 43.28 |
| 12:25:32 | -9 | 0.6 | 43.29 |
| 12:25:33 | -9 | 0.6 | 43.30 |
| 12:25:34 | -9 | 0.6 | 43.31 |
| 12:25:35 | -9 | 0.6 | 43.32 |
| 12:25:36 | -9 | 0.6 | 43.33 |
| 12:25:37 | -9 | 0.6 | 43.34 |
| 12:25:38 | -9 | 0.6 | 43.35 |
| 12:25:39 | -9 | 0.6 | 43.36 |
| 12:25:40 | -9 | 0.6 | 43.37 |
| 12:25:41 | -9 | 0.6 | 43.38 |
| 12:25:42 | -9 | 0.6 | 43.39 |
| 12:25:43 | -9 | 0.6 | 43.40 |
| 12:25:44 | -9 | 0.6 | 43.41 |
| 12:25:45 | -9 | 0.6 | 43.42 |
| 12:25:46 | -9 | 0.6 | 43.42 |
| 12:25:47 | -9 | 0.6 | 43.43 |
| 12:25:48 | -9 | 0.6 | 43.44 |
| 12:25:49 | -9 | 0.6 | 43.45 |
| 12:25:50 | -9 | 0.6 | 43.46 |
| 12:25:51 | -9 | 0.6 | 43.47 |
| 12:25:52 | -9 | 0.6 | 43.48 |
| 12:25:53 | -9 | 0.6 | 43.49 |
| 12:25:54 | -9 | 0.6 | 43.50 |
| 12:25:55 | -9 | 0.6 | 43.51 |
| 12:25:56 | -9 | 0.6 | 43.52 |
| 12:25:57 | -9 | 0.6 | 43.53 |
| 12:25:58 | -9 | 0.6 | 43.54 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:25:59 | -9 | 0.6 | 43.55 |
| 12:26:00 | -9 | 0.6 | 43.56 |
| 12:26:01 | -9 | 0.6 | 43.57 |
| 12:26:02 | -9 | 0.6 | 43.57 |
| 12:26:03 | -9 | 0.6 | 43.58 |
| 12:26:04 | -9 | 0.6 | 43.59 |
| 12:26:05 | -9 | 0.6 | 43.60 |
| 12:26:06 | -9 | 0.6 | 43.61 |
| 12:26:07 | -9 | 0.6 | 43.62 |
| 12:26:08 | -9 | 0.6 | 43.63 |
| 12:26:09 | -9 | 0.6 | 43.64 |
| 12:26:10 | -9 | 0.6 | 43.65 |
| 12:26:11 | -9 | 0.6 | 43.66 |
| 12:26:12 | -9 | 0.6 | 43.67 |
| 12:26:13 | -9 | 0.6 | 43.68 |
| 12:26:14 | -9 | 0.6 | 43.69 |
| 12:26:15 | -9 | 0.6 | 43.70 |
| 12:26:16 | -9 | 0.6 | 43.71 |
| 12:26:17 | -9 | 0.6 | 43.72 |
| 12:26:18 | -9 | 0.6 | 43.72 |
| 12:26:19 | -9 | 0.6 | 43.73 |
| 12:26:20 | -9 | 0.6 | 43.74 |
| 12:26:21 | -9 | 0.6 | 43.75 |
| 12:26:22 | -9 | 0.6 | 43.76 |
| 12:26:23 | -9 | 0.6 | 43.77 |
| 12:26:24 | -9 | 0.6 | 43.78 |
| 12:26:25 | -9 | 0.6 | 43.79 |
| 12:26:26 | -9 | 0.6 | 43.80 |
| 12:26:27 | -9 | 0.6 | 43.81 |
| 12:26:28 | -9 | 0.6 | 43.82 |
| 12:26:29 | -9 | 0.6 | 43.83 |
| 12:26:30 | -9 | 0.6 | 43.84 |
| 12:26:31 | -9 | 0.6 | 43.85 |
| 12:26:32 | -9 | 0.6 | 43.86 |
| 12:26:33 | -9 | 0.6 | 43.87 |
| 12:26:34 | -9 | 0.6 | 43.87 |
| 12:26:35 | -9 | 0.6 | 43.88 |
| 12:26:36 | -9 | 0.6 | 43.89 |
| 12:26:37 | -9 | 0.6 | 43.90 |
| 12:26:38 | -9 | 0.6 | 43.91 |
| 12:26:39 | -9 | 0.6 | 43.92 |
| 12:26:40 | -9 | 0.6 | 43.93 |
| 12:26:41 | -9 | 0.6 | 43.94 |
| 12:26:42 | -9 | 0.6 | 43.95 |
| 12:26:43 | -9 | 0.6 | 43.96 |
| 12:26:44 | -9 | 0.6 | 43.97 |
| 12:26:45 | -9 | 0.6 | 43.98 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:26:46 | -9 | 0.6 | 43.99 |
| 12:26:47 | -9 | 0.6 | 44.00 |
| 12:26:48 | -9 | 0.6 | 44.01 |
| 12:26:49 | -9 | 0.6 | 44.02 |
| 12:26:50 | -9 | 0.6 | 44.02 |
| 12:26:51 | -9 | 0.6 | 44.03 |
| 12:26:52 | -9 | 0.6 | 44.04 |
| 12:26:53 | -9 | 0.6 | 44.05 |
| 12:26:54 | -9 | 0.6 | 44.06 |
| 12:26:55 | -9 | 0.6 | 44.07 |
| 12:26:56 | -9 | 0.6 | 44.08 |
| 12:26:57 | -9 | 0.6 | 44.09 |
| 12:26:58 | -9 | 0.6 | 44.10 |
| 12:26:59 | -9 | 0.6 | 44.11 |
| 12:27:00 | -9 | 0.6 | 44.12 |
| 12:27:01 | -9 | 0.6 | 44.13 |
| 12:27:02 | -9 | 0.6 | 44.14 |
| 12:27:03 | -9 | 0.6 | 44.15 |
| 12:27:04 | -9 | 0.6 | 44.16 |
| 12:27:05 | -9 | 0.6 | 44.17 |
| 12:27:06 | -9 | 0.6 | 44.17 |
| 12:27:07 | -9 | 0.6 | 44.18 |
| 12:27:08 | -9 | 0.6 | 44.19 |
| 12:27:09 | -9 | 0.6 | 44.20 |
| 12:27:10 | -9 | 0.6 | 44.21 |
| 12:27:11 | -9 | 0.6 | 44.22 |
| 12:27:12 | -9 | 0.6 | 44.23 |
| 12:27:13 | -9 | 0.6 | 44.24 |
| 12:27:14 | -9 | 0.6 | 44.25 |
| 12:27:15 | -9 | 0.6 | 44.26 |
| 12:27:16 | -9 | 0.6 | 44.27 |
| 12:27:17 | -9 | 0.6 | 44.28 |
| 12:27:18 | -9 | 0.6 | 44.29 |
| 12:27:19 | -9 | 0.6 | 44.30 |
| 12:27:20 | -9 | 0.6 | 44.31 |
| 12:27:21 | -9 | 0.6 | 44.32 |
| 12:27:22 | -9 | 0.6 | 44.32 |
| 12:27:23 | -9 | 0.6 | 44.33 |
| 12:27:24 | -9 | 0.6 | 44.34 |
| 12:27:25 | -9 | 0.6 | 44.35 |
| 12:27:26 | -9 | 0.6 | 44.36 |
| 12:27:27 | -9 | 0.6 | 44.37 |
| 12:27:28 | -9 | 0.6 | 44.38 |
| 12:27:29 | -9 | 0.6 | 44.39 |
| 12:27:30 | -9 | 0.6 | 44.40 |
| 12:27:31 | -9 | 0.6 | 44.41 |
| 12:27:32 | -9 | 0.6 | 44.42 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:27:33 | -9 | 0.6 | 44.43 |
| 12:27:34 | -9 | 0.6 | 44.44 |
| 12:27:35 | -9 | 0.6 | 44.45 |
| 12:27:36 | -9 | 0.6 | 44.46 |
| 12:27:37 | -9 | 0.6 | 44.47 |
| 12:27:38 | -9 | 0.6 | 44.47 |
| 12:27:39 | -9 | 0.6 | 44.48 |
| 12:27:40 | -9 | 0.6 | 44.49 |
| 12:27:41 | -9 | 0.6 | 44.50 |
| 12:27:42 | -9 | 0.6 | 44.51 |
| 12:27:43 | -9 | 0.6 | 44.52 |
| 12:27:44 | -9 | 0.6 | 44.53 |
| 12:27:45 | -9 | 0.6 | 44.54 |
| 12:27:46 | -9 | 0.6 | 44.55 |
| 12:27:47 | -9 | 0.6 | 44.56 |
| 12:27:48 | -9 | 0.6 | 44.57 |
| 12:27:49 | -9 | 0.6 | 44.58 |
| 12:27:50 | -9 | 0.6 | 44.59 |
| 12:27:51 | -9 | 0.6 | 44.60 |
| 12:27:52 | -9 | 0.6 | 44.61 |
| 12:27:53 | -9 | 0.6 | 44.62 |
| 12:27:54 | -9 | 0.6 | 44.62 |
| 12:27:55 | -9 | 0.6 | 44.63 |
| 12:27:56 | -9 | 0.6 | 44.64 |
| 12:27:57 | -9 | 0.6 | 44.65 |
| 12:27:58 | -9 | 0.6 | 44.66 |
| 12:27:59 | -9 | 0.6 | 44.67 |
| 12:28:00 | -9 | 0.6 | 44.68 |
| 12:28:01 | -9 | 0.6 | 44.69 |
| 12:28:02 | -9 | 0.6 | 44.70 |
| 12:28:03 | -9 | 0.6 | 44.71 |
| 12:28:04 | -9 | 0.6 | 44.72 |
| 12:28:05 | -9 | 0.6 | 44.73 |
| 12:28:06 | -9 | 0.6 | 44.74 |
| 12:28:07 | -9 | 0.6 | 44.75 |
| 12:28:08 | -9 | 0.6 | 44.76 |
| 12:28:09 | -9 | 0.6 | 44.76 |
| 12:28:10 | -10 | 0.6 | 44.77 |
| 12:28:11 | -10 | 0.6 | 44.78 |
| 12:28:12 | -10 | 0.6 | 44.79 |
| 12:28:13 | -10 | 0.6 | 44.80 |
| 12:28:14 | -10 | 0.6 | 44.81 |
| 12:28:15 | -10 | 0.6 | 44.82 |
| 12:28:16 | -10 | 0.6 | 44.83 |
| 12:28:17 | -10 | 0.6 | 44.84 |
| 12:28:18 | -10 | 0.6 | 44.85 |
| 12:28:19 | -10 | 0.6 | 44.86 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:28:20 | -10 | 0.6 | 44.87 |
| 12:28:21 | -10 | 0.6 | 44.88 |
| 12:28:22 | -10 | 0.6 | 44.89 |
| 12:28:23 | -10 | 0.6 | 44.90 |
| 12:28:24 | -10 | 0.6 | 44.90 |
| 12:28:25 | -10 | 0.6 | 44.91 |
| 12:28:26 | -10 | 0.6 | 44.92 |
| 12:28:27 | -10 | 0.6 | 44.93 |
| 12:28:28 | -10 | 0.6 | 44.94 |
| 12:28:29 | -10 | 0.6 | 44.95 |
| 12:28:30 | -10 | 0.6 | 44.96 |
| 12:28:31 | -10 | 0.6 | 44.97 |
| 12:28:32 | -10 | 0.6 | 44.98 |
| 12:28:33 | -10 | 0.6 | 44.99 |
| 12:28:34 | -10 | 0.6 | 45.00 |
| 12:28:35 | -10 | 0.6 | 45.01 |
| 12:28:36 | -10 | 0.6 | 45.02 |
| 12:28:37 | -10 | 0.6 | 45.03 |
| 12:28:38 | -10 | 0.6 | 45.04 |
| 12:28:39 | -9 | 0.6 | 45.04 |
| 12:28:40 | -9 | 0.6 | 45.05 |
| 12:28:41 | -9 | 0.6 | 45.06 |
| 12:28:42 | -9 | 0.6 | 45.07 |
| 12:28:43 | -9 | 0.6 | 45.08 |
| 12:28:44 | -9 | 0.6 | 45.09 |
| 12:28:45 | -9 | 0.6 | 45.10 |
| 12:28:46 | -10 | 0.6 | 45.11 |
| 12:28:47 | -10 | 0.6 | 45.12 |
| 12:28:48 | -10 | 0.6 | 45.13 |
| 12:28:49 | -10 | 0.6 | 45.14 |
| 12:28:50 | -10 | 0.6 | 45.15 |
| 12:28:51 | -10 | 0.6 | 45.16 |
| 12:28:52 | -10 | 0.6 | 45.17 |
| 12:28:53 | -10 | 0.6 | 45.18 |
| 12:28:54 | -10 | 0.6 | 45.18 |
| 12:28:55 | -10 | 0.6 | 45.19 |
| 12:28:56 | -10 | 0.6 | 45.20 |
| 12:28:57 | -10 | 0.6 | 45.21 |
| 12:28:58 | -10 | 0.6 | 45.22 |
| 12:28:59 | -10 | 0.6 | 45.23 |
| 12:29:00 | -10 | 0.6 | 45.24 |
| 12:29:01 | -10 | 0.6 | 45.25 |
| 12:29:02 | -10 | 0.6 | 45.26 |
| 12:29:03 | -11 | 0.6 | 45.27 |
| 12:29:04 | -11 | 0.6 | 45.28 |
| 12:29:05 | -11 | 0.6 | 45.29 |
| 12:29:06 | -11 | 0.6 | 45.30 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:29:07 | -11 | 0.6 | 45.31 |
| 12:29:08 | -11 | 0.6 | 45.32 |
| 12:29:09 | -11 | 0.6 | 45.33 |
| 12:29:10 | -11 | 0.6 | 45.33 |
| 12:29:11 | -11 | 0.6 | 45.34 |
| 12:29:12 | -11 | 0.6 | 45.35 |
| 12:29:13 | -11 | 0.6 | 45.36 |
| 12:29:14 | -11 | 0.6 | 45.37 |
| 12:29:15 | -11 | 0.6 | 45.38 |
| 12:29:16 | -11 | 0.6 | 45.39 |
| 12:29:17 | -11 | 0.6 | 45.40 |
| 12:29:18 | -11 | 0.6 | 45.41 |
| 12:29:19 | -11 | 0.6 | 45.42 |
| 12:29:20 | -11 | 0.6 | 45.43 |
| 12:29:21 | -11 | 0.6 | 45.44 |
| 12:29:22 | -11 | 0.6 | 45.45 |
| 12:29:23 | -11 | 0.6 | 45.46 |
| 12:29:24 | -11 | 0.6 | 45.47 |
| 12:29:25 | -11 | 0.6 | 45.47 |
| 12:29:26 | -11 | 0.6 | 45.48 |
| 12:29:27 | -11 | 0.6 | 45.49 |
| 12:29:28 | -11 | 0.6 | 45.50 |
| 12:29:29 | -11 | 0.6 | 45.51 |
| 12:29:30 | -10 | 0.6 | 45.52 |
| 12:29:31 | -10 | 0.6 | 45.53 |
| 12:29:32 | -10 | 0.6 | 45.54 |
| 12:29:33 | -10 | 0.6 | 45.55 |
| 12:29:34 | -10 | 0.6 | 45.56 |
| 12:29:35 | -10 | 0.6 | 45.57 |
| 12:29:36 | -10 | 0.6 | 45.58 |
| 12:29:37 | -10 | 0.6 | 45.59 |
| 12:29:38 | -11 | 0.6 | 45.60 |
| 12:29:39 | -10 | 0.6 | 45.61 |
| 12:29:40 | -10 | 0.6 | 45.61 |
| 12:29:41 | -10 | 0.6 | 45.62 |
| 12:29:42 | -10 | 0.6 | 45.63 |
| 12:29:43 | -10 | 0.6 | 45.64 |
| 12:29:44 | -10 | 0.6 | 45.65 |
| 12:29:45 | -10 | 0.6 | 45.66 |
| 12:29:46 | -10 | 0.6 | 45.67 |
| 12:29:47 | -11 | 0.6 | 45.68 |
| 12:29:48 | -11 | 0.6 | 45.69 |
| 12:29:49 | -11 | 0.6 | 45.70 |
| 12:29:50 | -11 | 0.6 | 45.71 |
| 12:29:51 | -11 | 0.6 | 45.72 |
| 12:29:52 | -11 | 0.6 | 45.73 |
| 12:29:53 | -11 | 0.6 | 45.74 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:29:54 | -11 | 0.6 | 45.75 |
| 12:29:55 | -11 | 0.6 | 45.76 |
| 12:29:56 | -11 | 0.6 | 45.76 |
| 12:29:57 | -11 | 0.6 | 45.77 |
| 12:29:58 | -11 | 0.6 | 45.78 |
| 12:29:59 | -11 | 0.6 | 45.79 |
| 12:30:00 | -11 | 0.6 | 45.80 |
| 12:30:01 | -11 | 0.6 | 45.81 |
| 12:30:02 | -11 | 0.6 | 45.82 |
| 12:30:03 | -11 | 0.6 | 45.83 |
| 12:30:04 | -11 | 0.6 | 45.84 |
| 12:30:05 | -11 | 0.6 | 45.85 |
| 12:30:06 | -11 | 0.6 | 45.86 |
| 12:30:07 | -11 | 0.6 | 45.87 |
| 12:30:08 | -11 | 0.6 | 45.88 |
| 12:30:09 | -11 | 0.6 | 45.89 |
| 12:30:10 | -11 | 0.6 | 45.90 |
| 12:30:11 | -11 | 0.6 | 45.90 |
| 12:30:12 | -11 | 0.6 | 45.91 |
| 12:30:13 | -11 | 0.6 | 45.92 |
| 12:30:14 | -11 | 0.6 | 45.93 |
| 12:30:15 | -11 | 0.6 | 45.94 |
| 12:30:16 | -11 | 0.6 | 45.95 |
| 12:30:17 | -11 | 0.6 | 45.96 |
| 12:30:18 | -11 | 0.6 | 45.97 |
| 12:30:19 | -11 | 0.6 | 45.98 |
| 12:30:20 | -11 | 0.6 | 45.99 |
| 12:30:21 | -11 | 0.6 | 46.00 |
| 12:30:22 | -11 | 0.6 | 46.01 |
| 12:30:23 | -11 | 0.6 | 46.02 |
| 12:30:24 | -11 | 0.6 | 46.03 |
| 12:30:25 | -11 | 0.6 | 46.04 |
| 12:30:26 | -11 | 0.6 | 46.04 |
| 12:30:27 | -11 | 0.6 | 46.05 |
| 12:30:28 | -11 | 0.6 | 46.06 |
| 12:30:29 | -11 | 0.6 | 46.07 |
| 12:30:30 | -11 | 0.6 | 46.08 |
| 12:30:31 | -11 | 0.6 | 46.09 |
| 12:30:32 | -11 | 0.6 | 46.10 |
| 12:30:33 | -11 | 0.6 | 46.11 |
| 12:30:34 | -11 | 0.6 | 46.12 |
| 12:30:35 | -11 | 0.6 | 46.13 |
| 12:30:36 | -11 | 0.6 | 46.14 |
| 12:30:37 | -11 | 0.6 | 46.15 |
| 12:30:38 | -11 | 0.6 | 46.16 |
| 12:30:39 | -11 | 0.6 | 46.17 |
| 12:30:40 | -11 | 0.6 | 46.18 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:30:41 | -11 | 0.6 | 46.18 |
| 12:30:42 | -11 | 0.6 | 46.19 |
| 12:30:43 | -11 | 0.6 | 46.20 |
| 12:30:44 | -11 | 0.6 | 46.21 |
| 12:30:45 | -11 | 0.6 | 46.22 |
| 12:30:46 | -11 | 0.6 | 46.23 |
| 12:30:47 | -11 | 0.6 | 46.24 |
| 12:30:48 | -11 | 0.6 | 46.25 |
| 12:30:49 | -11 | 0.6 | 46.26 |
| 12:30:50 | -11 | 0.6 | 46.27 |
| 12:30:51 | -11 | 0.6 | 46.28 |
| 12:30:52 | -11 | 0.6 | 46.29 |
| 12:30:53 | -11 | 0.6 | 46.30 |
| 12:30:54 | -11 | 0.6 | 46.31 |
| 12:30:55 | -11 | 0.6 | 46.32 |
| 12:30:56 | -11 | 0.6 | 46.33 |
| 12:30:57 | -11 | 0.6 | 46.33 |
| 12:30:58 | -11 | 0.6 | 46.34 |
| 12:30:59 | -11 | 0.6 | 46.35 |
| 12:31:00 | -11 | 0.6 | 46.36 |
| 12:31:01 | -11 | 0.6 | 46.37 |
| 12:31:02 | -11 | 0.6 | 46.38 |
| 12:31:03 | -11 | 0.6 | 46.39 |
| 12:31:04 | -11 | 0.6 | 46.40 |
| 12:31:05 | -11 | 0.6 | 46.41 |
| 12:31:06 | -11 | 0.6 | 46.42 |
| 12:31:07 | -11 | 0.6 | 46.43 |
| 12:31:08 | -11 | 0.6 | 46.44 |
| 12:31:09 | -11 | 0.6 | 46.45 |
| 12:31:10 | -11 | 0.6 | 46.46 |
| 12:31:11 | -11 | 0.6 | 46.47 |
| 12:31:12 | -11 | 0.6 | 46.48 |
| 12:31:13 | -11 | 0.6 | 46.48 |
| 12:31:14 | -11 | 0.6 | 46.49 |
| 12:31:15 | -11 | 0.6 | 46.50 |
| 12:31:16 | -11 | 0.6 | 46.51 |
| 12:31:17 | -11 | 0.6 | 46.52 |
| 12:31:18 | -11 | 0.6 | 46.53 |
| 12:31:19 | -11 | 0.6 | 46.54 |
| 12:31:20 | -11 | 0.6 | 46.55 |
| 12:31:21 | -11 | 0.6 | 46.56 |
| 12:31:22 | -11 | 0.6 | 46.57 |
| 12:31:23 | -11 | 0.6 | 46.58 |
| 12:31:24 | -11 | 0.6 | 46.59 |
| 12:31:25 | -11 | 0.6 | 46.60 |
| 12:31:26 | -11 | 0.6 | 46.61 |
| 12:31:27 | -11 | 0.6 | 46.62 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:31:28 | -11 | 0.6 | 46.62 |
| 12:31:29 | -11 | 0.6 | 46.63 |
| 12:31:30 | -11 | 0.6 | 46.64 |
| 12:31:31 | -11 | 0.6 | 46.65 |
| 12:31:32 | -11 | 0.6 | 46.66 |
| 12:31:33 | -11 | 0.6 | 46.67 |
| 12:31:34 | -11 | 0.6 | 46.68 |
| 12:31:35 | -11 | 0.6 | 46.69 |
| 12:31:36 | -11 | 0.6 | 46.70 |
| 12:31:37 | -11 | 0.6 | 46.71 |
| 12:31:38 | -11 | 0.6 | 46.72 |
| 12:31:39 | -11 | 0.6 | 46.73 |
| 12:31:40 | -11 | 0.6 | 46.74 |
| 12:31:41 | -11 | 0.6 | 46.75 |
| 12:31:42 | -11 | 0.6 | 46.76 |
| 12:31:43 | -11 | 0.6 | 46.77 |
| 12:31:44 | -11 | 0.6 | 46.77 |
| 12:31:45 | -11 | 0.6 | 46.78 |
| 12:31:46 | -11 | 0.6 | 46.79 |
| 12:31:47 | -11 | 0.6 | 46.80 |
| 12:31:48 | -11 | 0.6 | 46.81 |
| 12:31:49 | -11 | 0.6 | 46.82 |
| 12:31:50 | -11 | 0.6 | 46.83 |
| 12:31:51 | -11 | 0.6 | 46.84 |
| 12:31:52 | -11 | 0.6 | 46.85 |
| 12:31:53 | -11 | 0.6 | 46.86 |
| 12:31:54 | -11 | 0.6 | 46.87 |
| 12:31:55 | -11 | 0.6 | 46.88 |
| 12:31:56 | -11 | 0.6 | 46.89 |
| 12:31:57 | -11 | 0.6 | 46.90 |
| 12:31:58 | -11 | 0.6 | 46.91 |
| 12:31:59 | -11 | 0.6 | 46.91 |
| 12:32:00 | -11 | 0.6 | 46.92 |
| 12:32:01 | -11 | 0.6 | 46.93 |
| 12:32:02 | -11 | 0.6 | 46.94 |
| 12:32:03 | -11 | 0.6 | 46.95 |
| 12:32:04 | -11 | 0.6 | 46.96 |
| 12:32:05 | -11 | 0.6 | 46.97 |
| 12:32:06 | -12 | 0.6 | 46.98 |
| 12:32:07 | -11 | 0.6 | 46.99 |
| 12:32:08 | -11 | 0.6 | 47.00 |
| 12:32:09 | -12 | 0.6 | 47.01 |
| 12:32:10 | -12 | 0.6 | 47.02 |
| 12:32:11 | -12 | 0.6 | 47.03 |
| 12:32:12 | -12 | 0.6 | 47.04 |
| 12:32:13 | -12 | 0.6 | 47.05 |
| 12:32:14 | -11 | 0.6 | 47.06 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:32:15 | -11 | 0.6 | 47.06 |
| 12:32:16 | -11 | 0.6 | 47.07 |
| 12:32:17 | -11 | 0.6 | 47.08 |
| 12:32:18 | -11 | 0.6 | 47.09 |
| 12:32:19 | -11 | 0.6 | 47.10 |
| 12:32:20 | -11 | 0.6 | 47.11 |
| 12:32:21 | -12 | 0.6 | 47.12 |
| 12:32:22 | -12 | 0.6 | 47.13 |
| 12:32:23 | -12 | 0.6 | 47.14 |
| 12:32:24 | -12 | 0.6 | 47.15 |
| 12:32:25 | -12 | 0.6 | 47.16 |
| 12:32:26 | -12 | 0.6 | 47.17 |
| 12:32:27 | -12 | 0.6 | 47.18 |
| 12:32:28 | -12 | 0.6 | 47.19 |
| 12:32:29 | -12 | 0.6 | 47.20 |
| 12:32:30 | -12 | 0.6 | 47.20 |
| 12:32:31 | -12 | 0.6 | 47.21 |
| 12:32:32 | -12 | 0.6 | 47.22 |
| 12:32:33 | -12 | 0.6 | 47.23 |
| 12:32:34 | -12 | 0.6 | 47.24 |
| 12:32:35 | -12 | 0.6 | 47.25 |
| 12:32:36 | -12 | 0.6 | 47.26 |
| 12:32:37 | -12 | 0.6 | 47.27 |
| 12:32:38 | -12 | 0.6 | 47.28 |
| 12:32:39 | -12 | 0.6 | 47.29 |
| 12:32:40 | -12 | 0.6 | 47.30 |
| 12:32:41 | -12 | 0.6 | 47.31 |
| 12:32:42 | -12 | 0.6 | 47.32 |
| 12:32:43 | -12 | 0.6 | 47.33 |
| 12:32:44 | -12 | 0.6 | 47.34 |
| 12:32:45 | -12 | 0.6 | 47.35 |
| 12:32:46 | -12 | 0.6 | 47.35 |
| 12:32:47 | -12 | 0.6 | 47.36 |
| 12:32:48 | -12 | 0.6 | 47.37 |
| 12:32:49 | -12 | 0.6 | 47.38 |
| 12:32:50 | -12 | 0.6 | 47.39 |
| 12:32:51 | -12 | 0.6 | 47.40 |
| 12:32:52 | -12 | 0.6 | 47.41 |
| 12:32:53 | -12 | 0.6 | 47.42 |
| 12:32:54 | -12 | 0.6 | 47.43 |
| 12:32:55 | -12 | 0.6 | 47.44 |
| 12:32:56 | -12 | 0.6 | 47.45 |
| 12:32:57 | -12 | 0.6 | 47.46 |
| 12:32:58 | -12 | 0.6 | 47.47 |
| 12:32:59 | -12 | 0.6 | 47.48 |
| 12:33:00 | -12 | 0.6 | 47.49 |
| 12:33:01 | -11 | 0.6 | 47.49 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:33:02 | -11 | 0.6 | 47.50 |
| 12:33:03 | -11 | 0.6 | 47.51 |
| 12:33:04 | -11 | 0.6 | 47.53 |
| 12:33:05 | -11 | 0.6 | 47.53 |
| 12:33:06 | -11 | 0.6 | 47.54 |
| 12:33:07 | -11 | 0.6 | 47.55 |
| 12:33:08 | -11 | 0.6 | 47.56 |
| 12:33:09 | -11 | 0.6 | 47.57 |
| 12:33:10 | -12 | 0.6 | 47.58 |
| 12:33:11 | -12 | 0.6 | 47.59 |
| 12:33:12 | -12 | 0.6 | 47.60 |
| 12:33:13 | -12 | 0.6 | 47.61 |
| 12:33:14 | -12 | 0.6 | 47.62 |
| 12:33:15 | -12 | 0.6 | 47.63 |
| 12:33:16 | -12 | 0.6 | 47.64 |
| 12:33:17 | -12 | 0.6 | 47.65 |
| 12:33:18 | -12 | 0.6 | 47.66 |
| 12:33:19 | -12 | 0.6 | 47.67 |
| 12:33:20 | -12 | 0.6 | 47.68 |
| 12:33:21 | -12 | 0.6 | 47.68 |
| 12:33:22 | -12 | 0.6 | 47.69 |
| 12:33:23 | -12 | 0.6 | 47.70 |
| 12:33:24 | -12 | 0.6 | 47.71 |
| 12:33:25 | -12 | 0.6 | 47.72 |
| 12:33:26 | -12 | 0.6 | 47.73 |
| 12:33:27 | -12 | 0.6 | 47.74 |
| 12:33:28 | -12 | 0.6 | 47.75 |
| 12:33:29 | -12 | 0.6 | 47.76 |
| 12:33:30 | -12 | 0.6 | 47.77 |
| 12:33:31 | -12 | 0.6 | 47.78 |
| 12:33:32 | -12 | 0.6 | 47.79 |
| 12:33:33 | -12 | 0.6 | 47.80 |
| 12:33:34 | -12 | 0.6 | 47.81 |
| 12:33:35 | -12 | 0.6 | 47.82 |
| 12:33:36 | -12 | 0.6 | 47.82 |
| 12:33:37 | -12 | 0.6 | 47.83 |
| 12:33:38 | -12 | 0.6 | 47.84 |
| 12:33:39 | -12 | 0.6 | 47.85 |
| 12:33:40 | -12 | 0.6 | 47.86 |
| 12:33:41 | -12 | 0.6 | 47.87 |
| 12:33:42 | -12 | 0.6 | 47.88 |
| 12:33:43 | -12 | 0.6 | 47.89 |
| 12:33:44 | -12 | 0.6 | 47.90 |
| 12:33:45 | -12 | 0.6 | 47.91 |
| 12:33:46 | -12 | 0.6 | 47.92 |
| 12:33:47 | -12 | 0.6 | 47.93 |
| 12:33:48 | -12 | 0.6 | 47.94 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:33:49 | -11 | 0.6 | 47.95 |
| 12:33:50 | -11 | 0.6 | 47.96 |
| 12:33:51 | -11 | 0.6 | 47.97 |
| 12:33:52 | -11 | 0.6 | 47.97 |
| 12:33:53 | -11 | 0.6 | 47.98 |
| 12:33:54 | -11 | 0.6 | 47.99 |
| 12:33:55 | -11 | 0.6 | 48.00 |
| 12:33:56 | -12 | 0.6 | 48.01 |
| 12:33:57 | -12 | 0.6 | 48.02 |
| 12:33:58 | -12 | 0.6 | 48.03 |
| 12:33:59 | -12 | 0.6 | 48.04 |
| 12:34:00 | -12 | 0.6 | 48.05 |
| 12:34:01 | -12 | 0.6 | 48.06 |
| 12:34:02 | -12 | 0.6 | 48.07 |
| 12:34:03 | -12 | 0.6 | 48.08 |
| 12:34:04 | -12 | 0.6 | 48.09 |
| 12:34:05 | -12 | 0.6 | 48.10 |
| 12:34:06 | -12 | 0.6 | 48.11 |
| 12:34:07 | -12 | 0.6 | 48.12 |
| 12:34:08 | -12 | 0.6 | 48.12 |
| 12:34:09 | -12 | 0.6 | 48.13 |
| 12:34:10 | -12 | 0.6 | 48.14 |
| 12:34:11 | -12 | 0.6 | 48.15 |
| 12:34:12 | -12 | 0.6 | 48.16 |
| 12:34:13 | -12 | 0.6 | 48.17 |
| 12:34:14 | -12 | 0.6 | 48.18 |
| 12:34:15 | -12 | 0.6 | 48.19 |
| 12:34:16 | -12 | 0.6 | 48.20 |
| 12:34:17 | -12 | 0.6 | 48.21 |
| 12:34:18 | -12 | 0.6 | 48.22 |
| 12:34:19 | -12 | 0.6 | 48.23 |
| 12:34:20 | -12 | 0.6 | 48.24 |
| 12:34:21 | -12 | 0.6 | 48.25 |
| 12:34:22 | -12 | 0.6 | 48.26 |
| 12:34:23 | -12 | 0.6 | 48.26 |
| 12:34:24 | -12 | 0.6 | 48.27 |
| 12:34:25 | -12 | 0.6 | 48.28 |
| 12:34:26 | -12 | 0.6 | 48.29 |
| 12:34:27 | -12 | 0.6 | 48.30 |
| 12:34:28 | -12 | 0.6 | 48.31 |
| 12:34:29 | -12 | 0.6 | 48.32 |
| 12:34:30 | -12 | 0.6 | 48.33 |
| 12:34:31 | -12 | 0.6 | 48.34 |
| 12:34:32 | -12 | 0.6 | 48.35 |
| 12:34:33 | -12 | 0.6 | 48.36 |
| 12:34:34 | -12 | 0.6 | 48.37 |
| 12:34:35 | -12 | 0.6 | 48.38 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:34:36 | -12 | 0.6 | 48.39 |
| 12:34:37 | -12 | 0.6 | 48.40 |
| 12:34:38 | -12 | 0.6 | 48.41 |
| 12:34:39 | -12 | 0.6 | 48.41 |
| 12:34:40 | -12 | 0.6 | 48.42 |
| 12:34:41 | -12 | 0.6 | 48.43 |
| 12:34:42 | -12 | 0.6 | 48.44 |
| 12:34:43 | -12 | 0.6 | 48.45 |
| 12:34:44 | -12 | 0.6 | 48.46 |
| 12:34:45 | -12 | 0.6 | 48.47 |
| 12:34:46 | -12 | 0.6 | 48.48 |
| 12:34:47 | -12 | 0.6 | 48.49 |
| 12:34:48 | -12 | 0.6 | 48.50 |
| 12:34:49 | -12 | 0.6 | 48.51 |
| 12:34:50 | -12 | 0.6 | 48.52 |
| 12:34:51 | -12 | 0.6 | 48.53 |
| 12:34:52 | -12 | 0.6 | 48.54 |
| 12:34:53 | -12 | 0.6 | 48.55 |
| 12:34:54 | -12 | 0.6 | 48.56 |
| 12:34:55 | -12 | 0.6 | 48.56 |
| 12:34:56 | -12 | 0.6 | 48.57 |
| 12:34:57 | -12 | 0.6 | 48.58 |
| 12:34:58 | -12 | 0.6 | 48.59 |
| 12:34:59 | -12 | 0.6 | 48.60 |
| 12:35:00 | -12 | 0.6 | 48.61 |
| 12:35:01 | -12 | 0.6 | 48.62 |
| 12:35:02 | -12 | 0.6 | 48.63 |
| 12:35:03 | -12 | 0.6 | 48.64 |
| 12:35:04 | -12 | 0.6 | 48.65 |
| 12:35:05 | -12 | 0.6 | 48.66 |
| 12:35:06 | -12 | 0.6 | 48.67 |
| 12:35:07 | -12 | 0.6 | 48.68 |
| 12:35:08 | -12 | 0.6 | 48.69 |
| 12:35:09 | -12 | 0.6 | 48.70 |
| 12:35:10 | -12 | 0.6 | 48.70 |
| 12:35:11 | -12 | 0.6 | 48.71 |
| 12:35:12 | -12 | 0.6 | 48.72 |
| 12:35:13 | -12 | 0.6 | 48.73 |
| 12:35:14 | -12 | 0.6 | 48.74 |
| 12:35:15 | -12 | 0.6 | 48.75 |
| 12:35:16 | -12 | 0.6 | 48.76 |
| 12:35:17 | -12 | 0.6 | 48.77 |
| 12:35:18 | -12 | 0.6 | 48.78 |
| 12:35:19 | -13 | 0.6 | 48.79 |
| 12:35:20 | -13 | 0.6 | 48.80 |
| 12:35:21 | -13 | 0.6 | 48.81 |
| 12:35:22 | -12 | 0.6 | 48.82 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:35:23 | -12 | 0.6 | 48.83 |
| 12:35:24 | -12 | 0.6 | 48.84 |
| 12:35:25 | -12 | 0.6 | 48.85 |
| 12:35:26 | -12 | 0.6 | 48.85 |
| 12:35:27 | -12 | 0.6 | 48.86 |
| 12:35:28 | -12 | 0.6 | 48.87 |
| 12:35:29 | -12 | 0.6 | 48.88 |
| 12:35:30 | -12 | 0.6 | 48.89 |
| 12:35:31 | -12 | 0.6 | 48.90 |
| 12:35:32 | -12 | 0.6 | 48.91 |
| 12:35:33 | -12 | 0.6 | 48.92 |
| 12:35:34 | -11 | 0.6 | 48.93 |
| 12:35:35 | -11 | 0.6 | 48.94 |
| 12:35:36 | -11 | 0.6 | 48.95 |
| 12:35:37 | -11 | 0.6 | 48.96 |
| 12:35:38 | -11 | 0.6 | 48.97 |
| 12:35:39 | -11 | 0.6 | 48.98 |
| 12:35:40 | -11 | 0.6 | 48.99 |
| 12:35:41 | -11 | 0.6 | 49.00 |
| 12:35:42 | -11 | 0.6 | 49.00 |
| 12:35:43 | -11 | 0.6 | 49.01 |
| 12:35:44 | -11 | 0.6 | 49.02 |
| 12:35:45 | -11 | 0.6 | 49.03 |
| 12:35:46 | -11 | 0.6 | 49.04 |
| 12:35:47 | -11 | 0.6 | 49.05 |
| 12:35:48 | -11 | 0.6 | 49.06 |
| 12:35:49 | -11 | 0.6 | 49.07 |
| 12:35:50 | -12 | 0.6 | 49.08 |
| 12:35:51 | -12 | 0.6 | 49.09 |
| 12:35:52 | -12 | 0.6 | 49.10 |
| 12:35:53 | -12 | 0.6 | 49.11 |
| 12:35:54 | -12 | 0.6 | 49.12 |
| 12:35:55 | -12 | 0.6 | 49.13 |
| 12:35:56 | -12 | 0.6 | 49.14 |
| 12:35:57 | -12 | 0.6 | 49.15 |
| 12:35:58 | -12 | 0.6 | 49.15 |
| 12:35:59 | -12 | 0.6 | 49.16 |
| 12:36:00 | -12 | 0.6 | 49.17 |
| 12:36:01 | -12 | 0.6 | 49.18 |
| 12:36:02 | -12 | 0.6 | 49.19 |
| 12:36:03 | -12 | 0.6 | 49.20 |
| 12:36:04 | -12 | 0.6 | 49.21 |
| 12:36:05 | -12 | 0.6 | 49.22 |
| 12:36:06 | -12 | 0.6 | 49.23 |
| 12:36:07 | -12 | 0.6 | 49.24 |
| 12:36:08 | -13 | 0.6 | 49.25 |
| 12:36:09 | -12 | 0.6 | 49.26 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:36:10 | -12 | 0.6 | 49.27 |
| 12:36:11 | -13 | 0.6 | 49.28 |
| 12:36:12 | -13 | 0.6 | 49.29 |
| 12:36:13 | -13 | 0.6 | 49.30 |
| 12:36:14 | -13 | 0.6 | 49.30 |
| 12:36:15 | -13 | 0.6 | 49.31 |
| 12:36:16 | -13 | 0.6 | 49.32 |
| 12:36:17 | -13 | 0.6 | 49.33 |
| 12:36:18 | -13 | 0.6 | 49.34 |
| 12:36:19 | -12 | 0.6 | 49.35 |
| 12:36:20 | -12 | 0.6 | 49.36 |
| 12:36:21 | -12 | 0.6 | 49.37 |
| 12:36:22 | -12 | 0.6 | 49.38 |
| 12:36:23 | -12 | 0.6 | 49.39 |
| 12:36:24 | -12 | 0.6 | 49.40 |
| 12:36:25 | -12 | 0.6 | 49.41 |
| 12:36:26 | -12 | 0.6 | 49.42 |
| 12:36:27 | -12 | 0.6 | 49.43 |
| 12:36:28 | -12 | 0.6 | 49.44 |
| 12:36:29 | -12 | 0.6 | 49.44 |
| 12:36:30 | -12 | 0.6 | 49.45 |
| 12:36:31 | -12 | 0.6 | 49.46 |
| 12:36:32 | -12 | 0.6 | 49.47 |
| 12:36:33 | -12 | 0.6 | 49.48 |
| 12:36:34 | -12 | 0.6 | 49.49 |
| 12:36:35 | -12 | 0.6 | 49.50 |
| 12:36:36 | -12 | 0.6 | 49.51 |
| 12:36:37 | -12 | 0.6 | 49.52 |
| 12:36:38 | -12 | 0.6 | 49.53 |
| 12:36:39 | -12 | 0.6 | 49.54 |
| 12:36:40 | -12 | 0.6 | 49.55 |
| 12:36:41 | -12 | 0.6 | 49.56 |
| 12:36:42 | -12 | 0.6 | 49.57 |
| 12:36:43 | -12 | 0.6 | 49.58 |
| 12:36:44 | -12 | 0.6 | 49.59 |
| 12:36:45 | -12 | 0.6 | 49.59 |
| 12:36:46 | -12 | 0.6 | 49.60 |
| 12:36:47 | -12 | 0.6 | 49.61 |
| 12:36:48 | -12 | 0.6 | 49.62 |
| 12:36:49 | -12 | 0.6 | 49.63 |
| 12:36:50 | -12 | 0.6 | 49.64 |
| 12:36:51 | -11 | 0.6 | 49.65 |
| 12:36:52 | -11 | 0.6 | 49.66 |
| 12:36:53 | -11 | 0.6 | 49.67 |
| 12:36:54 | -11 | 0.6 | 49.68 |
| 12:36:55 | -11 | 0.6 | 49.69 |
| 12:36:56 | -11 | 0.6 | 49.70 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:36:57 | -11 | 0.6 | 49.71 |
| 12:36:58 | -11 | 0.6 | 49.72 |
| 12:36:59 | -11 | 0.6 | 49.73 |
| 12:37:00 | -11 | 0.6 | 49.74 |
| 12:37:01 | -11 | 0.6 | 49.74 |
| 12:37:02 | -11 | 0.6 | 49.75 |
| 12:37:03 | -11 | 0.6 | 49.76 |
| 12:37:04 | -11 | 0.6 | 49.77 |
| 12:37:05 | -11 | 0.6 | 49.78 |
| 12:37:06 | -11 | 0.6 | 49.79 |
| 12:37:07 | -11 | 0.6 | 49.80 |
| 12:37:08 | -11 | 0.6 | 49.81 |
| 12:37:09 | -12 | 0.6 | 49.82 |
| 12:37:10 | -12 | 0.6 | 49.83 |
| 12:37:11 | -12 | 0.6 | 49.84 |
| 12:37:12 | -12 | 0.6 | 49.85 |
| 12:37:13 | -12 | 0.6 | 49.86 |
| 12:37:14 | -12 | 0.6 | 49.87 |
| 12:37:15 | -12 | 0.6 | 49.88 |
| 12:37:16 | -12 | 0.6 | 49.89 |
| 12:37:17 | -12 | 0.6 | 49.89 |
| 12:37:18 | -12 | 0.6 | 49.90 |
| 12:37:19 | -12 | 0.6 | 49.91 |
| 12:37:20 | -12 | 0.6 | 49.92 |
| 12:37:21 | -12 | 0.6 | 49.93 |
| 12:37:22 | -12 | 0.6 | 49.94 |
| 12:37:23 | -12 | 0.6 | 49.95 |
| 12:37:24 | -12 | 0.6 | 49.96 |
| 12:37:25 | -12 | 0.6 | 49.97 |
| 12:37:26 | -12 | 0.6 | 49.98 |
| 12:37:27 | -12 | 0.6 | 49.99 |
| 12:37:28 | -12 | 0.6 | 50.00 |
| 12:37:29 | -12 | 0.6 | 50.01 |
| 12:37:30 | -12 | 0.6 | 50.02 |
| 12:37:31 | -12 | 0.6 | 50.03 |
| 12:37:32 | -12 | 0.6 | 50.04 |
| 12:37:33 | -12 | 0.6 | 50.04 |
| 12:37:34 | -12 | 0.6 | 50.05 |
| 12:37:35 | -12 | 0.6 | 50.06 |
| 12:37:36 | -12 | 0.6 | 50.07 |
| 12:37:37 | -12 | 0.6 | 50.08 |
| 12:37:38 | -12 | 0.6 | 50.09 |
| 12:37:39 | -12 | 0.6 | 50.10 |
| 12:37:40 | -13 | 0.6 | 50.11 |
| 12:37:41 | -13 | 0.6 | 50.12 |
| 12:37:42 | -12 | 0.6 | 50.13 |
| 12:37:43 | -12 | 0.6 | 50.14 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:37:44 | -12 | 0.6 | 50.15 |
| 12:37:45 | -12 | 0.6 | 50.16 |
| 12:37:46 | -12 | 0.6 | 50.17 |
| 12:37:47 | -12 | 0.6 | 50.18 |
| 12:37:48 | -12 | 0.6 | 50.19 |
| 12:37:49 | -12 | 0.6 | 50.19 |
| 12:37:50 | -12 | 0.6 | 50.20 |
| 12:37:51 | -12 | 0.6 | 50.21 |
| 12:37:52 | -12 | 0.6 | 50.22 |
| 12:37:53 | -13 | 0.6 | 50.23 |
| 12:37:54 | -12 | 0.6 | 50.24 |
| 12:37:55 | -12 | 0.6 | 50.25 |
| 12:37:56 | -12 | 0.6 | 50.26 |
| 12:37:57 | -12 | 0.6 | 50.27 |
| 12:37:58 | -12 | 0.6 | 50.28 |
| 12:37:59 | -12 | 0.6 | 50.29 |
| 12:38:00 | -13 | 0.6 | 50.30 |
| 12:38:01 | -13 | 0.6 | 50.31 |
| 12:38:02 | -13 | 0.6 | 50.32 |
| 12:38:03 | -13 | 0.6 | 50.33 |
| 12:38:04 | -13 | 0.6 | 50.34 |
| 12:38:05 | -12 | 0.6 | 50.34 |
| 12:38:06 | -12 | 0.6 | 50.35 |
| 12:38:07 | -12 | 0.6 | 50.36 |
| 12:38:08 | -12 | 0.6 | 50.37 |
| 12:38:09 | -12 | 0.6 | 50.38 |
| 12:38:10 | -12 | 0.6 | 50.39 |
| 12:38:11 | -12 | 0.6 | 50.40 |
| 12:38:12 | -12 | 0.6 | 50.41 |
| 12:38:13 | -12 | 0.6 | 50.42 |
| 12:38:14 | -12 | 0.6 | 50.43 |
| 12:38:15 | -12 | 0.6 | 50.44 |
| 12:38:16 | -12 | 0.6 | 50.45 |
| 12:38:17 | -12 | 0.6 | 50.46 |
| 12:38:18 | -12 | 0.6 | 50.47 |
| 12:38:19 | -12 | 0.6 | 50.48 |
| 12:38:20 | -12 | 0.6 | 50.48 |
| 12:38:21 | -12 | 0.6 | 50.49 |
| 12:38:22 | -12 | 0.6 | 50.50 |
| 12:38:23 | -13 | 0.6 | 50.51 |
| 12:38:24 | -13 | 0.6 | 50.52 |
| 12:38:25 | -13 | 0.6 | 50.53 |
| 12:38:26 | -13 | 0.6 | 50.54 |
| 12:38:27 | -13 | 0.6 | 50.55 |
| 12:38:28 | -13 | 0.6 | 50.56 |
| 12:38:29 | -13 | 0.6 | 50.57 |
| 12:38:30 | -13 | 0.6 | 50.58 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:38:31 | -12 | 0.6 | 50.59 |
| 12:38:32 | -12 | 0.6 | 50.60 |
| 12:38:33 | -12 | 0.6 | 50.61 |
| 12:38:34 | -12 | 0.6 | 50.62 |
| 12:38:35 | -12 | 0.6 | 50.63 |
| 12:38:36 | -12 | 0.6 | 50.63 |
| 12:38:37 | -12 | 0.6 | 50.64 |
| 12:38:38 | -12 | 0.6 | 50.65 |
| 12:38:39 | -12 | 0.6 | 50.66 |
| 12:38:40 | -12 | 0.6 | 50.67 |
| 12:38:41 | -12 | 0.6 | 50.68 |
| 12:38:42 | -12 | 0.6 | 50.69 |
| 12:38:43 | -12 | 0.6 | 50.70 |
| 12:38:44 | -12 | 0.6 | 50.71 |
| 12:38:45 | -12 | 0.6 | 50.72 |
| 12:38:46 | -12 | 0.6 | 50.73 |
| 12:38:47 | -12 | 0.6 | 50.74 |
| 12:38:48 | -12 | 0.6 | 50.75 |
| 12:38:49 | -12 | 0.6 | 50.76 |
| 12:38:50 | -13 | 0.6 | 50.77 |
| 12:38:51 | -13 | 0.6 | 50.78 |
| 12:38:52 | -13 | 0.6 | 50.78 |
| 12:38:53 | -13 | 0.6 | 50.79 |
| 12:38:54 | -13 | 0.6 | 50.80 |
| 12:38:55 | -13 | 0.6 | 50.81 |
| 12:38:56 | -13 | 0.6 | 50.82 |
| 12:38:57 | -13 | 0.6 | 50.83 |
| 12:38:58 | -13 | 0.6 | 50.84 |
| 12:38:59 | -13 | 0.6 | 50.85 |
| 12:39:00 | -13 | 0.6 | 50.86 |
| 12:39:01 | -13 | 0.6 | 50.87 |
| 12:39:02 | -13 | 0.6 | 50.88 |
| 12:39:03 | -13 | 0.6 | 50.89 |
| 12:39:04 | -13 | 0.6 | 50.90 |
| 12:39:05 | -13 | 0.6 | 50.91 |
| 12:39:06 | -13 | 0.6 | 50.92 |
| 12:39:07 | -13 | 0.6 | 50.93 |
| 12:39:08 | -13 | 0.6 | 50.93 |
| 12:39:09 | -13 | 0.6 | 50.94 |
| 12:39:10 | -13 | 0.6 | 50.95 |
| 12:39:11 | -13 | 0.6 | 50.96 |
| 12:39:12 | -13 | 0.6 | 50.97 |
| 12:39:13 | -13 | 0.6 | 50.98 |
| 12:39:14 | -13 | 0.6 | 50.99 |
| 12:39:15 | -13 | 0.6 | 51.00 |
| 12:39:16 | -13 | 0.6 | 51.01 |
| 12:39:17 | -13 | 0.6 | 51.02 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:39:18 | -13 | 0.6 | 51.03 |
| 12:39:19 | -13 | 0.6 | 51.04 |
| 12:39:20 | -12 | 0.6 | 51.05 |
| 12:39:21 | -12 | 0.6 | 51.06 |
| 12:39:22 | -12 | 0.6 | 51.07 |
| 12:39:23 | -12 | 0.6 | 51.08 |
| 12:39:24 | -12 | 0.6 | 51.09 |
| 12:39:25 | -12 | 0.6 | 51.09 |
| 12:39:26 | -12 | 0.6 | 51.10 |
| 12:39:27 | -12 | 0.6 | 51.11 |
| 12:39:28 | -12 | 0.6 | 51.12 |
| 12:39:29 | -12 | 0.6 | 51.13 |
| 12:39:30 | -12 | 0.6 | 51.14 |
| 12:39:31 | -12 | 0.6 | 51.15 |
| 12:39:32 | -12 | 0.6 | 51.16 |
| 12:39:33 | -12 | 0.6 | 51.17 |
| 12:39:34 | -12 | 0.6 | 51.18 |
| 12:39:35 | -12 | 0.6 | 51.19 |
| 12:39:36 | -12 | 0.6 | 51.20 |
| 12:39:37 | -12 | 0.6 | 51.21 |
| 12:39:38 | -13 | 0.6 | 51.22 |
| 12:39:39 | -12 | 0.6 | 51.23 |
| 12:39:40 | -12 | 0.6 | 51.24 |
| 12:39:41 | -12 | 0.6 | 51.24 |
| 12:39:42 | -13 | 0.6 | 51.25 |
| 12:39:43 | -13 | 0.6 | 51.26 |
| 12:39:44 | -13 | 0.6 | 51.27 |
| 12:39:45 | -13 | 0.6 | 51.28 |
| 12:39:46 | -13 | 0.6 | 51.29 |
| 12:39:47 | -13 | 0.6 | 51.30 |
| 12:39:48 | -13 | 0.6 | 51.31 |
| 12:39:49 | -13 | 0.6 | 51.32 |
| 12:39:50 | -13 | 0.6 | 51.33 |
| 12:39:51 | -13 | 0.6 | 51.34 |
| 12:39:52 | -13 | 0.6 | 51.35 |
| 12:39:53 | -13 | 0.6 | 51.36 |
| 12:39:54 | -13 | 0.6 | 51.37 |
| 12:39:55 | -13 | 0.6 | 51.38 |
| 12:39:56 | -13 | 0.6 | 51.39 |
| 12:39:57 | -13 | 0.6 | 51.39 |
| 12:39:58 | -13 | 0.6 | 51.40 |
| 12:39:59 | -13 | 0.6 | 51.41 |
| 12:40:00 | -13 | 0.6 | 51.42 |
| 12:40:01 | -13 | 0.6 | 51.43 |
| 12:40:02 | -13 | 0.6 | 51.44 |
| 12:40:03 | -13 | 0.6 | 51.45 |
| 12:40:04 | -13 | 0.6 | 51.46 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:40:05 | -13 | 0.6 | 51.47 |
| 12:40:06 | -13 | 0.6 | 51.48 |
| 12:40:07 | -12 | 0.6 | 51.49 |
| 12:40:08 | -12 | 0.6 | 51.50 |
| 12:40:09 | -13 | 0.6 | 51.51 |
| 12:40:10 | -13 | 0.6 | 51.52 |
| 12:40:11 | -13 | 0.6 | 51.53 |
| 12:40:12 | -13 | 0.6 | 51.54 |
| 12:40:13 | -13 | 0.6 | 51.54 |
| 12:40:14 | -13 | 0.6 | 51.55 |
| 12:40:15 | -13 | 0.6 | 51.56 |
| 12:40:16 | -13 | 0.6 | 51.57 |
| 12:40:17 | -13 | 0.6 | 51.58 |
| 12:40:18 | -13 | 0.6 | 51.59 |
| 12:40:19 | -13 | 0.6 | 51.60 |
| 12:40:20 | -13 | 0.6 | 51.61 |
| 12:40:21 | -13 | 0.6 | 51.62 |
| 12:40:22 | -13 | 0.6 | 51.63 |
| 12:40:23 | -13 | 0.6 | 51.64 |
| 12:40:24 | -13 | 0.6 | 51.65 |
| 12:40:25 | -13 | 0.6 | 51.66 |
| 12:40:26 | -13 | 0.6 | 51.67 |
| 12:40:27 | -13 | 0.6 | 51.68 |
| 12:40:28 | -13 | 0.6 | 51.69 |
| 12:40:29 | -13 | 0.6 | 51.69 |
| 12:40:30 | -13 | 0.6 | 51.70 |
| 12:40:31 | -13 | 0.6 | 51.71 |
| 12:40:32 | -13 | 0.6 | 51.72 |
| 12:40:33 | -13 | 0.6 | 51.73 |
| 12:40:34 | -12 | 0.6 | 51.74 |
| 12:40:35 | -12 | 0.6 | 51.75 |
| 12:40:36 | -12 | 0.6 | 51.76 |
| 12:40:37 | -12 | 0.6 | 51.77 |
| 12:40:38 | -12 | 0.6 | 51.78 |
| 12:40:39 | -12 | 0.6 | 51.79 |
| 12:40:40 | -12 | 0.6 | 51.80 |
| 12:40:41 | -12 | 0.6 | 51.81 |
| 12:40:42 | -12 | 0.6 | 51.82 |
| 12:40:43 | -12 | 0.6 | 51.83 |
| 12:40:44 | -12 | 0.6 | 51.84 |
| 12:40:45 | -12 | 0.6 | 51.85 |
| 12:40:46 | -12 | 0.6 | 51.85 |
| 12:40:47 | -12 | 0.6 | 51.86 |
| 12:40:48 | -12 | 0.6 | 51.87 |
| 12:40:49 | -12 | 0.6 | 51.88 |
| 12:40:50 | -12 | 0.6 | 51.89 |
| 12:40:51 | -12 | 0.6 | 51.90 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:40:52 | -12 | 0.6 | 51.91 |
| 12:40:53 | -12 | 0.6 | 51.92 |
| 12:40:54 | -12 | 0.6 | 51.93 |
| 12:40:55 | -12 | 0.6 | 51.94 |
| 12:40:56 | -13 | 0.6 | 51.95 |
| 12:40:57 | -13 | 0.6 | 51.96 |
| 12:40:58 | -13 | 0.6 | 51.97 |
| 12:40:59 | -12 | 0.6 | 51.98 |
| 12:41:00 | -12 | 0.6 | 51.99 |
| 12:41:01 | -13 | 0.6 | 52.00 |
| 12:41:02 | -13 | 0.6 | 52.00 |
| 12:41:03 | -13 | 0.6 | 52.01 |
| 12:41:04 | -13 | 0.6 | 52.02 |
| 12:41:05 | -13 | 0.6 | 52.03 |
| 12:41:06 | -12 | 0.6 | 52.04 |
| 12:41:07 | -12 | 0.6 | 52.05 |
| 12:41:08 | -12 | 0.6 | 52.06 |
| 12:41:09 | -12 | 0.6 | 52.07 |
| 12:41:10 | -12 | 0.6 | 52.08 |
| 12:41:11 | -12 | 0.6 | 52.09 |
| 12:41:12 | -12 | 0.6 | 52.10 |
| 12:41:13 | -12 | 0.6 | 52.11 |
| 12:41:14 | -12 | 0.6 | 52.12 |
| 12:41:15 | -13 | 0.6 | 52.13 |
| 12:41:16 | -12 | 0.6 | 52.14 |
| 12:41:17 | -12 | 0.6 | 52.15 |
| 12:41:18 | -12 | 0.6 | 52.15 |
| 12:41:19 | -12 | 0.6 | 52.16 |
| 12:41:20 | -12 | 0.6 | 52.17 |
| 12:41:21 | -12 | 0.6 | 52.18 |
| 12:41:22 | -12 | 0.6 | 52.19 |
| 12:41:23 | -12 | 0.6 | 52.20 |
| 12:41:24 | -12 | 0.6 | 52.21 |
| 12:41:25 | -12 | 0.6 | 52.22 |
| 12:41:26 | -12 | 0.6 | 52.23 |
| 12:41:27 | -12 | 0.6 | 52.24 |
| 12:41:28 | -12 | 0.6 | 52.25 |
| 12:41:29 | -12 | 0.6 | 52.26 |
| 12:41:30 | -13 | 0.6 | 52.27 |
| 12:41:31 | -13 | 0.6 | 52.28 |
| 12:41:32 | -13 | 0.6 | 52.29 |
| 12:41:33 | -13 | 0.6 | 52.30 |
| 12:41:34 | -13 | 0.6 | 52.31 |
| 12:41:35 | -13 | 0.6 | 52.31 |
| 12:41:36 | -13 | 0.6 | 52.32 |
| 12:41:37 | -13 | 0.6 | 52.33 |
| 12:41:38 | -13 | 0.6 | 52.34 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:41:39 | -13 | 0.6 | 52.35 |
| 12:41:40 | -13 | 0.6 | 52.36 |
| 12:41:41 | -13 | 0.6 | 52.37 |
| 12:41:42 | -13 | 0.6 | 52.38 |
| 12:41:43 | -13 | 0.6 | 52.39 |
| 12:41:44 | -13 | 0.6 | 52.40 |
| 12:41:45 | -13 | 0.6 | 52.41 |
| 12:41:46 | -13 | 0.6 | 52.42 |
| 12:41:47 | -13 | 0.6 | 52.43 |
| 12:41:48 | -13 | 0.6 | 52.44 |
| 12:41:49 | -13 | 0.6 | 52.45 |
| 12:41:50 | -13 | 0.6 | 52.46 |
| 12:41:51 | -13 | 0.6 | 52.46 |
| 12:41:52 | -13 | 0.6 | 52.47 |
| 12:41:53 | -12 | 0.6 | 52.48 |
| 12:41:54 | -12 | 0.6 | 52.49 |
| 12:41:55 | -12 | 0.6 | 52.50 |
| 12:41:56 | -12 | 0.6 | 52.51 |
| 12:41:57 | -12 | 0.6 | 52.52 |
| 12:41:58 | -12 | 0.6 | 52.53 |
| 12:41:59 | -12 | 0.6 | 52.54 |
| 12:42:00 | -12 | 0.6 | 52.55 |
| 12:42:01 | -12 | 0.6 | 52.56 |
| 12:42:02 | -12 | 0.6 | 52.57 |
| 12:42:03 | -12 | 0.6 | 52.58 |
| 12:42:04 | -12 | 0.6 | 52.59 |
| 12:42:05 | -12 | 0.6 | 52.60 |
| 12:42:06 | -12 | 0.6 | 52.61 |
| 12:42:07 | -12 | 0.6 | 52.62 |
| 12:42:08 | -12 | 0.6 | 52.62 |
| 12:42:09 | -13 | 0.6 | 52.63 |
| 12:42:10 | -13 | 0.6 | 52.64 |
| 12:42:11 | -13 | 0.6 | 52.65 |
| 12:42:12 | -13 | 0.6 | 52.66 |
| 12:42:13 | -13 | 0.6 | 52.67 |
| 12:42:14 | -13 | 0.6 | 52.68 |
| 12:42:15 | -13 | 0.6 | 52.69 |
| 12:42:16 | -13 | 0.6 | 52.70 |
| 12:42:17 | -13 | 0.6 | 52.71 |
| 12:42:18 | -13 | 0.6 | 52.72 |
| 12:42:19 | -13 | 0.6 | 52.73 |
| 12:42:20 | -13 | 0.6 | 52.74 |
| 12:42:21 | -13 | 0.6 | 52.75 |
| 12:42:22 | -13 | 0.6 | 52.76 |
| 12:42:23 | -13 | 0.6 | 52.77 |
| 12:42:24 | -13 | 0.6 | 52.77 |
| 12:42:25 | -13 | 0.6 | 52.78 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:42:26 | -13 | 0.6 | 52.79 |
| 12:42:27 | -13 | 0.6 | 52.80 |
| 12:42:28 | -13 | 0.6 | 52.81 |
| 12:42:29 | -13 | 0.6 | 52.82 |
| 12:42:30 | -13 | 0.6 | 52.83 |
| 12:42:31 | -13 | 0.6 | 52.84 |
| 12:42:32 | -13 | 0.6 | 52.85 |
| 12:42:33 | -13 | 0.6 | 52.86 |
| 12:42:34 | -13 | 0.6 | 52.87 |
| 12:42:35 | -13 | 0.6 | 52.88 |
| 12:42:36 | -13 | 0.6 | 52.89 |
| 12:42:37 | -13 | 0.6 | 52.90 |
| 12:42:38 | -13 | 0.6 | 52.91 |
| 12:42:39 | -13 | 0.6 | 52.92 |
| 12:42:40 | -13 | 0.6 | 52.92 |
| 12:42:41 | -13 | 0.6 | 52.93 |
| 12:42:42 | -13 | 0.6 | 52.94 |
| 12:42:43 | -13 | 0.6 | 52.95 |
| 12:42:44 | -13 | 0.6 | 52.96 |
| 12:42:45 | -13 | 0.6 | 52.97 |
| 12:42:46 | -13 | 0.6 | 52.98 |
| 12:42:47 | -13 | 0.6 | 52.99 |
| 12:42:48 | -13 | 0.6 | 53.00 |
| 12:42:49 | -13 | 0.6 | 53.01 |
| 12:42:50 | -13 | 0.6 | 53.02 |
| 12:42:51 | -13 | 0.6 | 53.03 |
| 12:42:52 | -13 | 0.6 | 53.04 |
| 12:42:53 | -13 | 0.6 | 53.05 |
| 12:42:54 | -13 | 0.6 | 53.06 |
| 12:42:55 | -13 | 0.6 | 53.07 |
| 12:42:56 | -13 | 0.6 | 53.08 |
| 12:42:57 | -13 | 0.6 | 53.08 |
| 12:42:58 | -13 | 0.6 | 53.09 |
| 12:42:59 | -13 | 0.6 | 53.10 |
| 12:43:00 | -13 | 0.6 | 53.11 |
| 12:43:01 | -13 | 0.6 | 53.12 |
| 12:43:02 | -13 | 0.6 | 53.13 |
| 12:43:03 | -13 | 0.6 | 53.14 |
| 12:43:04 | -13 | 0.6 | 53.15 |
| 12:43:05 | -13 | 0.6 | 53.16 |
| 12:43:06 | -13 | 0.6 | 53.17 |
| 12:43:07 | -13 | 0.6 | 53.18 |
| 12:43:08 | -13 | 0.6 | 53.19 |
| 12:43:09 | -13 | 0.6 | 53.20 |
| 12:43:10 | -13 | 0.6 | 53.21 |
| 12:43:11 | -13 | 0.6 | 53.22 |
| 12:43:12 | -13 | 0.6 | 53.23 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:43:13 | -13 | 0.6 | 53.23 |
| 12:43:14 | -13 | 0.6 | 53.24 |
| 12:43:15 | -13 | 0.6 | 53.25 |
| 12:43:16 | -13 | 0.6 | 53.26 |
| 12:43:17 | -13 | 0.6 | 53.27 |
| 12:43:18 | -13 | 0.6 | 53.28 |
| 12:43:19 | -13 | 0.6 | 53.29 |
| 12:43:20 | -13 | 0.6 | 53.30 |
| 12:43:21 | -13 | 0.6 | 53.31 |
| 12:43:22 | -13 | 0.6 | 53.32 |
| 12:43:23 | -13 | 0.6 | 53.33 |
| 12:43:24 | -13 | 0.6 | 53.34 |
| 12:43:25 | -13 | 0.6 | 53.35 |
| 12:43:26 | -13 | 0.6 | 53.36 |
| 12:43:27 | -13 | 0.6 | 53.37 |
| 12:43:28 | -13 | 0.6 | 53.38 |
| 12:43:29 | -13 | 0.6 | 53.38 |
| 12:43:30 | -13 | 0.6 | 53.39 |
| 12:43:31 | -13 | 0.6 | 53.40 |
| 12:43:32 | -13 | 0.6 | 53.41 |
| 12:43:33 | -13 | 0.6 | 53.42 |
| 12:43:34 | -13 | 0.6 | 53.43 |
| 12:43:35 | -13 | 0.6 | 53.44 |
| 12:43:36 | -13 | 0.6 | 53.45 |
| 12:43:37 | -13 | 0.6 | 53.46 |
| 12:43:38 | -13 | 0.6 | 53.47 |
| 12:43:39 | -13 | 0.6 | 53.48 |
| 12:43:40 | -13 | 0.6 | 53.49 |
| 12:43:41 | -12 | 0.6 | 53.50 |
| 12:43:42 | -12 | 0.6 | 53.51 |
| 12:43:43 | -12 | 0.6 | 53.52 |
| 12:43:44 | -12 | 0.6 | 53.53 |
| 12:43:45 | -12 | 0.6 | 53.54 |
| 12:43:46 | -12 | 0.6 | 53.54 |
| 12:43:47 | -12 | 0.6 | 53.55 |
| 12:43:48 | -12 | 0.6 | 53.56 |
| 12:43:49 | -12 | 0.6 | 53.57 |
| 12:43:50 | -12 | 0.6 | 53.58 |
| 12:43:51 | -12 | 0.6 | 53.59 |
| 12:43:52 | -12 | 0.6 | 53.60 |
| 12:43:53 | -12 | 0.6 | 53.61 |
| 12:43:54 | -12 | 0.6 | 53.62 |
| 12:43:55 | -12 | 0.6 | 53.63 |
| 12:43:56 | -12 | 0.6 | 53.64 |
| 12:43:57 | -12 | 0.6 | 53.65 |
| 12:43:58 | -12 | 0.6 | 53.66 |
| 12:43:59 | -12 | 0.6 | 53.67 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:44:00 | -12 | 0.6 | 53.68 |
| 12:44:01 | -12 | 0.6 | 53.69 |
| 12:44:02 | -12 | 0.6 | 53.69 |
| 12:44:03 | -12 | 0.6 | 53.70 |
| 12:44:04 | -12 | 0.6 | 53.71 |
| 12:44:05 | -12 | 0.6 | 53.72 |
| 12:44:06 | -12 | 0.6 | 53.73 |
| 12:44:07 | -13 | 0.6 | 53.74 |
| 12:44:08 | -13 | 0.6 | 53.75 |
| 12:44:09 | -13 | 0.6 | 53.76 |
| 12:44:10 | -13 | 0.6 | 53.77 |
| 12:44:11 | -13 | 0.6 | 53.78 |
| 12:44:12 | -13 | 0.6 | 53.79 |
| 12:44:13 | -13 | 0.6 | 53.80 |
| 12:44:14 | -13 | 0.6 | 53.81 |
| 12:44:15 | -13 | 0.6 | 53.82 |
| 12:44:16 | -13 | 0.6 | 53.83 |
| 12:44:17 | -13 | 0.6 | 53.84 |
| 12:44:18 | -13 | 0.6 | 53.84 |
| 12:44:19 | -13 | 0.6 | 53.85 |
| 12:44:20 | -13 | 0.6 | 53.86 |
| 12:44:21 | -13 | 0.6 | 53.87 |
| 12:44:22 | -13 | 0.6 | 53.88 |
| 12:44:23 | -13 | 0.6 | 53.89 |
| 12:44:24 | -13 | 0.6 | 53.90 |
| 12:44:25 | -13 | 0.6 | 53.91 |
| 12:44:26 | -13 | 0.6 | 53.92 |
| 12:44:27 | -13 | 0.6 | 53.93 |
| 12:44:28 | -13 | 0.6 | 53.94 |
| 12:44:29 | -13 | 0.6 | 53.95 |
| 12:44:30 | -12 | 0.6 | 53.96 |
| 12:44:31 | -12 | 0.6 | 53.97 |
| 12:44:32 | -12 | 0.6 | 53.98 |
| 12:44:33 | -12 | 0.6 | 53.99 |
| 12:44:34 | -12 | 0.6 | 54.00 |
| 12:44:35 | -12 | 0.6 | 54.00 |
| 12:44:36 | -12 | 0.6 | 54.01 |
| 12:44:37 | -12 | 0.6 | 54.02 |
| 12:44:38 | -12 | 0.6 | 54.03 |
| 12:44:39 | -12 | 0.6 | 54.04 |
| 12:44:40 | -12 | 0.6 | 54.05 |
| 12:44:41 | -12 | 0.6 | 54.06 |
| 12:44:42 | -12 | 0.6 | 54.07 |
| 12:44:43 | -12 | 0.6 | 54.08 |
| 12:44:44 | -11 | 0.6 | 54.09 |
| 12:44:45 | -11 | 0.6 | 54.10 |
| 12:44:46 | -12 | 0.6 | 54.11 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:44:47 | -12 | 0.6 | 54.12 |
| 12:44:48 | -12 | 0.6 | 54.13 |
| 12:44:49 | -12 | 0.6 | 54.14 |
| 12:44:50 | -12 | 0.6 | 54.15 |
| 12:44:51 | -12 | 0.6 | 54.15 |
| 12:44:52 | -12 | 0.6 | 54.16 |
| 12:44:53 | -12 | 0.6 | 54.17 |
| 12:44:54 | -12 | 0.6 | 54.18 |
| 12:44:55 | -12 | 0.6 | 54.19 |
| 12:44:56 | -13 | 0.6 | 54.20 |
| 12:44:57 | -13 | 0.6 | 54.21 |
| 12:44:58 | -13 | 0.6 | 54.22 |
| 12:44:59 | -13 | 0.6 | 54.23 |
| 12:45:00 | -13 | 0.6 | 54.24 |
| 12:45:01 | -13 | 0.6 | 54.25 |
| 12:45:02 | -13 | 0.6 | 54.26 |
| 12:45:03 | -13 | 0.6 | 54.27 |
| 12:45:04 | -13 | 0.6 | 54.28 |
| 12:45:05 | -13 | 0.6 | 54.29 |
| 12:45:06 | -13 | 0.6 | 54.30 |
| 12:45:07 | -13 | 0.6 | 54.30 |
| 12:45:08 | -13 | 0.6 | 54.31 |
| 12:45:09 | -13 | 0.6 | 54.32 |
| 12:45:10 | -13 | 0.6 | 54.33 |
| 12:45:11 | -13 | 0.6 | 54.34 |
| 12:45:12 | -13 | 0.6 | 54.35 |
| 12:45:13 | -13 | 0.6 | 54.36 |
| 12:45:14 | -13 | 0.6 | 54.37 |
| 12:45:15 | -13 | 0.6 | 54.38 |
| 12:45:16 | -13 | 0.6 | 54.39 |
| 12:45:17 | -13 | 0.6 | 54.40 |
| 12:45:18 | -13 | 0.6 | 54.41 |
| 12:45:19 | -13 | 0.6 | 54.42 |
| 12:45:20 | -13 | 0.6 | 54.43 |
| 12:45:21 | -13 | 0.6 | 54.44 |
| 12:45:22 | -13 | 0.6 | 54.45 |
| 12:45:23 | -13 | 0.6 | 54.46 |
| 12:45:24 | -13 | 0.6 | 54.46 |
| 12:45:25 | -13 | 0.6 | 54.47 |
| 12:45:26 | -12 | 0.6 | 54.48 |
| 12:45:27 | -12 | 0.6 | 54.49 |
| 12:45:28 | -12 | 0.6 | 54.50 |
| 12:45:29 | -12 | 0.6 | 54.51 |
| 12:45:30 | -12 | 0.6 | 54.52 |
| 12:45:31 | -12 | 0.6 | 54.53 |
| 12:45:32 | -12 | 0.6 | 54.54 |
| 12:45:33 | -12 | 0.6 | 54.55 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:45:34 | -12 | 0.6 | 54.56 |
| 12:45:35 | -12 | 0.6 | 54.57 |
| 12:45:36 | -12 | 0.6 | 54.58 |
| 12:45:37 | -12 | 0.6 | 54.59 |
| 12:45:38 | -12 | 0.6 | 54.60 |
| 12:45:39 | -12 | 0.6 | 54.61 |
| 12:45:40 | -11 | 0.6 | 54.61 |
| 12:45:41 | -11 | 0.6 | 54.62 |
| 12:45:42 | -11 | 0.6 | 54.63 |
| 12:45:43 | -11 | 0.6 | 54.64 |
| 12:45:44 | -11 | 0.6 | 54.65 |
| 12:45:45 | -11 | 0.6 | 54.66 |
| 12:45:46 | -11 | 0.6 | 54.67 |
| 12:45:47 | -11 | 0.6 | 54.68 |
| 12:45:48 | -11 | 0.6 | 54.69 |
| 12:45:49 | -11 | 0.6 | 54.70 |
| 12:45:50 | -11 | 0.6 | 54.71 |
| 12:45:51 | -11 | 0.6 | 54.72 |
| 12:45:52 | -11 | 0.6 | 54.73 |
| 12:45:53 | -11 | 0.6 | 54.74 |
| 12:45:54 | -11 | 0.6 | 54.75 |
| 12:45:55 | -11 | 0.6 | 54.76 |
| 12:45:56 | -11 | 0.6 | 54.76 |
| 12:45:57 | -11 | 0.6 | 54.77 |
| 12:45:58 | -11 | 0.6 | 54.78 |
| 12:45:59 | -11 | 0.6 | 54.79 |
| 12:46:00 | -11 | 0.6 | 54.80 |
| 12:46:01 | -12 | 0.6 | 54.81 |
| 12:46:02 | -12 | 0.6 | 54.82 |
| 12:46:03 | -12 | 0.6 | 54.83 |
| 12:46:04 | -12 | 0.7 | 54.84 |
| 12:46:05 | -12 | 0.7 | 54.85 |
| 12:46:06 | -12 | 0.7 | 54.87 |
| 12:46:07 | -12 | 0.7 | 54.88 |
| 12:46:08 | -12 | 0.6 | 54.89 |
| 12:46:09 | -12 | 0.6 | 54.90 |
| 12:46:10 | -13 | 0.6 | 54.91 |
| 12:46:11 | -13 | 0.6 | 54.92 |
| 12:46:12 | -13 | 0.6 | 54.93 |
| 12:46:13 | -13 | 0.6 | 54.94 |
| 12:46:14 | -14 | 0.6 | 54.95 |
| 12:46:15 | -14 | 0.6 | 54.96 |
| 12:46:16 | -14 | 0.6 | 54.97 |
| 12:46:17 | -15 | 0.6 | 54.98 |
| 12:46:18 | -15 | 0.6 | 54.99 |
| 12:46:19 | -15 | 0.6 | 55.00 |
| 12:46:20 | -16 | 0.6 | 55.01 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:46:21 | -16 | 0.6 | 55.02 |
| 12:46:22 | -17 | 0.6 | 55.03 |
| 12:46:23 | -17 | 0.6 | 55.04 |
| 12:46:24 | -18 | 0.6 | 55.05 |
| 12:46:25 | -18 | 0.6 | 55.06 |
| 12:46:26 | -19 | 0.6 | 55.08 |
| 12:46:27 | -19 | 0.7 | 55.09 |
| 12:46:28 | -19 | 0.7 | 55.10 |
| 12:46:29 | -19 | 0.8 | 55.11 |
| 12:46:30 | -19 | 0.8 | 55.13 |
| 12:46:31 | -20 | 0.8 | 55.14 |
| 12:46:32 | -20 | 0.8 | 55.15 |
| 12:46:33 | -20 | 0.8 | 55.17 |
| 12:46:34 | -20 | 0.8 | 55.18 |
| 12:46:35 | -20 | 0.8 | 55.19 |
| 12:46:36 | -20 | 0.9 | 55.21 |
| 12:46:37 | -20 | 1.0 | 55.22 |
| 12:46:38 | -20 | 1.0 | 55.24 |
| 12:46:39 | -20 | 1.1 | 55.26 |
| 12:46:40 | -20 | 1.1 | 55.28 |
| 12:46:41 | -20 | 1.2 | 55.30 |
| 12:46:42 | -20 | 1.2 | 55.32 |
| 12:46:43 | -20 | 1.3 | 55.34 |
| 12:46:44 | -20 | 1.3 | 55.36 |
| 12:46:45 | -20 | 1.4 | 55.39 |
| 12:46:46 | -21 | 1.4 | 55.41 |
| 12:46:47 | -21 | 1.4 | 55.44 |
| 12:46:48 | -21 | 1.4 | 55.46 |
| 12:46:49 | -21 | 1.4 | 55.48 |
| 12:46:50 | -21 | 1.3 | 55.50 |
| 12:46:51 | -22 | 1.3 | 55.52 |
| 12:46:52 | -22 | 1.2 | 55.54 |
| 12:46:53 | -22 | 1.2 | 55.56 |
| 12:46:54 | -22 | 1.2 | 55.58 |
| 12:46:55 | -22 | 1.2 | 55.60 |
| 12:46:56 | -22 | 1.1 | 55.62 |
| 12:46:57 | -22 | 1.1 | 55.64 |
| 12:46:58 | -22 | 1.1 | 55.66 |
| 12:46:59 | -21 | 1.1 | 55.68 |
| 12:47:00 | -21 | 1.1 | 55.69 |
| 12:47:01 | -21 | 1.1 | 55.71 |
| 12:47:02 | -21 | 1.0 | 55.73 |
| 12:47:03 | -21 | 1.0 | 55.75 |
| 12:47:04 | -21 | 1.0 | 55.76 |
| 12:47:05 | -21 | 1.0 | 55.78 |
| 12:47:06 | -21 | 1.0 | 55.80 |
| 12:47:07 | -21 | 1.0 | 55.82 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:47:08 | -21 | 1.0 | 55.83 |
| 12:47:09 | -21 | 1.0 | 55.85 |
| 12:47:10 | -20 | 1.0 | 55.87 |
| 12:47:11 | -20 | 1.0 | 55.88 |
| 12:47:12 | -20 | 1.0 | 55.90 |
| 12:47:13 | -20 | 1.0 | 55.92 |
| 12:47:14 | -20 | 1.0 | 55.94 |
| 12:47:15 | -20 | 1.0 | 55.95 |
| 12:47:16 | -20 | 1.0 | 55.97 |
| 12:47:17 | -19 | 1.0 | 55.99 |
| 12:47:18 | -19 | 1.0 | 56.00 |
| 12:47:19 | -19 | 1.0 | 56.02 |
| 12:47:20 | -19 | 1.0 | 56.04 |
| 12:47:21 | -19 | 1.0 | 56.05 |
| 12:47:22 | -19 | 1.0 | 56.07 |
| 12:47:23 | -19 | 1.0 | 56.09 |
| 12:47:24 | -19 | 1.0 | 56.11 |
| 12:47:25 | -19 | 1.0 | 56.12 |
| 12:47:26 | -19 | 1.0 | 56.14 |
| 12:47:27 | -19 | 1.0 | 56.16 |
| 12:47:28 | -19 | 1.0 | 56.17 |
| 12:47:29 | -19 | 1.0 | 56.19 |
| 12:47:30 | -19 | 1.0 | 56.21 |
| 12:47:31 | -19 | 1.0 | 56.22 |
| 12:47:32 | -19 | 1.0 | 56.24 |
| 12:47:33 | -19 | 1.0 | 56.26 |
| 12:47:34 | -19 | 1.0 | 56.28 |
| 12:47:35 | -19 | 1.0 | 56.29 |
| 12:47:36 | -19 | 1.0 | 56.31 |
| 12:47:37 | -19 | 1.0 | 56.33 |
| 12:47:38 | -19 | 1.0 | 56.34 |
| 12:47:39 | -19 | 1.0 | 56.36 |
| 12:47:40 | -19 | 1.0 | 56.38 |
| 12:47:41 | -19 | 1.0 | 56.40 |
| 12:47:42 | -19 | 1.0 | 56.41 |
| 12:47:43 | -19 | 1.0 | 56.43 |
| 12:47:44 | -19 | 1.0 | 56.45 |
| 12:47:45 | -19 | 1.0 | 56.46 |
| 12:47:46 | -19 | 1.0 | 56.48 |
| 12:47:47 | -18 | 1.0 | 56.50 |
| 12:47:48 | -18 | 1.0 | 56.52 |
| 12:47:49 | -18 | 1.0 | 56.53 |
| 12:47:50 | -18 | 1.0 | 56.55 |
| 12:47:51 | -18 | 1.0 | 56.57 |
| 12:47:52 | -18 | 1.0 | 56.58 |
| 12:47:53 | -18 | 1.0 | 56.60 |
| 12:47:54 | -19 | 1.0 | 56.62 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:47:55 | -19 | 1.0 | 56.63 |
| 12:47:56 | -18 | 1.0 | 56.65 |
| 12:47:57 | -18 | 1.0 | 56.67 |
| 12:47:58 | -18 | 1.0 | 56.69 |
| 12:47:59 | -18 | 1.0 | 56.70 |
| 12:48:00 | -18 | 1.0 | 56.72 |
| 12:48:01 | -18 | 1.0 | 56.74 |
| 12:48:02 | -18 | 1.0 | 56.75 |
| 12:48:03 | -18 | 1.0 | 56.77 |
| 12:48:04 | -18 | 1.0 | 56.79 |
| 12:48:05 | -18 | 1.0 | 56.80 |
| 12:48:06 | -18 | 1.0 | 56.82 |
| 12:48:07 | -18 | 1.0 | 56.84 |
| 12:48:08 | -18 | 1.0 | 56.86 |
| 12:48:09 | -18 | 1.0 | 56.87 |
| 12:48:10 | -18 | 1.0 | 56.89 |
| 12:48:11 | -18 | 1.0 | 56.91 |
| 12:48:12 | -18 | 1.0 | 56.92 |
| 12:48:13 | -18 | 1.0 | 56.94 |
| 12:48:14 | -18 | 1.0 | 56.96 |
| 12:48:15 | -18 | 1.0 | 56.98 |
| 12:48:16 | -18 | 1.0 | 56.99 |
| 12:48:17 | -18 | 1.0 | 57.01 |
| 12:48:18 | -18 | 1.0 | 57.03 |
| 12:48:19 | -18 | 1.0 | 57.04 |
| 12:48:20 | -18 | 1.0 | 57.06 |
| 12:48:21 | -18 | 1.0 | 57.08 |
| 12:48:22 | -18 | 1.0 | 57.09 |
| 12:48:23 | -18 | 1.0 | 57.11 |
| 12:48:24 | -18 | 1.0 | 57.13 |
| 12:48:25 | -18 | 1.0 | 57.15 |
| 12:48:26 | -18 | 1.0 | 57.16 |
| 12:48:27 | -18 | 1.0 | 57.18 |
| 12:48:28 | -18 | 1.0 | 57.20 |
| 12:48:29 | -18 | 1.0 | 57.21 |
| 12:48:30 | -18 | 1.0 | 57.23 |
| 12:48:31 | -18 | 1.0 | 57.25 |
| 12:48:32 | -18 | 1.0 | 57.27 |
| 12:48:33 | -18 | 1.0 | 57.28 |
| 12:48:34 | -18 | 1.0 | 57.30 |
| 12:48:35 | -18 | 1.0 | 57.32 |
| 12:48:36 | -18 | 1.0 | 57.33 |
| 12:48:37 | -18 | 1.0 | 57.35 |
| 12:48:38 | -18 | 1.0 | 57.37 |
| 12:48:39 | -18 | 1.0 | 57.38 |
| 12:48:40 | -18 | 1.0 | 57.40 |
| 12:48:41 | -18 | 1.0 | 57.42 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:48:42 | -18 | 1.0 | 57.44 |
| 12:48:43 | -18 | 1.0 | 57.45 |
| 12:48:44 | -18 | 1.0 | 57.47 |
| 12:48:45 | -18 | 1.0 | 57.49 |
| 12:48:46 | -18 | 1.0 | 57.50 |
| 12:48:47 | -18 | 1.0 | 57.52 |
| 12:48:48 | -18 | 1.0 | 57.54 |
| 12:48:49 | -18 | 1.0 | 57.56 |
| 12:48:50 | -18 | 1.0 | 57.57 |
| 12:48:51 | -17 | 1.0 | 57.59 |
| 12:48:52 | -17 | 1.0 | 57.61 |
| 12:48:53 | -17 | 1.0 | 57.62 |
| 12:48:54 | -17 | 1.0 | 57.64 |
| 12:48:55 | -17 | 1.0 | 57.66 |
| 12:48:56 | -17 | 1.0 | 57.68 |
| 12:48:57 | -17 | 1.0 | 57.69 |
| 12:48:58 | -17 | 1.0 | 57.71 |
| 12:48:59 | -17 | 1.0 | 57.73 |
| 12:49:00 | -17 | 1.0 | 57.74 |
| 12:49:01 | -17 | 1.0 | 57.76 |
| 12:49:02 | -17 | 1.0 | 57.78 |
| 12:49:03 | -17 | 1.0 | 57.79 |
| 12:49:04 | -17 | 1.0 | 57.81 |
| 12:49:05 | -17 | 1.0 | 57.83 |
| 12:49:06 | -17 | 1.0 | 57.85 |
| 12:49:07 | -17 | 1.0 | 57.86 |
| 12:49:08 | -17 | 1.0 | 57.88 |
| 12:49:09 | -17 | 1.0 | 57.90 |
| 12:49:10 | -17 | 1.0 | 57.91 |
| 12:49:11 | -17 | 1.0 | 57.93 |
| 12:49:12 | -17 | 1.0 | 57.95 |
| 12:49:13 | -17 | 1.0 | 57.97 |
| 12:49:14 | -17 | 1.0 | 57.98 |
| 12:49:15 | -17 | 1.0 | 58.00 |
| 12:49:16 | -17 | 1.0 | 58.02 |
| 12:49:17 | -17 | 1.0 | 58.03 |
| 12:49:18 | -17 | 1.0 | 58.05 |
| 12:49:19 | -17 | 1.0 | 58.07 |
| 12:49:20 | -17 | 1.0 | 58.09 |
| 12:49:21 | -17 | 1.0 | 58.10 |
| 12:49:22 | -17 | 1.0 | 58.12 |
| 12:49:23 | -17 | 1.0 | 58.14 |
| 12:49:24 | -17 | 1.0 | 58.15 |
| 12:49:25 | -17 | 1.0 | 58.17 |
| 12:49:26 | -17 | 1.0 | 58.19 |
| 12:49:27 | -17 | 1.0 | 58.21 |
| 12:49:28 | -17 | 1.0 | 58.22 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:49:29 | -17 | 1.0 | 58.24 |
| 12:49:30 | -17 | 1.0 | 58.26 |
| 12:49:31 | -17 | 1.0 | 58.27 |
| 12:49:32 | -17 | 1.0 | 58.29 |
| 12:49:33 | -17 | 1.0 | 58.31 |
| 12:49:34 | -17 | 1.0 | 58.33 |
| 12:49:35 | -17 | 1.0 | 58.34 |
| 12:49:36 | -17 | 1.0 | 58.36 |
| 12:49:37 | -17 | 1.0 | 58.38 |
| 12:49:38 | -17 | 1.0 | 58.39 |
| 12:49:39 | -17 | 1.0 | 58.41 |
| 12:49:40 | -17 | 1.0 | 58.43 |
| 12:49:41 | -17 | 1.0 | 58.45 |
| 12:49:42 | -17 | 1.0 | 58.46 |
| 12:49:43 | -17 | 1.0 | 58.48 |
| 12:49:44 | -17 | 1.0 | 58.50 |
| 12:49:45 | -17 | 1.0 | 58.51 |
| 12:49:46 | -17 | 1.0 | 58.53 |
| 12:49:47 | -17 | 1.0 | 58.55 |
| 12:49:48 | -17 | 1.0 | 58.57 |
| 12:49:49 | -17 | 1.0 | 58.58 |
| 12:49:50 | -17 | 1.0 | 58.60 |
| 12:49:51 | -17 | 1.0 | 58.62 |
| 12:49:52 | -17 | 1.0 | 58.63 |
| 12:49:53 | -17 | 1.0 | 58.65 |
| 12:49:54 | -17 | 1.0 | 58.67 |
| 12:49:55 | -17 | 1.0 | 58.69 |
| 12:49:56 | -17 | 1.0 | 58.70 |
| 12:49:57 | -17 | 1.0 | 58.72 |
| 12:49:58 | -17 | 1.0 | 58.74 |
| 12:49:59 | -17 | 1.0 | 58.75 |
| 12:50:00 | -17 | 1.0 | 58.77 |
| 12:50:01 | -17 | 1.0 | 58.79 |
| 12:50:02 | -17 | 1.0 | 58.81 |
| 12:50:03 | -17 | 1.0 | 58.82 |
| 12:50:04 | -17 | 1.0 | 58.84 |
| 12:50:05 | -17 | 1.0 | 58.86 |
| 12:50:06 | -17 | 1.0 | 58.87 |
| 12:50:07 | -17 | 1.0 | 58.89 |
| 12:50:08 | -17 | 1.0 | 58.91 |
| 12:50:09 | -17 | 1.0 | 58.93 |
| 12:50:10 | -17 | 1.0 | 58.94 |
| 12:50:11 | -17 | 1.0 | 58.96 |
| 12:50:12 | -17 | 1.0 | 58.98 |
| 12:50:13 | -17 | 1.0 | 58.99 |
| 12:50:14 | -17 | 1.0 | 59.01 |
| 12:50:15 | -17 | 1.0 | 59.03 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:50:16 | -17 | 1.0 | 59.05 |
| 12:50:17 | -17 | 1.0 | 59.06 |
| 12:50:18 | -17 | 1.0 | 59.08 |
| 12:50:19 | -17 | 1.0 | 59.10 |
| 12:50:20 | -17 | 1.0 | 59.11 |
| 12:50:21 | -17 | 1.0 | 59.13 |
| 12:50:22 | -17 | 1.0 | 59.15 |
| 12:50:23 | -17 | 1.0 | 59.17 |
| 12:50:24 | -17 | 1.0 | 59.18 |
| 12:50:25 | -17 | 1.0 | 59.20 |
| 12:50:26 | -17 | 1.0 | 59.22 |
| 12:50:27 | -17 | 1.0 | 59.23 |
| 12:50:28 | -17 | 1.0 | 59.25 |
| 12:50:29 | -17 | 1.0 | 59.27 |
| 12:50:30 | -17 | 1.0 | 59.29 |
| 12:50:31 | -17 | 1.0 | 59.30 |
| 12:50:32 | -17 | 1.0 | 59.32 |
| 12:50:33 | -17 | 1.0 | 59.34 |
| 12:50:34 | -17 | 1.0 | 59.35 |
| 12:50:35 | -17 | 1.0 | 59.37 |
| 12:50:36 | -17 | 1.0 | 59.39 |
| 12:50:37 | -17 | 1.0 | 59.41 |
| 12:50:38 | -17 | 1.0 | 59.42 |
| 12:50:39 | -17 | 1.0 | 59.44 |
| 12:50:40 | -17 | 1.0 | 59.46 |
| 12:50:41 | -17 | 1.0 | 59.48 |
| 12:50:42 | -17 | 1.0 | 59.49 |
| 12:50:43 | -17 | 1.0 | 59.51 |
| 12:50:44 | -17 | 1.0 | 59.53 |
| 12:50:45 | -17 | 1.0 | 59.54 |
| 12:50:46 | -17 | 1.0 | 59.56 |
| 12:50:47 | -17 | 1.0 | 59.58 |
| 12:50:48 | -17 | 1.0 | 59.60 |
| 12:50:49 | -17 | 1.0 | 59.61 |
| 12:50:50 | -17 | 1.0 | 59.63 |
| 12:50:51 | -17 | 1.0 | 59.65 |
| 12:50:52 | -17 | 0.9 | 59.66 |
| 12:50:53 | -17 | 0.9 | 59.68 |
| 12:50:54 | -17 | 0.9 | 59.69 |
| 12:50:55 | -17 | 0.9 | 59.71 |
| 12:50:56 | -17 | 0.9 | 59.72 |
| 12:50:57 | -17 | 0.8 | 59.73 |
| 12:50:58 | -17 | 0.8 | 59.75 |
| 12:50:59 | -17 | 0.9 | 59.76 |
| 12:51:00 | -17 | 0.9 | 59.78 |
| 12:51:01 | -17 | 1.0 | 59.79 |
| 12:51:02 | -16 | 1.0 | 59.81 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:51:03 | -16 | 1.0 | 59.83 |
| 12:51:04 | -16 | 1.0 | 59.84 |
| 12:51:05 | -17 | 1.0 | 59.86 |
| 12:51:06 | -17 | 1.0 | 59.88 |
| 12:51:07 | -17 | 1.0 | 59.89 |
| 12:51:08 | -17 | 1.0 | 59.91 |
| 12:51:09 | -17 | 1.0 | 59.93 |
| 12:51:10 | -17 | 1.0 | 59.95 |
| 12:51:11 | -17 | 1.0 | 59.96 |
| 12:51:12 | -17 | 1.0 | 59.98 |
| 12:51:13 | -17 | 1.0 | 60.00 |
| 12:51:14 | -17 | 1.0 | 60.01 |
| 12:51:15 | -17 | 1.0 | 60.03 |
| 12:51:16 | -17 | 1.0 | 60.05 |
| 12:51:17 | -17 | 1.0 | 60.06 |
| 12:51:18 | -17 | 1.0 | 60.08 |
| 12:51:19 | -17 | 1.0 | 60.10 |
| 12:51:20 | -17 | 1.0 | 60.11 |
| 12:51:21 | -17 | 1.0 | 60.13 |
| 12:51:22 | -17 | 1.0 | 60.15 |
| 12:51:23 | -17 | 1.0 | 60.16 |
| 12:51:24 | -17 | 1.0 | 60.18 |
| 12:51:25 | -18 | 1.0 | 60.20 |
| 12:51:26 | -18 | 1.0 | 60.21 |
| 12:51:27 | -18 | 1.0 | 60.23 |
| 12:51:28 | -18 | 1.0 | 60.25 |
| 12:51:29 | -18 | 1.0 | 60.26 |
| 12:51:30 | -18 | 1.0 | 60.28 |
| 12:51:31 | -18 | 1.0 | 60.30 |
| 12:51:32 | -18 | 1.0 | 60.32 |
| 12:51:33 | -18 | 1.0 | 60.33 |
| 12:51:34 | -18 | 1.0 | 60.35 |
| 12:51:35 | -18 | 1.0 | 60.37 |
| 12:51:36 | -18 | 1.0 | 60.38 |
| 12:51:37 | -18 | 1.0 | 60.40 |
| 12:51:38 | -18 | 1.0 | 60.42 |
| 12:51:39 | -18 | 1.0 | 60.44 |
| 12:51:40 | -18 | 1.0 | 60.45 |
| 12:51:41 | -18 | 1.0 | 60.47 |
| 12:51:42 | -18 | 1.0 | 60.49 |
| 12:51:43 | -18 | 1.0 | 60.50 |
| 12:51:44 | -18 | 1.0 | 60.52 |
| 12:51:45 | -17 | 1.0 | 60.54 |
| 12:51:46 | -17 | 1.0 | 60.56 |
| 12:51:47 | -17 | 1.0 | 60.57 |
| 12:51:48 | -17 | 1.0 | 60.59 |
| 12:51:49 | -17 | 1.0 | 60.61 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:51:50 | -17 | 1.0 | 60.62 |
| 12:51:51 | -17 | 1.0 | 60.64 |
| 12:51:52 | -17 | 1.0 | 60.66 |
| 12:51:53 | -17 | 1.0 | 60.68 |
| 12:51:54 | -17 | 1.0 | 60.69 |
| 12:51:55 | -17 | 1.0 | 60.71 |
| 12:51:56 | -17 | 1.0 | 60.73 |
| 12:51:57 | -17 | 1.0 | 60.74 |
| 12:51:58 | -17 | 1.0 | 60.76 |
| 12:51:59 | -17 | 1.0 | 60.78 |
| 12:52:00 | -17 | 1.0 | 60.80 |
| 12:52:01 | -17 | 1.0 | 60.81 |
| 12:52:02 | -17 | 1.0 | 60.83 |
| 12:52:03 | -17 | 1.0 | 60.85 |
| 12:52:04 | -17 | 1.0 | 60.86 |
| 12:52:05 | -17 | 1.0 | 60.88 |
| 12:52:06 | -17 | 1.0 | 60.90 |
| 12:52:07 | -17 | 1.0 | 60.92 |
| 12:52:08 | -17 | 1.0 | 60.93 |
| 12:52:09 | -17 | 1.0 | 60.95 |
| 12:52:10 | -17 | 1.0 | 60.97 |
| 12:52:11 | -17 | 1.0 | 60.98 |
| 12:52:12 | -17 | 1.0 | 61.00 |
| 12:52:13 | -17 | 1.0 | 61.02 |
| 12:52:14 | -17 | 1.0 | 61.04 |
| 12:52:15 | -17 | 1.0 | 61.05 |
| 12:52:16 | -17 | 1.0 | 61.07 |
| 12:52:17 | -17 | 1.0 | 61.09 |
| 12:52:18 | -16 | 1.0 | 61.10 |
| 12:52:19 | -16 | 1.0 | 61.12 |
| 12:52:20 | -16 | 1.0 | 61.14 |
| 12:52:21 | -16 | 1.0 | 61.16 |
| 12:52:22 | -16 | 1.0 | 61.17 |
| 12:52:23 | -16 | 1.0 | 61.19 |
| 12:52:24 | -16 | 1.0 | 61.21 |
| 12:52:25 | -16 | 1.0 | 61.22 |
| 12:52:26 | -16 | 1.0 | 61.24 |
| 12:52:27 | -16 | 1.0 | 61.26 |
| 12:52:28 | -16 | 1.0 | 61.28 |
| 12:52:29 | -16 | 1.0 | 61.29 |
| 12:52:30 | -16 | 1.0 | 61.31 |
| 12:52:31 | -16 | 1.0 | 61.33 |
| 12:52:32 | -16 | 1.0 | 61.34 |
| 12:52:33 | -16 | 1.0 | 61.36 |
| 12:52:34 | -16 | 1.0 | 61.38 |
| 12:52:35 | -16 | 1.0 | 61.40 |
| 12:52:36 | -16 | 1.0 | 61.41 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:52:37 | -16 | 1.0 | 61.43 |
| 12:52:38 | -16 | 1.0 | 61.45 |
| 12:52:39 | -16 | 1.0 | 61.46 |
| 12:52:40 | -17 | 1.0 | 61.48 |
| 12:52:41 | -17 | 1.0 | 61.50 |
| 12:52:42 | -17 | 1.0 | 61.52 |
| 12:52:43 | -17 | 1.0 | 61.53 |
| 12:52:44 | -17 | 1.0 | 61.55 |
| 12:52:45 | -17 | 1.0 | 61.57 |
| 12:52:46 | -17 | 1.0 | 61.58 |
| 12:52:47 | -17 | 1.0 | 61.60 |
| 12:52:48 | -17 | 1.0 | 61.62 |
| 12:52:49 | -17 | 1.0 | 61.64 |
| 12:52:50 | -17 | 1.0 | 61.65 |
| 12:52:51 | -17 | 1.0 | 61.67 |
| 12:52:52 | -17 | 1.0 | 61.69 |
| 12:52:53 | -17 | 1.0 | 61.70 |
| 12:52:54 | -17 | 1.0 | 61.72 |
| 12:52:55 | -17 | 1.0 | 61.74 |
| 12:52:56 | -17 | 1.0 | 61.76 |
| 12:52:57 | -17 | 1.0 | 61.77 |
| 12:52:58 | -17 | 1.0 | 61.79 |
| 12:52:59 | -17 | 1.0 | 61.81 |
| 12:53:00 | -16 | 1.0 | 61.82 |
| 12:53:01 | -16 | 1.0 | 61.84 |
| 12:53:02 | -16 | 1.0 | 61.86 |
| 12:53:03 | -16 | 1.0 | 61.87 |
| 12:53:04 | -16 | 1.0 | 61.89 |
| 12:53:05 | -16 | 1.0 | 61.91 |
| 12:53:06 | -16 | 1.0 | 61.93 |
| 12:53:07 | -16 | 1.0 | 61.94 |
| 12:53:08 | -16 | 1.0 | 61.96 |
| 12:53:09 | -16 | 1.0 | 61.98 |
| 12:53:10 | -16 | 1.0 | 61.99 |
| 12:53:11 | -16 | 1.0 | 62.01 |
| 12:53:12 | -16 | 1.0 | 62.03 |
| 12:53:13 | -16 | 1.0 | 62.05 |
| 12:53:14 | -16 | 1.0 | 62.06 |
| 12:53:15 | -16 | 1.0 | 62.08 |
| 12:53:16 | -16 | 1.0 | 62.10 |
| 12:53:17 | -16 | 1.0 | 62.11 |
| 12:53:18 | -16 | 1.0 | 62.13 |
| 12:53:19 | -16 | 1.0 | 62.15 |
| 12:53:20 | -16 | 1.0 | 62.17 |
| 12:53:21 | -16 | 1.0 | 62.18 |
| 12:53:22 | -16 | 1.0 | 62.20 |
| 12:53:23 | -16 | 1.0 | 62.22 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:53:24 | -16 | 1.0 | 62.23 |
| 12:53:25 | -16 | 1.0 | 62.25 |
| 12:53:26 | -16 | 1.0 | 62.27 |
| 12:53:27 | -16 | 1.0 | 62.28 |
| 12:53:28 | -16 | 1.0 | 62.30 |
| 12:53:29 | -16 | 1.0 | 62.32 |
| 12:53:30 | -16 | 1.0 | 62.34 |
| 12:53:31 | -16 | 1.0 | 62.35 |
| 12:53:32 | -16 | 1.0 | 62.37 |
| 12:53:33 | -16 | 1.0 | 62.39 |
| 12:53:34 | -16 | 1.0 | 62.40 |
| 12:53:35 | -16 | 1.0 | 62.42 |
| 12:53:36 | -15 | 1.0 | 62.44 |
| 12:53:37 | -15 | 1.0 | 62.46 |
| 12:53:38 | -15 | 1.0 | 62.47 |
| 12:53:39 | -16 | 1.0 | 62.49 |
| 12:53:40 | -16 | 1.0 | 62.51 |
| 12:53:41 | -16 | 1.0 | 62.52 |
| 12:53:42 | -16 | 1.0 | 62.54 |
| 12:53:43 | -16 | 1.0 | 62.56 |
| 12:53:44 | -16 | 1.0 | 62.57 |
| 12:53:45 | -16 | 1.0 | 62.59 |
| 12:53:46 | -16 | 1.0 | 62.61 |
| 12:53:47 | -16 | 1.0 | 62.63 |
| 12:53:48 | -16 | 1.0 | 62.64 |
| 12:53:49 | -16 | 1.0 | 62.66 |
| 12:53:50 | -16 | 1.0 | 62.68 |
| 12:53:51 | -16 | 1.0 | 62.69 |
| 12:53:52 | -16 | 1.0 | 62.71 |
| 12:53:53 | -16 | 1.0 | 62.73 |
| 12:53:54 | -16 | 1.0 | 62.75 |
| 12:53:55 | -16 | 1.0 | 62.76 |
| 12:53:56 | -16 | 1.0 | 62.78 |
| 12:53:57 | -16 | 1.0 | 62.80 |
| 12:53:58 | -16 | 1.0 | 62.81 |
| 12:53:59 | -16 | 1.0 | 62.83 |
| 12:54:00 | -16 | 1.0 | 62.85 |
| 12:54:01 | -16 | 1.0 | 62.86 |
| 12:54:02 | -16 | 1.0 | 62.88 |
| 12:54:03 | -16 | 1.0 | 62.90 |
| 12:54:04 | -16 | 1.0 | 62.92 |
| 12:54:05 | -16 | 1.0 | 62.93 |
| 12:54:06 | -16 | 1.0 | 62.95 |
| 12:54:07 | -16 | 1.0 | 62.97 |
| 12:54:08 | -16 | 1.0 | 62.98 |
| 12:54:09 | -16 | 1.0 | 63.00 |
| 12:54:10 | -16 | 1.0 | 63.02 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:54:11 | -16 | 1.0 | 63.03 |
| 12:54:12 | -16 | 1.0 | 63.05 |
| 12:54:13 | -16 | 1.0 | 63.07 |
| 12:54:14 | -16 | 1.0 | 63.09 |
| 12:54:15 | -16 | 1.0 | 63.10 |
| 12:54:16 | -16 | 1.0 | 63.12 |
| 12:54:17 | -16 | 1.0 | 63.14 |
| 12:54:18 | -16 | 1.0 | 63.15 |
| 12:54:19 | -16 | 1.0 | 63.17 |
| 12:54:20 | -16 | 1.0 | 63.19 |
| 12:54:21 | -16 | 1.0 | 63.20 |
| 12:54:22 | -16 | 1.0 | 63.22 |
| 12:54:23 | -16 | 1.0 | 63.24 |
| 12:54:24 | -16 | 1.0 | 63.26 |
| 12:54:25 | -16 | 1.0 | 63.27 |
| 12:54:26 | -16 | 1.0 | 63.29 |
| 12:54:27 | -16 | 1.0 | 63.31 |
| 12:54:28 | -16 | 1.0 | 63.32 |
| 12:54:29 | -16 | 1.0 | 63.34 |
| 12:54:30 | -16 | 1.0 | 63.36 |
| 12:54:31 | -16 | 1.0 | 63.37 |
| 12:54:32 | -16 | 1.0 | 63.39 |
| 12:54:33 | -16 | 1.0 | 63.41 |
| 12:54:34 | -16 | 1.0 | 63.43 |
| 12:54:35 | -16 | 1.0 | 63.44 |
| 12:54:36 | -16 | 1.0 | 63.46 |
| 12:54:37 | -16 | 1.0 | 63.48 |
| 12:54:38 | -16 | 1.0 | 63.49 |
| 12:54:39 | -16 | 1.0 | 63.51 |
| 12:54:40 | -16 | 1.0 | 63.53 |
| 12:54:41 | -16 | 1.0 | 63.54 |
| 12:54:42 | -16 | 1.0 | 63.56 |
| 12:54:43 | -16 | 1.0 | 63.58 |
| 12:54:44 | -16 | 1.0 | 63.60 |
| 12:54:45 | -16 | 1.0 | 63.61 |
| 12:54:46 | -15 | 1.0 | 63.63 |
| 12:54:47 | -15 | 1.0 | 63.65 |
| 12:54:48 | -15 | 1.0 | 63.66 |
| 12:54:49 | -15 | 1.0 | 63.68 |
| 12:54:50 | -15 | 1.0 | 63.70 |
| 12:54:51 | -15 | 1.0 | 63.71 |
| 12:54:52 | -16 | 1.0 | 63.73 |
| 12:54:53 | -16 | 1.0 | 63.75 |
| 12:54:54 | -16 | 1.0 | 63.77 |
| 12:54:55 | -16 | 1.0 | 63.78 |
| 12:54:56 | -16 | 1.0 | 63.80 |
| 12:54:57 | -16 | 1.0 | 63.82 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:54:58 | -16 | 1.0 | 63.83 |
| 12:54:59 | -16 | 1.0 | 63.85 |
| 12:55:00 | -16 | 1.0 | 63.87 |
| 12:55:01 | -16 | 1.0 | 63.89 |
| 12:55:02 | -16 | 1.0 | 63.90 |
| 12:55:03 | -16 | 1.0 | 63.92 |
| 12:55:04 | -16 | 1.0 | 63.94 |
| 12:55:05 | -16 | 1.0 | 63.95 |
| 12:55:06 | -16 | 1.0 | 63.97 |
| 12:55:07 | -16 | 1.0 | 63.99 |
| 12:55:08 | -16 | 1.0 | 64.00 |
| 12:55:09 | -16 | 1.0 | 64.02 |
| 12:55:10 | -16 | 1.0 | 64.04 |
| 12:55:11 | -16 | 1.0 | 64.06 |
| 12:55:12 | -16 | 1.0 | 64.07 |
| 12:55:13 | -16 | 1.0 | 64.09 |
| 12:55:14 | -16 | 1.0 | 64.11 |
| 12:55:15 | -16 | 1.0 | 64.12 |
| 12:55:16 | -16 | 1.0 | 64.14 |
| 12:55:17 | -16 | 1.0 | 64.16 |
| 12:55:18 | -16 | 1.0 | 64.18 |
| 12:55:19 | -16 | 1.0 | 64.19 |
| 12:55:20 | -16 | 1.0 | 64.21 |
| 12:55:21 | -16 | 1.0 | 64.23 |
| 12:55:22 | -16 | 1.0 | 64.25 |
| 12:55:23 | -16 | 1.0 | 64.26 |
| 12:55:24 | -16 | 1.0 | 64.28 |
| 12:55:25 | -16 | 1.0 | 64.30 |
| 12:55:26 | -16 | 1.0 | 64.31 |
| 12:55:27 | -16 | 1.0 | 64.33 |
| 12:55:28 | -16 | 1.0 | 64.35 |
| 12:55:29 | -16 | 1.0 | 64.36 |
| 12:55:30 | -16 | 1.0 | 64.38 |
| 12:55:31 | -16 | 1.0 | 64.40 |
| 12:55:32 | -16 | 1.0 | 64.42 |
| 12:55:33 | -16 | 1.0 | 64.43 |
| 12:55:34 | -16 | 1.0 | 64.45 |
| 12:55:35 | -16 | 1.0 | 64.47 |
| 12:55:36 | -16 | 1.0 | 64.49 |
| 12:55:37 | -16 | 1.0 | 64.50 |
| 12:55:38 | -16 | 1.0 | 64.52 |
| 12:55:39 | -16 | 1.0 | 64.54 |
| 12:55:40 | -16 | 1.0 | 64.55 |
| 12:55:41 | -16 | 1.0 | 64.57 |
| 12:55:42 | -16 | 1.0 | 64.59 |
| 12:55:43 | -16 | 1.0 | 64.60 |
| 12:55:44 | -16 | 1.0 | 64.62 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:55:45 | -16 | 1.0 | 64.64 |
| 12:55:46 | -16 | 1.0 | 64.66 |
| 12:55:47 | -16 | 1.0 | 64.67 |
| 12:55:48 | -15 | 1.0 | 64.69 |
| 12:55:49 | -15 | 1.0 | 64.71 |
| 12:55:50 | -15 | 1.0 | 64.72 |
| 12:55:51 | -15 | 1.0 | 64.74 |
| 12:55:52 | -15 | 1.0 | 64.76 |
| 12:55:53 | -15 | 1.0 | 64.78 |
| 12:55:54 | -15 | 1.0 | 64.79 |
| 12:55:55 | -15 | 1.0 | 64.81 |
| 12:55:56 | -15 | 1.0 | 64.83 |
| 12:55:57 | -15 | 1.0 | 64.84 |
| 12:55:58 | -15 | 1.0 | 64.86 |
| 12:55:59 | -15 | 1.0 | 64.88 |
| 12:56:00 | -15 | 1.0 | 64.90 |
| 12:56:01 | -15 | 1.0 | 64.91 |
| 12:56:02 | -15 | 1.0 | 64.93 |
| 12:56:03 | -15 | 1.0 | 64.95 |
| 12:56:04 | -15 | 1.0 | 64.96 |
| 12:56:05 | -15 | 1.0 | 64.98 |
| 12:56:06 | -15 | 1.0 | 65.00 |
| 12:56:07 | -15 | 1.0 | 65.02 |
| 12:56:08 | -15 | 1.0 | 65.03 |
| 12:56:09 | -15 | 1.0 | 65.05 |
| 12:56:10 | -15 | 1.0 | 65.07 |
| 12:56:11 | -15 | 1.0 | 65.09 |
| 12:56:12 | -15 | 1.0 | 65.10 |
| 12:56:13 | -15 | 1.0 | 65.12 |
| 12:56:14 | -15 | 1.0 | 65.14 |
| 12:56:15 | -15 | 1.0 | 65.15 |
| 12:56:16 | -16 | 1.0 | 65.17 |
| 12:56:17 | -16 | 1.0 | 65.19 |
| 12:56:18 | -16 | 1.0 | 65.21 |
| 12:56:19 | -16 | 1.0 | 65.22 |
| 12:56:20 | -16 | 1.0 | 65.24 |
| 12:56:21 | -16 | 1.0 | 65.26 |
| 12:56:22 | -15 | 1.0 | 65.27 |
| 12:56:23 | -15 | 1.0 | 65.29 |
| 12:56:24 | -15 | 1.0 | 65.31 |
| 12:56:25 | -15 | 1.0 | 65.33 |
| 12:56:26 | -15 | 1.0 | 65.34 |
| 12:56:27 | -15 | 1.0 | 65.36 |
| 12:56:28 | -15 | 1.0 | 65.38 |
| 12:56:29 | -15 | 1.0 | 65.39 |
| 12:56:30 | -15 | 1.0 | 65.41 |
| 12:56:31 | -15 | 1.0 | 65.43 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:56:32 | -15 | 1.0 | 65.45 |
| 12:56:33 | -15 | 1.0 | 65.46 |
| 12:56:34 | -15 | 1.0 | 65.48 |
| 12:56:35 | -15 | 1.0 | 65.50 |
| 12:56:36 | -15 | 1.0 | 65.51 |
| 12:56:37 | -15 | 1.0 | 65.53 |
| 12:56:38 | -15 | 1.0 | 65.55 |
| 12:56:39 | -15 | 1.0 | 65.56 |
| 12:56:40 | -15 | 1.0 | 65.58 |
| 12:56:41 | -15 | 1.0 | 65.60 |
| 12:56:42 | -15 | 1.0 | 65.62 |
| 12:56:43 | -15 | 1.0 | 65.63 |
| 12:56:44 | -15 | 1.0 | 65.65 |
| 12:56:45 | -15 | 1.0 | 65.67 |
| 12:56:46 | -15 | 1.0 | 65.68 |
| 12:56:47 | -15 | 1.0 | 65.70 |
| 12:56:48 | -15 | 1.0 | 65.72 |
| 12:56:49 | -15 | 1.0 | 65.74 |
| 12:56:50 | -16 | 1.0 | 65.75 |
| 12:56:51 | -16 | 1.0 | 65.77 |
| 12:56:52 | -16 | 1.0 | 65.79 |
| 12:56:53 | -16 | 1.0 | 65.80 |
| 12:56:54 | -16 | 1.0 | 65.82 |
| 12:56:55 | -16 | 1.0 | 65.84 |
| 12:56:56 | -16 | 1.0 | 65.86 |
| 12:56:57 | -16 | 1.0 | 65.87 |
| 12:56:58 | -16 | 1.0 | 65.89 |
| 12:56:59 | -16 | 1.0 | 65.91 |
| 12:57:00 | -16 | 1.0 | 65.92 |
| 12:57:01 | -16 | 1.0 | 65.94 |
| 12:57:02 | -16 | 1.0 | 65.96 |
| 12:57:03 | -16 | 1.0 | 65.98 |
| 12:57:04 | -16 | 1.0 | 65.99 |
| 12:57:05 | -16 | 1.0 | 66.01 |
| 12:57:06 | -16 | 1.0 | 66.03 |
| 12:57:07 | -16 | 1.0 | 66.04 |
| 12:57:08 | -16 | 1.0 | 66.06 |
| 12:57:09 | -16 | 1.0 | 66.08 |
| 12:57:10 | -16 | 1.0 | 66.10 |
| 12:57:11 | -16 | 1.0 | 66.11 |
| 12:57:12 | -16 | 1.0 | 66.13 |
| 12:57:13 | -16 | 1.0 | 66.15 |
| 12:57:14 | -16 | 1.0 | 66.16 |
| 12:57:15 | -16 | 1.0 | 66.18 |
| 12:57:16 | -16 | 1.0 | 66.20 |
| 12:57:17 | -16 | 1.0 | 66.21 |
| 12:57:18 | -16 | 1.0 | 66.23 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:57:19 | -16 | 1.0 | 66.25 |
| 12:57:20 | -16 | 1.0 | 66.27 |
| 12:57:21 | -16 | 1.0 | 66.28 |
| 12:57:22 | -16 | 1.0 | 66.30 |
| 12:57:23 | -16 | 1.0 | 66.32 |
| 12:57:24 | -16 | 1.0 | 66.33 |
| 12:57:25 | -16 | 1.0 | 66.35 |
| 12:57:26 | -16 | 1.0 | 66.37 |
| 12:57:27 | -16 | 1.0 | 66.39 |
| 12:57:28 | -16 | 1.0 | 66.40 |
| 12:57:29 | -15 | 1.0 | 66.42 |
| 12:57:30 | -15 | 1.0 | 66.44 |
| 12:57:31 | -15 | 1.0 | 66.45 |
| 12:57:32 | -15 | 1.0 | 66.47 |
| 12:57:33 | -15 | 1.0 | 66.49 |
| 12:57:34 | -15 | 1.0 | 66.51 |
| 12:57:35 | -15 | 1.0 | 66.52 |
| 12:57:36 | -15 | 1.0 | 66.54 |
| 12:57:37 | -15 | 1.0 | 66.56 |
| 12:57:38 | -15 | 1.0 | 66.57 |
| 12:57:39 | -15 | 1.0 | 66.59 |
| 12:57:40 | -15 | 1.0 | 66.61 |
| 12:57:41 | -15 | 1.0 | 66.63 |
| 12:57:42 | -15 | 1.0 | 66.64 |
| 12:57:43 | -15 | 1.0 | 66.66 |
| 12:57:44 | -15 | 1.0 | 66.68 |
| 12:57:45 | -15 | 1.0 | 66.69 |
| 12:57:46 | -15 | 1.0 | 66.71 |
| 12:57:47 | -15 | 1.0 | 66.73 |
| 12:57:48 | -15 | 1.0 | 66.75 |
| 12:57:49 | -15 | 1.0 | 66.76 |
| 12:57:50 | -16 | 1.0 | 66.78 |
| 12:57:51 | -16 | 1.0 | 66.80 |
| 12:57:52 | -16 | 1.0 | 66.81 |
| 12:57:53 | -16 | 1.0 | 66.83 |
| 12:57:54 | -16 | 1.0 | 66.85 |
| 12:57:55 | -16 | 1.0 | 66.87 |
| 12:57:56 | -16 | 1.0 | 66.88 |
| 12:57:57 | -16 | 1.0 | 66.90 |
| 12:57:58 | -16 | 1.0 | 66.92 |
| 12:57:59 | -16 | 1.0 | 66.93 |
| 12:58:00 | -16 | 1.0 | 66.95 |
| 12:58:01 | -16 | 1.0 | 66.97 |
| 12:58:02 | -16 | 1.0 | 66.99 |
| 12:58:03 | -16 | 1.0 | 67.00 |
| 12:58:04 | -16 | 1.0 | 67.02 |
| 12:58:05 | -16 | 1.0 | 67.04 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:58:06 | -16 | 1.0 | 67.05 |
| 12:58:07 | -16 | 1.0 | 67.07 |
| 12:58:08 | -16 | 1.0 | 67.09 |
| 12:58:09 | -16 | 1.0 | 67.11 |
| 12:58:10 | -16 | 1.0 | 67.12 |
| 12:58:11 | -16 | 1.0 | 67.14 |
| 12:58:12 | -16 | 1.0 | 67.16 |
| 12:58:13 | -16 | 1.0 | 67.17 |
| 12:58:14 | -16 | 1.0 | 67.19 |
| 12:58:15 | -16 | 1.0 | 67.21 |
| 12:58:16 | -16 | 1.0 | 67.23 |
| 12:58:17 | -16 | 1.0 | 67.24 |
| 12:58:18 | -16 | 1.0 | 67.26 |
| 12:58:19 | -16 | 1.0 | 67.28 |
| 12:58:20 | -16 | 1.0 | 67.29 |
| 12:58:21 | -16 | 1.0 | 67.31 |
| 12:58:22 | -16 | 1.0 | 67.33 |
| 12:58:23 | -16 | 1.0 | 67.35 |
| 12:58:24 | -16 | 1.0 | 67.36 |
| 12:58:25 | -16 | 1.0 | 67.38 |
| 12:58:26 | -16 | 1.0 | 67.40 |
| 12:58:27 | -16 | 1.0 | 67.41 |
| 12:58:28 | -16 | 1.0 | 67.43 |
| 12:58:29 | -16 | 1.0 | 67.45 |
| 12:58:30 | -16 | 1.0 | 67.46 |
| 12:58:31 | -16 | 1.0 | 67.48 |
| 12:58:32 | -16 | 1.0 | 67.50 |
| 12:58:33 | -16 | 1.0 | 67.52 |
| 12:58:34 | -16 | 1.0 | 67.53 |
| 12:58:35 | -16 | 1.0 | 67.55 |
| 12:58:36 | -16 | 1.0 | 67.57 |
| 12:58:37 | -16 | 1.0 | 67.58 |
| 12:58:38 | -16 | 1.0 | 67.60 |
| 12:58:39 | -16 | 1.0 | 67.62 |
| 12:58:40 | -16 | 1.0 | 67.64 |
| 12:58:41 | -16 | 1.0 | 67.65 |
| 12:58:42 | -16 | 1.0 | 67.67 |
| 12:58:43 | -16 | 1.0 | 67.69 |
| 12:58:44 | -16 | 1.0 | 67.70 |
| 12:58:45 | -16 | 1.0 | 67.72 |
| 12:58:46 | -16 | 1.0 | 67.74 |
| 12:58:47 | -16 | 1.0 | 67.76 |
| 12:58:48 | -16 | 1.0 | 67.77 |
| 12:58:49 | -16 | 1.0 | 67.79 |
| 12:58:50 | -16 | 1.0 | 67.81 |
| 12:58:51 | -16 | 1.0 | 67.82 |
| 12:58:52 | -16 | 1.0 | 67.84 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:58:53 | -16 | 1.0 | 67.86 |
| 12:58:54 | -16 | 1.0 | 67.88 |
| 12:58:55 | -16 | 1.0 | 67.89 |
| 12:58:56 | -16 | 1.0 | 67.91 |
| 12:58:57 | -16 | 1.0 | 67.93 |
| 12:58:58 | -16 | 1.0 | 67.94 |
| 12:58:59 | -16 | 1.0 | 67.96 |
| 12:59:00 | -16 | 1.0 | 67.98 |
| 12:59:01 | -16 | 1.0 | 68.00 |
| 12:59:02 | -16 | 1.0 | 68.01 |
| 12:59:03 | -16 | 1.0 | 68.03 |
| 12:59:04 | -16 | 1.0 | 68.05 |
| 12:59:05 | -16 | 1.0 | 68.06 |
| 12:59:06 | -16 | 1.0 | 68.08 |
| 12:59:07 | -16 | 1.0 | 68.10 |
| 12:59:08 | -16 | 1.0 | 68.12 |
| 12:59:09 | -16 | 1.0 | 68.13 |
| 12:59:10 | -16 | 1.0 | 68.15 |
| 12:59:11 | -16 | 1.0 | 68.17 |
| 12:59:12 | -16 | 1.0 | 68.18 |
| 12:59:13 | -16 | 1.0 | 68.20 |
| 12:59:14 | -16 | 1.0 | 68.22 |
| 12:59:15 | -16 | 1.0 | 68.24 |
| 12:59:16 | -16 | 1.0 | 68.25 |
| 12:59:17 | -16 | 1.0 | 68.27 |
| 12:59:18 | -16 | 1.0 | 68.29 |
| 12:59:19 | -16 | 1.0 | 68.30 |
| 12:59:20 | -16 | 1.0 | 68.32 |
| 12:59:21 | -16 | 1.0 | 68.34 |
| 12:59:22 | -16 | 1.0 | 68.36 |
| 12:59:23 | -16 | 1.0 | 68.37 |
| 12:59:24 | -16 | 1.0 | 68.39 |
| 12:59:25 | -16 | 1.0 | 68.41 |
| 12:59:26 | -16 | 1.0 | 68.42 |
| 12:59:27 | -15 | 1.0 | 68.44 |
| 12:59:28 | -15 | 1.0 | 68.46 |
| 12:59:29 | -15 | 1.0 | 68.48 |
| 12:59:30 | -15 | 1.0 | 68.49 |
| 12:59:31 | -15 | 1.0 | 68.51 |
| 12:59:32 | -15 | 1.0 | 68.53 |
| 12:59:33 | -15 | 1.0 | 68.54 |
| 12:59:34 | -16 | 1.0 | 68.56 |
| 12:59:35 | -16 | 1.0 | 68.58 |
| 12:59:36 | -16 | 1.0 | 68.60 |
| 12:59:37 | -16 | 1.0 | 68.61 |
| 12:59:38 | -16 | 1.0 | 68.63 |
| 12:59:39 | -16 | 1.0 | 68.65 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 12:59:40 | -16 | 1.0 | 68.66 |
| 12:59:41 | -16 | 1.0 | 68.68 |
| 12:59:42 | -16 | 1.0 | 68.70 |
| 12:59:43 | -16 | 1.0 | 68.72 |
| 12:59:44 | -16 | 1.0 | 68.73 |
| 12:59:45 | -16 | 1.0 | 68.75 |
| 12:59:46 | -16 | 1.0 | 68.77 |
| 12:59:47 | -16 | 1.0 | 68.78 |
| 12:59:48 | -16 | 1.0 | 68.80 |
| 12:59:49 | -16 | 1.0 | 68.82 |
| 12:59:50 | -16 | 1.0 | 68.84 |
| 12:59:51 | -16 | 1.0 | 68.85 |
| 12:59:52 | -16 | 1.0 | 68.87 |
| 12:59:53 | -16 | 1.0 | 68.89 |
| 12:59:54 | -16 | 1.0 | 68.90 |
| 12:59:55 | -17 | 1.0 | 68.92 |
| 12:59:56 | -17 | 1.0 | 68.94 |
| 12:59:57 | -16 | 1.0 | 68.96 |
| 12:59:58 | -16 | 1.0 | 68.97 |
| 12:59:59 | -16 | 1.0 | 68.99 |
| 13:00:00 | -17 | 1.0 | 69.01 |
| 13:00:01 | -17 | 1.0 | 69.02 |
| 13:00:02 | -17 | 1.0 | 69.04 |
| 13:00:03 | -17 | 1.0 | 69.06 |
| 13:00:04 | -17 | 1.0 | 69.08 |
| 13:00:05 | -17 | 1.0 | 69.09 |
| 13:00:06 | -17 | 1.0 | 69.11 |
| 13:00:07 | -17 | 1.0 | 69.13 |
| 13:00:08 | -17 | 1.0 | 69.14 |
| 13:00:09 | -17 | 1.0 | 69.16 |
| 13:00:10 | -17 | 1.0 | 69.18 |
| 13:00:11 | -17 | 1.0 | 69.19 |
| 13:00:12 | -17 | 1.0 | 69.21 |
| 13:00:13 | -17 | 1.0 | 69.23 |
| 13:00:14 | -16 | 1.0 | 69.25 |
| 13:00:15 | -16 | 1.0 | 69.26 |
| 13:00:16 | -16 | 1.0 | 69.28 |
| 13:00:17 | -16 | 1.0 | 69.30 |
| 13:00:18 | -16 | 1.0 | 69.32 |
| 13:00:19 | -16 | 1.0 | 69.33 |
| 13:00:20 | -16 | 1.0 | 69.35 |
| 13:00:21 | -16 | 1.0 | 69.37 |
| 13:00:22 | -16 | 1.0 | 69.38 |
| 13:00:23 | -16 | 1.0 | 69.40 |
| 13:00:24 | -16 | 1.0 | 69.42 |
| 13:00:25 | -16 | 1.0 | 69.44 |
| 13:00:26 | -16 | 1.0 | 69.45 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:00:27 | -16 | 1.0 | 69.47 |
| 13:00:28 | -16 | 1.0 | 69.49 |
| 13:00:29 | -16 | 1.0 | 69.50 |
| 13:00:30 | -16 | 1.0 | 69.52 |
| 13:00:31 | -16 | 1.0 | 69.54 |
| 13:00:32 | -16 | 1.0 | 69.56 |
| 13:00:33 | -16 | 1.0 | 69.57 |
| 13:00:34 | -16 | 1.0 | 69.59 |
| 13:00:35 | -16 | 1.0 | 69.61 |
| 13:00:36 | -16 | 1.0 | 69.62 |
| 13:00:37 | -16 | 1.0 | 69.64 |
| 13:00:38 | -16 | 1.0 | 69.66 |
| 13:00:39 | -16 | 1.0 | 69.68 |
| 13:00:40 | -16 | 1.0 | 69.69 |
| 13:00:41 | -16 | 1.0 | 69.71 |
| 13:00:42 | -16 | 1.0 | 69.73 |
| 13:00:43 | -16 | 1.0 | 69.74 |
| 13:00:44 | -16 | 1.0 | 69.76 |
| 13:00:45 | -16 | 1.0 | 69.78 |
| 13:00:46 | -16 | 1.0 | 69.80 |
| 13:00:47 | -16 | 1.0 | 69.81 |
| 13:00:48 | -16 | 1.0 | 69.83 |
| 13:00:49 | -16 | 1.0 | 69.85 |
| 13:00:50 | -16 | 1.0 | 69.86 |
| 13:00:51 | -16 | 1.0 | 69.88 |
| 13:00:52 | -16 | 1.0 | 69.90 |
| 13:00:53 | -16 | 1.0 | 69.92 |
| 13:00:54 | -15 | 1.0 | 69.93 |
| 13:00:55 | -15 | 1.0 | 69.95 |
| 13:00:56 | -15 | 1.0 | 69.97 |
| 13:00:57 | -15 | 1.0 | 69.98 |
| 13:00:58 | -15 | 1.0 | 70.00 |
| 13:00:59 | -15 | 1.0 | 70.02 |
| 13:01:00 | -15 | 1.0 | 70.04 |
| 13:01:01 | -15 | 1.0 | 70.05 |
| 13:01:02 | -15 | 1.0 | 70.07 |
| 13:01:03 | -15 | 1.0 | 70.09 |
| 13:01:04 | -15 | 1.0 | 70.10 |
| 13:01:05 | -15 | 1.0 | 70.12 |
| 13:01:06 | -16 | 1.0 | 70.14 |
| 13:01:07 | -16 | 1.0 | 70.16 |
| 13:01:08 | -16 | 1.0 | 70.17 |
| 13:01:09 | -16 | 1.0 | 70.19 |
| 13:01:10 | -16 | 1.0 | 70.21 |
| 13:01:11 | -16 | 1.0 | 70.22 |
| 13:01:12 | -16 | 1.0 | 70.24 |
| 13:01:13 | -16 | 1.0 | 70.26 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:01:14 | -16 | 1.0 | 70.28 |
| 13:01:15 | -16 | 1.0 | 70.29 |
| 13:01:16 | -16 | 1.0 | 70.31 |
| 13:01:17 | -16 | 1.0 | 70.33 |
| 13:01:18 | -16 | 1.0 | 70.34 |
| 13:01:19 | -16 | 1.0 | 70.36 |
| 13:01:20 | -16 | 1.0 | 70.38 |
| 13:01:21 | -16 | 1.0 | 70.39 |
| 13:01:22 | -16 | 1.0 | 70.41 |
| 13:01:23 | -16 | 1.0 | 70.43 |
| 13:01:24 | -16 | 1.0 | 70.45 |
| 13:01:25 | -16 | 1.0 | 70.46 |
| 13:01:26 | -16 | 1.0 | 70.48 |
| 13:01:27 | -16 | 1.0 | 70.50 |
| 13:01:28 | -16 | 1.0 | 70.51 |
| 13:01:29 | -16 | 1.0 | 70.53 |
| 13:01:30 | -16 | 1.0 | 70.55 |
| 13:01:31 | -16 | 1.0 | 70.57 |
| 13:01:32 | -16 | 1.0 | 70.58 |
| 13:01:33 | -17 | 1.0 | 70.60 |
| 13:01:34 | -17 | 1.0 | 70.62 |
| 13:01:35 | -17 | 1.0 | 70.63 |
| 13:01:36 | -17 | 1.0 | 70.65 |
| 13:01:37 | -17 | 1.0 | 70.67 |
| 13:01:38 | -17 | 1.0 | 70.69 |
| 13:01:39 | -17 | 1.0 | 70.70 |
| 13:01:40 | -17 | 1.0 | 70.72 |
| 13:01:41 | -17 | 1.0 | 70.74 |
| 13:01:42 | -17 | 1.0 | 70.75 |
| 13:01:43 | -17 | 1.0 | 70.77 |
| 13:01:44 | -16 | 1.0 | 70.79 |
| 13:01:45 | -16 | 1.0 | 70.81 |
| 13:01:46 | -17 | 1.0 | 70.82 |
| 13:01:47 | -17 | 1.0 | 70.84 |
| 13:01:48 | -17 | 1.0 | 70.86 |
| 13:01:49 | -17 | 1.0 | 70.88 |
| 13:01:50 | -16 | 1.0 | 70.89 |
| 13:01:51 | -16 | 1.0 | 70.91 |
| 13:01:52 | -16 | 1.0 | 70.93 |
| 13:01:53 | -16 | 1.0 | 70.94 |
| 13:01:54 | -16 | 1.0 | 70.96 |
| 13:01:55 | -16 | 1.0 | 70.98 |
| 13:01:56 | -16 | 1.0 | 70.99 |
| 13:01:57 | -16 | 1.0 | 71.01 |
| 13:01:58 | -16 | 1.0 | 71.03 |
| 13:01:59 | -16 | 1.0 | 71.05 |
| 13:02:00 | -16 | 1.0 | 71.06 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:02:01 | -16 | 1.0 | 71.08 |
| 13:02:02 | -16 | 1.0 | 71.10 |
| 13:02:03 | -16 | 1.0 | 71.11 |
| 13:02:04 | -16 | 1.0 | 71.13 |
| 13:02:05 | -16 | 1.0 | 71.15 |
| 13:02:06 | -16 | 1.0 | 71.17 |
| 13:02:07 | -16 | 1.0 | 71.18 |
| 13:02:08 | -16 | 1.0 | 71.20 |
| 13:02:09 | -16 | 1.0 | 71.22 |
| 13:02:10 | -16 | 1.0 | 71.23 |
| 13:02:11 | -16 | 1.0 | 71.25 |
| 13:02:12 | -16 | 1.0 | 71.27 |
| 13:02:13 | -16 | 1.0 | 71.29 |
| 13:02:14 | -16 | 1.0 | 71.30 |
| 13:02:15 | -16 | 1.0 | 71.32 |
| 13:02:16 | -16 | 1.0 | 71.34 |
| 13:02:17 | -16 | 1.0 | 71.35 |
| 13:02:18 | -16 | 1.0 | 71.37 |
| 13:02:19 | -16 | 1.0 | 71.39 |
| 13:02:20 | -16 | 1.0 | 71.41 |
| 13:02:21 | -16 | 1.0 | 71.42 |
| 13:02:22 | -16 | 1.0 | 71.44 |
| 13:02:23 | -16 | 1.0 | 71.46 |
| 13:02:24 | -16 | 1.0 | 71.47 |
| 13:02:25 | -16 | 1.0 | 71.49 |
| 13:02:26 | -16 | 1.0 | 71.51 |
| 13:02:27 | -16 | 1.0 | 71.53 |
| 13:02:28 | -16 | 1.0 | 71.54 |
| 13:02:29 | -16 | 1.0 | 71.56 |
| 13:02:30 | -16 | 1.0 | 71.58 |
| 13:02:31 | -16 | 1.0 | 71.59 |
| 13:02:32 | -16 | 1.0 | 71.61 |
| 13:02:33 | -16 | 1.0 | 71.63 |
| 13:02:34 | -16 | 1.0 | 71.64 |
| 13:02:35 | -16 | 1.0 | 71.66 |
| 13:02:36 | -16 | 1.0 | 71.68 |
| 13:02:37 | -16 | 1.0 | 71.70 |
| 13:02:38 | -16 | 1.0 | 71.71 |
| 13:02:39 | -16 | 1.0 | 71.73 |
| 13:02:40 | -16 | 1.0 | 71.75 |
| 13:02:41 | -16 | 1.0 | 71.76 |
| 13:02:42 | -16 | 1.0 | 71.78 |
| 13:02:43 | -16 | 1.0 | 71.80 |
| 13:02:44 | -15 | 1.0 | 71.82 |
| 13:02:45 | -15 | 1.0 | 71.83 |
| 13:02:46 | -15 | 1.0 | 71.85 |
| 13:02:47 | -15 | 1.0 | 71.87 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:02:48 | -15 | 1.0 | 71.88 |
| 13:02:49 | -15 | 1.0 | 71.90 |
| 13:02:50 | -15 | 1.0 | 71.92 |
| 13:02:51 | -15 | 1.0 | 71.94 |
| 13:02:52 | -15 | 1.0 | 71.95 |
| 13:02:53 | -15 | 1.0 | 71.97 |
| 13:02:54 | -15 | 1.0 | 71.99 |
| 13:02:55 | -15 | 1.0 | 72.00 |
| 13:02:56 | -15 | 1.0 | 72.02 |
| 13:02:57 | -15 | 1.0 | 72.04 |
| 13:02:58 | -15 | 1.0 | 72.06 |
| 13:02:59 | -15 | 1.0 | 72.07 |
| 13:03:00 | -15 | 1.0 | 72.09 |
| 13:03:01 | -15 | 1.0 | 72.11 |
| 13:03:02 | -15 | 1.0 | 72.12 |
| 13:03:03 | -15 | 1.0 | 72.14 |
| 13:03:04 | -15 | 1.0 | 72.16 |
| 13:03:05 | -15 | 1.0 | 72.17 |
| 13:03:06 | -15 | 1.0 | 72.19 |
| 13:03:07 | -15 | 1.0 | 72.21 |
| 13:03:08 | -15 | 1.0 | 72.23 |
| 13:03:09 | -15 | 1.0 | 72.24 |
| 13:03:10 | -15 | 1.0 | 72.26 |
| 13:03:11 | -15 | 1.0 | 72.28 |
| 13:03:12 | -15 | 1.0 | 72.29 |
| 13:03:13 | -15 | 1.0 | 72.31 |
| 13:03:14 | -15 | 1.0 | 72.33 |
| 13:03:15 | -15 | 1.0 | 72.35 |
| 13:03:16 | -15 | 1.0 | 72.36 |
| 13:03:17 | -15 | 1.0 | 72.38 |
| 13:03:18 | -15 | 1.0 | 72.40 |
| 13:03:19 | -15 | 1.0 | 72.41 |
| 13:03:20 | -15 | 1.0 | 72.43 |
| 13:03:21 | -15 | 1.0 | 72.45 |
| 13:03:22 | -15 | 1.0 | 72.46 |
| 13:03:23 | -15 | 1.0 | 72.48 |
| 13:03:24 | -15 | 1.0 | 72.50 |
| 13:03:25 | -15 | 1.0 | 72.52 |
| 13:03:26 | -15 | 1.0 | 72.53 |
| 13:03:27 | -15 | 1.0 | 72.55 |
| 13:03:28 | -15 | 1.0 | 72.57 |
| 13:03:29 | -15 | 1.0 | 72.58 |
| 13:03:30 | -15 | 1.0 | 72.60 |
| 13:03:31 | -15 | 1.0 | 72.62 |
| 13:03:32 | -15 | 1.0 | 72.64 |
| 13:03:33 | -15 | 1.0 | 72.65 |
| 13:03:34 | -15 | 1.0 | 72.67 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:03:35 | -15 | 1.0 | 72.69 |
| 13:03:36 | -15 | 1.0 | 72.70 |
| 13:03:37 | -15 | 1.0 | 72.72 |
| 13:03:38 | -15 | 1.0 | 72.74 |
| 13:03:39 | -15 | 1.0 | 72.75 |
| 13:03:40 | -15 | 1.0 | 72.77 |
| 13:03:41 | -15 | 1.0 | 72.79 |
| 13:03:42 | -15 | 1.0 | 72.81 |
| 13:03:43 | -15 | 1.0 | 72.82 |
| 13:03:44 | -15 | 1.0 | 72.84 |
| 13:03:45 | -15 | 1.0 | 72.86 |
| 13:03:46 | -15 | 1.0 | 72.87 |
| 13:03:47 | -15 | 1.0 | 72.89 |
| 13:03:48 | -15 | 1.0 | 72.91 |
| 13:03:49 | -15 | 1.0 | 72.92 |
| 13:03:50 | -15 | 1.0 | 72.94 |
| 13:03:51 | -15 | 1.0 | 72.96 |
| 13:03:52 | -15 | 1.0 | 72.98 |
| 13:03:53 | -15 | 1.0 | 72.99 |
| 13:03:54 | -15 | 1.0 | 73.01 |
| 13:03:55 | -15 | 1.0 | 73.03 |
| 13:03:56 | -15 | 1.0 | 73.04 |
| 13:03:57 | -15 | 1.0 | 73.06 |
| 13:03:58 | -15 | 1.0 | 73.08 |
| 13:03:59 | -15 | 1.0 | 73.09 |
| 13:04:00 | -15 | 1.0 | 73.11 |
| 13:04:01 | -15 | 1.0 | 73.13 |
| 13:04:02 | -15 | 1.0 | 73.15 |
| 13:04:03 | -15 | 1.0 | 73.16 |
| 13:04:04 | -15 | 1.0 | 73.18 |
| 13:04:05 | -15 | 1.0 | 73.20 |
| 13:04:06 | -15 | 1.0 | 73.21 |
| 13:04:07 | -15 | 1.0 | 73.23 |
| 13:04:08 | -15 | 1.0 | 73.25 |
| 13:04:09 | -15 | 1.0 | 73.26 |
| 13:04:10 | -15 | 1.0 | 73.28 |
| 13:04:11 | -15 | 1.0 | 73.30 |
| 13:04:12 | -15 | 1.0 | 73.32 |
| 13:04:13 | -15 | 1.0 | 73.33 |
| 13:04:14 | -15 | 1.0 | 73.35 |
| 13:04:15 | -15 | 1.0 | 73.37 |
| 13:04:16 | -15 | 1.0 | 73.38 |
| 13:04:17 | -15 | 1.0 | 73.40 |
| 13:04:18 | -15 | 1.0 | 73.42 |
| 13:04:19 | -15 | 1.0 | 73.43 |
| 13:04:20 | -15 | 1.0 | 73.45 |
| 13:04:21 | -15 | 1.0 | 73.47 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:04:22 | -15 | 1.0 | 73.49 |
| 13:04:23 | -15 | 1.0 | 73.50 |
| 13:04:24 | -15 | 1.0 | 73.52 |
| 13:04:25 | -15 | 1.0 | 73.54 |
| 13:04:26 | -15 | 1.0 | 73.55 |
| 13:04:27 | -15 | 1.0 | 73.57 |
| 13:04:28 | -15 | 1.0 | 73.59 |
| 13:04:29 | -15 | 1.0 | 73.60 |
| 13:04:30 | -15 | 1.0 | 73.62 |
| 13:04:31 | -15 | 1.0 | 73.64 |
| 13:04:32 | -15 | 1.0 | 73.66 |
| 13:04:33 | -15 | 1.0 | 73.67 |
| 13:04:34 | -15 | 1.0 | 73.69 |
| 13:04:35 | -15 | 1.0 | 73.71 |
| 13:04:36 | -15 | 1.0 | 73.72 |
| 13:04:37 | -15 | 1.0 | 73.74 |
| 13:04:38 | -15 | 1.0 | 73.76 |
| 13:04:39 | -15 | 1.0 | 73.77 |
| 13:04:40 | -15 | 1.0 | 73.79 |
| 13:04:41 | -15 | 1.0 | 73.81 |
| 13:04:42 | -15 | 1.0 | 73.82 |
| 13:04:43 | -15 | 1.0 | 73.84 |
| 13:04:44 | -15 | 1.0 | 73.86 |
| 13:04:45 | -15 | 1.0 | 73.88 |
| 13:04:46 | -15 | 1.0 | 73.89 |
| 13:04:47 | -15 | 1.0 | 73.91 |
| 13:04:48 | -15 | 1.0 | 73.93 |
| 13:04:49 | -15 | 1.0 | 73.94 |
| 13:04:50 | -15 | 1.0 | 73.96 |
| 13:04:51 | -15 | 1.0 | 73.98 |
| 13:04:52 | -15 | 1.0 | 73.99 |
| 13:04:53 | -15 | 1.0 | 74.01 |
| 13:04:54 | -15 | 1.0 | 74.03 |
| 13:04:55 | -15 | 1.0 | 74.05 |
| 13:04:56 | -15 | 1.0 | 74.06 |
| 13:04:57 | -15 | 1.0 | 74.08 |
| 13:04:58 | -15 | 1.0 | 74.10 |
| 13:04:59 | -15 | 1.0 | 74.11 |
| 13:05:00 | -15 | 1.0 | 74.13 |
| 13:05:01 | -15 | 1.0 | 74.15 |
| 13:05:02 | -15 | 1.0 | 74.16 |
| 13:05:03 | -15 | 1.0 | 74.18 |
| 13:05:04 | -15 | 1.0 | 74.20 |
| 13:05:05 | -15 | 1.0 | 74.21 |
| 13:05:06 | -15 | 1.0 | 74.23 |
| 13:05:07 | -15 | 1.0 | 74.25 |
| 13:05:08 | -15 | 1.0 | 74.27 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:05:09 | -15 | 1.0 | 74.28 |
| 13:05:10 | -15 | 1.0 | 74.30 |
| 13:05:11 | -15 | 1.0 | 74.32 |
| 13:05:12 | -15 | 1.0 | 74.33 |
| 13:05:13 | -15 | 1.0 | 74.35 |
| 13:05:14 | -15 | 1.0 | 74.37 |
| 13:05:15 | -15 | 1.0 | 74.38 |
| 13:05:16 | -15 | 1.0 | 74.40 |
| 13:05:17 | -15 | 1.0 | 74.42 |
| 13:05:18 | -15 | 1.0 | 74.43 |
| 13:05:19 | -15 | 1.0 | 74.45 |
| 13:05:20 | -15 | 1.0 | 74.47 |
| 13:05:21 | -15 | 1.0 | 74.49 |
| 13:05:22 | -15 | 1.0 | 74.50 |
| 13:05:23 | -15 | 1.0 | 74.52 |
| 13:05:24 | -15 | 1.0 | 74.54 |
| 13:05:25 | -15 | 1.0 | 74.55 |
| 13:05:26 | -15 | 1.0 | 74.57 |
| 13:05:27 | -15 | 1.0 | 74.59 |
| 13:05:28 | -15 | 1.0 | 74.60 |
| 13:05:29 | -15 | 1.0 | 74.62 |
| 13:05:30 | -15 | 1.0 | 74.64 |
| 13:05:31 | -15 | 1.0 | 74.65 |
| 13:05:32 | -15 | 1.0 | 74.67 |
| 13:05:33 | -15 | 1.0 | 74.69 |
| 13:05:34 | -15 | 1.0 | 74.71 |
| 13:05:35 | -15 | 1.0 | 74.72 |
| 13:05:36 | -15 | 1.0 | 74.74 |
| 13:05:37 | -15 | 1.0 | 74.76 |
| 13:05:38 | -15 | 1.0 | 74.77 |
| 13:05:39 | -15 | 1.0 | 74.79 |
| 13:05:40 | -15 | 1.0 | 74.81 |
| 13:05:41 | -15 | 1.0 | 74.82 |
| 13:05:42 | -15 | 1.0 | 74.84 |
| 13:05:43 | -15 | 1.0 | 74.86 |
| 13:05:44 | -15 | 1.0 | 74.88 |
| 13:05:45 | -15 | 1.0 | 74.89 |
| 13:05:46 | -15 | 1.0 | 74.91 |
| 13:05:47 | -15 | 1.0 | 74.93 |
| 13:05:48 | -15 | 1.0 | 74.94 |
| 13:05:49 | -15 | 1.0 | 74.96 |
| 13:05:50 | -15 | 1.0 | 74.98 |
| 13:05:51 | -15 | 1.0 | 74.99 |
| 13:05:52 | -15 | 1.0 | 75.01 |
| 13:05:53 | -15 | 1.0 | 75.03 |
| 13:05:54 | -15 | 1.0 | 75.05 |
| 13:05:55 | -15 | 1.0 | 75.06 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:05:56 | -15 | 1.0 | 75.08 |
| 13:05:57 | -15 | 1.0 | 75.10 |
| 13:05:58 | -15 | 1.0 | 75.11 |
| 13:05:59 | -15 | 1.0 | 75.13 |
| 13:06:00 | -15 | 1.0 | 75.15 |
| 13:06:01 | -15 | 1.0 | 75.16 |
| 13:06:02 | -15 | 1.0 | 75.18 |
| 13:06:03 | -15 | 1.0 | 75.20 |
| 13:06:04 | -15 | 1.0 | 75.21 |
| 13:06:05 | -15 | 1.0 | 75.23 |
| 13:06:06 | -15 | 1.0 | 75.25 |
| 13:06:07 | -15 | 1.0 | 75.27 |
| 13:06:08 | -15 | 1.0 | 75.28 |
| 13:06:09 | -15 | 1.0 | 75.30 |
| 13:06:10 | -15 | 1.0 | 75.32 |
| 13:06:11 | -15 | 1.0 | 75.33 |
| 13:06:12 | -15 | 1.0 | 75.35 |
| 13:06:13 | -15 | 1.0 | 75.37 |
| 13:06:14 | -15 | 1.0 | 75.39 |
| 13:06:15 | -15 | 1.0 | 75.40 |
| 13:06:16 | -15 | 1.0 | 75.42 |
| 13:06:17 | -15 | 1.0 | 75.44 |
| 13:06:18 | -15 | 1.0 | 75.45 |
| 13:06:19 | -15 | 1.0 | 75.47 |
| 13:06:20 | -15 | 1.0 | 75.49 |
| 13:06:21 | -15 | 1.0 | 75.50 |
| 13:06:22 | -15 | 1.0 | 75.52 |
| 13:06:23 | -15 | 1.0 | 75.54 |
| 13:06:24 | -15 | 1.0 | 75.56 |
| 13:06:25 | -15 | 1.0 | 75.57 |
| 13:06:26 | -15 | 1.0 | 75.59 |
| 13:06:27 | -15 | 1.0 | 75.61 |
| 13:06:28 | -15 | 1.0 | 75.62 |
| 13:06:29 | -15 | 1.0 | 75.64 |
| 13:06:30 | -15 | 1.0 | 75.66 |
| 13:06:31 | -15 | 1.0 | 75.67 |
| 13:06:32 | -15 | 1.0 | 75.69 |
| 13:06:33 | -15 | 1.0 | 75.71 |
| 13:06:34 | -15 | 1.0 | 75.73 |
| 13:06:35 | -15 | 1.0 | 75.74 |
| 13:06:36 | -15 | 1.0 | 75.76 |
| 13:06:37 | -15 | 1.0 | 75.78 |
| 13:06:38 | -15 | 1.0 | 75.79 |
| 13:06:39 | -15 | 1.0 | 75.81 |
| 13:06:40 | -15 | 1.0 | 75.83 |
| 13:06:41 | -15 | 1.0 | 75.85 |
| 13:06:42 | -15 | 1.0 | 75.86 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:06:43 | -15 | 1.0 | 75.88 |
| 13:06:44 | -15 | 1.0 | 75.90 |
| 13:06:45 | -15 | 1.0 | 75.91 |
| 13:06:46 | -15 | 1.0 | 75.93 |
| 13:06:47 | -15 | 1.0 | 75.95 |
| 13:06:48 | -15 | 1.0 | 75.97 |
| 13:06:49 | -15 | 1.0 | 75.98 |
| 13:06:50 | -15 | 1.0 | 76.00 |
| 13:06:51 | -15 | 1.0 | 76.02 |
| 13:06:52 | -15 | 1.0 | 76.03 |
| 13:06:53 | -15 | 1.0 | 76.05 |
| 13:06:54 | -15 | 1.0 | 76.07 |
| 13:06:55 | -15 | 1.0 | 76.08 |
| 13:06:56 | -15 | 1.0 | 76.10 |
| 13:06:57 | -15 | 1.0 | 76.12 |
| 13:06:58 | -15 | 1.0 | 76.14 |
| 13:06:59 | -15 | 1.0 | 76.15 |
| 13:07:00 | -15 | 1.0 | 76.17 |
| 13:07:01 | -15 | 1.0 | 76.19 |
| 13:07:02 | -15 | 1.0 | 76.20 |
| 13:07:03 | -15 | 1.0 | 76.22 |
| 13:07:04 | -15 | 1.0 | 76.24 |
| 13:07:05 | -15 | 1.0 | 76.26 |
| 13:07:06 | -15 | 1.0 | 76.27 |
| 13:07:07 | -15 | 1.0 | 76.29 |
| 13:07:08 | -15 | 1.0 | 76.31 |
| 13:07:09 | -15 | 1.0 | 76.32 |
| 13:07:10 | -15 | 1.0 | 76.34 |
| 13:07:11 | -15 | 1.0 | 76.36 |
| 13:07:12 | -15 | 1.0 | 76.37 |
| 13:07:13 | -15 | 1.0 | 76.39 |
| 13:07:14 | -15 | 1.0 | 76.41 |
| 13:07:15 | -15 | 1.0 | 76.43 |
| 13:07:16 | -15 | 1.0 | 76.44 |
| 13:07:17 | -15 | 1.0 | 76.46 |
| 13:07:18 | -15 | 1.0 | 76.48 |
| 13:07:19 | -15 | 1.0 | 76.49 |
| 13:07:20 | -15 | 1.0 | 76.51 |
| 13:07:21 | -15 | 1.0 | 76.53 |
| 13:07:22 | -15 | 1.0 | 76.55 |
| 13:07:23 | -15 | 1.0 | 76.56 |
| 13:07:24 | -15 | 1.0 | 76.58 |
| 13:07:25 | -15 | 1.0 | 76.60 |
| 13:07:26 | -15 | 1.0 | 76.61 |
| 13:07:27 | -15 | 1.0 | 76.63 |
| 13:07:28 | -15 | 1.0 | 76.65 |
| 13:07:29 | -15 | 1.0 | 76.66 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:07:30 | -15 | 1.0 | 76.68 |
| 13:07:31 | -15 | 1.0 | 76.70 |
| 13:07:32 | -15 | 1.0 | 76.72 |
| 13:07:33 | -15 | 1.0 | 76.73 |
| 13:07:34 | -15 | 1.0 | 76.75 |
| 13:07:35 | -15 | 1.0 | 76.77 |
| 13:07:36 | -15 | 1.0 | 76.78 |
| 13:07:37 | -15 | 1.0 | 76.80 |
| 13:07:38 | -15 | 1.0 | 76.82 |
| 13:07:39 | -15 | 1.0 | 76.84 |
| 13:07:40 | -15 | 1.0 | 76.85 |
| 13:07:41 | -15 | 1.0 | 76.87 |
| 13:07:42 | -15 | 1.0 | 76.89 |
| 13:07:43 | -15 | 1.0 | 76.90 |
| 13:07:44 | -15 | 1.0 | 76.92 |
| 13:07:45 | -15 | 1.0 | 76.94 |
| 13:07:46 | -15 | 1.0 | 76.95 |
| 13:07:47 | -15 | 1.0 | 76.97 |
| 13:07:48 | -15 | 1.0 | 76.99 |
| 13:07:49 | -15 | 1.0 | 77.01 |
| 13:07:50 | -15 | 1.0 | 77.02 |
| 13:07:51 | -15 | 1.0 | 77.04 |
| 13:07:52 | -15 | 1.0 | 77.06 |
| 13:07:53 | -15 | 1.0 | 77.07 |
| 13:07:54 | -15 | 1.0 | 77.09 |
| 13:07:55 | -15 | 1.0 | 77.11 |
| 13:07:56 | -15 | 1.0 | 77.12 |
| 13:07:57 | -15 | 1.0 | 77.14 |
| 13:07:58 | -15 | 1.0 | 77.16 |
| 13:07:59 | -15 | 1.0 | 77.18 |
| 13:08:00 | -15 | 1.0 | 77.19 |
| 13:08:01 | -15 | 1.0 | 77.21 |
| 13:08:02 | -15 | 1.0 | 77.23 |
| 13:08:03 | -15 | 1.0 | 77.24 |
| 13:08:04 | -15 | 1.0 | 77.26 |
| 13:08:05 | -15 | 1.0 | 77.28 |
| 13:08:06 | -15 | 1.0 | 77.29 |
| 13:08:07 | -15 | 1.0 | 77.31 |
| 13:08:08 | -15 | 1.0 | 77.33 |
| 13:08:09 | -15 | 1.0 | 77.35 |
| 13:08:10 | -15 | 1.0 | 77.36 |
| 13:08:11 | -15 | 1.0 | 77.38 |
| 13:08:12 | -15 | 1.0 | 77.40 |
| 13:08:13 | -15 | 1.0 | 77.41 |
| 13:08:14 | -15 | 1.0 | 77.43 |
| 13:08:15 | -15 | 1.0 | 77.45 |
| 13:08:16 | -15 | 1.0 | 77.46 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:08:17 | -15 | 1.0 | 77.48 |
| 13:08:18 | -15 | 1.0 | 77.50 |
| 13:08:19 | -15 | 1.0 | 77.52 |
| 13:08:20 | -15 | 1.0 | 77.53 |
| 13:08:21 | -15 | 1.0 | 77.55 |
| 13:08:22 | -15 | 1.0 | 77.57 |
| 13:08:23 | -15 | 1.0 | 77.58 |
| 13:08:24 | -15 | 1.0 | 77.60 |
| 13:08:25 | -15 | 1.0 | 77.62 |
| 13:08:26 | -15 | 1.0 | 77.63 |
| 13:08:27 | -15 | 1.0 | 77.65 |
| 13:08:28 | -15 | 1.0 | 77.67 |
| 13:08:29 | -15 | 1.0 | 77.69 |
| 13:08:30 | -15 | 1.0 | 77.70 |
| 13:08:31 | -15 | 1.0 | 77.72 |
| 13:08:32 | -15 | 1.0 | 77.74 |
| 13:08:33 | -15 | 1.0 | 77.75 |
| 13:08:34 | -15 | 1.0 | 77.77 |
| 13:08:35 | -15 | 1.0 | 77.79 |
| 13:08:36 | -15 | 1.0 | 77.80 |
| 13:08:37 | -15 | 1.0 | 77.82 |
| 13:08:38 | -15 | 1.0 | 77.84 |
| 13:08:39 | -15 | 1.0 | 77.86 |
| 13:08:40 | -15 | 1.0 | 77.87 |
| 13:08:41 | -15 | 1.0 | 77.89 |
| 13:08:42 | -16 | 1.0 | 77.91 |
| 13:08:43 | -16 | 1.0 | 77.92 |
| 13:08:44 | -16 | 1.0 | 77.94 |
| 13:08:45 | -16 | 1.0 | 77.96 |
| 13:08:46 | -16 | 1.0 | 77.97 |
| 13:08:47 | -16 | 1.0 | 77.99 |
| 13:08:48 | -16 | 1.0 | 78.01 |
| 13:08:49 | -16 | 1.0 | 78.02 |
| 13:08:50 | -16 | 1.0 | 78.04 |
| 13:08:51 | -16 | 1.0 | 78.06 |
| 13:08:52 | -16 | 1.0 | 78.08 |
| 13:08:53 | -16 | 1.0 | 78.09 |
| 13:08:54 | -16 | 1.0 | 78.11 |
| 13:08:55 | -16 | 1.0 | 78.13 |
| 13:08:56 | -16 | 1.0 | 78.14 |
| 13:08:57 | -16 | 1.0 | 78.16 |
| 13:08:58 | -16 | 1.0 | 78.18 |
| 13:08:59 | -16 | 1.0 | 78.19 |
| 13:09:00 | -16 | 1.0 | 78.21 |
| 13:09:01 | -16 | 1.0 | 78.23 |
| 13:09:02 | -16 | 1.0 | 78.24 |
| 13:09:03 | -16 | 1.0 | 78.26 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:09:04 | -16 | 1.0 | 78.28 |
| 13:09:05 | -16 | 1.0 | 78.30 |
| 13:09:06 | -16 | 1.0 | 78.31 |
| 13:09:07 | -16 | 1.0 | 78.33 |
| 13:09:08 | -16 | 1.0 | 78.35 |
| 13:09:09 | -16 | 1.0 | 78.36 |
| 13:09:10 | -16 | 1.0 | 78.38 |
| 13:09:11 | -16 | 1.0 | 78.40 |
| 13:09:12 | -17 | 1.0 | 78.41 |
| 13:09:13 | -17 | 1.0 | 78.43 |
| 13:09:14 | -17 | 1.0 | 78.45 |
| 13:09:15 | -16 | 1.0 | 78.46 |
| 13:09:16 | -16 | 1.0 | 78.48 |
| 13:09:17 | -16 | 1.0 | 78.50 |
| 13:09:18 | -16 | 1.0 | 78.52 |
| 13:09:19 | -16 | 1.0 | 78.53 |
| 13:09:20 | -16 | 1.0 | 78.55 |
| 13:09:21 | -16 | 1.0 | 78.57 |
| 13:09:22 | -16 | 1.0 | 78.58 |
| 13:09:23 | -16 | 1.0 | 78.60 |
| 13:09:24 | -16 | 1.0 | 78.62 |
| 13:09:25 | -16 | 1.0 | 78.63 |
| 13:09:26 | -16 | 1.0 | 78.65 |
| 13:09:27 | -16 | 1.0 | 78.67 |
| 13:09:28 | -16 | 1.0 | 78.68 |
| 13:09:29 | -16 | 1.0 | 78.70 |
| 13:09:30 | -16 | 1.0 | 78.72 |
| 13:09:31 | -16 | 1.0 | 78.74 |
| 13:09:32 | -16 | 1.0 | 78.75 |
| 13:09:33 | -16 | 1.0 | 78.77 |
| 13:09:34 | -16 | 1.0 | 78.79 |
| 13:09:35 | -16 | 1.0 | 78.80 |
| 13:09:36 | -16 | 1.0 | 78.82 |
| 13:09:37 | -16 | 1.0 | 78.84 |
| 13:09:38 | -16 | 1.0 | 78.85 |
| 13:09:39 | -16 | 1.0 | 78.87 |
| 13:09:40 | -16 | 1.0 | 78.89 |
| 13:09:41 | -16 | 1.0 | 78.90 |
| 13:09:42 | -16 | 1.0 | 78.92 |
| 13:09:43 | -16 | 1.0 | 78.94 |
| 13:09:44 | -16 | 1.0 | 78.96 |
| 13:09:45 | -16 | 1.0 | 78.97 |
| 13:09:46 | -16 | 1.0 | 78.99 |
| 13:09:47 | -16 | 1.0 | 79.01 |
| 13:09:48 | -16 | 1.0 | 79.02 |
| 13:09:49 | -16 | 1.0 | 79.04 |
| 13:09:50 | -16 | 1.0 | 79.06 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:09:51 | -16 | 1.0 | 79.07 |
| 13:09:52 | -16 | 1.0 | 79.09 |
| 13:09:53 | -16 | 1.0 | 79.11 |
| 13:09:54 | -16 | 1.0 | 79.12 |
| 13:09:55 | -16 | 1.0 | 79.14 |
| 13:09:56 | -16 | 1.0 | 79.16 |
| 13:09:57 | -16 | 1.0 | 79.18 |
| 13:09:58 | -16 | 1.0 | 79.19 |
| 13:09:59 | -16 | 1.0 | 79.21 |
| 13:10:00 | -16 | 1.0 | 79.23 |
| 13:10:01 | -16 | 1.0 | 79.24 |
| 13:10:02 | -17 | 1.0 | 79.26 |
| 13:10:03 | -17 | 1.0 | 79.28 |
| 13:10:04 | -17 | 1.0 | 79.29 |
| 13:10:05 | -17 | 1.0 | 79.31 |
| 13:10:06 | -17 | 1.0 | 79.33 |
| 13:10:07 | -16 | 1.0 | 79.34 |
| 13:10:08 | -16 | 1.0 | 79.36 |
| 13:10:09 | -16 | 1.0 | 79.38 |
| 13:10:10 | -16 | 1.0 | 79.39 |
| 13:10:11 | -16 | 1.0 | 79.41 |
| 13:10:12 | -16 | 1.0 | 79.43 |
| 13:10:13 | -16 | 1.0 | 79.45 |
| 13:10:14 | -16 | 1.0 | 79.46 |
| 13:10:15 | -16 | 1.0 | 79.48 |
| 13:10:16 | -16 | 1.0 | 79.50 |
| 13:10:17 | -16 | 1.0 | 79.51 |
| 13:10:18 | -16 | 1.0 | 79.53 |
| 13:10:19 | -16 | 1.0 | 79.55 |
| 13:10:20 | -16 | 1.0 | 79.56 |
| 13:10:21 | -16 | 1.0 | 79.58 |
| 13:10:22 | -16 | 1.0 | 79.60 |
| 13:10:23 | -16 | 1.0 | 79.61 |
| 13:10:24 | -16 | 1.0 | 79.63 |
| 13:10:25 | -16 | 1.0 | 79.65 |
| 13:10:26 | -16 | 1.0 | 79.67 |
| 13:10:27 | -16 | 1.0 | 79.68 |
| 13:10:28 | -16 | 1.0 | 79.70 |
| 13:10:29 | -16 | 1.0 | 79.72 |
| 13:10:30 | -16 | 1.0 | 79.73 |
| 13:10:31 | -16 | 1.0 | 79.75 |
| 13:10:32 | -16 | 1.0 | 79.77 |
| 13:10:33 | -16 | 1.0 | 79.78 |
| 13:10:34 | -16 | 1.0 | 79.80 |
| 13:10:35 | -16 | 1.0 | 79.82 |
| 13:10:36 | -16 | 1.0 | 79.84 |
| 13:10:37 | -16 | 1.0 | 79.85 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:10:38 | -16 | 1.0 | 79.87 |
| 13:10:39 | -16 | 1.0 | 79.89 |
| 13:10:40 | -16 | 1.0 | 79.90 |
| 13:10:41 | -16 | 1.0 | 79.92 |
| 13:10:42 | -16 | 1.0 | 79.94 |
| 13:10:43 | -16 | 1.0 | 79.95 |
| 13:10:44 | -16 | 1.0 | 79.97 |
| 13:10:45 | -16 | 1.0 | 79.99 |
| 13:10:46 | -16 | 1.0 | 80.01 |
| 13:10:47 | -16 | 1.0 | 80.02 |
| 13:10:48 | -16 | 1.0 | 80.04 |
| 13:10:49 | -16 | 1.0 | 80.06 |
| 13:10:50 | -16 | 1.0 | 80.07 |
| 13:10:51 | -16 | 1.0 | 80.09 |
| 13:10:52 | -16 | 1.0 | 80.11 |
| 13:10:53 | -16 | 1.0 | 80.12 |
| 13:10:54 | -16 | 1.0 | 80.14 |
| 13:10:55 | -16 | 1.0 | 80.16 |
| 13:10:56 | -16 | 1.0 | 80.17 |
| 13:10:57 | -16 | 1.0 | 80.19 |
| 13:10:58 | -16 | 1.0 | 80.21 |
| 13:10:59 | -16 | 1.0 | 80.23 |
| 13:11:00 | -16 | 1.0 | 80.24 |
| 13:11:01 | -16 | 1.0 | 80.26 |
| 13:11:02 | -16 | 1.0 | 80.28 |
| 13:11:03 | -16 | 1.0 | 80.29 |
| 13:11:04 | -16 | 1.0 | 80.31 |
| 13:11:05 | -16 | 1.0 | 80.33 |
| 13:11:06 | -16 | 1.0 | 80.34 |
| 13:11:07 | -16 | 1.0 | 80.36 |
| 13:11:08 | -16 | 1.0 | 80.38 |
| 13:11:09 | -16 | 1.0 | 80.39 |
| 13:11:10 | -16 | 1.0 | 80.41 |
| 13:11:11 | -16 | 1.0 | 80.43 |
| 13:11:12 | -16 | 1.0 | 80.45 |
| 13:11:13 | -16 | 1.0 | 80.46 |
| 13:11:14 | -16 | 1.0 | 80.48 |
| 13:11:15 | -16 | 1.0 | 80.50 |
| 13:11:16 | -16 | 1.0 | 80.51 |
| 13:11:17 | -16 | 1.0 | 80.53 |
| 13:11:18 | -16 | 1.0 | 80.55 |
| 13:11:19 | -16 | 1.0 | 80.56 |
| 13:11:20 | -15 | 1.0 | 80.58 |
| 13:11:21 | -15 | 1.0 | 80.60 |
| 13:11:22 | -15 | 1.0 | 80.62 |
| 13:11:23 | -15 | 1.0 | 80.63 |
| 13:11:24 | -15 | 1.0 | 80.65 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:11:25 | -15 | 1.0 | 80.67 |
| 13:11:26 | -15 | 1.0 | 80.68 |
| 13:11:27 | -15 | 1.0 | 80.70 |
| 13:11:28 | -15 | 1.0 | 80.72 |
| 13:11:29 | -15 | 1.0 | 80.73 |
| 13:11:30 | -15 | 1.0 | 80.75 |
| 13:11:31 | -15 | 1.0 | 80.77 |
| 13:11:32 | -15 | 1.0 | 80.78 |
| 13:11:33 | -15 | 1.0 | 80.80 |
| 13:11:34 | -15 | 1.0 | 80.82 |
| 13:11:35 | -15 | 1.0 | 80.84 |
| 13:11:36 | -15 | 1.0 | 80.85 |
| 13:11:37 | -15 | 1.0 | 80.87 |
| 13:11:38 | -15 | 1.0 | 80.89 |
| 13:11:39 | -15 | 1.0 | 80.90 |
| 13:11:40 | -16 | 1.0 | 80.92 |
| 13:11:41 | -16 | 1.0 | 80.94 |
| 13:11:42 | -15 | 1.0 | 80.95 |
| 13:11:43 | -15 | 1.1 | 80.97 |
| 13:11:44 | -15 | 1.5 | 81.00 |
| 13:11:45 | -15 | 1.7 | 81.03 |
| 13:11:46 | -15 | 1.8 | 81.05 |
| 13:11:47 | -15 | 1.8 | 81.09 |
| 13:11:48 | -15 | 1.9 | 81.12 |
| 13:11:49 | -15 | 1.9 | 81.15 |
| 13:11:50 | -15 | 2.0 | 81.18 |
| 13:11:51 | -15 | 2.0 | 81.21 |
| 13:11:52 | -15 | 2.0 | 81.25 |
| 13:11:53 | -16 | 2.0 | 81.28 |
| 13:11:54 | -16 | 2.0 | 81.32 |
| 13:11:55 | -16 | 2.0 | 81.35 |
| 13:11:56 | -16 | 2.0 | 81.38 |
| 13:11:57 | -16 | 2.0 | 81.42 |
| 13:11:58 | -16 | 2.0 | 81.45 |
| 13:11:59 | -16 | 2.0 | 81.48 |
| 13:12:00 | -17 | 2.0 | 81.52 |
| 13:12:01 | -17 | 2.0 | 81.55 |
| 13:12:02 | -17 | 2.0 | 81.59 |
| 13:12:03 | -17 | 2.0 | 81.62 |
| 13:12:04 | -17 | 2.0 | 81.65 |
| 13:12:05 | -17 | 2.0 | 81.69 |
| 13:12:06 | -17 | 2.0 | 81.72 |
| 13:12:07 | -17 | 2.0 | 81.76 |
| 13:12:08 | -17 | 2.0 | 81.79 |
| 13:12:09 | -17 | 2.0 | 81.82 |
| 13:12:10 | -17 | 2.0 | 81.86 |
| 13:12:11 | -17 | 2.1 | 81.89 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:12:12 | -17 | 2.1 | 81.93 |
| 13:12:13 | -17 | 2.1 | 81.96 |
| 13:12:14 | -17 | 2.1 | 82.00 |
| 13:12:15 | -17 | 2.1 | 82.03 |
| 13:12:16 | -17 | 2.1 | 82.06 |
| 13:12:17 | -17 | 2.1 | 82.10 |
| 13:12:18 | -17 | 2.1 | 82.13 |
| 13:12:19 | -17 | 2.1 | 82.17 |
| 13:12:20 | -17 | 2.1 | 82.20 |
| 13:12:21 | -17 | 2.0 | 82.23 |
| 13:12:22 | -17 | 2.0 | 82.27 |
| 13:12:23 | -17 | 2.0 | 82.30 |
| 13:12:24 | -17 | 2.0 | 82.34 |
| 13:12:25 | -17 | 2.0 | 82.37 |
| 13:12:26 | -17 | 2.0 | 82.41 |
| 13:12:27 | -17 | 2.0 | 82.44 |
| 13:12:28 | -17 | 2.0 | 82.47 |
| 13:12:29 | -17 | 2.1 | 82.51 |
| 13:12:30 | -17 | 2.1 | 82.54 |
| 13:12:31 | -17 | 2.1 | 82.58 |
| 13:12:32 | -17 | 2.0 | 82.61 |
| 13:12:33 | -17 | 2.0 | 82.64 |
| 13:12:34 | -17 | 2.1 | 82.68 |
| 13:12:35 | -17 | 2.1 | 82.71 |
| 13:12:36 | -17 | 2.0 | 82.75 |
| 13:12:37 | -17 | 2.0 | 82.78 |
| 13:12:38 | -17 | 2.0 | 82.82 |
| 13:12:39 | -17 | 2.0 | 82.85 |
| 13:12:40 | -17 | 2.0 | 82.88 |
| 13:12:41 | -16 | 2.0 | 82.92 |
| 13:12:42 | -16 | 2.0 | 82.95 |
| 13:12:43 | -16 | 2.0 | 82.99 |
| 13:12:44 | -16 | 2.1 | 83.02 |
| 13:12:45 | -16 | 2.1 | 83.05 |
| 13:12:46 | -16 | 2.1 | 83.09 |
| 13:12:47 | -16 | 2.1 | 83.12 |
| 13:12:48 | -16 | 2.1 | 83.16 |
| 13:12:49 | -16 | 2.1 | 83.19 |
| 13:12:50 | -16 | 2.1 | 83.23 |
| 13:12:51 | -16 | 2.0 | 83.26 |
| 13:12:52 | -16 | 2.0 | 83.29 |
| 13:12:53 | -16 | 2.0 | 83.33 |
| 13:12:54 | -16 | 2.0 | 83.36 |
| 13:12:55 | -16 | 2.0 | 83.40 |
| 13:12:56 | -15 | 2.0 | 83.43 |
| 13:12:57 | -15 | 2.0 | 83.46 |
| 13:12:58 | -14 | 1.8 | 83.49 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:12:59 | -13 | 1.7 | 83.52 |
| 13:13:00 | -12 | 1.6 | 83.55 |
| 13:13:01 | -12 | 1.6 | 83.58 |
| 13:13:02 | -11 | 1.6 | 83.60 |
| 13:13:03 | -11 | 1.5 | 83.63 |
| 13:13:04 | -10 | 1.5 | 83.65 |
| 13:13:05 | -10 | 1.5 | 83.68 |
| 13:13:06 | -10 | 1.4 | 83.70 |
| 13:13:07 | -9 | 1.4 | 83.72 |
| 13:13:08 | -9 | 1.4 | 83.75 |
| 13:13:09 | -9 | 1.4 | 83.77 |
| 13:13:10 | -9 | 1.4 | 83.79 |
| 13:13:11 | -9 | 1.4 | 83.82 |
| 13:13:12 | -8 | 1.4 | 83.84 |
| 13:13:13 | -8 | 1.4 | 83.86 |
| 13:13:14 | -8 | 1.4 | 83.89 |
| 13:13:15 | -8 | 1.3 | 83.91 |
| 13:13:16 | -8 | 1.3 | 83.93 |
| 13:13:17 | -7 | 1.3 | 83.95 |
| 13:13:18 | -7 | 1.3 | 83.97 |
| 13:13:19 | -7 | 1.3 | 83.99 |
| 13:13:20 | -7 | 1.3 | 84.02 |
| 13:13:21 | -7 | 1.2 | 84.04 |
| 13:13:22 | -7 | 1.2 | 84.06 |
| 13:13:23 | -6 | 1.2 | 84.08 |
| 13:13:24 | -6 | 1.2 | 84.10 |
| 13:13:25 | -6 | 1.2 | 84.12 |
| 13:13:26 | -6 | 1.2 | 84.14 |
| 13:13:27 | -6 | 1.2 | 84.16 |
| 13:13:28 | -6 | 1.2 | 84.18 |
| 13:13:29 | -6 | 1.2 | 84.20 |
| 13:13:30 | -6 | 1.2 | 84.21 |
| 13:13:31 | -6 | 1.1 | 84.23 |
| 13:13:32 | -5 | 1.1 | 84.25 |
| 13:13:33 | -5 | 1.1 | 84.27 |
| 13:13:34 | -5 | 1.1 | 84.29 |
| 13:13:35 | -5 | 1.1 | 84.31 |
| 13:13:36 | -5 | 1.1 | 84.33 |
| 13:13:37 | -5 | 1.1 | 84.35 |
| 13:13:38 | -5 | 1.1 | 84.36 |
| 13:13:39 | -5 | 1.1 | 84.38 |
| 13:13:40 | -5 | 1.1 | 84.40 |
| 13:13:41 | -5 | 1.1 | 84.42 |
| 13:13:42 | -4 | 1.1 | 84.44 |
| 13:13:43 | -4 | 1.1 | 84.46 |
| 13:13:44 | -4 | 1.1 | 84.47 |
| 13:13:45 | -4 | 1.1 | 84.49 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:13:46 | -4 | 1.1 | 84.51 |
| 13:13:47 | -4 | 1.1 | 84.53 |
| 13:13:48 | -4 | 1.1 | 84.55 |
| 13:13:49 | -4 | 1.1 | 84.57 |
| 13:13:50 | -4 | 1.1 | 84.59 |
| 13:13:51 | -4 | 1.1 | 84.60 |
| 13:13:52 | -4 | 1.1 | 84.62 |
| 13:13:53 | -4 | 1.1 | 84.64 |
| 13:13:54 | -4 | 1.1 | 84.66 |
| 13:13:55 | -4 | 1.1 | 84.68 |
| 13:13:56 | -4 | 1.1 | 84.70 |
| 13:13:57 | -4 | 1.1 | 84.71 |
| 13:13:58 | -4 | 1.1 | 84.73 |
| 13:13:59 | -4 | 1.1 | 84.75 |
| 13:14:00 | -4 | 1.1 | 84.77 |
| 13:14:01 | -4 | 1.1 | 84.79 |
| 13:14:02 | -4 | 1.1 | 84.81 |
| 13:14:03 | -4 | 1.1 | 84.83 |
| 13:14:04 | -3 | 1.1 | 84.84 |
| 13:14:05 | -3 | 1.1 | 84.86 |
| 13:14:06 | -3 | 1.1 | 84.88 |
| 13:14:07 | -3 | 1.1 | 84.90 |
| 13:14:08 | -3 | 1.1 | 84.92 |
| 13:14:09 | -3 | 1.1 | 84.94 |
| 13:14:10 | -3 | 1.1 | 84.95 |
| 13:14:11 | -2 | 1.1 | 84.97 |
| 13:14:12 | -2 | 1.1 | 84.99 |
| 13:14:13 | -2 | 1.1 | 85.01 |
| 13:14:14 | -2 | 1.1 | 85.03 |
| 13:14:15 | -2 | 1.1 | 85.05 |
| 13:14:16 | -1 | 1.1 | 85.07 |
| 13:14:17 | -1 | 1.1 | 85.09 |
| 13:14:18 | -1 | 1.1 | 85.10 |
| 13:14:19 | -1 | 1.1 | 85.12 |
| 13:14:20 | 1 | 1.2 | 85.14 |
| 13:14:21 | 5 | 1.4 | 85.17 |
| 13:14:22 | 9 | 1.6 | 85.19 |
| 13:14:23 | 12 | 1.7 | 85.22 |
| 13:14:24 | 16 | 1.8 | 85.25 |
| 13:14:25 | 18 | 1.9 | 85.28 |
| 13:14:26 | 21 | 1.9 | 85.32 |
| 13:14:27 | 23 | 1.9 | 85.35 |
| 13:14:28 | 25 | 1.9 | 85.38 |
| 13:14:29 | 28 | 2.0 | 85.41 |
| 13:14:30 | 29 | 2.0 | 85.45 |
| 13:14:31 | 31 | 2.0 | 85.48 |
| 13:14:32 | 32 | 2.0 | 85.51 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:14:33 | 34 | 2.0 | 85.55 |
| 13:14:34 | 36 | 2.0 | 85.58 |
| 13:14:35 | 37 | 2.1 | 85.61 |
| 13:14:36 | 38 | 2.1 | 85.65 |
| 13:14:37 | 40 | 2.1 | 85.68 |
| 13:14:38 | 42 | 2.1 | 85.72 |
| 13:14:39 | 43 | 2.1 | 85.75 |
| 13:14:40 | 45 | 2.1 | 85.79 |
| 13:14:41 | 46 | 2.1 | 85.82 |
| 13:14:42 | 48 | 2.1 | 85.86 |
| 13:14:43 | 50 | 2.1 | 85.89 |
| 13:14:44 | 52 | 2.1 | 85.92 |
| 13:14:45 | 53 | 2.1 | 85.96 |
| 13:14:46 | 54 | 2.1 | 85.99 |
| 13:14:47 | 56 | 2.1 | 86.03 |
| 13:14:48 | 57 | 2.1 | 86.06 |
| 13:14:49 | 59 | 2.1 | 86.10 |
| 13:14:50 | 60 | 2.1 | 86.13 |
| 13:14:51 | 62 | 2.1 | 86.17 |
| 13:14:52 | 63 | 2.1 | 86.20 |
| 13:14:53 | 65 | 2.1 | 86.23 |
| 13:14:54 | 66 | 2.1 | 86.27 |
| 13:14:55 | 67 | 2.1 | 86.30 |
| 13:14:56 | 69 | 2.1 | 86.34 |
| 13:14:57 | 70 | 2.1 | 86.37 |
| 13:14:58 | 71 | 2.1 | 86.41 |
| 13:14:59 | 73 | 2.1 | 86.44 |
| 13:15:00 | 74 | 2.1 | 86.48 |
| 13:15:01 | 75 | 2.1 | 86.51 |
| 13:15:02 | 77 | 2.1 | 86.54 |
| 13:15:03 | 78 | 2.1 | 86.58 |
| 13:15:04 | 79 | 2.1 | 86.61 |
| 13:15:05 | 80 | 2.1 | 86.65 |
| 13:15:06 | 82 | 2.1 | 86.68 |
| 13:15:07 | 83 | 2.1 | 86.72 |
| 13:15:08 | 85 | 2.1 | 86.75 |
| 13:15:09 | 86 | 2.1 | 86.79 |
| 13:15:10 | 87 | 2.1 | 86.82 |
| 13:15:11 | 88 | 2.1 | 86.85 |
| 13:15:12 | 89 | 2.1 | 86.89 |
| 13:15:13 | 91 | 2.1 | 86.92 |
| 13:15:14 | 92 | 2.1 | 86.96 |
| 13:15:15 | 93 | 2.1 | 86.99 |
| 13:15:16 | 94 | 2.1 | 87.03 |
| 13:15:17 | 95 | 2.1 | 87.06 |
| 13:15:18 | 96 | 2.1 | 87.09 |
| 13:15:19 | 97 | 2.1 | 87.13 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:15:20 | 99 | 2.1 | 87.16 |
| 13:15:21 | 100 | 2.1 | 87.20 |
| 13:15:22 | 101 | 2.1 | 87.23 |
| 13:15:23 | 102 | 2.1 | 87.27 |
| 13:15:24 | 103 | 2.1 | 87.30 |
| 13:15:25 | 104 | 2.1 | 87.34 |
| 13:15:26 | 105 | 2.1 | 87.37 |
| 13:15:27 | 106 | 2.1 | 87.40 |
| 13:15:28 | 107 | 2.1 | 87.44 |
| 13:15:29 | 108 | 2.1 | 87.47 |
| 13:15:30 | 109 | 2.1 | 87.51 |
| 13:15:31 | 110 | 2.1 | 87.54 |
| 13:15:32 | 111 | 2.1 | 87.58 |
| 13:15:33 | 112 | 2.1 | 87.61 |
| 13:15:34 | 113 | 2.1 | 87.64 |
| 13:15:35 | 114 | 2.1 | 87.68 |
| 13:15:36 | 115 | 2.1 | 87.71 |
| 13:15:37 | 116 | 2.1 | 87.75 |
| 13:15:38 | 117 | 2.1 | 87.78 |
| 13:15:39 | 118 | 2.1 | 87.82 |
| 13:15:40 | 119 | 2.1 | 87.85 |
| 13:15:41 | 120 | 2.1 | 87.88 |
| 13:15:42 | 121 | 2.1 | 87.92 |
| 13:15:43 | 122 | 2.1 | 87.95 |
| 13:15:44 | 123 | 2.1 | 87.99 |
| 13:15:45 | 124 | 2.1 | 88.02 |
| 13:15:46 | 125 | 2.1 | 88.06 |
| 13:15:47 | 126 | 2.1 | 88.09 |
| 13:15:48 | 127 | 2.1 | 88.12 |
| 13:15:49 | 128 | 2.1 | 88.16 |
| 13:15:50 | 129 | 2.1 | 88.19 |
| 13:15:51 | 130 | 2.1 | 88.23 |
| 13:15:52 | 131 | 2.1 | 88.26 |
| 13:15:53 | 131 | 2.1 | 88.30 |
| 13:15:54 | 132 | 2.1 | 88.33 |
| 13:15:55 | 133 | 2.1 | 88.36 |
| 13:15:56 | 134 | 2.1 | 88.40 |
| 13:15:57 | 135 | 2.1 | 88.43 |
| 13:15:58 | 136 | 2.1 | 88.47 |
| 13:15:59 | 136 | 2.1 | 88.50 |
| 13:16:00 | 137 | 2.1 | 88.54 |
| 13:16:01 | 138 | 2.1 | 88.57 |
| 13:16:02 | 139 | 2.1 | 88.60 |
| 13:16:03 | 140 | 2.1 | 88.64 |
| 13:16:04 | 141 | 2.1 | 88.67 |
| 13:16:05 | 142 | 2.1 | 88.71 |
| 13:16:06 | 143 | 2.1 | 88.74 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:16:07 | 143 | 2.1 | 88.77 |
| 13:16:08 | 144 | 2.1 | 88.81 |
| 13:16:09 | 145 | 2.1 | 88.84 |
| 13:16:10 | 146 | 2.1 | 88.88 |
| 13:16:11 | 147 | 2.1 | 88.91 |
| 13:16:12 | 148 | 2.1 | 88.95 |
| 13:16:13 | 149 | 2.1 | 88.98 |
| 13:16:14 | 149 | 2.1 | 89.01 |
| 13:16:15 | 150 | 2.1 | 89.05 |
| 13:16:16 | 151 | 2.1 | 89.08 |
| 13:16:17 | 152 | 2.1 | 89.12 |
| 13:16:18 | 152 | 2.1 | 89.15 |
| 13:16:19 | 153 | 2.1 | 89.19 |
| 13:16:20 | 154 | 2.1 | 89.22 |
| 13:16:21 | 155 | 2.1 | 89.25 |
| 13:16:22 | 156 | 2.1 | 89.29 |
| 13:16:23 | 156 | 2.1 | 89.32 |
| 13:16:24 | 157 | 2.1 | 89.36 |
| 13:16:25 | 158 | 2.1 | 89.39 |
| 13:16:26 | 159 | 2.1 | 89.43 |
| 13:16:27 | 159 | 2.1 | 89.46 |
| 13:16:28 | 160 | 2.1 | 89.49 |
| 13:16:29 | 161 | 2.1 | 89.53 |
| 13:16:30 | 161 | 2.1 | 89.56 |
| 13:16:31 | 162 | 2.1 | 89.60 |
| 13:16:32 | 163 | 2.1 | 89.63 |
| 13:16:33 | 164 | 2.1 | 89.67 |
| 13:16:34 | 165 | 2.1 | 89.70 |
| 13:16:35 | 166 | 2.1 | 89.73 |
| 13:16:36 | 166 | 2.1 | 89.77 |
| 13:16:37 | 167 | 2.1 | 89.80 |
| 13:16:38 | 168 | 2.1 | 89.84 |
| 13:16:39 | 168 | 2.1 | 89.87 |
| 13:16:40 | 169 | 2.1 | 89.90 |
| 13:16:41 | 170 | 2.1 | 89.94 |
| 13:16:42 | 170 | 2.1 | 89.97 |
| 13:16:43 | 171 | 2.1 | 90.01 |
| 13:16:44 | 172 | 2.1 | 90.04 |
| 13:16:45 | 173 | 2.1 | 90.08 |
| 13:16:46 | 174 | 2.1 | 90.11 |
| 13:16:47 | 174 | 2.1 | 90.14 |
| 13:16:48 | 175 | 2.1 | 90.18 |
| 13:16:49 | 176 | 2.1 | 90.21 |
| 13:16:50 | 176 | 2.1 | 90.25 |
| 13:16:51 | 177 | 2.1 | 90.28 |
| 13:16:52 | 178 | 2.1 | 90.31 |
| 13:16:53 | 179 | 2.1 | 90.35 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:16:54 | 179 | 2.1 | 90.38 |
| 13:16:55 | 180 | 2.1 | 90.42 |
| 13:16:56 | 181 | 2.1 | 90.45 |
| 13:16:57 | 182 | 2.1 | 90.49 |
| 13:16:58 | 182 | 2.1 | 90.52 |
| 13:16:59 | 183 | 2.1 | 90.55 |
| 13:17:00 | 184 | 2.1 | 90.59 |
| 13:17:01 | 184 | 2.1 | 90.62 |
| 13:17:02 | 185 | 2.1 | 90.66 |
| 13:17:03 | 186 | 2.1 | 90.69 |
| 13:17:04 | 186 | 2.1 | 90.73 |
| 13:17:05 | 187 | 2.1 | 90.76 |
| 13:17:06 | 188 | 2.1 | 90.79 |
| 13:17:07 | 189 | 2.1 | 90.83 |
| 13:17:08 | 190 | 2.1 | 90.86 |
| 13:17:09 | 191 | 2.1 | 90.90 |
| 13:17:10 | 191 | 2.1 | 90.93 |
| 13:17:11 | 192 | 2.1 | 90.96 |
| 13:17:12 | 193 | 2.1 | 91.00 |
| 13:17:13 | 193 | 2.1 | 91.03 |
| 13:17:14 | 194 | 2.1 | 91.07 |
| 13:17:15 | 195 | 2.1 | 91.10 |
| 13:17:16 | 195 | 2.1 | 91.14 |
| 13:17:17 | 196 | 2.1 | 91.17 |
| 13:17:18 | 197 | 2.1 | 91.20 |
| 13:17:19 | 198 | 2.1 | 91.24 |
| 13:17:20 | 199 | 2.1 | 91.27 |
| 13:17:21 | 199 | 2.1 | 91.31 |
| 13:17:22 | 200 | 2.1 | 91.34 |
| 13:17:23 | 201 | 2.1 | 91.37 |
| 13:17:24 | 201 | 2.0 | 91.41 |
| 13:17:25 | 202 | 2.0 | 91.44 |
| 13:17:26 | 203 | 2.0 | 91.48 |
| 13:17:27 | 203 | 2.0 | 91.51 |
| 13:17:28 | 204 | 2.0 | 91.55 |
| 13:17:29 | 205 | 2.0 | 91.58 |
| 13:17:30 | 206 | 2.0 | 91.61 |
| 13:17:31 | 206 | 2.0 | 91.65 |
| 13:17:32 | 207 | 2.0 | 91.68 |
| 13:17:33 | 208 | 2.0 | 91.72 |
| 13:17:34 | 209 | 2.0 | 91.75 |
| 13:17:35 | 209 | 2.0 | 91.78 |
| 13:17:36 | 210 | 2.0 | 91.82 |
| 13:17:37 | 210 | 2.0 | 91.85 |
| 13:17:38 | 211 | 2.0 | 91.89 |
| 13:17:39 | 211 | 2.0 | 91.92 |
| 13:17:40 | 212 | 2.0 | 91.95 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:17:41 | 213 | 2.0 | 91.99 |
| 13:17:42 | 213 | 2.0 | 92.02 |
| 13:17:43 | 214 | 2.0 | 92.06 |
| 13:17:44 | 215 | 2.0 | 92.09 |
| 13:17:45 | 215 | 2.0 | 92.13 |
| 13:17:46 | 216 | 2.0 | 92.16 |
| 13:17:47 | 216 | 2.0 | 92.19 |
| 13:17:48 | 216 | 2.0 | 92.23 |
| 13:17:49 | 217 | 2.0 | 92.26 |
| 13:17:50 | 217 | 2.0 | 92.30 |
| 13:17:51 | 218 | 2.0 | 92.33 |
| 13:17:52 | 218 | 2.0 | 92.36 |
| 13:17:53 | 219 | 2.0 | 92.40 |
| 13:17:54 | 220 | 2.0 | 92.43 |
| 13:17:55 | 220 | 2.0 | 92.47 |
| 13:17:56 | 221 | 2.0 | 92.50 |
| 13:17:57 | 221 | 2.0 | 92.53 |
| 13:17:58 | 222 | 2.0 | 92.57 |
| 13:17:59 | 222 | 2.0 | 92.60 |
| 13:18:00 | 223 | 2.0 | 92.64 |
| 13:18:01 | 223 | 2.0 | 92.67 |
| 13:18:02 | 223 | 2.0 | 92.70 |
| 13:18:03 | 224 | 2.0 | 92.74 |
| 13:18:04 | 224 | 2.0 | 92.77 |
| 13:18:05 | 225 | 2.0 | 92.81 |
| 13:18:06 | 226 | 2.0 | 92.84 |
| 13:18:07 | 226 | 2.0 | 92.87 |
| 13:18:08 | 227 | 2.0 | 92.91 |
| 13:18:09 | 227 | 2.0 | 92.94 |
| 13:18:10 | 228 | 2.0 | 92.98 |
| 13:18:11 | 228 | 2.0 | 93.01 |
| 13:18:12 | 228 | 2.0 | 93.05 |
| 13:18:13 | 229 | 2.0 | 93.08 |
| 13:18:14 | 229 | 2.0 | 93.11 |
| 13:18:15 | 230 | 2.0 | 93.15 |
| 13:18:16 | 230 | 2.0 | 93.18 |
| 13:18:17 | 231 | 2.0 | 93.22 |
| 13:18:18 | 231 | 2.0 | 93.25 |
| 13:18:19 | 232 | 2.0 | 93.28 |
| 13:18:20 | 233 | 2.0 | 93.32 |
| 13:18:21 | 233 | 2.0 | 93.35 |
| 13:18:22 | 234 | 2.0 | 93.39 |
| 13:18:23 | 234 | 2.0 | 93.42 |
| 13:18:24 | 235 | 2.0 | 93.45 |
| 13:18:25 | 235 | 2.0 | 93.49 |
| 13:18:26 | 235 | 2.0 | 93.52 |
| 13:18:27 | 236 | 2.0 | 93.56 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:18:28 | 236 | 2.0 | 93.59 |
| 13:18:29 | 237 | 2.0 | 93.62 |
| 13:18:30 | 237 | 2.0 | 93.66 |
| 13:18:31 | 238 | 2.0 | 93.69 |
| 13:18:32 | 239 | 2.0 | 93.73 |
| 13:18:33 | 239 | 2.0 | 93.76 |
| 13:18:34 | 240 | 2.0 | 93.79 |
| 13:18:35 | 241 | 2.0 | 93.83 |
| 13:18:36 | 241 | 2.0 | 93.86 |
| 13:18:37 | 241 | 2.0 | 93.90 |
| 13:18:38 | 242 | 2.0 | 93.93 |
| 13:18:39 | 242 | 2.0 | 93.96 |
| 13:18:40 | 242 | 2.0 | 94.00 |
| 13:18:41 | 243 | 2.0 | 94.03 |
| 13:18:42 | 244 | 2.0 | 94.07 |
| 13:18:43 | 244 | 2.0 | 94.10 |
| 13:18:44 | 245 | 2.0 | 94.13 |
| 13:18:45 | 246 | 2.0 | 94.17 |
| 13:18:46 | 246 | 2.0 | 94.20 |
| 13:18:47 | 247 | 2.0 | 94.24 |
| 13:18:48 | 247 | 2.0 | 94.27 |
| 13:18:49 | 247 | 2.0 | 94.30 |
| 13:18:50 | 248 | 2.0 | 94.34 |
| 13:18:51 | 248 | 2.0 | 94.37 |
| 13:18:52 | 248 | 2.0 | 94.41 |
| 13:18:53 | 249 | 2.0 | 94.44 |
| 13:18:54 | 249 | 2.0 | 94.47 |
| 13:18:55 | 250 | 2.0 | 94.51 |
| 13:18:56 | 251 | 2.0 | 94.54 |
| 13:18:57 | 251 | 2.0 | 94.58 |
| 13:18:58 | 252 | 2.0 | 94.61 |
| 13:18:59 | 252 | 2.0 | 94.64 |
| 13:19:00 | 253 | 2.0 | 94.68 |
| 13:19:01 | 253 | 2.0 | 94.71 |
| 13:19:02 | 254 | 2.0 | 94.75 |
| 13:19:03 | 254 | 2.0 | 94.78 |
| 13:19:04 | 254 | 2.0 | 94.81 |
| 13:19:05 | 255 | 2.0 | 94.85 |
| 13:19:06 | 255 | 2.0 | 94.88 |
| 13:19:07 | 256 | 2.0 | 94.92 |
| 13:19:08 | 256 | 2.0 | 94.95 |
| 13:19:09 | 257 | 2.0 | 94.98 |
| 13:19:10 | 257 | 2.0 | 95.02 |
| 13:19:11 | 258 | 2.0 | 95.05 |
| 13:19:12 | 259 | 2.0 | 95.09 |
| 13:19:13 | 259 | 2.0 | 95.12 |
| 13:19:14 | 260 | 2.0 | 95.15 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:19:15 | 260 | 2.0 | 95.19 |
| 13:19:16 | 260 | 2.0 | 95.22 |
| 13:19:17 | 261 | 2.0 | 95.26 |
| 13:19:18 | 261 | 2.0 | 95.29 |
| 13:19:19 | 261 | 2.0 | 95.32 |
| 13:19:20 | 262 | 2.0 | 95.36 |
| 13:19:21 | 262 | 2.0 | 95.39 |
| 13:19:22 | 263 | 2.0 | 95.43 |
| 13:19:23 | 264 | 2.0 | 95.46 |
| 13:19:24 | 264 | 2.0 | 95.49 |
| 13:19:25 | 265 | 2.0 | 95.53 |
| 13:19:26 | 265 | 2.0 | 95.56 |
| 13:19:27 | 266 | 2.0 | 95.60 |
| 13:19:28 | 266 | 2.0 | 95.63 |
| 13:19:29 | 266 | 2.0 | 95.66 |
| 13:19:30 | 267 | 2.0 | 95.70 |
| 13:19:31 | 267 | 2.0 | 95.73 |
| 13:19:32 | 267 | 2.0 | 95.76 |
| 13:19:33 | 268 | 2.0 | 95.80 |
| 13:19:34 | 268 | 2.0 | 95.83 |
| 13:19:35 | 269 | 2.0 | 95.87 |
| 13:19:36 | 270 | 2.0 | 95.90 |
| 13:19:37 | 270 | 2.0 | 95.93 |
| 13:19:38 | 271 | 2.0 | 95.97 |
| 13:19:39 | 271 | 2.0 | 96.00 |
| 13:19:40 | 272 | 2.0 | 96.04 |
| 13:19:41 | 272 | 2.0 | 96.07 |
| 13:19:42 | 272 | 2.0 | 96.10 |
| 13:19:43 | 273 | 2.0 | 96.14 |
| 13:19:44 | 273 | 2.0 | 96.17 |
| 13:19:45 | 273 | 2.0 | 96.21 |
| 13:19:46 | 274 | 2.0 | 96.24 |
| 13:19:47 | 274 | 2.0 | 96.27 |
| 13:19:48 | 275 | 2.0 | 96.31 |
| 13:19:49 | 276 | 2.0 | 96.34 |
| 13:19:50 | 276 | 2.0 | 96.38 |
| 13:19:51 | 277 | 2.0 | 96.41 |
| 13:19:52 | 277 | 2.0 | 96.44 |
| 13:19:53 | 278 | 2.0 | 96.48 |
| 13:19:54 | 278 | 2.0 | 96.51 |
| 13:19:55 | 278 | 2.0 | 96.55 |
| 13:19:56 | 279 | 2.0 | 96.58 |
| 13:19:57 | 279 | 2.0 | 96.61 |
| 13:19:58 | 280 | 2.0 | 96.65 |
| 13:19:59 | 280 | 2.0 | 96.68 |
| 13:20:00 | 280 | 2.0 | 96.72 |
| 13:20:01 | 281 | 2.0 | 96.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:20:02 | 281 | 2.0 | 96.78 |
| 13:20:03 | 282 | 2.0 | 96.82 |
| 13:20:04 | 283 | 2.0 | 96.85 |
| 13:20:05 | 283 | 2.0 | 96.89 |
| 13:20:06 | 284 | 2.0 | 96.92 |
| 13:20:07 | 284 | 2.0 | 96.95 |
| 13:20:08 | 284 | 2.0 | 96.99 |
| 13:20:09 | 285 | 2.0 | 97.02 |
| 13:20:10 | 285 | 2.0 | 97.06 |
| 13:20:11 | 285 | 2.0 | 97.09 |
| 13:20:12 | 285 | 2.0 | 97.12 |
| 13:20:13 | 286 | 2.0 | 97.16 |
| 13:20:14 | 286 | 2.0 | 97.19 |
| 13:20:15 | 287 | 2.0 | 97.23 |
| 13:20:16 | 287 | 2.0 | 97.26 |
| 13:20:17 | 288 | 2.0 | 97.29 |
| 13:20:18 | 288 | 2.0 | 97.33 |
| 13:20:19 | 289 | 2.0 | 97.36 |
| 13:20:20 | 289 | 2.0 | 97.40 |
| 13:20:21 | 290 | 2.0 | 97.43 |
| 13:20:22 | 290 | 2.0 | 97.46 |
| 13:20:23 | 290 | 2.0 | 97.50 |
| 13:20:24 | 291 | 2.0 | 97.53 |
| 13:20:25 | 291 | 2.0 | 97.57 |
| 13:20:26 | 291 | 2.0 | 97.60 |
| 13:20:27 | 292 | 2.0 | 97.63 |
| 13:20:28 | 292 | 2.0 | 97.67 |
| 13:20:29 | 292 | 2.0 | 97.70 |
| 13:20:30 | 293 | 2.0 | 97.74 |
| 13:20:31 | 293 | 2.0 | 97.77 |
| 13:20:32 | 294 | 2.0 | 97.80 |
| 13:20:33 | 294 | 2.0 | 97.84 |
| 13:20:34 | 295 | 2.0 | 97.87 |
| 13:20:35 | 295 | 2.0 | 97.91 |
| 13:20:36 | 296 | 2.0 | 97.94 |
| 13:20:37 | 296 | 2.0 | 97.97 |
| 13:20:38 | 296 | 2.0 | 98.01 |
| 13:20:39 | 296 | 2.0 | 98.04 |
| 13:20:40 | 297 | 2.0 | 98.08 |
| 13:20:41 | 297 | 2.0 | 98.11 |
| 13:20:42 | 298 | 2.0 | 98.14 |
| 13:20:43 | 298 | 2.0 | 98.18 |
| 13:20:44 | 299 | 2.0 | 98.21 |
| 13:20:45 | 299 | 2.0 | 98.25 |
| 13:20:46 | 300 | 2.0 | 98.28 |
| 13:20:47 | 300 | 2.0 | 98.31 |
| 13:20:48 | 300 | 2.0 | 98.35 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:20:49 | 301 | 2.0 | 98.38 |
| 13:20:50 | 301 | 2.0 | 98.42 |
| 13:20:51 | 301 | 2.0 | 98.45 |
| 13:20:52 | 302 | 2.0 | 98.48 |
| 13:20:53 | 302 | 2.0 | 98.52 |
| 13:20:54 | 302 | 2.0 | 98.55 |
| 13:20:55 | 303 | 2.0 | 98.59 |
| 13:20:56 | 303 | 2.0 | 98.62 |
| 13:20:57 | 304 | 2.0 | 98.65 |
| 13:20:58 | 304 | 2.0 | 98.69 |
| 13:20:59 | 305 | 2.0 | 98.72 |
| 13:21:00 | 306 | 2.0 | 98.76 |
| 13:21:01 | 306 | 2.0 | 98.79 |
| 13:21:02 | 306 | 2.0 | 98.82 |
| 13:21:03 | 307 | 2.0 | 98.86 |
| 13:21:04 | 307 | 2.0 | 98.89 |
| 13:21:05 | 307 | 2.0 | 98.93 |
| 13:21:06 | 307 | 2.0 | 98.96 |
| 13:21:07 | 308 | 2.0 | 98.99 |
| 13:21:08 | 308 | 2.0 | 99.03 |
| 13:21:09 | 308 | 2.0 | 99.06 |
| 13:21:10 | 309 | 2.0 | 99.10 |
| 13:21:11 | 309 | 2.0 | 99.13 |
| 13:21:12 | 310 | 2.0 | 99.16 |
| 13:21:13 | 311 | 2.0 | 99.20 |
| 13:21:14 | 311 | 2.0 | 99.23 |
| 13:21:15 | 312 | 2.0 | 99.27 |
| 13:21:16 | 312 | 2.0 | 99.30 |
| 13:21:17 | 312 | 2.0 | 99.33 |
| 13:21:18 | 313 | 2.0 | 99.37 |
| 13:21:19 | 313 | 2.0 | 99.40 |
| 13:21:20 | 313 | 2.0 | 99.44 |
| 13:21:21 | 313 | 2.0 | 99.47 |
| 13:21:22 | 314 | 2.0 | 99.50 |
| 13:21:23 | 314 | 2.0 | 99.54 |
| 13:21:24 | 315 | 2.0 | 99.57 |
| 13:21:25 | 315 | 2.0 | 99.61 |
| 13:21:26 | 316 | 2.0 | 99.64 |
| 13:21:27 | 316 | 2.0 | 99.67 |
| 13:21:28 | 317 | 2.0 | 99.71 |
| 13:21:29 | 317 | 2.0 | 99.74 |
| 13:21:30 | 318 | 2.0 | 99.78 |
| 13:21:31 | 318 | 2.0 | 99.81 |
| 13:21:32 | 318 | 2.0 | 99.84 |
| 13:21:33 | 319 | 2.0 | 99.88 |
| 13:21:34 | 319 | 2.0 | 99.91 |
| 13:21:35 | 319 | 2.0 | 99.95 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:21:36 | 319 | 2.0 | 99.98 |
| 13:21:37 | 319 | 2.0 | 100.01 |
| 13:21:38 | 320 | 2.0 | 100.05 |
| 13:21:39 | 320 | 2.0 | 100.08 |
| 13:21:40 | 321 | 2.0 | 100.12 |
| 13:21:41 | 321 | 2.0 | 100.15 |
| 13:21:42 | 322 | 2.0 | 100.18 |
| 13:21:43 | 322 | 2.0 | 100.22 |
| 13:21:44 | 323 | 2.0 | 100.25 |
| 13:21:45 | 323 | 2.0 | 100.29 |
| 13:21:46 | 324 | 2.0 | 100.32 |
| 13:21:47 | 324 | 2.0 | 100.35 |
| 13:21:48 | 324 | 2.0 | 100.39 |
| 13:21:49 | 325 | 2.0 | 100.42 |
| 13:21:50 | 325 | 2.0 | 100.46 |
| 13:21:51 | 325 | 2.0 | 100.49 |
| 13:21:52 | 325 | 2.0 | 100.52 |
| 13:21:53 | 326 | 2.0 | 100.56 |
| 13:21:54 | 326 | 2.0 | 100.59 |
| 13:21:55 | 326 | 2.0 | 100.62 |
| 13:21:56 | 327 | 2.0 | 100.66 |
| 13:21:57 | 327 | 2.0 | 100.69 |
| 13:21:58 | 328 | 2.0 | 100.73 |
| 13:21:59 | 329 | 2.0 | 100.76 |
| 13:22:00 | 329 | 2.0 | 100.79 |
| 13:22:01 | 329 | 2.0 | 100.83 |
| 13:22:02 | 330 | 2.0 | 100.86 |
| 13:22:03 | 330 | 2.0 | 100.90 |
| 13:22:04 | 330 | 2.0 | 100.93 |
| 13:22:05 | 330 | 2.0 | 100.96 |
| 13:22:06 | 330 | 2.0 | 101.00 |
| 13:22:07 | 331 | 2.0 | 101.03 |
| 13:22:08 | 331 | 2.0 | 101.07 |
| 13:22:09 | 332 | 2.0 | 101.10 |
| 13:22:10 | 332 | 2.0 | 101.13 |
| 13:22:11 | 332 | 2.0 | 101.17 |
| 13:22:12 | 333 | 2.0 | 101.20 |
| 13:22:13 | 333 | 2.0 | 101.24 |
| 13:22:14 | 334 | 2.0 | 101.27 |
| 13:22:15 | 334 | 2.0 | 101.30 |
| 13:22:16 | 335 | 2.0 | 101.34 |
| 13:22:17 | 335 | 2.0 | 101.37 |
| 13:22:18 | 335 | 2.0 | 101.41 |
| 13:22:19 | 335 | 2.0 | 101.44 |
| 13:22:20 | 335 | 2.0 | 101.47 |
| 13:22:21 | 336 | 2.0 | 101.51 |
| 13:22:22 | 336 | 2.0 | 101.54 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:22:23 | 336 | 2.0 | 101.58 |
| 13:22:24 | 337 | 2.0 | 101.61 |
| 13:22:25 | 337 | 2.0 | 101.64 |
| 13:22:26 | 338 | 2.0 | 101.68 |
| 13:22:27 | 338 | 2.0 | 101.71 |
| 13:22:28 | 339 | 2.0 | 101.75 |
| 13:22:29 | 339 | 2.0 | 101.78 |
| 13:22:30 | 340 | 2.0 | 101.81 |
| 13:22:31 | 340 | 2.0 | 101.85 |
| 13:22:32 | 340 | 2.0 | 101.88 |
| 13:22:33 | 340 | 2.0 | 101.91 |
| 13:22:34 | 340 | 2.0 | 101.95 |
| 13:22:35 | 340 | 2.0 | 101.98 |
| 13:22:36 | 341 | 2.0 | 102.02 |
| 13:22:37 | 341 | 2.0 | 102.05 |
| 13:22:38 | 341 | 2.0 | 102.08 |
| 13:22:39 | 342 | 2.0 | 102.12 |
| 13:22:40 | 342 | 2.0 | 102.15 |
| 13:22:41 | 342 | 2.0 | 102.19 |
| 13:22:42 | 343 | 2.0 | 102.22 |
| 13:22:43 | 343 | 2.0 | 102.25 |
| 13:22:44 | 344 | 2.0 | 102.29 |
| 13:22:45 | 345 | 2.0 | 102.32 |
| 13:22:46 | 345 | 2.0 | 102.36 |
| 13:22:47 | 345 | 2.0 | 102.39 |
| 13:22:48 | 346 | 2.0 | 102.42 |
| 13:22:49 | 346 | 2.0 | 102.46 |
| 13:22:50 | 346 | 2.0 | 102.49 |
| 13:22:51 | 346 | 2.0 | 102.53 |
| 13:22:52 | 346 | 2.0 | 102.56 |
| 13:22:53 | 346 | 2.0 | 102.59 |
| 13:22:54 | 347 | 2.0 | 102.63 |
| 13:22:55 | 347 | 2.0 | 102.66 |
| 13:22:56 | 347 | 2.0 | 102.69 |
| 13:22:57 | 348 | 2.0 | 102.73 |
| 13:22:58 | 348 | 2.0 | 102.76 |
| 13:22:59 | 349 | 2.0 | 102.80 |
| 13:23:00 | 349 | 2.0 | 102.83 |
| 13:23:01 | 350 | 2.0 | 102.86 |
| 13:23:02 | 350 | 2.0 | 102.90 |
| 13:23:03 | 350 | 2.0 | 102.93 |
| 13:23:04 | 350 | 2.0 | 102.97 |
| 13:23:05 | 350 | 2.0 | 103.00 |
| 13:23:06 | 351 | 2.0 | 103.03 |
| 13:23:07 | 351 | 2.0 | 103.07 |
| 13:23:08 | 351 | 2.0 | 103.10 |
| 13:23:09 | 351 | 2.0 | 103.13 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:23:10 | 352 | 2.0 | 103.17 |
| 13:23:11 | 352 | 2.0 | 103.20 |
| 13:23:12 | 353 | 2.0 | 103.24 |
| 13:23:13 | 353 | 2.0 | 103.27 |
| 13:23:14 | 354 | 2.0 | 103.30 |
| 13:23:15 | 355 | 2.0 | 103.34 |
| 13:23:16 | 355 | 2.0 | 103.37 |
| 13:23:17 | 356 | 2.0 | 103.41 |
| 13:23:18 | 356 | 2.0 | 103.44 |
| 13:23:19 | 356 | 2.0 | 103.47 |
| 13:23:20 | 356 | 2.0 | 103.51 |
| 13:23:21 | 356 | 2.0 | 103.54 |
| 13:23:22 | 356 | 2.0 | 103.57 |
| 13:23:23 | 356 | 2.0 | 103.61 |
| 13:23:24 | 357 | 2.0 | 103.64 |
| 13:23:25 | 357 | 2.0 | 103.68 |
| 13:23:26 | 357 | 2.0 | 103.71 |
| 13:23:27 | 357 | 2.0 | 103.74 |
| 13:23:28 | 358 | 2.0 | 103.78 |
| 13:23:29 | 358 | 2.0 | 103.81 |
| 13:23:30 | 359 | 2.0 | 103.85 |
| 13:23:31 | 360 | 2.0 | 103.88 |
| 13:23:32 | 360 | 2.0 | 103.91 |
| 13:23:33 | 361 | 2.0 | 103.95 |
| 13:23:34 | 361 | 2.0 | 103.98 |
| 13:23:35 | 361 | 2.0 | 104.01 |
| 13:23:36 | 361 | 2.0 | 104.05 |
| 13:23:37 | 361 | 2.0 | 104.08 |
| 13:23:38 | 362 | 2.0 | 104.12 |
| 13:23:39 | 362 | 2.0 | 104.15 |
| 13:23:40 | 362 | 2.0 | 104.18 |
| 13:23:41 | 362 | 2.0 | 104.22 |
| 13:23:42 | 363 | 2.0 | 104.25 |
| 13:23:43 | 364 | 2.0 | 104.29 |
| 13:23:44 | 364 | 2.0 | 104.32 |
| 13:23:45 | 365 | 2.0 | 104.35 |
| 13:23:46 | 365 | 2.0 | 104.39 |
| 13:23:47 | 366 | 2.0 | 104.42 |
| 13:23:48 | 367 | 2.0 | 104.45 |
| 13:23:49 | 367 | 2.0 | 104.49 |
| 13:23:50 | 367 | 2.0 | 104.52 |
| 13:23:51 | 367 | 2.0 | 104.56 |
| 13:23:52 | 367 | 2.0 | 104.59 |
| 13:23:53 | 367 | 2.0 | 104.62 |
| 13:23:54 | 368 | 2.0 | 104.66 |
| 13:23:55 | 368 | 2.0 | 104.69 |
| 13:23:56 | 368 | 2.0 | 104.73 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:23:57 | 368 | 2.0 | 104.76 |
| 13:23:58 | 369 | 2.0 | 104.79 |
| 13:23:59 | 369 | 2.0 | 104.83 |
| 13:24:00 | 370 | 2.0 | 104.86 |
| 13:24:01 | 371 | 2.0 | 104.89 |
| 13:24:02 | 371 | 2.0 | 104.93 |
| 13:24:03 | 372 | 2.0 | 104.96 |
| 13:24:04 | 372 | 2.0 | 105.00 |
| 13:24:05 | 372 | 2.0 | 105.03 |
| 13:24:06 | 373 | 2.0 | 105.06 |
| 13:24:07 | 373 | 2.0 | 105.10 |
| 13:24:08 | 373 | 2.0 | 105.13 |
| 13:24:09 | 373 | 2.0 | 105.17 |
| 13:24:10 | 373 | 2.0 | 105.20 |
| 13:24:11 | 373 | 2.0 | 105.23 |
| 13:24:12 | 373 | 2.0 | 105.27 |
| 13:24:13 | 374 | 2.0 | 105.30 |
| 13:24:14 | 375 | 2.0 | 105.33 |
| 13:24:15 | 375 | 2.0 | 105.37 |
| 13:24:16 | 376 | 2.0 | 105.40 |
| 13:24:17 | 377 | 2.0 | 105.44 |
| 13:24:18 | 377 | 2.0 | 105.47 |
| 13:24:19 | 377 | 2.0 | 105.50 |
| 13:24:20 | 377 | 2.0 | 105.54 |
| 13:24:21 | 378 | 2.0 | 105.57 |
| 13:24:22 | 378 | 2.0 | 105.60 |
| 13:24:23 | 378 | 2.0 | 105.64 |
| 13:24:24 | 378 | 2.0 | 105.67 |
| 13:24:25 | 378 | 2.0 | 105.71 |
| 13:24:26 | 378 | 2.0 | 105.74 |
| 13:24:27 | 378 | 2.0 | 105.77 |
| 13:24:28 | 379 | 2.0 | 105.81 |
| 13:24:29 | 379 | 2.0 | 105.84 |
| 13:24:30 | 380 | 2.0 | 105.87 |
| 13:24:31 | 380 | 2.0 | 105.91 |
| 13:24:32 | 381 | 2.0 | 105.94 |
| 13:24:33 | 381 | 2.0 | 105.98 |
| 13:24:34 | 382 | 2.0 | 106.01 |
| 13:24:35 | 382 | 2.0 | 106.04 |
| 13:24:36 | 383 | 2.0 | 106.08 |
| 13:24:37 | 383 | 2.0 | 106.11 |
| 13:24:38 | 383 | 2.0 | 106.14 |
| 13:24:39 | 383 | 2.0 | 106.18 |
| 13:24:40 | 383 | 2.0 | 106.21 |
| 13:24:41 | 383 | 2.0 | 106.25 |
| 13:24:42 | 383 | 2.0 | 106.28 |
| 13:24:43 | 384 | 2.0 | 106.31 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:24:44 | 384 | 2.0 | 106.35 |
| 13:24:45 | 384 | 2.0 | 106.38 |
| 13:24:46 | 385 | 2.0 | 106.42 |
| 13:24:47 | 385 | 2.0 | 106.45 |
| 13:24:48 | 386 | 2.0 | 106.48 |
| 13:24:49 | 386 | 2.0 | 106.52 |
| 13:24:50 | 387 | 2.0 | 106.55 |
| 13:24:51 | 387 | 2.0 | 106.58 |
| 13:24:52 | 388 | 2.0 | 106.62 |
| 13:24:53 | 388 | 2.0 | 106.65 |
| 13:24:54 | 388 | 2.0 | 106.69 |
| 13:24:55 | 388 | 2.0 | 106.72 |
| 13:24:56 | 388 | 2.0 | 106.75 |
| 13:24:57 | 388 | 2.0 | 106.79 |
| 13:24:58 | 388 | 2.0 | 106.82 |
| 13:24:59 | 389 | 2.0 | 106.85 |
| 13:25:00 | 389 | 2.0 | 106.89 |
| 13:25:01 | 389 | 2.0 | 106.92 |
| 13:25:02 | 390 | 2.0 | 106.96 |
| 13:25:03 | 390 | 2.0 | 106.99 |
| 13:25:04 | 391 | 2.0 | 107.02 |
| 13:25:05 | 391 | 2.0 | 107.06 |
| 13:25:06 | 392 | 2.0 | 107.09 |
| 13:25:07 | 392 | 2.0 | 107.12 |
| 13:25:08 | 392 | 2.0 | 107.16 |
| 13:25:09 | 392 | 2.0 | 107.19 |
| 13:25:10 | 393 | 2.0 | 107.23 |
| 13:25:11 | 393 | 2.0 | 107.26 |
| 13:25:12 | 393 | 2.0 | 107.29 |
| 13:25:13 | 393 | 2.0 | 107.33 |
| 13:25:14 | 393 | 2.0 | 107.36 |
| 13:25:15 | 393 | 2.0 | 107.39 |
| 13:25:16 | 393 | 2.0 | 107.43 |
| 13:25:17 | 394 | 2.0 | 107.46 |
| 13:25:18 | 394 | 2.0 | 107.50 |
| 13:25:19 | 395 | 2.0 | 107.53 |
| 13:25:20 | 395 | 2.0 | 107.56 |
| 13:25:21 | 396 | 2.0 | 107.60 |
| 13:25:22 | 396 | 2.0 | 107.63 |
| 13:25:23 | 397 | 2.0 | 107.66 |
| 13:25:24 | 397 | 2.0 | 107.70 |
| 13:25:25 | 397 | 2.0 | 107.73 |
| 13:25:26 | 397 | 2.0 | 107.77 |
| 13:25:27 | 397 | 2.0 | 107.80 |
| 13:25:28 | 397 | 2.0 | 107.83 |
| 13:25:29 | 397 | 2.0 | 107.87 |
| 13:25:30 | 397 | 2.0 | 107.90 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:25:31 | 398 | 2.0 | 107.93 |
| 13:25:32 | 398 | 2.0 | 107.97 |
| 13:25:33 | 398 | 2.0 | 108.00 |
| 13:25:34 | 398 | 2.0 | 108.04 |
| 13:25:35 | 399 | 2.0 | 108.07 |
| 13:25:36 | 400 | 2.0 | 108.10 |
| 13:25:37 | 400 | 2.0 | 108.14 |
| 13:25:38 | 401 | 2.0 | 108.17 |
| 13:25:39 | 401 | 2.0 | 108.20 |
| 13:25:40 | 401 | 2.0 | 108.24 |
| 13:25:41 | 401 | 2.0 | 108.27 |
| 13:25:42 | 402 | 2.0 | 108.31 |
| 13:25:43 | 402 | 2.0 | 108.34 |
| 13:25:44 | 402 | 2.0 | 108.37 |
| 13:25:45 | 402 | 2.0 | 108.41 |
| 13:25:46 | 402 | 2.0 | 108.44 |
| 13:25:47 | 402 | 2.0 | 108.47 |
| 13:25:48 | 402 | 2.0 | 108.51 |
| 13:25:49 | 403 | 2.0 | 108.54 |
| 13:25:50 | 403 | 2.0 | 108.58 |
| 13:25:51 | 403 | 2.0 | 108.61 |
| 13:25:52 | 404 | 2.0 | 108.64 |
| 13:25:53 | 404 | 2.0 | 108.68 |
| 13:25:54 | 405 | 2.0 | 108.71 |
| 13:25:55 | 405 | 2.0 | 108.74 |
| 13:25:56 | 406 | 2.0 | 108.78 |
| 13:25:57 | 406 | 2.0 | 108.81 |
| 13:25:58 | 406 | 2.0 | 108.85 |
| 13:25:59 | 406 | 2.0 | 108.88 |
| 13:26:00 | 406 | 2.0 | 108.91 |
| 13:26:01 | 406 | 2.0 | 108.95 |
| 13:26:02 | 406 | 2.0 | 108.98 |
| 13:26:03 | 406 | 2.0 | 109.01 |
| 13:26:04 | 407 | 2.0 | 109.05 |
| 13:26:05 | 407 | 2.0 | 109.08 |
| 13:26:06 | 407 | 2.0 | 109.12 |
| 13:26:07 | 407 | 2.0 | 109.15 |
| 13:26:08 | 408 | 2.0 | 109.18 |
| 13:26:09 | 408 | 2.0 | 109.22 |
| 13:26:10 | 409 | 2.0 | 109.25 |
| 13:26:11 | 409 | 2.0 | 109.28 |
| 13:26:12 | 410 | 2.0 | 109.32 |
| 13:26:13 | 410 | 2.0 | 109.35 |
| 13:26:14 | 410 | 2.0 | 109.39 |
| 13:26:15 | 410 | 2.0 | 109.42 |
| 13:26:16 | 410 | 2.0 | 109.45 |
| 13:26:17 | 410 | 2.0 | 109.49 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:26:18 | 410 | 2.0 | 109.52 |
| 13:26:19 | 410 | 2.0 | 109.55 |
| 13:26:20 | 411 | 2.0 | 109.59 |
| 13:26:21 | 411 | 2.0 | 109.62 |
| 13:26:22 | 411 | 2.0 | 109.66 |
| 13:26:23 | 411 | 2.0 | 109.69 |
| 13:26:24 | 412 | 2.0 | 109.72 |
| 13:26:25 | 412 | 2.0 | 109.76 |
| 13:26:26 | 413 | 2.0 | 109.79 |
| 13:26:27 | 413 | 2.0 | 109.82 |
| 13:26:28 | 413 | 2.0 | 109.86 |
| 13:26:29 | 413 | 2.0 | 109.89 |
| 13:26:30 | 414 | 2.0 | 109.93 |
| 13:26:31 | 414 | 2.0 | 109.96 |
| 13:26:32 | 414 | 2.0 | 109.99 |
| 13:26:33 | 414 | 2.0 | 110.03 |
| 13:26:34 | 414 | 2.0 | 110.06 |
| 13:26:35 | 414 | 2.0 | 110.09 |
| 13:26:36 | 414 | 2.0 | 110.13 |
| 13:26:37 | 415 | 2.0 | 110.16 |
| 13:26:38 | 415 | 2.0 | 110.20 |
| 13:26:39 | 415 | 2.0 | 110.23 |
| 13:26:40 | 415 | 2.0 | 110.26 |
| 13:26:41 | 416 | 2.0 | 110.30 |
| 13:26:42 | 417 | 2.0 | 110.33 |
| 13:26:43 | 417 | 2.0 | 110.36 |
| 13:26:44 | 417 | 2.0 | 110.40 |
| 13:26:45 | 418 | 2.0 | 110.43 |
| 13:26:46 | 418 | 2.0 | 110.47 |
| 13:26:47 | 418 | 2.0 | 110.50 |
| 13:26:48 | 418 | 2.0 | 110.53 |
| 13:26:49 | 418 | 2.0 | 110.57 |
| 13:26:50 | 419 | 2.0 | 110.60 |
| 13:26:51 | 419 | 2.0 | 110.64 |
| 13:26:52 | 419 | 2.0 | 110.67 |
| 13:26:53 | 419 | 2.0 | 110.70 |
| 13:26:54 | 419 | 2.0 | 110.74 |
| 13:26:55 | 419 | 2.0 | 110.77 |
| 13:26:56 | 420 | 2.0 | 110.80 |
| 13:26:57 | 420 | 2.0 | 110.84 |
| 13:26:58 | 420 | 2.0 | 110.87 |
| 13:26:59 | 421 | 2.0 | 110.91 |
| 13:27:00 | 421 | 2.0 | 110.94 |
| 13:27:01 | 422 | 2.0 | 110.97 |
| 13:27:02 | 422 | 2.0 | 111.01 |
| 13:27:03 | 422 | 2.0 | 111.04 |
| 13:27:04 | 422 | 2.0 | 111.07 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:27:05 | 423 | 2.0 | 111.11 |
| 13:27:06 | 423 | 2.0 | 111.14 |
| 13:27:07 | 423 | 2.0 | 111.18 |
| 13:27:08 | 423 | 2.0 | 111.21 |
| 13:27:09 | 423 | 2.0 | 111.24 |
| 13:27:10 | 423 | 2.0 | 111.28 |
| 13:27:11 | 424 | 2.0 | 111.31 |
| 13:27:12 | 424 | 2.0 | 111.35 |
| 13:27:13 | 424 | 2.0 | 111.38 |
| 13:27:14 | 424 | 2.0 | 111.41 |
| 13:27:15 | 425 | 2.0 | 111.45 |
| 13:27:16 | 425 | 2.0 | 111.48 |
| 13:27:17 | 426 | 2.0 | 111.51 |
| 13:27:18 | 426 | 2.0 | 111.55 |
| 13:27:19 | 426 | 2.0 | 111.58 |
| 13:27:20 | 427 | 2.0 | 111.62 |
| 13:27:21 | 427 | 2.0 | 111.65 |
| 13:27:22 | 427 | 2.0 | 111.68 |
| 13:27:23 | 427 | 2.0 | 111.72 |
| 13:27:24 | 427 | 2.0 | 111.75 |
| 13:27:25 | 427 | 2.0 | 111.78 |
| 13:27:26 | 427 | 2.0 | 111.82 |
| 13:27:27 | 428 | 2.0 | 111.85 |
| 13:27:28 | 428 | 2.0 | 111.89 |
| 13:27:29 | 428 | 2.0 | 111.92 |
| 13:27:30 | 428 | 2.0 | 111.95 |
| 13:27:31 | 429 | 2.0 | 111.99 |
| 13:27:32 | 429 | 2.0 | 112.02 |
| 13:27:33 | 430 | 2.0 | 112.06 |
| 13:27:34 | 430 | 2.0 | 112.09 |
| 13:27:35 | 431 | 2.0 | 112.12 |
| 13:27:36 | 431 | 2.0 | 112.16 |
| 13:27:37 | 431 | 2.0 | 112.19 |
| 13:27:38 | 431 | 2.0 | 112.22 |
| 13:27:39 | 431 | 2.0 | 112.26 |
| 13:27:40 | 431 | 2.0 | 112.29 |
| 13:27:41 | 431 | 2.0 | 112.33 |
| 13:27:42 | 432 | 2.0 | 112.36 |
| 13:27:43 | 432 | 2.0 | 112.39 |
| 13:27:44 | 432 | 2.0 | 112.43 |
| 13:27:45 | 432 | 2.0 | 112.46 |
| 13:27:46 | 432 | 2.0 | 112.50 |
| 13:27:47 | 433 | 2.0 | 112.53 |
| 13:27:48 | 433 | 2.0 | 112.56 |
| 13:27:49 | 433 | 2.0 | 112.60 |
| 13:27:50 | 434 | 2.0 | 112.63 |
| 13:27:51 | 434 | 2.0 | 112.66 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:27:52 | 435 | 2.0 | 112.70 |
| 13:27:53 | 435 | 2.0 | 112.73 |
| 13:27:54 | 435 | 2.0 | 112.77 |
| 13:27:55 | 435 | 2.0 | 112.80 |
| 13:27:56 | 435 | 2.0 | 112.83 |
| 13:27:57 | 435 | 2.0 | 112.87 |
| 13:27:58 | 436 | 2.0 | 112.90 |
| 13:27:59 | 436 | 2.0 | 112.94 |
| 13:28:00 | 436 | 2.0 | 112.97 |
| 13:28:01 | 436 | 2.0 | 113.00 |
| 13:28:02 | 436 | 2.0 | 113.04 |
| 13:28:03 | 437 | 2.0 | 113.07 |
| 13:28:04 | 437 | 2.0 | 113.10 |
| 13:28:05 | 437 | 2.0 | 113.14 |
| 13:28:06 | 438 | 2.0 | 113.17 |
| 13:28:07 | 438 | 2.0 | 113.21 |
| 13:28:08 | 438 | 2.0 | 113.24 |
| 13:28:09 | 439 | 2.0 | 113.27 |
| 13:28:10 | 439 | 2.0 | 113.31 |
| 13:28:11 | 439 | 2.0 | 113.34 |
| 13:28:12 | 440 | 2.0 | 113.37 |
| 13:28:13 | 440 | 2.0 | 113.41 |
| 13:28:14 | 440 | 2.0 | 113.44 |
| 13:28:15 | 440 | 2.0 | 113.48 |
| 13:28:16 | 440 | 2.0 | 113.51 |
| 13:28:17 | 440 | 2.0 | 113.54 |
| 13:28:18 | 440 | 2.0 | 113.58 |
| 13:28:19 | 440 | 2.0 | 113.61 |
| 13:28:20 | 441 | 2.0 | 113.65 |
| 13:28:21 | 441 | 2.0 | 113.68 |
| 13:28:22 | 441 | 2.0 | 113.71 |
| 13:28:23 | 442 | 2.0 | 113.75 |
| 13:28:24 | 442 | 2.0 | 113.78 |
| 13:28:25 | 443 | 2.0 | 113.81 |
| 13:28:26 | 443 | 2.0 | 113.85 |
| 13:28:27 | 443 | 2.0 | 113.88 |
| 13:28:28 | 443 | 2.0 | 113.92 |
| 13:28:29 | 444 | 2.0 | 113.95 |
| 13:28:30 | 444 | 2.0 | 113.98 |
| 13:28:31 | 444 | 2.0 | 114.02 |
| 13:28:32 | 444 | 2.0 | 114.05 |
| 13:28:33 | 444 | 2.0 | 114.08 |
| 13:28:34 | 444 | 2.0 | 114.12 |
| 13:28:35 | 444 | 2.0 | 114.15 |
| 13:28:36 | 444 | 2.0 | 114.19 |
| 13:28:37 | 445 | 2.0 | 114.22 |
| 13:28:38 | 445 | 2.0 | 114.25 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:28:39 | 445 | 2.0 | 114.29 |
| 13:28:40 | 446 | 2.0 | 114.32 |
| 13:28:41 | 446 | 2.0 | 114.36 |
| 13:28:42 | 446 | 2.0 | 114.39 |
| 13:28:43 | 447 | 2.0 | 114.42 |
| 13:28:44 | 447 | 2.0 | 114.46 |
| 13:28:45 | 447 | 2.0 | 114.49 |
| 13:28:46 | 447 | 2.0 | 114.52 |
| 13:28:47 | 447 | 2.0 | 114.56 |
| 13:28:48 | 447 | 2.0 | 114.59 |
| 13:28:49 | 447 | 2.0 | 114.63 |
| 13:28:50 | 448 | 2.0 | 114.66 |
| 13:28:51 | 448 | 2.0 | 114.69 |
| 13:28:52 | 448 | 2.0 | 114.73 |
| 13:28:53 | 448 | 2.0 | 114.76 |
| 13:28:54 | 448 | 2.0 | 114.79 |
| 13:28:55 | 449 | 2.0 | 114.83 |
| 13:28:56 | 449 | 2.0 | 114.86 |
| 13:28:57 | 449 | 2.0 | 114.90 |
| 13:28:58 | 450 | 2.0 | 114.93 |
| 13:28:59 | 450 | 2.0 | 114.96 |
| 13:29:00 | 451 | 2.0 | 115.00 |
| 13:29:01 | 451 | 2.0 | 115.03 |
| 13:29:02 | 451 | 2.0 | 115.06 |
| 13:29:03 | 451 | 2.0 | 115.10 |
| 13:29:04 | 451 | 2.0 | 115.13 |
| 13:29:05 | 451 | 2.0 | 115.17 |
| 13:29:06 | 451 | 2.0 | 115.20 |
| 13:29:07 | 452 | 2.0 | 115.23 |
| 13:29:08 | 452 | 2.0 | 115.27 |
| 13:29:09 | 452 | 2.0 | 115.30 |
| 13:29:10 | 452 | 2.0 | 115.34 |
| 13:29:11 | 452 | 2.0 | 115.37 |
| 13:29:12 | 453 | 2.0 | 115.40 |
| 13:29:13 | 453 | 2.0 | 115.44 |
| 13:29:14 | 453 | 2.0 | 115.47 |
| 13:29:15 | 454 | 2.0 | 115.50 |
| 13:29:16 | 454 | 2.0 | 115.54 |
| 13:29:17 | 455 | 2.0 | 115.57 |
| 13:29:18 | 455 | 2.0 | 115.61 |
| 13:29:19 | 455 | 2.0 | 115.64 |
| 13:29:20 | 455 | 2.0 | 115.67 |
| 13:29:21 | 455 | 2.0 | 115.71 |
| 13:29:22 | 456 | 2.0 | 115.74 |
| 13:29:23 | 455 | 2.0 | 115.77 |
| 13:29:24 | 456 | 2.0 | 115.81 |
| 13:29:25 | 456 | 2.0 | 115.84 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:29:26 | 456 | 2.0 | 115.88 |
| 13:29:27 | 456 | 2.0 | 115.91 |
| 13:29:28 | 456 | 2.0 | 115.94 |
| 13:29:29 | 457 | 2.0 | 115.98 |
| 13:29:30 | 457 | 2.0 | 116.01 |
| 13:29:31 | 457 | 2.0 | 116.05 |
| 13:29:32 | 458 | 2.0 | 116.08 |
| 13:29:33 | 458 | 2.0 | 116.11 |
| 13:29:34 | 459 | 2.0 | 116.15 |
| 13:29:35 | 459 | 2.0 | 116.18 |
| 13:29:36 | 459 | 2.0 | 116.21 |
| 13:29:37 | 460 | 2.0 | 116.25 |
| 13:29:38 | 460 | 2.0 | 116.28 |
| 13:29:39 | 460 | 2.0 | 116.32 |
| 13:29:40 | 460 | 2.0 | 116.35 |
| 13:29:41 | 460 | 2.0 | 116.38 |
| 13:29:42 | 460 | 2.0 | 116.42 |
| 13:29:43 | 460 | 2.0 | 116.45 |
| 13:29:44 | 460 | 2.0 | 116.48 |
| 13:29:45 | 460 | 2.0 | 116.52 |
| 13:29:46 | 460 | 2.0 | 116.55 |
| 13:29:47 | 461 | 2.0 | 116.59 |
| 13:29:48 | 461 | 2.0 | 116.62 |
| 13:29:49 | 461 | 2.0 | 116.65 |
| 13:29:50 | 462 | 2.0 | 116.69 |
| 13:29:51 | 462 | 2.0 | 116.72 |
| 13:29:52 | 463 | 2.0 | 116.76 |
| 13:29:53 | 463 | 2.0 | 116.79 |
| 13:29:54 | 463 | 2.0 | 116.82 |
| 13:29:55 | 464 | 2.0 | 116.86 |
| 13:29:56 | 464 | 2.0 | 116.89 |
| 13:29:57 | 464 | 2.0 | 116.92 |
| 13:29:58 | 464 | 2.0 | 116.96 |
| 13:29:59 | 464 | 2.0 | 116.99 |
| 13:30:00 | 464 | 2.0 | 117.03 |
| 13:30:01 | 464 | 2.0 | 117.06 |
| 13:30:02 | 464 | 2.0 | 117.09 |
| 13:30:03 | 464 | 2.0 | 117.13 |
| 13:30:04 | 465 | 2.0 | 117.16 |
| 13:30:05 | 465 | 2.0 | 117.19 |
| 13:30:06 | 465 | 2.0 | 117.23 |
| 13:30:07 | 466 | 2.0 | 117.26 |
| 13:30:08 | 466 | 2.0 | 117.30 |
| 13:30:09 | 466 | 2.0 | 117.33 |
| 13:30:10 | 467 | 2.0 | 117.36 |
| 13:30:11 | 467 | 2.0 | 117.40 |
| 13:30:12 | 468 | 2.0 | 117.43 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:30:13 | 467 | 2.0 | 117.46 |
| 13:30:14 | 468 | 2.0 | 117.50 |
| 13:30:15 | 468 | 2.0 | 117.53 |
| 13:30:16 | 468 | 2.0 | 117.57 |
| 13:30:17 | 468 | 2.0 | 117.60 |
| 13:30:18 | 468 | 2.0 | 117.63 |
| 13:30:19 | 468 | 2.0 | 117.67 |
| 13:30:20 | 468 | 2.0 | 117.70 |
| 13:30:21 | 468 | 2.0 | 117.73 |
| 13:30:22 | 469 | 2.0 | 117.77 |
| 13:30:23 | 469 | 2.0 | 117.80 |
| 13:30:24 | 469 | 2.0 | 117.84 |
| 13:30:25 | 470 | 2.0 | 117.87 |
| 13:30:26 | 470 | 2.0 | 117.90 |
| 13:30:27 | 471 | 2.0 | 117.94 |
| 13:30:28 | 471 | 2.0 | 117.97 |
| 13:30:29 | 472 | 2.0 | 118.01 |
| 13:30:30 | 472 | 2.0 | 118.04 |
| 13:30:31 | 472 | 2.0 | 118.07 |
| 13:30:32 | 472 | 2.0 | 118.11 |
| 13:30:33 | 472 | 2.0 | 118.14 |
| 13:30:34 | 472 | 2.0 | 118.17 |
| 13:30:35 | 472 | 2.0 | 118.21 |
| 13:30:36 | 472 | 2.0 | 118.24 |
| 13:30:37 | 472 | 2.0 | 118.28 |
| 13:30:38 | 472 | 2.0 | 118.31 |
| 13:30:39 | 472 | 2.0 | 118.34 |
| 13:30:40 | 473 | 2.0 | 118.38 |
| 13:30:41 | 473 | 2.0 | 118.41 |
| 13:30:42 | 473 | 2.0 | 118.44 |
| 13:30:43 | 474 | 2.0 | 118.48 |
| 13:30:44 | 474 | 2.0 | 118.51 |
| 13:30:45 | 475 | 2.0 | 118.55 |
| 13:30:46 | 475 | 2.0 | 118.58 |
| 13:30:47 | 475 | 2.0 | 118.61 |
| 13:30:48 | 475 | 2.0 | 118.65 |
| 13:30:49 | 476 | 2.0 | 118.68 |
| 13:30:50 | 476 | 2.0 | 118.71 |
| 13:30:51 | 476 | 2.0 | 118.75 |
| 13:30:52 | 476 | 2.0 | 118.78 |
| 13:30:53 | 476 | 2.0 | 118.82 |
| 13:30:54 | 476 | 2.0 | 118.85 |
| 13:30:55 | 476 | 2.0 | 118.88 |
| 13:30:56 | 476 | 2.0 | 118.92 |
| 13:30:57 | 476 | 2.0 | 118.95 |
| 13:30:58 | 477 | 2.0 | 118.98 |
| 13:30:59 | 477 | 2.0 | 119.02 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:31:00 | 477 | 2.0 | 119.05 |
| 13:31:01 | 478 | 2.0 | 119.09 |
| 13:31:02 | 478 | 2.0 | 119.12 |
| 13:31:03 | 479 | 2.0 | 119.15 |
| 13:31:04 | 479 | 2.0 | 119.19 |
| 13:31:05 | 479 | 2.0 | 119.22 |
| 13:31:06 | 480 | 2.0 | 119.25 |
| 13:31:07 | 480 | 2.0 | 119.29 |
| 13:31:08 | 480 | 2.0 | 119.32 |
| 13:31:09 | 479 | 2.0 | 119.36 |
| 13:31:10 | 479 | 2.0 | 119.39 |
| 13:31:11 | 479 | 2.0 | 119.42 |
| 13:31:12 | 479 | 2.0 | 119.46 |
| 13:31:13 | 479 | 2.0 | 119.49 |
| 13:31:14 | 480 | 2.0 | 119.53 |
| 13:31:15 | 480 | 2.0 | 119.56 |
| 13:31:16 | 480 | 2.0 | 119.59 |
| 13:31:17 | 481 | 2.0 | 119.63 |
| 13:31:18 | 481 | 2.0 | 119.66 |
| 13:31:19 | 482 | 2.0 | 119.69 |
| 13:31:20 | 482 | 2.0 | 119.73 |
| 13:31:21 | 483 | 2.0 | 119.76 |
| 13:31:22 | 483 | 2.0 | 119.80 |
| 13:31:23 | 483 | 2.0 | 119.83 |
| 13:31:24 | 484 | 2.0 | 119.86 |
| 13:31:25 | 483 | 2.0 | 119.90 |
| 13:31:26 | 483 | 2.0 | 119.93 |
| 13:31:27 | 483 | 2.0 | 119.96 |
| 13:31:28 | 483 | 2.0 | 120.00 |
| 13:31:29 | 483 | 2.0 | 120.03 |
| 13:31:30 | 483 | 2.0 | 120.07 |
| 13:31:31 | 483 | 2.0 | 120.10 |
| 13:31:32 | 484 | 2.0 | 120.13 |
| 13:31:33 | 484 | 2.0 | 120.17 |
| 13:31:34 | 484 | 2.0 | 120.20 |
| 13:31:35 | 485 | 2.0 | 120.23 |
| 13:31:36 | 485 | 2.0 | 120.27 |
| 13:31:37 | 486 | 2.0 | 120.30 |
| 13:31:38 | 486 | 2.0 | 120.34 |
| 13:31:39 | 487 | 2.0 | 120.37 |
| 13:31:40 | 487 | 2.0 | 120.40 |
| 13:31:41 | 487 | 2.0 | 120.44 |
| 13:31:42 | 488 | 2.0 | 120.47 |
| 13:31:43 | 487 | 2.0 | 120.50 |
| 13:31:44 | 487 | 2.0 | 120.54 |
| 13:31:45 | 487 | 2.0 | 120.57 |
| 13:31:46 | 487 | 2.0 | 120.61 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:31:47 | 486 | 2.0 | 120.64 |
| 13:31:48 | 487 | 2.0 | 120.67 |
| 13:31:49 | 487 | 2.0 | 120.71 |
| 13:31:50 | 488 | 2.0 | 120.74 |
| 13:31:51 | 488 | 2.0 | 120.77 |
| 13:31:52 | 488 | 2.0 | 120.81 |
| 13:31:53 | 489 | 2.0 | 120.84 |
| 13:31:54 | 489 | 2.0 | 120.88 |
| 13:31:55 | 490 | 2.0 | 120.91 |
| 13:31:56 | 491 | 2.0 | 120.94 |
| 13:31:57 | 491 | 2.0 | 120.98 |
| 13:31:58 | 492 | 2.0 | 121.01 |
| 13:31:59 | 492 | 2.0 | 121.05 |
| 13:32:00 | 492 | 2.0 | 121.08 |
| 13:32:01 | 492 | 2.0 | 121.11 |
| 13:32:02 | 492 | 2.0 | 121.15 |
| 13:32:03 | 491 | 2.0 | 121.18 |
| 13:32:04 | 491 | 2.0 | 121.21 |
| 13:32:05 | 491 | 2.0 | 121.25 |
| 13:32:06 | 491 | 2.0 | 121.28 |
| 13:32:07 | 492 | 2.0 | 121.32 |
| 13:32:08 | 492 | 2.0 | 121.35 |
| 13:32:09 | 493 | 2.0 | 121.38 |
| 13:32:10 | 493 | 2.0 | 121.42 |
| 13:32:11 | 494 | 2.0 | 121.45 |
| 13:32:12 | 494 | 2.0 | 121.48 |
| 13:32:13 | 495 | 2.0 | 121.52 |
| 13:32:14 | 495 | 2.0 | 121.55 |
| 13:32:15 | 496 | 2.0 | 121.59 |
| 13:32:16 | 496 | 2.0 | 121.62 |
| 13:32:17 | 497 | 2.0 | 121.65 |
| 13:32:18 | 496 | 2.0 | 121.69 |
| 13:32:19 | 497 | 2.0 | 121.72 |
| 13:32:20 | 497 | 2.0 | 121.75 |
| 13:32:21 | 496 | 2.0 | 121.79 |
| 13:32:22 | 497 | 2.0 | 121.82 |
| 13:32:23 | 496 | 2.0 | 121.86 |
| 13:32:24 | 497 | 2.0 | 121.89 |
| 13:32:25 | 497 | 2.0 | 121.92 |
| 13:32:26 | 497 | 2.0 | 121.96 |
| 13:32:27 | 498 | 2.0 | 121.99 |
| 13:32:28 | 498 | 2.0 | 122.02 |
| 13:32:29 | 499 | 2.0 | 122.06 |
| 13:32:30 | 499 | 2.0 | 122.09 |
| 13:32:31 | 500 | 2.0 | 122.13 |
| 13:32:32 | 500 | 2.0 | 122.16 |
| 13:32:33 | 501 | 2.0 | 122.19 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:32:34 | 501 | 2.0 | 122.23 |
| 13:32:35 | 502 | 2.0 | 122.26 |
| 13:32:36 | 502 | 2.0 | 122.29 |
| 13:32:37 | 502 | 2.0 | 122.33 |
| 13:32:38 | 502 | 2.0 | 122.36 |
| 13:32:39 | 502 | 2.0 | 122.40 |
| 13:32:40 | 502 | 2.0 | 122.43 |
| 13:32:41 | 502 | 2.0 | 122.46 |
| 13:32:42 | 502 | 2.0 | 122.50 |
| 13:32:43 | 502 | 2.0 | 122.53 |
| 13:32:44 | 502 | 2.0 | 122.56 |
| 13:32:45 | 503 | 2.0 | 122.60 |
| 13:32:46 | 504 | 2.0 | 122.63 |
| 13:32:47 | 504 | 2.0 | 122.67 |
| 13:32:48 | 505 | 2.0 | 122.70 |
| 13:32:49 | 505 | 2.0 | 122.73 |
| 13:32:50 | 505 | 2.0 | 122.77 |
| 13:32:51 | 506 | 2.0 | 122.80 |
| 13:32:52 | 507 | 2.0 | 122.84 |
| 13:32:53 | 507 | 2.0 | 122.87 |
| 13:32:54 | 507 | 2.0 | 122.90 |
| 13:32:55 | 508 | 2.0 | 122.94 |
| 13:32:56 | 508 | 2.0 | 122.97 |
| 13:32:57 | 508 | 2.0 | 123.00 |
| 13:32:58 | 508 | 2.0 | 123.04 |
| 13:32:59 | 508 | 2.0 | 123.07 |
| 13:33:00 | 508 | 2.0 | 123.10 |
| 13:33:01 | 508 | 2.0 | 123.14 |
| 13:33:02 | 508 | 2.0 | 123.17 |
| 13:33:03 | 509 | 2.0 | 123.21 |
| 13:33:04 | 509 | 2.0 | 123.24 |
| 13:33:05 | 510 | 2.0 | 123.27 |
| 13:33:06 | 510 | 2.0 | 123.31 |
| 13:33:07 | 511 | 2.0 | 123.34 |
| 13:33:08 | 511 | 2.0 | 123.38 |
| 13:33:09 | 512 | 2.0 | 123.41 |
| 13:33:10 | 513 | 2.0 | 123.44 |
| 13:33:11 | 513 | 2.0 | 123.48 |
| 13:33:12 | 514 | 2.0 | 123.51 |
| 13:33:13 | 514 | 2.0 | 123.54 |
| 13:33:14 | 515 | 2.0 | 123.58 |
| 13:33:15 | 515 | 2.0 | 123.61 |
| 13:33:16 | 515 | 2.0 | 123.65 |
| 13:33:17 | 515 | 2.0 | 123.68 |
| 13:33:18 | 516 | 2.0 | 123.71 |
| 13:33:19 | 516 | 2.0 | 123.75 |
| 13:33:20 | 516 | 2.0 | 123.78 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:33:21 | 516 | 2.0 | 123.81 |
| 13:33:22 | 517 | 2.0 | 123.85 |
| 13:33:23 | 517 | 2.0 | 123.88 |
| 13:33:24 | 518 | 2.0 | 123.92 |
| 13:33:25 | 519 | 2.0 | 123.95 |
| 13:33:26 | 519 | 2.0 | 123.98 |
| 13:33:27 | 520 | 2.0 | 124.02 |
| 13:33:28 | 520 | 2.0 | 124.05 |
| 13:33:29 | 521 | 2.0 | 124.08 |
| 13:33:30 | 521 | 2.0 | 124.12 |
| 13:33:31 | 522 | 2.0 | 124.15 |
| 13:33:32 | 522 | 2.0 | 124.19 |
| 13:33:33 | 523 | 2.0 | 124.22 |
| 13:33:34 | 523 | 2.0 | 124.25 |
| 13:33:35 | 524 | 2.0 | 124.29 |
| 13:33:36 | 524 | 2.0 | 124.32 |
| 13:33:37 | 524 | 2.0 | 124.35 |
| 13:33:38 | 524 | 2.0 | 124.39 |
| 13:33:39 | 524 | 2.0 | 124.42 |
| 13:33:40 | 524 | 2.0 | 124.46 |
| 13:33:41 | 525 | 2.0 | 124.49 |
| 13:33:42 | 525 | 2.0 | 124.52 |
| 13:33:43 | 526 | 2.0 | 124.56 |
| 13:33:44 | 527 | 2.0 | 124.59 |
| 13:33:45 | 527 | 2.0 | 124.62 |
| 13:33:46 | 528 | 2.0 | 124.66 |
| 13:33:47 | 528 | 2.0 | 124.69 |
| 13:33:48 | 529 | 2.0 | 124.72 |
| 13:33:49 | 529 | 2.0 | 124.76 |
| 13:33:50 | 530 | 2.0 | 124.79 |
| 13:33:51 | 531 | 2.0 | 124.83 |
| 13:33:52 | 531 | 2.0 | 124.86 |
| 13:33:53 | 532 | 2.0 | 124.89 |
| 13:33:54 | 532 | 2.0 | 124.93 |
| 13:33:55 | 532 | 2.0 | 124.96 |
| 13:33:56 | 532 | 2.0 | 124.99 |
| 13:33:57 | 532 | 2.0 | 125.03 |
| 13:33:58 | 532 | 2.0 | 125.06 |
| 13:33:59 | 532 | 2.0 | 125.10 |
| 13:34:00 | 533 | 2.0 | 125.13 |
| 13:34:01 | 533 | 2.0 | 125.16 |
| 13:34:02 | 533 | 2.0 | 125.20 |
| 13:34:03 | 534 | 2.0 | 125.23 |
| 13:34:04 | 534 | 2.0 | 125.26 |
| 13:34:05 | 535 | 2.0 | 125.30 |
| 13:34:06 | 535 | 2.0 | 125.33 |
| 13:34:07 | 536 | 2.0 | 125.37 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:34:08 | 537 | 2.0 | 125.40 |
| 13:34:09 | 537 | 2.0 | 125.43 |
| 13:34:10 | 537 | 2.0 | 125.47 |
| 13:34:11 | 538 | 2.0 | 125.50 |
| 13:34:12 | 538 | 2.0 | 125.53 |
| 13:34:13 | 539 | 2.0 | 125.57 |
| 13:34:14 | 539 | 2.0 | 125.60 |
| 13:34:15 | 539 | 2.0 | 125.63 |
| 13:34:16 | 539 | 2.0 | 125.67 |
| 13:34:17 | 539 | 2.0 | 125.70 |
| 13:34:18 | 539 | 2.0 | 125.74 |
| 13:34:19 | 539 | 2.0 | 125.77 |
| 13:34:20 | 540 | 2.0 | 125.80 |
| 13:34:21 | 540 | 2.0 | 125.84 |
| 13:34:22 | 540 | 2.0 | 125.87 |
| 13:34:23 | 541 | 2.0 | 125.90 |
| 13:34:24 | 542 | 2.0 | 125.94 |
| 13:34:25 | 542 | 2.0 | 125.97 |
| 13:34:26 | 543 | 2.0 | 126.00 |
| 13:34:27 | 543 | 2.0 | 126.04 |
| 13:34:28 | 544 | 2.0 | 126.07 |
| 13:34:29 | 544 | 2.0 | 126.11 |
| 13:34:30 | 545 | 2.0 | 126.14 |
| 13:34:31 | 546 | 2.0 | 126.17 |
| 13:34:32 | 546 | 2.0 | 126.21 |
| 13:34:33 | 547 | 2.0 | 126.24 |
| 13:34:34 | 547 | 2.0 | 126.27 |
| 13:34:35 | 547 | 2.0 | 126.31 |
| 13:34:36 | 547 | 2.0 | 126.34 |
| 13:34:37 | 547 | 2.0 | 126.37 |
| 13:34:38 | 547 | 2.0 | 126.41 |
| 13:34:39 | 547 | 2.0 | 126.44 |
| 13:34:40 | 547 | 2.0 | 126.47 |
| 13:34:41 | 547 | 2.0 | 126.51 |
| 13:34:42 | 548 | 2.0 | 126.54 |
| 13:34:43 | 548 | 2.0 | 126.57 |
| 13:34:44 | 548 | 2.0 | 126.61 |
| 13:34:45 | 549 | 2.0 | 126.64 |
| 13:34:46 | 550 | 2.0 | 126.67 |
| 13:34:47 | 550 | 2.0 | 126.71 |
| 13:34:48 | 551 | 2.0 | 126.74 |
| 13:34:49 | 552 | 2.0 | 126.78 |
| 13:34:50 | 552 | 2.0 | 126.81 |
| 13:34:51 | 553 | 2.0 | 126.84 |
| 13:34:52 | 553 | 2.0 | 126.88 |
| 13:34:53 | 553 | 2.0 | 126.91 |
| 13:34:54 | 554 | 2.0 | 126.94 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:34:55 | 554 | 2.0 | 126.98 |
| 13:34:56 | 554 | 2.0 | 127.01 |
| 13:34:57 | 554 | 2.0 | 127.04 |
| 13:34:58 | 554 | 2.0 | 127.08 |
| 13:34:59 | 554 | 2.0 | 127.11 |
| 13:35:00 | 554 | 2.0 | 127.14 |
| 13:35:01 | 555 | 2.0 | 127.18 |
| 13:35:02 | 555 | 2.0 | 127.21 |
| 13:35:03 | 555 | 2.0 | 127.24 |
| 13:35:04 | 556 | 2.0 | 127.28 |
| 13:35:05 | 556 | 2.0 | 127.31 |
| 13:35:06 | 556 | 2.0 | 127.34 |
| 13:35:07 | 557 | 2.0 | 127.38 |
| 13:35:08 | 557 | 2.0 | 127.41 |
| 13:35:09 | 558 | 2.0 | 127.45 |
| 13:35:10 | 558 | 2.0 | 127.48 |
| 13:35:11 | 559 | 2.0 | 127.51 |
| 13:35:12 | 559 | 2.0 | 127.55 |
| 13:35:13 | 560 | 2.0 | 127.58 |
| 13:35:14 | 560 | 2.0 | 127.61 |
| 13:35:15 | 561 | 2.0 | 127.65 |
| 13:35:16 | 561 | 2.0 | 127.68 |
| 13:35:17 | 561 | 2.0 | 127.71 |
| 13:35:18 | 561 | 2.0 | 127.75 |
| 13:35:19 | 561 | 2.0 | 127.78 |
| 13:35:20 | 561 | 2.0 | 127.81 |
| 13:35:21 | 561 | 2.0 | 127.85 |
| 13:35:22 | 561 | 2.0 | 127.88 |
| 13:35:23 | 561 | 2.0 | 127.91 |
| 13:35:24 | 562 | 2.0 | 127.95 |
| 13:35:25 | 562 | 2.0 | 127.98 |
| 13:35:26 | 563 | 2.0 | 128.01 |
| 13:35:27 | 563 | 2.0 | 128.05 |
| 13:35:28 | 564 | 2.0 | 128.08 |
| 13:35:29 | 564 | 2.0 | 128.11 |
| 13:35:30 | 565 | 2.0 | 128.15 |
| 13:35:31 | 565 | 2.0 | 128.18 |
| 13:35:32 | 566 | 2.0 | 128.22 |
| 13:35:33 | 566 | 2.0 | 128.25 |
| 13:35:34 | 567 | 2.0 | 128.28 |
| 13:35:35 | 567 | 2.0 | 128.32 |
| 13:35:36 | 568 | 2.0 | 128.35 |
| 13:35:37 | 568 | 2.0 | 128.38 |
| 13:35:38 | 569 | 2.0 | 128.42 |
| 13:35:39 | 568 | 2.0 | 128.45 |
| 13:35:40 | 568 | 2.0 | 128.48 |
| 13:35:41 | 568 | 2.0 | 128.52 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:35:42 | 568 | 2.0 | 128.55 |
| 13:35:43 | 568 | 2.0 | 128.58 |
| 13:35:44 | 568 | 2.0 | 128.62 |
| 13:35:45 | 569 | 2.0 | 128.65 |
| 13:35:46 | 570 | 2.0 | 128.68 |
| 13:35:47 | 570 | 2.0 | 128.72 |
| 13:35:48 | 571 | 2.0 | 128.75 |
| 13:35:49 | 572 | 2.0 | 128.78 |
| 13:35:50 | 572 | 2.0 | 128.82 |
| 13:35:51 | 573 | 2.0 | 128.85 |
| 13:35:52 | 573 | 2.0 | 128.88 |
| 13:35:53 | 574 | 2.0 | 128.92 |
| 13:35:54 | 574 | 2.0 | 128.95 |
| 13:35:55 | 574 | 2.0 | 128.98 |
| 13:35:56 | 575 | 2.0 | 129.02 |
| 13:35:57 | 575 | 2.0 | 129.05 |
| 13:35:58 | 576 | 2.0 | 129.08 |
| 13:35:59 | 576 | 2.0 | 129.12 |
| 13:36:00 | 576 | 2.0 | 129.15 |
| 13:36:01 | 576 | 2.0 | 129.18 |
| 13:36:02 | 577 | 2.0 | 129.22 |
| 13:36:03 | 577 | 2.0 | 129.25 |
| 13:36:04 | 577 | 2.0 | 129.29 |
| 13:36:05 | 577 | 2.0 | 129.32 |
| 13:36:06 | 578 | 2.0 | 129.35 |
| 13:36:07 | 578 | 2.0 | 129.39 |
| 13:36:08 | 579 | 2.0 | 129.42 |
| 13:36:09 | 580 | 2.0 | 129.45 |
| 13:36:10 | 580 | 2.0 | 129.49 |
| 13:36:11 | 581 | 2.0 | 129.52 |
| 13:36:12 | 581 | 2.0 | 129.55 |
| 13:36:13 | 581 | 2.0 | 129.59 |
| 13:36:14 | 582 | 2.0 | 129.62 |
| 13:36:15 | 582 | 2.0 | 129.65 |
| 13:36:16 | 583 | 2.0 | 129.69 |
| 13:36:17 | 583 | 2.0 | 129.72 |
| 13:36:18 | 584 | 2.0 | 129.76 |
| 13:36:19 | 584 | 2.0 | 129.79 |
| 13:36:20 | 585 | 2.0 | 129.82 |
| 13:36:21 | 585 | 2.0 | 129.86 |
| 13:36:22 | 585 | 2.0 | 129.89 |
| 13:36:23 | 585 | 2.0 | 129.92 |
| 13:36:24 | 585 | 2.0 | 129.96 |
| 13:36:25 | 585 | 2.0 | 129.99 |
| 13:36:26 | 586 | 2.0 | 130.02 |
| 13:36:27 | 586 | 2.0 | 130.06 |
| 13:36:28 | 586 | 2.0 | 130.09 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:36:29 | 586 | 2.0 | 130.13 |
| 13:36:30 | 587 | 2.0 | 130.16 |
| 13:36:31 | 588 | 2.0 | 130.19 |
| 13:36:32 | 588 | 2.0 | 130.23 |
| 13:36:33 | 589 | 2.0 | 130.26 |
| 13:36:34 | 589 | 2.0 | 130.29 |
| 13:36:35 | 590 | 2.0 | 130.33 |
| 13:36:36 | 590 | 2.0 | 130.36 |
| 13:36:37 | 591 | 2.0 | 130.39 |
| 13:36:38 | 591 | 2.0 | 130.43 |
| 13:36:39 | 592 | 2.0 | 130.46 |
| 13:36:40 | 592 | 2.0 | 130.49 |
| 13:36:41 | 593 | 2.0 | 130.53 |
| 13:36:42 | 593 | 2.0 | 130.56 |
| 13:36:43 | 593 | 2.0 | 130.60 |
| 13:36:44 | 594 | 2.0 | 130.63 |
| 13:36:45 | 594 | 2.0 | 130.66 |
| 13:36:46 | 594 | 2.0 | 130.70 |
| 13:36:47 | 594 | 2.0 | 130.73 |
| 13:36:48 | 594 | 2.0 | 130.76 |
| 13:36:49 | 594 | 2.0 | 130.80 |
| 13:36:50 | 594 | 2.0 | 130.83 |
| 13:36:51 | 595 | 2.0 | 130.86 |
| 13:36:52 | 595 | 2.0 | 130.90 |
| 13:36:53 | 596 | 2.0 | 130.93 |
| 13:36:54 | 597 | 2.0 | 130.96 |
| 13:36:55 | 597 | 2.0 | 131.00 |
| 13:36:56 | 598 | 2.0 | 131.03 |
| 13:36:57 | 598 | 2.0 | 131.07 |
| 13:36:58 | 599 | 2.0 | 131.10 |
| 13:36:59 | 599 | 2.0 | 131.13 |
| 13:37:00 | 599 | 2.0 | 131.17 |
| 13:37:01 | 600 | 2.0 | 131.20 |
| 13:37:02 | 600 | 2.0 | 131.23 |
| 13:37:03 | 600 | 2.0 | 131.27 |
| 13:37:04 | 601 | 2.0 | 131.30 |
| 13:37:05 | 602 | 2.0 | 131.33 |
| 13:37:06 | 602 | 2.0 | 131.37 |
| 13:37:07 | 602 | 2.0 | 131.40 |
| 13:37:08 | 603 | 2.0 | 131.43 |
| 13:37:09 | 602 | 2.0 | 131.47 |
| 13:37:10 | 602 | 2.0 | 131.50 |
| 13:37:11 | 602 | 2.0 | 131.54 |
| 13:37:12 | 602 | 2.0 | 131.57 |
| 13:37:13 | 602 | 2.0 | 131.60 |
| 13:37:14 | 603 | 2.0 | 131.64 |
| 13:37:15 | 603 | 2.0 | 131.67 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:37:16 | 603 | 2.0 | 131.70 |
| 13:37:17 | 604 | 2.0 | 131.74 |
| 13:37:18 | 604 | 2.0 | 131.77 |
| 13:37:19 | 605 | 2.0 | 131.80 |
| 13:37:20 | 605 | 2.0 | 131.84 |
| 13:37:21 | 605 | 2.0 | 131.87 |
| 13:37:22 | 606 | 2.0 | 131.90 |
| 13:37:23 | 606 | 2.0 | 131.94 |
| 13:37:24 | 607 | 2.0 | 131.97 |
| 13:37:25 | 607 | 2.0 | 132.01 |
| 13:37:26 | 607 | 2.0 | 132.04 |
| 13:37:27 | 608 | 2.0 | 132.07 |
| 13:37:28 | 609 | 2.0 | 132.11 |
| 13:37:29 | 609 | 2.0 | 132.14 |
| 13:37:30 | 609 | 2.0 | 132.17 |
| 13:37:31 | 609 | 2.0 | 132.21 |
| 13:37:32 | 609 | 2.0 | 132.24 |
| 13:37:33 | 609 | 2.0 | 132.27 |
| 13:37:34 | 609 | 2.0 | 132.31 |
| 13:37:35 | 609 | 2.0 | 132.34 |
| 13:37:36 | 609 | 2.0 | 132.37 |
| 13:37:37 | 609 | 2.0 | 132.41 |
| 13:37:38 | 610 | 2.0 | 132.44 |
| 13:37:39 | 610 | 2.0 | 132.47 |
| 13:37:40 | 611 | 2.0 | 132.51 |
| 13:37:41 | 612 | 2.0 | 132.54 |
| 13:37:42 | 612 | 2.0 | 132.58 |
| 13:37:43 | 613 | 2.0 | 132.61 |
| 13:37:44 | 613 | 2.0 | 132.64 |
| 13:37:45 | 613 | 2.0 | 132.68 |
| 13:37:46 | 614 | 2.0 | 132.71 |
| 13:37:47 | 614 | 2.0 | 132.74 |
| 13:37:48 | 614 | 2.0 | 132.78 |
| 13:37:49 | 614 | 2.0 | 132.81 |
| 13:37:50 | 615 | 2.0 | 132.84 |
| 13:37:51 | 616 | 2.0 | 132.88 |
| 13:37:52 | 616 | 2.0 | 132.91 |
| 13:37:53 | 616 | 2.0 | 132.94 |
| 13:37:54 | 617 | 2.0 | 132.98 |
| 13:37:55 | 617 | 2.0 | 133.01 |
| 13:37:56 | 618 | 2.0 | 133.04 |
| 13:37:57 | 618 | 2.0 | 133.08 |
| 13:37:58 | 618 | 2.0 | 133.11 |
| 13:37:59 | 618 | 2.0 | 133.15 |
| 13:38:00 | 618 | 2.0 | 133.18 |
| 13:38:01 | 618 | 2.0 | 133.21 |
| 13:38:02 | 618 | 2.0 | 133.25 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:38:03 | 619 | 2.0 | 133.28 |
| 13:38:04 | 619 | 2.0 | 133.31 |
| 13:38:05 | 619 | 2.0 | 133.35 |
| 13:38:06 | 620 | 2.0 | 133.38 |
| 13:38:07 | 621 | 2.0 | 133.41 |
| 13:38:08 | 621 | 2.0 | 133.45 |
| 13:38:09 | 622 | 2.0 | 133.48 |
| 13:38:10 | 622 | 2.0 | 133.51 |
| 13:38:11 | 623 | 2.0 | 133.55 |
| 13:38:12 | 623 | 2.0 | 133.58 |
| 13:38:13 | 623 | 2.0 | 133.62 |
| 13:38:14 | 624 | 2.0 | 133.65 |
| 13:38:15 | 624 | 2.0 | 133.68 |
| 13:38:16 | 624 | 2.0 | 133.72 |
| 13:38:17 | 625 | 2.0 | 133.75 |
| 13:38:18 | 625 | 2.0 | 133.78 |
| 13:38:19 | 626 | 2.0 | 133.82 |
| 13:38:20 | 626 | 2.0 | 133.85 |
| 13:38:21 | 626 | 2.0 | 133.88 |
| 13:38:22 | 627 | 2.0 | 133.92 |
| 13:38:23 | 627 | 2.0 | 133.95 |
| 13:38:24 | 627 | 2.0 | 133.98 |
| 13:38:25 | 627 | 2.0 | 134.02 |
| 13:38:26 | 627 | 2.0 | 134.05 |
| 13:38:27 | 627 | 2.0 | 134.08 |
| 13:38:28 | 627 | 2.0 | 134.12 |
| 13:38:29 | 628 | 2.0 | 134.15 |
| 13:38:30 | 628 | 2.0 | 134.19 |
| 13:38:31 | 629 | 2.0 | 134.22 |
| 13:38:32 | 630 | 2.0 | 134.25 |
| 13:38:33 | 630 | 2.0 | 134.29 |
| 13:38:34 | 631 | 2.0 | 134.32 |
| 13:38:35 | 631 | 2.0 | 134.35 |
| 13:38:36 | 632 | 2.0 | 134.39 |
| 13:38:37 | 632 | 2.0 | 134.42 |
| 13:38:38 | 632 | 2.0 | 134.45 |
| 13:38:39 | 633 | 2.0 | 134.49 |
| 13:38:40 | 633 | 2.0 | 134.52 |
| 13:38:41 | 633 | 2.0 | 134.55 |
| 13:38:42 | 634 | 2.0 | 134.59 |
| 13:38:43 | 634 | 2.0 | 134.62 |
| 13:38:44 | 635 | 2.0 | 134.65 |
| 13:38:45 | 635 | 2.0 | 134.69 |
| 13:38:46 | 636 | 2.0 | 134.72 |
| 13:38:47 | 636 | 2.0 | 134.75 |
| 13:38:48 | 636 | 2.0 | 134.79 |
| 13:38:49 | 637 | 2.0 | 134.82 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:38:50 | 637 | 2.0 | 134.86 |
| 13:38:51 | 637 | 2.0 | 134.89 |
| 13:38:52 | 637 | 2.0 | 134.92 |
| 13:38:53 | 637 | 2.0 | 134.96 |
| 13:38:54 | 638 | 2.0 | 134.99 |
| 13:38:55 | 638 | 2.0 | 135.02 |
| 13:38:56 | 638 | 2.0 | 135.06 |
| 13:38:57 | 639 | 2.0 | 135.09 |
| 13:38:58 | 639 | 2.0 | 135.12 |
| 13:38:59 | 640 | 2.0 | 135.16 |
| 13:39:00 | 641 | 2.0 | 135.19 |
| 13:39:01 | 641 | 2.0 | 135.22 |
| 13:39:02 | 642 | 2.0 | 135.26 |
| 13:39:03 | 642 | 2.0 | 135.29 |
| 13:39:04 | 642 | 2.0 | 135.32 |
| 13:39:05 | 642 | 2.0 | 135.36 |
| 13:39:06 | 643 | 2.0 | 135.39 |
| 13:39:07 | 643 | 2.0 | 135.42 |
| 13:39:08 | 643 | 2.0 | 135.46 |
| 13:39:09 | 644 | 2.0 | 135.49 |
| 13:39:10 | 644 | 2.0 | 135.52 |
| 13:39:11 | 644 | 2.0 | 135.56 |
| 13:39:12 | 645 | 2.0 | 135.59 |
| 13:39:13 | 645 | 2.0 | 135.63 |
| 13:39:14 | 646 | 2.0 | 135.66 |
| 13:39:15 | 646 | 2.0 | 135.69 |
| 13:39:16 | 647 | 2.0 | 135.73 |
| 13:39:17 | 647 | 2.0 | 135.76 |
| 13:39:18 | 647 | 2.0 | 135.79 |
| 13:39:19 | 647 | 2.0 | 135.83 |
| 13:39:20 | 647 | 2.0 | 135.86 |
| 13:39:21 | 648 | 2.0 | 135.89 |
| 13:39:22 | 648 | 2.0 | 135.93 |
| 13:39:23 | 649 | 2.0 | 135.96 |
| 13:39:24 | 649 | 2.0 | 135.99 |
| 13:39:25 | 649 | 2.0 | 136.03 |
| 13:39:26 | 650 | 2.0 | 136.06 |
| 13:39:27 | 650 | 2.0 | 136.09 |
| 13:39:28 | 650 | 2.0 | 136.13 |
| 13:39:29 | 651 | 2.0 | 136.16 |
| 13:39:30 | 653 | 2.0 | 136.19 |
| 13:39:31 | 655 | 2.1 | 136.23 |
| 13:39:32 | 657 | 2.1 | 136.26 |
| 13:39:33 | 659 | 2.2 | 136.30 |
| 13:39:34 | 660 | 2.2 | 136.34 |
| 13:39:35 | 662 | 2.2 | 136.37 |
| 13:39:36 | 664 | 2.3 | 136.41 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:39:37 | 666 | 2.3 | 136.45 |
| 13:39:38 | 669 | 2.4 | 136.49 |
| 13:39:39 | 672 | 2.4 | 136.53 |
| 13:39:40 | 675 | 2.5 | 136.57 |
| 13:39:41 | 678 | 2.5 | 136.61 |
| 13:39:42 | 680 | 2.5 | 136.65 |
| 13:39:43 | 682 | 2.6 | 136.70 |
| 13:39:44 | 684 | 2.6 | 136.74 |
| 13:39:45 | 688 | 2.6 | 136.78 |
| 13:39:46 | 691 | 2.7 | 136.83 |
| 13:39:47 | 695 | 2.7 | 136.87 |
| 13:39:48 | 699 | 2.8 | 136.92 |
| 13:39:49 | 702 | 2.8 | 136.97 |
| 13:39:50 | 706 | 2.8 | 137.01 |
| 13:39:51 | 709 | 2.9 | 137.06 |
| 13:39:52 | 713 | 2.9 | 137.11 |
| 13:39:53 | 717 | 2.9 | 137.16 |
| 13:39:54 | 720 | 3.0 | 137.21 |
| 13:39:55 | 723 | 3.0 | 137.26 |
| 13:39:56 | 727 | 3.0 | 137.31 |
| 13:39:57 | 730 | 3.0 | 137.36 |
| 13:39:58 | 732 | 3.0 | 137.41 |
| 13:39:59 | 736 | 3.0 | 137.46 |
| 13:40:00 | 739 | 3.0 | 137.51 |
| 13:40:01 | 742 | 3.0 | 137.56 |
| 13:40:02 | 745 | 3.0 | 137.61 |
| 13:40:03 | 748 | 3.0 | 137.66 |
| 13:40:04 | 750 | 3.0 | 137.71 |
| 13:40:05 | 753 | 3.0 | 137.76 |
| 13:40:06 | 755 | 3.0 | 137.81 |
| 13:40:07 | 758 | 3.0 | 137.86 |
| 13:40:08 | 760 | 3.0 | 137.91 |
| 13:40:09 | 763 | 3.0 | 137.96 |
| 13:40:10 | 766 | 3.0 | 138.01 |
| 13:40:11 | 768 | 3.0 | 138.06 |
| 13:40:12 | 771 | 3.0 | 138.11 |
| 13:40:13 | 774 | 3.0 | 138.17 |
| 13:40:14 | 776 | 3.0 | 138.22 |
| 13:40:15 | 778 | 3.0 | 138.27 |
| 13:40:16 | 781 | 3.0 | 138.32 |
| 13:40:17 | 783 | 3.0 | 138.37 |
| 13:40:18 | 786 | 3.0 | 138.42 |
| 13:40:19 | 789 | 3.0 | 138.47 |
| 13:40:20 | 792 | 3.0 | 138.52 |
| 13:40:21 | 794 | 3.0 | 138.57 |
| 13:40:22 | 796 | 3.0 | 138.62 |
| 13:40:23 | 799 | 3.0 | 138.67 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:40:24 | 801 | 3.0 | 138.72 |
| 13:40:25 | 803 | 3.0 | 138.77 |
| 13:40:26 | 805 | 3.0 | 138.82 |
| 13:40:27 | 808 | 3.0 | 138.87 |
| 13:40:28 | 810 | 3.0 | 138.92 |
| 13:40:29 | 812 | 3.0 | 138.97 |
| 13:40:30 | 815 | 3.0 | 139.02 |
| 13:40:31 | 817 | 3.0 | 139.07 |
| 13:40:32 | 819 | 3.0 | 139.12 |
| 13:40:33 | 822 | 3.0 | 139.18 |
| 13:40:34 | 824 | 3.0 | 139.23 |
| 13:40:35 | 827 | 3.0 | 139.28 |
| 13:40:36 | 829 | 3.0 | 139.33 |
| 13:40:37 | 831 | 3.0 | 139.38 |
| 13:40:38 | 834 | 3.0 | 139.43 |
| 13:40:39 | 836 | 3.0 | 139.48 |
| 13:40:40 | 837 | 3.0 | 139.53 |
| 13:40:41 | 840 | 3.0 | 139.58 |
| 13:40:42 | 843 | 3.0 | 139.63 |
| 13:40:43 | 845 | 3.0 | 139.68 |
| 13:40:44 | 847 | 3.0 | 139.73 |
| 13:40:45 | 849 | 3.0 | 139.78 |
| 13:40:46 | 851 | 3.0 | 139.83 |
| 13:40:47 | 854 | 3.0 | 139.88 |
| 13:40:48 | 855 | 3.0 | 139.93 |
| 13:40:49 | 857 | 3.0 | 139.98 |
| 13:40:50 | 860 | 3.0 | 140.03 |
| 13:40:51 | 862 | 3.0 | 140.08 |
| 13:40:52 | 863 | 3.0 | 140.13 |
| 13:40:53 | 865 | 3.0 | 140.19 |
| 13:40:54 | 867 | 3.0 | 140.24 |
| 13:40:55 | 870 | 3.0 | 140.29 |
| 13:40:56 | 872 | 3.0 | 140.34 |
| 13:40:57 | 875 | 3.0 | 140.39 |
| 13:40:58 | 876 | 3.0 | 140.44 |
| 13:40:59 | 879 | 3.0 | 140.49 |
| 13:41:00 | 881 | 3.0 | 140.54 |
| 13:41:01 | 881 | 3.0 | 140.59 |
| 13:41:02 | 867 | 3.0 | 140.64 |
| 13:41:03 | 858 | 3.0 | 140.69 |
| 13:41:04 | 851 | 3.0 | 140.74 |
| 13:41:05 | 848 | 3.0 | 140.79 |
| 13:41:06 | 845 | 3.0 | 140.84 |
| 13:41:07 | 843 | 3.0 | 140.89 |
| 13:41:08 | 842 | 3.0 | 140.94 |
| 13:41:09 | 843 | 3.0 | 140.99 |
| 13:41:10 | 846 | 3.0 | 141.04 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:41:11 | 851 | 3.0 | 141.09 |
| 13:41:12 | 857 | 3.0 | 141.14 |
| 13:41:13 | 862 | 3.0 | 141.19 |
| 13:41:14 | 867 | 3.0 | 141.24 |
| 13:41:15 | 872 | 3.0 | 141.30 |
| 13:41:16 | 875 | 3.0 | 141.35 |
| 13:41:17 | 878 | 3.0 | 141.40 |
| 13:41:18 | 882 | 3.0 | 141.45 |
| 13:41:19 | 883 | 3.0 | 141.50 |
| 13:41:20 | 885 | 3.0 | 141.55 |
| 13:41:21 | 887 | 3.0 | 141.60 |
| 13:41:22 | 889 | 3.0 | 141.65 |
| 13:41:23 | 891 | 3.0 | 141.70 |
| 13:41:24 | 893 | 3.0 | 141.75 |
| 13:41:25 | 895 | 3.0 | 141.80 |
| 13:41:26 | 898 | 3.0 | 141.85 |
| 13:41:27 | 900 | 3.0 | 141.90 |
| 13:41:28 | 903 | 3.0 | 141.95 |
| 13:41:29 | 905 | 3.0 | 142.00 |
| 13:41:30 | 908 | 3.0 | 142.05 |
| 13:41:31 | 911 | 3.0 | 142.10 |
| 13:41:32 | 913 | 3.0 | 142.15 |
| 13:41:33 | 916 | 3.0 | 142.20 |
| 13:41:34 | 919 | 3.0 | 142.25 |
| 13:41:35 | 922 | 3.0 | 142.30 |
| 13:41:36 | 925 | 3.0 | 142.35 |
| 13:41:37 | 927 | 3.0 | 142.41 |
| 13:41:38 | 930 | 3.0 | 142.46 |
| 13:41:39 | 933 | 3.0 | 142.51 |
| 13:41:40 | 936 | 3.0 | 142.56 |
| 13:41:41 | 939 | 3.0 | 142.61 |
| 13:41:42 | 942 | 3.0 | 142.66 |
| 13:41:43 | 944 | 3.0 | 142.71 |
| 13:41:44 | 946 | 3.0 | 142.76 |
| 13:41:45 | 949 | 3.0 | 142.81 |
| 13:41:46 | 952 | 3.0 | 142.86 |
| 13:41:47 | 954 | 3.0 | 142.91 |
| 13:41:48 | 957 | 3.0 | 142.96 |
| 13:41:49 | 959 | 3.0 | 143.01 |
| 13:41:50 | 962 | 3.0 | 143.06 |
| 13:41:51 | 964 | 3.0 | 143.11 |
| 13:41:52 | 967 | 3.0 | 143.16 |
| 13:41:53 | 969 | 3.0 | 143.21 |
| 13:41:54 | 972 | 3.0 | 143.26 |
| 13:41:55 | 974 | 3.0 | 143.31 |
| 13:41:56 | 976 | 3.0 | 143.36 |
| 13:41:57 | 979 | 3.0 | 143.41 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:41:58 | 981 | 3.0 | 143.46 |
| 13:41:59 | 984 | 3.0 | 143.51 |
| 13:42:00 | 986 | 3.0 | 143.56 |
| 13:42:01 | 987 | 3.0 | 143.61 |
| 13:42:02 | 991 | 3.0 | 143.67 |
| 13:42:03 | 993 | 3.0 | 143.72 |
| 13:42:04 | 995 | 3.0 | 143.77 |
| 13:42:05 | 998 | 3.0 | 143.82 |
| 13:42:06 | 1000 | 3.0 | 143.87 |
| 13:42:07 | 1002 | 3.0 | 143.92 |
| 13:42:08 | 1004 | 3.0 | 143.97 |
| 13:42:09 | 1007 | 3.0 | 144.02 |
| 13:42:10 | 1009 | 3.0 | 144.07 |
| 13:42:11 | 1011 | 3.0 | 144.12 |
| 13:42:12 | 1013 | 3.0 | 144.17 |
| 13:42:13 | 1015 | 3.0 | 144.22 |
| 13:42:14 | 1017 | 3.0 | 144.27 |
| 13:42:15 | 1019 | 3.0 | 144.32 |
| 13:42:16 | 1022 | 3.0 | 144.37 |
| 13:42:17 | 1024 | 3.0 | 144.42 |
| 13:42:18 | 1026 | 3.0 | 144.47 |
| 13:42:19 | 1028 | 3.0 | 144.52 |
| 13:42:20 | 1030 | 3.0 | 144.57 |
| 13:42:21 | 1032 | 3.0 | 144.62 |
| 13:42:22 | 1034 | 3.0 | 144.67 |
| 13:42:23 | 1037 | 3.0 | 144.72 |
| 13:42:24 | 1039 | 3.0 | 144.77 |
| 13:42:25 | 1041 | 3.0 | 144.82 |
| 13:42:26 | 1043 | 3.0 | 144.87 |
| 13:42:27 | 1046 | 3.0 | 144.93 |
| 13:42:28 | 1048 | 3.0 | 144.98 |
| 13:42:29 | 1049 | 3.0 | 145.03 |
| 13:42:30 | 1052 | 3.0 | 145.08 |
| 13:42:31 | 1054 | 3.0 | 145.13 |
| 13:42:32 | 1056 | 3.0 | 145.18 |
| 13:42:33 | 1058 | 3.0 | 145.23 |
| 13:42:34 | 1060 | 3.0 | 145.28 |
| 13:42:35 | 1062 | 3.0 | 145.33 |
| 13:42:36 | 1064 | 3.0 | 145.38 |
| 13:42:37 | 1066 | 3.0 | 145.43 |
| 13:42:38 | 1068 | 3.0 | 145.48 |
| 13:42:39 | 1070 | 3.0 | 145.53 |
| 13:42:40 | 1072 | 3.0 | 145.58 |
| 13:42:41 | 1075 | 3.0 | 145.63 |
| 13:42:42 | 1078 | 3.0 | 145.68 |
| 13:42:43 | 1079 | 3.0 | 145.73 |
| 13:42:44 | 1082 | 3.0 | 145.78 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:42:45 | 1084 | 3.0 | 145.83 |
| 13:42:46 | 1086 | 3.0 | 145.88 |
| 13:42:47 | 1088 | 3.0 | 145.93 |
| 13:42:48 | 1091 | 3.0 | 145.98 |
| 13:42:49 | 1093 | 3.0 | 146.03 |
| 13:42:50 | 1095 | 3.0 | 146.08 |
| 13:42:51 | 1097 | 3.0 | 146.13 |
| 13:42:52 | 1098 | 3.0 | 146.18 |
| 13:42:53 | 1100 | 3.0 | 146.23 |
| 13:42:54 | 1103 | 3.0 | 146.29 |
| 13:42:55 | 1105 | 3.0 | 146.34 |
| 13:42:56 | 1107 | 3.0 | 146.39 |
| 13:42:57 | 1109 | 3.0 | 146.44 |
| 13:42:58 | 1110 | 3.0 | 146.49 |
| 13:42:59 | 1113 | 3.0 | 146.54 |
| 13:43:00 | 1115 | 3.0 | 146.59 |
| 13:43:01 | 1116 | 3.0 | 146.64 |
| 13:43:02 | 1119 | 3.0 | 146.69 |
| 13:43:03 | 1121 | 3.0 | 146.74 |
| 13:43:04 | 1123 | 3.0 | 146.79 |
| 13:43:05 | 1125 | 3.0 | 146.84 |
| 13:43:06 | 1126 | 3.0 | 146.89 |
| 13:43:07 | 1128 | 3.0 | 146.94 |
| 13:43:08 | 1130 | 3.0 | 146.99 |
| 13:43:09 | 1131 | 3.0 | 147.04 |
| 13:43:10 | 1131 | 3.0 | 147.09 |
| 13:43:11 | 1133 | 3.0 | 147.14 |
| 13:43:12 | 1133 | 3.0 | 147.19 |
| 13:43:13 | 1135 | 3.0 | 147.24 |
| 13:43:14 | 1136 | 3.0 | 147.29 |
| 13:43:15 | 1138 | 3.0 | 147.34 |
| 13:43:16 | 1139 | 3.0 | 147.39 |
| 13:43:17 | 1141 | 3.0 | 147.44 |
| 13:43:18 | 1143 | 3.0 | 147.49 |
| 13:43:19 | 1144 | 3.0 | 147.54 |
| 13:43:20 | 1146 | 3.0 | 147.59 |
| 13:43:21 | 1148 | 3.0 | 147.64 |
| 13:43:22 | 1150 | 3.0 | 147.70 |
| 13:43:23 | 1152 | 3.0 | 147.75 |
| 13:43:24 | 1153 | 3.0 | 147.80 |
| 13:43:25 | 1155 | 3.0 | 147.85 |
| 13:43:26 | 1157 | 3.0 | 147.90 |
| 13:43:27 | 1158 | 3.0 | 147.95 |
| 13:43:28 | 1160 | 3.0 | 148.00 |
| 13:43:29 | 1161 | 3.0 | 148.05 |
| 13:43:30 | 1162 | 3.0 | 148.10 |
| 13:43:31 | 1164 | 3.0 | 148.15 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:43:32 | 1166 | 3.0 | 148.20 |
| 13:43:33 | 1167 | 3.0 | 148.25 |
| 13:43:34 | 1169 | 3.0 | 148.30 |
| 13:43:35 | 1170 | 3.0 | 148.35 |
| 13:43:36 | 1172 | 3.0 | 148.40 |
| 13:43:37 | 1174 | 3.0 | 148.45 |
| 13:43:38 | 1175 | 3.0 | 148.50 |
| 13:43:39 | 1176 | 3.0 | 148.55 |
| 13:43:40 | 1178 | 3.0 | 148.60 |
| 13:43:41 | 1179 | 3.0 | 148.65 |
| 13:43:42 | 1181 | 3.0 | 148.70 |
| 13:43:43 | 1183 | 3.0 | 148.75 |
| 13:43:44 | 1185 | 3.0 | 148.80 |
| 13:43:45 | 1186 | 3.0 | 148.85 |
| 13:43:46 | 1188 | 3.0 | 148.90 |
| 13:43:47 | 1189 | 3.0 | 148.95 |
| 13:43:48 | 1192 | 3.0 | 149.00 |
| 13:43:49 | 1193 | 3.0 | 149.05 |
| 13:43:50 | 1195 | 3.0 | 149.10 |
| 13:43:51 | 1196 | 3.0 | 149.15 |
| 13:43:52 | 1198 | 3.0 | 149.21 |
| 13:43:53 | 1199 | 3.0 | 149.26 |
| 13:43:54 | 1202 | 3.0 | 149.31 |
| 13:43:55 | 1203 | 3.0 | 149.36 |
| 13:43:56 | 1205 | 3.0 | 149.41 |
| 13:43:57 | 1206 | 3.0 | 149.46 |
| 13:43:58 | 1208 | 3.0 | 149.51 |
| 13:43:59 | 1209 | 3.0 | 149.56 |
| 13:44:00 | 1211 | 3.0 | 149.61 |
| 13:44:01 | 1213 | 3.0 | 149.66 |
| 13:44:02 | 1214 | 3.0 | 149.71 |
| 13:44:03 | 1216 | 3.0 | 149.76 |
| 13:44:04 | 1218 | 3.0 | 149.81 |
| 13:44:05 | 1219 | 3.0 | 149.86 |
| 13:44:06 | 1221 | 3.0 | 149.91 |
| 13:44:07 | 1221 | 3.0 | 149.96 |
| 13:44:08 | 1222 | 3.0 | 150.01 |
| 13:44:09 | 1225 | 3.0 | 150.06 |
| 13:44:10 | 1226 | 3.0 | 150.11 |
| 13:44:11 | 1228 | 3.0 | 150.16 |
| 13:44:12 | 1229 | 3.0 | 150.21 |
| 13:44:13 | 1231 | 3.0 | 150.26 |
| 13:44:14 | 1233 | 3.0 | 150.31 |
| 13:44:15 | 1234 | 3.0 | 150.36 |
| 13:44:16 | 1236 | 3.0 | 150.41 |
| 13:44:17 | 1238 | 3.0 | 150.46 |
| 13:44:18 | 1240 | 3.0 | 150.51 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:44:19 | 1242 | 3.0 | 150.56 |
| 13:44:20 | 1243 | 3.0 | 150.61 |
| 13:44:21 | 1245 | 3.0 | 150.66 |
| 13:44:22 | 1246 | 3.0 | 150.71 |
| 13:44:23 | 1248 | 3.0 | 150.77 |
| 13:44:24 | 1248 | 3.0 | 150.82 |
| 13:44:25 | 1249 | 3.0 | 150.87 |
| 13:44:26 | 1249 | 3.0 | 150.92 |
| 13:44:27 | 1251 | 3.0 | 150.97 |
| 13:44:28 | 1253 | 3.0 | 151.02 |
| 13:44:29 | 1255 | 3.0 | 151.07 |
| 13:44:30 | 1256 | 3.0 | 151.12 |
| 13:44:31 | 1258 | 3.0 | 151.17 |
| 13:44:32 | 1260 | 3.0 | 151.22 |
| 13:44:33 | 1262 | 3.0 | 151.27 |
| 13:44:34 | 1264 | 3.0 | 151.32 |
| 13:44:35 | 1265 | 3.0 | 151.37 |
| 13:44:36 | 1266 | 3.0 | 151.42 |
| 13:44:37 | 1267 | 3.0 | 151.47 |
| 13:44:38 | 1268 | 3.0 | 151.52 |
| 13:44:39 | 1270 | 3.0 | 151.57 |
| 13:44:40 | 1271 | 3.0 | 151.62 |
| 13:44:41 | 1272 | 3.0 | 151.67 |
| 13:44:42 | 1273 | 3.0 | 151.72 |
| 13:44:43 | 1274 | 3.0 | 151.77 |
| 13:44:44 | 1276 | 3.0 | 151.82 |
| 13:44:45 | 1277 | 3.0 | 151.87 |
| 13:44:46 | 1279 | 3.0 | 151.92 |
| 13:44:47 | 1281 | 3.0 | 151.97 |
| 13:44:48 | 1282 | 3.0 | 152.02 |
| 13:44:49 | 1284 | 3.0 | 152.07 |
| 13:44:50 | 1285 | 3.0 | 152.12 |
| 13:44:51 | 1288 | 3.0 | 152.17 |
| 13:44:52 | 1290 | 3.0 | 152.22 |
| 13:44:53 | 1291 | 3.0 | 152.27 |
| 13:44:54 | 1293 | 3.0 | 152.33 |
| 13:44:55 | 1295 | 3.0 | 152.38 |
| 13:44:56 | 1296 | 3.0 | 152.43 |
| 13:44:57 | 1298 | 3.0 | 152.48 |
| 13:44:58 | 1300 | 3.0 | 152.53 |
| 13:44:59 | 1301 | 3.0 | 152.58 |
| 13:45:00 | 1303 | 3.0 | 152.63 |
| 13:45:01 | 1305 | 3.0 | 152.68 |
| 13:45:02 | 1307 | 3.0 | 152.73 |
| 13:45:03 | 1309 | 3.0 | 152.78 |
| 13:45:04 | 1311 | 3.0 | 152.83 |
| 13:45:05 | 1313 | 3.0 | 152.88 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:45:06 | 1315 | 3.0 | 152.93 |
| 13:45:07 | 1317 | 3.0 | 152.98 |
| 13:45:08 | 1319 | 3.0 | 153.03 |
| 13:45:09 | 1321 | 3.0 | 153.08 |
| 13:45:10 | 1323 | 3.0 | 153.13 |
| 13:45:11 | 1326 | 3.0 | 153.18 |
| 13:45:12 | 1328 | 3.0 | 153.23 |
| 13:45:13 | 1330 | 3.0 | 153.28 |
| 13:45:14 | 1332 | 3.0 | 153.33 |
| 13:45:15 | 1334 | 3.0 | 153.38 |
| 13:45:16 | 1336 | 3.0 | 153.43 |
| 13:45:17 | 1338 | 3.0 | 153.48 |
| 13:45:18 | 1340 | 3.0 | 153.53 |
| 13:45:19 | 1342 | 3.0 | 153.58 |
| 13:45:20 | 1344 | 3.0 | 153.63 |
| 13:45:21 | 1347 | 3.0 | 153.68 |
| 13:45:22 | 1349 | 3.0 | 153.73 |
| 13:45:23 | 1351 | 3.0 | 153.78 |
| 13:45:24 | 1353 | 3.0 | 153.83 |
| 13:45:25 | 1355 | 3.0 | 153.88 |
| 13:45:26 | 1357 | 3.0 | 153.93 |
| 13:45:27 | 1360 | 3.0 | 153.98 |
| 13:45:28 | 1362 | 3.0 | 154.04 |
| 13:45:29 | 1365 | 3.0 | 154.09 |
| 13:45:30 | 1367 | 3.0 | 154.14 |
| 13:45:31 | 1370 | 3.0 | 154.19 |
| 13:45:32 | 1373 | 3.0 | 154.24 |
| 13:45:33 | 1375 | 3.0 | 154.29 |
| 13:45:34 | 1377 | 3.0 | 154.34 |
| 13:45:35 | 1379 | 3.0 | 154.39 |
| 13:45:36 | 1381 | 3.0 | 154.44 |
| 13:45:37 | 1383 | 3.0 | 154.49 |
| 13:45:38 | 1385 | 3.0 | 154.54 |
| 13:45:39 | 1387 | 3.0 | 154.59 |
| 13:45:40 | 1389 | 3.0 | 154.64 |
| 13:45:41 | 1391 | 3.0 | 154.69 |
| 13:45:42 | 1393 | 3.0 | 154.74 |
| 13:45:43 | 1395 | 3.0 | 154.79 |
| 13:45:44 | 1397 | 3.0 | 154.84 |
| 13:45:45 | 1400 | 3.0 | 154.89 |
| 13:45:46 | 1403 | 3.0 | 154.94 |
| 13:45:47 | 1406 | 3.0 | 154.99 |
| 13:45:48 | 1408 | 3.0 | 155.04 |
| 13:45:49 | 1410 | 3.0 | 155.09 |
| 13:45:50 | 1412 | 3.0 | 155.14 |
| 13:45:51 | 1415 | 3.0 | 155.19 |
| 13:45:52 | 1418 | 3.0 | 155.24 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:45:53 | 1419 | 3.0 | 155.29 |
| 13:45:54 | 1422 | 3.0 | 155.34 |
| 13:45:55 | 1424 | 3.0 | 155.39 |
| 13:45:56 | 1427 | 3.0 | 155.44 |
| 13:45:57 | 1429 | 3.0 | 155.49 |
| 13:45:58 | 1431 | 3.0 | 155.54 |
| 13:45:59 | 1433 | 3.0 | 155.59 |
| 13:46:00 | 1435 | 3.0 | 155.64 |
| 13:46:01 | 1437 | 3.0 | 155.69 |
| 13:46:02 | 1440 | 3.0 | 155.74 |
| 13:46:03 | 1442 | 3.0 | 155.79 |
| 13:46:04 | 1444 | 3.0 | 155.85 |
| 13:46:05 | 1446 | 3.0 | 155.90 |
| 13:46:06 | 1448 | 3.0 | 155.95 |
| 13:46:07 | 1451 | 3.0 | 156.00 |
| 13:46:08 | 1453 | 3.0 | 156.05 |
| 13:46:09 | 1456 | 3.0 | 156.10 |
| 13:46:10 | 1458 | 3.0 | 156.15 |
| 13:46:11 | 1460 | 3.0 | 156.20 |
| 13:46:12 | 1462 | 3.0 | 156.25 |
| 13:46:13 | 1465 | 3.0 | 156.30 |
| 13:46:14 | 1467 | 3.0 | 156.35 |
| 13:46:15 | 1469 | 3.0 | 156.40 |
| 13:46:16 | 1471 | 3.0 | 156.45 |
| 13:46:17 | 1473 | 3.0 | 156.50 |
| 13:46:18 | 1476 | 3.0 | 156.55 |
| 13:46:19 | 1478 | 3.0 | 156.60 |
| 13:46:20 | 1481 | 3.0 | 156.65 |
| 13:46:21 | 1483 | 3.0 | 156.70 |
| 13:46:22 | 1485 | 3.0 | 156.75 |
| 13:46:23 | 1487 | 3.0 | 156.80 |
| 13:46:24 | 1489 | 3.0 | 156.85 |
| 13:46:25 | 1491 | 3.0 | 156.90 |
| 13:46:26 | 1493 | 3.0 | 156.95 |
| 13:46:27 | 1495 | 3.0 | 157.00 |
| 13:46:28 | 1497 | 3.0 | 157.05 |
| 13:46:29 | 1500 | 3.0 | 157.10 |
| 13:46:30 | 1502 | 3.0 | 157.15 |
| 13:46:31 | 1505 | 3.0 | 157.20 |
| 13:46:32 | 1507 | 3.0 | 157.25 |
| 13:46:33 | 1509 | 3.0 | 157.30 |
| 13:46:34 | 1512 | 3.0 | 157.35 |
| 13:46:35 | 1514 | 3.0 | 157.40 |
| 13:46:36 | 1517 | 3.0 | 157.45 |
| 13:46:37 | 1519 | 3.0 | 157.50 |
| 13:46:38 | 1521 | 3.0 | 157.55 |
| 13:46:39 | 1523 | 3.0 | 157.60 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:46:40 | 1526 | 3.0 | 157.65 |
| 13:46:41 | 1528 | 3.0 | 157.70 |
| 13:46:42 | 1530 | 3.0 | 157.75 |
| 13:46:43 | 1533 | 3.0 | 157.80 |
| 13:46:44 | 1534 | 3.0 | 157.85 |
| 13:46:45 | 1536 | 3.0 | 157.90 |
| 13:46:46 | 1538 | 3.0 | 157.96 |
| 13:46:47 | 1540 | 3.0 | 158.01 |
| 13:46:48 | 1542 | 3.0 | 158.06 |
| 13:46:49 | 1544 | 3.0 | 158.11 |
| 13:46:50 | 1546 | 3.0 | 158.16 |
| 13:46:51 | 1548 | 3.0 | 158.21 |
| 13:46:52 | 1550 | 3.0 | 158.26 |
| 13:46:53 | 1552 | 3.0 | 158.31 |
| 13:46:54 | 1555 | 3.0 | 158.36 |
| 13:46:55 | 1557 | 3.0 | 158.41 |
| 13:46:56 | 1559 | 3.0 | 158.46 |
| 13:46:57 | 1561 | 3.0 | 158.51 |
| 13:46:58 | 1563 | 3.0 | 158.56 |
| 13:46:59 | 1566 | 3.0 | 158.61 |
| 13:47:00 | 1568 | 3.0 | 158.66 |
| 13:47:01 | 1570 | 3.0 | 158.71 |
| 13:47:02 | 1572 | 3.0 | 158.76 |
| 13:47:03 | 1574 | 3.0 | 158.81 |
| 13:47:04 | 1575 | 3.0 | 158.86 |
| 13:47:05 | 1576 | 3.0 | 158.91 |
| 13:47:06 | 1577 | 3.0 | 158.96 |
| 13:47:07 | 1578 | 3.0 | 159.01 |
| 13:47:08 | 1579 | 3.0 | 159.06 |
| 13:47:09 | 1581 | 3.0 | 159.11 |
| 13:47:10 | 1582 | 3.0 | 159.16 |
| 13:47:11 | 1583 | 3.0 | 159.21 |
| 13:47:12 | 1585 | 3.0 | 159.26 |
| 13:47:13 | 1586 | 3.0 | 159.31 |
| 13:47:14 | 1587 | 3.0 | 159.36 |
| 13:47:15 | 1589 | 3.0 | 159.41 |
| 13:47:16 | 1590 | 3.0 | 159.46 |
| 13:47:17 | 1592 | 3.0 | 159.51 |
| 13:47:18 | 1593 | 3.0 | 159.56 |
| 13:47:19 | 1594 | 3.0 | 159.61 |
| 13:47:20 | 1597 | 3.0 | 159.66 |
| 13:47:21 | 1598 | 3.0 | 159.71 |
| 13:47:22 | 1599 | 3.0 | 159.76 |
| 13:47:23 | 1601 | 3.0 | 159.81 |
| 13:47:24 | 1603 | 3.0 | 159.86 |
| 13:47:25 | 1605 | 3.0 | 159.91 |
| 13:47:26 | 1607 | 3.0 | 159.96 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:47:27 | 1609 | 3.0 | 160.01 |
| 13:47:28 | 1611 | 3.0 | 160.06 |
| 13:47:29 | 1612 | 3.0 | 160.11 |
| 13:47:30 | 1615 | 3.0 | 160.16 |
| 13:47:31 | 1617 | 3.0 | 160.21 |
| 13:47:32 | 1619 | 3.0 | 160.26 |
| 13:47:33 | 1621 | 3.0 | 160.31 |
| 13:47:34 | 1623 | 3.0 | 160.36 |
| 13:47:35 | 1625 | 3.0 | 160.41 |
| 13:47:36 | 1627 | 3.0 | 160.46 |
| 13:47:37 | 1630 | 3.0 | 160.51 |
| 13:47:38 | 1632 | 3.0 | 160.56 |
| 13:47:39 | 1634 | 3.0 | 160.61 |
| 13:47:40 | 1637 | 3.0 | 160.66 |
| 13:47:41 | 1639 | 3.0 | 160.71 |
| 13:47:42 | 1642 | 3.0 | 160.77 |
| 13:47:43 | 1644 | 3.0 | 160.82 |
| 13:47:44 | 1646 | 3.0 | 160.87 |
| 13:47:45 | 1648 | 3.0 | 160.92 |
| 13:47:46 | 1650 | 3.0 | 160.97 |
| 13:47:47 | 1651 | 3.0 | 161.02 |
| 13:47:48 | 1652 | 3.0 | 161.07 |
| 13:47:49 | 1653 | 3.0 | 161.12 |
| 13:47:50 | 1654 | 3.0 | 161.17 |
| 13:47:51 | 1655 | 3.0 | 161.22 |
| 13:47:52 | 1656 | 3.0 | 161.27 |
| 13:47:53 | 1657 | 3.0 | 161.32 |
| 13:47:54 | 1658 | 3.0 | 161.37 |
| 13:47:55 | 1659 | 3.0 | 161.42 |
| 13:47:56 | 1660 | 3.0 | 161.47 |
| 13:47:57 | 1661 | 3.0 | 161.52 |
| 13:47:58 | 1662 | 3.0 | 161.57 |
| 13:47:59 | 1663 | 3.0 | 161.62 |
| 13:48:00 | 1663 | 3.0 | 161.67 |
| 13:48:01 | 1665 | 3.0 | 161.72 |
| 13:48:02 | 1665 | 3.0 | 161.77 |
| 13:48:03 | 1666 | 3.0 | 161.82 |
| 13:48:04 | 1667 | 3.0 | 161.87 |
| 13:48:05 | 1667 | 3.0 | 161.92 |
| 13:48:06 | 1668 | 3.0 | 161.97 |
| 13:48:07 | 1668 | 3.0 | 162.02 |
| 13:48:08 | 1668 | 3.0 | 162.07 |
| 13:48:09 | 1668 | 3.0 | 162.12 |
| 13:48:10 | 1669 | 3.0 | 162.17 |
| 13:48:11 | 1669 | 3.0 | 162.22 |
| 13:48:12 | 1670 | 3.0 | 162.27 |
| 13:48:13 | 1670 | 3.0 | 162.32 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:48:14 | 1671 | 3.0 | 162.37 |
| 13:48:15 | 1671 | 3.0 | 162.42 |
| 13:48:16 | 1672 | 3.0 | 162.47 |
| 13:48:17 | 1673 | 3.0 | 162.52 |
| 13:48:18 | 1673 | 3.0 | 162.57 |
| 13:48:19 | 1674 | 3.0 | 162.62 |
| 13:48:20 | 1674 | 3.0 | 162.67 |
| 13:48:21 | 1675 | 3.0 | 162.72 |
| 13:48:22 | 1675 | 3.0 | 162.77 |
| 13:48:23 | 1676 | 3.0 | 162.82 |
| 13:48:24 | 1676 | 3.0 | 162.87 |
| 13:48:25 | 1676 | 3.0 | 162.92 |
| 13:48:26 | 1677 | 3.0 | 162.97 |
| 13:48:27 | 1677 | 3.0 | 163.02 |
| 13:48:28 | 1678 | 3.0 | 163.07 |
| 13:48:29 | 1679 | 3.0 | 163.12 |
| 13:48:30 | 1679 | 3.0 | 163.17 |
| 13:48:31 | 1679 | 3.0 | 163.22 |
| 13:48:32 | 1680 | 3.0 | 163.27 |
| 13:48:33 | 1681 | 3.0 | 163.32 |
| 13:48:34 | 1682 | 3.0 | 163.37 |
| 13:48:35 | 1682 | 3.0 | 163.42 |
| 13:48:36 | 1683 | 3.0 | 163.47 |
| 13:48:37 | 1684 | 3.0 | 163.52 |
| 13:48:38 | 1685 | 3.0 | 163.57 |
| 13:48:39 | 1685 | 3.0 | 163.62 |
| 13:48:40 | 1686 | 3.0 | 163.68 |
| 13:48:41 | 1687 | 3.0 | 163.73 |
| 13:48:42 | 1687 | 3.0 | 163.78 |
| 13:48:43 | 1688 | 3.0 | 163.83 |
| 13:48:44 | 1689 | 3.0 | 163.88 |
| 13:48:45 | 1691 | 3.0 | 163.93 |
| 13:48:46 | 1692 | 3.0 | 163.98 |
| 13:48:47 | 1693 | 3.0 | 164.03 |
| 13:48:48 | 1694 | 3.0 | 164.08 |
| 13:48:49 | 1696 | 3.0 | 164.13 |
| 13:48:50 | 1697 | 3.0 | 164.18 |
| 13:48:51 | 1697 | 3.0 | 164.23 |
| 13:48:52 | 1698 | 3.0 | 164.28 |
| 13:48:53 | 1699 | 3.0 | 164.33 |
| 13:48:54 | 1699 | 3.0 | 164.38 |
| 13:48:55 | 1701 | 3.0 | 164.43 |
| 13:48:56 | 1702 | 3.0 | 164.48 |
| 13:48:57 | 1702 | 3.0 | 164.53 |
| 13:48:58 | 1703 | 3.0 | 164.58 |
| 13:48:59 | 1703 | 3.0 | 164.63 |
| 13:49:00 | 1703 | 3.0 | 164.68 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:49:01 | 1704 | 3.0 | 164.73 |
| 13:49:02 | 1704 | 3.0 | 164.78 |
| 13:49:03 | 1705 | 3.0 | 164.83 |
| 13:49:04 | 1706 | 3.0 | 164.88 |
| 13:49:05 | 1707 | 3.0 | 164.93 |
| 13:49:06 | 1707 | 3.0 | 164.98 |
| 13:49:07 | 1709 | 3.0 | 165.03 |
| 13:49:08 | 1709 | 3.0 | 165.08 |
| 13:49:09 | 1710 | 3.0 | 165.13 |
| 13:49:10 | 1711 | 3.0 | 165.18 |
| 13:49:11 | 1712 | 3.0 | 165.23 |
| 13:49:12 | 1713 | 3.0 | 165.28 |
| 13:49:13 | 1714 | 3.0 | 165.33 |
| 13:49:14 | 1714 | 3.0 | 165.38 |
| 13:49:15 | 1714 | 3.0 | 165.43 |
| 13:49:16 | 1714 | 3.0 | 165.48 |
| 13:49:17 | 1715 | 3.0 | 165.53 |
| 13:49:18 | 1715 | 3.0 | 165.58 |
| 13:49:19 | 1716 | 3.0 | 165.63 |
| 13:49:20 | 1717 | 3.0 | 165.68 |
| 13:49:21 | 1717 | 3.0 | 165.73 |
| 13:49:22 | 1718 | 3.0 | 165.78 |
| 13:49:23 | 1719 | 3.0 | 165.83 |
| 13:49:24 | 1720 | 3.0 | 165.88 |
| 13:49:25 | 1721 | 3.0 | 165.93 |
| 13:49:26 | 1721 | 3.0 | 165.98 |
| 13:49:27 | 1722 | 3.0 | 166.03 |
| 13:49:28 | 1723 | 3.0 | 166.08 |
| 13:49:29 | 1724 | 3.0 | 166.13 |
| 13:49:30 | 1724 | 3.0 | 166.18 |
| 13:49:31 | 1725 | 3.0 | 166.23 |
| 13:49:32 | 1725 | 3.0 | 166.28 |
| 13:49:33 | 1726 | 3.0 | 166.33 |
| 13:49:34 | 1726 | 3.0 | 166.38 |
| 13:49:35 | 1727 | 3.0 | 166.43 |
| 13:49:36 | 1727 | 3.0 | 166.48 |
| 13:49:37 | 1727 | 3.0 | 166.53 |
| 13:49:38 | 1728 | 3.0 | 166.58 |
| 13:49:39 | 1728 | 3.0 | 166.63 |
| 13:49:40 | 1729 | 3.0 | 166.68 |
| 13:49:41 | 1729 | 3.0 | 166.74 |
| 13:49:42 | 1730 | 3.0 | 166.79 |
| 13:49:43 | 1730 | 3.0 | 166.84 |
| 13:49:44 | 1731 | 3.0 | 166.89 |
| 13:49:45 | 1732 | 3.0 | 166.94 |
| 13:49:46 | 1733 | 3.0 | 166.99 |
| 13:49:47 | 1733 | 3.0 | 167.04 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:49:48 | 1733 | 3.0 | 167.09 |
| 13:49:49 | 1733 | 3.0 | 167.14 |
| 13:49:50 | 1734 | 3.0 | 167.19 |
| 13:49:51 | 1735 | 3.0 | 167.24 |
| 13:49:52 | 1735 | 3.0 | 167.29 |
| 13:49:53 | 1736 | 3.0 | 167.34 |
| 13:49:54 | 1736 | 3.0 | 167.39 |
| 13:49:55 | 1737 | 3.0 | 167.44 |
| 13:49:56 | 1738 | 3.0 | 167.49 |
| 13:49:57 | 1738 | 3.0 | 167.54 |
| 13:49:58 | 1738 | 3.0 | 167.59 |
| 13:49:59 | 1739 | 3.0 | 167.64 |
| 13:50:00 | 1739 | 3.0 | 167.69 |
| 13:50:01 | 1739 | 3.0 | 167.74 |
| 13:50:02 | 1740 | 3.0 | 167.79 |
| 13:50:03 | 1741 | 3.0 | 167.84 |
| 13:50:04 | 1741 | 3.0 | 167.89 |
| 13:50:05 | 1742 | 3.0 | 167.94 |
| 13:50:06 | 1742 | 3.0 | 167.99 |
| 13:50:07 | 1742 | 3.0 | 168.04 |
| 13:50:08 | 1744 | 3.0 | 168.09 |
| 13:50:09 | 1744 | 3.0 | 168.14 |
| 13:50:10 | 1745 | 3.0 | 168.19 |
| 13:50:11 | 1746 | 3.0 | 168.24 |
| 13:50:12 | 1745 | 3.0 | 168.29 |
| 13:50:13 | 1746 | 3.0 | 168.34 |
| 13:50:14 | 1747 | 3.0 | 168.39 |
| 13:50:15 | 1747 | 3.0 | 168.44 |
| 13:50:16 | 1748 | 3.0 | 168.49 |
| 13:50:17 | 1748 | 3.0 | 168.54 |
| 13:50:18 | 1748 | 3.0 | 168.59 |
| 13:50:19 | 1749 | 3.0 | 168.64 |
| 13:50:20 | 1750 | 3.0 | 168.69 |
| 13:50:21 | 1751 | 3.0 | 168.74 |
| 13:50:22 | 1751 | 3.0 | 168.79 |
| 13:50:23 | 1752 | 3.0 | 168.84 |
| 13:50:24 | 1752 | 3.0 | 168.89 |
| 13:50:25 | 1753 | 3.0 | 168.94 |
| 13:50:26 | 1754 | 3.0 | 168.99 |
| 13:50:27 | 1754 | 3.0 | 169.04 |
| 13:50:28 | 1755 | 3.0 | 169.09 |
| 13:50:29 | 1755 | 3.0 | 169.14 |
| 13:50:30 | 1756 | 3.0 | 169.19 |
| 13:50:31 | 1757 | 3.0 | 169.24 |
| 13:50:32 | 1758 | 3.0 | 169.29 |
| 13:50:33 | 1758 | 3.0 | 169.34 |
| 13:50:34 | 1759 | 3.0 | 169.39 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:50:35 | 1759 | 3.0 | 169.44 |
| 13:50:36 | 1760 | 3.0 | 169.49 |
| 13:50:37 | 1761 | 3.0 | 169.54 |
| 13:50:38 | 1762 | 3.0 | 169.59 |
| 13:50:39 | 1762 | 3.0 | 169.64 |
| 13:50:40 | 1762 | 3.0 | 169.69 |
| 13:50:41 | 1762 | 3.0 | 169.74 |
| 13:50:42 | 1763 | 3.0 | 169.79 |
| 13:50:43 | 1763 | 3.0 | 169.85 |
| 13:50:44 | 1763 | 3.0 | 169.90 |
| 13:50:45 | 1764 | 3.0 | 169.95 |
| 13:50:46 | 1764 | 3.0 | 170.00 |
| 13:50:47 | 1765 | 3.0 | 170.05 |
| 13:50:48 | 1766 | 3.0 | 170.10 |
| 13:50:49 | 1766 | 3.0 | 170.15 |
| 13:50:50 | 1766 | 3.0 | 170.20 |
| 13:50:51 | 1767 | 3.0 | 170.25 |
| 13:50:52 | 1767 | 3.0 | 170.30 |
| 13:50:53 | 1767 | 3.0 | 170.35 |
| 13:50:54 | 1768 | 3.0 | 170.40 |
| 13:50:55 | 1768 | 3.0 | 170.45 |
| 13:50:56 | 1768 | 3.0 | 170.50 |
| 13:50:57 | 1769 | 3.0 | 170.55 |
| 13:50:58 | 1769 | 3.0 | 170.60 |
| 13:50:59 | 1769 | 3.0 | 170.65 |
| 13:51:00 | 1770 | 3.0 | 170.70 |
| 13:51:01 | 1770 | 3.0 | 170.75 |
| 13:51:02 | 1770 | 3.0 | 170.80 |
| 13:51:03 | 1771 | 3.0 | 170.85 |
| 13:51:04 | 1771 | 3.0 | 170.90 |
| 13:51:05 | 1772 | 3.0 | 170.95 |
| 13:51:06 | 1772 | 3.0 | 171.00 |
| 13:51:07 | 1772 | 3.0 | 171.05 |
| 13:51:08 | 1772 | 3.0 | 171.10 |
| 13:51:09 | 1773 | 3.0 | 171.15 |
| 13:51:10 | 1773 | 3.0 | 171.20 |
| 13:51:11 | 1774 | 3.0 | 171.25 |
| 13:51:12 | 1774 | 3.0 | 171.30 |
| 13:51:13 | 1774 | 3.0 | 171.35 |
| 13:51:14 | 1775 | 3.0 | 171.40 |
| 13:51:15 | 1775 | 3.0 | 171.45 |
| 13:51:16 | 1775 | 3.0 | 171.50 |
| 13:51:17 | 1776 | 3.0 | 171.55 |
| 13:51:18 | 1776 | 3.0 | 171.60 |
| 13:51:19 | 1776 | 3.0 | 171.65 |
| 13:51:20 | 1777 | 3.0 | 171.70 |
| 13:51:21 | 1777 | 3.0 | 171.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:51:22 | 1777 | 3.0 | 171.80 |
| 13:51:23 | 1778 | 3.0 | 171.85 |
| 13:51:24 | 1778 | 3.0 | 171.90 |
| 13:51:25 | 1778 | 3.0 | 171.95 |
| 13:51:26 | 1779 | 3.0 | 172.00 |
| 13:51:27 | 1779 | 3.0 | 172.05 |
| 13:51:28 | 1780 | 3.0 | 172.10 |
| 13:51:29 | 1780 | 3.0 | 172.15 |
| 13:51:30 | 1780 | 3.0 | 172.20 |
| 13:51:31 | 1781 | 3.0 | 172.25 |
| 13:51:32 | 1781 | 3.0 | 172.30 |
| 13:51:33 | 1781 | 3.0 | 172.35 |
| 13:51:34 | 1781 | 3.0 | 172.40 |
| 13:51:35 | 1781 | 3.0 | 172.45 |
| 13:51:36 | 1780 | 3.0 | 172.50 |
| 13:51:37 | 1781 | 3.0 | 172.55 |
| 13:51:38 | 1781 | 3.0 | 172.60 |
| 13:51:39 | 1781 | 3.0 | 172.65 |
| 13:51:40 | 1782 | 3.0 | 172.70 |
| 13:51:41 | 1781 | 3.0 | 172.75 |
| 13:51:42 | 1781 | 3.0 | 172.80 |
| 13:51:43 | 1782 | 3.0 | 172.85 |
| 13:51:44 | 1782 | 3.0 | 172.90 |
| 13:51:45 | 1782 | 3.0 | 172.95 |
| 13:51:46 | 1783 | 3.0 | 173.01 |
| 13:51:47 | 1782 | 3.0 | 173.06 |
| 13:51:48 | 1783 | 3.0 | 173.11 |
| 13:51:49 | 1783 | 3.0 | 173.16 |
| 13:51:50 | 1783 | 3.0 | 173.21 |
| 13:51:51 | 1784 | 3.0 | 173.26 |
| 13:51:52 | 1784 | 3.0 | 173.31 |
| 13:51:53 | 1783 | 3.0 | 173.36 |
| 13:51:54 | 1784 | 3.0 | 173.41 |
| 13:51:55 | 1784 | 3.0 | 173.46 |
| 13:51:56 | 1784 | 3.0 | 173.51 |
| 13:51:57 | 1785 | 3.0 | 173.56 |
| 13:51:58 | 1785 | 3.0 | 173.61 |
| 13:51:59 | 1785 | 3.0 | 173.66 |
| 13:52:00 | 1785 | 3.0 | 173.71 |
| 13:52:01 | 1786 | 3.0 | 173.76 |
| 13:52:02 | 1786 | 3.0 | 173.81 |
| 13:52:03 | 1787 | 3.0 | 173.86 |
| 13:52:04 | 1787 | 3.0 | 173.91 |
| 13:52:05 | 1787 | 3.0 | 173.96 |
| 13:52:06 | 1788 | 3.0 | 174.01 |
| 13:52:07 | 1788 | 3.0 | 174.06 |
| 13:52:08 | 1788 | 3.0 | 174.11 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:52:09 | 1789 | 3.0 | 174.16 |
| 13:52:10 | 1789 | 3.0 | 174.21 |
| 13:52:11 | 1790 | 3.0 | 174.26 |
| 13:52:12 | 1790 | 3.0 | 174.31 |
| 13:52:13 | 1790 | 3.0 | 174.36 |
| 13:52:14 | 1791 | 3.0 | 174.41 |
| 13:52:15 | 1791 | 3.0 | 174.46 |
| 13:52:16 | 1791 | 3.0 | 174.51 |
| 13:52:17 | 1792 | 3.0 | 174.56 |
| 13:52:18 | 1793 | 3.0 | 174.61 |
| 13:52:19 | 1793 | 3.0 | 174.66 |
| 13:52:20 | 1793 | 3.0 | 174.71 |
| 13:52:21 | 1794 | 3.0 | 174.76 |
| 13:52:22 | 1794 | 3.0 | 174.81 |
| 13:52:23 | 1794 | 3.0 | 174.86 |
| 13:52:24 | 1795 | 3.0 | 174.91 |
| 13:52:25 | 1795 | 3.0 | 174.96 |
| 13:52:26 | 1796 | 3.0 | 175.01 |
| 13:52:27 | 1796 | 3.0 | 175.06 |
| 13:52:28 | 1796 | 3.0 | 175.11 |
| 13:52:29 | 1797 | 3.0 | 175.16 |
| 13:52:30 | 1797 | 3.0 | 175.21 |
| 13:52:31 | 1797 | 3.0 | 175.26 |
| 13:52:32 | 1798 | 3.0 | 175.31 |
| 13:52:33 | 1798 | 3.0 | 175.36 |
| 13:52:34 | 1798 | 3.0 | 175.41 |
| 13:52:35 | 1799 | 3.0 | 175.46 |
| 13:52:36 | 1799 | 3.0 | 175.51 |
| 13:52:37 | 1799 | 3.0 | 175.56 |
| 13:52:38 | 1800 | 3.0 | 175.61 |
| 13:52:39 | 1800 | 3.0 | 175.66 |
| 13:52:40 | 1801 | 3.0 | 175.71 |
| 13:52:41 | 1801 | 3.0 | 175.76 |
| 13:52:42 | 1802 | 3.0 | 175.81 |
| 13:52:43 | 1802 | 3.0 | 175.86 |
| 13:52:44 | 1802 | 3.0 | 175.91 |
| 13:52:45 | 1802 | 3.0 | 175.96 |
| 13:52:46 | 1803 | 3.0 | 176.01 |
| 13:52:47 | 1804 | 3.0 | 176.07 |
| 13:52:48 | 1804 | 3.0 | 176.12 |
| 13:52:49 | 1805 | 3.0 | 176.17 |
| 13:52:50 | 1805 | 3.0 | 176.22 |
| 13:52:51 | 1805 | 3.0 | 176.27 |
| 13:52:52 | 1806 | 3.0 | 176.32 |
| 13:52:53 | 1807 | 3.0 | 176.37 |
| 13:52:54 | 1807 | 3.0 | 176.42 |
| 13:52:55 | 1807 | 3.0 | 176.47 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:52:56 | 1808 | 3.0 | 176.52 |
| 13:52:57 | 1808 | 3.0 | 176.57 |
| 13:52:58 | 1809 | 3.0 | 176.62 |
| 13:52:59 | 1809 | 3.0 | 176.67 |
| 13:53:00 | 1810 | 3.0 | 176.72 |
| 13:53:01 | 1810 | 3.0 | 176.77 |
| 13:53:02 | 1810 | 3.0 | 176.82 |
| 13:53:03 | 1811 | 3.0 | 176.87 |
| 13:53:04 | 1812 | 3.0 | 176.92 |
| 13:53:05 | 1812 | 3.0 | 176.97 |
| 13:53:06 | 1812 | 3.0 | 177.02 |
| 13:53:07 | 1812 | 3.0 | 177.07 |
| 13:53:08 | 1812 | 3.0 | 177.12 |
| 13:53:09 | 1813 | 3.0 | 177.17 |
| 13:53:10 | 1814 | 3.0 | 177.22 |
| 13:53:11 | 1813 | 3.0 | 177.27 |
| 13:53:12 | 1813 | 3.0 | 177.32 |
| 13:53:13 | 1814 | 3.0 | 177.37 |
| 13:53:14 | 1814 | 3.0 | 177.42 |
| 13:53:15 | 1815 | 3.0 | 177.47 |
| 13:53:16 | 1815 | 3.0 | 177.52 |
| 13:53:17 | 1816 | 3.0 | 177.57 |
| 13:53:18 | 1816 | 3.0 | 177.62 |
| 13:53:19 | 1817 | 3.0 | 177.67 |
| 13:53:20 | 1817 | 3.0 | 177.72 |
| 13:53:21 | 1819 | 3.0 | 177.77 |
| 13:53:22 | 1819 | 3.0 | 177.82 |
| 13:53:23 | 1819 | 3.0 | 177.87 |
| 13:53:24 | 1820 | 3.0 | 177.92 |
| 13:53:25 | 1820 | 3.0 | 177.97 |
| 13:53:26 | 1821 | 3.0 | 178.02 |
| 13:53:27 | 1822 | 3.0 | 178.07 |
| 13:53:28 | 1821 | 3.0 | 178.12 |
| 13:53:29 | 1822 | 3.0 | 178.17 |
| 13:53:30 | 1822 | 3.0 | 178.22 |
| 13:53:31 | 1823 | 3.0 | 178.27 |
| 13:53:32 | 1824 | 3.0 | 178.32 |
| 13:53:33 | 1825 | 3.0 | 178.37 |
| 13:53:34 | 1825 | 3.0 | 178.42 |
| 13:53:35 | 1826 | 3.0 | 178.47 |
| 13:53:36 | 1827 | 3.0 | 178.52 |
| 13:53:37 | 1827 | 3.0 | 178.57 |
| 13:53:38 | 1828 | 3.0 | 178.62 |
| 13:53:39 | 1827 | 3.0 | 178.67 |
| 13:53:40 | 1827 | 3.0 | 178.72 |
| 13:53:41 | 1828 | 3.0 | 178.77 |
| 13:53:42 | 1828 | 3.0 | 178.82 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:53:43 | 1828 | 3.0 | 178.88 |
| 13:53:44 | 1829 | 3.0 | 178.93 |
| 13:53:45 | 1829 | 3.0 | 178.98 |
| 13:53:46 | 1830 | 3.0 | 179.03 |
| 13:53:47 | 1830 | 3.0 | 179.08 |
| 13:53:48 | 1831 | 3.0 | 179.13 |
| 13:53:49 | 1831 | 3.0 | 179.18 |
| 13:53:50 | 1832 | 3.0 | 179.23 |
| 13:53:51 | 1832 | 3.0 | 179.28 |
| 13:53:52 | 1832 | 3.0 | 179.33 |
| 13:53:53 | 1833 | 3.0 | 179.38 |
| 13:53:54 | 1833 | 3.0 | 179.43 |
| 13:53:55 | 1834 | 3.0 | 179.48 |
| 13:53:56 | 1834 | 3.0 | 179.53 |
| 13:53:57 | 1834 | 3.0 | 179.58 |
| 13:53:58 | 1835 | 3.0 | 179.63 |
| 13:53:59 | 1835 | 3.0 | 179.68 |
| 13:54:00 | 1835 | 3.0 | 179.73 |
| 13:54:01 | 1836 | 3.0 | 179.78 |
| 13:54:02 | 1836 | 3.0 | 179.83 |
| 13:54:03 | 1837 | 3.0 | 179.88 |
| 13:54:04 | 1838 | 3.0 | 179.93 |
| 13:54:05 | 1838 | 3.0 | 179.98 |
| 13:54:06 | 1839 | 3.0 | 180.03 |
| 13:54:07 | 1839 | 3.0 | 180.08 |
| 13:54:08 | 1840 | 3.0 | 180.13 |
| 13:54:09 | 1841 | 3.0 | 180.18 |
| 13:54:10 | 1842 | 3.0 | 180.23 |
| 13:54:11 | 1842 | 3.0 | 180.28 |
| 13:54:12 | 1842 | 3.0 | 180.33 |
| 13:54:13 | 1843 | 3.0 | 180.38 |
| 13:54:14 | 1843 | 3.0 | 180.43 |
| 13:54:15 | 1843 | 2.9 | 180.48 |
| 13:54:16 | 1842 | 2.9 | 180.53 |
| 13:54:17 | 1842 | 2.9 | 180.57 |
| 13:54:18 | 1842 | 2.8 | 180.62 |
| 13:54:19 | 1841 | 2.8 | 180.67 |
| 13:54:20 | 1840 | 2.8 | 180.71 |
| 13:54:21 | 1840 | 2.8 | 180.76 |
| 13:54:22 | 1839 | 2.8 | 180.81 |
| 13:54:23 | 1839 | 2.8 | 180.85 |
| 13:54:24 | 1839 | 2.8 | 180.90 |
| 13:54:25 | 1840 | 2.8 | 180.95 |
| 13:54:26 | 1840 | 2.8 | 180.99 |
| 13:54:27 | 1840 | 2.8 | 181.04 |
| 13:54:28 | 1841 | 2.8 | 181.09 |
| 13:54:29 | 1842 | 2.8 | 181.14 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:54:30 | 1844 | 2.8 | 181.18 |
| 13:54:31 | 1845 | 2.8 | 181.23 |
| 13:54:32 | 1846 | 2.8 | 181.28 |
| 13:54:33 | 1846 | 2.8 | 181.33 |
| 13:54:34 | 1846 | 2.8 | 181.37 |
| 13:54:35 | 1846 | 2.8 | 181.42 |
| 13:54:36 | 1845 | 2.8 | 181.47 |
| 13:54:37 | 1845 | 2.8 | 181.51 |
| 13:54:38 | 1845 | 2.8 | 181.56 |
| 13:54:39 | 1846 | 2.8 | 181.61 |
| 13:54:40 | 1847 | 2.8 | 181.66 |
| 13:54:41 | 1848 | 2.8 | 181.70 |
| 13:54:42 | 1849 | 2.8 | 181.75 |
| 13:54:43 | 1849 | 2.8 | 181.80 |
| 13:54:44 | 1850 | 2.8 | 181.85 |
| 13:54:45 | 1850 | 2.8 | 181.89 |
| 13:54:46 | 1851 | 2.8 | 181.94 |
| 13:54:47 | 1851 | 2.8 | 181.99 |
| 13:54:48 | 1852 | 2.8 | 182.04 |
| 13:54:49 | 1854 | 2.8 | 182.08 |
| 13:54:50 | 1854 | 2.8 | 182.13 |
| 13:54:51 | 1855 | 2.8 | 182.18 |
| 13:54:52 | 1855 | 2.8 | 182.23 |
| 13:54:53 | 1855 | 2.8 | 182.27 |
| 13:54:54 | 1855 | 2.8 | 182.32 |
| 13:54:55 | 1854 | 2.8 | 182.37 |
| 13:54:56 | 1855 | 2.8 | 182.42 |
| 13:54:57 | 1855 | 2.9 | 182.46 |
| 13:54:58 | 1858 | 2.9 | 182.51 |
| 13:54:59 | 1859 | 2.9 | 182.56 |
| 13:55:00 | 1861 | 2.9 | 182.61 |
| 13:55:01 | 1862 | 3.0 | 182.66 |
| 13:55:02 | 1864 | 3.0 | 182.71 |
| 13:55:03 | 1865 | 3.0 | 182.76 |
| 13:55:04 | 1865 | 3.0 | 182.81 |
| 13:55:05 | 1867 | 3.0 | 182.86 |
| 13:55:06 | 1867 | 3.0 | 182.91 |
| 13:55:07 | 1868 | 3.0 | 182.96 |
| 13:55:08 | 1868 | 3.0 | 183.01 |
| 13:55:09 | 1869 | 3.0 | 183.06 |
| 13:55:10 | 1869 | 3.0 | 183.11 |
| 13:55:11 | 1870 | 3.0 | 183.16 |
| 13:55:12 | 1871 | 3.0 | 183.21 |
| 13:55:13 | 1871 | 3.0 | 183.26 |
| 13:55:14 | 1872 | 3.0 | 183.31 |
| 13:55:15 | 1874 | 3.0 | 183.36 |
| 13:55:16 | 1874 | 3.0 | 183.41 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:55:17 | 1875 | 3.0 | 183.46 |
| 13:55:18 | 1877 | 3.0 | 183.51 |
| 13:55:19 | 1877 | 3.0 | 183.56 |
| 13:55:20 | 1878 | 3.0 | 183.61 |
| 13:55:21 | 1880 | 3.0 | 183.66 |
| 13:55:22 | 1880 | 3.0 | 183.71 |
| 13:55:23 | 1880 | 3.0 | 183.76 |
| 13:55:24 | 1881 | 3.0 | 183.81 |
| 13:55:25 | 1882 | 3.0 | 183.86 |
| 13:55:26 | 1882 | 3.0 | 183.91 |
| 13:55:27 | 1883 | 3.0 | 183.96 |
| 13:55:28 | 1884 | 3.0 | 184.01 |
| 13:55:29 | 1884 | 3.0 | 184.06 |
| 13:55:30 | 1885 | 3.0 | 184.12 |
| 13:55:31 | 1886 | 3.0 | 184.17 |
| 13:55:32 | 1887 | 3.0 | 184.22 |
| 13:55:33 | 1887 | 3.0 | 184.27 |
| 13:55:34 | 1888 | 3.0 | 184.32 |
| 13:55:35 | 1889 | 3.0 | 184.37 |
| 13:55:36 | 1889 | 3.0 | 184.42 |
| 13:55:37 | 1889 | 3.0 | 184.47 |
| 13:55:38 | 1890 | 3.0 | 184.52 |
| 13:55:39 | 1890 | 3.0 | 184.57 |
| 13:55:40 | 1891 | 3.0 | 184.62 |
| 13:55:41 | 1891 | 3.0 | 184.67 |
| 13:55:42 | 1892 | 3.0 | 184.72 |
| 13:55:43 | 1893 | 3.0 | 184.77 |
| 13:55:44 | 1894 | 3.0 | 184.82 |
| 13:55:45 | 1895 | 3.0 | 184.87 |
| 13:55:46 | 1895 | 3.0 | 184.92 |
| 13:55:47 | 1896 | 3.0 | 184.97 |
| 13:55:48 | 1898 | 3.0 | 185.02 |
| 13:55:49 | 1898 | 3.0 | 185.07 |
| 13:55:50 | 1899 | 3.0 | 185.12 |
| 13:55:51 | 1900 | 3.0 | 185.17 |
| 13:55:52 | 1900 | 3.0 | 185.22 |
| 13:55:53 | 1900 | 3.0 | 185.27 |
| 13:55:54 | 1900 | 3.0 | 185.32 |
| 13:55:55 | 1901 | 3.0 | 185.37 |
| 13:55:56 | 1901 | 3.0 | 185.42 |
| 13:55:57 | 1902 | 3.0 | 185.47 |
| 13:55:58 | 1903 | 3.0 | 185.52 |
| 13:55:59 | 1903 | 3.0 | 185.57 |
| 13:56:00 | 1903 | 3.0 | 185.63 |
| 13:56:01 | 1905 | 3.0 | 185.68 |
| 13:56:02 | 1905 | 3.0 | 185.73 |
| 13:56:03 | 1905 | 3.0 | 185.78 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:56:04 | 1906 | 3.0 | 185.83 |
| 13:56:05 | 1907 | 3.0 | 185.88 |
| 13:56:06 | 1907 | 3.0 | 185.93 |
| 13:56:07 | 1908 | 3.0 | 185.98 |
| 13:56:08 | 1908 | 3.0 | 186.03 |
| 13:56:09 | 1908 | 3.0 | 186.08 |
| 13:56:10 | 1908 | 3.0 | 186.13 |
| 13:56:11 | 1909 | 3.0 | 186.18 |
| 13:56:12 | 1909 | 3.0 | 186.23 |
| 13:56:13 | 1909 | 3.0 | 186.28 |
| 13:56:14 | 1910 | 3.0 | 186.33 |
| 13:56:15 | 1911 | 3.0 | 186.38 |
| 13:56:16 | 1911 | 3.0 | 186.43 |
| 13:56:17 | 1912 | 3.0 | 186.48 |
| 13:56:18 | 1912 | 3.0 | 186.53 |
| 13:56:19 | 1913 | 3.0 | 186.58 |
| 13:56:20 | 1913 | 3.0 | 186.63 |
| 13:56:21 | 1914 | 3.0 | 186.68 |
| 13:56:22 | 1914 | 3.0 | 186.73 |
| 13:56:23 | 1914 | 3.0 | 186.78 |
| 13:56:24 | 1914 | 3.0 | 186.83 |
| 13:56:25 | 1914 | 3.0 | 186.88 |
| 13:56:26 | 1914 | 3.0 | 186.93 |
| 13:56:27 | 1915 | 3.0 | 186.98 |
| 13:56:28 | 1916 | 3.0 | 187.03 |
| 13:56:29 | 1915 | 3.0 | 187.08 |
| 13:56:30 | 1913 | 2.9 | 187.13 |
| 13:56:31 | 1912 | 2.9 | 187.18 |
| 13:56:32 | 1923 | 3.2 | 187.23 |
| 13:56:33 | 1956 | 3.8 | 187.30 |
| 13:56:34 | 1964 | 4.0 | 187.36 |
| 13:56:35 | 1964 | 4.0 | 187.43 |
| 13:56:36 | 1962 | 4.0 | 187.50 |
| 13:56:37 | 1959 | 4.0 | 187.56 |
| 13:56:38 | 1965 | 4.0 | 187.63 |
| 13:56:39 | 1971 | 4.0 | 187.70 |
| 13:56:40 | 1972 | 3.9 | 187.76 |
| 13:56:41 | 1974 | 3.9 | 187.83 |
| 13:56:42 | 1976 | 3.9 | 187.89 |
| 13:56:43 | 1978 | 3.9 | 187.96 |
| 13:56:44 | 1981 | 3.9 | 188.02 |
| 13:56:45 | 1985 | 3.9 | 188.09 |
| 13:56:46 | 1986 | 3.9 | 188.15 |
| 13:56:47 | 1989 | 3.9 | 188.22 |
| 13:56:48 | 1991 | 3.9 | 188.28 |
| 13:56:49 | 1993 | 3.9 | 188.35 |
| 13:56:50 | 1997 | 3.9 | 188.42 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:56:51 | 1999 | 3.9 | 188.48 |
| 13:56:52 | 2000 | 3.9 | 188.55 |
| 13:56:53 | 2004 | 3.9 | 188.61 |
| 13:56:54 | 2006 | 3.9 | 188.68 |
| 13:56:55 | 2008 | 3.9 | 188.74 |
| 13:56:56 | 2012 | 3.9 | 188.81 |
| 13:56:57 | 2014 | 3.9 | 188.87 |
| 13:56:58 | 2017 | 3.9 | 188.94 |
| 13:56:59 | 2019 | 3.9 | 189.00 |
| 13:57:00 | 2022 | 4.0 | 189.07 |
| 13:57:01 | 2023 | 4.0 | 189.14 |
| 13:57:02 | 2026 | 4.0 | 189.20 |
| 13:57:03 | 2027 | 4.0 | 189.27 |
| 13:57:04 | 2030 | 4.0 | 189.33 |
| 13:57:05 | 2031 | 4.0 | 189.40 |
| 13:57:06 | 2035 | 4.0 | 189.47 |
| 13:57:07 | 2035 | 4.0 | 189.53 |
| 13:57:08 | 2039 | 4.0 | 189.60 |
| 13:57:09 | 2040 | 4.0 | 189.66 |
| 13:57:10 | 2043 | 4.0 | 189.73 |
| 13:57:11 | 2044 | 4.0 | 189.80 |
| 13:57:12 | 2047 | 4.0 | 189.86 |
| 13:57:13 | 2048 | 4.0 | 189.93 |
| 13:57:14 | 2050 | 4.0 | 189.99 |
| 13:57:15 | 2052 | 4.0 | 190.06 |
| 13:57:16 | 2054 | 4.0 | 190.13 |
| 13:57:17 | 2055 | 4.0 | 190.19 |
| 13:57:18 | 2055 | 4.0 | 190.26 |
| 13:57:19 | 2056 | 4.0 | 190.33 |
| 13:57:20 | 2057 | 4.0 | 190.39 |
| 13:57:21 | 2059 | 4.0 | 190.46 |
| 13:57:22 | 2060 | 4.0 | 190.52 |
| 13:57:23 | 2063 | 4.0 | 190.59 |
| 13:57:24 | 2065 | 4.0 | 190.66 |
| 13:57:25 | 2067 | 4.0 | 190.72 |
| 13:57:26 | 2067 | 4.0 | 190.79 |
| 13:57:27 | 2070 | 4.0 | 190.86 |
| 13:57:28 | 2071 | 4.0 | 190.92 |
| 13:57:29 | 2073 | 4.0 | 190.99 |
| 13:57:30 | 2073 | 4.0 | 191.05 |
| 13:57:31 | 2075 | 4.0 | 191.12 |
| 13:57:32 | 2075 | 4.0 | 191.19 |
| 13:57:33 | 2077 | 4.0 | 191.25 |
| 13:57:34 | 2078 | 4.0 | 191.32 |
| 13:57:35 | 2080 | 4.0 | 191.38 |
| 13:57:36 | 2081 | 4.0 | 191.45 |
| 13:57:37 | 2083 | 4.0 | 191.52 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:57:38 | 2084 | 4.0 | 191.58 |
| 13:57:39 | 2086 | 4.0 | 191.65 |
| 13:57:40 | 2087 | 4.0 | 191.72 |
| 13:57:41 | 2089 | 4.0 | 191.78 |
| 13:57:42 | 2089 | 4.0 | 191.85 |
| 13:57:43 | 2091 | 4.0 | 191.91 |
| 13:57:44 | 2092 | 4.0 | 191.98 |
| 13:57:45 | 2094 | 4.0 | 192.05 |
| 13:57:46 | 2095 | 4.0 | 192.11 |
| 13:57:47 | 2097 | 4.0 | 192.18 |
| 13:57:48 | 2097 | 4.0 | 192.25 |
| 13:57:49 | 2100 | 4.0 | 192.31 |
| 13:57:50 | 2100 | 4.0 | 192.38 |
| 13:57:51 | 2102 | 4.0 | 192.44 |
| 13:57:52 | 2102 | 4.0 | 192.51 |
| 13:57:53 | 2104 | 4.0 | 192.58 |
| 13:57:54 | 2105 | 4.0 | 192.64 |
| 13:57:55 | 2107 | 4.0 | 192.71 |
| 13:57:56 | 2107 | 4.0 | 192.78 |
| 13:57:57 | 2109 | 4.0 | 192.84 |
| 13:57:58 | 2110 | 4.0 | 192.91 |
| 13:57:59 | 2111 | 4.0 | 192.97 |
| 13:58:00 | 2113 | 4.0 | 193.04 |
| 13:58:01 | 2114 | 4.0 | 193.11 |
| 13:58:02 | 2115 | 4.0 | 193.17 |
| 13:58:03 | 2117 | 4.0 | 193.24 |
| 13:58:04 | 2119 | 4.0 | 193.31 |
| 13:58:05 | 2120 | 4.0 | 193.37 |
| 13:58:06 | 2122 | 4.0 | 193.44 |
| 13:58:07 | 2123 | 4.0 | 193.50 |
| 13:58:08 | 2124 | 4.0 | 193.57 |
| 13:58:09 | 2125 | 4.0 | 193.64 |
| 13:58:10 | 2126 | 4.0 | 193.70 |
| 13:58:11 | 2127 | 4.0 | 193.77 |
| 13:58:12 | 2128 | 4.0 | 193.84 |
| 13:58:13 | 2129 | 4.0 | 193.90 |
| 13:58:14 | 2131 | 4.0 | 193.97 |
| 13:58:15 | 2131 | 4.0 | 194.03 |
| 13:58:16 | 2133 | 4.0 | 194.10 |
| 13:58:17 | 2134 | 4.0 | 194.17 |
| 13:58:18 | 2136 | 4.0 | 194.23 |
| 13:58:19 | 2137 | 4.0 | 194.30 |
| 13:58:20 | 2139 | 4.0 | 194.38 |
| 13:58:21 | 2139 | 4.0 | 194.38 |
| 13:58:22 | 2140 | 4.0 | 194.44 |
| 13:58:23 | 2141 | 4.0 | 194.51 |
| 13:58:24 | 2142 | 4.0 | 194.58 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:58:25 | 2143 | 4.0 | 194.64 |
| 13:58:26 | 2143 | 4.0 | 194.71 |
| 13:58:27 | 2145 | 4.0 | 194.78 |
| 13:58:28 | 2146 | 4.0 | 194.84 |
| 13:58:29 | 2148 | 4.0 | 194.91 |
| 13:58:30 | 2150 | 4.0 | 194.97 |
| 13:58:31 | 2152 | 4.0 | 195.04 |
| 13:58:32 | 2152 | 4.0 | 195.11 |
| 13:58:33 | 2154 | 4.0 | 195.17 |
| 13:58:34 | 2154 | 4.0 | 195.24 |
| 13:58:35 | 2156 | 4.0 | 195.31 |
| 13:58:36 | 2156 | 4.0 | 195.37 |
| 13:58:37 | 2158 | 4.0 | 195.44 |
| 13:58:38 | 2158 | 4.0 | 195.50 |
| 13:58:39 | 2160 | 4.0 | 195.57 |
| 13:58:40 | 2160 | 4.0 | 195.64 |
| 13:58:41 | 2162 | 4.0 | 195.70 |
| 13:58:42 | 2162 | 4.0 | 195.77 |
| 13:58:43 | 2164 | 4.0 | 195.83 |
| 13:58:44 | 2164 | 4.0 | 195.90 |
| 13:58:45 | 2167 | 4.0 | 195.97 |
| 13:58:46 | 2167 | 4.0 | 196.03 |
| 13:58:47 | 2169 | 4.0 | 196.10 |
| 13:58:48 | 2169 | 4.0 | 196.17 |
| 13:58:49 | 2171 | 4.0 | 196.23 |
| 13:58:50 | 2171 | 4.0 | 196.30 |
| 13:58:51 | 2173 | 4.0 | 196.36 |
| 13:58:52 | 2173 | 4.0 | 196.43 |
| 13:58:53 | 2173 | 4.0 | 196.50 |
| 13:58:54 | 2174 | 4.0 | 196.56 |
| 13:58:55 | 2176 | 4.0 | 196.63 |
| 13:58:56 | 2176 | 4.0 | 196.69 |
| 13:58:57 | 2178 | 4.0 | 196.76 |
| 13:58:58 | 2179 | 4.0 | 196.83 |
| 13:58:59 | 2181 | 4.0 | 196.89 |
| 13:59:00 | 2182 | 4.0 | 196.96 |
| 13:59:01 | 2184 | 4.0 | 197.03 |
| 13:59:02 | 2184 | 4.0 | 197.09 |
| 13:59:03 | 2185 | 4.0 | 197.16 |
| 13:59:04 | 2185 | 4.0 | 197.22 |
| 13:59:05 | 2186 | 4.0 | 197.29 |
| 13:59:06 | 2186 | 4.0 | 197.36 |
| 13:59:07 | 2186 | 4.0 | 197.42 |
| 13:59:08 | 2187 | 4.0 | 197.49 |
| 13:59:09 | 2188 | 4.0 | 197.55 |
| 13:59:10 | 2189 | 4.0 | 197.62 |
| 13:59:11 | 2190 | 4.0 | 197.69 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:59:12 | 2192 | 4.0 | 197.75 |
| 13:59:13 | 2192 | 4.0 | 197.82 |
| 13:59:14 | 2193 | 4.0 | 197.89 |
| 13:59:15 | 2193 | 4.0 | 197.95 |
| 13:59:16 | 2194 | 4.0 | 198.02 |
| 13:59:17 | 2194 | 4.0 | 198.08 |
| 13:59:18 | 2195 | 4.0 | 198.15 |
| 13:59:19 | 2195 | 4.0 | 198.22 |
| 13:59:20 | 2196 | 4.0 | 198.28 |
| 13:59:21 | 2196 | 4.0 | 198.35 |
| 13:59:22 | 2197 | 4.0 | 198.41 |
| 13:59:23 | 2197 | 4.0 | 198.48 |
| 13:59:24 | 2199 | 4.0 | 198.55 |
| 13:59:25 | 2199 | 4.0 | 198.61 |
| 13:59:26 | 2201 | 4.0 | 198.68 |
| 13:59:27 | 2202 | 4.0 | 198.74 |
| 13:59:28 | 2203 | 4.0 | 198.81 |
| 13:59:29 | 2203 | 4.0 | 198.88 |
| 13:59:30 | 2205 | 4.0 | 198.94 |
| 13:59:31 | 2204 | 4.0 | 199.01 |
| 13:59:32 | 2206 | 4.0 | 199.08 |
| 13:59:33 | 2205 | 4.0 | 199.14 |
| 13:59:34 | 2207 | 4.0 | 199.21 |
| 13:59:35 | 2206 | 4.0 | 199.27 |
| 13:59:36 | 2208 | 4.0 | 199.34 |
| 13:59:37 | 2207 | 4.0 | 199.41 |
| 13:59:38 | 2209 | 4.0 | 199.47 |
| 13:59:39 | 2209 | 4.0 | 199.54 |
| 13:59:40 | 2211 | 4.0 | 199.60 |
| 13:59:41 | 2211 | 4.0 | 199.67 |
| 13:59:42 | 2212 | 4.0 | 199.74 |
| 13:59:43 | 2213 | 4.0 | 199.80 |
| 13:59:44 | 2215 | 4.0 | 199.87 |
| 13:59:45 | 2215 | 4.0 | 199.94 |
| 13:59:46 | 2215 | 4.0 | 200.00 |
| 13:59:47 | 2216 | 4.0 | 200.07 |
| 13:59:48 | 2217 | 4.0 | 200.13 |
| 13:59:49 | 2217 | 4.0 | 200.20 |
| 13:59:50 | 2218 | 4.0 | 200.27 |
| 13:59:51 | 2218 | 4.0 | 200.33 |
| 13:59:52 | 2220 | 4.0 | 200.40 |
| 13:59:53 | 2220 | 4.0 | 200.46 |
| 13:59:54 | 2222 | 4.0 | 200.53 |
| 13:59:55 | 2222 | 4.0 | 200.60 |
| 13:59:56 | 2223 | 4.0 | 200.66 |
| 13:59:57 | 2223 | 4.0 | 200.73 |
| 13:59:58 | 2224 | 4.0 | 200.80 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 13:59:59 | 2224 | 4.0 | 200.86 |
| 14:00:00 | 2224 | 4.0 | 200.93 |
| 14:00:01 | 2225 | 4.0 | 200.99 |
| 14:00:02 | 2225 | 4.0 | 201.06 |
| 14:00:03 | 2226 | 4.0 | 201.13 |
| 14:00:04 | 2227 | 4.0 | 201.19 |
| 14:00:05 | 2228 | 4.0 | 201.26 |
| 14:00:06 | 2228 | 4.0 | 201.32 |
| 14:00:07 | 2230 | 4.0 | 201.39 |
| 14:00:08 | 2230 | 4.0 | 201.46 |
| 14:00:09 | 2231 | 4.0 | 201.52 |
| 14:00:10 | 2231 | 4.0 | 201.59 |
| 14:00:11 | 2232 | 4.0 | 201.65 |
| 14:00:12 | 2232 | 4.0 | 201.72 |
| 14:00:13 | 2233 | 4.0 | 201.79 |
| 14:00:14 | 2232 | 4.0 | 201.85 |
| 14:00:15 | 2233 | 4.0 | 201.92 |
| 14:00:16 | 2233 | 4.0 | 201.99 |
| 14:00:17 | 2234 | 4.0 | 202.05 |
| 14:00:18 | 2233 | 4.0 | 202.12 |
| 14:00:19 | 2235 | 4.0 | 202.18 |
| 14:00:20 | 2235 | 4.0 | 202.25 |
| 14:00:21 | 2236 | 4.0 | 202.32 |
| 14:00:22 | 2235 | 4.0 | 202.38 |
| 14:00:23 | 2237 | 4.0 | 202.45 |
| 14:00:24 | 2236 | 4.0 | 202.52 |
| 14:00:25 | 2237 | 4.0 | 202.58 |
| 14:00:26 | 2236 | 4.0 | 202.65 |
| 14:00:27 | 2236 | 4.0 | 202.71 |
| 14:00:28 | 2235 | 4.0 | 202.78 |
| 14:00:29 | 2236 | 4.0 | 202.85 |
| 14:00:30 | 2235 | 4.0 | 202.91 |
| 14:00:31 | 2237 | 4.0 | 202.98 |
| 14:00:32 | 2236 | 4.0 | 203.05 |
| 14:00:33 | 2237 | 4.0 | 203.11 |
| 14:00:34 | 2237 | 4.0 | 203.18 |
| 14:00:35 | 2239 | 4.0 | 203.24 |
| 14:00:36 | 2239 | 4.0 | 203.31 |
| 14:00:37 | 2239 | 4.0 | 203.38 |
| 14:00:38 | 2239 | 4.0 | 203.44 |
| 14:00:39 | 2240 | 4.0 | 203.51 |
| 14:00:40 | 2240 | 4.0 | 203.58 |
| 14:00:41 | 2240 | 4.0 | 203.64 |
| 14:00:42 | 2239 | 4.0 | 203.71 |
| 14:00:43 | 2239 | 4.0 | 203.77 |
| 14:00:44 | 2239 | 4.0 | 203.84 |
| 14:00:45 | 2239 | 4.0 | 203.91 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:00:46 | 2240 | 4.0 | 203.97 |
| 14:00:47 | 2241 | 4.0 | 204.04 |
| 14:00:48 | 2241 | 4.0 | 204.11 |
| 14:00:49 | 2242 | 4.0 | 204.17 |
| 14:00:50 | 2243 | 4.0 | 204.24 |
| 14:00:51 | 2243 | 4.0 | 204.30 |
| 14:00:52 | 2244 | 4.0 | 204.37 |
| 14:00:53 | 2243 | 4.0 | 204.44 |
| 14:00:54 | 2244 | 4.0 | 204.50 |
| 14:00:55 | 2243 | 4.0 | 204.57 |
| 14:00:56 | 2243 | 4.0 | 204.64 |
| 14:00:57 | 2242 | 4.0 | 204.70 |
| 14:00:58 | 2242 | 4.0 | 204.77 |
| 14:00:59 | 2242 | 4.0 | 204.83 |
| 14:01:00 | 2243 | 4.0 | 204.90 |
| 14:01:01 | 2243 | 4.0 | 204.97 |
| 14:01:02 | 2243 | 4.0 | 205.03 |
| 14:01:03 | 2244 | 4.0 | 205.10 |
| 14:01:04 | 2245 | 4.0 | 205.17 |
| 14:01:05 | 2245 | 4.0 | 205.23 |
| 14:01:06 | 2246 | 4.0 | 205.30 |
| 14:01:07 | 2245 | 4.0 | 205.36 |
| 14:01:08 | 2246 | 4.0 | 205.43 |
| 14:01:09 | 2245 | 4.0 | 205.50 |
| 14:01:10 | 2246 | 4.0 | 205.56 |
| 14:01:11 | 2246 | 4.0 | 205.63 |
| 14:01:12 | 2247 | 4.0 | 205.69 |
| 14:01:13 | 2246 | 4.0 | 205.76 |
| 14:01:14 | 2247 | 4.0 | 205.83 |
| 14:01:15 | 2246 | 4.0 | 205.89 |
| 14:01:16 | 2247 | 4.0 | 205.96 |
| 14:01:17 | 2247 | 4.0 | 206.03 |
| 14:01:18 | 2248 | 4.0 | 206.09 |
| 14:01:19 | 2247 | 4.0 | 206.16 |
| 14:01:20 | 2248 | 4.0 | 206.22 |
| 14:01:21 | 2247 | 4.0 | 206.29 |
| 14:01:22 | 2248 | 4.0 | 206.36 |
| 14:01:23 | 2246 | 4.0 | 206.42 |
| 14:01:24 | 2246 | 4.0 | 206.49 |
| 14:01:25 | 2245 | 4.0 | 206.56 |
| 14:01:26 | 2245 | 4.0 | 206.62 |
| 14:01:27 | 2244 | 4.0 | 206.69 |
| 14:01:28 | 2245 | 4.0 | 206.75 |
| 14:01:29 | 2244 | 4.0 | 206.82 |
| 14:01:30 | 2244 | 4.0 | 206.89 |
| 14:01:31 | 2243 | 4.0 | 206.95 |
| 14:01:32 | 2243 | 4.0 | 207.02 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:01:33 | 2242 | 4.0 | 207.09 |
| 14:01:34 | 2242 | 4.0 | 207.15 |
| 14:01:35 | 2241 | 4.0 | 207.22 |
| 14:01:36 | 2241 | 4.0 | 207.28 |
| 14:01:37 | 2241 | 4.0 | 207.35 |
| 14:01:38 | 2240 | 4.0 | 207.42 |
| 14:01:39 | 2240 | 4.0 | 207.48 |
| 14:01:40 | 2240 | 4.0 | 207.55 |
| 14:01:41 | 2241 | 4.0 | 207.62 |
| 14:01:42 | 2241 | 4.0 | 207.68 |
| 14:01:43 | 2241 | 4.0 | 207.75 |
| 14:01:44 | 2241 | 4.0 | 207.81 |
| 14:01:45 | 2242 | 4.0 | 207.88 |
| 14:01:46 | 2241 | 4.0 | 207.95 |
| 14:01:47 | 2242 | 4.0 | 208.01 |
| 14:01:48 | 2241 | 4.0 | 208.08 |
| 14:01:49 | 2242 | 4.0 | 208.14 |
| 14:01:50 | 2242 | 4.0 | 208.21 |
| 14:01:51 | 2242 | 4.0 | 208.28 |
| 14:01:52 | 2242 | 4.0 | 208.34 |
| 14:01:53 | 2243 | 4.0 | 208.41 |
| 14:01:54 | 2242 | 4.0 | 208.47 |
| 14:01:55 | 2244 | 4.0 | 208.54 |
| 14:01:56 | 2244 | 4.0 | 208.61 |
| 14:01:57 | 2245 | 4.0 | 208.67 |
| 14:01:58 | 2245 | 4.0 | 208.74 |
| 14:01:59 | 2246 | 4.0 | 208.80 |
| 14:02:00 | 2246 | 4.0 | 208.87 |
| 14:02:01 | 2247 | 4.0 | 208.94 |
| 14:02:02 | 2246 | 4.0 | 209.01 |
| 14:02:03 | 2247 | 4.0 | 209.08 |
| 14:02:04 | 2246 | 4.0 | 209.15 |
| 14:02:05 | 2247 | 4.0 | 209.22 |
| 14:02:06 | 2246 | 4.0 | 209.29 |
| 14:02:07 | 2247 | 4.0 | 209.35 |
| 14:02:08 | 2246 | 4.0 | 209.42 |
| 14:02:09 | 2247 | 4.0 | 209.48 |
| 14:02:10 | 2247 | 4.0 | 209.55 |
| 14:02:11 | 2247 | 4.0 | 209.62 |
| 14:02:12 | 2247 | 4.0 | 209.68 |
| 14:02:13 | 2248 | 4.0 | 209.75 |
| 14:02:14 | 2247 | 4.0 | 209.82 |
| 14:02:15 | 2248 | 4.0 | 209.88 |
| 14:02:16 | 2248 | 4.0 | 209.95 |
| 14:02:17 | 2249 | 4.0 | 210.01 |
| 14:02:18 | 2249 | 4.0 | 210.08 |
| 14:02:19 | 2250 | 4.0 | 210.15 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:02:20 | 2249 | 4.0 | 210.21 |
| 14:02:21 | 2250 | 4.0 | 210.28 |
| 14:02:22 | 2249 | 4.0 | 210.35 |
| 14:02:23 | 2250 | 4.0 | 210.41 |
| 14:02:24 | 2248 | 4.0 | 210.48 |
| 14:02:25 | 2249 | 4.0 | 210.54 |
| 14:02:26 | 2249 | 4.0 | 210.61 |
| 14:02:27 | 2249 | 4.0 | 210.68 |
| 14:02:28 | 2249 | 4.0 | 210.74 |
| 14:02:29 | 2250 | 4.0 | 210.81 |
| 14:02:30 | 2250 | 4.0 | 210.88 |
| 14:02:31 | 2251 | 4.0 | 210.94 |
| 14:02:32 | 2251 | 4.0 | 211.01 |
| 14:02:33 | 2251 | 4.0 | 211.07 |
| 14:02:34 | 2251 | 4.0 | 211.14 |
| 14:02:35 | 2251 | 4.0 | 211.21 |
| 14:02:36 | 2250 | 4.0 | 211.27 |
| 14:02:37 | 2251 | 4.0 | 211.34 |
| 14:02:38 | 2250 | 4.0 | 211.41 |
| 14:02:39 | 2251 | 4.0 | 211.47 |
| 14:02:40 | 2250 | 4.0 | 211.54 |
| 14:02:41 | 2251 | 4.0 | 211.60 |
| 14:02:42 | 2250 | 4.0 | 211.67 |
| 14:02:43 | 2251 | 4.0 | 211.74 |
| 14:02:44 | 2251 | 4.0 | 211.80 |
| 14:02:45 | 2251 | 4.0 | 211.87 |
| 14:02:46 | 2251 | 4.0 | 211.94 |
| 14:02:47 | 2251 | 4.0 | 212.00 |
| 14:02:48 | 2251 | 4.0 | 212.07 |
| 14:02:49 | 2250 | 4.0 | 212.13 |
| 14:02:50 | 2251 | 4.0 | 212.20 |
| 14:02:51 | 2250 | 4.0 | 212.27 |
| 14:02:52 | 2251 | 4.0 | 212.33 |
| 14:02:53 | 2250 | 4.0 | 212.40 |
| 14:02:54 | 2250 | 4.0 | 212.46 |
| 14:02:55 | 2250 | 4.0 | 212.53 |
| 14:02:56 | 2250 | 4.0 | 212.60 |
| 14:02:57 | 2250 | 4.0 | 212.66 |
| 14:02:58 | 2250 | 4.0 | 212.73 |
| 14:02:59 | 2250 | 4.0 | 212.80 |
| 14:03:00 | 2250 | 4.0 | 212.86 |
| 14:03:01 | 2250 | 4.0 | 212.93 |
| 14:03:02 | 2250 | 4.0 | 212.99 |
| 14:03:03 | 2249 | 4.0 | 213.06 |
| 14:03:04 | 2249 | 4.0 | 213.13 |
| 14:03:05 | 2248 | 4.0 | 213.19 |
| 14:03:06 | 2248 | 4.0 | 213.26 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:03:07 | 2247 | 4.0 | 213.33 |
| 14:03:08 | 2248 | 4.0 | 213.39 |
| 14:03:09 | 2247 | 4.0 | 213.46 |
| 14:03:10 | 2248 | 4.0 | 213.52 |
| 14:03:11 | 2248 | 4.0 | 213.59 |
| 14:03:12 | 2249 | 4.0 | 213.66 |
| 14:03:13 | 2248 | 4.0 | 213.72 |
| 14:03:14 | 2249 | 4.0 | 213.79 |
| 14:03:15 | 2248 | 4.0 | 213.85 |
| 14:03:16 | 2248 | 4.0 | 213.92 |
| 14:03:17 | 2247 | 4.0 | 213.99 |
| 14:03:18 | 2248 | 4.0 | 214.05 |
| 14:03:19 | 2247 | 4.0 | 214.12 |
| 14:03:20 | 2247 | 4.0 | 214.19 |
| 14:03:21 | 2246 | 4.0 | 214.25 |
| 14:03:22 | 2247 | 4.0 | 214.32 |
| 14:03:23 | 2247 | 4.0 | 214.38 |
| 14:03:24 | 2248 | 4.0 | 214.45 |
| 14:03:25 | 2247 | 4.0 | 214.52 |
| 14:03:26 | 2248 | 4.0 | 214.58 |
| 14:03:27 | 2247 | 4.0 | 214.65 |
| 14:03:28 | 2248 | 4.0 | 214.71 |
| 14:03:29 | 2247 | 4.0 | 214.78 |
| 14:03:30 | 2248 | 4.0 | 214.85 |
| 14:03:31 | 2247 | 4.0 | 214.91 |
| 14:03:32 | 2247 | 4.0 | 214.98 |
| 14:03:33 | 2247 | 4.0 | 215.05 |
| 14:03:34 | 2247 | 4.0 | 215.11 |
| 14:03:35 | 2247 | 4.0 | 215.18 |
| 14:03:36 | 2247 | 4.0 | 215.24 |
| 14:03:37 | 2246 | 4.0 | 215.31 |
| 14:03:38 | 2248 | 4.0 | 215.38 |
| 14:03:39 | 2247 | 4.0 | 215.44 |
| 14:03:40 | 2248 | 4.0 | 215.51 |
| 14:03:41 | 2248 | 4.0 | 215.57 |
| 14:03:42 | 2248 | 4.0 | 215.64 |
| 14:03:43 | 2248 | 4.0 | 215.71 |
| 14:03:44 | 2248 | 4.0 | 215.77 |
| 14:03:45 | 2247 | 4.0 | 215.84 |
| 14:03:46 | 2247 | 4.0 | 215.91 |
| 14:03:47 | 2246 | 4.0 | 215.97 |
| 14:03:48 | 2246 | 4.0 | 216.04 |
| 14:03:49 | 2246 | 4.0 | 216.10 |
| 14:03:50 | 2246 | 4.0 | 216.17 |
| 14:03:51 | 2247 | 4.0 | 216.24 |
| 14:03:52 | 2246 | 4.0 | 216.30 |
| 14:03:53 | 2247 | 4.0 | 216.37 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:03:54 | 2247 | 4.0 | 216.44 |
| 14:03:55 | 2247 | 4.0 | 216.50 |
| 14:03:56 | 2246 | 4.0 | 216.57 |
| 14:03:57 | 2247 | 4.0 | 216.63 |
| 14:03:58 | 2246 | 4.0 | 216.70 |
| 14:03:59 | 2246 | 4.0 | 216.77 |
| 14:04:00 | 2245 | 4.0 | 216.83 |
| 14:04:01 | 2245 | 4.0 | 216.90 |
| 14:04:02 | 2245 | 4.0 | 216.96 |
| 14:04:03 | 2245 | 4.0 | 217.03 |
| 14:04:04 | 2244 | 4.0 | 217.10 |
| 14:04:05 | 2245 | 4.0 | 217.16 |
| 14:04:06 | 2243 | 4.0 | 217.23 |
| 14:04:07 | 2244 | 4.0 | 217.30 |
| 14:04:08 | 2243 | 4.0 | 217.36 |
| 14:04:09 | 2244 | 4.0 | 217.43 |
| 14:04:10 | 2242 | 4.0 | 217.49 |
| 14:04:11 | 2243 | 4.0 | 217.56 |
| 14:04:12 | 2241 | 4.0 | 217.63 |
| 14:04:13 | 2242 | 4.0 | 217.69 |
| 14:04:14 | 2241 | 4.0 | 217.76 |
| 14:04:15 | 2241 | 4.0 | 217.82 |
| 14:04:16 | 2240 | 4.0 | 217.89 |
| 14:04:17 | 2240 | 4.0 | 217.96 |
| 14:04:18 | 2239 | 4.0 | 218.02 |
| 14:04:19 | 2240 | 4.0 | 218.09 |
| 14:04:20 | 2239 | 4.0 | 218.16 |
| 14:04:21 | 2239 | 4.0 | 218.22 |
| 14:04:22 | 2238 | 4.0 | 218.29 |
| 14:04:23 | 2239 | 4.0 | 218.35 |
| 14:04:24 | 2237 | 4.0 | 218.42 |
| 14:04:25 | 2237 | 4.0 | 218.49 |
| 14:04:26 | 2235 | 4.0 | 218.55 |
| 14:04:27 | 2235 | 4.0 | 218.62 |
| 14:04:28 | 2234 | 4.0 | 218.69 |
| 14:04:29 | 2234 | 4.0 | 218.75 |
| 14:04:30 | 2233 | 4.0 | 218.82 |
| 14:04:31 | 2233 | 4.0 | 218.88 |
| 14:04:32 | 2232 | 4.0 | 218.95 |
| 14:04:33 | 2232 | 4.0 | 219.02 |
| 14:04:34 | 2232 | 4.0 | 219.08 |
| 14:04:35 | 2232 | 4.0 | 219.15 |
| 14:04:36 | 2232 | 4.0 | 219.22 |
| 14:04:37 | 2231 | 4.0 | 219.28 |
| 14:04:38 | 2231 | 4.0 | 219.35 |
| 14:04:39 | 2230 | 4.0 | 219.41 |
| 14:04:40 | 2230 | 4.0 | 219.48 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:04:41 | 2230 | 4.0 | 219.55 |
| 14:04:42 | 2230 | 4.0 | 219.61 |
| 14:04:43 | 2229 | 4.0 | 219.68 |
| 14:04:44 | 2229 | 4.0 | 219.75 |
| 14:04:45 | 2229 | 4.0 | 219.81 |
| 14:04:46 | 2228 | 4.0 | 219.88 |
| 14:04:47 | 2228 | 4.0 | 219.94 |
| 14:04:48 | 2229 | 4.0 | 220.01 |
| 14:04:49 | 2228 | 4.0 | 220.08 |
| 14:04:50 | 2229 | 4.0 | 220.14 |
| 14:04:51 | 2228 | 4.0 | 220.21 |
| 14:04:52 | 2228 | 4.0 | 220.28 |
| 14:04:53 | 2226 | 4.0 | 220.34 |
| 14:04:54 | 2226 | 4.0 | 220.41 |
| 14:04:55 | 2225 | 4.0 | 220.47 |
| 14:04:56 | 2225 | 4.0 | 220.54 |
| 14:04:57 | 2223 | 4.0 | 220.61 |
| 14:04:58 | 2223 | 4.0 | 220.67 |
| 14:04:59 | 2222 | 4.0 | 220.74 |
| 14:05:00 | 2223 | 4.0 | 220.81 |
| 14:05:01 | 2222 | 4.0 | 220.87 |
| 14:05:02 | 2223 | 4.0 | 220.94 |
| 14:05:03 | 2222 | 4.0 | 221.00 |
| 14:05:04 | 2223 | 4.0 | 221.07 |
| 14:05:05 | 2222 | 4.0 | 221.14 |
| 14:05:06 | 2222 | 4.0 | 221.20 |
| 14:05:07 | 2221 | 4.0 | 221.27 |
| 14:05:08 | 2221 | 4.0 | 221.34 |
| 14:05:09 | 2220 | 4.0 | 221.40 |
| 14:05:10 | 2220 | 4.0 | 221.47 |
| 14:05:11 | 2219 | 4.0 | 221.53 |
| 14:05:12 | 2220 | 4.0 | 221.60 |
| 14:05:13 | 2219 | 4.0 | 221.67 |
| 14:05:14 | 2220 | 4.0 | 221.73 |
| 14:05:15 | 2219 | 4.0 | 221.80 |
| 14:05:16 | 2220 | 4.0 | 221.87 |
| 14:05:17 | 2219 | 4.0 | 221.93 |
| 14:05:18 | 2220 | 4.0 | 222.00 |
| 14:05:19 | 2219 | 4.0 | 222.06 |
| 14:05:20 | 2219 | 4.0 | 222.13 |
| 14:05:21 | 2219 | 4.0 | 222.20 |
| 14:05:22 | 2219 | 4.0 | 222.26 |
| 14:05:23 | 2219 | 4.0 | 222.33 |
| 14:05:24 | 2219 | 4.0 | 222.40 |
| 14:05:25 | 2219 | 4.0 | 222.46 |
| 14:05:26 | 2219 | 4.0 | 222.53 |
| 14:05:27 | 2219 | 4.0 | 222.59 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:05:28 | 2220 | 4.0 | 222.66 |
| 14:05:29 | 2220 | 4.0 | 222.73 |
| 14:05:30 | 2221 | 4.0 | 222.79 |
| 14:05:31 | 2221 | 4.0 | 222.86 |
| 14:05:32 | 2221 | 4.0 | 222.93 |
| 14:05:33 | 2221 | 4.0 | 222.99 |
| 14:05:34 | 2221 | 4.0 | 223.06 |
| 14:05:35 | 2221 | 4.0 | 223.12 |
| 14:05:36 | 2220 | 4.0 | 223.19 |
| 14:05:37 | 2220 | 4.0 | 223.26 |
| 14:05:38 | 2220 | 4.0 | 223.32 |
| 14:05:39 | 2220 | 4.0 | 223.39 |
| 14:05:40 | 2220 | 4.0 | 223.46 |
| 14:05:41 | 2221 | 4.0 | 223.52 |
| 14:05:42 | 2221 | 4.0 | 223.59 |
| 14:05:43 | 2222 | 4.0 | 223.65 |
| 14:05:44 | 2222 | 4.0 | 223.72 |
| 14:05:45 | 2223 | 4.0 | 223.79 |
| 14:05:46 | 2222 | 4.0 | 223.85 |
| 14:05:47 | 2223 | 4.0 | 223.92 |
| 14:05:48 | 2222 | 4.0 | 223.99 |
| 14:05:49 | 2222 | 4.0 | 224.05 |
| 14:05:50 | 2222 | 4.0 | 224.12 |
| 14:05:51 | 2222 | 4.0 | 224.18 |
| 14:05:52 | 2222 | 4.0 | 224.25 |
| 14:05:53 | 2222 | 4.0 | 224.32 |
| 14:05:54 | 2222 | 4.0 | 224.38 |
| 14:05:55 | 2223 | 4.0 | 224.45 |
| 14:05:56 | 2222 | 4.0 | 224.52 |
| 14:05:57 | 2224 | 4.0 | 224.58 |
| 14:05:58 | 2223 | 4.0 | 224.65 |
| 14:05:59 | 2224 | 4.0 | 224.71 |
| 14:06:00 | 2223 | 4.0 | 224.78 |
| 14:06:01 | 2224 | 4.0 | 224.85 |
| 14:06:02 | 2223 | 4.0 | 224.91 |
| 14:06:03 | 2224 | 4.0 | 224.98 |
| 14:06:04 | 2223 | 4.0 | 225.05 |
| 14:06:05 | 2224 | 4.0 | 225.11 |
| 14:06:06 | 2223 | 4.0 | 225.18 |
| 14:06:07 | 2224 | 4.0 | 225.24 |
| 14:06:08 | 2223 | 4.0 | 225.31 |
| 14:06:09 | 2225 | 4.0 | 225.38 |
| 14:06:10 | 2224 | 4.0 | 225.44 |
| 14:06:11 | 2225 | 4.0 | 225.51 |
| 14:06:12 | 2224 | 4.0 | 225.58 |
| 14:06:13 | 2226 | 4.0 | 225.64 |
| 14:06:14 | 2225 | 4.0 | 225.71 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:06:15 | 2225 | 4.0 | 225.77 |
| 14:06:16 | 2224 | 4.0 | 225.84 |
| 14:06:17 | 2224 | 4.0 | 225.91 |
| 14:06:18 | 2224 | 4.0 | 225.97 |
| 14:06:19 | 2224 | 4.0 | 226.04 |
| 14:06:20 | 2223 | 4.0 | 226.11 |
| 14:06:21 | 2224 | 4.0 | 226.17 |
| 14:06:22 | 2224 | 4.0 | 226.24 |
| 14:06:23 | 2225 | 4.0 | 226.30 |
| 14:06:24 | 2225 | 4.0 | 226.37 |
| 14:06:25 | 2226 | 4.0 | 226.44 |
| 14:06:26 | 2225 | 4.0 | 226.50 |
| 14:06:27 | 2225 | 4.0 | 226.57 |
| 14:06:28 | 2225 | 4.0 | 226.64 |
| 14:06:29 | 2224 | 4.0 | 226.70 |
| 14:06:30 | 2225 | 4.0 | 226.77 |
| 14:06:31 | 2225 | 4.0 | 226.83 |
| 14:06:32 | 2225 | 4.0 | 226.90 |
| 14:06:33 | 2225 | 4.0 | 226.97 |
| 14:06:34 | 2225 | 4.0 | 227.03 |
| 14:06:35 | 2225 | 4.0 | 227.10 |
| 14:06:36 | 2225 | 4.0 | 227.17 |
| 14:06:37 | 2224 | 4.0 | 227.23 |
| 14:06:38 | 2225 | 4.0 | 227.30 |
| 14:06:39 | 2225 | 4.0 | 227.36 |
| 14:06:40 | 2226 | 4.0 | 227.43 |
| 14:06:41 | 2225 | 4.0 | 227.50 |
| 14:06:42 | 2226 | 4.0 | 227.56 |
| 14:06:43 | 2225 | 4.0 | 227.63 |
| 14:06:44 | 2226 | 4.0 | 227.70 |
| 14:06:45 | 2224 | 4.0 | 227.76 |
| 14:06:46 | 2225 | 4.0 | 227.83 |
| 14:06:47 | 2225 | 4.0 | 227.89 |
| 14:06:48 | 2226 | 4.0 | 227.96 |
| 14:06:49 | 2226 | 4.0 | 228.03 |
| 14:06:50 | 2227 | 4.0 | 228.09 |
| 14:06:51 | 2227 | 4.0 | 228.16 |
| 14:06:52 | 2228 | 4.0 | 228.23 |
| 14:06:53 | 2227 | 4.0 | 228.29 |
| 14:06:54 | 2228 | 4.0 | 228.36 |
| 14:06:55 | 2228 | 4.0 | 228.42 |
| 14:06:56 | 2228 | 4.0 | 228.49 |
| 14:06:57 | 2227 | 4.0 | 228.56 |
| 14:06:58 | 2227 | 4.0 | 228.62 |
| 14:06:59 | 2227 | 4.0 | 228.69 |
| 14:07:00 | 2228 | 4.0 | 228.76 |
| 14:07:01 | 2227 | 4.0 | 228.82 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:07:02 | 2228 | 4.0 | 228.89 |
| 14:07:03 | 2227 | 4.0 | 228.95 |
| 14:07:04 | 2228 | 4.0 | 229.02 |
| 14:07:05 | 2227 | 4.0 | 229.09 |
| 14:07:06 | 2228 | 4.0 | 229.15 |
| 14:07:07 | 2227 | 4.0 | 229.22 |
| 14:07:08 | 2228 | 4.0 | 229.29 |
| 14:07:09 | 2228 | 4.0 | 229.35 |
| 14:07:10 | 2228 | 4.0 | 229.42 |
| 14:07:11 | 2227 | 4.0 | 229.48 |
| 14:07:12 | 2227 | 4.0 | 229.55 |
| 14:07:13 | 2226 | 4.0 | 229.62 |
| 14:07:14 | 2227 | 4.0 | 229.68 |
| 14:07:15 | 2227 | 4.0 | 229.75 |
| 14:07:16 | 2227 | 4.0 | 229.82 |
| 14:07:17 | 2227 | 4.0 | 229.88 |
| 14:07:18 | 2228 | 4.0 | 229.95 |
| 14:07:19 | 2228 | 4.0 | 230.01 |
| 14:07:20 | 2229 | 4.0 | 230.08 |
| 14:07:21 | 2229 | 4.0 | 230.15 |
| 14:07:22 | 2229 | 4.0 | 230.21 |
| 14:07:23 | 2229 | 4.0 | 230.28 |
| 14:07:24 | 2228 | 4.0 | 230.35 |
| 14:07:25 | 2228 | 4.0 | 230.41 |
| 14:07:26 | 2227 | 4.0 | 230.48 |
| 14:07:27 | 2228 | 4.0 | 230.54 |
| 14:07:28 | 2227 | 4.0 | 230.61 |
| 14:07:29 | 2228 | 4.0 | 230.68 |
| 14:07:30 | 2228 | 4.0 | 230.74 |
| 14:07:31 | 2228 | 4.0 | 230.81 |
| 14:07:32 | 2228 | 4.0 | 230.87 |
| 14:07:33 | 2228 | 4.0 | 230.94 |
| 14:07:34 | 2227 | 4.0 | 231.01 |
| 14:07:35 | 2228 | 4.0 | 231.07 |
| 14:07:36 | 2228 | 4.0 | 231.14 |
| 14:07:37 | 2229 | 4.0 | 231.21 |
| 14:07:38 | 2228 | 4.0 | 231.27 |
| 14:07:39 | 2228 | 4.0 | 231.34 |
| 14:07:40 | 2228 | 4.0 | 231.40 |
| 14:07:41 | 2228 | 4.0 | 231.47 |
| 14:07:42 | 2227 | 4.0 | 231.54 |
| 14:07:43 | 2228 | 4.0 | 231.60 |
| 14:07:44 | 2227 | 4.0 | 231.67 |
| 14:07:45 | 2229 | 4.0 | 231.74 |
| 14:07:46 | 2228 | 4.0 | 231.80 |
| 14:07:47 | 2230 | 4.0 | 231.87 |
| 14:07:48 | 2229 | 4.0 | 231.93 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:07:49 | 2230 | 4.0 | 232.00 |
| 14:07:50 | 2229 | 4.0 | 232.07 |
| 14:07:51 | 2229 | 4.0 | 232.13 |
| 14:07:52 | 2228 | 4.0 | 232.20 |
| 14:07:53 | 2228 | 4.0 | 232.27 |
| 14:07:54 | 2228 | 4.0 | 232.33 |
| 14:07:55 | 2228 | 4.0 | 232.40 |
| 14:07:56 | 2228 | 4.0 | 232.46 |
| 14:07:57 | 2229 | 4.0 | 232.53 |
| 14:07:58 | 2229 | 4.0 | 232.60 |
| 14:07:59 | 2230 | 4.0 | 232.66 |
| 14:08:00 | 2230 | 4.0 | 232.73 |
| 14:08:01 | 2231 | 4.0 | 232.80 |
| 14:08:02 | 2230 | 4.0 | 232.86 |
| 14:08:03 | 2230 | 4.0 | 232.93 |
| 14:08:04 | 2230 | 4.0 | 232.99 |
| 14:08:05 | 2230 | 4.0 | 233.06 |
| 14:08:06 | 2229 | 4.0 | 233.13 |
| 14:08:07 | 2230 | 4.0 | 233.19 |
| 14:08:08 | 2229 | 4.0 | 233.26 |
| 14:08:09 | 2230 | 4.0 | 233.32 |
| 14:08:10 | 2230 | 4.0 | 233.39 |
| 14:08:11 | 2230 | 4.0 | 233.46 |
| 14:08:12 | 2230 | 4.0 | 233.52 |
| 14:08:13 | 2230 | 4.0 | 233.59 |
| 14:08:14 | 2230 | 4.0 | 233.66 |
| 14:08:15 | 2231 | 4.0 | 233.72 |
| 14:08:16 | 2231 | 4.0 | 233.79 |
| 14:08:17 | 2230 | 4.0 | 233.85 |
| 14:08:18 | 2231 | 4.0 | 233.92 |
| 14:08:19 | 2230 | 4.0 | 233.99 |
| 14:08:20 | 2231 | 4.0 | 234.05 |
| 14:08:21 | 2230 | 4.0 | 234.12 |
| 14:08:22 | 2230 | 4.0 | 234.19 |
| 14:08:23 | 2230 | 4.0 | 234.25 |
| 14:08:24 | 2231 | 4.0 | 234.32 |
| 14:08:25 | 2230 | 4.0 | 234.38 |
| 14:08:26 | 2232 | 4.0 | 234.45 |
| 14:08:27 | 2231 | 4.0 | 234.52 |
| 14:08:28 | 2233 | 4.0 | 234.58 |
| 14:08:29 | 2232 | 4.0 | 234.65 |
| 14:08:30 | 2233 | 4.0 | 234.72 |
| 14:08:31 | 2232 | 4.0 | 234.78 |
| 14:08:32 | 2232 | 4.0 | 234.85 |
| 14:08:33 | 2231 | 4.0 | 234.91 |
| 14:08:34 | 2232 | 4.0 | 234.98 |
| 14:08:35 | 2231 | 4.0 | 235.05 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:08:36 | 2231 | 4.0 | 235.11 |
| 14:08:37 | 2231 | 4.0 | 235.18 |
| 14:08:38 | 2232 | 4.0 | 235.25 |
| 14:08:39 | 2232 | 4.0 | 235.31 |
| 14:08:40 | 2233 | 4.0 | 235.38 |
| 14:08:41 | 2232 | 4.0 | 235.44 |
| 14:08:42 | 2234 | 4.0 | 235.51 |
| 14:08:43 | 2233 | 4.0 | 235.58 |
| 14:08:44 | 2233 | 4.0 | 235.64 |
| 14:08:45 | 2232 | 4.0 | 235.71 |
| 14:08:46 | 2233 | 4.0 | 235.77 |
| 14:08:47 | 2232 | 4.0 | 235.84 |
| 14:08:48 | 2233 | 4.0 | 235.91 |
| 14:08:49 | 2232 | 4.0 | 235.97 |
| 14:08:50 | 2233 | 4.0 | 236.04 |
| 14:08:51 | 2232 | 4.0 | 236.11 |
| 14:08:52 | 2234 | 4.0 | 236.17 |
| 14:08:53 | 2233 | 4.0 | 236.24 |
| 14:08:54 | 2234 | 4.0 | 236.30 |
| 14:08:55 | 2234 | 4.0 | 236.37 |
| 14:08:56 | 2234 | 4.0 | 236.44 |
| 14:08:57 | 2234 | 4.0 | 236.50 |
| 14:08:58 | 2235 | 4.0 | 236.57 |
| 14:08:59 | 2234 | 4.0 | 236.64 |
| 14:09:00 | 2234 | 4.0 | 236.70 |
| 14:09:01 | 2234 | 4.0 | 236.77 |
| 14:09:02 | 2234 | 4.0 | 236.83 |
| 14:09:03 | 2234 | 4.0 | 236.90 |
| 14:09:04 | 2235 | 4.0 | 236.97 |
| 14:09:05 | 2235 | 4.0 | 237.03 |
| 14:09:06 | 2235 | 4.0 | 237.10 |
| 14:09:07 | 2236 | 4.0 | 237.17 |
| 14:09:08 | 2236 | 4.0 | 237.23 |
| 14:09:09 | 2237 | 4.0 | 237.30 |
| 14:09:10 | 2237 | 4.0 | 237.36 |
| 14:09:11 | 2238 | 4.0 | 237.43 |
| 14:09:12 | 2237 | 4.0 | 237.50 |
| 14:09:13 | 2238 | 4.0 | 237.56 |
| 14:09:14 | 2237 | 4.0 | 237.63 |
| 14:09:15 | 2238 | 4.0 | 237.70 |
| 14:09:16 | 2237 | 4.0 | 237.76 |
| 14:09:17 | 2237 | 4.0 | 237.83 |
| 14:09:18 | 2237 | 4.0 | 237.89 |
| 14:09:19 | 2238 | 4.0 | 237.96 |
| 14:09:20 | 2238 | 4.0 | 238.03 |
| 14:09:21 | 2239 | 4.0 | 238.09 |
| 14:09:22 | 2239 | 4.0 | 238.16 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:09:23 | 2240 | 4.0 | 238.23 |
| 14:09:24 | 2239 | 4.0 | 238.29 |
| 14:09:25 | 2240 | 4.0 | 238.36 |
| 14:09:26 | 2239 | 4.0 | 238.42 |
| 14:09:27 | 2240 | 4.0 | 238.49 |
| 14:09:28 | 2239 | 4.0 | 238.56 |
| 14:09:29 | 2240 | 4.0 | 238.62 |
| 14:09:30 | 2239 | 4.0 | 238.69 |
| 14:09:31 | 2240 | 4.0 | 238.75 |
| 14:09:32 | 2239 | 4.0 | 238.82 |
| 14:09:33 | 2241 | 4.0 | 238.89 |
| 14:09:34 | 2240 | 4.0 | 238.95 |
| 14:09:35 | 2242 | 4.0 | 239.02 |
| 14:09:36 | 2241 | 4.0 | 239.09 |
| 14:09:37 | 2242 | 4.0 | 239.15 |
| 14:09:38 | 2241 | 4.0 | 239.22 |
| 14:09:39 | 2243 | 4.0 | 239.28 |
| 14:09:40 | 2241 | 4.0 | 239.35 |
| 14:09:41 | 2242 | 4.0 | 239.42 |
| 14:09:42 | 2241 | 4.0 | 239.48 |
| 14:09:43 | 2242 | 4.0 | 239.55 |
| 14:09:44 | 2241 | 4.0 | 239.62 |
| 14:09:45 | 2242 | 4.0 | 239.68 |
| 14:09:46 | 2241 | 4.0 | 239.75 |
| 14:09:47 | 2243 | 4.0 | 239.81 |
| 14:09:48 | 2243 | 4.0 | 239.88 |
| 14:09:49 | 2244 | 4.0 | 239.95 |
| 14:09:50 | 2244 | 4.0 | 240.01 |
| 14:09:51 | 2245 | 4.0 | 240.08 |
| 14:09:52 | 2244 | 4.0 | 240.15 |
| 14:09:53 | 2244 | 4.0 | 240.21 |
| 14:09:54 | 2244 | 4.0 | 240.28 |
| 14:09:55 | 2244 | 4.0 | 240.34 |
| 14:09:56 | 2243 | 4.0 | 240.41 |
| 14:09:57 | 2244 | 4.0 | 240.48 |
| 14:09:58 | 2243 | 4.0 | 240.54 |
| 14:09:59 | 2245 | 4.0 | 240.61 |
| 14:10:00 | 2244 | 4.0 | 240.68 |
| 14:10:01 | 2245 | 4.0 | 240.74 |
| 14:10:02 | 2246 | 4.0 | 240.81 |
| 14:10:03 | 2246 | 4.0 | 240.87 |
| 14:10:04 | 2246 | 4.0 | 240.94 |
| 14:10:05 | 2246 | 4.0 | 241.01 |
| 14:10:06 | 2247 | 4.0 | 241.07 |
| 14:10:07 | 2246 | 4.0 | 241.14 |
| 14:10:08 | 2247 | 4.0 | 241.21 |
| 14:10:09 | 2246 | 4.0 | 241.27 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:10:10 | 2247 | 4.0 | 241.34 |
| 14:10:11 | 2247 | 4.0 | 241.40 |
| 14:10:12 | 2247 | 4.0 | 241.47 |
| 14:10:13 | 2247 | 4.0 | 241.54 |
| 14:10:14 | 2248 | 4.0 | 241.60 |
| 14:10:15 | 2247 | 4.0 | 241.67 |
| 14:10:16 | 2248 | 4.0 | 241.73 |
| 14:10:17 | 2248 | 4.0 | 241.80 |
| 14:10:18 | 2249 | 4.0 | 241.87 |
| 14:10:19 | 2248 | 4.0 | 241.93 |
| 14:10:20 | 2249 | 4.0 | 242.00 |
| 14:10:21 | 2248 | 4.0 | 242.07 |
| 14:10:22 | 2249 | 4.0 | 242.13 |
| 14:10:23 | 2248 | 4.0 | 242.20 |
| 14:10:24 | 2249 | 4.0 | 242.26 |
| 14:10:25 | 2248 | 4.0 | 242.33 |
| 14:10:26 | 2249 | 4.0 | 242.40 |
| 14:10:27 | 2249 | 4.0 | 242.46 |
| 14:10:28 | 2251 | 4.0 | 242.53 |
| 14:10:29 | 2250 | 4.0 | 242.60 |
| 14:10:30 | 2252 | 4.0 | 242.66 |
| 14:10:31 | 2251 | 4.0 | 242.73 |
| 14:10:32 | 2252 | 4.0 | 242.79 |
| 14:10:33 | 2252 | 4.0 | 242.86 |
| 14:10:34 | 2252 | 4.0 | 242.93 |
| 14:10:35 | 2251 | 4.0 | 242.99 |
| 14:10:36 | 2252 | 4.0 | 243.06 |
| 14:10:37 | 2251 | 4.0 | 243.13 |
| 14:10:38 | 2252 | 4.0 | 243.19 |
| 14:10:39 | 2251 | 4.0 | 243.26 |
| 14:10:40 | 2252 | 4.0 | 243.32 |
| 14:10:41 | 2252 | 4.0 | 243.39 |
| 14:10:42 | 2252 | 4.0 | 243.46 |
| 14:10:43 | 2252 | 4.0 | 243.52 |
| 14:10:44 | 2253 | 4.0 | 243.59 |
| 14:10:45 | 2253 | 4.0 | 243.65 |
| 14:10:46 | 2254 | 4.0 | 243.72 |
| 14:10:47 | 2254 | 4.0 | 243.79 |
| 14:10:48 | 2254 | 4.0 | 243.85 |
| 14:10:49 | 2254 | 4.0 | 243.92 |
| 14:10:50 | 2254 | 4.0 | 243.99 |
| 14:10:51 | 2254 | 4.0 | 244.05 |
| 14:10:52 | 2254 | 4.0 | 244.12 |
| 14:10:53 | 2253 | 4.0 | 244.18 |
| 14:10:54 | 2254 | 4.0 | 244.25 |
| 14:10:55 | 2253 | 4.0 | 244.32 |
| 14:10:56 | 2254 | 4.0 | 244.38 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:10:57 | 2254 | 4.0 | 244.45 |
| 14:10:58 | 2255 | 4.0 | 244.52 |
| 14:10:59 | 2254 | 4.0 | 244.58 |
| 14:11:00 | 2255 | 4.0 | 244.65 |
| 14:11:01 | 2254 | 4.0 | 244.71 |
| 14:11:02 | 2254 | 4.0 | 244.78 |
| 14:11:03 | 2254 | 4.0 | 244.85 |
| 14:11:04 | 2253 | 4.0 | 244.91 |
| 14:11:05 | 2252 | 4.0 | 244.98 |
| 14:11:06 | 2252 | 4.0 | 245.05 |
| 14:11:07 | 2252 | 4.0 | 245.11 |
| 14:11:08 | 2252 | 4.0 | 245.18 |
| 14:11:09 | 2253 | 4.0 | 245.24 |
| 14:11:10 | 2252 | 4.0 | 245.31 |
| 14:11:11 | 2253 | 4.0 | 245.38 |
| 14:11:12 | 2253 | 4.0 | 245.44 |
| 14:11:13 | 2254 | 4.0 | 245.51 |
| 14:11:14 | 2253 | 4.0 | 245.58 |
| 14:11:15 | 2254 | 4.0 | 245.64 |
| 14:11:16 | 2253 | 4.0 | 245.71 |
| 14:11:17 | 2253 | 4.0 | 245.77 |
| 14:11:18 | 2252 | 4.0 | 245.84 |
| 14:11:19 | 2252 | 4.0 | 245.91 |
| 14:11:20 | 2251 | 4.0 | 245.97 |
| 14:11:21 | 2251 | 4.0 | 246.04 |
| 14:11:22 | 2250 | 4.0 | 246.10 |
| 14:11:23 | 2251 | 4.0 | 246.17 |
| 14:11:24 | 2250 | 4.0 | 246.24 |
| 14:11:25 | 2251 | 4.0 | 246.30 |
| 14:11:26 | 2250 | 4.0 | 246.37 |
| 14:11:27 | 2251 | 4.0 | 246.44 |
| 14:11:28 | 2250 | 4.0 | 246.50 |
| 14:11:29 | 2251 | 4.0 | 246.57 |
| 14:11:30 | 2250 | 4.0 | 246.63 |
| 14:11:31 | 2250 | 4.0 | 246.70 |
| 14:11:32 | 2249 | 4.0 | 246.77 |
| 14:11:33 | 2249 | 4.0 | 246.83 |
| 14:11:34 | 2249 | 4.0 | 246.90 |
| 14:11:35 | 2249 | 4.0 | 246.97 |
| 14:11:36 | 2248 | 4.0 | 247.03 |
| 14:11:37 | 2249 | 4.0 | 247.10 |
| 14:11:38 | 2249 | 4.0 | 247.16 |
| 14:11:39 | 2250 | 4.0 | 247.23 |
| 14:11:40 | 2250 | 4.0 | 247.30 |
| 14:11:41 | 2250 | 4.0 | 247.36 |
| 14:11:42 | 2249 | 4.0 | 247.43 |
| 14:11:43 | 2250 | 4.0 | 247.50 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:11:44 | 2248 | 4.0 | 247.56 |
| 14:11:45 | 2249 | 4.0 | 247.63 |
| 14:11:46 | 2248 | 4.0 | 247.69 |
| 14:11:47 | 2248 | 4.0 | 247.76 |
| 14:11:48 | 2248 | 4.0 | 247.83 |
| 14:11:49 | 2249 | 4.0 | 247.89 |
| 14:11:50 | 2249 | 4.0 | 247.96 |
| 14:11:51 | 2249 | 4.0 | 248.03 |
| 14:11:52 | 2249 | 4.0 | 248.09 |
| 14:11:53 | 2249 | 4.0 | 248.16 |
| 14:11:54 | 2249 | 4.0 | 248.22 |
| 14:11:55 | 2249 | 4.0 | 248.29 |
| 14:11:56 | 2249 | 4.0 | 248.36 |
| 14:11:57 | 2248 | 4.0 | 248.42 |
| 14:11:58 | 2249 | 4.0 | 248.49 |
| 14:11:59 | 2248 | 4.0 | 248.55 |
| 14:12:00 | 2248 | 4.0 | 248.62 |
| 14:12:01 | 2248 | 4.0 | 248.69 |
| 14:12:02 | 2248 | 4.0 | 248.75 |
| 14:12:03 | 2248 | 4.0 | 248.82 |
| 14:12:04 | 2249 | 4.0 | 248.89 |
| 14:12:05 | 2249 | 4.0 | 248.95 |
| 14:12:06 | 2250 | 4.0 | 249.02 |
| 14:12:07 | 2249 | 4.0 | 249.08 |
| 14:12:08 | 2250 | 4.0 | 249.15 |
| 14:12:09 | 2250 | 4.0 | 249.22 |
| 14:12:10 | 2250 | 4.0 | 249.28 |
| 14:12:11 | 2249 | 4.0 | 249.35 |
| 14:12:12 | 2250 | 4.0 | 249.42 |
| 14:12:13 | 2249 | 4.0 | 249.48 |
| 14:12:14 | 2250 | 4.0 | 249.55 |
| 14:12:15 | 2249 | 4.0 | 249.61 |
| 14:12:16 | 2250 | 4.0 | 249.68 |
| 14:12:17 | 2250 | 4.0 | 249.75 |
| 14:12:18 | 2251 | 4.0 | 249.81 |
| 14:12:19 | 2251 | 4.0 | 249.88 |
| 14:12:20 | 2252 | 4.0 | 249.95 |
| 14:12:21 | 2252 | 4.0 | 250.01 |
| 14:12:22 | 2253 | 4.0 | 250.08 |
| 14:12:23 | 2253 | 4.0 | 250.14 |
| 14:12:24 | 2254 | 4.0 | 250.21 |
| 14:12:25 | 2256 | 4.1 | 250.28 |
| 14:12:26 | 2257 | 4.1 | 250.35 |
| 14:12:27 | 2256 | 4.0 | 250.41 |
| 14:12:28 | 2255 | 4.1 | 250.48 |
| 14:12:29 | 2257 | 4.1 | 250.55 |
| 14:12:30 | 2261 | 4.2 | 250.62 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:12:31 | 2264 | 4.2 | 250.69 |
| 14:12:32 | 2266 | 4.3 | 250.76 |
| 14:12:33 | 2266 | 4.3 | 250.83 |
| 14:12:34 | 2267 | 4.3 | 250.90 |
| 14:12:35 | 2268 | 4.3 | 250.98 |
| 14:12:36 | 2266 | 4.2 | 251.05 |
| 14:12:37 | 2266 | 4.2 | 251.12 |
| 14:12:38 | 2268 | 4.3 | 251.19 |
| 14:12:39 | 2269 | 4.2 | 251.26 |
| 14:12:40 | 2270 | 4.2 | 251.33 |
| 14:12:41 | 2270 | 4.3 | 251.40 |
| 14:12:42 | 2273 | 4.2 | 251.47 |
| 14:12:43 | 2273 | 4.3 | 251.54 |
| 14:12:44 | 2273 | 4.2 | 251.61 |
| 14:12:45 | 2273 | 4.3 | 251.68 |
| 14:12:46 | 2273 | 4.2 | 251.75 |
| 14:12:47 | 2274 | 4.2 | 251.82 |
| 14:12:48 | 2274 | 4.2 | 251.89 |
| 14:12:49 | 2275 | 4.2 | 251.96 |
| 14:12:50 | 2275 | 4.2 | 252.03 |
| 14:12:51 | 2275 | 4.2 | 252.10 |
| 14:12:52 | 2277 | 4.2 | 252.17 |
| 14:12:53 | 2279 | 4.3 | 252.24 |
| 14:12:54 | 2279 | 4.2 | 252.31 |
| 14:12:55 | 2277 | 4.2 | 252.38 |
| 14:12:56 | 2277 | 4.3 | 252.45 |
| 14:12:57 | 2279 | 4.2 | 252.52 |
| 14:12:58 | 2279 | 4.2 | 252.59 |
| 14:12:59 | 2279 | 4.2 | 252.66 |
| 14:13:00 | 2280 | 4.2 | 252.73 |
| 14:13:01 | 2280 | 4.2 | 252.80 |
| 14:13:02 | 2279 | 4.2 | 252.87 |
| 14:13:03 | 2280 | 4.2 | 252.94 |
| 14:13:04 | 2280 | 4.2 | 253.01 |
| 14:13:05 | 2276 | 4.2 | 253.08 |
| 14:13:06 | 2276 | 4.2 | 253.15 |
| 14:13:07 | 2277 | 4.2 | 253.22 |
| 14:13:08 | 2275 | 4.2 | 253.29 |
| 14:13:09 | 2275 | 4.2 | 253.36 |
| 14:13:10 | 2275 | 4.2 | 253.43 |
| 14:13:11 | 2275 | 4.2 | 253.50 |
| 14:13:12 | 2276 | 4.2 | 253.57 |
| 14:13:13 | 2277 | 4.2 | 253.64 |
| 14:13:14 | 2278 | 4.1 | 253.71 |
| 14:13:15 | 2280 | 4.2 | 253.78 |
| 14:13:16 | 2281 | 4.2 | 253.85 |
| 14:13:17 | 2282 | 4.1 | 253.92 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:13:18 | 2282 | 4.2 | 253.99 |
| 14:13:19 | 2283 | 4.2 | 254.06 |
| 14:13:20 | 2281 | 4.1 | 254.13 |
| 14:13:21 | 2280 | 4.2 | 254.20 |
| 14:13:22 | 2279 | 4.2 | 254.27 |
| 14:13:23 | 2277 | 4.2 | 254.34 |
| 14:13:24 | 2277 | 4.2 | 254.41 |
| 14:13:25 | 2279 | 4.2 | 254.48 |
| 14:13:26 | 2279 | 4.1 | 254.55 |
| 14:13:27 | 2280 | 4.1 | 254.62 |
| 14:13:28 | 2281 | 4.2 | 254.69 |
| 14:13:29 | 2284 | 4.2 | 254.76 |
| 14:13:30 | 2285 | 4.3 | 254.83 |
| 14:13:31 | 2282 | 4.2 | 254.90 |
| 14:13:32 | 2282 | 4.2 | 254.97 |
| 14:13:33 | 2282 | 4.3 | 255.04 |
| 14:13:34 | 2282 | 4.2 | 255.11 |
| 14:13:35 | 2283 | 4.2 | 255.18 |
| 14:13:36 | 2283 | 4.2 | 255.25 |
| 14:13:37 | 2281 | 4.2 | 255.32 |
| 14:13:38 | 2283 | 4.2 | 255.39 |
| 14:13:39 | 2283 | 4.3 | 255.46 |
| 14:13:40 | 2284 | 4.2 | 255.53 |
| 14:13:41 | 2283 | 4.2 | 255.60 |
| 14:13:42 | 2286 | 4.3 | 255.67 |
| 14:13:43 | 2284 | 4.2 | 255.74 |
| 14:13:44 | 2284 | 4.2 | 255.81 |
| 14:13:45 | 2285 | 4.2 | 255.88 |
| 14:13:46 | 2286 | 4.2 | 255.95 |
| 14:13:47 | 2287 | 4.1 | 256.02 |
| 14:13:48 | 2285 | 4.1 | 256.09 |
| 14:13:49 | 2288 | 4.1 | 256.16 |
| 14:13:50 | 2294 | 4.4 | 256.23 |
| 14:13:51 | 2313 | 4.7 | 256.31 |
| 14:13:52 | 2342 | 5.1 | 256.39 |
| 14:13:53 | 2346 | 5.3 | 256.48 |
| 14:13:54 | 2347 | 5.3 | 256.57 |
| 14:13:55 | 2343 | 5.3 | 256.66 |
| 14:13:56 | 2339 | 5.2 | 256.74 |
| 14:13:57 | 2340 | 5.1 | 256.83 |
| 14:13:58 | 2340 | 5.1 | 256.91 |
| 14:13:59 | 2343 | 5.0 | 257.00 |
| 14:14:00 | 2343 | 5.0 | 257.08 |
| 14:14:01 | 2343 | 5.0 | 257.16 |
| 14:14:02 | 2343 | 5.0 | 257.25 |
| 14:14:03 | 2343 | 4.9 | 257.33 |
| 14:14:04 | 2346 | 4.9 | 257.41 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:14:05 | 2346 | 4.9 | 257.49 |
| 14:14:06 | 2348 | 4.9 | 257.58 |
| 14:14:07 | 2349 | 4.9 | 257.66 |
| 14:14:08 | 2349 | 4.9 | 257.74 |
| 14:14:09 | 2352 | 4.9 | 257.82 |
| 14:14:10 | 2352 | 4.9 | 257.90 |
| 14:14:11 | 2355 | 4.9 | 257.99 |
| 14:14:12 | 2355 | 4.9 | 258.07 |
| 14:14:13 | 2357 | 4.9 | 258.15 |
| 14:14:14 | 2358 | 4.9 | 258.23 |
| 14:14:15 | 2359 | 4.9 | 258.31 |
| 14:14:16 | 2361 | 4.9 | 258.39 |
| 14:14:17 | 2360 | 4.9 | 258.48 |
| 14:14:18 | 2362 | 4.9 | 258.56 |
| 14:14:19 | 2362 | 4.9 | 258.64 |
| 14:14:20 | 2363 | 4.9 | 258.72 |
| 14:14:21 | 2365 | 4.9 | 258.80 |
| 14:14:22 | 2365 | 4.9 | 258.88 |
| 14:14:23 | 2367 | 4.9 | 258.97 |
| 14:14:24 | 2366 | 4.9 | 259.05 |
| 14:14:25 | 2368 | 4.9 | 259.13 |
| 14:14:26 | 2368 | 4.9 | 259.21 |
| 14:14:27 | 2368 | 4.9 | 259.29 |
| 14:14:28 | 2370 | 4.9 | 259.38 |
| 14:14:29 | 2370 | 4.9 | 259.46 |
| 14:14:30 | 2372 | 4.9 | 259.54 |
| 14:14:31 | 2372 | 4.9 | 259.62 |
| 14:14:32 | 2374 | 4.9 | 259.70 |
| 14:14:33 | 2374 | 4.9 | 259.78 |
| 14:14:34 | 2375 | 4.9 | 259.87 |
| 14:14:35 | 2377 | 4.9 | 259.95 |
| 14:14:36 | 2377 | 4.9 | 260.03 |
| 14:14:37 | 2379 | 4.9 | 260.11 |
| 14:14:38 | 2379 | 4.9 | 260.19 |
| 14:14:39 | 2381 | 4.9 | 260.28 |
| 14:14:40 | 2381 | 4.9 | 260.36 |
| 14:14:41 | 2382 | 4.9 | 260.44 |
| 14:14:42 | 2383 | 4.9 | 260.52 |
| 14:14:43 | 2383 | 4.9 | 260.60 |
| 14:14:44 | 2385 | 4.9 | 260.68 |
| 14:14:45 | 2384 | 4.9 | 260.77 |
| 14:14:46 | 2385 | 4.9 | 260.85 |
| 14:14:47 | 2386 | 4.9 | 260.93 |
| 14:14:48 | 2385 | 4.9 | 261.01 |
| 14:14:49 | 2386 | 4.9 | 261.09 |
| 14:14:50 | 2385 | 4.9 | 261.17 |
| 14:14:51 | 2387 | 4.9 | 261.26 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:14:52 | 2386 | 4.9 | 261.34 |
| 14:14:53 | 2387 | 4.9 | 261.42 |
| 14:14:54 | 2388 | 4.9 | 261.50 |
| 14:14:55 | 2388 | 4.9 | 261.58 |
| 14:14:56 | 2390 | 4.9 | 261.67 |
| 14:14:57 | 2389 | 4.9 | 261.75 |
| 14:14:58 | 2391 | 4.9 | 261.83 |
| 14:14:59 | 2391 | 4.9 | 261.91 |
| 14:15:00 | 2392 | 4.9 | 261.99 |
| 14:15:01 | 2393 | 4.9 | 262.07 |
| 14:15:02 | 2393 | 4.9 | 262.16 |
| 14:15:03 | 2395 | 4.9 | 262.24 |
| 14:15:04 | 2394 | 4.9 | 262.32 |
| 14:15:05 | 2396 | 4.9 | 262.40 |
| 14:15:06 | 2396 | 4.9 | 262.48 |
| 14:15:07 | 2396 | 4.9 | 262.56 |
| 14:15:08 | 2398 | 4.9 | 262.65 |
| 14:15:09 | 2397 | 4.9 | 262.73 |
| 14:15:10 | 2399 | 4.9 | 262.81 |
| 14:15:11 | 2399 | 4.9 | 262.89 |
| 14:15:12 | 2399 | 4.9 | 262.97 |
| 14:15:13 | 2400 | 4.9 | 263.06 |
| 14:15:14 | 2400 | 4.9 | 263.14 |
| 14:15:15 | 2401 | 4.9 | 263.22 |
| 14:15:16 | 2399 | 4.9 | 263.30 |
| 14:15:17 | 2401 | 4.9 | 263.38 |
| 14:15:18 | 2400 | 4.9 | 263.46 |
| 14:15:19 | 2400 | 4.9 | 263.55 |
| 14:15:20 | 2401 | 4.9 | 263.63 |
| 14:15:21 | 2401 | 4.9 | 263.71 |
| 14:15:22 | 2402 | 4.9 | 263.79 |
| 14:15:23 | 2401 | 4.9 | 263.87 |
| 14:15:24 | 2403 | 4.9 | 263.95 |
| 14:15:25 | 2402 | 4.9 | 264.04 |
| 14:15:26 | 2403 | 4.9 | 264.12 |
| 14:15:27 | 2404 | 4.9 | 264.20 |
| 14:15:28 | 2404 | 4.9 | 264.28 |
| 14:15:29 | 2406 | 4.9 | 264.36 |
| 14:15:30 | 2406 | 4.9 | 264.45 |
| 14:15:31 | 2408 | 4.9 | 264.53 |
| 14:15:32 | 2408 | 4.9 | 264.61 |
| 14:15:33 | 2407 | 4.9 | 264.69 |
| 14:15:34 | 2408 | 4.9 | 264.77 |
| 14:15:35 | 2408 | 4.9 | 264.85 |
| 14:15:36 | 2409 | 4.9 | 264.94 |
| 14:15:37 | 2408 | 4.9 | 265.02 |
| 14:15:38 | 2409 | 4.9 | 265.10 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:15:39 | 2408 | 4.9 | 265.18 |
| 14:15:40 | 2408 | 4.9 | 265.26 |
| 14:15:41 | 2409 | 4.9 | 265.34 |
| 14:15:42 | 2408 | 4.9 | 265.43 |
| 14:15:43 | 2409 | 4.9 | 265.51 |
| 14:15:44 | 2408 | 4.9 | 265.59 |
| 14:15:45 | 2409 | 4.9 | 265.67 |
| 14:15:46 | 2410 | 4.9 | 265.75 |
| 14:15:47 | 2409 | 4.9 | 265.84 |
| 14:15:48 | 2410 | 4.9 | 265.92 |
| 14:15:49 | 2409 | 4.9 | 266.00 |
| 14:15:50 | 2411 | 4.9 | 266.08 |
| 14:15:51 | 2411 | 4.9 | 266.16 |
| 14:15:52 | 2412 | 4.9 | 266.24 |
| 14:15:53 | 2413 | 4.9 | 266.33 |
| 14:15:54 | 2412 | 4.9 | 266.41 |
| 14:15:55 | 2414 | 4.9 | 266.49 |
| 14:15:56 | 2413 | 4.9 | 266.57 |
| 14:15:57 | 2415 | 4.9 | 266.65 |
| 14:15:58 | 2414 | 4.9 | 266.73 |
| 14:15:59 | 2414 | 4.9 | 266.82 |
| 14:16:00 | 2415 | 4.9 | 266.90 |
| 14:16:01 | 2414 | 4.9 | 266.98 |
| 14:16:02 | 2415 | 4.9 | 267.06 |
| 14:16:03 | 2414 | 4.9 | 267.14 |
| 14:16:04 | 2415 | 4.9 | 267.23 |
| 14:16:05 | 2415 | 4.9 | 267.31 |
| 14:16:06 | 2414 | 4.9 | 267.39 |
| 14:16:07 | 2415 | 4.9 | 267.47 |
| 14:16:08 | 2415 | 4.9 | 267.55 |
| 14:16:09 | 2416 | 4.9 | 267.63 |
| 14:16:10 | 2416 | 4.9 | 267.72 |
| 14:16:11 | 2416 | 4.9 | 267.80 |
| 14:16:12 | 2417 | 4.9 | 267.88 |
| 14:16:13 | 2417 | 4.9 | 267.96 |
| 14:16:14 | 2418 | 4.9 | 268.04 |
| 14:16:15 | 2417 | 4.9 | 268.13 |
| 14:16:16 | 2417 | 4.9 | 268.21 |
| 14:16:17 | 2415 | 4.9 | 268.29 |
| 14:16:18 | 2416 | 4.9 | 268.37 |
| 14:16:19 | 2415 | 4.9 | 268.45 |
| 14:16:20 | 2414 | 4.9 | 268.53 |
| 14:16:21 | 2415 | 4.9 | 268.62 |
| 14:16:22 | 2413 | 4.9 | 268.70 |
| 14:16:23 | 2414 | 4.9 | 268.78 |
| 14:16:24 | 2412 | 4.9 | 268.86 |
| 14:16:25 | 2412 | 4.9 | 268.94 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:16:26 | 2412 | 4.9 | 269.03 |
| 14:16:27 | 2410 | 4.9 | 269.11 |
| 14:16:28 | 2410 | 4.9 | 269.19 |
| 14:16:29 | 2409 | 4.9 | 269.27 |
| 14:16:30 | 2409 | 4.9 | 269.35 |
| 14:16:31 | 2408 | 4.9 | 269.44 |
| 14:16:32 | 2406 | 4.9 | 269.52 |
| 14:16:33 | 2406 | 4.9 | 269.60 |
| 14:16:34 | 2405 | 4.9 | 269.68 |
| 14:16:35 | 2406 | 4.9 | 269.76 |
| 14:16:36 | 2405 | 4.9 | 269.85 |
| 14:16:37 | 2405 | 4.9 | 269.93 |
| 14:16:38 | 2404 | 4.9 | 270.01 |
| 14:16:39 | 2404 | 4.9 | 270.09 |
| 14:16:40 | 2404 | 4.9 | 270.18 |
| 14:16:41 | 2403 | 4.9 | 270.26 |
| 14:16:42 | 2404 | 4.9 | 270.34 |
| 14:16:43 | 2403 | 4.9 | 270.42 |
| 14:16:44 | 2404 | 4.9 | 270.50 |
| 14:16:45 | 2403 | 4.9 | 270.59 |
| 14:16:46 | 2403 | 4.9 | 270.67 |
| 14:16:47 | 2404 | 4.9 | 270.75 |
| 14:16:48 | 2403 | 4.9 | 270.83 |
| 14:16:49 | 2405 | 4.9 | 270.91 |
| 14:16:50 | 2404 | 4.9 | 271.00 |
| 14:16:51 | 2405 | 4.9 | 271.08 |
| 14:16:52 | 2405 | 4.9 | 271.16 |
| 14:16:53 | 2404 | 4.9 | 271.24 |
| 14:16:54 | 2405 | 4.9 | 271.32 |
| 14:16:55 | 2405 | 4.9 | 271.41 |
| 14:16:56 | 2407 | 4.9 | 271.49 |
| 14:16:57 | 2407 | 4.9 | 271.57 |
| 14:16:58 | 2407 | 4.9 | 271.65 |
| 14:16:59 | 2407 | 4.9 | 271.73 |
| 14:17:00 | 2407 | 4.9 | 271.82 |
| 14:17:01 | 2408 | 4.9 | 271.90 |
| 14:17:02 | 2407 | 4.9 | 271.98 |
| 14:17:03 | 2408 | 4.9 | 272.06 |
| 14:17:04 | 2408 | 4.9 | 272.14 |
| 14:17:05 | 2408 | 4.9 | 272.23 |
| 14:17:06 | 2409 | 4.9 | 272.31 |
| 14:17:07 | 2408 | 4.9 | 272.39 |
| 14:17:08 | 2410 | 4.9 | 272.47 |
| 14:17:09 | 2408 | 4.9 | 272.55 |
| 14:17:10 | 2409 | 4.9 | 272.64 |
| 14:17:11 | 2409 | 4.9 | 272.72 |
| 14:17:12 | 2409 | 4.9 | 272.80 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:17:13 | 2410 | 4.9 | 272.88 |
| 14:17:14 | 2408 | 4.9 | 272.96 |
| 14:17:15 | 2409 | 4.9 | 273.05 |
| 14:17:16 | 2408 | 4.9 | 273.13 |
| 14:17:17 | 2408 | 4.9 | 273.21 |
| 14:17:18 | 2409 | 4.9 | 273.29 |
| 14:17:19 | 2408 | 4.9 | 273.37 |
| 14:17:20 | 2410 | 4.9 | 273.46 |
| 14:17:21 | 2409 | 4.9 | 273.54 |
| 14:17:22 | 2411 | 4.9 | 273.62 |
| 14:17:23 | 2410 | 4.9 | 273.70 |
| 14:17:24 | 2411 | 4.9 | 273.78 |
| 14:17:25 | 2411 | 4.9 | 273.87 |
| 14:17:26 | 2411 | 4.9 | 273.95 |
| 14:17:27 | 2413 | 4.9 | 274.03 |
| 14:17:28 | 2412 | 4.9 | 274.11 |
| 14:17:29 | 2414 | 4.9 | 274.19 |
| 14:17:30 | 2414 | 4.9 | 274.28 |
| 14:17:31 | 2414 | 4.9 | 274.36 |
| 14:17:32 | 2415 | 4.9 | 274.44 |
| 14:17:33 | 2414 | 4.9 | 274.52 |
| 14:17:34 | 2416 | 4.9 | 274.60 |
| 14:17:35 | 2415 | 4.9 | 274.69 |
| 14:17:36 | 2416 | 4.9 | 274.77 |
| 14:17:37 | 2415 | 4.9 | 274.85 |
| 14:17:38 | 2415 | 4.9 | 274.93 |
| 14:17:39 | 2415 | 4.9 | 275.01 |
| 14:17:40 | 2413 | 4.9 | 275.09 |
| 14:17:41 | 2415 | 4.9 | 275.18 |
| 14:17:42 | 2414 | 4.9 | 275.26 |
| 14:17:43 | 2415 | 4.9 | 275.34 |
| 14:17:44 | 2414 | 4.9 | 275.42 |
| 14:17:45 | 2415 | 4.9 | 275.50 |
| 14:17:46 | 2415 | 4.9 | 275.59 |
| 14:17:47 | 2414 | 4.9 | 275.67 |
| 14:17:48 | 2415 | 4.9 | 275.75 |
| 14:17:49 | 2413 | 4.9 | 275.83 |
| 14:17:50 | 2415 | 4.9 | 275.91 |
| 14:17:51 | 2415 | 4.9 | 276.00 |
| 14:17:52 | 2415 | 4.9 | 276.08 |
| 14:17:53 | 2417 | 4.9 | 276.16 |
| 14:17:54 | 2416 | 4.9 | 276.24 |
| 14:17:55 | 2417 | 4.9 | 276.32 |
| 14:17:56 | 2416 | 4.9 | 276.41 |
| 14:17:57 | 2417 | 4.9 | 276.49 |
| 14:17:58 | 2417 | 4.9 | 276.57 |
| 14:17:59 | 2417 | 4.9 | 276.65 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:18:00 | 2417 | 4.9 | 276.73 |
| 14:18:01 | 2416 | 4.9 | 276.82 |
| 14:18:02 | 2417 | 4.9 | 276.90 |
| 14:18:03 | 2416 | 4.9 | 276.98 |
| 14:18:04 | 2416 | 4.9 | 277.06 |
| 14:18:05 | 2417 | 4.9 | 277.14 |
| 14:18:06 | 2416 | 4.9 | 277.23 |
| 14:18:07 | 2417 | 4.9 | 277.31 |
| 14:18:08 | 2416 | 4.9 | 277.39 |
| 14:18:09 | 2417 | 4.9 | 277.47 |
| 14:18:10 | 2416 | 4.9 | 277.55 |
| 14:18:11 | 2416 | 4.9 | 277.64 |
| 14:18:12 | 2417 | 4.9 | 277.72 |
| 14:18:13 | 2415 | 4.9 | 277.80 |
| 14:18:14 | 2417 | 4.9 | 277.88 |
| 14:18:15 | 2415 | 4.9 | 277.96 |
| 14:18:16 | 2416 | 4.9 | 278.05 |
| 14:18:17 | 2416 | 4.9 | 278.13 |
| 14:18:18 | 2416 | 4.9 | 278.21 |
| 14:18:19 | 2418 | 4.9 | 278.29 |
| 14:18:20 | 2416 | 4.9 | 278.37 |
| 14:18:21 | 2418 | 4.9 | 278.46 |
| 14:18:22 | 2417 | 4.9 | 278.54 |
| 14:18:23 | 2416 | 4.9 | 278.62 |
| 14:18:24 | 2416 | 4.9 | 278.70 |
| 14:18:25 | 2415 | 4.9 | 278.78 |
| 14:18:26 | 2416 | 4.9 | 278.87 |
| 14:18:27 | 2415 | 4.9 | 278.95 |
| 14:18:28 | 2415 | 4.9 | 279.03 |
| 14:18:29 | 2414 | 4.9 | 279.11 |
| 14:18:30 | 2413 | 4.9 | 279.19 |
| 14:18:31 | 2414 | 4.9 | 279.28 |
| 14:18:32 | 2413 | 4.9 | 279.36 |
| 14:18:33 | 2415 | 4.9 | 279.44 |
| 14:18:34 | 2414 | 4.9 | 279.52 |
| 14:18:35 | 2415 | 4.9 | 279.60 |
| 14:18:36 | 2414 | 4.9 | 279.69 |
| 14:18:37 | 2414 | 4.9 | 279.77 |
| 14:18:38 | 2415 | 4.9 | 279.85 |
| 14:18:39 | 2414 | 4.9 | 279.93 |
| 14:18:40 | 2416 | 4.9 | 280.01 |
| 14:18:41 | 2415 | 4.9 | 280.10 |
| 14:18:42 | 2416 | 4.9 | 280.18 |
| 14:18:43 | 2417 | 4.9 | 280.26 |
| 14:18:44 | 2417 | 4.9 | 280.34 |
| 14:18:45 | 2419 | 4.9 | 280.42 |
| 14:18:46 | 2417 | 4.9 | 280.51 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:18:47 | 2418 | 4.9 | 280.59 |
| 14:18:48 | 2418 | 4.9 | 280.67 |
| 14:18:49 | 2418 | 4.9 | 280.75 |
| 14:18:50 | 2418 | 4.9 | 280.83 |
| 14:18:51 | 2417 | 4.9 | 280.92 |
| 14:18:52 | 2418 | 4.9 | 281.00 |
| 14:18:53 | 2416 | 4.9 | 281.08 |
| 14:18:54 | 2417 | 4.9 | 281.16 |
| 14:18:55 | 2416 | 4.9 | 281.24 |
| 14:18:56 | 2416 | 4.9 | 281.33 |
| 14:18:57 | 2416 | 4.9 | 281.41 |
| 14:18:58 | 2416 | 4.9 | 281.49 |
| 14:18:59 | 2417 | 4.9 | 281.57 |
| 14:19:00 | 2416 | 4.9 | 281.65 |
| 14:19:01 | 2417 | 4.9 | 281.74 |
| 14:19:02 | 2416 | 4.9 | 281.82 |
| 14:19:03 | 2417 | 4.9 | 281.90 |
| 14:19:04 | 2418 | 4.9 | 281.98 |
| 14:19:05 | 2417 | 4.9 | 282.06 |
| 14:19:06 | 2419 | 4.9 | 282.15 |
| 14:19:07 | 2418 | 4.9 | 282.23 |
| 14:19:08 | 2419 | 4.9 | 282.31 |
| 14:19:09 | 2419 | 4.9 | 282.39 |
| 14:19:10 | 2419 | 4.9 | 282.47 |
| 14:19:11 | 2420 | 4.9 | 282.56 |
| 14:19:12 | 2419 | 4.9 | 282.64 |
| 14:19:13 | 2420 | 4.9 | 282.72 |
| 14:19:14 | 2419 | 4.9 | 282.80 |
| 14:19:15 | 2420 | 4.9 | 282.88 |
| 14:19:16 | 2419 | 4.9 | 282.97 |
| 14:19:17 | 2418 | 4.9 | 283.05 |
| 14:19:18 | 2419 | 4.9 | 283.13 |
| 14:19:19 | 2418 | 4.9 | 283.21 |
| 14:19:20 | 2419 | 4.9 | 283.29 |
| 14:19:21 | 2417 | 4.9 | 283.38 |
| 14:19:22 | 2417 | 4.9 | 283.46 |
| 14:19:23 | 2417 | 4.9 | 283.54 |
| 14:19:24 | 2416 | 4.9 | 283.62 |
| 14:19:25 | 2418 | 4.9 | 283.70 |
| 14:19:26 | 2416 | 4.9 | 283.79 |
| 14:19:27 | 2418 | 4.9 | 283.87 |
| 14:19:28 | 2418 | 4.9 | 283.95 |
| 14:19:29 | 2418 | 4.9 | 284.03 |
| 14:19:30 | 2419 | 4.9 | 284.11 |
| 14:19:31 | 2419 | 4.9 | 284.20 |
| 14:19:32 | 2420 | 4.9 | 284.28 |
| 14:19:33 | 2419 | 4.9 | 284.36 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:19:34 | 2421 | 4.9 | 284.44 |
| 14:19:35 | 2420 | 4.9 | 284.52 |
| 14:19:36 | 2421 | 4.9 | 284.61 |
| 14:19:37 | 2421 | 4.9 | 284.69 |
| 14:19:38 | 2420 | 4.9 | 284.77 |
| 14:19:39 | 2421 | 4.9 | 284.85 |
| 14:19:40 | 2420 | 4.9 | 284.93 |
| 14:19:41 | 2420 | 4.9 | 285.02 |
| 14:19:42 | 2420 | 4.9 | 285.10 |
| 14:19:43 | 2420 | 4.9 | 285.18 |
| 14:19:44 | 2421 | 4.9 | 285.26 |
| 14:19:45 | 2419 | 4.9 | 285.34 |
| 14:19:46 | 2421 | 4.9 | 285.43 |
| 14:19:47 | 2420 | 4.9 | 285.51 |
| 14:19:48 | 2421 | 4.9 | 285.59 |
| 14:19:49 | 2420 | 4.9 | 285.67 |
| 14:19:50 | 2421 | 4.9 | 285.75 |
| 14:19:51 | 2421 | 4.9 | 285.84 |
| 14:19:52 | 2421 | 4.9 | 285.92 |
| 14:19:53 | 2422 | 4.9 | 286.00 |
| 14:19:54 | 2421 | 4.9 | 286.08 |
| 14:19:55 | 2422 | 4.9 | 286.16 |
| 14:19:56 | 2422 | 4.9 | 286.25 |
| 14:19:57 | 2422 | 4.9 | 286.33 |
| 14:19:58 | 2424 | 4.9 | 286.41 |
| 14:19:59 | 2423 | 4.9 | 286.49 |
| 14:20:00 | 2425 | 4.9 | 286.57 |
| 14:20:01 | 2424 | 4.9 | 286.66 |
| 14:20:02 | 2424 | 4.9 | 286.74 |
| 14:20:03 | 2425 | 4.9 | 286.82 |
| 14:20:04 | 2424 | 4.9 | 286.90 |
| 14:20:05 | 2425 | 4.9 | 286.98 |
| 14:20:06 | 2424 | 4.9 | 287.07 |
| 14:20:07 | 2425 | 4.9 | 287.15 |
| 14:20:08 | 2424 | 4.9 | 287.23 |
| 14:20:09 | 2424 | 4.9 | 287.31 |
| 14:20:10 | 2425 | 4.9 | 287.39 |
| 14:20:11 | 2424 | 4.9 | 287.48 |
| 14:20:12 | 2425 | 4.9 | 287.56 |
| 14:20:13 | 2424 | 4.9 | 287.64 |
| 14:20:14 | 2425 | 4.9 | 287.72 |
| 14:20:15 | 2425 | 4.9 | 287.80 |
| 14:20:16 | 2425 | 4.9 | 287.89 |
| 14:20:17 | 2426 | 4.9 | 287.97 |
| 14:20:18 | 2425 | 4.9 | 288.05 |
| 14:20:19 | 2427 | 4.9 | 288.13 |
| 14:20:20 | 2426 | 4.9 | 288.21 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:20:21 | 2427 | 4.9 | 288.30 |
| 14:20:22 | 2427 | 4.9 | 288.38 |
| 14:20:23 | 2427 | 4.9 | 288.46 |
| 14:20:24 | 2429 | 4.9 | 288.54 |
| 14:20:25 | 2427 | 4.9 | 288.62 |
| 14:20:26 | 2429 | 4.9 | 288.71 |
| 14:20:27 | 2428 | 4.9 | 288.79 |
| 14:20:28 | 2429 | 4.9 | 288.87 |
| 14:20:29 | 2430 | 4.9 | 288.95 |
| 14:20:30 | 2428 | 4.9 | 289.03 |
| 14:20:31 | 2429 | 4.9 | 289.12 |
| 14:20:32 | 2429 | 4.9 | 289.20 |
| 14:20:33 | 2430 | 4.9 | 289.28 |
| 14:20:34 | 2429 | 4.9 | 289.36 |
| 14:20:35 | 2429 | 4.9 | 289.44 |
| 14:20:36 | 2429 | 4.9 | 289.53 |
| 14:20:37 | 2429 | 4.9 | 289.61 |
| 14:20:38 | 2430 | 4.9 | 289.69 |
| 14:20:39 | 2429 | 4.9 | 289.77 |
| 14:20:40 | 2430 | 4.9 | 289.85 |
| 14:20:41 | 2429 | 4.9 | 289.94 |
| 14:20:42 | 2430 | 4.9 | 290.02 |
| 14:20:43 | 2431 | 4.9 | 290.10 |
| 14:20:44 | 2430 | 4.9 | 290.18 |
| 14:20:45 | 2432 | 4.9 | 290.26 |
| 14:20:46 | 2431 | 4.9 | 290.35 |
| 14:20:47 | 2432 | 4.9 | 290.43 |
| 14:20:48 | 2433 | 4.9 | 290.51 |
| 14:20:49 | 2433 | 4.9 | 290.59 |
| 14:20:50 | 2435 | 4.9 | 290.67 |
| 14:20:51 | 2434 | 4.9 | 290.76 |
| 14:20:52 | 2436 | 4.9 | 290.84 |
| 14:20:53 | 2435 | 4.9 | 290.92 |
| 14:20:54 | 2437 | 4.9 | 291.00 |
| 14:20:55 | 2436 | 4.9 | 291.08 |
| 14:20:56 | 2436 | 4.9 | 291.17 |
| 14:20:57 | 2437 | 4.9 | 291.25 |
| 14:20:58 | 2436 | 4.9 | 291.33 |
| 14:20:59 | 2437 | 4.9 | 291.41 |
| 14:21:00 | 2436 | 4.9 | 291.49 |
| 14:21:01 | 2436 | 4.9 | 291.58 |
| 14:21:02 | 2436 | 4.9 | 291.66 |
| 14:21:03 | 2435 | 4.9 | 291.74 |
| 14:21:04 | 2436 | 4.9 | 291.82 |
| 14:21:05 | 2435 | 4.9 | 291.90 |
| 14:21:06 | 2436 | 4.9 | 291.98 |
| 14:21:07 | 2435 | 4.9 | 292.07 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:21:08 | 2436 | 4.9 | 292.15 |
| 14:21:09 | 2436 | 4.9 | 292.23 |
| 14:21:10 | 2435 | 4.9 | 292.31 |
| 14:21:11 | 2438 | 4.9 | 292.39 |
| 14:21:12 | 2437 | 4.9 | 292.48 |
| 14:21:13 | 2439 | 4.9 | 292.56 |
| 14:21:14 | 2438 | 4.9 | 292.64 |
| 14:21:15 | 2439 | 4.9 | 292.72 |
| 14:21:16 | 2439 | 4.9 | 292.80 |
| 14:21:17 | 2438 | 4.9 | 292.89 |
| 14:21:18 | 2440 | 4.9 | 292.97 |
| 14:21:19 | 2438 | 4.9 | 293.05 |
| 14:21:20 | 2440 | 4.9 | 293.13 |
| 14:21:21 | 2440 | 4.9 | 293.21 |
| 14:21:22 | 2439 | 4.9 | 293.30 |
| 14:21:23 | 2440 | 4.9 | 293.38 |
| 14:21:24 | 2439 | 4.9 | 293.46 |
| 14:21:25 | 2440 | 4.9 | 293.54 |
| 14:21:26 | 2439 | 4.9 | 293.62 |
| 14:21:27 | 2439 | 4.9 | 293.71 |
| 14:21:28 | 2439 | 4.9 | 293.79 |
| 14:21:29 | 2439 | 4.9 | 293.87 |
| 14:21:30 | 2440 | 4.9 | 293.95 |
| 14:21:31 | 2440 | 4.9 | 294.03 |
| 14:21:32 | 2441 | 4.9 | 294.12 |
| 14:21:33 | 2440 | 4.9 | 294.20 |
| 14:21:34 | 2440 | 4.9 | 294.28 |
| 14:21:35 | 2442 | 4.9 | 294.36 |
| 14:21:36 | 2441 | 4.9 | 294.44 |
| 14:21:37 | 2443 | 4.9 | 294.53 |
| 14:21:38 | 2441 | 4.9 | 294.61 |
| 14:21:39 | 2443 | 4.9 | 294.69 |
| 14:21:40 | 2443 | 4.9 | 294.77 |
| 14:21:41 | 2444 | 4.9 | 294.85 |
| 14:21:42 | 2444 | 4.9 | 294.93 |
| 14:21:43 | 2444 | 4.9 | 295.02 |
| 14:21:44 | 2446 | 4.9 | 295.10 |
| 14:21:45 | 2444 | 4.9 | 295.18 |
| 14:21:46 | 2444 | 4.9 | 295.26 |
| 14:21:47 | 2444 | 4.9 | 295.34 |
| 14:21:48 | 2444 | 4.9 | 295.43 |
| 14:21:49 | 2445 | 4.9 | 295.51 |
| 14:21:50 | 2444 | 4.9 | 295.59 |
| 14:21:51 | 2445 | 4.9 | 295.67 |
| 14:21:52 | 2444 | 4.9 | 295.75 |
| 14:21:53 | 2444 | 4.9 | 295.84 |
| 14:21:54 | 2444 | 4.9 | 295.92 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:21:55 | 2443 | 4.9 | 296.00 |
| 14:21:56 | 2445 | 4.9 | 296.08 |
| 14:21:57 | 2444 | 4.9 | 296.16 |
| 14:21:58 | 2446 | 4.9 | 296.25 |
| 14:21:59 | 2444 | 4.9 | 296.33 |
| 14:22:00 | 2446 | 4.9 | 296.41 |
| 14:22:01 | 2446 | 4.9 | 296.49 |
| 14:22:02 | 2446 | 4.9 | 296.57 |
| 14:22:03 | 2448 | 4.9 | 296.66 |
| 14:22:04 | 2447 | 4.9 | 296.74 |
| 14:22:05 | 2449 | 4.9 | 296.82 |
| 14:22:06 | 2448 | 4.9 | 296.90 |
| 14:22:07 | 2449 | 4.9 | 296.98 |
| 14:22:08 | 2450 | 4.9 | 297.07 |
| 14:22:09 | 2449 | 4.9 | 297.15 |
| 14:22:10 | 2450 | 4.9 | 297.23 |
| 14:22:11 | 2449 | 4.9 | 297.31 |
| 14:22:12 | 2450 | 4.9 | 297.39 |
| 14:22:13 | 2450 | 4.9 | 297.47 |
| 14:22:14 | 2449 | 4.9 | 297.56 |
| 14:22:15 | 2450 | 4.9 | 297.64 |
| 14:22:16 | 2449 | 4.9 | 297.72 |
| 14:22:17 | 2449 | 4.9 | 297.80 |
| 14:22:18 | 2448 | 4.9 | 297.88 |
| 14:22:19 | 2449 | 4.9 | 297.97 |
| 14:22:20 | 2448 | 4.9 | 298.05 |
| 14:22:21 | 2449 | 4.9 | 298.13 |
| 14:22:22 | 2449 | 4.9 | 298.21 |
| 14:22:23 | 2449 | 4.9 | 298.29 |
| 14:22:24 | 2450 | 4.9 | 298.38 |
| 14:22:25 | 2449 | 4.9 | 298.46 |
| 14:22:26 | 2450 | 4.9 | 298.54 |
| 14:22:27 | 2450 | 4.9 | 298.62 |
| 14:22:28 | 2450 | 4.9 | 298.70 |
| 14:22:29 | 2452 | 4.9 | 298.79 |
| 14:22:30 | 2451 | 4.9 | 298.87 |
| 14:22:31 | 2453 | 4.9 | 298.95 |
| 14:22:32 | 2452 | 4.9 | 299.03 |
| 14:22:33 | 2452 | 4.9 | 299.11 |
| 14:22:34 | 2453 | 4.9 | 299.19 |
| 14:22:35 | 2452 | 4.9 | 299.28 |
| 14:22:36 | 2453 | 4.9 | 299.36 |
| 14:22:37 | 2452 | 4.9 | 299.44 |
| 14:22:38 | 2453 | 4.9 | 299.52 |
| 14:22:39 | 2452 | 4.9 | 299.60 |
| 14:22:40 | 2453 | 4.9 | 299.69 |
| 14:22:41 | 2453 | 4.9 | 299.77 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:22:42 | 2452 | 4.9 | 299.85 |
| 14:22:43 | 2453 | 4.9 | 299.93 |
| 14:22:44 | 2452 | 4.9 | 300.01 |
| 14:22:45 | 2453 | 4.9 | 300.10 |
| 14:22:46 | 2452 | 4.9 | 300.18 |
| 14:22:47 | 2452 | 4.9 | 300.26 |
| 14:22:48 | 2453 | 4.9 | 300.34 |
| 14:22:49 | 2452 | 4.9 | 300.42 |
| 14:22:50 | 2454 | 4.9 | 300.50 |
| 14:22:51 | 2453 | 4.9 | 300.59 |
| 14:22:52 | 2454 | 4.9 | 300.67 |
| 14:22:53 | 2454 | 4.9 | 300.75 |
| 14:22:54 | 2454 | 4.9 | 300.83 |
| 14:22:55 | 2456 | 4.9 | 300.91 |
| 14:22:56 | 2454 | 4.9 | 301.00 |
| 14:22:57 | 2456 | 4.9 | 301.08 |
| 14:22:58 | 2456 | 4.9 | 301.16 |
| 14:22:59 | 2456 | 4.9 | 301.24 |
| 14:23:00 | 2457 | 4.9 | 301.32 |
| 14:23:01 | 2456 | 4.9 | 301.41 |
| 14:23:02 | 2457 | 4.9 | 301.49 |
| 14:23:03 | 2456 | 4.9 | 301.57 |
| 14:23:04 | 2457 | 4.9 | 301.65 |
| 14:23:05 | 2456 | 4.9 | 301.73 |
| 14:23:06 | 2456 | 4.9 | 301.81 |
| 14:23:07 | 2456 | 4.9 | 301.90 |
| 14:23:08 | 2455 | 4.9 | 301.98 |
| 14:23:09 | 2457 | 4.9 | 302.06 |
| 14:23:10 | 2456 | 4.9 | 302.14 |
| 14:23:11 | 2457 | 4.9 | 302.22 |
| 14:23:12 | 2456 | 4.9 | 302.31 |
| 14:23:13 | 2457 | 4.9 | 302.39 |
| 14:23:14 | 2457 | 4.9 | 302.47 |
| 14:23:15 | 2456 | 4.9 | 302.55 |
| 14:23:16 | 2458 | 4.9 | 302.63 |
| 14:23:17 | 2457 | 4.9 | 302.72 |
| 14:23:18 | 2458 | 4.9 | 302.80 |
| 14:23:19 | 2458 | 4.9 | 302.88 |
| 14:23:20 | 2458 | 4.9 | 302.96 |
| 14:23:21 | 2459 | 4.9 | 303.04 |
| 14:23:22 | 2458 | 4.9 | 303.12 |
| 14:23:23 | 2460 | 4.9 | 303.21 |
| 14:23:24 | 2459 | 4.9 | 303.29 |
| 14:23:25 | 2460 | 4.9 | 303.37 |
| 14:23:26 | 2460 | 4.9 | 303.45 |
| 14:23:27 | 2459 | 4.9 | 303.53 |
| 14:23:28 | 2461 | 4.9 | 303.62 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:23:29 | 2459 | 4.9 | 303.70 |
| 14:23:30 | 2461 | 4.9 | 303.78 |
| 14:23:31 | 2460 | 4.9 | 303.86 |
| 14:23:32 | 2460 | 4.9 | 303.94 |
| 14:23:33 | 2461 | 4.9 | 304.02 |
| 14:23:34 | 2460 | 4.9 | 304.11 |
| 14:23:35 | 2461 | 4.9 | 304.19 |
| 14:23:36 | 2460 | 4.9 | 304.27 |
| 14:23:37 | 2461 | 4.9 | 304.35 |
| 14:23:38 | 2461 | 4.9 | 304.43 |
| 14:23:39 | 2461 | 4.9 | 304.52 |
| 14:23:40 | 2463 | 4.9 | 304.60 |
| 14:23:41 | 2462 | 4.9 | 304.68 |
| 14:23:42 | 2464 | 4.9 | 304.76 |
| 14:23:43 | 2463 | 4.9 | 304.84 |
| 14:23:44 | 2464 | 4.9 | 304.93 |
| 14:23:45 | 2464 | 4.9 | 305.01 |
| 14:23:46 | 2464 | 4.9 | 305.09 |
| 14:23:47 | 2465 | 4.9 | 305.17 |
| 14:23:48 | 2464 | 4.9 | 305.25 |
| 14:23:49 | 2465 | 4.9 | 305.33 |
| 14:23:50 | 2463 | 4.9 | 305.42 |
| 14:23:51 | 2465 | 4.9 | 305.50 |
| 14:23:52 | 2464 | 4.9 | 305.58 |
| 14:23:53 | 2464 | 4.9 | 305.66 |
| 14:23:54 | 2464 | 4.9 | 305.74 |
| 14:23:55 | 2463 | 4.9 | 305.83 |
| 14:23:56 | 2464 | 4.9 | 305.91 |
| 14:23:57 | 2463 | 4.9 | 305.99 |
| 14:23:58 | 2463 | 4.9 | 306.07 |
| 14:23:59 | 2464 | 4.9 | 306.15 |
| 14:24:00 | 2463 | 4.9 | 306.23 |
| 14:24:01 | 2464 | 4.9 | 306.32 |
| 14:24:02 | 2463 | 4.9 | 306.40 |
| 14:24:03 | 2464 | 4.9 | 306.48 |
| 14:24:04 | 2463 | 4.9 | 306.56 |
| 14:24:05 | 2464 | 4.9 | 306.64 |
| 14:24:06 | 2464 | 4.9 | 306.73 |
| 14:24:07 | 2464 | 4.9 | 306.81 |
| 14:24:08 | 2466 | 4.9 | 306.89 |
| 14:24:09 | 2465 | 4.9 | 306.97 |
| 14:24:10 | 2467 | 4.9 | 307.05 |
| 14:24:11 | 2466 | 4.9 | 307.14 |
| 14:24:12 | 2467 | 4.9 | 307.22 |
| 14:24:13 | 2468 | 4.9 | 307.30 |
| 14:24:14 | 2466 | 4.9 | 307.38 |
| 14:24:15 | 2468 | 4.9 | 307.46 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:24:16 | 2466 | 4.9 | 307.54 |
| 14:24:17 | 2467 | 4.9 | 307.63 |
| 14:24:18 | 2467 | 4.9 | 307.71 |
| 14:24:19 | 2466 | 4.9 | 307.79 |
| 14:24:20 | 2467 | 4.9 | 307.87 |
| 14:24:21 | 2465 | 4.9 | 307.95 |
| 14:24:22 | 2467 | 4.9 | 308.04 |
| 14:24:23 | 2465 | 4.9 | 308.12 |
| 14:24:24 | 2466 | 4.9 | 308.20 |
| 14:24:25 | 2465 | 4.9 | 308.28 |
| 14:24:26 | 2466 | 4.9 | 308.36 |
| 14:24:27 | 2467 | 4.9 | 308.44 |
| 14:24:28 | 2466 | 4.9 | 308.53 |
| 14:24:29 | 2468 | 4.9 | 308.61 |
| 14:24:30 | 2466 | 4.9 | 308.69 |
| 14:24:31 | 2468 | 4.9 | 308.77 |
| 14:24:32 | 2468 | 4.9 | 308.85 |
| 14:24:33 | 2467 | 4.9 | 308.94 |
| 14:24:34 | 2469 | 4.9 | 309.02 |
| 14:24:35 | 2468 | 4.9 | 309.10 |
| 14:24:36 | 2470 | 4.9 | 309.18 |
| 14:24:37 | 2469 | 4.9 | 309.26 |
| 14:24:38 | 2469 | 4.9 | 309.34 |
| 14:24:39 | 2470 | 4.9 | 309.43 |
| 14:24:40 | 2468 | 4.9 | 309.51 |
| 14:24:41 | 2470 | 4.9 | 309.59 |
| 14:24:42 | 2468 | 4.9 | 309.67 |
| 14:24:43 | 2469 | 4.9 | 309.75 |
| 14:24:44 | 2469 | 4.9 | 309.84 |
| 14:24:45 | 2469 | 4.9 | 309.92 |
| 14:24:46 | 2469 | 4.9 | 310.00 |
| 14:24:47 | 2468 | 4.9 | 310.08 |
| 14:24:48 | 2469 | 4.9 | 310.16 |
| 14:24:49 | 2468 | 4.9 | 310.25 |
| 14:24:50 | 2469 | 4.9 | 310.33 |
| 14:24:51 | 2468 | 4.9 | 310.41 |
| 14:24:52 | 2469 | 4.9 | 310.49 |
| 14:24:53 | 2470 | 4.9 | 310.57 |
| 14:24:54 | 2469 | 4.9 | 310.65 |
| 14:24:55 | 2471 | 4.9 | 310.74 |
| 14:24:56 | 2470 | 4.9 | 310.82 |
| 14:24:57 | 2471 | 4.9 | 310.90 |
| 14:24:58 | 2471 | 4.9 | 310.98 |
| 14:24:59 | 2471 | 4.9 | 311.06 |
| 14:25:00 | 2472 | 4.9 | 311.15 |
| 14:25:01 | 2471 | 4.9 | 311.23 |
| 14:25:02 | 2473 | 4.9 | 311.31 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:25:03 | 2472 | 4.9 | 311.39 |
| 14:25:04 | 2472 | 4.9 | 311.47 |
| 14:25:05 | 2473 | 4.9 | 311.55 |
| 14:25:06 | 2472 | 4.9 | 311.64 |
| 14:25:07 | 2472 | 4.9 | 311.72 |
| 14:25:08 | 2471 | 4.9 | 311.80 |
| 14:25:09 | 2472 | 4.9 | 311.88 |
| 14:25:10 | 2471 | 4.9 | 311.96 |
| 14:25:11 | 2471 | 4.9 | 312.05 |
| 14:25:12 | 2471 | 4.9 | 312.13 |
| 14:25:13 | 2471 | 4.9 | 312.21 |
| 14:25:14 | 2472 | 4.9 | 312.29 |
| 14:25:15 | 2471 | 4.9 | 312.37 |
| 14:25:16 | 2472 | 4.9 | 312.45 |
| 14:25:17 | 2471 | 4.9 | 312.54 |
| 14:25:18 | 2472 | 4.9 | 312.62 |
| 14:25:19 | 2473 | 4.9 | 312.70 |
| 14:25:20 | 2472 | 4.9 | 312.78 |
| 14:25:21 | 2474 | 4.9 | 312.86 |
| 14:25:22 | 2473 | 4.9 | 312.95 |
| 14:25:23 | 2474 | 4.9 | 313.03 |
| 14:25:24 | 2475 | 4.9 | 313.11 |
| 14:25:25 | 2475 | 4.9 | 313.19 |
| 14:25:26 | 2476 | 4.9 | 313.27 |
| 14:25:27 | 2476 | 4.9 | 313.35 |
| 14:25:28 | 2478 | 4.9 | 313.44 |
| 14:25:29 | 2476 | 4.9 | 313.52 |
| 14:25:30 | 2477 | 4.9 | 313.60 |
| 14:25:31 | 2477 | 4.9 | 313.68 |
| 14:25:32 | 2476 | 4.9 | 313.76 |
| 14:25:33 | 2477 | 4.9 | 313.85 |
| 14:25:34 | 2476 | 4.9 | 313.93 |
| 14:25:35 | 2477 | 4.9 | 314.01 |
| 14:25:36 | 2476 | 4.9 | 314.09 |
| 14:25:37 | 2477 | 4.9 | 314.17 |
| 14:25:38 | 2476 | 4.9 | 314.25 |
| 14:25:39 | 2475 | 4.9 | 314.34 |
| 14:25:40 | 2476 | 4.9 | 314.42 |
| 14:25:41 | 2475 | 4.9 | 314.50 |
| 14:25:42 | 2477 | 4.9 | 314.58 |
| 14:25:43 | 2476 | 4.9 | 314.66 |
| 14:25:44 | 2477 | 4.9 | 314.75 |
| 14:25:45 | 2477 | 4.9 | 314.83 |
| 14:25:46 | 2477 | 4.9 | 314.91 |
| 14:25:47 | 2478 | 4.9 | 314.99 |
| 14:25:48 | 2477 | 4.9 | 315.07 |
| 14:25:49 | 2479 | 4.9 | 315.15 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:25:50 | 2478 | 4.9 | 315.24 |
| 14:25:51 | 2479 | 4.9 | 315.32 |
| 14:25:52 | 2479 | 4.9 | 315.40 |
| 14:25:53 | 2478 | 4.9 | 315.48 |
| 14:25:54 | 2480 | 4.9 | 315.56 |
| 14:25:55 | 2478 | 4.9 | 315.64 |
| 14:25:56 | 2479 | 4.9 | 315.73 |
| 14:25:57 | 2479 | 4.9 | 315.81 |
| 14:25:58 | 2479 | 4.9 | 315.89 |
| 14:25:59 | 2479 | 4.9 | 315.97 |
| 14:26:00 | 2478 | 4.9 | 316.05 |
| 14:26:01 | 2479 | 4.9 | 316.14 |
| 14:26:02 | 2478 | 4.9 | 316.22 |
| 14:26:03 | 2478 | 4.9 | 316.30 |
| 14:26:04 | 2478 | 4.9 | 316.38 |
| 14:26:05 | 2478 | 4.9 | 316.46 |
| 14:26:06 | 2479 | 4.9 | 316.54 |
| 14:26:07 | 2478 | 4.9 | 316.63 |
| 14:26:08 | 2480 | 4.9 | 316.71 |
| 14:26:09 | 2479 | 4.9 | 316.79 |
| 14:26:10 | 2481 | 4.9 | 316.87 |
| 14:26:11 | 2481 | 4.9 | 316.95 |
| 14:26:12 | 2481 | 4.9 | 317.03 |
| 14:26:13 | 2482 | 4.9 | 317.12 |
| 14:26:14 | 2481 | 4.9 | 317.20 |
| 14:26:15 | 2483 | 4.9 | 317.28 |
| 14:26:16 | 2482 | 4.9 | 317.36 |
| 14:26:17 | 2483 | 4.9 | 317.44 |
| 14:26:18 | 2483 | 4.9 | 317.53 |
| 14:26:19 | 2482 | 4.9 | 317.61 |
| 14:26:20 | 2484 | 4.9 | 317.69 |
| 14:26:21 | 2483 | 4.9 | 317.77 |
| 14:26:22 | 2483 | 4.9 | 317.85 |
| 14:26:23 | 2483 | 4.9 | 317.93 |
| 14:26:24 | 2482 | 4.9 | 318.02 |
| 14:26:25 | 2483 | 4.9 | 318.10 |
| 14:26:26 | 2482 | 4.9 | 318.18 |
| 14:26:27 | 2484 | 4.9 | 318.26 |
| 14:26:28 | 2483 | 4.9 | 318.34 |
| 14:26:29 | 2483 | 4.9 | 318.43 |
| 14:26:30 | 2483 | 4.9 | 318.51 |
| 14:26:31 | 2483 | 4.9 | 318.59 |
| 14:26:32 | 2483 | 4.9 | 318.67 |
| 14:26:33 | 2483 | 4.9 | 318.75 |
| 14:26:34 | 2485 | 4.9 | 318.83 |
| 14:26:35 | 2483 | 4.9 | 318.92 |
| 14:26:36 | 2485 | 4.9 | 319.00 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:26:37 | 2485 | 4.9 | 319.08 |
| 14:26:38 | 2485 | 4.9 | 319.16 |
| 14:26:39 | 2486 | 4.9 | 319.24 |
| 14:26:40 | 2485 | 4.9 | 319.32 |
| 14:26:41 | 2486 | 4.9 | 319.41 |
| 14:26:42 | 2486 | 4.9 | 319.49 |
| 14:26:43 | 2487 | 4.9 | 319.57 |
| 14:26:44 | 2487 | 4.9 | 319.65 |
| 14:26:45 | 2486 | 4.9 | 319.73 |
| 14:26:46 | 2488 | 4.9 | 319.82 |
| 14:26:47 | 2486 | 4.9 | 319.90 |
| 14:26:48 | 2487 | 4.9 | 319.98 |
| 14:26:49 | 2487 | 4.9 | 320.06 |
| 14:26:50 | 2487 | 4.9 | 320.14 |
| 14:26:51 | 2487 | 4.9 | 320.22 |
| 14:26:52 | 2486 | 4.9 | 320.31 |
| 14:26:53 | 2487 | 4.9 | 320.39 |
| 14:26:54 | 2485 | 4.9 | 320.47 |
| 14:26:55 | 2486 | 4.9 | 320.55 |
| 14:26:56 | 2485 | 4.9 | 320.63 |
| 14:26:57 | 2486 | 4.9 | 320.72 |
| 14:26:58 | 2486 | 4.9 | 320.80 |
| 14:26:59 | 2485 | 4.9 | 320.88 |
| 14:27:00 | 2487 | 4.9 | 320.96 |
| 14:27:01 | 2486 | 4.9 | 321.04 |
| 14:27:02 | 2487 | 4.9 | 321.12 |
| 14:27:03 | 2487 | 4.9 | 321.21 |
| 14:27:04 | 2487 | 4.9 | 321.29 |
| 14:27:05 | 2488 | 4.9 | 321.37 |
| 14:27:06 | 2487 | 4.9 | 321.45 |
| 14:27:07 | 2489 | 4.9 | 321.53 |
| 14:27:08 | 2488 | 4.9 | 321.61 |
| 14:27:09 | 2489 | 4.9 | 321.70 |
| 14:27:10 | 2489 | 4.9 | 321.78 |
| 14:27:11 | 2488 | 4.9 | 321.86 |
| 14:27:12 | 2489 | 4.9 | 321.94 |
| 14:27:13 | 2488 | 4.9 | 322.02 |
| 14:27:14 | 2489 | 4.9 | 322.11 |
| 14:27:15 | 2488 | 4.9 | 322.19 |
| 14:27:16 | 2488 | 4.9 | 322.27 |
| 14:27:17 | 2488 | 4.9 | 322.35 |
| 14:27:18 | 2488 | 4.9 | 322.43 |
| 14:27:19 | 2489 | 4.9 | 322.51 |
| 14:27:20 | 2488 | 4.9 | 322.60 |
| 14:27:21 | 2490 | 4.9 | 322.68 |
| 14:27:22 | 2489 | 4.9 | 322.76 |
| 14:27:23 | 2489 | 4.9 | 322.84 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:27:24 | 2490 | 4.9 | 322.92 |
| 14:27:25 | 2489 | 4.9 | 323.00 |
| 14:27:26 | 2491 | 4.9 | 323.09 |
| 14:27:27 | 2490 | 4.9 | 323.17 |
| 14:27:28 | 2492 | 4.9 | 323.25 |
| 14:27:29 | 2491 | 4.9 | 323.33 |
| 14:27:30 | 2491 | 4.9 | 323.41 |
| 14:27:31 | 2492 | 4.9 | 323.50 |
| 14:27:32 | 2491 | 4.9 | 323.58 |
| 14:27:33 | 2493 | 4.9 | 323.66 |
| 14:27:34 | 2491 | 4.9 | 323.74 |
| 14:27:35 | 2493 | 4.9 | 323.82 |
| 14:27:36 | 2492 | 4.9 | 323.90 |
| 14:27:37 | 2492 | 4.9 | 323.99 |
| 14:27:38 | 2492 | 4.9 | 324.07 |
| 14:27:39 | 2491 | 4.9 | 324.15 |
| 14:27:40 | 2492 | 4.9 | 324.23 |
| 14:27:41 | 2491 | 4.9 | 324.31 |
| 14:27:42 | 2491 | 4.9 | 324.39 |
| 14:27:43 | 2491 | 4.9 | 324.48 |
| 14:27:44 | 2490 | 4.9 | 324.56 |
| 14:27:45 | 2491 | 4.9 | 324.64 |
| 14:27:46 | 2489 | 4.9 | 324.72 |
| 14:27:47 | 2490 | 4.9 | 324.80 |
| 14:27:48 | 2489 | 4.9 | 324.88 |
| 14:27:49 | 2490 | 4.9 | 324.97 |
| 14:27:50 | 2491 | 4.9 | 325.05 |
| 14:27:51 | 2490 | 4.9 | 325.13 |
| 14:27:52 | 2492 | 4.9 | 325.21 |
| 14:27:53 | 2491 | 4.9 | 325.29 |
| 14:27:54 | 2493 | 4.9 | 325.38 |
| 14:27:55 | 2492 | 4.9 | 325.46 |
| 14:27:56 | 2493 | 4.9 | 325.54 |
| 14:27:57 | 2493 | 4.9 | 325.62 |
| 14:27:58 | 2493 | 4.9 | 325.70 |
| 14:27:59 | 2495 | 4.9 | 325.78 |
| 14:28:00 | 2493 | 4.9 | 325.87 |
| 14:28:01 | 2494 | 4.9 | 325.95 |
| 14:28:02 | 2493 | 4.9 | 326.03 |
| 14:28:03 | 2493 | 4.9 | 326.11 |
| 14:28:04 | 2494 | 4.9 | 326.19 |
| 14:28:05 | 2492 | 4.9 | 326.28 |
| 14:28:06 | 2493 | 4.9 | 326.36 |
| 14:28:07 | 2492 | 4.9 | 326.44 |
| 14:28:08 | 2493 | 4.9 | 326.52 |
| 14:28:09 | 2492 | 4.9 | 326.60 |
| 14:28:10 | 2492 | 4.9 | 326.68 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:28:11 | 2492 | 4.9 | 326.77 |
| 14:28:12 | 2491 | 4.9 | 326.85 |
| 14:28:13 | 2492 | 4.9 | 326.93 |
| 14:28:14 | 2491 | 4.9 | 327.01 |
| 14:28:15 | 2492 | 4.9 | 327.09 |
| 14:28:16 | 2492 | 4.9 | 327.17 |
| 14:28:17 | 2492 | 4.9 | 327.26 |
| 14:28:18 | 2493 | 4.9 | 327.34 |
| 14:28:19 | 2492 | 4.9 | 327.42 |
| 14:28:20 | 2493 | 4.9 | 327.50 |
| 14:28:21 | 2493 | 4.9 | 327.58 |
| 14:28:22 | 2493 | 4.9 | 327.66 |
| 14:28:23 | 2493 | 4.9 | 327.75 |
| 14:28:24 | 2492 | 4.9 | 327.83 |
| 14:28:25 | 2494 | 4.9 | 327.91 |
| 14:28:26 | 2493 | 4.9 | 327.99 |
| 14:28:27 | 2494 | 4.9 | 328.07 |
| 14:28:28 | 2493 | 4.9 | 328.16 |
| 14:28:29 | 2493 | 4.9 | 328.24 |
| 14:28:30 | 2493 | 4.9 | 328.32 |
| 14:28:31 | 2492 | 4.9 | 328.40 |
| 14:28:32 | 2493 | 4.9 | 328.48 |
| 14:28:33 | 2491 | 4.9 | 328.56 |
| 14:28:34 | 2493 | 4.9 | 328.65 |
| 14:28:35 | 2492 | 4.9 | 328.73 |
| 14:28:36 | 2492 | 4.9 | 328.81 |
| 14:28:37 | 2492 | 4.9 | 328.89 |
| 14:28:38 | 2491 | 4.9 | 328.97 |
| 14:28:39 | 2492 | 4.9 | 329.05 |
| 14:28:40 | 2491 | 4.9 | 329.14 |
| 14:28:41 | 2493 | 4.9 | 329.22 |
| 14:28:42 | 2492 | 4.9 | 329.30 |
| 14:28:43 | 2492 | 4.9 | 329.38 |
| 14:28:44 | 2493 | 4.9 | 329.46 |
| 14:28:45 | 2492 | 4.9 | 329.55 |
| 14:28:46 | 2494 | 4.9 | 329.63 |
| 14:28:47 | 2492 | 4.9 | 329.71 |
| 14:28:48 | 2493 | 4.9 | 329.79 |
| 14:28:49 | 2493 | 4.9 | 329.87 |
| 14:28:50 | 2493 | 4.9 | 329.95 |
| 14:28:51 | 2494 | 4.9 | 330.04 |
| 14:28:52 | 2493 | 4.9 | 330.12 |
| 14:28:53 | 2493 | 4.9 | 330.20 |
| 14:28:54 | 2492 | 4.9 | 330.28 |
| 14:28:55 | 2492 | 4.9 | 330.36 |
| 14:28:56 | 2493 | 4.9 | 330.44 |
| 14:28:57 | 2492 | 4.9 | 330.53 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:28:58 | 2493 | 4.9 | 330.61 |
| 14:28:59 | 2492 | 4.9 | 330.69 |
| 14:29:00 | 2418 | 2.9 | 330.74 |
| 14:29:01 | 2289 | 0.1 | 330.74 |
| 14:29:02 | 2213 | 0.1 | 330.74 |
| 14:29:03 | 2234 | 0.1 | 330.74 |
| 14:29:04 | 2344 | 0.1 | 330.74 |
| 14:29:05 | 2381 | 0.0 | 330.74 |
| 14:29:06 | 2349 | 0.0 | 330.74 |
| 14:29:07 | 2273 | 0.0 | 330.74 |
| 14:29:08 | 2244 | 0.0 | 330.75 |
| 14:29:09 | 2264 | 0.0 | 330.75 |
| 14:29:10 | 2303 | 0.0 | 330.75 |
| 14:29:11 | 2309 | 0.0 | 330.75 |
| 14:29:12 | 2289 | 0.0 | 330.75 |
| 14:29:13 | 2265 | 0.0 | 330.75 |
| 14:29:14 | 2259 | 0.0 | 330.75 |
| 14:29:15 | 2264 | 0.0 | 330.75 |
| 14:29:16 | 2272 | 0.0 | 330.75 |
| 14:29:17 | 2274 | 0.0 | 330.75 |
| 14:29:18 | 2268 | 0.0 | 330.75 |
| 14:29:19 | 2258 | 0.0 | 330.75 |
| 14:29:20 | 2257 | 0.0 | 330.75 |
| 14:29:21 | 2261 | 0.0 | 330.75 |
| 14:29:22 | 2263 | 0.0 | 330.75 |
| 14:29:23 | 2260 | 0.0 | 330.75 |
| 14:29:24 | 2254 | 0.0 | 330.75 |
| 14:29:25 | 2249 | 0.0 | 330.75 |
| 14:29:26 | 2249 | 0.0 | 330.75 |
| 14:29:27 | 2250 | 0.0 | 330.75 |
| 14:29:28 | 2250 | 0.0 | 330.75 |
| 14:29:29 | 2246 | 0.0 | 330.75 |
| 14:29:30 | 2241 | 0.0 | 330.75 |
| 14:29:31 | 2238 | 0.0 | 330.75 |
| 14:29:32 | 2238 | 0.0 | 330.75 |
| 14:29:33 | 2238 | 0.0 | 330.75 |
| 14:29:34 | 2237 | 0.0 | 330.75 |
| 14:29:35 | 2233 | 0.0 | 330.75 |
| 14:29:36 | 2230 | 0.0 | 330.75 |
| 14:29:37 | 2228 | 0.0 | 330.75 |
| 14:29:38 | 2228 | 0.0 | 330.75 |
| 14:29:39 | 2226 | 0.0 | 330.75 |
| 14:29:40 | 2224 | 0.0 | 330.75 |
| 14:29:41 | 2222 | 0.0 | 330.75 |
| 14:29:42 | 2219 | 0.0 | 330.75 |
| 14:29:43 | 2217 | 0.0 | 330.75 |
| 14:29:44 | 2216 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:29:45 | 2215 | 0.0 | 330.75 |
| 14:29:46 | 2212 | 0.0 | 330.75 |
| 14:29:47 | 2210 | 0.0 | 330.75 |
| 14:29:48 | 2208 | 0.0 | 330.75 |
| 14:29:49 | 2207 | 0.0 | 330.75 |
| 14:29:50 | 2205 | 0.0 | 330.75 |
| 14:29:51 | 2204 | 0.0 | 330.75 |
| 14:29:52 | 2201 | 0.0 | 330.75 |
| 14:29:53 | 2199 | 0.0 | 330.75 |
| 14:29:54 | 2198 | 0.0 | 330.75 |
| 14:29:55 | 2196 | 0.0 | 330.75 |
| 14:29:56 | 2195 | 0.0 | 330.75 |
| 14:29:57 | 2193 | 0.0 | 330.75 |
| 14:29:58 | 2191 | 0.0 | 330.75 |
| 14:29:59 | 2189 | 0.0 | 330.75 |
| 14:30:00 | 2187 | 0.0 | 330.75 |
| 14:30:01 | 2186 | 0.0 | 330.75 |
| 14:30:02 | 2185 | 0.0 | 330.75 |
| 14:30:03 | 2183 | 0.0 | 330.75 |
| 14:30:04 | 2181 | 0.0 | 330.75 |
| 14:30:05 | 2179 | 0.0 | 330.75 |
| 14:30:06 | 2178 | 0.0 | 330.75 |
| 14:30:07 | 2176 | 0.0 | 330.75 |
| 14:30:08 | 2175 | 0.0 | 330.75 |
| 14:30:09 | 2173 | 0.0 | 330.75 |
| 14:30:10 | 2171 | 0.0 | 330.75 |
| 14:30:11 | 2170 | 0.0 | 330.75 |
| 14:30:12 | 2169 | 0.0 | 330.75 |
| 14:30:13 | 2167 | 0.0 | 330.75 |
| 14:30:14 | 2165 | 0.0 | 330.75 |
| 14:30:15 | 2164 | 0.0 | 330.75 |
| 14:30:16 | 2162 | 0.0 | 330.75 |
| 14:30:17 | 2161 | 0.0 | 330.75 |
| 14:30:18 | 2159 | 0.0 | 330.75 |
| 14:30:19 | 2157 | 0.0 | 330.75 |
| 14:30:20 | 2156 | 0.0 | 330.75 |
| 14:30:21 | 2155 | 0.0 | 330.75 |
| 14:30:22 | 2153 | 0.0 | 330.75 |
| 14:30:23 | 2152 | 0.0 | 330.75 |
| 14:30:24 | 2150 | 0.0 | 330.75 |
| 14:30:25 | 2149 | 0.0 | 330.75 |
| 14:30:26 | 2147 | 0.0 | 330.75 |
| 14:30:27 | 2146 | 0.0 | 330.75 |
| 14:30:28 | 2144 | 0.0 | 330.75 |
| 14:30:29 | 2143 | 0.0 | 330.75 |
| 14:30:30 | 2141 | 0.0 | 330.75 |
| 14:30:31 | 2140 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:30:32 | 2139 | 0.0 | 330.75 |
| 14:30:33 | 2137 | 0.0 | 330.75 |
| 14:30:34 | 2136 | 0.0 | 330.75 |
| 14:30:35 | 2134 | 0.0 | 330.75 |
| 14:30:36 | 2133 | 0.0 | 330.75 |
| 14:30:37 | 2132 | 0.0 | 330.75 |
| 14:30:38 | 2130 | 0.0 | 330.75 |
| 14:30:39 | 2128 | 0.0 | 330.75 |
| 14:30:40 | 2128 | 0.0 | 330.75 |
| 14:30:41 | 2126 | 0.0 | 330.75 |
| 14:30:42 | 2124 | 0.0 | 330.75 |
| 14:30:43 | 2124 | 0.0 | 330.75 |
| 14:30:44 | 2122 | 0.0 | 330.75 |
| 14:30:45 | 2121 | 0.0 | 330.75 |
| 14:30:46 | 2120 | 0.0 | 330.75 |
| 14:30:47 | 2118 | 0.0 | 330.75 |
| 14:30:48 | 2117 | 0.0 | 330.75 |
| 14:30:49 | 2115 | 0.0 | 330.75 |
| 14:30:50 | 2114 | 0.0 | 330.75 |
| 14:30:51 | 2113 | 0.0 | 330.75 |
| 14:30:52 | 2111 | 0.0 | 330.75 |
| 14:30:53 | 2110 | 0.0 | 330.75 |
| 14:30:54 | 2109 | 0.0 | 330.75 |
| 14:30:55 | 2107 | 0.0 | 330.75 |
| 14:30:56 | 2106 | 0.0 | 330.75 |
| 14:30:57 | 2105 | 0.0 | 330.75 |
| 14:30:58 | 2104 | 0.0 | 330.75 |
| 14:30:59 | 2102 | 0.0 | 330.75 |
| 14:31:00 | 2101 | 0.0 | 330.75 |
| 14:31:01 | 2100 | 0.0 | 330.75 |
| 14:31:02 | 2098 | 0.0 | 330.75 |
| 14:31:03 | 2097 | 0.0 | 330.75 |
| 14:31:04 | 2096 | 0.0 | 330.75 |
| 14:31:05 | 2095 | 0.0 | 330.75 |
| 14:31:06 | 2093 | 0.0 | 330.75 |
| 14:31:07 | 2092 | 0.0 | 330.75 |
| 14:31:08 | 2090 | 0.0 | 330.75 |
| 14:31:09 | 2089 | 0.0 | 330.75 |
| 14:31:10 | 2088 | 0.0 | 330.75 |
| 14:31:11 | 2087 | 0.0 | 330.75 |
| 14:31:12 | 2085 | 0.0 | 330.75 |
| 14:31:13 | 2084 | 0.0 | 330.75 |
| 14:31:14 | 2083 | 0.0 | 330.75 |
| 14:31:15 | 2082 | 0.0 | 330.75 |
| 14:31:16 | 2081 | 0.0 | 330.75 |
| 14:31:17 | 2079 | 0.0 | 330.75 |
| 14:31:18 | 2078 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:31:19 | 2077 | 0.0 | 330.75 |
| 14:31:20 | 2076 | 0.0 | 330.75 |
| 14:31:21 | 2074 | 0.0 | 330.75 |
| 14:31:22 | 2073 | 0.0 | 330.75 |
| 14:31:23 | 2072 | 0.0 | 330.75 |
| 14:31:24 | 2071 | 0.0 | 330.75 |
| 14:31:25 | 2070 | 0.0 | 330.75 |
| 14:31:26 | 2069 | 0.0 | 330.75 |
| 14:31:27 | 2067 | 0.0 | 330.75 |
| 14:31:28 | 2066 | 0.0 | 330.75 |
| 14:31:29 | 2065 | 0.0 | 330.75 |
| 14:31:30 | 2063 | 0.0 | 330.75 |
| 14:31:31 | 2062 | 0.0 | 330.75 |
| 14:31:32 | 2061 | 0.0 | 330.75 |
| 14:31:33 | 2060 | 0.0 | 330.75 |
| 14:31:34 | 2059 | 0.0 | 330.75 |
| 14:31:35 | 2058 | 0.0 | 330.75 |
| 14:31:36 | 2057 | 0.0 | 330.75 |
| 14:31:37 | 2055 | 0.0 | 330.75 |
| 14:31:38 | 2054 | 0.0 | 330.75 |
| 14:31:39 | 2053 | 0.0 | 330.75 |
| 14:31:40 | 2052 | 0.0 | 330.75 |
| 14:31:41 | 2051 | 0.0 | 330.75 |
| 14:31:42 | 2049 | 0.0 | 330.75 |
| 14:31:43 | 2048 | 0.0 | 330.75 |
| 14:31:44 | 2047 | 0.0 | 330.75 |
| 14:31:45 | 2046 | 0.0 | 330.75 |
| 14:31:46 | 2045 | 0.0 | 330.75 |
| 14:31:47 | 2044 | 0.0 | 330.75 |
| 14:31:48 | 2042 | 0.0 | 330.75 |
| 14:31:49 | 2041 | 0.0 | 330.75 |
| 14:31:50 | 2040 | 0.0 | 330.75 |
| 14:31:51 | 2039 | 0.0 | 330.75 |
| 14:31:52 | 2038 | 0.0 | 330.75 |
| 14:31:53 | 2037 | 0.0 | 330.75 |
| 14:31:54 | 2036 | 0.0 | 330.75 |
| 14:31:55 | 2035 | 0.0 | 330.75 |
| 14:31:56 | 2033 | 0.0 | 330.75 |
| 14:31:57 | 2032 | 0.0 | 330.75 |
| 14:31:58 | 2031 | 0.0 | 330.75 |
| 14:31:59 | 2030 | 0.0 | 330.75 |
| 14:32:00 | 2029 | 0.0 | 330.75 |
| 14:32:01 | 2028 | 0.0 | 330.75 |
| 14:32:02 | 2027 | 0.0 | 330.75 |
| 14:32:03 | 2026 | 0.0 | 330.75 |
| 14:32:04 | 2025 | 0.0 | 330.75 |
| 14:32:05 | 2023 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:32:06 | 2022 | 0.0 | 330.75 |
| 14:32:07 | 2021 | 0.0 | 330.75 |
| 14:32:08 | 2020 | 0.0 | 330.75 |
| 14:32:09 | 2019 | 0.0 | 330.75 |
| 14:32:10 | 2018 | 0.0 | 330.75 |
| 14:32:11 | 2017 | 0.0 | 330.75 |
| 14:32:12 | 2016 | 0.0 | 330.75 |
| 14:32:13 | 2015 | 0.0 | 330.75 |
| 14:32:14 | 2014 | 0.0 | 330.75 |
| 14:32:15 | 2013 | 0.0 | 330.75 |
| 14:32:16 | 2012 | 0.0 | 330.75 |
| 14:32:17 | 2011 | 0.0 | 330.75 |
| 14:32:18 | 2010 | 0.0 | 330.75 |
| 14:32:19 | 2009 | 0.0 | 330.75 |
| 14:32:20 | 2008 | 0.0 | 330.75 |
| 14:32:21 | 2007 | 0.0 | 330.75 |
| 14:32:22 | 2006 | 0.0 | 330.75 |
| 14:32:23 | 2005 | 0.0 | 330.75 |
| 14:32:24 | 2004 | 0.0 | 330.75 |
| 14:32:25 | 2002 | 0.0 | 330.75 |
| 14:32:26 | 2001 | 0.0 | 330.75 |
| 14:32:27 | 2000 | 0.0 | 330.75 |
| 14:32:28 | 1999 | 0.0 | 330.75 |
| 14:32:29 | 1998 | 0.0 | 330.75 |
| 14:32:30 | 1997 | 0.0 | 330.75 |
| 14:32:31 | 1996 | 0.0 | 330.75 |
| 14:32:32 | 1995 | 0.0 | 330.75 |
| 14:32:33 | 1994 | 0.0 | 330.75 |
| 14:32:34 | 1993 | 0.0 | 330.75 |
| 14:32:35 | 1992 | 0.0 | 330.75 |
| 14:32:36 | 1991 | 0.0 | 330.75 |
| 14:32:37 | 1990 | 0.0 | 330.75 |
| 14:32:38 | 1990 | 0.0 | 330.75 |
| 14:32:39 | 1989 | 0.0 | 330.75 |
| 14:32:40 | 1988 | 0.0 | 330.75 |
| 14:32:41 | 1987 | 0.0 | 330.75 |
| 14:32:42 | 1986 | 0.0 | 330.75 |
| 14:32:43 | 1985 | 0.0 | 330.75 |
| 14:32:44 | 1984 | 0.0 | 330.75 |
| 14:32:45 | 1983 | 0.0 | 330.75 |
| 14:32:46 | 1981 | 0.0 | 330.75 |
| 14:32:47 | 1980 | 0.0 | 330.75 |
| 14:32:48 | 1979 | 0.0 | 330.75 |
| 14:32:49 | 1978 | 0.0 | 330.75 |
| 14:32:50 | 1977 | 0.0 | 330.75 |
| 14:32:51 | 1976 | 0.0 | 330.75 |
| 14:32:52 | 1976 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:32:53 | 1975 | 0.0 | 330.75 |
| 14:32:54 | 1974 | 0.0 | 330.75 |
| 14:32:55 | 1973 | 0.0 | 330.75 |
| 14:32:56 | 1972 | 0.0 | 330.75 |
| 14:32:57 | 1971 | 0.0 | 330.75 |
| 14:32:58 | 1970 | 0.0 | 330.75 |
| 14:32:59 | 1969 | 0.0 | 330.75 |
| 14:33:00 | 1968 | 0.0 | 330.75 |
| 14:33:01 | 1967 | 0.0 | 330.75 |
| 14:33:02 | 1966 | 0.0 | 330.75 |
| 14:33:03 | 1965 | 0.0 | 330.75 |
| 14:33:04 | 1964 | 0.0 | 330.75 |
| 14:33:05 | 1963 | 0.0 | 330.75 |
| 14:33:06 | 1962 | 0.0 | 330.75 |
| 14:33:07 | 1961 | 0.0 | 330.75 |
| 14:33:08 | 1960 | 0.0 | 330.75 |
| 14:33:09 | 1959 | 0.0 | 330.75 |
| 14:33:10 | 1958 | 0.0 | 330.75 |
| 14:33:11 | 1957 | 0.0 | 330.75 |
| 14:33:12 | 1956 | 0.0 | 330.75 |
| 14:33:13 | 1955 | 0.0 | 330.75 |
| 14:33:14 | 1954 | 0.0 | 330.75 |
| 14:33:15 | 1953 | 0.0 | 330.75 |
| 14:33:16 | 1953 | 0.0 | 330.75 |
| 14:33:17 | 1952 | 0.0 | 330.75 |
| 14:33:18 | 1951 | 0.0 | 330.75 |
| 14:33:19 | 1950 | 0.0 | 330.75 |
| 14:33:20 | 1949 | 0.0 | 330.75 |
| 14:33:21 | 1948 | 0.0 | 330.75 |
| 14:33:22 | 1947 | 0.0 | 330.75 |
| 14:33:23 | 1946 | 0.0 | 330.75 |
| 14:33:24 | 1945 | 0.0 | 330.75 |
| 14:33:25 | 1944 | 0.0 | 330.75 |
| 14:33:26 | 1943 | 0.0 | 330.75 |
| 14:33:27 | 1942 | 0.0 | 330.75 |
| 14:33:28 | 1941 | 0.0 | 330.75 |
| 14:33:29 | 1940 | 0.0 | 330.75 |
| 14:33:30 | 1939 | 0.0 | 330.75 |
| 14:33:31 | 1938 | 0.0 | 330.75 |
| 14:33:32 | 1937 | 0.0 | 330.75 |
| 14:33:33 | 1937 | 0.0 | 330.75 |
| 14:33:34 | 1936 | 0.0 | 330.75 |
| 14:33:35 | 1935 | 0.0 | 330.75 |
| 14:33:36 | 1934 | 0.0 | 330.75 |
| 14:33:37 | 1933 | 0.0 | 330.75 |
| 14:33:38 | 1932 | 0.0 | 330.75 |
| 14:33:39 | 1931 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:33:40 | 1930 | 0.0 | 330.75 |
| 14:33:41 | 1929 | 0.0 | 330.75 |
| 14:33:42 | 1928 | 0.0 | 330.75 |
| 14:33:43 | 1928 | 0.0 | 330.75 |
| 14:33:44 | 1926 | 0.0 | 330.75 |
| 14:33:45 | 1925 | 0.0 | 330.75 |
| 14:33:46 | 1925 | 0.0 | 330.75 |
| 14:33:47 | 1924 | 0.0 | 330.75 |
| 14:33:48 | 1923 | 0.0 | 330.75 |
| 14:33:49 | 1922 | 0.0 | 330.75 |
| 14:33:50 | 1921 | 0.0 | 330.75 |
| 14:33:51 | 1920 | 0.0 | 330.75 |
| 14:33:52 | 1919 | 0.0 | 330.75 |
| 14:33:53 | 1918 | 0.0 | 330.75 |
| 14:33:54 | 1917 | 0.0 | 330.75 |
| 14:33:55 | 1917 | 0.0 | 330.75 |
| 14:33:56 | 1916 | 0.0 | 330.75 |
| 14:33:57 | 1915 | 0.0 | 330.75 |
| 14:33:58 | 1914 | 0.0 | 330.75 |
| 14:33:59 | 1913 | 0.0 | 330.75 |
| 14:34:00 | 1912 | 0.0 | 330.75 |
| 14:34:01 | 1911 | 0.0 | 330.75 |
| 14:34:02 | 1910 | 0.0 | 330.75 |
| 14:34:03 | 1909 | 0.0 | 330.75 |
| 14:34:04 | 1909 | 0.0 | 330.75 |
| 14:34:05 | 1907 | 0.0 | 330.75 |
| 14:34:06 | 1907 | 0.0 | 330.75 |
| 14:34:07 | 1906 | 0.0 | 330.75 |
| 14:34:08 | 1905 | 0.0 | 330.75 |
| 14:34:09 | 1904 | 0.0 | 330.75 |
| 14:34:10 | 1903 | 0.0 | 330.75 |
| 14:34:11 | 1902 | 0.0 | 330.75 |
| 14:34:12 | 1901 | 0.0 | 330.75 |
| 14:34:13 | 1901 | 0.0 | 330.75 |
| 14:34:14 | 1900 | 0.0 | 330.75 |
| 14:34:15 | 1899 | 0.0 | 330.75 |
| 14:34:16 | 1898 | 0.0 | 330.75 |
| 14:34:17 | 1897 | 0.0 | 330.75 |
| 14:34:18 | 1896 | 0.0 | 330.75 |
| 14:34:19 | 1895 | 0.0 | 330.75 |
| 14:34:20 | 1895 | 0.0 | 330.75 |
| 14:34:21 | 1894 | 0.0 | 330.75 |
| 14:34:22 | 1893 | 0.0 | 330.75 |
| 14:34:23 | 1892 | 0.0 | 330.75 |
| 14:34:24 | 1891 | 0.0 | 330.75 |
| 14:34:25 | 1890 | 0.0 | 330.75 |
| 14:34:26 | 1889 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:34:27 | 1889 | 0.0 | 330.75 |
| 14:34:28 | 1888 | 0.0 | 330.75 |
| 14:34:29 | 1887 | 0.0 | 330.75 |
| 14:34:30 | 1886 | 0.0 | 330.75 |
| 14:34:31 | 1885 | 0.0 | 330.75 |
| 14:34:32 | 1884 | 0.0 | 330.75 |
| 14:34:33 | 1883 | 0.0 | 330.75 |
| 14:34:34 | 1882 | 0.0 | 330.75 |
| 14:34:35 | 1882 | 0.0 | 330.75 |
| 14:34:36 | 1881 | 0.0 | 330.75 |
| 14:34:37 | 1880 | 0.0 | 330.75 |
| 14:34:38 | 1879 | 0.0 | 330.75 |
| 14:34:39 | 1878 | 0.0 | 330.75 |
| 14:34:40 | 1877 | 0.0 | 330.75 |
| 14:34:41 | 1877 | 0.0 | 330.75 |
| 14:34:42 | 1876 | 0.0 | 330.75 |
| 14:34:43 | 1875 | 0.0 | 330.75 |
| 14:34:44 | 1874 | 0.0 | 330.75 |
| 14:34:45 | 1873 | 0.0 | 330.75 |
| 14:34:46 | 1872 | 0.0 | 330.75 |
| 14:34:47 | 1872 | 0.0 | 330.75 |
| 14:34:48 | 1871 | 0.0 | 330.75 |
| 14:34:49 | 1870 | 0.0 | 330.75 |
| 14:34:50 | 1869 | 0.0 | 330.75 |
| 14:34:51 | 1868 | 0.0 | 330.75 |
| 14:34:52 | 1867 | 0.0 | 330.75 |
| 14:34:53 | 1867 | 0.0 | 330.75 |
| 14:34:54 | 1866 | 0.0 | 330.75 |
| 14:34:55 | 1865 | 0.0 | 330.75 |
| 14:34:56 | 1864 | 0.0 | 330.75 |
| 14:34:57 | 1863 | 0.0 | 330.75 |
| 14:34:58 | 1862 | 0.0 | 330.75 |
| 14:34:59 | 1862 | 0.0 | 330.75 |
| 14:35:00 | 1861 | 0.0 | 330.75 |
| 14:35:01 | 1860 | 0.0 | 330.75 |
| 14:35:02 | 1859 | 0.0 | 330.75 |
| 14:35:03 | 1858 | 0.0 | 330.75 |
| 14:35:04 | 1858 | 0.0 | 330.75 |
| 14:35:05 | 1857 | 0.0 | 330.75 |
| 14:35:06 | 1856 | 0.0 | 330.75 |
| 14:35:07 | 1855 | 0.0 | 330.75 |
| 14:35:08 | 1854 | 0.0 | 330.75 |
| 14:35:09 | 1853 | 0.0 | 330.75 |
| 14:35:10 | 1852 | 0.0 | 330.75 |
| 14:35:11 | 1852 | 0.0 | 330.75 |
| 14:35:12 | 1851 | 0.0 | 330.75 |
| 14:35:13 | 1850 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:35:14 | 1849 | 0.0 | 330.75 |
| 14:35:15 | 1848 | 0.0 | 330.75 |
| 14:35:16 | 1848 | 0.0 | 330.75 |
| 14:35:17 | 1847 | 0.0 | 330.75 |
| 14:35:18 | 1846 | 0.0 | 330.75 |
| 14:35:19 | 1845 | 0.0 | 330.75 |
| 14:35:20 | 1844 | 0.0 | 330.75 |
| 14:35:21 | 1843 | 0.0 | 330.75 |
| 14:35:22 | 1843 | 0.0 | 330.75 |
| 14:35:23 | 1842 | 0.0 | 330.75 |
| 14:35:24 | 1841 | 0.0 | 330.75 |
| 14:35:25 | 1840 | 0.0 | 330.75 |
| 14:35:26 | 1839 | 0.0 | 330.75 |
| 14:35:27 | 1839 | 0.0 | 330.75 |
| 14:35:28 | 1838 | 0.0 | 330.75 |
| 14:35:29 | 1837 | 0.0 | 330.75 |
| 14:35:30 | 1836 | 0.0 | 330.75 |
| 14:35:31 | 1835 | 0.0 | 330.75 |
| 14:35:32 | 1834 | 0.0 | 330.75 |
| 14:35:33 | 1834 | 0.0 | 330.75 |
| 14:35:34 | 1833 | 0.0 | 330.75 |
| 14:35:35 | 1832 | 0.0 | 330.75 |
| 14:35:36 | 1831 | 0.0 | 330.75 |
| 14:35:37 | 1830 | 0.0 | 330.75 |
| 14:35:38 | 1829 | 0.0 | 330.75 |
| 14:35:39 | 1829 | 0.0 | 330.75 |
| 14:35:40 | 1828 | 0.0 | 330.75 |
| 14:35:41 | 1827 | 0.0 | 330.75 |
| 14:35:42 | 1826 | 0.0 | 330.75 |
| 14:35:43 | 1826 | 0.0 | 330.75 |
| 14:35:44 | 1825 | 0.0 | 330.75 |
| 14:35:45 | 1824 | 0.0 | 330.75 |
| 14:35:46 | 1823 | 0.0 | 330.75 |
| 14:35:47 | 1822 | 0.0 | 330.75 |
| 14:35:48 | 1822 | 0.0 | 330.75 |
| 14:35:49 | 1821 | 0.0 | 330.75 |
| 14:35:50 | 1820 | 0.0 | 330.75 |
| 14:35:51 | 1819 | 0.0 | 330.75 |
| 14:35:52 | 1818 | 0.0 | 330.75 |
| 14:35:53 | 1817 | 0.0 | 330.75 |
| 14:35:54 | 1817 | 0.0 | 330.75 |
| 14:35:55 | 1816 | 0.0 | 330.75 |
| 14:35:56 | 1815 | 0.0 | 330.75 |
| 14:35:57 | 1814 | 0.0 | 330.75 |
| 14:35:58 | 1813 | 0.0 | 330.75 |
| 14:35:59 | 1813 | 0.0 | 330.75 |
| 14:36:00 | 1812 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:36:01 | 1811 | 0.0 | 330.75 |
| 14:36:02 | 1810 | 0.0 | 330.75 |
| 14:36:03 | 1809 | 0.0 | 330.75 |
| 14:36:04 | 1809 | 0.0 | 330.75 |
| 14:36:05 | 1808 | 0.0 | 330.75 |
| 14:36:06 | 1807 | 0.0 | 330.75 |
| 14:36:07 | 1806 | 0.0 | 330.75 |
| 14:36:08 | 1805 | 0.0 | 330.75 |
| 14:36:09 | 1805 | 0.0 | 330.75 |
| 14:36:10 | 1804 | 0.0 | 330.75 |
| 14:36:11 | 1803 | 0.0 | 330.75 |
| 14:36:12 | 1802 | 0.0 | 330.75 |
| 14:36:13 | 1801 | 0.0 | 330.75 |
| 14:36:14 | 1800 | 0.0 | 330.75 |
| 14:36:15 | 1799 | 0.0 | 330.75 |
| 14:36:16 | 1799 | 0.0 | 330.75 |
| 14:36:17 | 1798 | 0.0 | 330.75 |
| 14:36:18 | 1797 | 0.0 | 330.75 |
| 14:36:19 | 1796 | 0.0 | 330.75 |
| 14:36:20 | 1796 | 0.0 | 330.75 |
| 14:36:21 | 1795 | 0.0 | 330.75 |
| 14:36:22 | 1794 | 0.0 | 330.75 |
| 14:36:23 | 1793 | 0.0 | 330.75 |
| 14:36:24 | 1793 | 0.0 | 330.75 |
| 14:36:25 | 1792 | 0.0 | 330.75 |
| 14:36:26 | 1791 | 0.0 | 330.75 |
| 14:36:27 | 1790 | 0.0 | 330.75 |
| 14:36:28 | 1790 | 0.0 | 330.75 |
| 14:36:29 | 1789 | 0.0 | 330.75 |
| 14:36:30 | 1788 | 0.0 | 330.75 |
| 14:36:31 | 1787 | 0.0 | 330.75 |
| 14:36:32 | 1786 | 0.0 | 330.75 |
| 14:36:33 | 1786 | 0.0 | 330.75 |
| 14:36:34 | 1785 | 0.0 | 330.75 |
| 14:36:35 | 1784 | 0.0 | 330.75 |
| 14:36:36 | 1783 | 0.0 | 330.75 |
| 14:36:37 | 1782 | 0.0 | 330.75 |
| 14:36:38 | 1782 | 0.0 | 330.75 |
| 14:36:39 | 1781 | 0.0 | 330.75 |
| 14:36:40 | 1780 | 0.0 | 330.75 |
| 14:36:41 | 1779 | 0.0 | 330.75 |
| 14:36:42 | 1779 | 0.0 | 330.75 |
| 14:36:43 | 1778 | 0.0 | 330.75 |
| 14:36:44 | 1777 | 0.0 | 330.75 |
| 14:36:45 | 1776 | 0.0 | 330.75 |
| 14:36:46 | 1776 | 0.0 | 330.75 |
| 14:36:47 | 1775 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:36:48 | 1774 | 0.0 | 330.75 |
| 14:36:49 | 1773 | 0.0 | 330.75 |
| 14:36:50 | 1773 | 0.0 | 330.75 |
| 14:36:51 | 1772 | 0.0 | 330.75 |
| 14:36:52 | 1771 | 0.0 | 330.75 |
| 14:36:53 | 1770 | 0.0 | 330.75 |
| 14:36:54 | 1769 | 0.0 | 330.75 |
| 14:36:55 | 1769 | 0.0 | 330.75 |
| 14:36:56 | 1768 | 0.0 | 330.75 |
| 14:36:57 | 1767 | 0.0 | 330.75 |
| 14:36:58 | 1766 | 0.0 | 330.75 |
| 14:36:59 | 1765 | 0.0 | 330.75 |
| 14:37:00 | 1765 | 0.0 | 330.75 |
| 14:37:01 | 1764 | 0.0 | 330.75 |
| 14:37:02 | 1763 | 0.0 | 330.75 |
| 14:37:03 | 1763 | 0.0 | 330.75 |
| 14:37:04 | 1762 | 0.0 | 330.75 |
| 14:37:05 | 1761 | 0.0 | 330.75 |
| 14:37:06 | 1760 | 0.0 | 330.75 |
| 14:37:07 | 1760 | 0.0 | 330.75 |
| 14:37:08 | 1759 | 0.0 | 330.75 |
| 14:37:09 | 1758 | 0.0 | 330.75 |
| 14:37:10 | 1758 | 0.0 | 330.75 |
| 14:37:11 | 1757 | 0.0 | 330.75 |
| 14:37:12 | 1756 | 0.0 | 330.75 |
| 14:37:13 | 1755 | 0.0 | 330.75 |
| 14:37:14 | 1755 | 0.0 | 330.75 |
| 14:37:15 | 1754 | 0.0 | 330.75 |
| 14:37:16 | 1753 | 0.0 | 330.75 |
| 14:37:17 | 1752 | 0.0 | 330.75 |
| 14:37:18 | 1751 | 0.0 | 330.75 |
| 14:37:19 | 1751 | 0.0 | 330.75 |
| 14:37:20 | 1750 | 0.0 | 330.75 |
| 14:37:21 | 1749 | 0.0 | 330.75 |
| 14:37:22 | 1748 | 0.0 | 330.75 |
| 14:37:23 | 1748 | 0.0 | 330.75 |
| 14:37:24 | 1747 | 0.0 | 330.75 |
| 14:37:25 | 1746 | 0.0 | 330.75 |
| 14:37:26 | 1746 | 0.0 | 330.75 |
| 14:37:27 | 1745 | 0.0 | 330.75 |
| 14:37:28 | 1744 | 0.0 | 330.75 |
| 14:37:29 | 1743 | 0.0 | 330.75 |
| 14:37:30 | 1743 | 0.0 | 330.75 |
| 14:37:31 | 1742 | 0.0 | 330.75 |
| 14:37:32 | 1741 | 0.0 | 330.75 |
| 14:37:33 | 1740 | 0.0 | 330.75 |
| 14:37:34 | 1740 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:37:35 | 1739 | 0.0 | 330.75 |
| 14:37:36 | 1738 | 0.0 | 330.75 |
| 14:37:37 | 1737 | 0.0 | 330.75 |
| 14:37:38 | 1737 | 0.0 | 330.75 |
| 14:37:39 | 1736 | 0.0 | 330.75 |
| 14:37:40 | 1735 | 0.0 | 330.75 |
| 14:37:41 | 1734 | 0.0 | 330.75 |
| 14:37:42 | 1734 | 0.0 | 330.75 |
| 14:37:43 | 1733 | 0.0 | 330.75 |
| 14:37:44 | 1732 | 0.0 | 330.75 |
| 14:37:45 | 1731 | 0.0 | 330.75 |
| 14:37:46 | 1731 | 0.0 | 330.75 |
| 14:37:47 | 1730 | 0.0 | 330.75 |
| 14:37:48 | 1729 | 0.0 | 330.75 |
| 14:37:49 | 1729 | 0.0 | 330.75 |
| 14:37:50 | 1728 | 0.0 | 330.75 |
| 14:37:51 | 1727 | 0.0 | 330.75 |
| 14:37:52 | 1726 | 0.0 | 330.75 |
| 14:37:53 | 1726 | 0.0 | 330.75 |
| 14:37:54 | 1725 | 0.0 | 330.75 |
| 14:37:55 | 1724 | 0.0 | 330.75 |
| 14:37:56 | 1724 | 0.0 | 330.75 |
| 14:37:57 | 1723 | 0.0 | 330.75 |
| 14:37:58 | 1722 | 0.0 | 330.75 |
| 14:37:59 | 1721 | 0.0 | 330.75 |
| 14:38:00 | 1721 | 0.0 | 330.75 |
| 14:38:01 | 1720 | 0.0 | 330.75 |
| 14:38:02 | 1719 | 0.0 | 330.75 |
| 14:38:03 | 1718 | 0.0 | 330.75 |
| 14:38:04 | 1718 | 0.0 | 330.75 |
| 14:38:05 | 1717 | 0.0 | 330.75 |
| 14:38:06 | 1716 | 0.0 | 330.75 |
| 14:38:07 | 1715 | 0.0 | 330.75 |
| 14:38:08 | 1715 | 0.0 | 330.75 |
| 14:38:09 | 1714 | 0.0 | 330.75 |
| 14:38:10 | 1713 | 0.0 | 330.75 |
| 14:38:11 | 1713 | 0.0 | 330.75 |
| 14:38:12 | 1712 | 0.0 | 330.75 |
| 14:38:13 | 1711 | 0.0 | 330.75 |
| 14:38:14 | 1710 | 0.0 | 330.75 |
| 14:38:15 | 1710 | 0.0 | 330.75 |
| 14:38:16 | 1709 | 0.0 | 330.75 |
| 14:38:17 | 1708 | 0.0 | 330.75 |
| 14:38:18 | 1708 | 0.0 | 330.75 |
| 14:38:19 | 1707 | 0.0 | 330.75 |
| 14:38:20 | 1706 | 0.0 | 330.75 |
| 14:38:21 | 1705 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:38:22 | 1705 | 0.0 | 330.75 |
| 14:38:23 | 1704 | 0.0 | 330.75 |
| 14:38:24 | 1703 | 0.0 | 330.75 |
| 14:38:25 | 1703 | 0.0 | 330.75 |
| 14:38:26 | 1702 | 0.0 | 330.75 |
| 14:38:27 | 1701 | 0.0 | 330.75 |
| 14:38:28 | 1700 | 0.0 | 330.75 |
| 14:38:29 | 1700 | 0.0 | 330.75 |
| 14:38:30 | 1699 | 0.0 | 330.75 |
| 14:38:31 | 1698 | 0.0 | 330.75 |
| 14:38:32 | 1698 | 0.0 | 330.75 |
| 14:38:33 | 1697 | 0.0 | 330.75 |
| 14:38:34 | 1696 | 0.0 | 330.75 |
| 14:38:35 | 1696 | 0.0 | 330.75 |
| 14:38:36 | 1695 | 0.0 | 330.75 |
| 14:38:37 | 1694 | 0.0 | 330.75 |
| 14:38:38 | 1694 | 0.0 | 330.75 |
| 14:38:39 | 1693 | 0.0 | 330.75 |
| 14:38:40 | 1692 | 0.0 | 330.75 |
| 14:38:41 | 1691 | 0.0 | 330.75 |
| 14:38:42 | 1691 | 0.0 | 330.75 |
| 14:38:43 | 1690 | 0.0 | 330.75 |
| 14:38:44 | 1689 | 0.0 | 330.75 |
| 14:38:45 | 1689 | 0.0 | 330.75 |
| 14:38:46 | 1688 | 0.0 | 330.75 |
| 14:38:47 | 1687 | 0.0 | 330.75 |
| 14:38:48 | 1686 | 0.0 | 330.75 |
| 14:38:49 | 1686 | 0.0 | 330.75 |
| 14:38:50 | 1685 | 0.0 | 330.75 |
| 14:38:51 | 1684 | 0.0 | 330.75 |
| 14:38:52 | 1684 | 0.0 | 330.75 |
| 14:38:53 | 1683 | 0.0 | 330.75 |
| 14:38:54 | 1682 | 0.0 | 330.75 |
| 14:38:55 | 1682 | 0.0 | 330.75 |
| 14:38:56 | 1681 | 0.0 | 330.75 |
| 14:38:57 | 1680 | 0.0 | 330.75 |
| 14:38:58 | 1679 | 0.0 | 330.75 |
| 14:38:59 | 1679 | 0.0 | 330.75 |
| 14:39:00 | 1678 | 0.0 | 330.75 |
| 14:39:01 | 1677 | 0.0 | 330.75 |
| 14:39:02 | 1677 | 0.0 | 330.75 |
| 14:39:03 | 1676 | 0.0 | 330.75 |
| 14:39:04 | 1675 | 0.0 | 330.75 |
| 14:39:05 | 1675 | 0.0 | 330.75 |
| 14:39:06 | 1674 | 0.0 | 330.75 |
| 14:39:07 | 1673 | 0.0 | 330.75 |
| 14:39:08 | 1673 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:39:09 | 1672 | 0.0 | 330.75 |
| 14:39:10 | 1671 | 0.0 | 330.75 |
| 14:39:11 | 1671 | 0.0 | 330.75 |
| 14:39:12 | 1670 | 0.0 | 330.75 |
| 14:39:13 | 1669 | 0.0 | 330.75 |
| 14:39:14 | 1669 | 0.0 | 330.75 |
| 14:39:15 | 1668 | 0.0 | 330.75 |
| 14:39:16 | 1667 | 0.0 | 330.75 |
| 14:39:17 | 1667 | 0.0 | 330.75 |
| 14:39:18 | 1666 | 0.0 | 330.75 |
| 14:39:19 | 1665 | 0.0 | 330.75 |
| 14:39:20 | 1664 | 0.0 | 330.75 |
| 14:39:21 | 1664 | 0.0 | 330.75 |
| 14:39:22 | 1663 | 0.0 | 330.75 |
| 14:39:23 | 1662 | 0.0 | 330.75 |
| 14:39:24 | 1662 | 0.0 | 330.75 |
| 14:39:25 | 1661 | 0.0 | 330.75 |
| 14:39:26 | 1660 | 0.0 | 330.75 |
| 14:39:27 | 1660 | 0.0 | 330.75 |
| 14:39:28 | 1659 | 0.0 | 330.75 |
| 14:39:29 | 1658 | 0.0 | 330.75 |
| 14:39:30 | 1658 | 0.0 | 330.75 |
| 14:39:31 | 1657 | 0.0 | 330.75 |
| 14:39:32 | 1656 | 0.0 | 330.75 |
| 14:39:33 | 1656 | 0.0 | 330.75 |
| 14:39:34 | 1655 | 0.0 | 330.75 |
| 14:39:35 | 1654 | 0.0 | 330.75 |
| 14:39:36 | 1654 | 0.0 | 330.75 |
| 14:39:37 | 1653 | 0.0 | 330.75 |
| 14:39:38 | 1652 | 0.0 | 330.75 |
| 14:39:39 | 1652 | 0.0 | 330.75 |
| 14:39:40 | 1651 | 0.0 | 330.75 |
| 14:39:41 | 1650 | 0.0 | 330.75 |
| 14:39:42 | 1649 | 0.0 | 330.75 |
| 14:39:43 | 1649 | 0.0 | 330.75 |
| 14:39:44 | 1648 | 0.0 | 330.75 |
| 14:39:45 | 1647 | 0.0 | 330.75 |
| 14:39:46 | 1647 | 0.0 | 330.75 |
| 14:39:47 | 1646 | 0.0 | 330.75 |
| 14:39:48 | 1645 | 0.0 | 330.75 |
| 14:39:49 | 1645 | 0.0 | 330.75 |
| 14:39:50 | 1644 | 0.0 | 330.75 |
| 14:39:51 | 1643 | 0.0 | 330.75 |
| 14:39:52 | 1643 | 0.0 | 330.75 |
| 14:39:53 | 1642 | 0.0 | 330.75 |
| 14:39:54 | 1641 | 0.0 | 330.75 |
| 14:39:55 | 1641 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:39:56 | 1640 | 0.0 | 330.75 |
| 14:39:57 | 1639 | 0.0 | 330.75 |
| 14:39:58 | 1639 | 0.0 | 330.75 |
| 14:39:59 | 1638 | 0.0 | 330.75 |
| 14:40:00 | 1637 | 0.0 | 330.75 |
| 14:40:01 | 1637 | 0.0 | 330.75 |
| 14:40:02 | 1636 | 0.0 | 330.75 |
| 14:40:03 | 1635 | 0.0 | 330.75 |
| 14:40:04 | 1635 | 0.0 | 330.75 |
| 14:40:05 | 1634 | 0.0 | 330.75 |
| 14:40:06 | 1633 | 0.0 | 330.75 |
| 14:40:07 | 1633 | 0.0 | 330.75 |
| 14:40:08 | 1632 | 0.0 | 330.75 |
| 14:40:09 | 1631 | 0.0 | 330.75 |
| 14:40:10 | 1631 | 0.0 | 330.75 |
| 14:40:11 | 1630 | 0.0 | 330.75 |
| 14:40:12 | 1629 | 0.0 | 330.75 |
| 14:40:13 | 1629 | 0.0 | 330.75 |
| 14:40:14 | 1628 | 0.0 | 330.75 |
| 14:40:15 | 1627 | 0.0 | 330.75 |
| 14:40:16 | 1627 | 0.0 | 330.75 |
| 14:40:17 | 1626 | 0.0 | 330.75 |
| 14:40:18 | 1625 | 0.0 | 330.75 |
| 14:40:19 | 1625 | 0.0 | 330.75 |
| 14:40:20 | 1624 | 0.0 | 330.75 |
| 14:40:21 | 1624 | 0.0 | 330.75 |
| 14:40:22 | 1623 | 0.0 | 330.75 |
| 14:40:23 | 1622 | 0.0 | 330.75 |
| 14:40:24 | 1621 | 0.0 | 330.75 |
| 14:40:25 | 1621 | 0.0 | 330.75 |
| 14:40:26 | 1620 | 0.0 | 330.75 |
| 14:40:27 | 1619 | 0.0 | 330.75 |
| 14:40:28 | 1619 | 0.0 | 330.75 |
| 14:40:29 | 1618 | 0.0 | 330.75 |
| 14:40:30 | 1617 | 0.0 | 330.75 |
| 14:40:31 | 1617 | 0.0 | 330.75 |
| 14:40:32 | 1616 | 0.0 | 330.75 |
| 14:40:33 | 1616 | 0.0 | 330.75 |
| 14:40:34 | 1615 | 0.0 | 330.75 |
| 14:40:35 | 1614 | 0.0 | 330.75 |
| 14:40:36 | 1614 | 0.0 | 330.75 |
| 14:40:37 | 1613 | 0.0 | 330.75 |
| 14:40:38 | 1612 | 0.0 | 330.75 |
| 14:40:39 | 1612 | 0.0 | 330.75 |
| 14:40:40 | 1611 | 0.0 | 330.75 |
| 14:40:41 | 1610 | 0.0 | 330.75 |
| 14:40:42 | 1610 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:40:43 | 1609 | 0.0 | 330.75 |
| 14:40:44 | 1608 | 0.0 | 330.75 |
| 14:40:45 | 1608 | 0.0 | 330.75 |
| 14:40:46 | 1607 | 0.0 | 330.75 |
| 14:40:47 | 1606 | 0.0 | 330.75 |
| 14:40:48 | 1606 | 0.0 | 330.75 |
| 14:40:49 | 1605 | 0.0 | 330.75 |
| 14:40:50 | 1604 | 0.0 | 330.75 |
| 14:40:51 | 1604 | 0.0 | 330.75 |
| 14:40:52 | 1603 | 0.0 | 330.75 |
| 14:40:53 | 1602 | 0.0 | 330.75 |
| 14:40:54 | 1602 | 0.0 | 330.75 |
| 14:40:55 | 1601 | 0.0 | 330.75 |
| 14:40:56 | 1601 | 0.0 | 330.75 |
| 14:40:57 | 1600 | 0.0 | 330.75 |
| 14:40:58 | 1599 | 0.0 | 330.75 |
| 14:40:59 | 1599 | 0.0 | 330.75 |
| 14:41:00 | 1598 | 0.0 | 330.75 |
| 14:41:01 | 1597 | 0.0 | 330.75 |
| 14:41:02 | 1597 | 0.0 | 330.75 |
| 14:41:03 | 1596 | 0.0 | 330.75 |
| 14:41:04 | 1595 | 0.0 | 330.75 |
| 14:41:05 | 1595 | 0.0 | 330.75 |
| 14:41:06 | 1594 | 0.0 | 330.75 |
| 14:41:07 | 1593 | 0.0 | 330.75 |
| 14:41:08 | 1593 | 0.0 | 330.75 |
| 14:41:09 | 1592 | 0.0 | 330.75 |
| 14:41:10 | 1591 | 0.0 | 330.75 |
| 14:41:11 | 1591 | 0.0 | 330.75 |
| 14:41:12 | 1590 | 0.0 | 330.75 |
| 14:41:13 | 1589 | 0.0 | 330.75 |
| 14:41:14 | 1589 | 0.0 | 330.75 |
| 14:41:15 | 1588 | 0.0 | 330.75 |
| 14:41:16 | 1588 | 0.0 | 330.75 |
| 14:41:17 | 1587 | 0.0 | 330.75 |
| 14:41:18 | 1586 | 0.0 | 330.75 |
| 14:41:19 | 1586 | 0.0 | 330.75 |
| 14:41:20 | 1585 | 0.0 | 330.75 |
| 14:41:21 | 1584 | 0.0 | 330.75 |
| 14:41:22 | 1584 | 0.0 | 330.75 |
| 14:41:23 | 1583 | 0.0 | 330.75 |
| 14:41:24 | 1582 | 0.0 | 330.75 |
| 14:41:25 | 1582 | 0.0 | 330.75 |
| 14:41:26 | 1581 | 0.0 | 330.75 |
| 14:41:27 | 1580 | 0.0 | 330.75 |
| 14:41:28 | 1580 | 0.0 | 330.75 |
| 14:41:29 | 1579 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:41:30 | 1579 | 0.0 | 330.75 |
| 14:41:31 | 1578 | 0.0 | 330.75 |
| 14:41:32 | 1577 | 0.0 | 330.75 |
| 14:41:33 | 1577 | 0.0 | 330.75 |
| 14:41:34 | 1576 | 0.0 | 330.75 |
| 14:41:35 | 1575 | 0.0 | 330.75 |
| 14:41:36 | 1575 | 0.0 | 330.75 |
| 14:41:37 | 1574 | 0.0 | 330.75 |
| 14:41:38 | 1574 | 0.0 | 330.75 |
| 14:41:39 | 1573 | 0.0 | 330.75 |
| 14:41:40 | 1572 | 0.0 | 330.75 |
| 14:41:41 | 1572 | 0.0 | 330.75 |
| 14:41:42 | 1571 | 0.0 | 330.75 |
| 14:41:43 | 1570 | 0.0 | 330.75 |
| 14:41:44 | 1570 | 0.0 | 330.75 |
| 14:41:45 | 1569 | 0.0 | 330.75 |
| 14:41:46 | 1569 | 0.0 | 330.75 |
| 14:41:47 | 1568 | 0.0 | 330.75 |
| 14:41:48 | 1567 | 0.0 | 330.75 |
| 14:41:49 | 1567 | 0.0 | 330.75 |
| 14:41:50 | 1566 | 0.0 | 330.75 |
| 14:41:51 | 1565 | 0.0 | 330.75 |
| 14:41:52 | 1565 | 0.0 | 330.75 |
| 14:41:53 | 1564 | 0.0 | 330.75 |
| 14:41:54 | 1564 | 0.0 | 330.75 |
| 14:41:55 | 1563 | 0.0 | 330.75 |
| 14:41:56 | 1562 | 0.0 | 330.75 |
| 14:41:57 | 1562 | 0.0 | 330.75 |
| 14:41:58 | 1561 | 0.0 | 330.75 |
| 14:41:59 | 1560 | 0.0 | 330.75 |
| 14:42:00 | 1560 | 0.0 | 330.75 |
| 14:42:01 | 1559 | 0.0 | 330.75 |
| 14:42:02 | 1559 | 0.0 | 330.75 |
| 14:42:03 | 1558 | 0.0 | 330.75 |
| 14:42:04 | 1557 | 0.0 | 330.75 |
| 14:42:05 | 1557 | 0.0 | 330.75 |
| 14:42:06 | 1556 | 0.0 | 330.75 |
| 14:42:07 | 1555 | 0.0 | 330.75 |
| 14:42:08 | 1555 | 0.0 | 330.75 |
| 14:42:09 | 1554 | 0.0 | 330.75 |
| 14:42:10 | 1553 | 0.0 | 330.75 |
| 14:42:11 | 1553 | 0.0 | 330.75 |
| 14:42:12 | 1552 | 0.0 | 330.75 |
| 14:42:13 | 1552 | 0.0 | 330.75 |
| 14:42:14 | 1551 | 0.0 | 330.75 |
| 14:42:15 | 1550 | 0.0 | 330.75 |
| 14:42:16 | 1550 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:42:17 | 1549 | 0.0 | 330.75 |
| 14:42:18 | 1549 | 0.0 | 330.75 |
| 14:42:19 | 1548 | 0.0 | 330.75 |
| 14:42:20 | 1547 | 0.0 | 330.75 |
| 14:42:21 | 1547 | 0.0 | 330.75 |
| 14:42:22 | 1546 | 0.0 | 330.75 |
| 14:42:23 | 1546 | 0.0 | 330.75 |
| 14:42:24 | 1545 | 0.0 | 330.75 |
| 14:42:25 | 1544 | 0.0 | 330.75 |
| 14:42:26 | 1544 | 0.0 | 330.75 |
| 14:42:27 | 1543 | 0.0 | 330.75 |
| 14:42:28 | 1543 | 0.0 | 330.75 |
| 14:42:29 | 1542 | 0.0 | 330.75 |
| 14:42:30 | 1541 | 0.0 | 330.75 |
| 14:42:31 | 1541 | 0.0 | 330.75 |
| 14:42:32 | 1540 | 0.0 | 330.75 |
| 14:42:33 | 1539 | 0.0 | 330.75 |
| 14:42:34 | 1539 | 0.0 | 330.75 |
| 14:42:35 | 1538 | 0.0 | 330.75 |
| 14:42:36 | 1538 | 0.0 | 330.75 |
| 14:42:37 | 1537 | 0.0 | 330.75 |
| 14:42:38 | 1536 | 0.0 | 330.75 |
| 14:42:39 | 1536 | 0.0 | 330.75 |
| 14:42:40 | 1535 | 0.0 | 330.75 |
| 14:42:41 | 1535 | 0.0 | 330.75 |
| 14:42:42 | 1534 | 0.0 | 330.75 |
| 14:42:43 | 1533 | 0.0 | 330.75 |
| 14:42:44 | 1533 | 0.0 | 330.75 |
| 14:42:45 | 1532 | 0.0 | 330.75 |
| 14:42:46 | 1532 | 0.0 | 330.75 |
| 14:42:47 | 1531 | 0.0 | 330.75 |
| 14:42:48 | 1530 | 0.0 | 330.75 |
| 14:42:49 | 1530 | 0.0 | 330.75 |
| 14:42:50 | 1529 | 0.0 | 330.75 |
| 14:42:51 | 1528 | 0.0 | 330.75 |
| 14:42:52 | 1528 | 0.0 | 330.75 |
| 14:42:53 | 1527 | 0.0 | 330.75 |
| 14:42:54 | 1527 | 0.0 | 330.75 |
| 14:42:55 | 1526 | 0.0 | 330.75 |
| 14:42:56 | 1525 | 0.0 | 330.75 |
| 14:42:57 | 1525 | 0.0 | 330.75 |
| 14:42:58 | 1524 | 0.0 | 330.75 |
| 14:42:59 | 1524 | 0.0 | 330.75 |
| 14:43:00 | 1523 | 0.0 | 330.75 |
| 14:43:01 | 1522 | 0.0 | 330.75 |
| 14:43:02 | 1522 | 0.0 | 330.75 |
| 14:43:03 | 1521 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:43:04 | 1521 | 0.0 | 330.75 |
| 14:43:05 | 1520 | 0.0 | 330.75 |
| 14:43:06 | 1519 | 0.0 | 330.75 |
| 14:43:07 | 1519 | 0.0 | 330.75 |
| 14:43:08 | 1518 | 0.0 | 330.75 |
| 14:43:09 | 1517 | 0.0 | 330.75 |
| 14:43:10 | 1517 | 0.0 | 330.75 |
| 14:43:11 | 1516 | 0.0 | 330.75 |
| 14:43:12 | 1516 | 0.0 | 330.75 |
| 14:43:13 | 1515 | 0.0 | 330.75 |
| 14:43:14 | 1515 | 0.0 | 330.75 |
| 14:43:15 | 1514 | 0.0 | 330.75 |
| 14:43:16 | 1514 | 0.0 | 330.75 |
| 14:43:17 | 1513 | 0.0 | 330.75 |
| 14:43:18 | 1512 | 0.0 | 330.75 |
| 14:43:19 | 1512 | 0.0 | 330.75 |
| 14:43:20 | 1511 | 0.0 | 330.75 |
| 14:43:21 | 1510 | 0.0 | 330.75 |
| 14:43:22 | 1510 | 0.0 | 330.75 |
| 14:43:23 | 1509 | 0.0 | 330.75 |
| 14:43:24 | 1509 | 0.0 | 330.75 |
| 14:43:25 | 1508 | 0.0 | 330.75 |
| 14:43:26 | 1507 | 0.0 | 330.75 |
| 14:43:27 | 1507 | 0.0 | 330.75 |
| 14:43:28 | 1506 | 0.0 | 330.75 |
| 14:43:29 | 1506 | 0.0 | 330.75 |
| 14:43:30 | 1505 | 0.0 | 330.75 |
| 14:43:31 | 1504 | 0.0 | 330.75 |
| 14:43:32 | 1504 | 0.0 | 330.75 |
| 14:43:33 | 1503 | 0.0 | 330.75 |
| 14:43:34 | 1503 | 0.0 | 330.75 |
| 14:43:35 | 1502 | 0.0 | 330.75 |
| 14:43:36 | 1502 | 0.0 | 330.75 |
| 14:43:37 | 1501 | 0.0 | 330.75 |
| 14:43:38 | 1500 | 0.0 | 330.75 |
| 14:43:39 | 1500 | 0.0 | 330.75 |
| 14:43:40 | 1499 | 0.0 | 330.75 |
| 14:43:41 | 1499 | 0.0 | 330.75 |
| 14:43:42 | 1498 | 0.0 | 330.75 |
| 14:43:43 | 1498 | 0.0 | 330.75 |
| 14:43:44 | 1497 | 0.0 | 330.75 |
| 14:43:45 | 1496 | 0.0 | 330.75 |
| 14:43:46 | 1496 | 0.0 | 330.75 |
| 14:43:47 | 1495 | 0.0 | 330.75 |
| 14:43:48 | 1495 | 0.0 | 330.75 |
| 14:43:49 | 1494 | 0.0 | 330.75 |
| 14:43:50 | 1494 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:43:51 | 1493 | 0.0 | 330.75 |
| 14:43:52 | 1492 | 0.0 | 330.75 |
| 14:43:53 | 1492 | 0.0 | 330.75 |
| 14:43:54 | 1491 | 0.0 | 330.75 |
| 14:43:55 | 1491 | 0.0 | 330.75 |
| 14:43:56 | 1490 | 0.0 | 330.75 |
| 14:43:57 | 1489 | 0.0 | 330.75 |
| 14:43:58 | 1489 | 0.0 | 330.75 |
| 14:43:59 | 1488 | 0.0 | 330.75 |
| 14:44:00 | 1488 | 0.0 | 330.75 |
| 14:44:01 | 1487 | 0.0 | 330.75 |
| 14:44:02 | 1487 | 0.0 | 330.75 |
| 14:44:03 | 1486 | 0.0 | 330.75 |
| 14:44:04 | 1485 | 0.0 | 330.75 |
| 14:44:05 | 1485 | 0.0 | 330.75 |
| 14:44:06 | 1484 | 0.0 | 330.75 |
| 14:44:07 | 1484 | 0.0 | 330.75 |
| 14:44:08 | 1483 | 0.0 | 330.75 |
| 14:44:09 | 1483 | 0.0 | 330.75 |
| 14:44:10 | 1482 | 0.0 | 330.75 |
| 14:44:11 | 1481 | 0.0 | 330.75 |
| 14:44:12 | 1481 | 0.0 | 330.75 |
| 14:44:13 | 1480 | 0.0 | 330.75 |
| 14:44:14 | 1480 | 0.0 | 330.75 |
| 14:44:15 | 1479 | 0.0 | 330.75 |
| 14:44:16 | 1479 | 0.0 | 330.75 |
| 14:44:17 | 1478 | 0.0 | 330.75 |
| 14:44:18 | 1477 | 0.0 | 330.75 |
| 14:44:19 | 1477 | 0.0 | 330.75 |
| 14:44:20 | 1476 | 0.0 | 330.75 |
| 14:44:21 | 1476 | 0.0 | 330.75 |
| 14:44:22 | 1475 | 0.0 | 330.75 |
| 14:44:23 | 1475 | 0.0 | 330.75 |
| 14:44:24 | 1474 | 0.0 | 330.75 |
| 14:44:25 | 1473 | 0.0 | 330.75 |
| 14:44:26 | 1473 | 0.0 | 330.75 |
| 14:44:27 | 1472 | 0.0 | 330.75 |
| 14:44:28 | 1472 | 0.0 | 330.75 |
| 14:44:29 | 1471 | 0.0 | 330.75 |
| 14:44:30 | 1471 | 0.0 | 330.75 |
| 14:44:31 | 1470 | 0.0 | 330.75 |
| 14:44:32 | 1470 | 0.0 | 330.75 |
| 14:44:33 | 1469 | 0.0 | 330.75 |
| 14:44:34 | 1468 | 0.0 | 330.75 |
| 14:44:35 | 1468 | 0.0 | 330.75 |
| 14:44:36 | 1467 | 0.0 | 330.75 |
| 14:44:37 | 1467 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:44:38 | 1466 | 0.0 | 330.75 |
| 14:44:39 | 1465 | 0.0 | 330.75 |
| 14:44:40 | 1465 | 0.0 | 330.75 |
| 14:44:41 | 1464 | 0.0 | 330.75 |
| 14:44:42 | 1464 | 0.0 | 330.75 |
| 14:44:43 | 1463 | 0.0 | 330.75 |
| 14:44:44 | 1463 | 0.0 | 330.75 |
| 14:44:45 | 1462 | 0.0 | 330.75 |
| 14:44:46 | 1462 | 0.0 | 330.75 |
| 14:44:47 | 1461 | 0.0 | 330.75 |
| 14:44:48 | 1461 | 0.0 | 330.75 |
| 14:44:49 | 1460 | 0.0 | 330.75 |
| 14:44:50 | 1460 | 0.0 | 330.75 |
| 14:44:51 | 1459 | 0.0 | 330.75 |
| 14:44:52 | 1458 | 0.0 | 330.75 |
| 14:44:53 | 1458 | 0.0 | 330.75 |
| 14:44:54 | 1457 | 0.0 | 330.75 |
| 14:44:55 | 1457 | 0.0 | 330.75 |
| 14:44:56 | 1456 | 0.0 | 330.75 |
| 14:44:57 | 1456 | 0.0 | 330.75 |
| 14:44:58 | 1455 | 0.0 | 330.75 |
| 14:44:59 | 1454 | 0.0 | 330.75 |
| 14:45:00 | 1454 | 0.0 | 330.75 |
| 14:45:01 | 1453 | 0.0 | 330.75 |
| 14:45:02 | 1453 | 0.0 | 330.75 |
| 14:45:03 | 1452 | 0.0 | 330.75 |
| 14:45:04 | 1452 | 0.0 | 330.75 |
| 14:45:05 | 1451 | 0.0 | 330.75 |
| 14:45:06 | 1451 | 0.0 | 330.75 |
| 14:45:07 | 1450 | 0.0 | 330.75 |
| 14:45:08 | 1450 | 0.0 | 330.75 |
| 14:45:09 | 1449 | 0.0 | 330.75 |
| 14:45:10 | 1448 | 0.0 | 330.75 |
| 14:45:11 | 1448 | 0.0 | 330.75 |
| 14:45:12 | 1447 | 0.0 | 330.75 |
| 14:45:13 | 1447 | 0.0 | 330.75 |
| 14:45:14 | 1446 | 0.0 | 330.75 |
| 14:45:15 | 1446 | 0.0 | 330.75 |
| 14:45:16 | 1445 | 0.0 | 330.75 |
| 14:45:17 | 1445 | 0.0 | 330.75 |
| 14:45:18 | 1444 | 0.0 | 330.75 |
| 14:45:19 | 1443 | 0.0 | 330.75 |
| 14:45:20 | 1443 | 0.0 | 330.75 |
| 14:45:21 | 1442 | 0.0 | 330.75 |
| 14:45:22 | 1442 | 0.0 | 330.75 |
| 14:45:23 | 1441 | 0.0 | 330.75 |
| 14:45:24 | 1441 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:45:25 | 1440 | 0.0 | 330.75 |
| 14:45:26 | 1439 | 0.0 | 330.75 |
| 14:45:27 | 1439 | 0.0 | 330.75 |
| 14:45:28 | 1439 | 0.0 | 330.75 |
| 14:45:29 | 1438 | 0.0 | 330.75 |
| 14:45:30 | 1438 | 0.0 | 330.75 |
| 14:45:31 | 1437 | 0.0 | 330.75 |
| 14:45:32 | 1436 | 0.0 | 330.75 |
| 14:45:33 | 1436 | 0.0 | 330.75 |
| 14:45:34 | 1435 | 0.0 | 330.75 |
| 14:45:35 | 1435 | 0.0 | 330.75 |
| 14:45:36 | 1434 | 0.0 | 330.75 |
| 14:45:37 | 1434 | 0.0 | 330.75 |
| 14:45:38 | 1433 | 0.0 | 330.75 |
| 14:45:39 | 1433 | 0.0 | 330.75 |
| 14:45:40 | 1432 | 0.0 | 330.75 |
| 14:45:41 | 1431 | 0.0 | 330.75 |
| 14:45:42 | 1431 | 0.0 | 330.75 |
| 14:45:43 | 1430 | 0.0 | 330.75 |
| 14:45:44 | 1430 | 0.0 | 330.75 |
| 14:45:45 | 1429 | 0.0 | 330.75 |
| 14:45:46 | 1429 | 0.0 | 330.75 |
| 14:45:47 | 1428 | 0.0 | 330.75 |
| 14:45:48 | 1427 | 0.0 | 330.75 |
| 14:45:49 | 1427 | 0.0 | 330.75 |
| 14:45:50 | 1427 | 0.0 | 330.75 |
| 14:45:51 | 1426 | 0.0 | 330.75 |
| 14:45:52 | 1426 | 0.0 | 330.75 |
| 14:45:53 | 1425 | 0.0 | 330.75 |
| 14:45:54 | 1424 | 0.0 | 330.75 |
| 14:45:55 | 1424 | 0.0 | 330.75 |
| 14:45:56 | 1424 | 0.0 | 330.75 |
| 14:45:57 | 1423 | 0.0 | 330.75 |
| 14:45:58 | 1422 | 0.0 | 330.75 |
| 14:45:59 | 1422 | 0.0 | 330.75 |
| 14:46:00 | 1421 | 0.0 | 330.75 |
| 14:46:01 | 1421 | 0.0 | 330.75 |
| 14:46:02 | 1420 | 0.0 | 330.75 |
| 14:46:03 | 1420 | 0.0 | 330.75 |
| 14:46:04 | 1419 | 0.0 | 330.75 |
| 14:46:05 | 1419 | 0.0 | 330.75 |
| 14:46:06 | 1418 | 0.0 | 330.75 |
| 14:46:07 | 1418 | 0.0 | 330.75 |
| 14:46:08 | 1417 | 0.0 | 330.75 |
| 14:46:09 | 1416 | 0.0 | 330.75 |
| 14:46:10 | 1416 | 0.0 | 330.75 |
| 14:46:11 | 1415 | 0.0 | 330.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:46:12 | 1415 | 0.0 | 330.75 |
| 14:46:13 | 1414 | 0.0 | 330.75 |
| 14:46:14 | 1414 | 0.0 | 330.75 |
| 14:46:15 | 1413 | 0.0 | 330.75 |
| 14:46:16 | 1413 | 0.0 | 330.75 |
| 14:46:17 | 1412 | 0.0 | 330.75 |
| 14:46:18 | 1412 | 0.0 | 330.75 |
| 14:46:19 | 1411 | 0.0 | 330.75 |
| 14:46:20 | 1410 | 0.0 | 330.75 |
| 14:46:21 | 1410 | 0.0 | 330.75 |
| 14:46:22 | 1409 | 0.0 | 330.75 |
| 14:46:23 | 1409 | 0.0 | 330.75 |
| 14:46:24 | 1408 | 0.0 | 330.75 |
| 14:46:25 | 1408 | 0.0 | 330.75 |
| 14:46:26 | 1407 | 0.0 | 330.75 |
| 14:46:27 | 1407 | 0.0 | 330.75 |
| 14:46:28 | 1406 | 0.0 | 330.75 |
| 14:46:29 | 1406 | 0.0 | 330.75 |
| 14:46:30 | 1406 | 0.0 | 330.75 |
| 14:46:31 | 1405 | 0.0 | 330.75 |
| 14:46:32 | 1404 | 0.0 | 330.75 |
| 14:46:33 | 1404 | 0.0 | 330.75 |
| 14:46:34 | 1403 | 0.0 | 330.75 |
| 14:46:35 | 1403 | 0.0 | 330.75 |
| 14:46:36 | 1403 | 0.0 | 330.75 |
| 14:46:37 | 1402 | 0.0 | 330.75 |
| 14:46:38 | 1401 | 0.0 | 330.75 |
| 14:46:39 | 1400 | 0.0 | 330.75 |
| 14:46:40 | 1399 | 0.0 | 330.75 |
| 14:46:41 | 1399 | 0.0 | 330.75 |
| 14:46:42 | 1398 | 0.0 | 330.75 |
| 14:46:43 | 1397 | 0.0 | 330.75 |
| 14:46:44 | 1397 | 0.0 | 330.75 |
| 14:46:45 | 1396 | 0.0 | 330.75 |
| 14:46:46 | 1396 | 0.0 | 330.75 |
| 14:46:47 | 1397 | 0.0 | 330.75 |
| 14:46:48 | 1399 | 0.1 | 330.75 |
| 14:46:49 | 1403 | 0.2 | 330.75 |
| 14:46:50 | 1404 | 0.3 | 330.76 |
| 14:46:51 | 1405 | 0.5 | 330.77 |
| 14:46:52 | 1408 | 0.8 | 330.78 |
| 14:46:53 | 1414 | 1.1 | 330.80 |
| 14:46:54 | 1419 | 1.2 | 330.82 |
| 14:46:55 | 1421 | 1.3 | 330.84 |
| 14:46:56 | 1423 | 1.5 | 330.87 |
| 14:46:57 | 1427 | 1.7 | 330.90 |
| 14:46:58 | 1433 | 1.7 | 330.92 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:46:59 | 1438 | 1.8 | 330.95 |
| 14:47:00 | 1441 | 1.8 | 330.98 |
| 14:47:01 | 1444 | 1.9 | 331.02 |
| 14:47:02 | 1447 | 1.9 | 331.05 |
| 14:47:03 | 1453 | 1.9 | 331.08 |
| 14:47:04 | 1457 | 1.9 | 331.11 |
| 14:47:05 | 1460 | 1.9 | 331.14 |
| 14:47:06 | 1463 | 1.9 | 331.17 |
| 14:47:07 | 1466 | 1.9 | 331.21 |
| 14:47:08 | 1469 | 1.9 | 331.24 |
| 14:47:09 | 1473 | 1.9 | 331.27 |
| 14:47:10 | 1476 | 1.9 | 331.30 |
| 14:47:11 | 1479 | 1.9 | 331.33 |
| 14:47:12 | 1483 | 1.9 | 331.37 |
| 14:47:13 | 1487 | 2.0 | 331.40 |
| 14:47:14 | 1493 | 2.1 | 331.43 |
| 14:47:15 | 1498 | 2.1 | 331.47 |
| 14:47:16 | 1502 | 2.2 | 331.51 |
| 14:47:17 | 1506 | 2.3 | 331.54 |
| 14:47:18 | 1511 | 2.3 | 331.58 |
| 14:47:19 | 1517 | 2.4 | 331.62 |
| 14:47:20 | 1522 | 2.4 | 331.66 |
| 14:47:21 | 1527 | 2.5 | 331.70 |
| 14:47:22 | 1531 | 2.5 | 331.75 |
| 14:47:23 | 1535 | 2.5 | 331.79 |
| 14:47:24 | 1542 | 2.6 | 331.83 |
| 14:47:25 | 1546 | 2.6 | 331.87 |
| 14:47:26 | 1550 | 2.6 | 331.92 |
| 14:47:27 | 1554 | 2.6 | 331.96 |
| 14:47:28 | 1558 | 2.6 | 332.00 |
| 14:47:29 | 1562 | 2.6 | 332.05 |
| 14:47:30 | 1567 | 2.6 | 332.09 |
| 14:47:31 | 1570 | 2.6 | 332.14 |
| 14:47:32 | 1574 | 2.6 | 332.18 |
| 14:47:33 | 1578 | 2.6 | 332.22 |
| 14:47:34 | 1582 | 2.6 | 332.27 |
| 14:47:35 | 1586 | 2.6 | 332.31 |
| 14:47:36 | 1590 | 2.6 | 332.35 |
| 14:47:37 | 1593 | 2.6 | 332.40 |
| 14:47:38 | 1597 | 2.6 | 332.44 |
| 14:47:39 | 1601 | 2.6 | 332.49 |
| 14:47:40 | 1604 | 2.6 | 332.53 |
| 14:47:41 | 1608 | 2.6 | 332.57 |
| 14:47:42 | 1612 | 2.6 | 332.62 |
| 14:47:43 | 1615 | 2.6 | 332.66 |
| 14:47:44 | 1621 | 2.6 | 332.70 |
| 14:47:45 | 1624 | 2.6 | 332.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:47:46 | 1627 | 2.6 | 332.79 |
| 14:47:47 | 1631 | 2.6 | 332.84 |
| 14:47:48 | 1634 | 2.6 | 332.88 |
| 14:47:49 | 1638 | 2.6 | 332.92 |
| 14:47:50 | 1642 | 2.6 | 332.97 |
| 14:47:51 | 1645 | 2.6 | 333.01 |
| 14:47:52 | 1648 | 2.6 | 333.05 |
| 14:47:53 | 1652 | 2.6 | 333.10 |
| 14:47:54 | 1654 | 2.6 | 333.14 |
| 14:47:55 | 1658 | 2.6 | 333.19 |
| 14:47:56 | 1661 | 2.6 | 333.23 |
| 14:47:57 | 1664 | 2.6 | 333.27 |
| 14:47:58 | 1667 | 2.6 | 333.32 |
| 14:47:59 | 1671 | 2.6 | 333.36 |
| 14:48:00 | 1673 | 2.6 | 333.40 |
| 14:48:01 | 1677 | 2.6 | 333.45 |
| 14:48:02 | 1680 | 2.6 | 333.49 |
| 14:48:03 | 1682 | 2.6 | 333.53 |
| 14:48:04 | 1685 | 2.6 | 333.58 |
| 14:48:05 | 1689 | 2.6 | 333.62 |
| 14:48:06 | 1691 | 2.6 | 333.67 |
| 14:48:07 | 1695 | 2.6 | 333.71 |
| 14:48:08 | 1698 | 2.6 | 333.75 |
| 14:48:09 | 1700 | 2.6 | 333.80 |
| 14:48:10 | 1703 | 2.6 | 333.84 |
| 14:48:11 | 1706 | 2.6 | 333.88 |
| 14:48:12 | 1709 | 2.6 | 333.93 |
| 14:48:13 | 1712 | 2.6 | 333.97 |
| 14:48:14 | 1715 | 2.6 | 334.02 |
| 14:48:15 | 1718 | 2.6 | 334.06 |
| 14:48:16 | 1720 | 2.6 | 334.10 |
| 14:48:17 | 1722 | 2.6 | 334.14 |
| 14:48:18 | 1723 | 2.5 | 334.19 |
| 14:48:19 | 1724 | 2.5 | 334.23 |
| 14:48:20 | 1726 | 2.5 | 334.27 |
| 14:48:21 | 1728 | 2.5 | 334.31 |
| 14:48:22 | 1731 | 2.5 | 334.35 |
| 14:48:23 | 1733 | 2.4 | 334.39 |
| 14:48:24 | 1733 | 2.4 | 334.43 |
| 14:48:25 | 1734 | 2.4 | 334.47 |
| 14:48:26 | 1735 | 2.4 | 334.51 |
| 14:48:27 | 1736 | 2.4 | 334.55 |
| 14:48:28 | 1738 | 2.4 | 334.59 |
| 14:48:29 | 1742 | 2.4 | 334.63 |
| 14:48:30 | 1746 | 2.4 | 334.67 |
| 14:48:31 | 1750 | 2.4 | 334.71 |
| 14:48:32 | 1751 | 2.4 | 334.75 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:48:33 | 1752 | 2.4 | 334.79 |
| 14:48:34 | 1753 | 2.4 | 334.83 |
| 14:48:35 | 1754 | 2.4 | 334.87 |
| 14:48:36 | 1754 | 2.3 | 334.91 |
| 14:48:37 | 1756 | 2.3 | 334.95 |
| 14:48:38 | 1757 | 2.3 | 334.99 |
| 14:48:39 | 1757 | 2.3 | 335.02 |
| 14:48:40 | 1756 | 2.2 | 335.06 |
| 14:48:41 | 1755 | 2.1 | 335.09 |
| 14:48:42 | 1755 | 2.1 | 335.13 |
| 14:48:43 | 1757 | 2.0 | 335.16 |
| 14:48:44 | 1758 | 2.0 | 335.20 |
| 14:48:45 | 1758 | 2.0 | 335.23 |
| 14:48:46 | 1757 | 2.0 | 335.26 |
| 14:48:47 | 1758 | 2.0 | 335.30 |
| 14:48:48 | 1760 | 2.0 | 335.33 |
| 14:48:49 | 1761 | 2.0 | 335.36 |
| 14:48:50 | 1762 | 2.0 | 335.39 |
| 14:48:51 | 1762 | 2.0 | 335.43 |
| 14:48:52 | 1763 | 2.0 | 335.46 |
| 14:48:53 | 1763 | 2.0 | 335.49 |
| 14:48:54 | 1764 | 2.0 | 335.52 |
| 14:48:55 | 1765 | 2.0 | 335.56 |
| 14:48:56 | 1765 | 1.9 | 335.59 |
| 14:48:57 | 1764 | 1.9 | 335.62 |
| 14:48:58 | 1763 | 1.8 | 335.65 |
| 14:48:59 | 1763 | 1.8 | 335.68 |
| 14:49:00 | 1763 | 1.8 | 335.71 |
| 14:49:01 | 1763 | 1.7 | 335.74 |
| 14:49:02 | 1761 | 1.7 | 335.77 |
| 14:49:03 | 1759 | 1.6 | 335.79 |
| 14:49:04 | 1758 | 1.6 | 335.82 |
| 14:49:05 | 1756 | 1.5 | 335.84 |
| 14:49:06 | 1756 | 1.5 | 335.87 |
| 14:49:07 | 1755 | 1.5 | 335.89 |
| 14:49:08 | 1753 | 1.4 | 335.92 |
| 14:49:09 | 1752 | 1.4 | 335.94 |
| 14:49:10 | 1752 | 1.4 | 335.96 |
| 14:49:11 | 1752 | 1.4 | 335.99 |
| 14:49:12 | 1752 | 1.4 | 336.01 |
| 14:49:13 | 1751 | 1.4 | 336.04 |
| 14:49:14 | 1750 | 1.5 | 336.06 |
| 14:49:15 | 1749 | 1.5 | 336.09 |
| 14:49:16 | 1749 | 1.5 | 336.11 |
| 14:49:17 | 1749 | 1.5 | 336.14 |
| 14:49:18 | 1749 | 1.5 | 336.16 |
| 14:49:19 | 1748 | 1.6 | 336.19 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:49:20 | 1748 | 1.6 | 336.21 |
| 14:49:21 | 1748 | 1.6 | 336.24 |
| 14:49:22 | 1748 | 1.6 | 336.27 |
| 14:49:23 | 1747 | 1.6 | 336.29 |
| 14:49:24 | 1747 | 1.6 | 336.32 |
| 14:49:25 | 1747 | 1.6 | 336.35 |
| 14:49:26 | 1747 | 1.6 | 336.37 |
| 14:49:27 | 1747 | 1.6 | 336.40 |
| 14:49:28 | 1747 | 1.6 | 336.43 |
| 14:49:29 | 1747 | 1.6 | 336.45 |
| 14:49:30 | 1747 | 1.6 | 336.48 |
| 14:49:31 | 1747 | 1.6 | 336.51 |
| 14:49:32 | 1747 | 1.6 | 336.54 |
| 14:49:33 | 1748 | 1.6 | 336.56 |
| 14:49:34 | 1748 | 1.6 | 336.59 |
| 14:49:35 | 1748 | 1.6 | 336.62 |
| 14:49:36 | 1748 | 1.6 | 336.65 |
| 14:49:37 | 1748 | 1.6 | 336.67 |
| 14:49:38 | 1748 | 1.6 | 336.70 |
| 14:49:39 | 1749 | 1.6 | 336.73 |
| 14:49:40 | 1749 | 1.6 | 336.75 |
| 14:49:41 | 1749 | 1.6 | 336.78 |
| 14:49:42 | 1749 | 1.6 | 336.81 |
| 14:49:43 | 1749 | 1.6 | 336.84 |
| 14:49:44 | 1750 | 1.6 | 336.86 |
| 14:49:45 | 1750 | 1.6 | 336.89 |
| 14:49:46 | 1750 | 1.6 | 336.92 |
| 14:49:47 | 1750 | 1.6 | 336.94 |
| 14:49:48 | 1750 | 1.6 | 336.97 |
| 14:49:49 | 1750 | 1.6 | 337.00 |
| 14:49:50 | 1750 | 1.6 | 337.03 |
| 14:49:51 | 1751 | 1.6 | 337.05 |
| 14:49:52 | 1751 | 1.6 | 337.08 |
| 14:49:53 | 1751 | 1.6 | 337.11 |
| 14:49:54 | 1751 | 1.6 | 337.13 |
| 14:49:55 | 1751 | 1.6 | 337.16 |
| 14:49:56 | 1751 | 1.6 | 337.19 |
| 14:49:57 | 1751 | 1.6 | 337.21 |
| 14:49:58 | 1751 | 1.5 | 337.24 |
| 14:49:59 | 1749 | 1.5 | 337.26 |
| 14:50:00 | 1749 | 1.5 | 337.29 |
| 14:50:01 | 1749 | 1.4 | 337.31 |
| 14:50:02 | 1747 | 1.4 | 337.33 |
| 14:50:03 | 1746 | 1.3 | 337.36 |
| 14:50:04 | 1745 | 1.3 | 337.38 |
| 14:50:05 | 1742 | 1.2 | 337.40 |
| 14:50:06 | 1741 | 1.2 | 337.42 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:50:07 | 1740 | 1.1 | 337.44 |
| 14:50:08 | 1739 | 1.1 | 337.45 |
| 14:50:09 | 1737 | 1.1 | 337.47 |
| 14:50:10 | 1731 | 0.8 | 337.49 |
| 14:50:11 | 1727 | 0.7 | 337.50 |
| 14:50:12 | 1724 | 0.6 | 337.51 |
| 14:50:13 | 1724 | 0.5 | 337.52 |
| 14:50:14 | 1724 | 0.6 | 337.53 |
| 14:50:15 | 1723 | 0.5 | 337.53 |
| 14:50:16 | 1719 | 0.5 | 337.54 |
| 14:50:17 | 1716 | 0.5 | 337.55 |
| 14:50:18 | 1713 | 0.5 | 337.56 |
| 14:50:19 | 1714 | 0.5 | 337.57 |
| 14:50:20 | 1712 | 0.5 | 337.58 |
| 14:50:21 | 1712 | 0.5 | 337.59 |
| 14:50:22 | 1709 | 0.6 | 337.60 |
| 14:50:23 | 1708 | 0.6 | 337.61 |
| 14:50:24 | 1706 | 0.6 | 337.62 |
| 14:50:25 | 1706 | 0.6 | 337.63 |
| 14:50:26 | 1705 | 0.7 | 337.64 |
| 14:50:27 | 1706 | 0.8 | 337.65 |
| 14:50:28 | 1710 | 1.2 | 337.67 |
| 14:50:29 | 1715 | 1.4 | 337.69 |
| 14:50:30 | 1714 | 1.4 | 337.72 |
| 14:50:31 | 1709 | 1.4 | 337.74 |
| 14:50:32 | 1703 | 1.4 | 337.76 |
| 14:50:33 | 1704 | 1.4 | 337.79 |
| 14:50:34 | 1705 | 1.3 | 337.81 |
| 14:50:35 | 1707 | 1.3 | 337.83 |
| 14:50:36 | 1705 | 1.3 | 337.85 |
| 14:50:37 | 1705 | 1.3 | 337.88 |
| 14:50:38 | 1704 | 1.3 | 337.90 |
| 14:50:39 | 1705 | 1.3 | 337.92 |
| 14:50:40 | 1705 | 1.3 | 337.94 |
| 14:50:41 | 1705 | 1.3 | 337.96 |
| 14:50:42 | 1705 | 1.3 | 337.98 |
| 14:50:43 | 1705 | 1.3 | 338.01 |
| 14:50:44 | 1705 | 1.3 | 338.03 |
| 14:50:45 | 1706 | 1.2 | 338.05 |
| 14:50:46 | 1708 | 1.2 | 338.07 |
| 14:50:47 | 1708 | 1.2 | 338.09 |
| 14:50:48 | 1708 | 1.2 | 338.11 |
| 14:50:49 | 1709 | 1.3 | 338.13 |
| 14:50:50 | 1709 | 1.3 | 338.15 |
| 14:50:51 | 1709 | 1.3 | 338.17 |
| 14:50:52 | 1710 | 1.3 | 338.19 |
| 14:50:53 | 1710 | 1.3 | 338.21 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:50:54 | 1711 | 1.3 | 338.24 |
| 14:50:55 | 1711 | 1.3 | 338.26 |
| 14:50:56 | 1711 | 1.3 | 338.28 |
| 14:50:57 | 1711 | 1.3 | 338.30 |
| 14:50:58 | 1712 | 1.3 | 338.32 |
| 14:50:59 | 1712 | 1.3 | 338.34 |
| 14:51:00 | 1713 | 1.3 | 338.36 |
| 14:51:01 | 1713 | 1.3 | 338.38 |
| 14:51:02 | 1713 | 1.3 | 338.40 |
| 14:51:03 | 1713 | 1.3 | 338.42 |
| 14:51:04 | 1714 | 1.3 | 338.45 |
| 14:51:05 | 1713 | 1.3 | 338.47 |
| 14:51:06 | 1714 | 1.3 | 338.49 |
| 14:51:07 | 1714 | 1.3 | 338.51 |
| 14:51:08 | 1714 | 1.3 | 338.53 |
| 14:51:09 | 1715 | 1.3 | 338.55 |
| 14:51:10 | 1715 | 1.3 | 338.57 |
| 14:51:11 | 1715 | 1.3 | 338.59 |
| 14:51:12 | 1715 | 1.3 | 338.61 |
| 14:51:13 | 1716 | 1.3 | 338.63 |
| 14:51:14 | 1716 | 1.3 | 338.66 |
| 14:51:15 | 1717 | 1.3 | 338.68 |
| 14:51:16 | 1717 | 1.2 | 338.70 |
| 14:51:17 | 1717 | 1.2 | 338.72 |
| 14:51:18 | 1717 | 1.2 | 338.74 |
| 14:51:19 | 1717 | 1.2 | 338.76 |
| 14:51:20 | 1717 | 1.2 | 338.78 |
| 14:51:21 | 1717 | 1.2 | 338.80 |
| 14:51:22 | 1717 | 1.2 | 338.82 |
| 14:51:23 | 1717 | 1.2 | 338.84 |
| 14:51:24 | 1718 | 1.2 | 338.86 |
| 14:51:25 | 1717 | 1.2 | 338.88 |
| 14:51:26 | 1717 | 1.2 | 338.90 |
| 14:51:27 | 1717 | 1.2 | 338.92 |
| 14:51:28 | 1717 | 1.2 | 338.94 |
| 14:51:29 | 1718 | 1.2 | 338.96 |
| 14:51:30 | 1719 | 1.2 | 338.98 |
| 14:51:31 | 1719 | 1.2 | 339.00 |
| 14:51:32 | 1718 | 1.2 | 339.02 |
| 14:51:33 | 1719 | 1.2 | 339.05 |
| 14:51:34 | 1718 | 1.2 | 339.07 |
| 14:51:35 | 1717 | 1.2 | 339.09 |
| 14:51:36 | 1716 | 1.2 | 339.11 |
| 14:51:37 | 1714 | 1.1 | 339.12 |
| 14:51:38 | 1713 | 1.1 | 339.14 |
| 14:51:39 | 1712 | 1.0 | 339.16 |
| 14:51:40 | 1710 | 1.0 | 339.18 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:51:41 | 1710 | 0.9 | 339.19 |
| 14:51:42 | 1707 | 0.9 | 339.20 |
| 14:51:43 | 1705 | 0.8 | 339.22 |
| 14:51:44 | 1704 | 0.7 | 339.23 |
| 14:51:45 | 1703 | 0.7 | 339.24 |
| 14:51:46 | 1701 | 0.6 | 339.25 |
| 14:51:47 | 1699 | 0.6 | 339.26 |
| 14:51:48 | 1696 | 0.5 | 339.27 |
| 14:51:49 | 1695 | 0.5 | 339.28 |
| 14:51:50 | 1693 | 0.4 | 339.28 |
| 14:51:51 | 1691 | 0.4 | 339.29 |
| 14:51:52 | 1688 | 0.4 | 339.30 |
| 14:51:53 | 1686 | 0.3 | 339.30 |
| 14:51:54 | 1683 | 0.3 | 339.31 |
| 14:51:55 | 1681 | 0.3 | 339.31 |
| 14:51:56 | 1679 | 0.3 | 339.32 |
| 14:51:57 | 1676 | 0.3 | 339.32 |
| 14:51:58 | 1675 | 0.3 | 339.33 |
| 14:51:59 | 1673 | 0.3 | 339.33 |
| 14:52:00 | 1671 | 0.3 | 339.34 |
| 14:52:01 | 1671 | 0.3 | 339.34 |
| 14:52:02 | 1671 | 0.4 | 339.35 |
| 14:52:03 | 1671 | 0.4 | 339.36 |
| 14:52:04 | 1668 | 0.5 | 339.36 |
| 14:52:05 | 1667 | 0.5 | 339.37 |
| 14:52:06 | 1668 | 0.6 | 339.38 |
| 14:52:07 | 1669 | 0.6 | 339.39 |
| 14:52:08 | 1669 | 0.7 | 339.40 |
| 14:52:09 | 1666 | 0.7 | 339.42 |
| 14:52:10 | 1664 | 0.8 | 339.43 |
| 14:52:11 | 1664 | 0.8 | 339.44 |
| 14:52:12 | 1666 | 0.9 | 339.46 |
| 14:52:13 | 1667 | 0.9 | 339.47 |
| 14:52:14 | 1667 | 0.9 | 339.49 |
| 14:52:15 | 1666 | 1.0 | 339.50 |
| 14:52:16 | 1666 | 1.0 | 339.52 |
| 14:52:17 | 1667 | 1.0 | 339.54 |
| 14:52:18 | 1668 | 1.1 | 339.56 |
| 14:52:19 | 1668 | 1.1 | 339.58 |
| 14:52:20 | 1668 | 1.1 | 339.59 |
| 14:52:21 | 1669 | 1.2 | 339.61 |
| 14:52:22 | 1667 | 1.2 | 339.63 |
| 14:52:23 | 1667 | 1.2 | 339.65 |
| 14:52:24 | 1668 | 1.2 | 339.67 |
| 14:52:25 | 1669 | 1.2 | 339.69 |
| 14:52:26 | 1670 | 1.2 | 339.71 |
| 14:52:27 | 1670 | 1.2 | 339.73 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:52:28 | 1671 | 1.2 | 339.75 |
| 14:52:29 | 1672 | 1.2 | 339.77 |
| 14:52:30 | 1673 | 1.2 | 339.79 |
| 14:52:31 | 1674 | 1.2 | 339.81 |
| 14:52:32 | 1675 | 1.3 | 339.84 |
| 14:52:33 | 1676 | 1.3 | 339.86 |
| 14:52:34 | 1676 | 1.3 | 339.88 |
| 14:52:35 | 1677 | 1.3 | 339.90 |
| 14:52:36 | 1678 | 1.3 | 339.92 |
| 14:52:37 | 1679 | 1.3 | 339.94 |
| 14:52:38 | 1680 | 1.3 | 339.96 |
| 14:52:39 | 1681 | 1.3 | 339.98 |
| 14:52:40 | 1681 | 1.3 | 340.01 |
| 14:52:41 | 1682 | 1.3 | 340.03 |
| 14:52:42 | 1683 | 1.3 | 340.05 |
| 14:52:43 | 1684 | 1.3 | 340.07 |
| 14:52:44 | 1685 | 1.3 | 340.09 |
| 14:52:45 | 1686 | 1.3 | 340.11 |
| 14:52:46 | 1687 | 1.3 | 340.14 |
| 14:52:47 | 1688 | 1.3 | 340.16 |
| 14:52:48 | 1689 | 1.3 | 340.18 |
| 14:52:49 | 1689 | 1.3 | 340.20 |
| 14:52:50 | 1690 | 1.3 | 340.22 |
| 14:52:51 | 1691 | 1.3 | 340.25 |
| 14:52:52 | 1692 | 1.3 | 340.27 |
| 14:52:53 | 1693 | 1.3 | 340.29 |
| 14:52:54 | 1694 | 1.3 | 340.31 |
| 14:52:55 | 1695 | 1.3 | 340.33 |
| 14:52:56 | 1695 | 1.3 | 340.36 |
| 14:52:57 | 1696 | 1.3 | 340.38 |
| 14:52:58 | 1697 | 1.3 | 340.40 |
| 14:52:59 | 1697 | 1.3 | 340.42 |
| 14:53:00 | 1696 | 1.3 | 340.44 |
| 14:53:01 | 1695 | 1.2 | 340.47 |
| 14:53:02 | 1694 | 1.2 | 340.49 |
| 14:53:03 | 1695 | 1.2 | 340.51 |
| 14:53:04 | 1696 | 1.2 | 340.52 |
| 14:53:05 | 1696 | 1.1 | 340.54 |
| 14:53:06 | 1696 | 1.1 | 340.56 |
| 14:53:07 | 1695 | 1.1 | 340.58 |
| 14:53:08 | 1695 | 1.1 | 340.60 |
| 14:53:09 | 1696 | 1.1 | 340.62 |
| 14:53:10 | 1696 | 1.1 | 340.64 |
| 14:53:11 | 1696 | 1.1 | 340.65 |
| 14:53:12 | 1695 | 1.1 | 340.67 |
| 14:53:13 | 1695 | 1.1 | 340.69 |
| 14:53:14 | 1695 | 1.1 | 340.71 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:53:15 | 1696 | 1.1 | 340.73 |
| 14:53:16 | 1696 | 1.1 | 340.74 |
| 14:53:17 | 1696 | 1.1 | 340.76 |
| 14:53:18 | 1696 | 1.1 | 340.78 |
| 14:53:19 | 1695 | 1.0 | 340.80 |
| 14:53:20 | 1695 | 1.0 | 340.81 |
| 14:53:21 | 1695 | 1.0 | 340.83 |
| 14:53:22 | 1694 | 1.0 | 340.85 |
| 14:53:23 | 1693 | 1.0 | 340.86 |
| 14:53:24 | 1692 | 1.0 | 340.88 |
| 14:53:25 | 1691 | 0.9 | 340.90 |
| 14:53:26 | 1691 | 0.9 | 340.91 |
| 14:53:27 | 1691 | 0.9 | 340.93 |
| 14:53:28 | 1691 | 0.9 | 340.94 |
| 14:53:29 | 1690 | 0.9 | 340.96 |
| 14:53:30 | 1689 | 0.9 | 340.97 |
| 14:53:31 | 1689 | 0.9 | 340.99 |
| 14:53:32 | 1688 | 0.9 | 341.00 |
| 14:53:33 | 1688 | 0.9 | 341.02 |
| 14:53:34 | 1688 | 0.9 | 341.03 |
| 14:53:35 | 1687 | 0.9 | 341.05 |
| 14:53:36 | 1687 | 0.9 | 341.06 |
| 14:53:37 | 1686 | 0.9 | 341.08 |
| 14:53:38 | 1686 | 0.9 | 341.09 |
| 14:53:39 | 1685 | 0.9 | 341.11 |
| 14:53:40 | 1685 | 0.9 | 341.12 |
| 14:53:41 | 1685 | 0.9 | 341.14 |
| 14:53:42 | 1684 | 0.9 | 341.15 |
| 14:53:43 | 1684 | 0.9 | 341.16 |
| 14:53:44 | 1683 | 0.9 | 341.18 |
| 14:53:45 | 1683 | 0.9 | 341.19 |
| 14:53:46 | 1682 | 0.9 | 341.21 |
| 14:53:47 | 1682 | 0.9 | 341.22 |
| 14:53:48 | 1681 | 0.9 | 341.24 |
| 14:53:49 | 1681 | 0.9 | 341.25 |
| 14:53:50 | 1681 | 0.9 | 341.27 |
| 14:53:51 | 1680 | 0.9 | 341.28 |
| 14:53:52 | 1680 | 0.9 | 341.30 |
| 14:53:53 | 1680 | 0.9 | 341.31 |
| 14:53:54 | 1679 | 0.9 | 341.33 |
| 14:53:55 | 1679 | 0.9 | 341.34 |
| 14:53:56 | 1679 | 0.9 | 341.36 |
| 14:53:57 | 1679 | 0.9 | 341.37 |
| 14:53:58 | 1678 | 0.9 | 341.39 |
| 14:53:59 | 1678 | 0.9 | 341.40 |
| 14:54:00 | 1678 | 0.9 | 341.42 |
| 14:54:01 | 1677 | 0.9 | 341.43 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:54:02 | 1677 | 0.9 | 341.45 |
| 14:54:03 | 1677 | 0.9 | 341.46 |
| 14:54:04 | 1676 | 0.9 | 341.48 |
| 14:54:05 | 1676 | 0.9 | 341.49 |
| 14:54:06 | 1676 | 0.9 | 341.51 |
| 14:54:07 | 1675 | 0.9 | 341.52 |
| 14:54:08 | 1675 | 0.9 | 341.54 |
| 14:54:09 | 1675 | 0.9 | 341.55 |
| 14:54:10 | 1675 | 0.9 | 341.57 |
| 14:54:11 | 1674 | 0.9 | 341.58 |
| 14:54:12 | 1674 | 0.9 | 341.60 |
| 14:54:13 | 1674 | 0.9 | 341.61 |
| 14:54:14 | 1674 | 0.9 | 341.63 |
| 14:54:15 | 1673 | 0.9 | 341.64 |
| 14:54:16 | 1673 | 0.9 | 341.66 |
| 14:54:17 | 1673 | 0.9 | 341.67 |
| 14:54:18 | 1672 | 0.9 | 341.69 |
| 14:54:19 | 1672 | 0.9 | 341.70 |
| 14:54:20 | 1672 | 0.9 | 341.72 |
| 14:54:21 | 1672 | 0.9 | 341.73 |
| 14:54:22 | 1672 | 0.9 | 341.75 |
| 14:54:23 | 1672 | 0.9 | 341.76 |
| 14:54:24 | 1671 | 0.9 | 341.78 |
| 14:54:25 | 1671 | 0.9 | 341.79 |
| 14:54:26 | 1671 | 0.9 | 341.81 |
| 14:54:27 | 1671 | 0.9 | 341.82 |
| 14:54:28 | 1671 | 0.9 | 341.84 |
| 14:54:29 | 1670 | 0.9 | 341.85 |
| 14:54:30 | 1670 | 0.9 | 341.87 |
| 14:54:31 | 1670 | 0.9 | 341.88 |
| 14:54:32 | 1669 | 0.9 | 341.90 |
| 14:54:33 | 1669 | 0.9 | 341.91 |
| 14:54:34 | 1669 | 0.9 | 341.93 |
| 14:54:35 | 1669 | 0.9 | 341.94 |
| 14:54:36 | 1669 | 0.9 | 341.96 |
| 14:54:37 | 1669 | 0.9 | 341.97 |
| 14:54:38 | 1668 | 0.9 | 341.99 |
| 14:54:39 | 1668 | 0.9 | 342.00 |
| 14:54:40 | 1668 | 0.9 | 342.02 |
| 14:54:41 | 1668 | 0.9 | 342.03 |
| 14:54:42 | 1668 | 0.9 | 342.05 |
| 14:54:43 | 1668 | 0.9 | 342.06 |
| 14:54:44 | 1668 | 0.9 | 342.08 |
| 14:54:45 | 1667 | 0.9 | 342.09 |
| 14:54:46 | 1667 | 0.9 | 342.11 |
| 14:54:47 | 1667 | 0.9 | 342.12 |
| 14:54:48 | 1667 | 0.9 | 342.14 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:54:49 | 1667 | 0.9 | 342.15 |
| 14:54:50 | 1667 | 0.9 | 342.17 |
| 14:54:51 | 1666 | 0.9 | 342.18 |
| 14:54:52 | 1666 | 0.9 | 342.20 |
| 14:54:53 | 1666 | 0.9 | 342.21 |
| 14:54:54 | 1666 | 0.9 | 342.23 |
| 14:54:55 | 1666 | 0.9 | 342.24 |
| 14:54:56 | 1665 | 0.9 | 342.26 |
| 14:54:57 | 1665 | 0.9 | 342.27 |
| 14:54:58 | 1665 | 0.9 | 342.29 |
| 14:54:59 | 1665 | 0.9 | 342.30 |
| 14:55:00 | 1665 | 0.9 | 342.32 |
| 14:55:01 | 1665 | 0.9 | 342.33 |
| 14:55:02 | 1665 | 0.9 | 342.35 |
| 14:55:03 | 1665 | 0.9 | 342.36 |
| 14:55:04 | 1665 | 0.9 | 342.38 |
| 14:55:05 | 1665 | 0.9 | 342.39 |
| 14:55:06 | 1664 | 0.9 | 342.41 |
| 14:55:07 | 1664 | 0.9 | 342.42 |
| 14:55:08 | 1664 | 0.9 | 342.44 |
| 14:55:09 | 1664 | 0.9 | 342.45 |
| 14:55:10 | 1664 | 0.9 | 342.47 |
| 14:55:11 | 1664 | 0.9 | 342.48 |
| 14:55:12 | 1664 | 0.9 | 342.50 |
| 14:55:13 | 1663 | 0.9 | 342.51 |
| 14:55:14 | 1663 | 0.9 | 342.53 |
| 14:55:15 | 1663 | 0.9 | 342.54 |
| 14:55:16 | 1663 | 0.9 | 342.56 |
| 14:55:17 | 1663 | 0.9 | 342.57 |
| 14:55:18 | 1663 | 0.9 | 342.59 |
| 14:55:19 | 1663 | 0.9 | 342.60 |
| 14:55:20 | 1663 | 0.9 | 342.62 |
| 14:55:21 | 1662 | 0.9 | 342.63 |
| 14:55:22 | 1662 | 0.9 | 342.65 |
| 14:55:23 | 1662 | 0.9 | 342.66 |
| 14:55:24 | 1662 | 0.9 | 342.68 |
| 14:55:25 | 1662 | 0.9 | 342.69 |
| 14:55:26 | 1662 | 0.9 | 342.71 |
| 14:55:27 | 1662 | 0.9 | 342.72 |
| 14:55:28 | 1662 | 0.9 | 342.74 |
| 14:55:29 | 1662 | 0.9 | 342.75 |
| 14:55:30 | 1661 | 0.9 | 342.77 |
| 14:55:31 | 1661 | 0.9 | 342.78 |
| 14:55:32 | 1661 | 0.9 | 342.80 |
| 14:55:33 | 1661 | 0.9 | 342.81 |
| 14:55:34 | 1661 | 0.9 | 342.83 |
| 14:55:35 | 1661 | 0.9 | 342.84 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:55:36 | 1661 | 0.9 | 342.86 |
| 14:55:37 | 1661 | 0.9 | 342.87 |
| 14:55:38 | 1661 | 0.9 | 342.89 |
| 14:55:39 | 1661 | 0.9 | 342.90 |
| 14:55:40 | 1661 | 0.9 | 342.92 |
| 14:55:41 | 1661 | 0.9 | 342.93 |
| 14:55:42 | 1660 | 0.9 | 342.95 |
| 14:55:43 | 1660 | 0.9 | 342.96 |
| 14:55:44 | 1660 | 0.9 | 342.98 |
| 14:55:45 | 1660 | 0.9 | 342.99 |
| 14:55:46 | 1660 | 0.9 | 343.01 |
| 14:55:47 | 1660 | 0.9 | 343.02 |
| 14:55:48 | 1660 | 0.9 | 343.04 |
| 14:55:49 | 1660 | 0.9 | 343.05 |
| 14:55:50 | 1660 | 0.9 | 343.07 |
| 14:55:51 | 1659 | 0.9 | 343.08 |
| 14:55:52 | 1659 | 0.9 | 343.10 |
| 14:55:53 | 1659 | 0.9 | 343.11 |
| 14:55:54 | 1659 | 0.9 | 343.13 |
| 14:55:55 | 1659 | 0.9 | 343.14 |
| 14:55:56 | 1659 | 0.9 | 343.16 |
| 14:55:57 | 1659 | 0.9 | 343.17 |
| 14:55:58 | 1659 | 0.9 | 343.19 |
| 14:55:59 | 1659 | 0.9 | 343.20 |
| 14:56:00 | 1659 | 0.9 | 343.22 |
| 14:56:01 | 1659 | 0.9 | 343.23 |
| 14:56:02 | 1659 | 0.9 | 343.25 |
| 14:56:03 | 1659 | 0.9 | 343.26 |
| 14:56:04 | 1659 | 0.9 | 343.28 |
| 14:56:05 | 1659 | 0.9 | 343.29 |
| 14:56:06 | 1659 | 0.9 | 343.31 |
| 14:56:07 | 1659 | 0.9 | 343.32 |
| 14:56:08 | 1658 | 0.9 | 343.34 |
| 14:56:09 | 1658 | 0.9 | 343.35 |
| 14:56:10 | 1658 | 0.9 | 343.37 |
| 14:56:11 | 1658 | 0.9 | 343.38 |
| 14:56:12 | 1658 | 0.9 | 343.40 |
| 14:56:13 | 1658 | 0.9 | 343.42 |
| 14:56:14 | 1658 | 0.9 | 343.43 |
| 14:56:15 | 1658 | 0.9 | 343.45 |
| 14:56:16 | 1658 | 0.9 | 343.46 |
| 14:56:17 | 1658 | 0.9 | 343.48 |
| 14:56:18 | 1658 | 0.9 | 343.49 |
| 14:56:19 | 1658 | 0.9 | 343.51 |
| 14:56:20 | 1659 | 0.9 | 343.52 |
| 14:56:21 | 1659 | 0.9 | 343.54 |
| 14:56:22 | 1659 | 1.0 | 343.55 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:56:23 | 1659 | 1.0 | 343.57 |
| 14:56:24 | 1659 | 1.0 | 343.59 |
| 14:56:25 | 1659 | 1.0 | 343.60 |
| 14:56:26 | 1659 | 1.0 | 343.62 |
| 14:56:27 | 1659 | 1.0 | 343.63 |
| 14:56:28 | 1659 | 1.0 | 343.65 |
| 14:56:29 | 1659 | 1.0 | 343.67 |
| 14:56:30 | 1660 | 1.0 | 343.68 |
| 14:56:31 | 1660 | 1.0 | 343.70 |
| 14:56:32 | 1660 | 1.0 | 343.72 |
| 14:56:33 | 1660 | 1.0 | 343.73 |
| 14:56:34 | 1660 | 1.0 | 343.75 |
| 14:56:35 | 1660 | 1.0 | 343.77 |
| 14:56:36 | 1661 | 1.0 | 343.78 |
| 14:56:37 | 1661 | 1.0 | 343.80 |
| 14:56:38 | 1661 | 1.0 | 343.82 |
| 14:56:39 | 1661 | 1.0 | 343.83 |
| 14:56:40 | 1661 | 1.0 | 343.85 |
| 14:56:41 | 1662 | 1.0 | 343.87 |
| 14:56:42 | 1662 | 1.0 | 343.88 |
| 14:56:43 | 1662 | 1.0 | 343.90 |
| 14:56:44 | 1662 | 1.0 | 343.92 |
| 14:56:45 | 1662 | 1.0 | 343.93 |
| 14:56:46 | 1663 | 1.0 | 343.95 |
| 14:56:47 | 1663 | 1.0 | 343.97 |
| 14:56:48 | 1663 | 1.0 | 343.98 |
| 14:56:49 | 1663 | 1.0 | 344.00 |
| 14:56:50 | 1663 | 1.0 | 344.02 |
| 14:56:51 | 1663 | 1.0 | 344.03 |
| 14:56:52 | 1663 | 1.0 | 344.05 |
| 14:56:53 | 1663 | 1.0 | 344.07 |
| 14:56:54 | 1664 | 1.0 | 344.08 |
| 14:56:55 | 1664 | 1.0 | 344.10 |
| 14:56:56 | 1664 | 1.0 | 344.12 |
| 14:56:57 | 1664 | 1.0 | 344.13 |
| 14:56:58 | 1664 | 1.0 | 344.15 |
| 14:56:59 | 1664 | 1.0 | 344.17 |
| 14:57:00 | 1664 | 1.0 | 344.18 |
| 14:57:01 | 1664 | 1.0 | 344.20 |
| 14:57:02 | 1664 | 1.0 | 344.22 |
| 14:57:03 | 1664 | 1.0 | 344.23 |
| 14:57:04 | 1664 | 1.0 | 344.25 |
| 14:57:05 | 1664 | 1.0 | 344.27 |
| 14:57:06 | 1664 | 1.0 | 344.28 |
| 14:57:07 | 1664 | 1.0 | 344.30 |
| 14:57:08 | 1665 | 1.0 | 344.32 |
| 14:57:09 | 1665 | 1.0 | 344.33 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:57:10 | 1665 | 1.0 | 344.35 |
| 14:57:11 | 1665 | 1.0 | 344.37 |
| 14:57:12 | 1665 | 1.0 | 344.38 |
| 14:57:13 | 1665 | 1.0 | 344.40 |
| 14:57:14 | 1666 | 1.0 | 344.42 |
| 14:57:15 | 1666 | 1.0 | 344.43 |
| 14:57:16 | 1666 | 1.0 | 344.45 |
| 14:57:17 | 1666 | 1.0 | 344.47 |
| 14:57:18 | 1666 | 1.0 | 344.48 |
| 14:57:19 | 1666 | 1.0 | 344.50 |
| 14:57:20 | 1666 | 1.0 | 344.52 |
| 14:57:21 | 1666 | 1.0 | 344.53 |
| 14:57:22 | 1666 | 1.0 | 344.55 |
| 14:57:23 | 1666 | 1.0 | 344.57 |
| 14:57:24 | 1667 | 1.0 | 344.58 |
| 14:57:25 | 1667 | 1.0 | 344.60 |
| 14:57:26 | 1667 | 1.0 | 344.62 |
| 14:57:27 | 1667 | 1.0 | 344.63 |
| 14:57:28 | 1667 | 1.0 | 344.65 |
| 14:57:29 | 1667 | 1.0 | 344.67 |
| 14:57:30 | 1667 | 1.0 | 344.68 |
| 14:57:31 | 1667 | 1.0 | 344.70 |
| 14:57:32 | 1667 | 1.0 | 344.72 |
| 14:57:33 | 1667 | 1.0 | 344.73 |
| 14:57:34 | 1668 | 1.0 | 344.75 |
| 14:57:35 | 1668 | 1.0 | 344.76 |
| 14:57:36 | 1668 | 1.0 | 344.78 |
| 14:57:37 | 1668 | 1.0 | 344.80 |
| 14:57:38 | 1668 | 1.0 | 344.81 |
| 14:57:39 | 1668 | 1.0 | 344.83 |
| 14:57:40 | 1668 | 1.0 | 344.85 |
| 14:57:41 | 1668 | 1.0 | 344.86 |
| 14:57:42 | 1668 | 1.0 | 344.88 |
| 14:57:43 | 1668 | 1.0 | 344.90 |
| 14:57:44 | 1669 | 1.0 | 344.91 |
| 14:57:45 | 1668 | 1.0 | 344.93 |
| 14:57:46 | 1669 | 1.0 | 344.95 |
| 14:57:47 | 1669 | 1.0 | 344.96 |
| 14:57:48 | 1669 | 1.0 | 344.98 |
| 14:57:49 | 1669 | 1.0 | 345.00 |
| 14:57:50 | 1669 | 1.0 | 345.01 |
| 14:57:51 | 1669 | 1.0 | 345.03 |
| 14:57:52 | 1669 | 1.0 | 345.05 |
| 14:57:53 | 1669 | 1.0 | 345.06 |
| 14:57:54 | 1669 | 1.0 | 345.08 |
| 14:57:55 | 1670 | 1.0 | 345.10 |
| 14:57:56 | 1669 | 1.0 | 345.11 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:57:57 | 1670 | 1.0 | 345.13 |
| 14:57:58 | 1670 | 1.0 | 345.15 |
| 14:57:59 | 1670 | 1.0 | 345.16 |
| 14:58:00 | 1670 | 1.0 | 345.18 |
| 14:58:01 | 1670 | 1.0 | 345.20 |
| 14:58:02 | 1670 | 1.0 | 345.21 |
| 14:58:03 | 1670 | 1.0 | 345.23 |
| 14:58:04 | 1670 | 1.0 | 345.25 |
| 14:58:05 | 1669 | 1.0 | 345.26 |
| 14:58:06 | 1669 | 1.0 | 345.28 |
| 14:58:07 | 1669 | 1.0 | 345.30 |
| 14:58:08 | 1669 | 1.0 | 345.31 |
| 14:58:09 | 1669 | 1.0 | 345.33 |
| 14:58:10 | 1669 | 1.0 | 345.35 |
| 14:58:11 | 1670 | 1.0 | 345.36 |
| 14:58:12 | 1670 | 1.0 | 345.38 |
| 14:58:13 | 1670 | 1.0 | 345.40 |
| 14:58:14 | 1670 | 1.0 | 345.41 |
| 14:58:15 | 1670 | 1.0 | 345.43 |
| 14:58:16 | 1670 | 1.0 | 345.45 |
| 14:58:17 | 1670 | 1.0 | 345.46 |
| 14:58:18 | 1670 | 1.0 | 345.48 |
| 14:58:19 | 1670 | 1.0 | 345.50 |
| 14:58:20 | 1670 | 1.0 | 345.51 |
| 14:58:21 | 1671 | 1.0 | 345.53 |
| 14:58:22 | 1671 | 1.0 | 345.55 |
| 14:58:23 | 1671 | 1.0 | 345.56 |
| 14:58:24 | 1671 | 1.0 | 345.58 |
| 14:58:25 | 1671 | 1.0 | 345.60 |
| 14:58:26 | 1671 | 1.0 | 345.61 |
| 14:58:27 | 1671 | 1.0 | 345.63 |
| 14:58:28 | 1671 | 1.0 | 345.65 |
| 14:58:29 | 1671 | 1.0 | 345.66 |
| 14:58:30 | 1671 | 1.0 | 345.68 |
| 14:58:31 | 1671 | 1.0 | 345.70 |
| 14:58:32 | 1671 | 1.0 | 345.71 |
| 14:58:33 | 1671 | 1.0 | 345.73 |
| 14:58:34 | 1671 | 1.0 | 345.75 |
| 14:58:35 | 1671 | 1.0 | 345.76 |
| 14:58:36 | 1672 | 1.0 | 345.78 |
| 14:58:37 | 1672 | 1.0 | 345.80 |
| 14:58:38 | 1672 | 1.0 | 345.81 |
| 14:58:39 | 1672 | 1.0 | 345.83 |
| 14:58:40 | 1672 | 1.0 | 345.85 |
| 14:58:41 | 1672 | 1.0 | 345.86 |
| 14:58:42 | 1672 | 1.0 | 345.88 |
| 14:58:43 | 1672 | 1.0 | 345.89 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:58:44 | 1672 | 1.0 | 345.91 |
| 14:58:45 | 1672 | 1.0 | 345.93 |
| 14:58:46 | 1672 | 1.0 | 345.94 |
| 14:58:47 | 1672 | 1.0 | 345.96 |
| 14:58:48 | 1672 | 1.0 | 345.98 |
| 14:58:49 | 1672 | 1.0 | 345.99 |
| 14:58:50 | 1672 | 1.0 | 346.01 |
| 14:58:51 | 1672 | 1.0 | 346.03 |
| 14:58:52 | 1673 | 1.0 | 346.04 |
| 14:58:53 | 1673 | 1.0 | 346.06 |
| 14:58:54 | 1673 | 1.0 | 346.08 |
| 14:58:55 | 1673 | 1.0 | 346.09 |
| 14:58:56 | 1673 | 1.0 | 346.11 |
| 14:58:57 | 1673 | 1.0 | 346.13 |
| 14:58:58 | 1673 | 1.0 | 346.14 |
| 14:58:59 | 1673 | 1.0 | 346.16 |
| 14:59:00 | 1673 | 1.0 | 346.18 |
| 14:59:01 | 1673 | 1.0 | 346.19 |
| 14:59:02 | 1673 | 1.0 | 346.21 |
| 14:59:03 | 1673 | 1.0 | 346.23 |
| 14:59:04 | 1673 | 1.0 | 346.24 |
| 14:59:05 | 1673 | 1.0 | 346.26 |
| 14:59:06 | 1673 | 1.0 | 346.28 |
| 14:59:07 | 1673 | 1.0 | 346.29 |
| 14:59:08 | 1673 | 1.0 | 346.31 |
| 14:59:09 | 1673 | 1.0 | 346.33 |
| 14:59:10 | 1673 | 1.0 | 346.34 |
| 14:59:11 | 1673 | 1.0 | 346.36 |
| 14:59:12 | 1674 | 1.0 | 346.38 |
| 14:59:13 | 1674 | 1.0 | 346.39 |
| 14:59:14 | 1674 | 1.0 | 346.41 |
| 14:59:15 | 1674 | 1.0 | 346.43 |
| 14:59:16 | 1674 | 1.0 | 346.44 |
| 14:59:17 | 1674 | 1.0 | 346.46 |
| 14:59:18 | 1674 | 1.0 | 346.48 |
| 14:59:19 | 1674 | 1.0 | 346.49 |
| 14:59:20 | 1674 | 1.0 | 346.51 |
| 14:59:21 | 1673 | 1.0 | 346.53 |
| 14:59:22 | 1673 | 1.0 | 346.54 |
| 14:59:23 | 1673 | 1.0 | 346.56 |
| 14:59:24 | 1673 | 1.0 | 346.58 |
| 14:59:25 | 1674 | 1.0 | 346.59 |
| 14:59:26 | 1674 | 1.0 | 346.61 |
| 14:59:27 | 1674 | 1.0 | 346.63 |
| 14:59:28 | 1674 | 1.0 | 346.64 |
| 14:59:29 | 1674 | 1.0 | 346.66 |
| 14:59:30 | 1674 | 1.0 | 346.68 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 14:59:31 | 1674 | 1.0 | 346.69 |
| 14:59:32 | 1674 | 1.0 | 346.71 |
| 14:59:33 | 1674 | 1.0 | 346.73 |
| 14:59:34 | 1674 | 1.0 | 346.74 |
| 14:59:35 | 1674 | 1.0 | 346.76 |
| 14:59:36 | 1674 | 1.0 | 346.78 |
| 14:59:37 | 1674 | 1.0 | 346.79 |
| 14:59:38 | 1674 | 1.0 | 346.81 |
| 14:59:39 | 1674 | 1.0 | 346.82 |
| 14:59:40 | 1674 | 1.0 | 346.84 |
| 14:59:41 | 1675 | 1.0 | 346.86 |
| 14:59:42 | 1675 | 1.0 | 346.87 |
| 14:59:43 | 1675 | 1.0 | 346.89 |
| 14:59:44 | 1675 | 1.0 | 346.91 |
| 14:59:45 | 1675 | 1.0 | 346.92 |
| 14:59:46 | 1675 | 1.0 | 346.94 |
| 14:59:47 | 1675 | 1.0 | 346.96 |
| 14:59:48 | 1675 | 1.0 | 346.97 |
| 14:59:49 | 1675 | 1.0 | 346.99 |
| 14:59:50 | 1675 | 1.0 | 347.01 |
| 14:59:51 | 1675 | 1.0 | 347.02 |
| 14:59:52 | 1675 | 1.0 | 347.04 |
| 14:59:53 | 1675 | 1.0 | 347.06 |
| 14:59:54 | 1676 | 1.0 | 347.07 |
| 14:59:55 | 1676 | 1.0 | 347.09 |
| 14:59:56 | 1676 | 1.0 | 347.11 |
| 14:59:57 | 1676 | 1.0 | 347.12 |
| 14:59:58 | 1676 | 1.0 | 347.14 |
| 14:59:59 | 1676 | 1.0 | 347.16 |
| 15:00:00 | 1676 | 1.0 | 347.17 |
| 15:00:01 | 1676 | 1.0 | 347.19 |
| 15:00:02 | 1676 | 1.0 | 347.21 |
| 15:00:03 | 1676 | 1.0 | 347.22 |
| 15:00:04 | 1676 | 1.0 | 347.24 |
| 15:00:05 | 1676 | 1.0 | 347.26 |
| 15:00:06 | 1676 | 1.0 | 347.27 |
| 15:00:07 | 1676 | 1.0 | 347.29 |
| 15:00:08 | 1677 | 1.0 | 347.31 |
| 15:00:09 | 1677 | 1.0 | 347.32 |
| 15:00:10 | 1677 | 1.0 | 347.34 |
| 15:00:11 | 1677 | 1.0 | 347.36 |
| 15:00:12 | 1677 | 1.0 | 347.37 |
| 15:00:13 | 1677 | 1.0 | 347.39 |
| 15:00:14 | 1677 | 1.0 | 347.41 |
| 15:00:15 | 1677 | 1.0 | 347.42 |
| 15:00:16 | 1677 | 1.0 | 347.44 |
| 15:00:17 | 1677 | 1.0 | 347.46 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:00:18 | 1677 | 1.0 | 347.47 |
| 15:00:19 | 1677 | 1.0 | 347.49 |
| 15:00:20 | 1677 | 1.0 | 347.51 |
| 15:00:21 | 1677 | 1.0 | 347.52 |
| 15:00:22 | 1677 | 1.0 | 347.54 |
| 15:00:23 | 1677 | 1.0 | 347.56 |
| 15:00:24 | 1677 | 1.0 | 347.57 |
| 15:00:25 | 1677 | 1.0 | 347.59 |
| 15:00:26 | 1677 | 1.0 | 347.61 |
| 15:00:27 | 1677 | 1.0 | 347.62 |
| 15:00:28 | 1677 | 1.0 | 347.64 |
| 15:00:29 | 1677 | 1.0 | 347.66 |
| 15:00:30 | 1677 | 1.0 | 347.67 |
| 15:00:31 | 1676 | 1.0 | 347.69 |
| 15:00:32 | 1670 | 0.6 | 347.70 |
| 15:00:33 | 1667 | 0.6 | 347.71 |
| 15:00:34 | 1663 | 0.4 | 347.72 |
| 15:00:35 | 1667 | 0.4 | 347.72 |
| 15:00:36 | 1667 | 0.3 | 347.73 |
| 15:00:37 | 1670 | 0.4 | 347.73 |
| 15:00:38 | 1665 | 0.4 | 347.74 |
| 15:00:39 | 1663 | 0.4 | 347.75 |
| 15:00:40 | 1660 | 0.4 | 347.75 |
| 15:00:41 | 1662 | 0.5 | 347.76 |
| 15:00:42 | 1665 | 0.5 | 347.77 |
| 15:00:43 | 1664 | 0.6 | 347.78 |
| 15:00:44 | 1664 | 0.6 | 347.79 |
| 15:00:45 | 1655 | 0.7 | 347.80 |
| 15:00:46 | 1650 | 0.6 | 347.81 |
| 15:00:47 | 1650 | 0.7 | 347.82 |
| 15:00:48 | 1652 | 0.6 | 347.83 |
| 15:00:49 | 1653 | 0.7 | 347.84 |
| 15:00:50 | 1654 | 0.6 | 347.85 |
| 15:00:51 | 1649 | 0.7 | 347.86 |
| 15:00:52 | 1651 | 0.6 | 347.88 |
| 15:00:53 | 1649 | 0.7 | 347.89 |
| 15:00:54 | 1651 | 0.6 | 347.90 |
| 15:00:55 | 1649 | 0.7 | 347.91 |
| 15:00:56 | 1649 | 0.7 | 347.92 |
| 15:00:57 | 1647 | 0.7 | 347.93 |
| 15:00:58 | 1644 | 0.5 | 347.94 |
| 15:00:59 | 1638 | 0.3 | 347.95 |
| 15:01:00 | 1633 | 0.2 | 347.95 |
| 15:01:01 | 1633 | 0.2 | 347.95 |
| 15:01:02 | 1635 | 0.1 | 347.96 |
| 15:01:03 | 1636 | 0.1 | 347.96 |
| 15:01:04 | 1634 | 0.1 | 347.96 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:01:05 | 1630 | 0.1 | 347.96 |
| 15:01:06 | 1627 | 0.0 | 347.96 |
| 15:01:07 | 1626 | 0.0 | 347.96 |
| 15:01:08 | 1627 | 0.0 | 347.96 |
| 15:01:09 | 1626 | 0.0 | 347.96 |
| 15:01:10 | 1624 | 0.0 | 347.96 |
| 15:01:11 | 1620 | 0.0 | 347.96 |
| 15:01:12 | 1618 | 0.0 | 347.96 |
| 15:01:13 | 1617 | 0.0 | 347.96 |
| 15:01:14 | 1617 | 0.0 | 347.96 |
| 15:01:15 | 1615 | 0.0 | 347.96 |
| 15:01:16 | 1613 | 0.0 | 347.96 |
| 15:01:17 | 1611 | 0.0 | 347.96 |
| 15:01:18 | 1609 | 0.0 | 347.96 |
| 15:01:19 | 1607 | 0.0 | 347.96 |
| 15:01:20 | 1606 | 0.0 | 347.96 |
| 15:01:21 | 1605 | 0.0 | 347.96 |
| 15:01:22 | 1603 | 0.0 | 347.96 |
| 15:01:23 | 1601 | 0.0 | 347.96 |
| 15:01:24 | 1599 | 0.0 | 347.96 |
| 15:01:25 | 1597 | 0.0 | 347.96 |
| 15:01:26 | 1596 | 0.0 | 347.96 |
| 15:01:27 | 1594 | 0.0 | 347.96 |
| 15:01:28 | 1593 | 0.0 | 347.96 |
| 15:01:29 | 1591 | 0.0 | 347.96 |
| 15:01:30 | 1589 | 0.0 | 347.96 |
| 15:01:31 | 1588 | 0.0 | 347.96 |
| 15:01:32 | 1586 | 0.0 | 347.96 |
| 15:01:33 | 1584 | 0.0 | 347.96 |
| 15:01:34 | 1583 | 0.0 | 347.96 |
| 15:01:35 | 1581 | 0.0 | 347.96 |
| 15:01:36 | 1580 | 0.0 | 347.96 |
| 15:01:37 | 1578 | 0.0 | 347.96 |
| 15:01:38 | 1577 | 0.0 | 347.96 |
| 15:01:39 | 1576 | 0.0 | 347.96 |
| 15:01:40 | 1574 | 0.0 | 347.96 |
| 15:01:41 | 1573 | 0.0 | 347.96 |
| 15:01:42 | 1571 | 0.0 | 347.96 |
| 15:01:43 | 1570 | 0.0 | 347.96 |
| 15:01:44 | 1568 | 0.0 | 347.96 |
| 15:01:45 | 1567 | 0.0 | 347.96 |
| 15:01:46 | 1566 | 0.0 | 347.96 |
| 15:01:47 | 1564 | 0.0 | 347.96 |
| 15:01:48 | 1563 | 0.0 | 347.96 |
| 15:01:49 | 1562 | 0.0 | 347.96 |
| 15:01:50 | 1561 | 0.0 | 347.96 |
| 15:01:51 | 1559 | 0.0 | 347.96 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:01:52 | 1558 | 0.0 | 347.96 |
| 15:01:53 | 1557 | 0.0 | 347.96 |
| 15:01:54 | 1555 | 0.0 | 347.96 |
| 15:01:55 | 1554 | 0.0 | 347.96 |
| 15:01:56 | 1553 | 0.0 | 347.96 |
| 15:01:57 | 1552 | 0.0 | 347.96 |
| 15:01:58 | 1551 | 0.0 | 347.96 |
| 15:01:59 | 1549 | 0.0 | 347.96 |
| 15:02:00 | 1548 | 0.0 | 347.96 |
| 15:02:01 | 1547 | 0.0 | 347.96 |
| 15:02:02 | 1546 | 0.0 | 347.96 |
| 15:02:03 | 1545 | 0.0 | 347.96 |
| 15:02:04 | 1544 | 0.0 | 347.96 |
| 15:02:05 | 1543 | 0.0 | 347.96 |
| 15:02:06 | 1542 | 0.0 | 347.96 |
| 15:02:07 | 1541 | 0.0 | 347.96 |
| 15:02:08 | 1540 | 0.0 | 347.96 |
| 15:02:09 | 1539 | 0.0 | 347.96 |
| 15:02:10 | 1537 | 0.0 | 347.96 |
| 15:02:11 | 1536 | 0.0 | 347.96 |
| 15:02:12 | 1535 | 0.0 | 347.96 |
| 15:02:13 | 1534 | 0.0 | 347.96 |
| 15:02:14 | 1533 | 0.0 | 347.96 |
| 15:02:15 | 1532 | 0.0 | 347.96 |
| 15:02:16 | 1531 | 0.0 | 347.96 |
| 15:02:17 | 1530 | 0.0 | 347.96 |
| 15:02:18 | 1529 | 0.0 | 347.96 |
| 15:02:19 | 1528 | 0.0 | 347.96 |
| 15:02:20 | 1527 | 0.0 | 347.96 |
| 15:02:21 | 1526 | 0.0 | 347.96 |
| 15:02:22 | 1525 | 0.0 | 347.96 |
| 15:02:23 | 1524 | 0.0 | 347.96 |
| 15:02:24 | 1523 | 0.0 | 347.96 |
| 15:02:25 | 1522 | 0.0 | 347.96 |
| 15:02:26 | 1521 | 0.0 | 347.96 |
| 15:02:27 | 1520 | 0.0 | 347.96 |
| 15:02:28 | 1519 | 0.0 | 347.96 |
| 15:02:29 | 1520 | 0.0 | 347.96 |
| 15:02:30 | 1523 | 0.2 | 347.97 |
| 15:02:31 | 1525 | 0.3 | 347.97 |
| 15:02:32 | 1525 | 0.3 | 347.98 |
| 15:02:33 | 1522 | 0.4 | 347.98 |
| 15:02:34 | 1520 | 0.5 | 347.99 |
| 15:02:35 | 1521 | 0.5 | 348.00 |
| 15:02:36 | 1523 | 0.6 | 348.01 |
| 15:02:37 | 1524 | 0.6 | 348.02 |
| 15:02:38 | 1523 | 0.6 | 348.03 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:02:39 | 1522 | 0.7 | 348.04 |
| 15:02:40 | 1521 | 0.7 | 348.05 |
| 15:02:41 | 1522 | 0.7 | 348.06 |
| 15:02:42 | 1523 | 0.7 | 348.07 |
| 15:02:43 | 1523 | 0.8 | 348.09 |
| 15:02:44 | 1522 | 0.8 | 348.10 |
| 15:02:45 | 1522 | 0.8 | 348.11 |
| 15:02:46 | 1517 | 0.7 | 348.12 |
| 15:02:47 | 1512 | 0.4 | 348.13 |
| 15:02:48 | 1507 | 0.3 | 348.14 |
| 15:02:49 | 1507 | 0.2 | 348.14 |
| 15:02:50 | 1510 | 0.2 | 348.14 |
| 15:02:51 | 1512 | 0.1 | 348.14 |
| 15:02:52 | 1511 | 0.1 | 348.15 |
| 15:02:53 | 1508 | 0.1 | 348.15 |
| 15:02:54 | 1505 | 0.0 | 348.15 |
| 15:02:55 | 1506 | 0.0 | 348.15 |
| 15:02:56 | 1506 | 0.0 | 348.15 |
| 15:02:57 | 1507 | 0.0 | 348.15 |
| 15:02:58 | 1506 | 0.0 | 348.15 |
| 15:02:59 | 1504 | 0.0 | 348.15 |
| 15:03:00 | 1503 | 0.0 | 348.15 |
| 15:03:01 | 1503 | 0.0 | 348.15 |
| 15:03:02 | 1503 | 0.0 | 348.15 |
| 15:03:03 | 1503 | 0.0 | 348.15 |
| 15:03:04 | 1501 | 0.0 | 348.15 |
| 15:03:05 | 1500 | 0.0 | 348.15 |
| 15:03:06 | 1498 | 0.0 | 348.15 |
| 15:03:07 | 1498 | 0.0 | 348.15 |
| 15:03:08 | 1497 | 0.0 | 348.15 |
| 15:03:09 | 1497 | 0.0 | 348.15 |
| 15:03:10 | 1495 | 0.0 | 348.15 |
| 15:03:11 | 1494 | 0.0 | 348.15 |
| 15:03:12 | 1493 | 0.0 | 348.15 |
| 15:03:13 | 1492 | 0.0 | 348.15 |
| 15:03:14 | 1492 | 0.0 | 348.15 |
| 15:03:15 | 1490 | 0.0 | 348.15 |
| 15:03:16 | 1489 | 0.0 | 348.15 |
| 15:03:17 | 1488 | 0.0 | 348.15 |
| 15:03:18 | 1488 | 0.0 | 348.15 |
| 15:03:19 | 1487 | 0.0 | 348.15 |
| 15:03:20 | 1486 | 0.0 | 348.15 |
| 15:03:21 | 1485 | 0.0 | 348.15 |
| 15:03:22 | 1485 | 0.0 | 348.15 |
| 15:03:23 | 1484 | 0.0 | 348.15 |
| 15:03:24 | 1483 | 0.0 | 348.15 |
| 15:03:25 | 1482 | 0.0 | 348.15 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:03:26 | 1481 | 0.0 | 348.15 |
| 15:03:27 | 1481 | 0.0 | 348.15 |
| 15:03:28 | 1480 | 0.0 | 348.15 |
| 15:03:29 | 1479 | 0.0 | 348.15 |
| 15:03:30 | 1478 | 0.0 | 348.15 |
| 15:03:31 | 1477 | 0.0 | 348.15 |
| 15:03:32 | 1477 | 0.0 | 348.15 |
| 15:03:33 | 1476 | 0.0 | 348.15 |
| 15:03:34 | 1475 | 0.0 | 348.15 |
| 15:03:35 | 1474 | 0.0 | 348.15 |
| 15:03:36 | 1473 | 0.0 | 348.15 |
| 15:03:37 | 1472 | 0.0 | 348.15 |
| 15:03:38 | 1471 | 0.0 | 348.15 |
| 15:03:39 | 1470 | 0.0 | 348.15 |
| 15:03:40 | 1470 | 0.0 | 348.15 |
| 15:03:41 | 1469 | 0.0 | 348.15 |
| 15:03:42 | 1468 | 0.0 | 348.15 |
| 15:03:43 | 1467 | 0.0 | 348.15 |
| 15:03:44 | 1466 | 0.0 | 348.15 |
| 15:03:45 | 1466 | 0.0 | 348.15 |
| 15:03:46 | 1465 | 0.0 | 348.15 |
| 15:03:47 | 1464 | 0.0 | 348.15 |
| 15:03:48 | 1463 | 0.0 | 348.15 |
| 15:03:49 | 1463 | 0.0 | 348.15 |
| 15:03:50 | 1462 | 0.0 | 348.15 |
| 15:03:51 | 1461 | 0.0 | 348.15 |
| 15:03:52 | 1460 | 0.0 | 348.15 |
| 15:03:53 | 1460 | 0.0 | 348.15 |
| 15:03:54 | 1459 | 0.0 | 348.15 |
| 15:03:55 | 1458 | 0.0 | 348.15 |
| 15:03:56 | 1457 | 0.0 | 348.15 |
| 15:03:57 | 1457 | 0.0 | 348.15 |
| 15:03:58 | 1456 | 0.0 | 348.15 |
| 15:03:59 | 1455 | 0.0 | 348.15 |
| 15:04:00 | 1454 | 0.0 | 348.15 |
| 15:04:01 | 1453 | 0.0 | 348.15 |
| 15:04:02 | 1453 | 0.0 | 348.15 |
| 15:04:03 | 1452 | 0.0 | 348.15 |
| 15:04:04 | 1451 | 0.0 | 348.15 |
| 15:04:05 | 1450 | 0.0 | 348.15 |
| 15:04:06 | 1450 | 0.0 | 348.15 |
| 15:04:07 | 1449 | 0.0 | 348.15 |
| 15:04:08 | 1448 | 0.0 | 348.15 |
| 15:04:09 | 1447 | 0.0 | 348.15 |
| 15:04:10 | 1447 | 0.0 | 348.15 |
| 15:04:11 | 1446 | 0.0 | 348.15 |
| 15:04:12 | 1445 | 0.0 | 348.15 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:04:13 | 1445 | 0.0 | 348.15 |
| 15:04:14 | 1444 | 0.0 | 348.15 |
| 15:04:15 | 1443 | 0.0 | 348.15 |
| 15:04:16 | 1442 | 0.0 | 348.15 |
| 15:04:17 | 1442 | 0.0 | 348.15 |
| 15:04:18 | 1441 | 0.0 | 348.15 |
| 15:04:19 | 1440 | 0.0 | 348.15 |
| 15:04:20 | 1440 | 0.0 | 348.15 |
| 15:04:21 | 1439 | 0.0 | 348.15 |
| 15:04:22 | 1438 | 0.0 | 348.15 |
| 15:04:23 | 1437 | 0.0 | 348.15 |
| 15:04:24 | 1436 | 0.0 | 348.15 |
| 15:04:25 | 1436 | 0.0 | 348.15 |
| 15:04:26 | 1435 | 0.0 | 348.15 |
| 15:04:27 | 1434 | 0.0 | 348.15 |
| 15:04:28 | 1433 | 0.0 | 348.15 |
| 15:04:29 | 1433 | 0.0 | 348.15 |
| 15:04:30 | 1432 | 0.0 | 348.15 |
| 15:04:31 | 1431 | 0.0 | 348.15 |
| 15:04:32 | 1431 | 0.0 | 348.15 |
| 15:04:33 | 1430 | 0.0 | 348.15 |
| 15:04:34 | 1433 | 0.1 | 348.15 |
| 15:04:35 | 1438 | 0.4 | 348.16 |
| 15:04:36 | 1443 | 0.5 | 348.17 |
| 15:04:37 | 1443 | 0.6 | 348.18 |
| 15:04:38 | 1440 | 0.7 | 348.19 |
| 15:04:39 | 1437 | 0.7 | 348.20 |
| 15:04:40 | 1439 | 0.8 | 348.21 |
| 15:04:41 | 1442 | 0.8 | 348.23 |
| 15:04:42 | 1445 | 0.8 | 348.24 |
| 15:04:43 | 1444 | 0.9 | 348.25 |
| 15:04:44 | 1442 | 0.9 | 348.27 |
| 15:04:45 | 1442 | 0.9 | 348.28 |
| 15:04:46 | 1444 | 0.9 | 348.30 |
| 15:04:47 | 1445 | 0.9 | 348.31 |
| 15:04:48 | 1446 | 0.9 | 348.33 |
| 15:04:49 | 1446 | 0.9 | 348.34 |
| 15:04:50 | 1446 | 0.9 | 348.36 |
| 15:04:51 | 1447 | 0.9 | 348.37 |
| 15:04:52 | 1448 | 0.9 | 348.39 |
| 15:04:53 | 1450 | 0.9 | 348.41 |
| 15:04:54 | 1451 | 0.9 | 348.42 |
| 15:04:55 | 1451 | 0.9 | 348.44 |
| 15:04:56 | 1452 | 0.9 | 348.45 |
| 15:04:57 | 1454 | 0.9 | 348.47 |
| 15:04:58 | 1455 | 0.9 | 348.48 |
| 15:04:59 | 1457 | 0.9 | 348.50 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:05:00 | 1458 | 0.9 | 348.51 |
| 15:05:01 | 1458 | 0.9 | 348.53 |
| 15:05:02 | 1460 | 0.9 | 348.55 |
| 15:05:03 | 1461 | 1.0 | 348.56 |
| 15:05:04 | 1462 | 1.0 | 348.58 |
| 15:05:05 | 1463 | 1.0 | 348.59 |
| 15:05:06 | 1464 | 1.0 | 348.61 |
| 15:05:07 | 1465 | 1.0 | 348.63 |
| 15:05:08 | 1466 | 1.0 | 348.64 |
| 15:05:09 | 1467 | 1.0 | 348.66 |
| 15:05:10 | 1468 | 1.0 | 348.67 |
| 15:05:11 | 1468 | 1.0 | 348.69 |
| 15:05:12 | 1469 | 1.0 | 348.71 |
| 15:05:13 | 1470 | 1.0 | 348.72 |
| 15:05:14 | 1471 | 1.0 | 348.74 |
| 15:05:15 | 1472 | 1.0 | 348.75 |
| 15:05:16 | 1472 | 1.0 | 348.77 |
| 15:05:17 | 1473 | 1.0 | 348.78 |
| 15:05:18 | 1474 | 1.0 | 348.80 |
| 15:05:19 | 1475 | 1.0 | 348.82 |
| 15:05:20 | 1476 | 1.0 | 348.83 |
| 15:05:21 | 1477 | 1.0 | 348.85 |
| 15:05:22 | 1477 | 1.0 | 348.86 |
| 15:05:23 | 1478 | 1.0 | 348.88 |
| 15:05:24 | 1479 | 1.0 | 348.90 |
| 15:05:25 | 1480 | 1.0 | 348.91 |
| 15:05:26 | 1481 | 1.0 | 348.93 |
| 15:05:27 | 1482 | 1.0 | 348.94 |
| 15:05:28 | 1482 | 1.0 | 348.96 |
| 15:05:29 | 1483 | 1.0 | 348.98 |
| 15:05:30 | 1483 | 1.0 | 348.99 |
| 15:05:31 | 1484 | 1.0 | 349.01 |
| 15:05:32 | 1484 | 1.0 | 349.02 |
| 15:05:33 | 1485 | 1.0 | 349.04 |
| 15:05:34 | 1486 | 1.0 | 349.05 |
| 15:05:35 | 1486 | 1.0 | 349.07 |
| 15:05:36 | 1487 | 1.0 | 349.09 |
| 15:05:37 | 1488 | 1.0 | 349.10 |
| 15:05:38 | 1488 | 1.0 | 349.12 |
| 15:05:39 | 1489 | 1.0 | 349.13 |
| 15:05:40 | 1490 | 1.0 | 349.15 |
| 15:05:41 | 1490 | 1.0 | 349.17 |
| 15:05:42 | 1491 | 1.0 | 349.18 |
| 15:05:43 | 1492 | 1.0 | 349.20 |
| 15:05:44 | 1492 | 1.0 | 349.21 |
| 15:05:45 | 1493 | 1.0 | 349.23 |
| 15:05:46 | 1493 | 1.0 | 349.25 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:05:47 | 1494 | 1.0 | 349.26 |
| 15:05:48 | 1495 | 1.0 | 349.28 |
| 15:05:49 | 1495 | 1.0 | 349.29 |
| 15:05:50 | 1496 | 1.0 | 349.31 |
| 15:05:51 | 1496 | 1.0 | 349.33 |
| 15:05:52 | 1497 | 1.0 | 349.34 |
| 15:05:53 | 1497 | 1.0 | 349.36 |
| 15:05:54 | 1498 | 1.0 | 349.37 |
| 15:05:55 | 1498 | 1.0 | 349.39 |
| 15:05:56 | 1499 | 1.0 | 349.40 |
| 15:05:57 | 1500 | 1.0 | 349.42 |
| 15:05:58 | 1500 | 1.0 | 349.44 |
| 15:05:59 | 1500 | 1.0 | 349.45 |
| 15:06:00 | 1501 | 1.0 | 349.47 |
| 15:06:01 | 1501 | 1.0 | 349.48 |
| 15:06:02 | 1502 | 1.0 | 349.50 |
| 15:06:03 | 1502 | 1.0 | 349.52 |
| 15:06:04 | 1503 | 1.0 | 349.53 |
| 15:06:05 | 1503 | 1.0 | 349.55 |
| 15:06:06 | 1504 | 1.0 | 349.56 |
| 15:06:07 | 1505 | 1.0 | 349.58 |
| 15:06:08 | 1505 | 1.0 | 349.60 |
| 15:06:09 | 1506 | 1.0 | 349.61 |
| 15:06:10 | 1506 | 1.0 | 349.63 |
| 15:06:11 | 1506 | 1.0 | 349.64 |
| 15:06:12 | 1507 | 1.0 | 349.66 |
| 15:06:13 | 1508 | 1.0 | 349.67 |
| 15:06:14 | 1508 | 1.0 | 349.69 |
| 15:06:15 | 1508 | 1.0 | 349.71 |
| 15:06:16 | 1509 | 1.0 | 349.72 |
| 15:06:17 | 1509 | 1.0 | 349.74 |
| 15:06:18 | 1510 | 1.0 | 349.75 |
| 15:06:19 | 1510 | 1.0 | 349.77 |
| 15:06:20 | 1511 | 1.0 | 349.79 |
| 15:06:21 | 1511 | 1.0 | 349.80 |
| 15:06:22 | 1511 | 1.0 | 349.82 |
| 15:06:23 | 1512 | 1.0 | 349.83 |
| 15:06:24 | 1512 | 1.0 | 349.85 |
| 15:06:25 | 1513 | 1.0 | 349.87 |
| 15:06:26 | 1513 | 1.0 | 349.88 |
| 15:06:27 | 1514 | 1.0 | 349.90 |
| 15:06:28 | 1514 | 1.0 | 349.91 |
| 15:06:29 | 1514 | 1.0 | 349.93 |
| 15:06:30 | 1515 | 1.0 | 349.94 |
| 15:06:31 | 1515 | 1.0 | 349.96 |
| 15:06:32 | 1515 | 1.0 | 349.98 |
| 15:06:33 | 1516 | 1.0 | 349.99 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:06:34 | 1516 | 1.0 | 350.01 |
| 15:06:35 | 1517 | 1.0 | 350.02 |
| 15:06:36 | 1517 | 1.0 | 350.04 |
| 15:06:37 | 1518 | 1.0 | 350.06 |
| 15:06:38 | 1518 | 1.0 | 350.07 |
| 15:06:39 | 1518 | 1.0 | 350.09 |
| 15:06:40 | 1519 | 1.0 | 350.10 |
| 15:06:41 | 1519 | 1.0 | 350.12 |
| 15:06:42 | 1519 | 1.0 | 350.14 |
| 15:06:43 | 1520 | 1.0 | 350.15 |
| 15:06:44 | 1520 | 1.0 | 350.17 |
| 15:06:45 | 1520 | 1.0 | 350.18 |
| 15:06:46 | 1521 | 1.0 | 350.20 |
| 15:06:47 | 1521 | 1.0 | 350.21 |
| 15:06:48 | 1521 | 1.0 | 350.23 |
| 15:06:49 | 1522 | 1.0 | 350.25 |
| 15:06:50 | 1522 | 1.0 | 350.26 |
| 15:06:51 | 1522 | 1.0 | 350.28 |
| 15:06:52 | 1523 | 1.0 | 350.29 |
| 15:06:53 | 1523 | 1.0 | 350.31 |
| 15:06:54 | 1523 | 1.0 | 350.33 |
| 15:06:55 | 1524 | 1.0 | 350.34 |
| 15:06:56 | 1524 | 1.0 | 350.36 |
| 15:06:57 | 1524 | 1.0 | 350.37 |
| 15:06:58 | 1524 | 1.0 | 350.39 |
| 15:06:59 | 1525 | 1.0 | 350.40 |
| 15:07:00 | 1525 | 1.0 | 350.42 |
| 15:07:01 | 1525 | 1.0 | 350.44 |
| 15:07:02 | 1526 | 1.0 | 350.45 |
| 15:07:03 | 1526 | 1.0 | 350.47 |
| 15:07:04 | 1526 | 1.0 | 350.48 |
| 15:07:05 | 1527 | 1.0 | 350.50 |
| 15:07:06 | 1527 | 1.0 | 350.52 |
| 15:07:07 | 1527 | 1.0 | 350.53 |
| 15:07:08 | 1528 | 1.0 | 350.55 |
| 15:07:09 | 1528 | 1.0 | 350.56 |
| 15:07:10 | 1528 | 1.0 | 350.58 |
| 15:07:11 | 1529 | 1.0 | 350.60 |
| 15:07:12 | 1529 | 1.0 | 350.61 |
| 15:07:13 | 1529 | 1.0 | 350.63 |
| 15:07:14 | 1530 | 1.0 | 350.64 |
| 15:07:15 | 1530 | 1.0 | 350.66 |
| 15:07:16 | 1530 | 1.0 | 350.67 |
| 15:07:17 | 1530 | 1.0 | 350.69 |
| 15:07:18 | 1531 | 1.0 | 350.71 |
| 15:07:19 | 1531 | 1.0 | 350.72 |
| 15:07:20 | 1531 | 1.0 | 350.74 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:07:21 | 1531 | 1.0 | 350.75 |
| 15:07:22 | 1532 | 1.0 | 350.77 |
| 15:07:23 | 1532 | 1.0 | 350.79 |
| 15:07:24 | 1533 | 1.0 | 350.80 |
| 15:07:25 | 1533 | 1.0 | 350.82 |
| 15:07:26 | 1533 | 1.0 | 350.83 |
| 15:07:27 | 1533 | 1.0 | 350.85 |
| 15:07:28 | 1533 | 1.0 | 350.87 |
| 15:07:29 | 1533 | 1.0 | 350.88 |
| 15:07:30 | 1534 | 1.0 | 350.90 |
| 15:07:31 | 1534 | 1.0 | 350.91 |
| 15:07:32 | 1534 | 1.0 | 350.93 |
| 15:07:33 | 1535 | 1.0 | 350.94 |
| 15:07:34 | 1535 | 1.0 | 350.96 |
| 15:07:35 | 1536 | 1.0 | 350.98 |
| 15:07:36 | 1536 | 1.0 | 350.99 |
| 15:07:37 | 1536 | 1.0 | 351.01 |
| 15:07:38 | 1536 | 1.0 | 351.02 |
| 15:07:39 | 1536 | 1.0 | 351.04 |
| 15:07:40 | 1537 | 1.0 | 351.06 |
| 15:07:41 | 1537 | 1.0 | 351.07 |
| 15:07:42 | 1537 | 1.0 | 351.09 |
| 15:07:43 | 1537 | 1.0 | 351.10 |
| 15:07:44 | 1537 | 1.0 | 351.12 |
| 15:07:45 | 1538 | 1.0 | 351.14 |
| 15:07:46 | 1538 | 1.0 | 351.15 |
| 15:07:47 | 1538 | 1.0 | 351.17 |
| 15:07:48 | 1539 | 1.0 | 351.18 |
| 15:07:49 | 1539 | 1.0 | 351.20 |
| 15:07:50 | 1539 | 1.0 | 351.21 |
| 15:07:51 | 1539 | 1.0 | 351.23 |
| 15:07:52 | 1540 | 1.0 | 351.25 |
| 15:07:53 | 1540 | 1.0 | 351.26 |
| 15:07:54 | 1540 | 1.0 | 351.28 |
| 15:07:55 | 1540 | 1.0 | 351.29 |
| 15:07:56 | 1540 | 1.0 | 351.31 |
| 15:07:57 | 1540 | 1.0 | 351.33 |
| 15:07:58 | 1541 | 1.0 | 351.34 |
| 15:07:59 | 1541 | 1.0 | 351.36 |
| 15:08:00 | 1541 | 1.0 | 351.37 |
| 15:08:01 | 1542 | 1.0 | 351.39 |
| 15:08:02 | 1542 | 1.0 | 351.41 |
| 15:08:03 | 1542 | 1.0 | 351.42 |
| 15:08:04 | 1543 | 1.0 | 351.44 |
| 15:08:05 | 1543 | 1.0 | 351.45 |
| 15:08:06 | 1543 | 1.0 | 351.47 |
| 15:08:07 | 1543 | 1.0 | 351.48 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:08:08 | 1543 | 1.0 | 351.50 |
| 15:08:09 | 1544 | 1.0 | 351.52 |
| 15:08:10 | 1544 | 1.0 | 351.53 |
| 15:08:11 | 1544 | 1.0 | 351.55 |
| 15:08:12 | 1545 | 1.0 | 351.56 |
| 15:08:13 | 1545 | 1.0 | 351.58 |
| 15:08:14 | 1545 | 1.0 | 351.60 |
| 15:08:15 | 1545 | 1.0 | 351.61 |
| 15:08:16 | 1546 | 1.0 | 351.63 |
| 15:08:17 | 1546 | 1.0 | 351.64 |
| 15:08:18 | 1546 | 1.0 | 351.66 |
| 15:08:19 | 1546 | 1.0 | 351.68 |
| 15:08:20 | 1546 | 1.0 | 351.69 |
| 15:08:21 | 1546 | 1.0 | 351.71 |
| 15:08:22 | 1547 | 1.0 | 351.72 |
| 15:08:23 | 1547 | 1.0 | 351.74 |
| 15:08:24 | 1547 | 1.0 | 351.75 |
| 15:08:25 | 1547 | 1.0 | 351.77 |
| 15:08:26 | 1547 | 1.0 | 351.79 |
| 15:08:27 | 1547 | 1.0 | 351.80 |
| 15:08:28 | 1548 | 1.0 | 351.82 |
| 15:08:29 | 1548 | 1.0 | 351.83 |
| 15:08:30 | 1548 | 1.0 | 351.85 |
| 15:08:31 | 1548 | 1.0 | 351.87 |
| 15:08:32 | 1549 | 1.0 | 351.88 |
| 15:08:33 | 1549 | 1.0 | 351.90 |
| 15:08:34 | 1549 | 1.0 | 351.91 |
| 15:08:35 | 1549 | 1.0 | 351.93 |
| 15:08:36 | 1549 | 1.0 | 351.95 |
| 15:08:37 | 1550 | 1.0 | 351.96 |
| 15:08:38 | 1550 | 1.0 | 351.98 |
| 15:08:39 | 1550 | 1.0 | 351.99 |
| 15:08:40 | 1550 | 1.0 | 352.01 |
| 15:08:41 | 1550 | 1.0 | 352.02 |
| 15:08:42 | 1551 | 1.0 | 352.04 |
| 15:08:43 | 1551 | 1.0 | 352.06 |
| 15:08:44 | 1551 | 1.0 | 352.07 |
| 15:08:45 | 1551 | 1.0 | 352.09 |
| 15:08:46 | 1552 | 1.0 | 352.10 |
| 15:08:47 | 1552 | 1.0 | 352.12 |
| 15:08:48 | 1552 | 1.0 | 352.14 |
| 15:08:49 | 1552 | 1.0 | 352.15 |
| 15:08:50 | 1552 | 1.0 | 352.17 |
| 15:08:51 | 1553 | 1.0 | 352.18 |
| 15:08:52 | 1553 | 1.0 | 352.20 |
| 15:08:53 | 1553 | 1.0 | 352.22 |
| 15:08:54 | 1553 | 1.0 | 352.23 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:08:55 | 1553 | 1.0 | 352.25 |
| 15:08:56 | 1553 | 1.0 | 352.26 |
| 15:08:57 | 1553 | 1.0 | 352.28 |
| 15:08:58 | 1554 | 1.0 | 352.29 |
| 15:08:59 | 1554 | 1.0 | 352.31 |
| 15:09:00 | 1554 | 1.0 | 352.33 |
| 15:09:01 | 1554 | 1.0 | 352.34 |
| 15:09:02 | 1555 | 1.0 | 352.36 |
| 15:09:03 | 1555 | 1.0 | 352.37 |
| 15:09:04 | 1555 | 1.0 | 352.39 |
| 15:09:05 | 1555 | 1.0 | 352.41 |
| 15:09:06 | 1555 | 1.0 | 352.42 |
| 15:09:07 | 1556 | 1.0 | 352.44 |
| 15:09:08 | 1556 | 1.0 | 352.45 |
| 15:09:09 | 1556 | 1.0 | 352.47 |
| 15:09:10 | 1556 | 1.0 | 352.49 |
| 15:09:11 | 1556 | 1.0 | 352.50 |
| 15:09:12 | 1557 | 1.0 | 352.52 |
| 15:09:13 | 1557 | 1.0 | 352.53 |
| 15:09:14 | 1557 | 1.0 | 352.55 |
| 15:09:15 | 1558 | 1.0 | 352.56 |
| 15:09:16 | 1558 | 1.0 | 352.58 |
| 15:09:17 | 1558 | 1.0 | 352.60 |
| 15:09:18 | 1558 | 1.0 | 352.61 |
| 15:09:19 | 1558 | 1.0 | 352.63 |
| 15:09:20 | 1558 | 1.0 | 352.64 |
| 15:09:21 | 1559 | 1.0 | 352.66 |
| 15:09:22 | 1559 | 1.0 | 352.68 |
| 15:09:23 | 1559 | 1.0 | 352.69 |
| 15:09:24 | 1559 | 1.0 | 352.71 |
| 15:09:25 | 1559 | 1.0 | 352.72 |
| 15:09:26 | 1559 | 1.0 | 352.74 |
| 15:09:27 | 1560 | 1.0 | 352.76 |
| 15:09:28 | 1560 | 1.0 | 352.77 |
| 15:09:29 | 1560 | 1.0 | 352.79 |
| 15:09:30 | 1561 | 1.0 | 352.80 |
| 15:09:31 | 1561 | 1.0 | 352.82 |
| 15:09:32 | 1561 | 1.0 | 352.83 |
| 15:09:33 | 1561 | 1.0 | 352.85 |
| 15:09:34 | 1561 | 1.0 | 352.87 |
| 15:09:35 | 1561 | 1.0 | 352.88 |
| 15:09:36 | 1561 | 1.0 | 352.90 |
| 15:09:37 | 1562 | 1.0 | 352.91 |
| 15:09:38 | 1562 | 1.0 | 352.93 |
| 15:09:39 | 1562 | 1.0 | 352.95 |
| 15:09:40 | 1562 | 1.0 | 352.96 |
| 15:09:41 | 1563 | 1.0 | 352.98 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:09:42 | 1563 | 1.0 | 352.99 |
| 15:09:43 | 1563 | 1.0 | 353.01 |
| 15:09:44 | 1563 | 1.0 | 353.03 |
| 15:09:45 | 1563 | 1.0 | 353.04 |
| 15:09:46 | 1563 | 1.0 | 353.06 |
| 15:09:47 | 1563 | 1.0 | 353.07 |
| 15:09:48 | 1564 | 1.0 | 353.09 |
| 15:09:49 | 1564 | 1.0 | 353.10 |
| 15:09:50 | 1564 | 1.0 | 353.12 |
| 15:09:51 | 1564 | 1.0 | 353.14 |
| 15:09:52 | 1565 | 1.0 | 353.15 |
| 15:09:53 | 1565 | 1.0 | 353.17 |
| 15:09:54 | 1565 | 1.0 | 353.18 |
| 15:09:55 | 1565 | 1.0 | 353.20 |
| 15:09:56 | 1565 | 1.0 | 353.22 |
| 15:09:57 | 1565 | 1.0 | 353.23 |
| 15:09:58 | 1566 | 1.0 | 353.25 |
| 15:09:59 | 1566 | 1.0 | 353.26 |
| 15:10:00 | 1566 | 1.0 | 353.28 |
| 15:10:01 | 1566 | 1.0 | 353.30 |
| 15:10:02 | 1566 | 1.0 | 353.31 |
| 15:10:03 | 1566 | 1.0 | 353.33 |
| 15:10:04 | 1566 | 1.0 | 353.34 |
| 15:10:05 | 1567 | 1.0 | 353.36 |
| 15:10:06 | 1567 | 1.0 | 353.37 |
| 15:10:07 | 1567 | 1.0 | 353.39 |
| 15:10:08 | 1567 | 1.0 | 353.41 |
| 15:10:09 | 1568 | 1.0 | 353.42 |
| 15:10:10 | 1568 | 1.0 | 353.44 |
| 15:10:11 | 1568 | 1.0 | 353.45 |
| 15:10:12 | 1568 | 1.0 | 353.47 |
| 15:10:13 | 1568 | 1.0 | 353.49 |
| 15:10:14 | 1568 | 1.0 | 353.50 |
| 15:10:15 | 1568 | 1.0 | 353.52 |
| 15:10:16 | 1569 | 1.0 | 353.53 |
| 15:10:17 | 1569 | 1.0 | 353.55 |
| 15:10:18 | 1569 | 1.0 | 353.57 |
| 15:10:19 | 1569 | 1.0 | 353.58 |
| 15:10:20 | 1569 | 1.0 | 353.60 |
| 15:10:21 | 1570 | 1.0 | 353.61 |
| 15:10:22 | 1570 | 1.0 | 353.63 |
| 15:10:23 | 1570 | 1.0 | 353.64 |
| 15:10:24 | 1570 | 1.0 | 353.66 |
| 15:10:25 | 1570 | 1.0 | 353.68 |
| 15:10:26 | 1570 | 1.0 | 353.69 |
| 15:10:27 | 1570 | 1.0 | 353.71 |
| 15:10:28 | 1570 | 1.0 | 353.72 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:10:29 | 1571 | 1.0 | 353.74 |
| 15:10:30 | 1571 | 1.0 | 353.76 |
| 15:10:31 | 1571 | 1.0 | 353.77 |
| 15:10:32 | 1571 | 1.0 | 353.79 |
| 15:10:33 | 1571 | 1.0 | 353.80 |
| 15:10:34 | 1572 | 1.0 | 353.82 |
| 15:10:35 | 1572 | 1.0 | 353.84 |
| 15:10:36 | 1572 | 1.0 | 353.85 |
| 15:10:37 | 1572 | 1.0 | 353.87 |
| 15:10:38 | 1572 | 1.0 | 353.88 |
| 15:10:39 | 1573 | 1.0 | 353.90 |
| 15:10:40 | 1573 | 1.0 | 353.91 |
| 15:10:41 | 1573 | 1.0 | 353.93 |
| 15:10:42 | 1573 | 1.0 | 353.95 |
| 15:10:43 | 1573 | 1.0 | 353.96 |
| 15:10:44 | 1573 | 1.0 | 353.98 |
| 15:10:45 | 1573 | 1.0 | 353.99 |
| 15:10:46 | 1573 | 1.0 | 354.01 |
| 15:10:47 | 1574 | 1.0 | 354.03 |
| 15:10:48 | 1574 | 1.0 | 354.04 |
| 15:10:49 | 1574 | 1.0 | 354.06 |
| 15:10:50 | 1574 | 1.0 | 354.07 |
| 15:10:51 | 1574 | 1.0 | 354.09 |
| 15:10:52 | 1574 | 1.0 | 354.10 |
| 15:10:53 | 1574 | 1.0 | 354.12 |
| 15:10:54 | 1574 | 1.0 | 354.14 |
| 15:10:55 | 1575 | 1.0 | 354.15 |
| 15:10:56 | 1575 | 1.0 | 354.17 |
| 15:10:57 | 1575 | 1.0 | 354.18 |
| 15:10:58 | 1575 | 1.0 | 354.20 |
| 15:10:59 | 1575 | 1.0 | 354.22 |
| 15:11:00 | 1576 | 1.0 | 354.23 |
| 15:11:01 | 1576 | 1.0 | 354.25 |
| 15:11:02 | 1576 | 1.0 | 354.26 |
| 15:11:03 | 1576 | 1.0 | 354.28 |
| 15:11:04 | 1576 | 1.0 | 354.30 |
| 15:11:05 | 1577 | 1.0 | 354.31 |
| 15:11:06 | 1577 | 1.0 | 354.33 |
| 15:11:07 | 1577 | 1.0 | 354.34 |
| 15:11:08 | 1577 | 1.0 | 354.36 |
| 15:11:09 | 1577 | 1.0 | 354.37 |
| 15:11:10 | 1577 | 1.0 | 354.39 |
| 15:11:11 | 1577 | 1.0 | 354.41 |
| 15:11:12 | 1577 | 1.0 | 354.42 |
| 15:11:13 | 1578 | 1.0 | 354.44 |
| 15:11:14 | 1578 | 1.0 | 354.45 |
| 15:11:15 | 1578 | 1.0 | 354.47 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:11:16 | 1578 | 1.0 | 354.49 |
| 15:11:17 | 1578 | 1.0 | 354.50 |
| 15:11:18 | 1579 | 1.0 | 354.52 |
| 15:11:19 | 1579 | 1.0 | 354.53 |
| 15:11:20 | 1579 | 1.0 | 354.55 |
| 15:11:21 | 1579 | 1.0 | 354.57 |
| 15:11:22 | 1579 | 1.0 | 354.58 |
| 15:11:23 | 1579 | 1.0 | 354.60 |
| 15:11:24 | 1579 | 1.0 | 354.61 |
| 15:11:25 | 1579 | 1.0 | 354.63 |
| 15:11:26 | 1580 | 1.0 | 354.64 |
| 15:11:27 | 1580 | 1.0 | 354.66 |
| 15:11:28 | 1580 | 1.0 | 354.68 |
| 15:11:29 | 1580 | 1.0 | 354.69 |
| 15:11:30 | 1580 | 1.0 | 354.71 |
| 15:11:31 | 1580 | 1.0 | 354.72 |
| 15:11:32 | 1581 | 1.0 | 354.74 |
| 15:11:33 | 1581 | 1.0 | 354.76 |
| 15:11:34 | 1581 | 1.0 | 354.77 |
| 15:11:35 | 1581 | 1.0 | 354.79 |
| 15:11:36 | 1581 | 1.0 | 354.80 |
| 15:11:37 | 1581 | 1.0 | 354.82 |
| 15:11:38 | 1582 | 1.0 | 354.84 |
| 15:11:39 | 1582 | 1.0 | 354.85 |
| 15:11:40 | 1582 | 1.0 | 354.87 |
| 15:11:41 | 1582 | 1.0 | 354.88 |
| 15:11:42 | 1582 | 1.0 | 354.90 |
| 15:11:43 | 1582 | 1.0 | 354.91 |
| 15:11:44 | 1583 | 1.0 | 354.93 |
| 15:11:45 | 1583 | 1.0 | 354.95 |
| 15:11:46 | 1583 | 1.0 | 354.96 |
| 15:11:47 | 1583 | 1.0 | 354.98 |
| 15:11:48 | 1583 | 1.0 | 354.99 |
| 15:11:49 | 1583 | 1.0 | 355.01 |
| 15:11:50 | 1583 | 1.0 | 355.03 |
| 15:11:51 | 1583 | 1.0 | 355.04 |
| 15:11:52 | 1583 | 1.0 | 355.06 |
| 15:11:53 | 1584 | 1.0 | 355.07 |
| 15:11:54 | 1584 | 1.0 | 355.09 |
| 15:11:55 | 1584 | 1.0 | 355.11 |
| 15:11:56 | 1584 | 1.0 | 355.12 |
| 15:11:57 | 1584 | 1.0 | 355.14 |
| 15:11:58 | 1585 | 1.0 | 355.15 |
| 15:11:59 | 1585 | 1.0 | 355.17 |
| 15:12:00 | 1585 | 1.0 | 355.18 |
| 15:12:01 | 1585 | 1.0 | 355.20 |
| 15:12:02 | 1585 | 1.0 | 355.22 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:12:03 | 1586 | 1.0 | 355.23 |
| 15:12:04 | 1586 | 1.0 | 355.25 |
| 15:12:05 | 1586 | 1.0 | 355.26 |
| 15:12:06 | 1586 | 1.0 | 355.28 |
| 15:12:07 | 1586 | 1.0 | 355.30 |
| 15:12:08 | 1586 | 1.0 | 355.31 |
| 15:12:09 | 1586 | 1.0 | 355.33 |
| 15:12:10 | 1586 | 1.0 | 355.34 |
| 15:12:11 | 1586 | 1.0 | 355.36 |
| 15:12:12 | 1587 | 1.0 | 355.38 |
| 15:12:13 | 1587 | 1.0 | 355.39 |
| 15:12:14 | 1587 | 1.0 | 355.41 |
| 15:12:15 | 1587 | 1.0 | 355.42 |
| 15:12:16 | 1587 | 1.0 | 355.44 |
| 15:12:17 | 1587 | 1.0 | 355.45 |
| 15:12:18 | 1587 | 1.0 | 355.47 |
| 15:12:19 | 1587 | 1.0 | 355.49 |
| 15:12:20 | 1587 | 1.0 | 355.50 |
| 15:12:21 | 1588 | 1.0 | 355.52 |
| 15:12:22 | 1588 | 1.0 | 355.53 |
| 15:12:23 | 1588 | 1.0 | 355.55 |
| 15:12:24 | 1588 | 1.0 | 355.57 |
| 15:12:25 | 1588 | 1.0 | 355.58 |
| 15:12:26 | 1588 | 1.0 | 355.60 |
| 15:12:27 | 1589 | 1.0 | 355.61 |
| 15:12:28 | 1589 | 1.0 | 355.63 |
| 15:12:29 | 1589 | 1.0 | 355.64 |
| 15:12:30 | 1589 | 1.0 | 355.66 |
| 15:12:31 | 1589 | 1.0 | 355.68 |
| 15:12:32 | 1589 | 1.0 | 355.69 |
| 15:12:33 | 1589 | 1.0 | 355.71 |
| 15:12:34 | 1589 | 1.0 | 355.72 |
| 15:12:35 | 1590 | 1.0 | 355.74 |
| 15:12:36 | 1590 | 1.0 | 355.76 |
| 15:12:37 | 1590 | 1.0 | 355.77 |
| 15:12:38 | 1590 | 1.0 | 355.79 |
| 15:12:39 | 1590 | 1.0 | 355.80 |
| 15:12:40 | 1590 | 1.0 | 355.82 |
| 15:12:41 | 1590 | 1.0 | 355.84 |
| 15:12:42 | 1590 | 1.0 | 355.85 |
| 15:12:43 | 1591 | 1.0 | 355.87 |
| 15:12:44 | 1590 | 1.0 | 355.88 |
| 15:12:45 | 1591 | 1.0 | 355.90 |
| 15:12:46 | 1591 | 1.0 | 355.91 |
| 15:12:47 | 1591 | 1.0 | 355.93 |
| 15:12:48 | 1591 | 1.0 | 355.95 |
| 15:12:49 | 1591 | 1.0 | 355.96 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:12:50 | 1591 | 1.0 | 355.98 |
| 15:12:51 | 1592 | 1.0 | 355.99 |
| 15:12:52 | 1592 | 1.0 | 356.01 |
| 15:12:53 | 1592 | 1.0 | 356.03 |
| 15:12:54 | 1592 | 1.0 | 356.04 |
| 15:12:55 | 1592 | 1.0 | 356.06 |
| 15:12:56 | 1592 | 1.0 | 356.07 |
| 15:12:57 | 1592 | 1.0 | 356.09 |
| 15:12:58 | 1592 | 1.0 | 356.11 |
| 15:12:59 | 1593 | 1.0 | 356.12 |
| 15:13:00 | 1593 | 1.0 | 356.14 |
| 15:13:01 | 1593 | 1.0 | 356.15 |
| 15:13:02 | 1593 | 1.0 | 356.17 |
| 15:13:03 | 1593 | 1.0 | 356.18 |
| 15:13:04 | 1594 | 1.0 | 356.20 |
| 15:13:05 | 1594 | 1.0 | 356.22 |
| 15:13:06 | 1594 | 1.0 | 356.23 |
| 15:13:07 | 1594 | 1.0 | 356.25 |
| 15:13:08 | 1594 | 1.0 | 356.26 |
| 15:13:09 | 1594 | 1.0 | 356.28 |
| 15:13:10 | 1594 | 1.0 | 356.30 |
| 15:13:11 | 1594 | 1.0 | 356.31 |
| 15:13:12 | 1594 | 1.0 | 356.33 |
| 15:13:13 | 1594 | 1.0 | 356.34 |
| 15:13:14 | 1594 | 1.0 | 356.36 |
| 15:13:15 | 1595 | 1.0 | 356.37 |
| 15:13:16 | 1595 | 1.0 | 356.39 |
| 15:13:17 | 1595 | 1.0 | 356.41 |
| 15:13:18 | 1595 | 1.0 | 356.42 |
| 15:13:19 | 1596 | 1.0 | 356.44 |
| 15:13:20 | 1596 | 1.0 | 356.45 |
| 15:13:21 | 1596 | 1.0 | 356.47 |
| 15:13:22 | 1596 | 1.0 | 356.49 |
| 15:13:23 | 1596 | 1.0 | 356.50 |
| 15:13:24 | 1596 | 1.0 | 356.52 |
| 15:13:25 | 1596 | 1.0 | 356.53 |
| 15:13:26 | 1596 | 1.0 | 356.55 |
| 15:13:27 | 1597 | 1.0 | 356.57 |
| 15:13:28 | 1597 | 1.0 | 356.58 |
| 15:13:29 | 1597 | 1.0 | 356.60 |
| 15:13:30 | 1597 | 1.0 | 356.61 |
| 15:13:31 | 1597 | 1.0 | 356.63 |
| 15:13:32 | 1597 | 1.0 | 356.64 |
| 15:13:33 | 1598 | 1.0 | 356.66 |
| 15:13:34 | 1598 | 1.0 | 356.68 |
| 15:13:35 | 1598 | 1.0 | 356.69 |
| 15:13:36 | 1598 | 1.0 | 356.71 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:13:37 | 1598 | 1.0 | 356.72 |
| 15:13:38 | 1598 | 1.0 | 356.74 |
| 15:13:39 | 1598 | 1.0 | 356.76 |
| 15:13:40 | 1598 | 1.0 | 356.77 |
| 15:13:41 | 1598 | 1.0 | 356.79 |
| 15:13:42 | 1598 | 1.0 | 356.80 |
| 15:13:43 | 1598 | 1.0 | 356.82 |
| 15:13:44 | 1598 | 1.0 | 356.83 |
| 15:13:45 | 1599 | 1.0 | 356.85 |
| 15:13:46 | 1599 | 1.0 | 356.87 |
| 15:13:47 | 1599 | 1.0 | 356.88 |
| 15:13:48 | 1599 | 1.0 | 356.90 |
| 15:13:49 | 1600 | 1.0 | 356.91 |
| 15:13:50 | 1599 | 1.0 | 356.93 |
| 15:13:51 | 1600 | 1.0 | 356.95 |
| 15:13:52 | 1600 | 1.0 | 356.96 |
| 15:13:53 | 1600 | 1.0 | 356.98 |
| 15:13:54 | 1600 | 1.0 | 356.99 |
| 15:13:55 | 1600 | 1.0 | 357.01 |
| 15:13:56 | 1600 | 1.0 | 357.03 |
| 15:13:57 | 1600 | 1.0 | 357.04 |
| 15:13:58 | 1601 | 1.0 | 357.06 |
| 15:13:59 | 1601 | 1.0 | 357.07 |
| 15:14:00 | 1601 | 1.0 | 357.09 |
| 15:14:01 | 1601 | 1.0 | 357.10 |
| 15:14:02 | 1601 | 1.0 | 357.12 |
| 15:14:03 | 1601 | 1.0 | 357.14 |
| 15:14:04 | 1601 | 1.0 | 357.15 |
| 15:14:05 | 1601 | 1.0 | 357.17 |
| 15:14:06 | 1601 | 1.0 | 357.18 |
| 15:14:07 | 1601 | 1.0 | 357.20 |
| 15:14:08 | 1602 | 1.0 | 357.22 |
| 15:14:09 | 1602 | 1.0 | 357.23 |
| 15:14:10 | 1602 | 1.0 | 357.25 |
| 15:14:11 | 1602 | 1.0 | 357.26 |
| 15:14:12 | 1602 | 1.0 | 357.28 |
| 15:14:13 | 1602 | 1.0 | 357.29 |
| 15:14:14 | 1602 | 1.0 | 357.31 |
| 15:14:15 | 1602 | 1.0 | 357.33 |
| 15:14:16 | 1603 | 1.0 | 357.34 |
| 15:14:17 | 1603 | 1.0 | 357.36 |
| 15:14:18 | 1603 | 1.0 | 357.37 |
| 15:14:19 | 1603 | 1.0 | 357.39 |
| 15:14:20 | 1603 | 1.0 | 357.41 |
| 15:14:21 | 1603 | 1.0 | 357.42 |
| 15:14:22 | 1603 | 1.0 | 357.44 |
| 15:14:23 | 1603 | 1.0 | 357.45 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:14:24 | 1603 | 1.0 | 357.47 |
| 15:14:25 | 1603 | 1.0 | 357.49 |
| 15:14:26 | 1604 | 1.0 | 357.50 |
| 15:14:27 | 1604 | 1.0 | 357.52 |
| 15:14:28 | 1604 | 1.0 | 357.53 |
| 15:14:29 | 1604 | 1.0 | 357.55 |
| 15:14:30 | 1604 | 1.0 | 357.56 |
| 15:14:31 | 1604 | 1.0 | 357.58 |
| 15:14:32 | 1604 | 1.0 | 357.60 |
| 15:14:33 | 1604 | 1.0 | 357.61 |
| 15:14:34 | 1604 | 1.0 | 357.63 |
| 15:14:35 | 1604 | 1.0 | 357.64 |
| 15:14:36 | 1604 | 1.0 | 357.66 |
| 15:14:37 | 1604 | 1.0 | 357.68 |
| 15:14:38 | 1605 | 1.0 | 357.69 |
| 15:14:39 | 1605 | 1.0 | 357.71 |
| 15:14:40 | 1605 | 1.0 | 357.72 |
| 15:14:41 | 1605 | 1.0 | 357.74 |
| 15:14:42 | 1605 | 1.0 | 357.75 |
| 15:14:43 | 1605 | 1.0 | 357.77 |
| 15:14:44 | 1605 | 1.0 | 357.79 |
| 15:14:45 | 1605 | 1.0 | 357.80 |
| 15:14:46 | 1605 | 1.0 | 357.82 |
| 15:14:47 | 1605 | 1.0 | 357.83 |
| 15:14:48 | 1605 | 1.0 | 357.85 |
| 15:14:49 | 1605 | 1.0 | 357.87 |
| 15:14:50 | 1605 | 1.0 | 357.88 |
| 15:14:51 | 1605 | 1.0 | 357.90 |
| 15:14:52 | 1605 | 1.0 | 357.91 |
| 15:14:53 | 1606 | 1.0 | 357.93 |
| 15:14:54 | 1606 | 1.0 | 357.95 |
| 15:14:55 | 1606 | 1.0 | 357.96 |
| 15:14:56 | 1606 | 1.0 | 357.98 |
| 15:14:57 | 1606 | 1.0 | 357.99 |
| 15:14:58 | 1606 | 1.0 | 358.01 |
| 15:14:59 | 1606 | 1.0 | 358.02 |
| 15:15:00 | 1606 | 1.0 | 358.04 |
| 15:15:01 | 1606 | 1.0 | 358.06 |
| 15:15:02 | 1606 | 1.0 | 358.07 |
| 15:15:03 | 1607 | 1.0 | 358.09 |
| 15:15:04 | 1607 | 1.0 | 358.10 |
| 15:15:05 | 1607 | 1.0 | 358.12 |
| 15:15:06 | 1607 | 1.0 | 358.14 |
| 15:15:07 | 1607 | 1.0 | 358.15 |
| 15:15:08 | 1607 | 1.0 | 358.17 |
| 15:15:09 | 1607 | 1.0 | 358.18 |
| 15:15:10 | 1607 | 1.0 | 358.20 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:15:11 | 1607 | 1.0 | 358.21 |
| 15:15:12 | 1607 | 1.0 | 358.23 |
| 15:15:13 | 1607 | 1.0 | 358.25 |
| 15:15:14 | 1607 | 1.0 | 358.26 |
| 15:15:15 | 1607 | 1.0 | 358.28 |
| 15:15:16 | 1607 | 1.0 | 358.29 |
| 15:15:17 | 1607 | 1.0 | 358.31 |
| 15:15:18 | 1607 | 1.0 | 358.33 |
| 15:15:19 | 1608 | 1.0 | 358.34 |
| 15:15:20 | 1608 | 1.0 | 358.36 |
| 15:15:21 | 1608 | 1.0 | 358.37 |
| 15:15:22 | 1608 | 1.0 | 358.39 |
| 15:15:23 | 1608 | 1.0 | 358.40 |
| 15:15:24 | 1608 | 1.0 | 358.42 |
| 15:15:25 | 1608 | 1.0 | 358.44 |
| 15:15:26 | 1608 | 1.0 | 358.45 |
| 15:15:27 | 1608 | 1.0 | 358.47 |
| 15:15:28 | 1608 | 1.0 | 358.48 |
| 15:15:29 | 1608 | 1.0 | 358.50 |
| 15:15:30 | 1608 | 1.0 | 358.52 |
| 15:15:31 | 1609 | 1.0 | 358.53 |
| 15:15:32 | 1609 | 1.0 | 358.55 |
| 15:15:33 | 1609 | 1.0 | 358.56 |
| 15:15:34 | 1609 | 1.0 | 358.58 |
| 15:15:35 | 1609 | 1.0 | 358.60 |
| 15:15:36 | 1609 | 1.0 | 358.61 |
| 15:15:37 | 1609 | 1.0 | 358.63 |
| 15:15:38 | 1609 | 1.0 | 358.64 |
| 15:15:39 | 1609 | 1.0 | 358.66 |
| 15:15:40 | 1609 | 1.0 | 358.67 |
| 15:15:41 | 1609 | 1.0 | 358.69 |
| 15:15:42 | 1610 | 1.0 | 358.71 |
| 15:15:43 | 1610 | 1.0 | 358.72 |
| 15:15:44 | 1610 | 1.0 | 358.74 |
| 15:15:45 | 1610 | 1.0 | 358.75 |
| 15:15:46 | 1610 | 1.0 | 358.77 |
| 15:15:47 | 1610 | 1.0 | 358.79 |
| 15:15:48 | 1610 | 1.0 | 358.80 |
| 15:15:49 | 1610 | 1.0 | 358.82 |
| 15:15:50 | 1610 | 1.0 | 358.83 |
| 15:15:51 | 1610 | 0.9 | 358.85 |
| 15:15:52 | 1610 | 1.0 | 358.86 |
| 15:15:53 | 1610 | 1.0 | 358.88 |
| 15:15:54 | 1610 | 1.0 | 358.90 |
| 15:15:55 | 1610 | 1.0 | 358.91 |
| 15:15:56 | 1611 | 1.0 | 358.93 |
| 15:15:57 | 1610 | 1.0 | 358.94 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:15:58 | 1611 | 1.0 | 358.96 |
| 15:15:59 | 1611 | 1.0 | 358.98 |
| 15:16:00 | 1611 | 1.0 | 358.99 |
| 15:16:01 | 1611 | 1.0 | 359.01 |
| 15:16:02 | 1611 | 1.0 | 359.02 |
| 15:16:03 | 1611 | 1.0 | 359.04 |
| 15:16:04 | 1611 | 1.0 | 359.05 |
| 15:16:05 | 1611 | 1.0 | 359.07 |
| 15:16:06 | 1611 | 1.0 | 359.09 |
| 15:16:07 | 1611 | 1.0 | 359.10 |
| 15:16:08 | 1612 | 1.0 | 359.12 |
| 15:16:09 | 1612 | 1.0 | 359.13 |
| 15:16:10 | 1612 | 1.0 | 359.15 |
| 15:16:11 | 1612 | 1.0 | 359.17 |
| 15:16:12 | 1612 | 1.0 | 359.18 |
| 15:16:13 | 1612 | 1.0 | 359.20 |
| 15:16:14 | 1612 | 1.0 | 359.21 |
| 15:16:15 | 1612 | 1.0 | 359.23 |
| 15:16:16 | 1612 | 1.0 | 359.25 |
| 15:16:17 | 1612 | 1.0 | 359.26 |
| 15:16:18 | 1612 | 1.0 | 359.28 |
| 15:16:19 | 1612 | 1.0 | 359.29 |
| 15:16:20 | 1613 | 1.0 | 359.31 |
| 15:16:21 | 1613 | 1.0 | 359.32 |
| 15:16:22 | 1613 | 1.0 | 359.34 |
| 15:16:23 | 1613 | 1.0 | 359.36 |
| 15:16:24 | 1613 | 1.0 | 359.37 |
| 15:16:25 | 1613 | 1.0 | 359.39 |
| 15:16:26 | 1613 | 1.0 | 359.40 |
| 15:16:27 | 1613 | 1.0 | 359.42 |
| 15:16:28 | 1613 | 1.0 | 359.44 |
| 15:16:29 | 1613 | 1.0 | 359.45 |
| 15:16:30 | 1614 | 1.0 | 359.47 |
| 15:16:31 | 1614 | 1.0 | 359.48 |
| 15:16:32 | 1614 | 1.0 | 359.50 |
| 15:16:33 | 1614 | 1.0 | 359.51 |
| 15:16:34 | 1614 | 1.0 | 359.53 |
| 15:16:35 | 1614 | 1.0 | 359.55 |
| 15:16:36 | 1614 | 1.0 | 359.56 |
| 15:16:37 | 1614 | 1.0 | 359.58 |
| 15:16:38 | 1615 | 1.0 | 359.59 |
| 15:16:39 | 1614 | 1.0 | 359.61 |
| 15:16:40 | 1615 | 1.0 | 359.63 |
| 15:16:41 | 1615 | 1.0 | 359.64 |
| 15:16:42 | 1615 | 1.0 | 359.66 |
| 15:16:43 | 1615 | 1.0 | 359.67 |
| 15:16:44 | 1615 | 1.0 | 359.69 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:16:45 | 1615 | 1.0 | 359.70 |
| 15:16:46 | 1615 | 1.0 | 359.72 |
| 15:16:47 | 1615 | 1.0 | 359.74 |
| 15:16:48 | 1615 | 1.0 | 359.75 |
| 15:16:49 | 1615 | 1.0 | 359.77 |
| 15:16:50 | 1615 | 1.0 | 359.78 |
| 15:16:51 | 1615 | 1.0 | 359.80 |
| 15:16:52 | 1615 | 1.0 | 359.82 |
| 15:16:53 | 1616 | 1.0 | 359.83 |
| 15:16:54 | 1616 | 1.0 | 359.85 |
| 15:16:55 | 1616 | 1.0 | 359.86 |
| 15:16:56 | 1616 | 1.0 | 359.88 |
| 15:16:57 | 1616 | 1.0 | 359.90 |
| 15:16:58 | 1616 | 1.0 | 359.91 |
| 15:16:59 | 1616 | 1.0 | 359.93 |
| 15:17:00 | 1616 | 1.0 | 359.94 |
| 15:17:01 | 1616 | 1.0 | 359.96 |
| 15:17:02 | 1616 | 1.0 | 359.97 |
| 15:17:03 | 1616 | 1.0 | 359.99 |
| 15:17:04 | 1616 | 1.0 | 360.01 |
| 15:17:05 | 1616 | 1.0 | 360.02 |
| 15:17:06 | 1616 | 1.0 | 360.04 |
| 15:17:07 | 1617 | 1.0 | 360.05 |
| 15:17:08 | 1617 | 1.0 | 360.07 |
| 15:17:09 | 1617 | 1.0 | 360.09 |
| 15:17:10 | 1617 | 1.0 | 360.10 |
| 15:17:11 | 1617 | 1.0 | 360.12 |
| 15:17:12 | 1617 | 1.0 | 360.13 |
| 15:17:13 | 1617 | 1.0 | 360.15 |
| 15:17:14 | 1617 | 1.0 | 360.16 |
| 15:17:15 | 1617 | 1.0 | 360.18 |
| 15:17:16 | 1617 | 1.0 | 360.20 |
| 15:17:17 | 1617 | 1.0 | 360.21 |
| 15:17:18 | 1618 | 1.0 | 360.23 |
| 15:17:19 | 1618 | 1.0 | 360.24 |
| 15:17:20 | 1618 | 1.0 | 360.26 |
| 15:17:21 | 1618 | 1.0 | 360.28 |
| 15:17:22 | 1618 | 1.0 | 360.29 |
| 15:17:23 | 1618 | 1.0 | 360.31 |
| 15:17:24 | 1618 | 1.0 | 360.32 |
| 15:17:25 | 1618 | 0.9 | 360.34 |
| 15:17:26 | 1618 | 1.0 | 360.36 |
| 15:17:27 | 1618 | 1.0 | 360.37 |
| 15:17:28 | 1618 | 1.0 | 360.39 |
| 15:17:29 | 1618 | 1.0 | 360.40 |
| 15:17:30 | 1618 | 1.0 | 360.42 |
| 15:17:31 | 1619 | 1.0 | 360.43 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:17:32 | 1619 | 1.0 | 360.45 |
| 15:17:33 | 1619 | 1.0 | 360.47 |
| 15:17:34 | 1619 | 1.0 | 360.48 |
| 15:17:35 | 1619 | 1.0 | 360.50 |
| 15:17:36 | 1619 | 1.0 | 360.51 |
| 15:17:37 | 1619 | 1.0 | 360.53 |
| 15:17:38 | 1619 | 1.0 | 360.55 |
| 15:17:39 | 1619 | 1.0 | 360.56 |
| 15:17:40 | 1619 | 1.0 | 360.58 |
| 15:17:41 | 1619 | 1.0 | 360.59 |
| 15:17:42 | 1619 | 1.0 | 360.61 |
| 15:17:43 | 1619 | 1.0 | 360.62 |
| 15:17:44 | 1619 | 1.0 | 360.64 |
| 15:17:45 | 1619 | 1.0 | 360.66 |
| 15:17:46 | 1620 | 1.0 | 360.67 |
| 15:17:47 | 1620 | 1.0 | 360.69 |
| 15:17:48 | 1620 | 1.0 | 360.70 |
| 15:17:49 | 1620 | 1.0 | 360.72 |
| 15:17:50 | 1620 | 1.0 | 360.74 |
| 15:17:51 | 1620 | 1.0 | 360.75 |
| 15:17:52 | 1620 | 1.0 | 360.77 |
| 15:17:53 | 1620 | 1.0 | 360.78 |
| 15:17:54 | 1620 | 1.0 | 360.80 |
| 15:17:55 | 1620 | 1.0 | 360.82 |
| 15:17:56 | 1620 | 1.0 | 360.83 |
| 15:17:57 | 1620 | 1.0 | 360.85 |
| 15:17:58 | 1620 | 1.0 | 360.86 |
| 15:17:59 | 1621 | 1.0 | 360.88 |
| 15:18:00 | 1621 | 1.0 | 360.89 |
| 15:18:01 | 1621 | 1.0 | 360.91 |
| 15:18:02 | 1620 | 1.0 | 360.93 |
| 15:18:03 | 1620 | 1.0 | 360.94 |
| 15:18:04 | 1621 | 1.0 | 360.96 |
| 15:18:05 | 1621 | 1.0 | 360.97 |
| 15:18:06 | 1621 | 1.0 | 360.99 |
| 15:18:07 | 1621 | 1.0 | 361.01 |
| 15:18:08 | 1621 | 1.0 | 361.02 |
| 15:18:09 | 1621 | 1.0 | 361.04 |
| 15:18:10 | 1621 | 1.0 | 361.05 |
| 15:18:11 | 1621 | 1.0 | 361.07 |
| 15:18:12 | 1621 | 1.0 | 361.08 |
| 15:18:13 | 1622 | 1.0 | 361.10 |
| 15:18:14 | 1622 | 1.0 | 361.12 |
| 15:18:15 | 1622 | 1.0 | 361.13 |
| 15:18:16 | 1622 | 1.0 | 361.15 |
| 15:18:17 | 1622 | 1.0 | 361.16 |
| 15:18:18 | 1622 | 1.0 | 361.18 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:18:19 | 1622 | 1.0 | 361.20 |
| 15:18:20 | 1622 | 1.0 | 361.21 |
| 15:18:21 | 1622 | 1.0 | 361.23 |
| 15:18:22 | 1622 | 1.0 | 361.24 |
| 15:18:23 | 1622 | 1.0 | 361.26 |
| 15:18:24 | 1622 | 1.0 | 361.27 |
| 15:18:25 | 1622 | 1.0 | 361.29 |
| 15:18:26 | 1623 | 1.0 | 361.31 |
| 15:18:27 | 1622 | 1.0 | 361.32 |
| 15:18:28 | 1622 | 1.0 | 361.34 |
| 15:18:29 | 1623 | 1.0 | 361.35 |
| 15:18:30 | 1623 | 1.0 | 361.37 |
| 15:18:31 | 1622 | 1.0 | 361.39 |
| 15:18:32 | 1623 | 1.0 | 361.40 |
| 15:18:33 | 1623 | 1.0 | 361.42 |
| 15:18:34 | 1623 | 1.0 | 361.43 |
| 15:18:35 | 1623 | 1.0 | 361.45 |
| 15:18:36 | 1623 | 1.0 | 361.47 |
| 15:18:37 | 1623 | 1.0 | 361.48 |
| 15:18:38 | 1623 | 1.0 | 361.50 |
| 15:18:39 | 1623 | 1.0 | 361.51 |
| 15:18:40 | 1623 | 1.0 | 361.53 |
| 15:18:41 | 1623 | 1.0 | 361.54 |
| 15:18:42 | 1624 | 1.0 | 361.56 |
| 15:18:43 | 1624 | 1.0 | 361.58 |
| 15:18:44 | 1624 | 1.0 | 361.59 |
| 15:18:45 | 1624 | 1.0 | 361.61 |
| 15:18:46 | 1623 | 1.0 | 361.62 |
| 15:18:47 | 1624 | 1.0 | 361.64 |
| 15:18:48 | 1624 | 1.0 | 361.66 |
| 15:18:49 | 1624 | 1.0 | 361.67 |
| 15:18:50 | 1624 | 1.0 | 361.69 |
| 15:18:51 | 1624 | 1.0 | 361.70 |
| 15:18:52 | 1624 | 0.9 | 361.72 |
| 15:18:53 | 1624 | 1.0 | 361.73 |
| 15:18:54 | 1624 | 1.0 | 361.75 |
| 15:18:55 | 1624 | 1.0 | 361.77 |
| 15:18:56 | 1624 | 1.0 | 361.78 |
| 15:18:57 | 1624 | 1.0 | 361.80 |
| 15:18:58 | 1625 | 1.0 | 361.81 |
| 15:18:59 | 1625 | 1.0 | 361.83 |
| 15:19:00 | 1625 | 1.0 | 361.85 |
| 15:19:01 | 1625 | 1.0 | 361.86 |
| 15:19:02 | 1625 | 1.0 | 361.88 |
| 15:19:03 | 1625 | 1.0 | 361.89 |
| 15:19:04 | 1625 | 1.0 | 361.91 |
| 15:19:05 | 1625 | 1.0 | 361.92 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:19:06 | 1625 | 1.0 | 361.94 |
| 15:19:07 | 1625 | 1.0 | 361.96 |
| 15:19:08 | 1625 | 1.0 | 361.97 |
| 15:19:09 | 1625 | 1.0 | 361.99 |
| 15:19:10 | 1625 | 1.0 | 362.00 |
| 15:19:11 | 1625 | 1.0 | 362.02 |
| 15:19:12 | 1625 | 1.0 | 362.04 |
| 15:19:13 | 1625 | 1.0 | 362.05 |
| 15:19:14 | 1626 | 1.0 | 362.07 |
| 15:19:15 | 1626 | 1.0 | 362.08 |
| 15:19:16 | 1626 | 1.0 | 362.10 |
| 15:19:17 | 1626 | 1.0 | 362.12 |
| 15:19:18 | 1626 | 0.9 | 362.13 |
| 15:19:19 | 1626 | 1.0 | 362.15 |
| 15:19:20 | 1626 | 1.0 | 362.16 |
| 15:19:21 | 1626 | 1.0 | 362.18 |
| 15:19:22 | 1626 | 1.0 | 362.19 |
| 15:19:23 | 1626 | 1.0 | 362.21 |
| 15:19:24 | 1626 | 1.0 | 362.23 |
| 15:19:25 | 1626 | 1.0 | 362.24 |
| 15:19:26 | 1626 | 1.0 | 362.26 |
| 15:19:27 | 1626 | 1.0 | 362.27 |
| 15:19:28 | 1626 | 1.0 | 362.29 |
| 15:19:29 | 1627 | 1.0 | 362.31 |
| 15:19:30 | 1627 | 1.0 | 362.32 |
| 15:19:31 | 1627 | 1.0 | 362.34 |
| 15:19:32 | 1627 | 1.0 | 362.35 |
| 15:19:33 | 1627 | 1.0 | 362.37 |
| 15:19:34 | 1627 | 1.0 | 362.38 |
| 15:19:35 | 1627 | 1.0 | 362.40 |
| 15:19:36 | 1627 | 1.0 | 362.42 |
| 15:19:37 | 1627 | 1.0 | 362.43 |
| 15:19:38 | 1627 | 0.9 | 362.45 |
| 15:19:39 | 1627 | 1.0 | 362.46 |
| 15:19:40 | 1627 | 1.0 | 362.48 |
| 15:19:41 | 1627 | 1.0 | 362.50 |
| 15:19:42 | 1627 | 1.0 | 362.51 |
| 15:19:43 | 1627 | 1.0 | 362.53 |
| 15:19:44 | 1628 | 1.0 | 362.54 |
| 15:19:45 | 1628 | 1.0 | 362.56 |
| 15:19:46 | 1628 | 1.0 | 362.57 |
| 15:19:47 | 1627 | 1.0 | 362.59 |
| 15:19:48 | 1628 | 1.0 | 362.61 |
| 15:19:49 | 1628 | 1.0 | 362.62 |
| 15:19:50 | 1628 | 0.9 | 362.64 |
| 15:19:51 | 1628 | 1.0 | 362.65 |
| 15:19:52 | 1628 | 1.0 | 362.67 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:19:53 | 1628 | 1.0 | 362.69 |
| 15:19:54 | 1628 | 0.9 | 362.70 |
| 15:19:55 | 1628 | 1.0 | 362.72 |
| 15:19:56 | 1628 | 1.0 | 362.73 |
| 15:19:57 | 1629 | 1.0 | 362.75 |
| 15:19:58 | 1629 | 1.0 | 362.76 |
| 15:19:59 | 1629 | 0.9 | 362.78 |
| 15:20:00 | 1628 | 1.0 | 362.80 |
| 15:20:01 | 1629 | 1.0 | 362.81 |
| 15:20:02 | 1629 | 1.0 | 362.83 |
| 15:20:03 | 1628 | 1.0 | 362.84 |
| 15:20:04 | 1629 | 0.9 | 362.86 |
| 15:20:05 | 1629 | 1.0 | 362.88 |
| 15:20:06 | 1629 | 1.0 | 362.89 |
| 15:20:07 | 1629 | 1.0 | 362.91 |
| 15:20:08 | 1629 | 1.0 | 362.92 |
| 15:20:09 | 1629 | 1.0 | 362.94 |
| 15:20:10 | 1629 | 1.0 | 362.96 |
| 15:20:11 | 1629 | 0.9 | 362.97 |
| 15:20:12 | 1629 | 1.0 | 362.99 |
| 15:20:13 | 1629 | 1.0 | 363.00 |
| 15:20:14 | 1629 | 1.0 | 363.02 |
| 15:20:15 | 1629 | 0.9 | 363.03 |
| 15:20:16 | 1629 | 1.0 | 363.05 |
| 15:20:17 | 1629 | 1.0 | 363.07 |
| 15:20:18 | 1630 | 1.0 | 363.08 |
| 15:20:19 | 1630 | 1.0 | 363.10 |
| 15:20:20 | 1630 | 1.0 | 363.11 |
| 15:20:21 | 1630 | 1.0 | 363.13 |
| 15:20:22 | 1630 | 1.0 | 363.15 |
| 15:20:23 | 1630 | 1.0 | 363.16 |
| 15:20:24 | 1630 | 0.9 | 363.18 |
| 15:20:25 | 1630 | 1.0 | 363.19 |
| 15:20:26 | 1630 | 1.0 | 363.21 |
| 15:20:27 | 1630 | 1.0 | 363.22 |
| 15:20:28 | 1630 | 1.0 | 363.24 |
| 15:20:29 | 1630 | 1.0 | 363.26 |
| 15:20:30 | 1630 | 1.0 | 363.27 |
| 15:20:31 | 1630 | 1.0 | 363.29 |
| 15:20:32 | 1630 | 1.0 | 363.30 |
| 15:20:33 | 1630 | 1.0 | 363.32 |
| 15:20:34 | 1630 | 1.0 | 363.34 |
| 15:20:35 | 1631 | 1.0 | 363.35 |
| 15:20:36 | 1631 | 0.9 | 363.37 |
| 15:20:37 | 1631 | 1.0 | 363.38 |
| 15:20:38 | 1631 | 1.0 | 363.40 |
| 15:20:39 | 1631 | 1.0 | 363.41 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:20:40 | 1631 | 1.0 | 363.43 |
| 15:20:41 | 1631 | 1.0 | 363.45 |
| 15:20:42 | 1631 | 1.0 | 363.46 |
| 15:20:43 | 1631 | 1.0 | 363.48 |
| 15:20:44 | 1631 | 1.0 | 363.49 |
| 15:20:45 | 1631 | 1.0 | 363.51 |
| 15:20:46 | 1631 | 0.9 | 363.53 |
| 15:20:47 | 1631 | 1.0 | 363.54 |
| 15:20:48 | 1631 | 1.0 | 363.56 |
| 15:20:49 | 1632 | 1.0 | 363.57 |
| 15:20:50 | 1632 | 1.0 | 363.59 |
| 15:20:51 | 1632 | 1.0 | 363.60 |
| 15:20:52 | 1632 | 1.0 | 363.62 |
| 15:20:53 | 1631 | 1.0 | 363.64 |
| 15:20:54 | 1631 | 1.0 | 363.65 |
| 15:20:55 | 1631 | 1.0 | 363.67 |
| 15:20:56 | 1631 | 1.0 | 363.68 |
| 15:20:57 | 1632 | 0.9 | 363.70 |
| 15:20:58 | 1632 | 1.0 | 363.72 |
| 15:20:59 | 1632 | 1.0 | 363.73 |
| 15:21:00 | 1632 | 1.0 | 363.75 |
| 15:21:01 | 1632 | 1.0 | 363.76 |
| 15:21:02 | 1632 | 1.0 | 363.78 |
| 15:21:03 | 1632 | 1.0 | 363.79 |
| 15:21:04 | 1632 | 1.0 | 363.81 |
| 15:21:05 | 1632 | 1.0 | 363.83 |
| 15:21:06 | 1632 | 1.0 | 363.84 |
| 15:21:07 | 1632 | 1.0 | 363.86 |
| 15:21:08 | 1632 | 1.0 | 363.87 |
| 15:21:09 | 1632 | 0.9 | 363.89 |
| 15:21:10 | 1632 | 1.0 | 363.91 |
| 15:21:11 | 1632 | 1.0 | 363.92 |
| 15:21:12 | 1632 | 1.0 | 363.94 |
| 15:21:13 | 1632 | 1.0 | 363.95 |
| 15:21:14 | 1633 | 1.0 | 363.97 |
| 15:21:15 | 1633 | 1.0 | 363.98 |
| 15:21:16 | 1633 | 1.0 | 364.00 |
| 15:21:17 | 1633 | 1.0 | 364.02 |
| 15:21:18 | 1633 | 1.0 | 364.03 |
| 15:21:19 | 1633 | 1.0 | 364.05 |
| 15:21:20 | 1633 | 1.0 | 364.06 |
| 15:21:21 | 1633 | 1.0 | 364.08 |
| 15:21:22 | 1633 | 0.9 | 364.10 |
| 15:21:23 | 1633 | 1.0 | 364.11 |
| 15:21:24 | 1633 | 1.0 | 364.13 |
| 15:21:25 | 1633 | 1.0 | 364.14 |
| 15:21:26 | 1633 | 1.0 | 364.16 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:21:27 | 1633 | 1.0 | 364.18 |
| 15:21:28 | 1633 | 1.0 | 364.19 |
| 15:21:29 | 1634 | 1.0 | 364.21 |
| 15:21:30 | 1633 | 1.0 | 364.22 |
| 15:21:31 | 1633 | 1.0 | 364.24 |
| 15:21:32 | 1633 | 1.0 | 364.25 |
| 15:21:33 | 1633 | 0.9 | 364.27 |
| 15:21:34 | 1634 | 1.0 | 364.29 |
| 15:21:35 | 1634 | 1.0 | 364.30 |
| 15:21:36 | 1634 | 1.0 | 364.32 |
| 15:21:37 | 1634 | 1.0 | 364.33 |
| 15:21:38 | 1634 | 1.0 | 364.35 |
| 15:21:39 | 1634 | 1.0 | 364.37 |
| 15:21:40 | 1634 | 1.0 | 364.38 |
| 15:21:41 | 1634 | 1.0 | 364.40 |
| 15:21:42 | 1634 | 1.0 | 364.41 |
| 15:21:43 | 1634 | 0.9 | 364.43 |
| 15:21:44 | 1634 | 1.0 | 364.44 |
| 15:21:45 | 1634 | 1.0 | 364.46 |
| 15:21:46 | 1634 | 1.0 | 364.48 |
| 15:21:47 | 1634 | 1.0 | 364.49 |
| 15:21:48 | 1634 | 1.0 | 364.51 |
| 15:21:49 | 1634 | 1.0 | 364.52 |
| 15:21:50 | 1634 | 1.0 | 364.54 |
| 15:21:51 | 1635 | 1.0 | 364.56 |
| 15:21:52 | 1635 | 1.0 | 364.57 |
| 15:21:53 | 1635 | 1.0 | 364.59 |
| 15:21:54 | 1635 | 0.9 | 364.60 |
| 15:21:55 | 1635 | 1.0 | 364.62 |
| 15:21:56 | 1635 | 1.0 | 364.63 |
| 15:21:57 | 1635 | 1.0 | 364.65 |
| 15:21:58 | 1635 | 1.0 | 364.67 |
| 15:21:59 | 1635 | 0.9 | 364.68 |
| 15:22:00 | 1635 | 1.0 | 364.70 |
| 15:22:01 | 1635 | 1.0 | 364.71 |
| 15:22:02 | 1635 | 1.0 | 364.73 |
| 15:22:03 | 1635 | 1.0 | 364.75 |
| 15:22:04 | 1635 | 1.0 | 364.76 |
| 15:22:05 | 1636 | 1.0 | 364.78 |
| 15:22:06 | 1636 | 1.0 | 364.79 |
| 15:22:07 | 1636 | 0.9 | 364.81 |
| 15:22:08 | 1636 | 0.9 | 364.82 |
| 15:22:09 | 1636 | 1.0 | 364.84 |
| 15:22:10 | 1636 | 1.0 | 364.86 |
| 15:22:11 | 1636 | 1.0 | 364.87 |
| 15:22:12 | 1636 | 1.0 | 364.89 |
| 15:22:13 | 1636 | 1.0 | 364.90 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:22:14 | 1636 | 1.0 | 364.92 |
| 15:22:15 | 1636 | 0.9 | 364.94 |
| 15:22:16 | 1636 | 1.0 | 364.95 |
| 15:22:17 | 1636 | 1.0 | 364.97 |
| 15:22:18 | 1636 | 1.0 | 364.98 |
| 15:22:19 | 1637 | 0.9 | 365.00 |
| 15:22:20 | 1637 | 0.9 | 365.01 |
| 15:22:21 | 1637 | 1.0 | 365.03 |
| 15:22:22 | 1637 | 1.0 | 365.05 |
| 15:22:23 | 1637 | 1.0 | 365.06 |
| 15:22:24 | 1637 | 1.0 | 365.08 |
| 15:22:25 | 1637 | 1.0 | 365.09 |
| 15:22:26 | 1637 | 1.0 | 365.11 |
| 15:22:27 | 1637 | 1.0 | 365.13 |
| 15:22:28 | 1637 | 1.0 | 365.14 |
| 15:22:29 | 1637 | 0.9 | 365.16 |
| 15:22:30 | 1637 | 1.0 | 365.17 |
| 15:22:31 | 1637 | 1.0 | 365.19 |
| 15:22:32 | 1638 | 1.0 | 365.20 |
| 15:22:33 | 1637 | 1.0 | 365.22 |
| 15:22:34 | 1638 | 1.0 | 365.24 |
| 15:22:35 | 1638 | 1.0 | 365.25 |
| 15:22:36 | 1637 | 1.0 | 365.27 |
| 15:22:37 | 1637 | 1.0 | 365.28 |
| 15:22:38 | 1637 | 1.0 | 365.30 |
| 15:22:39 | 1638 | 1.0 | 365.32 |
| 15:22:40 | 1638 | 0.9 | 365.33 |
| 15:22:41 | 1638 | 0.9 | 365.35 |
| 15:22:42 | 1638 | 1.0 | 365.36 |
| 15:22:43 | 1638 | 1.0 | 365.38 |
| 15:22:44 | 1638 | 1.0 | 365.40 |
| 15:22:45 | 1638 | 1.0 | 365.41 |
| 15:22:46 | 1638 | 1.0 | 365.43 |
| 15:22:47 | 1638 | 1.0 | 365.44 |
| 15:22:48 | 1639 | 1.0 | 365.46 |
| 15:22:49 | 1638 | 0.9 | 365.47 |
| 15:22:50 | 1639 | 1.0 | 365.49 |
| 15:22:51 | 1639 | 1.0 | 365.51 |
| 15:22:52 | 1639 | 1.0 | 365.52 |
| 15:22:53 | 1639 | 1.0 | 365.54 |
| 15:22:54 | 1639 | 1.0 | 365.55 |
| 15:22:55 | 1639 | 1.0 | 365.57 |
| 15:22:56 | 1639 | 1.0 | 365.59 |
| 15:22:57 | 1639 | 1.0 | 365.60 |
| 15:22:58 | 1639 | 1.0 | 365.62 |
| 15:22:59 | 1639 | 1.0 | 365.63 |
| 15:23:00 | 1639 | 1.0 | 365.65 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:23:01 | 1639 | 0.9 | 365.66 |
| 15:23:02 | 1639 | 1.0 | 365.68 |
| 15:23:03 | 1639 | 1.0 | 365.70 |
| 15:23:04 | 1639 | 1.0 | 365.71 |
| 15:23:05 | 1639 | 1.0 | 365.73 |
| 15:23:06 | 1639 | 1.0 | 365.74 |
| 15:23:07 | 1639 | 1.0 | 365.76 |
| 15:23:08 | 1640 | 1.0 | 365.78 |
| 15:23:09 | 1640 | 1.0 | 365.79 |
| 15:23:10 | 1640 | 1.0 | 365.81 |
| 15:23:11 | 1640 | 1.0 | 365.82 |
| 15:23:12 | 1640 | 1.0 | 365.84 |
| 15:23:13 | 1640 | 0.9 | 365.85 |
| 15:23:14 | 1640 | 1.0 | 365.87 |
| 15:23:15 | 1640 | 1.0 | 365.89 |
| 15:23:16 | 1640 | 1.0 | 365.90 |
| 15:23:17 | 1640 | 0.9 | 365.92 |
| 15:23:18 | 1640 | 1.0 | 365.93 |
| 15:23:19 | 1640 | 1.0 | 365.95 |
| 15:23:20 | 1640 | 1.0 | 365.97 |
| 15:23:21 | 1640 | 1.0 | 365.98 |
| 15:23:22 | 1640 | 0.9 | 366.00 |
| 15:23:23 | 1641 | 1.0 | 366.01 |
| 15:23:24 | 1640 | 1.0 | 366.03 |
| 15:23:25 | 1641 | 1.0 | 366.04 |
| 15:23:26 | 1641 | 1.0 | 366.06 |
| 15:23:27 | 1641 | 0.9 | 366.08 |
| 15:23:28 | 1641 | 1.0 | 366.09 |
| 15:23:29 | 1641 | 1.0 | 366.11 |
| 15:23:30 | 1641 | 1.0 | 366.12 |
| 15:23:31 | 1641 | 1.0 | 366.14 |
| 15:23:32 | 1641 | 1.0 | 366.16 |
| 15:23:33 | 1641 | 1.0 | 366.17 |
| 15:23:34 | 1641 | 1.0 | 366.19 |
| 15:23:35 | 1641 | 1.0 | 366.20 |
| 15:23:36 | 1641 | 1.0 | 366.22 |
| 15:23:37 | 1642 | 1.0 | 366.23 |
| 15:23:38 | 1642 | 0.9 | 366.25 |
| 15:23:39 | 1641 | 1.0 | 366.27 |
| 15:23:40 | 1642 | 1.0 | 366.28 |
| 15:23:41 | 1642 | 1.0 | 366.30 |
| 15:23:42 | 1642 | 1.0 | 366.31 |
| 15:23:43 | 1642 | 1.0 | 366.33 |
| 15:23:44 | 1642 | 1.0 | 366.35 |
| 15:23:45 | 1642 | 1.0 | 366.36 |
| 15:23:46 | 1642 | 1.0 | 366.38 |
| 15:23:47 | 1642 | 0.9 | 366.39 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:23:48 | 1642 | 0.9 | 366.41 |
| 15:23:49 | 1642 | 1.0 | 366.42 |
| 15:23:50 | 1643 | 1.0 | 366.44 |
| 15:23:51 | 1643 | 0.9 | 366.46 |
| 15:23:52 | 1643 | 1.0 | 366.47 |
| 15:23:53 | 1642 | 1.0 | 366.49 |
| 15:23:54 | 1642 | 1.0 | 366.50 |
| 15:23:55 | 1642 | 1.0 | 366.52 |
| 15:23:56 | 1643 | 1.0 | 366.54 |
| 15:23:57 | 1643 | 1.0 | 366.55 |
| 15:23:58 | 1643 | 1.0 | 366.57 |
| 15:23:59 | 1643 | 0.9 | 366.58 |
| 15:24:00 | 1643 | 1.0 | 366.60 |
| 15:24:01 | 1643 | 1.0 | 366.61 |
| 15:24:02 | 1643 | 1.0 | 366.63 |
| 15:24:03 | 1643 | 1.0 | 366.65 |
| 15:24:04 | 1643 | 1.0 | 366.66 |
| 15:24:05 | 1643 | 1.0 | 366.68 |
| 15:24:06 | 1643 | 1.0 | 366.69 |
| 15:24:07 | 1643 | 1.0 | 366.71 |
| 15:24:08 | 1643 | 0.9 | 366.73 |
| 15:24:09 | 1643 | 1.0 | 366.74 |
| 15:24:10 | 1643 | 1.0 | 366.76 |
| 15:24:11 | 1643 | 1.0 | 366.77 |
| 15:24:12 | 1643 | 0.9 | 366.79 |
| 15:24:13 | 1643 | 1.0 | 366.81 |
| 15:24:14 | 1644 | 1.0 | 366.82 |
| 15:24:15 | 1644 | 1.0 | 366.84 |
| 15:24:16 | 1644 | 1.0 | 366.85 |
| 15:24:17 | 1644 | 1.0 | 366.87 |
| 15:24:18 | 1644 | 1.0 | 366.88 |
| 15:24:19 | 1644 | 1.0 | 366.90 |
| 15:24:20 | 1644 | 0.9 | 366.92 |
| 15:24:21 | 1644 | 1.0 | 366.93 |
| 15:24:22 | 1644 | 1.0 | 366.95 |
| 15:24:23 | 1644 | 1.0 | 366.96 |
| 15:24:24 | 1644 | 0.9 | 366.98 |
| 15:24:25 | 1644 | 1.0 | 367.00 |
| 15:24:26 | 1645 | 1.0 | 367.01 |
| 15:24:27 | 1645 | 1.0 | 367.03 |
| 15:24:28 | 1645 | 1.0 | 367.04 |
| 15:24:29 | 1645 | 1.0 | 367.06 |
| 15:24:30 | 1645 | 1.0 | 367.07 |
| 15:24:31 | 1645 | 1.0 | 367.09 |
| 15:24:32 | 1645 | 1.0 | 367.11 |
| 15:24:33 | 1645 | 0.9 | 367.12 |
| 15:24:34 | 1645 | 1.0 | 367.14 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:24:35 | 1645 | 1.0 | 367.15 |
| 15:24:36 | 1645 | 1.0 | 367.17 |
| 15:24:37 | 1645 | 1.0 | 367.19 |
| 15:24:38 | 1645 | 1.0 | 367.20 |
| 15:24:39 | 1645 | 1.0 | 367.22 |
| 15:24:40 | 1645 | 0.9 | 367.23 |
| 15:24:41 | 1645 | 1.0 | 367.25 |
| 15:24:42 | 1645 | 1.0 | 367.26 |
| 15:24:43 | 1646 | 1.0 | 367.28 |
| 15:24:44 | 1646 | 1.0 | 367.30 |
| 15:24:45 | 1645 | 0.9 | 367.31 |
| 15:24:46 | 1645 | 1.0 | 367.33 |
| 15:24:47 | 1645 | 1.0 | 367.34 |
| 15:24:48 | 1645 | 1.0 | 367.36 |
| 15:24:49 | 1645 | 1.0 | 367.38 |
| 15:24:50 | 1645 | 1.0 | 367.39 |
| 15:24:51 | 1646 | 1.0 | 367.41 |
| 15:24:52 | 1646 | 1.0 | 367.42 |
| 15:24:53 | 1646 | 1.0 | 367.44 |
| 15:24:54 | 1646 | 1.0 | 367.45 |
| 15:24:55 | 1646 | 1.0 | 367.47 |
| 15:24:56 | 1646 | 1.0 | 367.49 |
| 15:24:57 | 1646 | 1.0 | 367.50 |
| 15:24:58 | 1646 | 0.9 | 367.52 |
| 15:24:59 | 1646 | 1.0 | 367.53 |
| 15:25:00 | 1646 | 1.0 | 367.55 |
| 15:25:01 | 1646 | 0.9 | 367.57 |
| 15:25:02 | 1646 | 1.0 | 367.58 |
| 15:25:03 | 1646 | 1.0 | 367.60 |
| 15:25:04 | 1646 | 1.0 | 367.61 |
| 15:25:05 | 1647 | 1.0 | 367.63 |
| 15:25:06 | 1647 | 0.9 | 367.64 |
| 15:25:07 | 1647 | 1.0 | 367.66 |
| 15:25:08 | 1647 | 1.0 | 367.68 |
| 15:25:09 | 1647 | 0.9 | 367.69 |
| 15:25:10 | 1647 | 1.0 | 367.71 |
| 15:25:11 | 1647 | 1.0 | 367.72 |
| 15:25:12 | 1647 | 1.0 | 367.74 |
| 15:25:13 | 1647 | 1.0 | 367.76 |
| 15:25:14 | 1647 | 0.9 | 367.77 |
| 15:25:15 | 1647 | 1.0 | 367.79 |
| 15:25:16 | 1647 | 1.0 | 367.80 |
| 15:25:17 | 1647 | 1.0 | 367.82 |
| 15:25:18 | 1647 | 0.9 | 367.83 |
| 15:25:19 | 1647 | 1.0 | 367.85 |
| 15:25:20 | 1647 | 1.0 | 367.87 |
| 15:25:21 | 1648 | 1.0 | 367.88 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:25:22 | 1647 | 1.0 | 367.90 |
| 15:25:23 | 1647 | 1.0 | 367.91 |
| 15:25:24 | 1648 | 1.0 | 367.93 |
| 15:25:25 | 1647 | 1.0 | 367.95 |
| 15:25:26 | 1647 | 1.0 | 367.96 |
| 15:25:27 | 1647 | 1.0 | 367.98 |
| 15:25:28 | 1647 | 1.0 | 367.99 |
| 15:25:29 | 1648 | 1.0 | 368.01 |
| 15:25:30 | 1648 | 0.9 | 368.02 |
| 15:25:31 | 1648 | 0.9 | 368.04 |
| 15:25:32 | 1648 | 1.0 | 368.06 |
| 15:25:33 | 1648 | 1.0 | 368.07 |
| 15:25:34 | 1648 | 1.0 | 368.09 |
| 15:25:35 | 1648 | 0.9 | 368.10 |
| 15:25:36 | 1648 | 1.0 | 368.12 |
| 15:25:37 | 1648 | 1.0 | 368.14 |
| 15:25:38 | 1648 | 1.0 | 368.15 |
| 15:25:39 | 1648 | 1.0 | 368.17 |
| 15:25:40 | 1648 | 0.9 | 368.18 |
| 15:25:41 | 1648 | 1.0 | 368.20 |
| 15:25:42 | 1648 | 0.9 | 368.21 |
| 15:25:43 | 1648 | 0.9 | 368.23 |
| 15:25:44 | 1648 | 1.0 | 368.25 |
| 15:25:45 | 1649 | 1.0 | 368.26 |
| 15:25:46 | 1649 | 1.0 | 368.28 |
| 15:25:47 | 1649 | 1.0 | 368.29 |
| 15:25:48 | 1649 | 1.0 | 368.31 |
| 15:25:49 | 1649 | 1.0 | 368.33 |
| 15:25:50 | 1649 | 1.0 | 368.34 |
| 15:25:51 | 1649 | 0.9 | 368.36 |
| 15:25:52 | 1649 | 0.9 | 368.37 |
| 15:25:53 | 1649 | 1.0 | 368.39 |
| 15:25:54 | 1649 | 1.0 | 368.40 |
| 15:25:55 | 1649 | 1.0 | 368.42 |
| 15:25:56 | 1649 | 0.9 | 368.44 |
| 15:25:57 | 1649 | 1.0 | 368.45 |
| 15:25:58 | 1649 | 1.0 | 368.47 |
| 15:25:59 | 1649 | 1.0 | 368.48 |
| 15:26:00 | 1649 | 1.0 | 368.50 |
| 15:26:01 | 1649 | 0.9 | 368.52 |
| 15:26:02 | 1649 | 1.0 | 368.53 |
| 15:26:03 | 1649 | 0.9 | 368.55 |
| 15:26:04 | 1649 | 1.0 | 368.56 |
| 15:26:05 | 1649 | 1.0 | 368.58 |
| 15:26:06 | 1649 | 1.0 | 368.60 |
| 15:26:07 | 1649 | 1.0 | 368.61 |
| 15:26:08 | 1650 | 1.0 | 368.63 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:26:09 | 1650 | 1.0 | 368.64 |
| 15:26:10 | 1650 | 1.0 | 368.66 |
| 15:26:11 | 1650 | 1.0 | 368.67 |
| 15:26:12 | 1650 | 0.9 | 368.69 |
| 15:26:13 | 1650 | 1.0 | 368.71 |
| 15:26:14 | 1650 | 1.0 | 368.72 |
| 15:26:15 | 1650 | 1.0 | 368.74 |
| 15:26:16 | 1650 | 0.9 | 368.75 |
| 15:26:17 | 1650 | 0.9 | 368.77 |
| 15:26:18 | 1650 | 1.0 | 368.79 |
| 15:26:19 | 1650 | 1.0 | 368.80 |
| 15:26:20 | 1650 | 1.0 | 368.82 |
| 15:26:21 | 1650 | 1.0 | 368.83 |
| 15:26:22 | 1650 | 1.0 | 368.85 |
| 15:26:23 | 1650 | 1.0 | 368.86 |
| 15:26:24 | 1650 | 0.9 | 368.88 |
| 15:26:25 | 1651 | 1.0 | 368.90 |
| 15:26:26 | 1651 | 0.9 | 368.91 |
| 15:26:27 | 1651 | 1.0 | 368.93 |
| 15:26:28 | 1651 | 0.9 | 368.94 |
| 15:26:29 | 1651 | 1.0 | 368.96 |
| 15:26:30 | 1651 | 1.0 | 368.98 |
| 15:26:31 | 1651 | 1.0 | 368.99 |
| 15:26:32 | 1650 | 1.0 | 369.01 |
| 15:26:33 | 1650 | 1.0 | 369.02 |
| 15:26:34 | 1651 | 1.0 | 369.04 |
| 15:26:35 | 1651 | 1.0 | 369.05 |
| 15:26:36 | 1651 | 1.0 | 369.07 |
| 15:26:37 | 1651 | 0.9 | 369.09 |
| 15:26:38 | 1651 | 0.9 | 369.10 |
| 15:26:39 | 1651 | 1.0 | 369.12 |
| 15:26:40 | 1651 | 1.0 | 369.13 |
| 15:26:41 | 1651 | 1.0 | 369.15 |
| 15:26:42 | 1651 | 1.0 | 369.17 |
| 15:26:43 | 1651 | 1.0 | 369.18 |
| 15:26:44 | 1651 | 1.0 | 369.20 |
| 15:26:45 | 1651 | 1.0 | 369.21 |
| 15:26:46 | 1652 | 1.0 | 369.23 |
| 15:26:47 | 1652 | 1.0 | 369.24 |
| 15:26:48 | 1652 | 0.9 | 369.26 |
| 15:26:49 | 1652 | 0.9 | 369.28 |
| 15:26:50 | 1652 | 0.9 | 369.29 |
| 15:26:51 | 1652 | 1.0 | 369.31 |
| 15:26:52 | 1652 | 1.0 | 369.32 |
| 15:26:53 | 1652 | 1.0 | 369.34 |
| 15:26:54 | 1652 | 1.0 | 369.36 |
| 15:26:55 | 1652 | 1.0 | 369.37 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:26:56 | 1652 | 1.0 | 369.39 |
| 15:26:57 | 1652 | 1.0 | 369.40 |
| 15:26:58 | 1652 | 0.9 | 369.42 |
| 15:26:59 | 1652 | 0.9 | 369.43 |
| 15:27:00 | 1652 | 0.9 | 369.45 |
| 15:27:01 | 1652 | 1.0 | 369.47 |
| 15:27:02 | 1652 | 1.0 | 369.48 |
| 15:27:03 | 1652 | 0.9 | 369.50 |
| 15:27:04 | 1653 | 1.0 | 369.51 |
| 15:27:05 | 1653 | 1.0 | 369.53 |
| 15:27:06 | 1653 | 0.9 | 369.55 |
| 15:27:07 | 1653 | 1.0 | 369.56 |
| 15:27:08 | 1653 | 1.0 | 369.58 |
| 15:27:09 | 1653 | 0.9 | 369.59 |
| 15:27:10 | 1653 | 0.9 | 369.61 |
| 15:27:11 | 1653 | 0.9 | 369.62 |
| 15:27:12 | 1653 | 0.9 | 369.64 |
| 15:27:13 | 1653 | 1.0 | 369.66 |
| 15:27:14 | 1653 | 0.9 | 369.67 |
| 15:27:15 | 1653 | 1.0 | 369.69 |
| 15:27:16 | 1653 | 1.0 | 369.70 |
| 15:27:17 | 1653 | 1.0 | 369.72 |
| 15:27:18 | 1653 | 1.0 | 369.74 |
| 15:27:19 | 1653 | 0.9 | 369.75 |
| 15:27:20 | 1653 | 1.0 | 369.77 |
| 15:27:21 | 1653 | 1.0 | 369.78 |
| 15:27:22 | 1653 | 1.0 | 369.80 |
| 15:27:23 | 1653 | 0.9 | 369.81 |
| 15:27:24 | 1653 | 0.9 | 369.83 |
| 15:27:25 | 1653 | 1.0 | 369.85 |
| 15:27:26 | 1654 | 0.9 | 369.86 |
| 15:27:27 | 1654 | 1.0 | 369.88 |
| 15:27:28 | 1654 | 1.0 | 369.89 |
| 15:27:29 | 1654 | 1.0 | 369.91 |
| 15:27:30 | 1654 | 1.0 | 369.93 |
| 15:27:31 | 1654 | 0.9 | 369.94 |
| 15:27:32 | 1654 | 1.0 | 369.96 |
| 15:27:33 | 1654 | 1.0 | 369.97 |
| 15:27:34 | 1654 | 0.9 | 369.99 |
| 15:27:35 | 1654 | 0.9 | 370.00 |
| 15:27:36 | 1654 | 1.0 | 370.02 |
| 15:27:37 | 1654 | 1.0 | 370.04 |
| 15:27:38 | 1654 | 1.0 | 370.05 |
| 15:27:39 | 1654 | 1.0 | 370.07 |
| 15:27:40 | 1654 | 0.9 | 370.08 |
| 15:27:41 | 1654 | 1.0 | 370.10 |
| 15:27:42 | 1654 | 1.0 | 370.12 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:27:43 | 1654 | 1.0 | 370.13 |
| 15:27:44 | 1654 | 0.9 | 370.15 |
| 15:27:45 | 1654 | 1.0 | 370.16 |
| 15:27:46 | 1654 | 1.0 | 370.18 |
| 15:27:47 | 1654 | 0.9 | 370.19 |
| 15:27:48 | 1654 | 1.0 | 370.21 |
| 15:27:49 | 1654 | 1.0 | 370.23 |
| 15:27:50 | 1654 | 1.0 | 370.24 |
| 15:27:51 | 1655 | 1.0 | 370.26 |
| 15:27:52 | 1655 | 1.0 | 370.27 |
| 15:27:53 | 1655 | 1.0 | 370.29 |
| 15:27:54 | 1655 | 1.0 | 370.31 |
| 15:27:55 | 1655 | 1.0 | 370.32 |
| 15:27:56 | 1655 | 0.9 | 370.34 |
| 15:27:57 | 1655 | 1.0 | 370.35 |
| 15:27:58 | 1655 | 1.0 | 370.37 |
| 15:27:59 | 1655 | 1.0 | 370.38 |
| 15:28:00 | 1655 | 0.9 | 370.40 |
| 15:28:01 | 1655 | 0.9 | 370.42 |
| 15:28:02 | 1655 | 1.0 | 370.43 |
| 15:28:03 | 1655 | 1.0 | 370.45 |
| 15:28:04 | 1655 | 1.0 | 370.46 |
| 15:28:05 | 1655 | 0.9 | 370.48 |
| 15:28:06 | 1655 | 1.0 | 370.50 |
| 15:28:07 | 1655 | 1.0 | 370.51 |
| 15:28:08 | 1656 | 1.0 | 370.53 |
| 15:28:09 | 1655 | 1.0 | 370.54 |
| 15:28:10 | 1656 | 1.0 | 370.56 |
| 15:28:11 | 1656 | 1.0 | 370.57 |
| 15:28:12 | 1656 | 1.0 | 370.59 |
| 15:28:13 | 1656 | 1.0 | 370.61 |
| 15:28:14 | 1656 | 1.0 | 370.62 |
| 15:28:15 | 1656 | 1.0 | 370.64 |
| 15:28:16 | 1656 | 0.9 | 370.65 |
| 15:28:17 | 1656 | 0.9 | 370.67 |
| 15:28:18 | 1656 | 1.0 | 370.69 |
| 15:28:19 | 1656 | 1.0 | 370.70 |
| 15:28:20 | 1656 | 1.0 | 370.72 |
| 15:28:21 | 1656 | 0.9 | 370.73 |
| 15:28:22 | 1656 | 1.0 | 370.75 |
| 15:28:23 | 1656 | 1.0 | 370.77 |
| 15:28:24 | 1656 | 1.0 | 370.78 |
| 15:28:25 | 1656 | 1.0 | 370.80 |
| 15:28:26 | 1656 | 1.0 | 370.81 |
| 15:28:27 | 1656 | 1.0 | 370.83 |
| 15:28:28 | 1656 | 1.0 | 370.84 |
| 15:28:29 | 1656 | 1.0 | 370.86 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:28:30 | 1656 | 1.0 | 370.88 |
| 15:28:31 | 1657 | 1.0 | 370.89 |
| 15:28:32 | 1657 | 0.9 | 370.91 |
| 15:28:33 | 1657 | 1.0 | 370.92 |
| 15:28:34 | 1657 | 1.0 | 370.94 |
| 15:28:35 | 1657 | 1.0 | 370.96 |
| 15:28:36 | 1657 | 1.0 | 370.97 |
| 15:28:37 | 1657 | 0.9 | 370.99 |
| 15:28:38 | 1657 | 1.0 | 371.00 |
| 15:28:39 | 1657 | 1.0 | 371.02 |
| 15:28:40 | 1657 | 1.0 | 371.03 |
| 15:28:41 | 1657 | 1.0 | 371.05 |
| 15:28:42 | 1657 | 0.9 | 371.07 |
| 15:28:43 | 1657 | 1.0 | 371.08 |
| 15:28:44 | 1657 | 1.0 | 371.10 |
| 15:28:45 | 1658 | 1.0 | 371.11 |
| 15:28:46 | 1657 | 1.0 | 371.13 |
| 15:28:47 | 1658 | 1.0 | 371.15 |
| 15:28:48 | 1658 | 1.0 | 371.16 |
| 15:28:49 | 1658 | 1.0 | 371.18 |
| 15:28:50 | 1658 | 1.0 | 371.19 |
| 15:28:51 | 1658 | 1.0 | 371.21 |
| 15:28:52 | 1658 | 1.0 | 371.22 |
| 15:28:53 | 1658 | 0.9 | 371.24 |
| 15:28:54 | 1658 | 0.9 | 371.26 |
| 15:28:55 | 1658 | 1.0 | 371.27 |
| 15:28:56 | 1658 | 1.0 | 371.29 |
| 15:28:57 | 1658 | 1.0 | 371.30 |
| 15:28:58 | 1658 | 0.9 | 371.32 |
| 15:28:59 | 1658 | 1.0 | 371.34 |
| 15:29:00 | 1658 | 1.0 | 371.35 |
| 15:29:01 | 1658 | 1.0 | 371.37 |
| 15:29:02 | 1658 | 1.0 | 371.38 |
| 15:29:03 | 1658 | 0.9 | 371.40 |
| 15:29:04 | 1658 | 1.0 | 371.41 |
| 15:29:05 | 1658 | 1.0 | 371.43 |
| 15:29:06 | 1658 | 0.9 | 371.45 |
| 15:29:07 | 1658 | 0.9 | 371.46 |
| 15:29:08 | 1659 | 0.9 | 371.48 |
| 15:29:09 | 1659 | 1.0 | 371.49 |
| 15:29:10 | 1659 | 0.9 | 371.51 |
| 15:29:11 | 1659 | 1.0 | 371.53 |
| 15:29:12 | 1659 | 1.0 | 371.54 |
| 15:29:13 | 1659 | 1.0 | 371.56 |
| 15:29:14 | 1659 | 0.9 | 371.57 |
| 15:29:15 | 1659 | 0.9 | 371.59 |
| 15:29:16 | 1659 | 1.0 | 371.60 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:29:17 | 1659 | 1.0 | 371.62 |
| 15:29:18 | 1659 | 0.9 | 371.64 |
| 15:29:19 | 1659 | 0.9 | 371.65 |
| 15:29:20 | 1659 | 1.0 | 371.67 |
| 15:29:21 | 1659 | 1.0 | 371.68 |
| 15:29:22 | 1659 | 1.0 | 371.70 |
| 15:29:23 | 1659 | 1.0 | 371.72 |
| 15:29:24 | 1659 | 0.9 | 371.73 |
| 15:29:25 | 1659 | 1.0 | 371.75 |
| 15:29:26 | 1659 | 1.0 | 371.76 |
| 15:29:27 | 1659 | 0.9 | 371.78 |
| 15:29:28 | 1659 | 0.9 | 371.79 |
| 15:29:29 | 1659 | 0.9 | 371.81 |
| 15:29:30 | 1659 | 0.9 | 371.83 |
| 15:29:31 | 1659 | 1.0 | 371.84 |
| 15:29:32 | 1659 | 1.0 | 371.86 |
| 15:29:33 | 1660 | 1.0 | 371.87 |
| 15:29:34 | 1660 | 1.0 | 371.89 |
| 15:29:35 | 1660 | 0.9 | 371.91 |
| 15:29:36 | 1660 | 1.0 | 371.92 |
| 15:29:37 | 1660 | 1.0 | 371.94 |
| 15:29:38 | 1660 | 1.0 | 371.95 |
| 15:29:39 | 1660 | 0.9 | 371.97 |
| 15:29:40 | 1660 | 0.9 | 371.98 |
| 15:29:41 | 1660 | 1.0 | 372.00 |
| 15:29:42 | 1660 | 1.0 | 372.02 |
| 15:29:43 | 1660 | 1.0 | 372.03 |
| 15:29:44 | 1660 | 1.0 | 372.05 |
| 15:29:45 | 1660 | 1.0 | 372.06 |
| 15:29:46 | 1660 | 1.0 | 372.08 |
| 15:29:47 | 1660 | 1.0 | 372.10 |
| 15:29:48 | 1661 | 0.9 | 372.11 |
| 15:29:49 | 1661 | 0.9 | 372.13 |
| 15:29:50 | 1661 | 0.9 | 372.14 |
| 15:29:51 | 1661 | 1.0 | 372.16 |
| 15:29:52 | 1660 | 1.0 | 372.17 |
| 15:29:53 | 1660 | 0.9 | 372.19 |
| 15:29:54 | 1660 | 1.0 | 372.21 |
| 15:29:55 | 1660 | 1.0 | 372.22 |
| 15:29:56 | 1660 | 1.0 | 372.24 |
| 15:29:57 | 1660 | 1.0 | 372.25 |
| 15:29:58 | 1661 | 1.0 | 372.27 |
| 15:29:59 | 1661 | 1.0 | 372.29 |
| 15:30:00 | 1661 | 0.9 | 372.30 |
| 15:30:01 | 1661 | 0.9 | 372.32 |
| 15:30:02 | 1661 | 1.0 | 372.33 |
| 15:30:03 | 1661 | 1.0 | 372.35 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:30:04 | 1661 | 1.0 | 372.36 |
| 15:30:05 | 1661 | 1.0 | 372.38 |
| 15:30:06 | 1661 | 1.0 | 372.40 |
| 15:30:07 | 1661 | 1.0 | 372.41 |
| 15:30:08 | 1661 | 1.0 | 372.43 |
| 15:30:09 | 1661 | 0.9 | 372.44 |
| 15:30:10 | 1661 | 0.9 | 372.46 |
| 15:30:11 | 1661 | 1.0 | 372.48 |
| 15:30:12 | 1661 | 1.0 | 372.49 |
| 15:30:13 | 1661 | 0.9 | 372.51 |
| 15:30:14 | 1661 | 0.9 | 372.52 |
| 15:30:15 | 1661 | 1.0 | 372.54 |
| 15:30:16 | 1661 | 1.0 | 372.55 |
| 15:30:17 | 1661 | 1.0 | 372.57 |
| 15:30:18 | 1661 | 1.0 | 372.59 |
| 15:30:19 | 1661 | 1.0 | 372.60 |
| 15:30:20 | 1661 | 1.0 | 372.62 |
| 15:30:21 | 1661 | 0.9 | 372.63 |
| 15:30:22 | 1662 | 1.0 | 372.65 |
| 15:30:23 | 1662 | 1.0 | 372.67 |
| 15:30:24 | 1662 | 1.0 | 372.68 |
| 15:30:25 | 1662 | 1.0 | 372.70 |
| 15:30:26 | 1662 | 0.9 | 372.71 |
| 15:30:27 | 1662 | 1.0 | 372.73 |
| 15:30:28 | 1662 | 1.0 | 372.75 |
| 15:30:29 | 1662 | 1.0 | 372.76 |
| 15:30:30 | 1662 | 1.0 | 372.78 |
| 15:30:31 | 1662 | 1.0 | 372.79 |
| 15:30:32 | 1662 | 1.0 | 372.81 |
| 15:30:33 | 1662 | 0.9 | 372.82 |
| 15:30:34 | 1662 | 1.0 | 372.84 |
| 15:30:35 | 1662 | 1.0 | 372.86 |
| 15:30:36 | 1662 | 1.0 | 372.87 |
| 15:30:37 | 1662 | 0.9 | 372.89 |
| 15:30:38 | 1662 | 1.0 | 372.90 |
| 15:30:39 | 1663 | 1.0 | 372.92 |
| 15:30:40 | 1662 | 1.0 | 372.94 |
| 15:30:41 | 1663 | 1.0 | 372.95 |
| 15:30:42 | 1662 | 0.9 | 372.97 |
| 15:30:43 | 1662 | 1.0 | 372.98 |
| 15:30:44 | 1662 | 1.0 | 373.00 |
| 15:30:45 | 1662 | 1.0 | 373.01 |
| 15:30:46 | 1662 | 0.9 | 373.03 |
| 15:30:47 | 1663 | 0.9 | 373.05 |
| 15:30:48 | 1663 | 1.0 | 373.06 |
| 15:30:49 | 1663 | 1.0 | 373.08 |
| 15:30:50 | 1663 | 1.0 | 373.09 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:30:51 | 1663 | 1.0 | 373.11 |
| 15:30:52 | 1663 | 1.0 | 373.13 |
| 15:30:53 | 1663 | 1.0 | 373.14 |
| 15:30:54 | 1663 | 0.9 | 373.16 |
| 15:30:55 | 1663 | 1.0 | 373.17 |
| 15:30:56 | 1663 | 0.9 | 373.19 |
| 15:30:57 | 1663 | 0.9 | 373.20 |
| 15:30:58 | 1663 | 0.9 | 373.22 |
| 15:30:59 | 1663 | 1.0 | 373.24 |
| 15:31:00 | 1663 | 1.0 | 373.25 |
| 15:31:01 | 1663 | 1.0 | 373.27 |
| 15:31:02 | 1663 | 1.0 | 373.28 |
| 15:31:03 | 1663 | 1.0 | 373.30 |
| 15:31:04 | 1663 | 1.0 | 373.32 |
| 15:31:05 | 1664 | 1.0 | 373.33 |
| 15:31:06 | 1663 | 1.0 | 373.35 |
| 15:31:07 | 1663 | 0.9 | 373.36 |
| 15:31:08 | 1663 | 0.9 | 373.38 |
| 15:31:09 | 1663 | 1.0 | 373.39 |
| 15:31:10 | 1664 | 1.0 | 373.41 |
| 15:31:11 | 1664 | 0.9 | 373.43 |
| 15:31:12 | 1664 | 1.0 | 373.44 |
| 15:31:13 | 1664 | 1.0 | 373.46 |
| 15:31:14 | 1664 | 1.0 | 373.47 |
| 15:31:15 | 1664 | 1.0 | 373.49 |
| 15:31:16 | 1664 | 0.9 | 373.51 |
| 15:31:17 | 1664 | 0.9 | 373.52 |
| 15:31:18 | 1664 | 0.9 | 373.54 |
| 15:31:19 | 1664 | 0.9 | 373.55 |
| 15:31:20 | 1664 | 1.0 | 373.57 |
| 15:31:21 | 1664 | 0.9 | 373.58 |
| 15:31:22 | 1664 | 1.0 | 373.60 |
| 15:31:23 | 1664 | 0.9 | 373.62 |
| 15:31:24 | 1664 | 0.9 | 373.63 |
| 15:31:25 | 1664 | 1.0 | 373.65 |
| 15:31:26 | 1665 | 1.0 | 373.66 |
| 15:31:27 | 1665 | 0.9 | 373.68 |
| 15:31:28 | 1665 | 0.9 | 373.70 |
| 15:31:29 | 1665 | 0.9 | 373.71 |
| 15:31:30 | 1665 | 1.0 | 373.73 |
| 15:31:31 | 1665 | 1.0 | 373.74 |
| 15:31:32 | 1665 | 0.9 | 373.76 |
| 15:31:33 | 1665 | 1.0 | 373.77 |
| 15:31:34 | 1665 | 1.0 | 373.79 |
| 15:31:35 | 1665 | 1.0 | 373.81 |
| 15:31:36 | 1665 | 1.0 | 373.82 |
| 15:31:37 | 1665 | 0.9 | 373.84 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:31:38 | 1665 | 1.0 | 373.85 |
| 15:31:39 | 1666 | 0.9 | 373.87 |
| 15:31:40 | 1665 | 0.9 | 373.89 |
| 15:31:41 | 1665 | 0.9 | 373.90 |
| 15:31:42 | 1665 | 0.9 | 373.92 |
| 15:31:43 | 1665 | 1.0 | 373.93 |
| 15:31:44 | 1665 | 0.9 | 373.95 |
| 15:31:45 | 1665 | 0.9 | 373.96 |
| 15:31:46 | 1665 | 1.0 | 373.98 |
| 15:31:47 | 1666 | 1.0 | 374.00 |
| 15:31:48 | 1665 | 1.0 | 374.01 |
| 15:31:49 | 1666 | 0.9 | 374.03 |
| 15:31:50 | 1666 | 0.9 | 374.04 |
| 15:31:51 | 1666 | 1.0 | 374.06 |
| 15:31:52 | 1666 | 1.0 | 374.08 |
| 15:31:53 | 1666 | 0.9 | 374.09 |
| 15:31:54 | 1666 | 0.9 | 374.11 |
| 15:31:55 | 1666 | 0.9 | 374.12 |
| 15:31:56 | 1666 | 1.0 | 374.14 |
| 15:31:57 | 1666 | 1.0 | 374.15 |
| 15:31:58 | 1666 | 0.9 | 374.17 |
| 15:31:59 | 1666 | 1.0 | 374.19 |
| 15:32:00 | 1666 | 0.9 | 374.20 |
| 15:32:01 | 1666 | 1.0 | 374.22 |
| 15:32:02 | 1666 | 1.0 | 374.23 |
| 15:32:03 | 1666 | 1.0 | 374.25 |
| 15:32:04 | 1666 | 1.0 | 374.27 |
| 15:32:05 | 1666 | 0.9 | 374.28 |
| 15:32:06 | 1666 | 0.9 | 374.30 |
| 15:32:07 | 1666 | 1.0 | 374.31 |
| 15:32:08 | 1666 | 1.0 | 374.33 |
| 15:32:09 | 1666 | 1.0 | 374.34 |
| 15:32:10 | 1666 | 1.0 | 374.36 |
| 15:32:11 | 1666 | 1.0 | 374.38 |
| 15:32:12 | 1666 | 1.0 | 374.39 |
| 15:32:13 | 1666 | 1.0 | 374.41 |
| 15:32:14 | 1666 | 0.9 | 374.42 |
| 15:32:15 | 1666 | 0.9 | 374.44 |
| 15:32:16 | 1667 | 1.0 | 374.46 |
| 15:32:17 | 1667 | 1.0 | 374.47 |
| 15:32:18 | 1667 | 1.0 | 374.49 |
| 15:32:19 | 1667 | 0.9 | 374.50 |
| 15:32:20 | 1667 | 1.0 | 374.52 |
| 15:32:21 | 1667 | 0.9 | 374.53 |
| 15:32:22 | 1667 | 1.0 | 374.55 |
| 15:32:23 | 1667 | 1.0 | 374.57 |
| 15:32:24 | 1667 | 1.0 | 374.58 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:32:25 | 1667 | 1.0 | 374.60 |
| 15:32:26 | 1667 | 0.9 | 374.61 |
| 15:32:27 | 1667 | 1.0 | 374.63 |
| 15:32:28 | 1667 | 1.0 | 374.65 |
| 15:32:29 | 1667 | 1.0 | 374.66 |
| 15:32:30 | 1667 | 0.9 | 374.68 |
| 15:32:31 | 1667 | 1.0 | 374.69 |
| 15:32:32 | 1667 | 1.0 | 374.71 |
| 15:32:33 | 1667 | 1.0 | 374.72 |
| 15:32:34 | 1667 | 0.9 | 374.74 |
| 15:32:35 | 1667 | 0.9 | 374.76 |
| 15:32:36 | 1667 | 0.9 | 374.77 |
| 15:32:37 | 1667 | 0.9 | 374.79 |
| 15:32:38 | 1667 | 1.0 | 374.80 |
| 15:32:39 | 1667 | 0.9 | 374.82 |
| 15:32:40 | 1668 | 1.0 | 374.84 |
| 15:32:41 | 1668 | 1.0 | 374.85 |
| 15:32:42 | 1668 | 0.9 | 374.87 |
| 15:32:43 | 1668 | 1.0 | 374.88 |
| 15:32:44 | 1668 | 1.0 | 374.90 |
| 15:32:45 | 1668 | 1.0 | 374.91 |
| 15:32:46 | 1668 | 0.9 | 374.93 |
| 15:32:47 | 1668 | 0.9 | 374.95 |
| 15:32:48 | 1668 | 0.9 | 374.96 |
| 15:32:49 | 1668 | 0.9 | 374.98 |
| 15:32:50 | 1668 | 0.9 | 374.99 |
| 15:32:51 | 1668 | 0.9 | 375.01 |
| 15:32:52 | 1668 | 1.0 | 375.03 |
| 15:32:53 | 1668 | 1.0 | 375.04 |
| 15:32:54 | 1668 | 1.0 | 375.06 |
| 15:32:55 | 1668 | 0.9 | 375.07 |
| 15:32:56 | 1668 | 1.0 | 375.09 |
| 15:32:57 | 1668 | 1.0 | 375.10 |
| 15:32:58 | 1668 | 0.9 | 375.12 |
| 15:32:59 | 1668 | 1.0 | 375.14 |
| 15:33:00 | 1668 | 0.9 | 375.15 |
| 15:33:01 | 1668 | 0.9 | 375.17 |
| 15:33:02 | 1668 | 0.9 | 375.18 |
| 15:33:03 | 1668 | 0.9 | 375.20 |
| 15:33:04 | 1669 | 1.0 | 375.22 |
| 15:33:05 | 1669 | 1.0 | 375.23 |
| 15:33:06 | 1669 | 1.0 | 375.25 |
| 15:33:07 | 1669 | 0.9 | 375.26 |
| 15:33:08 | 1669 | 0.9 | 375.28 |
| 15:33:09 | 1669 | 1.0 | 375.29 |
| 15:33:10 | 1669 | 0.9 | 375.31 |
| 15:33:11 | 1669 | 0.9 | 375.33 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:33:12 | 1669 | 0.9 | 375.34 |
| 15:33:13 | 1669 | 1.0 | 375.36 |
| 15:33:14 | 1669 | 1.0 | 375.37 |
| 15:33:15 | 1669 | 1.0 | 375.39 |
| 15:33:16 | 1669 | 0.9 | 375.41 |
| 15:33:17 | 1669 | 1.0 | 375.42 |
| 15:33:18 | 1669 | 1.0 | 375.44 |
| 15:33:19 | 1669 | 1.0 | 375.45 |
| 15:33:20 | 1669 | 1.0 | 375.47 |
| 15:33:21 | 1669 | 0.9 | 375.48 |
| 15:33:22 | 1669 | 0.9 | 375.50 |
| 15:33:23 | 1669 | 1.0 | 375.52 |
| 15:33:24 | 1669 | 0.9 | 375.53 |
| 15:33:25 | 1669 | 1.0 | 375.55 |
| 15:33:26 | 1669 | 1.0 | 375.56 |
| 15:33:27 | 1669 | 1.0 | 375.58 |
| 15:33:28 | 1670 | 1.0 | 375.60 |
| 15:33:29 | 1670 | 0.9 | 375.61 |
| 15:33:30 | 1670 | 1.0 | 375.63 |
| 15:33:31 | 1670 | 1.0 | 375.64 |
| 15:33:32 | 1670 | 0.9 | 375.66 |
| 15:33:33 | 1670 | 0.9 | 375.67 |
| 15:33:34 | 1670 | 0.9 | 375.69 |
| 15:33:35 | 1670 | 1.0 | 375.71 |
| 15:33:36 | 1670 | 1.0 | 375.72 |
| 15:33:37 | 1670 | 0.9 | 375.74 |
| 15:33:38 | 1670 | 1.0 | 375.75 |
| 15:33:39 | 1670 | 1.0 | 375.77 |
| 15:33:40 | 1670 | 1.0 | 375.79 |
| 15:33:41 | 1671 | 1.0 | 375.80 |
| 15:33:42 | 1670 | 0.9 | 375.82 |
| 15:33:43 | 1671 | 1.0 | 375.83 |
| 15:33:44 | 1671 | 0.9 | 375.85 |
| 15:33:45 | 1670 | 0.9 | 375.86 |
| 15:33:46 | 1670 | 0.9 | 375.88 |
| 15:33:47 | 1670 | 1.0 | 375.90 |
| 15:33:48 | 1670 | 0.9 | 375.91 |
| 15:33:49 | 1671 | 0.9 | 375.93 |
| 15:33:50 | 1671 | 1.0 | 375.94 |
| 15:33:51 | 1671 | 1.0 | 375.96 |
| 15:33:52 | 1671 | 1.0 | 375.98 |
| 15:33:53 | 1671 | 0.9 | 375.99 |
| 15:33:54 | 1671 | 0.9 | 376.01 |
| 15:33:55 | 1671 | 1.0 | 376.02 |
| 15:33:56 | 1671 | 0.9 | 376.04 |
| 15:33:57 | 1671 | 0.9 | 376.05 |
| 15:33:58 | 1671 | 0.9 | 376.07 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:33:59 | 1671 | 1.0 | 376.09 |
| 15:34:00 | 1671 | 1.0 | 376.10 |
| 15:34:01 | 1671 | 1.0 | 376.12 |
| 15:34:02 | 1671 | 1.0 | 376.13 |
| 15:34:03 | 1671 | 0.9 | 376.15 |
| 15:34:04 | 1671 | 1.0 | 376.17 |
| 15:34:05 | 1671 | 0.9 | 376.18 |
| 15:34:06 | 1672 | 0.9 | 376.20 |
| 15:34:07 | 1672 | 0.9 | 376.21 |
| 15:34:08 | 1672 | 0.9 | 376.23 |
| 15:34:09 | 1672 | 0.9 | 376.24 |
| 15:34:10 | 1672 | 0.9 | 376.26 |
| 15:34:11 | 1672 | 1.0 | 376.28 |
| 15:34:12 | 1672 | 1.0 | 376.29 |
| 15:34:13 | 1672 | 1.0 | 376.31 |
| 15:34:14 | 1671 | 0.9 | 376.32 |
| 15:34:15 | 1672 | 0.9 | 376.34 |
| 15:34:16 | 1672 | 1.0 | 376.36 |
| 15:34:17 | 1672 | 1.0 | 376.37 |
| 15:34:18 | 1672 | 0.9 | 376.39 |
| 15:34:19 | 1672 | 0.9 | 376.40 |
| 15:34:20 | 1672 | 1.0 | 376.42 |
| 15:34:21 | 1672 | 1.0 | 376.43 |
| 15:34:22 | 1672 | 1.0 | 376.45 |
| 15:34:23 | 1672 | 0.9 | 376.47 |
| 15:34:24 | 1672 | 0.9 | 376.48 |
| 15:34:25 | 1672 | 1.0 | 376.50 |
| 15:34:26 | 1672 | 1.0 | 376.51 |
| 15:34:27 | 1672 | 0.9 | 376.53 |
| 15:34:28 | 1672 | 0.9 | 376.55 |
| 15:34:29 | 1673 | 0.9 | 376.56 |
| 15:34:30 | 1673 | 0.9 | 376.58 |
| 15:34:31 | 1673 | 0.9 | 376.59 |
| 15:34:32 | 1673 | 1.0 | 376.61 |
| 15:34:33 | 1672 | 1.0 | 376.62 |
| 15:34:34 | 1672 | 1.0 | 376.64 |
| 15:34:35 | 1672 | 0.9 | 376.66 |
| 15:34:36 | 1673 | 1.0 | 376.67 |
| 15:34:37 | 1673 | 1.0 | 376.69 |
| 15:34:38 | 1673 | 1.0 | 376.70 |
| 15:34:39 | 1673 | 0.9 | 376.72 |
| 15:34:40 | 1673 | 0.9 | 376.74 |
| 15:34:41 | 1673 | 1.0 | 376.75 |
| 15:34:42 | 1673 | 1.0 | 376.77 |
| 15:34:43 | 1673 | 1.0 | 376.78 |
| 15:34:44 | 1673 | 0.9 | 376.80 |
| 15:34:45 | 1673 | 1.0 | 376.81 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:34:46 | 1673 | 1.0 | 376.83 |
| 15:34:47 | 1673 | 0.9 | 376.85 |
| 15:34:48 | 1673 | 1.0 | 376.86 |
| 15:34:49 | 1673 | 0.9 | 376.88 |
| 15:34:50 | 1673 | 0.9 | 376.89 |
| 15:34:51 | 1673 | 0.9 | 376.91 |
| 15:34:52 | 1673 | 0.9 | 376.93 |
| 15:34:53 | 1673 | 1.0 | 376.94 |
| 15:34:54 | 1674 | 1.0 | 376.96 |
| 15:34:55 | 1674 | 0.9 | 376.97 |
| 15:34:56 | 1674 | 1.0 | 376.99 |
| 15:34:57 | 1674 | 1.0 | 377.00 |
| 15:34:58 | 1674 | 1.0 | 377.02 |
| 15:34:59 | 1674 | 1.0 | 377.04 |
| 15:35:00 | 1673 | 0.9 | 377.05 |
| 15:35:01 | 1673 | 0.9 | 377.07 |
| 15:35:02 | 1673 | 0.9 | 377.08 |
| 15:35:03 | 1674 | 1.0 | 377.10 |
| 15:35:04 | 1674 | 0.9 | 377.12 |
| 15:35:05 | 1674 | 0.9 | 377.13 |
| 15:35:06 | 1674 | 0.9 | 377.15 |
| 15:35:07 | 1674 | 1.0 | 377.16 |
| 15:35:08 | 1674 | 1.0 | 377.18 |
| 15:35:09 | 1674 | 1.0 | 377.19 |
| 15:35:10 | 1674 | 1.0 | 377.21 |
| 15:35:11 | 1674 | 0.9 | 377.23 |
| 15:35:12 | 1674 | 0.9 | 377.24 |
| 15:35:13 | 1674 | 0.9 | 377.26 |
| 15:35:14 | 1674 | 0.9 | 377.27 |
| 15:35:15 | 1674 | 1.0 | 377.29 |
| 15:35:16 | 1674 | 0.9 | 377.31 |
| 15:35:17 | 1674 | 1.0 | 377.32 |
| 15:35:18 | 1675 | 1.0 | 377.34 |
| 15:35:19 | 1675 | 1.0 | 377.35 |
| 15:35:20 | 1675 | 1.0 | 377.37 |
| 15:35:21 | 1675 | 0.9 | 377.38 |
| 15:35:22 | 1675 | 1.0 | 377.40 |
| 15:35:23 | 1675 | 0.9 | 377.42 |
| 15:35:24 | 1675 | 1.0 | 377.43 |
| 15:35:25 | 1675 | 0.9 | 377.45 |
| 15:35:26 | 1675 | 0.9 | 377.46 |
| 15:35:27 | 1675 | 1.0 | 377.48 |
| 15:35:28 | 1674 | 0.9 | 377.50 |
| 15:35:29 | 1675 | 1.0 | 377.51 |
| 15:35:30 | 1675 | 1.0 | 377.53 |
| 15:35:31 | 1675 | 1.0 | 377.54 |
| 15:35:32 | 1675 | 1.0 | 377.56 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:35:33 | 1675 | 0.9 | 377.57 |
| 15:35:34 | 1675 | 0.9 | 377.59 |
| 15:35:35 | 1675 | 0.9 | 377.61 |
| 15:35:36 | 1675 | 0.9 | 377.62 |
| 15:35:37 | 1675 | 0.9 | 377.64 |
| 15:35:38 | 1675 | 1.0 | 377.65 |
| 15:35:39 | 1675 | 1.0 | 377.67 |
| 15:35:40 | 1675 | 1.0 | 377.69 |
| 15:35:41 | 1675 | 1.0 | 377.70 |
| 15:35:42 | 1676 | 0.9 | 377.72 |
| 15:35:43 | 1676 | 1.0 | 377.73 |
| 15:35:44 | 1676 | 1.0 | 377.75 |
| 15:35:45 | 1676 | 0.9 | 377.76 |
| 15:35:46 | 1676 | 0.9 | 377.78 |
| 15:35:47 | 1676 | 0.9 | 377.80 |
| 15:35:48 | 1676 | 0.9 | 377.81 |
| 15:35:49 | 1676 | 1.0 | 377.83 |
| 15:35:50 | 1676 | 1.0 | 377.84 |
| 15:35:51 | 1675 | 1.0 | 377.86 |
| 15:35:52 | 1676 | 1.0 | 377.88 |
| 15:35:53 | 1676 | 1.0 | 377.89 |
| 15:35:54 | 1676 | 0.9 | 377.91 |
| 15:35:55 | 1676 | 1.0 | 377.92 |
| 15:35:56 | 1676 | 1.0 | 377.94 |
| 15:35:57 | 1676 | 0.9 | 377.95 |
| 15:35:58 | 1676 | 0.9 | 377.97 |
| 15:35:59 | 1676 | 0.9 | 377.99 |
| 15:36:00 | 1676 | 1.0 | 378.00 |
| 15:36:01 | 1676 | 1.0 | 378.02 |
| 15:36:02 | 1676 | 0.9 | 378.03 |
| 15:36:03 | 1676 | 0.9 | 378.05 |
| 15:36:04 | 1676 | 1.0 | 378.07 |
| 15:36:05 | 1676 | 1.0 | 378.08 |
| 15:36:06 | 1676 | 0.9 | 378.10 |
| 15:36:07 | 1676 | 0.9 | 378.11 |
| 15:36:08 | 1676 | 0.9 | 378.13 |
| 15:36:09 | 1676 | 0.9 | 378.14 |
| 15:36:10 | 1676 | 0.9 | 378.16 |
| 15:36:11 | 1676 | 0.9 | 378.18 |
| 15:36:12 | 1676 | 1.0 | 378.19 |
| 15:36:13 | 1676 | 1.0 | 378.21 |
| 15:36:14 | 1676 | 0.9 | 378.22 |
| 15:36:15 | 1676 | 0.9 | 378.24 |
| 15:36:16 | 1676 | 1.0 | 378.26 |
| 15:36:17 | 1676 | 1.0 | 378.27 |
| 15:36:18 | 1677 | 0.9 | 378.29 |
| 15:36:19 | 1677 | 0.9 | 378.30 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:36:20 | 1677 | 0.9 | 378.32 |
| 15:36:21 | 1677 | 0.9 | 378.33 |
| 15:36:22 | 1677 | 1.0 | 378.35 |
| 15:36:23 | 1677 | 0.9 | 378.37 |
| 15:36:24 | 1677 | 0.9 | 378.38 |
| 15:36:25 | 1677 | 1.0 | 378.40 |
| 15:36:26 | 1677 | 1.0 | 378.41 |
| 15:36:27 | 1677 | 1.0 | 378.43 |
| 15:36:28 | 1677 | 0.9 | 378.45 |
| 15:36:29 | 1677 | 1.0 | 378.46 |
| 15:36:30 | 1677 | 0.9 | 378.48 |
| 15:36:31 | 1677 | 0.9 | 378.49 |
| 15:36:32 | 1677 | 0.9 | 378.51 |
| 15:36:33 | 1677 | 0.9 | 378.52 |
| 15:36:34 | 1677 | 0.9 | 378.54 |
| 15:36:35 | 1677 | 0.9 | 378.56 |
| 15:36:36 | 1677 | 0.9 | 378.57 |
| 15:36:37 | 1677 | 1.0 | 378.59 |
| 15:36:38 | 1677 | 1.0 | 378.60 |
| 15:36:39 | 1677 | 0.9 | 378.62 |
| 15:36:40 | 1677 | 0.9 | 378.64 |
| 15:36:41 | 1678 | 0.9 | 378.65 |
| 15:36:42 | 1678 | 0.9 | 378.67 |
| 15:36:43 | 1678 | 0.9 | 378.68 |
| 15:36:44 | 1678 | 0.9 | 378.70 |
| 15:36:45 | 1678 | 0.9 | 378.71 |
| 15:36:46 | 1678 | 1.0 | 378.73 |
| 15:36:47 | 1678 | 1.0 | 378.75 |
| 15:36:48 | 1678 | 1.0 | 378.76 |
| 15:36:49 | 1678 | 1.0 | 378.78 |
| 15:36:50 | 1678 | 1.0 | 378.79 |
| 15:36:51 | 1678 | 1.0 | 378.81 |
| 15:36:52 | 1678 | 1.0 | 378.83 |
| 15:36:53 | 1678 | 0.9 | 378.84 |
| 15:36:54 | 1678 | 0.9 | 378.86 |
| 15:36:55 | 1679 | 0.9 | 378.87 |
| 15:36:56 | 1679 | 0.9 | 378.89 |
| 15:36:57 | 1679 | 0.9 | 378.90 |
| 15:36:58 | 1679 | 1.0 | 378.92 |
| 15:36:59 | 1679 | 1.0 | 378.94 |
| 15:37:00 | 1679 | 0.9 | 378.95 |
| 15:37:01 | 1679 | 1.0 | 378.97 |
| 15:37:02 | 1679 | 0.9 | 378.98 |
| 15:37:03 | 1679 | 1.0 | 379.00 |
| 15:37:04 | 1679 | 1.0 | 379.02 |
| 15:37:05 | 1679 | 0.9 | 379.03 |
| 15:37:06 | 1679 | 0.9 | 379.05 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:37:07 | 1679 | 1.0 | 379.06 |
| 15:37:08 | 1679 | 1.0 | 379.08 |
| 15:37:09 | 1679 | 0.9 | 379.09 |
| 15:37:10 | 1679 | 0.9 | 379.11 |
| 15:37:11 | 1679 | 1.0 | 379.13 |
| 15:37:12 | 1679 | 1.0 | 379.14 |
| 15:37:13 | 1679 | 0.9 | 379.16 |
| 15:37:14 | 1679 | 0.9 | 379.17 |
| 15:37:15 | 1679 | 1.0 | 379.19 |
| 15:37:16 | 1679 | 0.9 | 379.21 |
| 15:37:17 | 1679 | 0.9 | 379.22 |
| 15:37:18 | 1680 | 1.0 | 379.24 |
| 15:37:19 | 1680 | 1.0 | 379.25 |
| 15:37:20 | 1680 | 1.0 | 379.27 |
| 15:37:21 | 1680 | 0.9 | 379.28 |
| 15:37:22 | 1680 | 1.0 | 379.30 |
| 15:37:23 | 1680 | 1.0 | 379.32 |
| 15:37:24 | 1680 | 1.0 | 379.33 |
| 15:37:25 | 1680 | 0.9 | 379.35 |
| 15:37:26 | 1680 | 0.9 | 379.36 |
| 15:37:27 | 1680 | 0.9 | 379.38 |
| 15:37:28 | 1680 | 1.0 | 379.40 |
| 15:37:29 | 1680 | 0.9 | 379.41 |
| 15:37:30 | 1680 | 0.9 | 379.43 |
| 15:37:31 | 1680 | 0.9 | 379.44 |
| 15:37:32 | 1680 | 1.0 | 379.46 |
| 15:37:33 | 1680 | 1.0 | 379.47 |
| 15:37:34 | 1680 | 1.0 | 379.49 |
| 15:37:35 | 1680 | 0.9 | 379.51 |
| 15:37:36 | 1681 | 1.0 | 379.52 |
| 15:37:37 | 1680 | 0.9 | 379.54 |
| 15:37:38 | 1680 | 0.9 | 379.55 |
| 15:37:39 | 1680 | 1.0 | 379.57 |
| 15:37:40 | 1680 | 0.9 | 379.59 |
| 15:37:41 | 1680 | 0.9 | 379.60 |
| 15:37:42 | 1680 | 0.9 | 379.62 |
| 15:37:43 | 1680 | 1.0 | 379.63 |
| 15:37:44 | 1681 | 1.0 | 379.65 |
| 15:37:45 | 1681 | 1.0 | 379.66 |
| 15:37:46 | 1681 | 0.9 | 379.68 |
| 15:37:47 | 1681 | 0.9 | 379.70 |
| 15:37:48 | 1681 | 1.0 | 379.71 |
| 15:37:49 | 1681 | 1.0 | 379.73 |
| 15:37:50 | 1681 | 0.9 | 379.74 |
| 15:37:51 | 1681 | 0.9 | 379.76 |
| 15:37:52 | 1681 | 0.9 | 379.78 |
| 15:37:53 | 1681 | 1.0 | 379.79 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:37:54 | 1681 | 1.0 | 379.81 |
| 15:37:55 | 1681 | 1.0 | 379.82 |
| 15:37:56 | 1681 | 1.0 | 379.84 |
| 15:37:57 | 1681 | 1.0 | 379.85 |
| 15:37:58 | 1681 | 0.9 | 379.87 |
| 15:37:59 | 1681 | 0.9 | 379.89 |
| 15:38:00 | 1681 | 1.0 | 379.90 |
| 15:38:01 | 1681 | 1.0 | 379.92 |
| 15:38:02 | 1681 | 0.9 | 379.93 |
| 15:38:03 | 1681 | 0.9 | 379.95 |
| 15:38:04 | 1681 | 1.0 | 379.97 |
| 15:38:05 | 1681 | 1.0 | 379.98 |
| 15:38:06 | 1681 | 1.0 | 380.00 |
| 15:38:07 | 1681 | 1.0 | 380.01 |
| 15:38:08 | 1681 | 0.9 | 380.03 |
| 15:38:09 | 1681 | 1.0 | 380.04 |
| 15:38:10 | 1681 | 0.9 | 380.06 |
| 15:38:11 | 1682 | 0.9 | 380.08 |
| 15:38:12 | 1682 | 0.9 | 380.09 |
| 15:38:13 | 1682 | 0.9 | 380.11 |
| 15:38:14 | 1682 | 0.9 | 380.12 |
| 15:38:15 | 1682 | 1.0 | 380.14 |
| 15:38:16 | 1682 | 0.9 | 380.16 |
| 15:38:17 | 1682 | 1.0 | 380.17 |
| 15:38:18 | 1682 | 1.0 | 380.19 |
| 15:38:19 | 1682 | 1.0 | 380.20 |
| 15:38:20 | 1682 | 1.0 | 380.22 |
| 15:38:21 | 1682 | 1.0 | 380.23 |
| 15:38:22 | 1682 | 1.0 | 380.25 |
| 15:38:23 | 1682 | 0.9 | 380.27 |
| 15:38:24 | 1682 | 0.9 | 380.28 |
| 15:38:25 | 1682 | 1.0 | 380.30 |
| 15:38:26 | 1682 | 1.0 | 380.31 |
| 15:38:27 | 1682 | 1.0 | 380.33 |
| 15:38:28 | 1682 | 0.9 | 380.35 |
| 15:38:29 | 1682 | 1.0 | 380.36 |
| 15:38:30 | 1682 | 1.0 | 380.38 |
| 15:38:31 | 1682 | 1.0 | 380.39 |
| 15:38:32 | 1682 | 0.9 | 380.41 |
| 15:38:33 | 1682 | 0.9 | 380.42 |
| 15:38:34 | 1682 | 0.9 | 380.44 |
| 15:38:35 | 1683 | 0.9 | 380.46 |
| 15:38:36 | 1682 | 0.9 | 380.47 |
| 15:38:37 | 1682 | 0.9 | 380.49 |
| 15:38:38 | 1682 | 1.0 | 380.50 |
| 15:38:39 | 1682 | 0.9 | 380.52 |
| 15:38:40 | 1683 | 1.0 | 380.54 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:38:41 | 1682 | 1.0 | 380.55 |
| 15:38:42 | 1682 | 1.0 | 380.57 |
| 15:38:43 | 1683 | 1.0 | 380.58 |
| 15:38:44 | 1682 | 0.9 | 380.60 |
| 15:38:45 | 1683 | 0.9 | 380.61 |
| 15:38:46 | 1683 | 0.9 | 380.63 |
| 15:38:47 | 1683 | 1.0 | 380.65 |
| 15:38:48 | 1683 | 0.9 | 380.66 |
| 15:38:49 | 1683 | 0.9 | 380.68 |
| 15:38:50 | 1683 | 1.0 | 380.69 |
| 15:38:51 | 1683 | 1.0 | 380.71 |
| 15:38:52 | 1683 | 1.0 | 380.73 |
| 15:38:53 | 1683 | 0.9 | 380.74 |
| 15:38:54 | 1683 | 0.9 | 380.76 |
| 15:38:55 | 1683 | 1.0 | 380.77 |
| 15:38:56 | 1683 | 0.9 | 380.79 |
| 15:38:57 | 1683 | 0.9 | 380.80 |
| 15:38:58 | 1683 | 0.9 | 380.82 |
| 15:38:59 | 1684 | 1.0 | 380.84 |
| 15:39:00 | 1684 | 0.9 | 380.85 |
| 15:39:01 | 1684 | 0.9 | 380.87 |
| 15:39:02 | 1683 | 1.0 | 380.88 |
| 15:39:03 | 1683 | 1.0 | 380.90 |
| 15:39:04 | 1683 | 1.0 | 380.92 |
| 15:39:05 | 1683 | 0.9 | 380.93 |
| 15:39:06 | 1683 | 0.9 | 380.95 |
| 15:39:07 | 1684 | 0.9 | 380.96 |
| 15:39:08 | 1684 | 0.9 | 380.98 |
| 15:39:09 | 1684 | 0.9 | 380.99 |
| 15:39:10 | 1684 | 0.9 | 381.01 |
| 15:39:11 | 1684 | 0.9 | 381.03 |
| 15:39:12 | 1684 | 1.0 | 381.04 |
| 15:39:13 | 1684 | 1.0 | 381.06 |
| 15:39:14 | 1684 | 0.9 | 381.07 |
| 15:39:15 | 1684 | 0.9 | 381.09 |
| 15:39:16 | 1684 | 1.0 | 381.11 |
| 15:39:17 | 1684 | 1.0 | 381.12 |
| 15:39:18 | 1684 | 0.9 | 381.14 |
| 15:39:19 | 1684 | 0.9 | 381.15 |
| 15:39:20 | 1684 | 0.9 | 381.17 |
| 15:39:21 | 1684 | 0.9 | 381.18 |
| 15:39:22 | 1684 | 0.9 | 381.20 |
| 15:39:23 | 1685 | 1.0 | 381.22 |
| 15:39:24 | 1684 | 1.0 | 381.23 |
| 15:39:25 | 1684 | 1.0 | 381.25 |
| 15:39:26 | 1684 | 0.9 | 381.26 |
| 15:39:27 | 1684 | 1.0 | 381.28 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:39:28 | 1684 | 0.9 | 381.29 |
| 15:39:29 | 1684 | 0.9 | 381.31 |
| 15:39:30 | 1684 | 0.9 | 381.33 |
| 15:39:31 | 1684 | 0.9 | 381.34 |
| 15:39:32 | 1684 | 0.9 | 381.36 |
| 15:39:33 | 1684 | 1.0 | 381.37 |
| 15:39:34 | 1685 | 0.9 | 381.39 |
| 15:39:35 | 1685 | 1.0 | 381.41 |
| 15:39:36 | 1685 | 1.0 | 381.42 |
| 15:39:37 | 1685 | 1.0 | 381.44 |
| 15:39:38 | 1685 | 1.0 | 381.45 |
| 15:39:39 | 1685 | 0.9 | 381.47 |
| 15:39:40 | 1685 | 0.9 | 381.48 |
| 15:39:41 | 1685 | 0.9 | 381.50 |
| 15:39:42 | 1684 | 0.9 | 381.52 |
| 15:39:43 | 1685 | 1.0 | 381.53 |
| 15:39:44 | 1685 | 0.9 | 381.55 |
| 15:39:45 | 1685 | 1.0 | 381.56 |
| 15:39:46 | 1685 | 1.0 | 381.58 |
| 15:39:47 | 1685 | 0.9 | 381.60 |
| 15:39:48 | 1685 | 1.0 | 381.61 |
| 15:39:49 | 1685 | 1.0 | 381.63 |
| 15:39:50 | 1685 | 0.9 | 381.64 |
| 15:39:51 | 1685 | 0.9 | 381.66 |
| 15:39:52 | 1685 | 0.9 | 381.67 |
| 15:39:53 | 1685 | 0.9 | 381.69 |
| 15:39:54 | 1685 | 1.0 | 381.71 |
| 15:39:55 | 1685 | 0.9 | 381.72 |
| 15:39:56 | 1685 | 0.9 | 381.74 |
| 15:39:57 | 1686 | 1.0 | 381.75 |
| 15:39:58 | 1686 | 0.9 | 381.77 |
| 15:39:59 | 1686 | 1.0 | 381.79 |
| 15:40:00 | 1686 | 1.0 | 381.80 |
| 15:40:01 | 1686 | 1.0 | 381.82 |
| 15:40:02 | 1686 | 0.9 | 381.83 |
| 15:40:03 | 1685 | 0.9 | 381.85 |
| 15:40:04 | 1686 | 0.9 | 381.86 |
| 15:40:05 | 1686 | 1.0 | 381.88 |
| 15:40:06 | 1686 | 1.0 | 381.90 |
| 15:40:07 | 1686 | 0.9 | 381.91 |
| 15:40:08 | 1686 | 0.9 | 381.93 |
| 15:40:09 | 1686 | 1.0 | 381.94 |
| 15:40:10 | 1686 | 1.0 | 381.96 |
| 15:40:11 | 1686 | 0.9 | 381.98 |
| 15:40:12 | 1686 | 0.9 | 381.99 |
| 15:40:13 | 1686 | 0.9 | 382.01 |
| 15:40:14 | 1686 | 0.9 | 382.02 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:40:15 | 1686 | 0.9 | 382.04 |
| 15:40:16 | 1686 | 0.9 | 382.05 |
| 15:40:17 | 1686 | 0.9 | 382.07 |
| 15:40:18 | 1686 | 0.9 | 382.09 |
| 15:40:19 | 1686 | 0.9 | 382.10 |
| 15:40:20 | 1686 | 1.0 | 382.12 |
| 15:40:21 | 1686 | 0.9 | 382.13 |
| 15:40:22 | 1686 | 1.0 | 382.15 |
| 15:40:23 | 1687 | 0.9 | 382.17 |
| 15:40:24 | 1687 | 0.9 | 382.18 |
| 15:40:25 | 1687 | 0.9 | 382.20 |
| 15:40:26 | 1687 | 0.9 | 382.21 |
| 15:40:27 | 1686 | 0.9 | 382.23 |
| 15:40:28 | 1686 | 0.9 | 382.24 |
| 15:40:29 | 1686 | 0.9 | 382.26 |
| 15:40:30 | 1686 | 1.0 | 382.28 |
| 15:40:31 | 1687 | 1.0 | 382.29 |
| 15:40:32 | 1687 | 0.9 | 382.31 |
| 15:40:33 | 1687 | 0.9 | 382.32 |
| 15:40:34 | 1687 | 0.9 | 382.34 |
| 15:40:35 | 1687 | 0.9 | 382.36 |
| 15:40:36 | 1687 | 1.0 | 382.37 |
| 15:40:37 | 1687 | 0.9 | 382.39 |
| 15:40:38 | 1687 | 0.9 | 382.40 |
| 15:40:39 | 1687 | 0.9 | 382.42 |
| 15:40:40 | 1687 | 0.9 | 382.43 |
| 15:40:41 | 1687 | 1.0 | 382.45 |
| 15:40:42 | 1687 | 1.0 | 382.47 |
| 15:40:43 | 1687 | 1.0 | 382.48 |
| 15:40:44 | 1687 | 1.0 | 382.50 |
| 15:40:45 | 1687 | 0.9 | 382.51 |
| 15:40:46 | 1687 | 0.9 | 382.53 |
| 15:40:47 | 1687 | 0.9 | 382.55 |
| 15:40:48 | 1687 | 0.9 | 382.56 |
| 15:40:49 | 1687 | 0.9 | 382.58 |
| 15:40:50 | 1687 | 0.9 | 382.59 |
| 15:40:51 | 1687 | 1.0 | 382.61 |
| 15:40:52 | 1688 | 1.0 | 382.62 |
| 15:40:53 | 1687 | 0.9 | 382.64 |
| 15:40:54 | 1687 | 0.9 | 382.66 |
| 15:40:55 | 1687 | 1.0 | 382.67 |
| 15:40:56 | 1687 | 1.0 | 382.69 |
| 15:40:57 | 1687 | 0.9 | 382.70 |
| 15:40:58 | 1687 | 0.9 | 382.72 |
| 15:40:59 | 1688 | 0.9 | 382.74 |
| 15:41:00 | 1688 | 0.9 | 382.75 |
| 15:41:01 | 1688 | 0.9 | 382.77 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:41:02 | 1688 | 0.9 | 382.78 |
| 15:41:03 | 1688 | 0.9 | 382.80 |
| 15:41:04 | 1687 | 1.0 | 382.81 |
| 15:41:05 | 1687 | 0.9 | 382.83 |
| 15:41:06 | 1687 | 0.9 | 382.85 |
| 15:41:07 | 1688 | 0.9 | 382.86 |
| 15:41:08 | 1688 | 0.9 | 382.88 |
| 15:41:09 | 1688 | 0.9 | 382.89 |
| 15:41:10 | 1688 | 0.9 | 382.91 |
| 15:41:11 | 1688 | 0.9 | 382.93 |
| 15:41:12 | 1688 | 0.9 | 382.94 |
| 15:41:13 | 1688 | 1.0 | 382.96 |
| 15:41:14 | 1688 | 0.9 | 382.97 |
| 15:41:15 | 1688 | 0.9 | 382.99 |
| 15:41:16 | 1688 | 0.9 | 383.00 |
| 15:41:17 | 1688 | 1.0 | 383.02 |
| 15:41:18 | 1688 | 0.9 | 383.04 |
| 15:41:19 | 1688 | 0.9 | 383.05 |
| 15:41:20 | 1688 | 0.9 | 383.07 |
| 15:41:21 | 1688 | 0.9 | 383.08 |
| 15:41:22 | 1688 | 0.9 | 383.10 |
| 15:41:23 | 1688 | 0.9 | 383.12 |
| 15:41:24 | 1689 | 0.9 | 383.13 |
| 15:41:25 | 1689 | 1.0 | 383.15 |
| 15:41:26 | 1688 | 0.9 | 383.16 |
| 15:41:27 | 1688 | 1.0 | 383.18 |
| 15:41:28 | 1688 | 1.0 | 383.19 |
| 15:41:29 | 1688 | 1.0 | 383.21 |
| 15:41:30 | 1688 | 0.9 | 383.23 |
| 15:41:31 | 1688 | 0.9 | 383.24 |
| 15:41:32 | 1688 | 0.9 | 383.26 |
| 15:41:33 | 1688 | 0.9 | 383.27 |
| 15:41:34 | 1688 | 0.9 | 383.29 |
| 15:41:35 | 1688 | 0.9 | 383.31 |
| 15:41:36 | 1689 | 0.9 | 383.32 |
| 15:41:37 | 1689 | 1.0 | 383.34 |
| 15:41:38 | 1689 | 1.0 | 383.35 |
| 15:41:39 | 1689 | 0.9 | 383.37 |
| 15:41:40 | 1689 | 0.9 | 383.38 |
| 15:41:41 | 1689 | 0.9 | 383.40 |
| 15:41:42 | 1688 | 0.9 | 383.42 |
| 15:41:43 | 1689 | 0.9 | 383.43 |
| 15:41:44 | 1688 | 0.9 | 383.45 |
| 15:41:45 | 1689 | 0.9 | 383.46 |
| 15:41:46 | 1689 | 0.9 | 383.48 |
| 15:41:47 | 1689 | 0.9 | 383.50 |
| 15:41:48 | 1689 | 1.0 | 383.51 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:41:49 | 1689 | 1.0 | 383.53 |
| 15:41:50 | 1689 | 1.0 | 383.54 |
| 15:41:51 | 1689 | 0.9 | 383.56 |
| 15:41:52 | 1689 | 0.9 | 383.57 |
| 15:41:53 | 1689 | 0.9 | 383.59 |
| 15:41:54 | 1689 | 0.9 | 383.61 |
| 15:41:55 | 1689 | 0.9 | 383.62 |
| 15:41:56 | 1689 | 0.9 | 383.64 |
| 15:41:57 | 1689 | 0.9 | 383.65 |
| 15:41:58 | 1689 | 0.9 | 383.67 |
| 15:41:59 | 1689 | 1.0 | 383.69 |
| 15:42:00 | 1689 | 0.9 | 383.70 |
| 15:42:01 | 1689 | 1.0 | 383.72 |
| 15:42:02 | 1689 | 0.9 | 383.73 |
| 15:42:03 | 1689 | 1.0 | 383.75 |
| 15:42:04 | 1689 | 1.0 | 383.76 |
| 15:42:05 | 1689 | 0.9 | 383.78 |
| 15:42:06 | 1689 | 0.9 | 383.80 |
| 15:42:07 | 1689 | 0.9 | 383.81 |
| 15:42:08 | 1689 | 0.9 | 383.83 |
| 15:42:09 | 1689 | 1.0 | 383.84 |
| 15:42:10 | 1689 | 1.0 | 383.86 |
| 15:42:11 | 1689 | 1.0 | 383.87 |
| 15:42:12 | 1689 | 0.9 | 383.89 |
| 15:42:13 | 1689 | 0.9 | 383.91 |
| 15:42:14 | 1689 | 1.0 | 383.92 |
| 15:42:15 | 1689 | 1.0 | 383.94 |
| 15:42:16 | 1689 | 0.9 | 383.95 |
| 15:42:17 | 1689 | 0.9 | 383.97 |
| 15:42:18 | 1689 | 0.9 | 383.99 |
| 15:42:19 | 1689 | 0.9 | 384.00 |
| 15:42:20 | 1689 | 1.0 | 384.02 |
| 15:42:21 | 1689 | 0.9 | 384.03 |
| 15:42:22 | 1689 | 1.0 | 384.05 |
| 15:42:23 | 1690 | 1.0 | 384.06 |
| 15:42:24 | 1690 | 1.0 | 384.08 |
| 15:42:25 | 1690 | 1.0 | 384.10 |
| 15:42:26 | 1690 | 0.9 | 384.11 |
| 15:42:27 | 1690 | 0.9 | 384.13 |
| 15:42:28 | 1690 | 0.9 | 384.14 |
| 15:42:29 | 1690 | 0.9 | 384.16 |
| 15:42:30 | 1690 | 0.9 | 384.18 |
| 15:42:31 | 1690 | 0.9 | 384.19 |
| 15:42:32 | 1690 | 1.0 | 384.21 |
| 15:42:33 | 1690 | 0.9 | 384.22 |
| 15:42:34 | 1690 | 0.9 | 384.24 |
| 15:42:35 | 1690 | 1.0 | 384.25 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:42:36 | 1690 | 1.0 | 384.27 |
| 15:42:37 | 1690 | 0.9 | 384.29 |
| 15:42:38 | 1690 | 0.9 | 384.30 |
| 15:42:39 | 1690 | 0.9 | 384.32 |
| 15:42:40 | 1690 | 0.9 | 384.33 |
| 15:42:41 | 1690 | 0.9 | 384.35 |
| 15:42:42 | 1690 | 0.9 | 384.37 |
| 15:42:43 | 1690 | 0.9 | 384.38 |
| 15:42:44 | 1690 | 1.0 | 384.40 |
| 15:42:45 | 1690 | 1.0 | 384.41 |
| 15:42:46 | 1690 | 0.9 | 384.43 |
| 15:42:47 | 1690 | 0.9 | 384.44 |
| 15:42:48 | 1691 | 1.0 | 384.46 |
| 15:42:49 | 1691 | 0.9 | 384.48 |
| 15:42:50 | 1690 | 0.9 | 384.49 |
| 15:42:51 | 1691 | 0.9 | 384.51 |
| 15:42:52 | 1691 | 0.9 | 384.52 |
| 15:42:53 | 1690 | 0.9 | 384.54 |
| 15:42:54 | 1691 | 0.9 | 384.56 |
| 15:42:55 | 1691 | 0.9 | 384.57 |
| 15:42:56 | 1691 | 1.0 | 384.59 |
| 15:42:57 | 1691 | 1.0 | 384.60 |
| 15:42:58 | 1691 | 0.9 | 384.62 |
| 15:42:59 | 1691 | 0.9 | 384.63 |
| 15:43:00 | 1691 | 0.9 | 384.65 |
| 15:43:01 | 1691 | 0.9 | 384.67 |
| 15:43:02 | 1691 | 0.9 | 384.68 |
| 15:43:03 | 1691 | 0.9 | 384.70 |
| 15:43:04 | 1691 | 0.9 | 384.71 |
| 15:43:05 | 1691 | 0.9 | 384.73 |
| 15:43:06 | 1690 | 1.0 | 384.75 |
| 15:43:07 | 1690 | 0.9 | 384.76 |
| 15:43:08 | 1691 | 0.9 | 384.78 |
| 15:43:09 | 1691 | 1.0 | 384.79 |
| 15:43:10 | 1691 | 0.9 | 384.81 |
| 15:43:11 | 1691 | 0.9 | 384.82 |
| 15:43:12 | 1691 | 0.9 | 384.84 |
| 15:43:13 | 1691 | 1.0 | 384.86 |
| 15:43:14 | 1691 | 0.9 | 384.87 |
| 15:43:15 | 1691 | 0.9 | 384.89 |
| 15:43:16 | 1691 | 0.9 | 384.90 |
| 15:43:17 | 1691 | 1.0 | 384.92 |
| 15:43:18 | 1691 | 1.0 | 384.94 |
| 15:43:19 | 1691 | 0.9 | 384.95 |
| 15:43:20 | 1691 | 0.9 | 384.97 |
| 15:43:21 | 1691 | 1.0 | 384.98 |
| 15:43:22 | 1691 | 1.0 | 385.00 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:43:23 | 1691 | 0.9 | 385.01 |
| 15:43:24 | 1691 | 0.9 | 385.03 |
| 15:43:25 | 1691 | 0.9 | 385.05 |
| 15:43:26 | 1692 | 1.0 | 385.06 |
| 15:43:27 | 1691 | 1.0 | 385.08 |
| 15:43:28 | 1691 | 0.9 | 385.09 |
| 15:43:29 | 1691 | 0.9 | 385.11 |
| 15:43:30 | 1691 | 1.0 | 385.13 |
| 15:43:31 | 1691 | 1.0 | 385.14 |
| 15:43:32 | 1691 | 1.0 | 385.16 |
| 15:43:33 | 1692 | 1.0 | 385.17 |
| 15:43:34 | 1692 | 0.9 | 385.19 |
| 15:43:35 | 1691 | 0.9 | 385.20 |
| 15:43:36 | 1691 | 0.9 | 385.22 |
| 15:43:37 | 1692 | 0.9 | 385.24 |
| 15:43:38 | 1692 | 1.0 | 385.25 |
| 15:43:39 | 1692 | 0.9 | 385.27 |
| 15:43:40 | 1692 | 1.0 | 385.28 |
| 15:43:41 | 1691 | 0.9 | 385.30 |
| 15:43:42 | 1691 | 1.0 | 385.32 |
| 15:43:43 | 1691 | 1.0 | 385.33 |
| 15:43:44 | 1691 | 0.9 | 385.35 |
| 15:43:45 | 1691 | 0.9 | 385.36 |
| 15:43:46 | 1691 | 0.9 | 385.38 |
| 15:43:47 | 1692 | 0.9 | 385.39 |
| 15:43:48 | 1692 | 0.9 | 385.41 |
| 15:43:49 | 1692 | 0.9 | 385.43 |
| 15:43:50 | 1692 | 0.9 | 385.44 |
| 15:43:51 | 1692 | 0.9 | 385.46 |
| 15:43:52 | 1692 | 1.0 | 385.47 |
| 15:43:53 | 1692 | 1.0 | 385.49 |
| 15:43:54 | 1691 | 1.0 | 385.51 |
| 15:43:55 | 1692 | 0.9 | 385.52 |
| 15:43:56 | 1692 | 0.9 | 385.54 |
| 15:43:57 | 1692 | 0.9 | 385.55 |
| 15:43:58 | 1692 | 0.9 | 385.57 |
| 15:43:59 | 1692 | 1.0 | 385.58 |
| 15:44:00 | 1692 | 0.9 | 385.60 |
| 15:44:01 | 1692 | 0.9 | 385.62 |
| 15:44:02 | 1692 | 0.9 | 385.63 |
| 15:44:03 | 1692 | 0.9 | 385.65 |
| 15:44:04 | 1692 | 1.0 | 385.66 |
| 15:44:05 | 1692 | 0.9 | 385.68 |
| 15:44:06 | 1692 | 0.9 | 385.70 |
| 15:44:07 | 1692 | 0.9 | 385.71 |
| 15:44:08 | 1692 | 0.9 | 385.73 |
| 15:44:09 | 1692 | 0.9 | 385.74 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:44:10 | 1692 | 0.9 | 385.76 |
| 15:44:11 | 1692 | 0.9 | 385.77 |
| 15:44:12 | 1692 | 0.9 | 385.79 |
| 15:44:13 | 1692 | 0.9 | 385.81 |
| 15:44:14 | 1692 | 1.0 | 385.82 |
| 15:44:15 | 1692 | 0.9 | 385.84 |
| 15:44:16 | 1692 | 0.9 | 385.85 |
| 15:44:17 | 1692 | 0.9 | 385.87 |
| 15:44:18 | 1692 | 0.9 | 385.89 |
| 15:44:19 | 1692 | 0.9 | 385.90 |
| 15:44:20 | 1692 | 0.9 | 385.92 |
| 15:44:21 | 1692 | 0.9 | 385.93 |
| 15:44:22 | 1692 | 0.9 | 385.95 |
| 15:44:23 | 1692 | 0.9 | 385.96 |
| 15:44:24 | 1693 | 0.9 | 385.98 |
| 15:44:25 | 1693 | 1.0 | 386.00 |
| 15:44:26 | 1693 | 0.9 | 386.01 |
| 15:44:27 | 1693 | 0.9 | 386.03 |
| 15:44:28 | 1693 | 0.9 | 386.04 |
| 15:44:29 | 1693 | 0.9 | 386.06 |
| 15:44:30 | 1692 | 0.9 | 386.08 |
| 15:44:31 | 1692 | 0.9 | 386.09 |
| 15:44:32 | 1692 | 0.9 | 386.11 |
| 15:44:33 | 1693 | 0.9 | 386.12 |
| 15:44:34 | 1693 | 0.9 | 386.14 |
| 15:44:35 | 1693 | 1.0 | 386.15 |
| 15:44:36 | 1693 | 1.0 | 386.17 |
| 15:44:37 | 1693 | 0.9 | 386.19 |
| 15:44:38 | 1693 | 0.9 | 386.20 |
| 15:44:39 | 1693 | 0.9 | 386.22 |
| 15:44:40 | 1693 | 0.9 | 386.23 |
| 15:44:41 | 1693 | 0.9 | 386.25 |
| 15:44:42 | 1693 | 0.9 | 386.26 |
| 15:44:43 | 1693 | 0.9 | 386.28 |
| 15:44:44 | 1693 | 0.9 | 386.30 |
| 15:44:45 | 1693 | 0.9 | 386.31 |
| 15:44:46 | 1693 | 1.0 | 386.33 |
| 15:44:47 | 1693 | 0.9 | 386.34 |
| 15:44:48 | 1693 | 1.0 | 386.36 |
| 15:44:49 | 1693 | 0.9 | 386.38 |
| 15:44:50 | 1693 | 1.0 | 386.39 |
| 15:44:51 | 1693 | 0.9 | 386.41 |
| 15:44:52 | 1693 | 0.9 | 386.42 |
| 15:44:53 | 1693 | 0.9 | 386.44 |
| 15:44:54 | 1693 | 0.9 | 386.45 |
| 15:44:55 | 1693 | 0.9 | 386.47 |
| 15:44:56 | 1693 | 0.9 | 386.49 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:44:57 | 1693 | 1.0 | 386.50 |
| 15:44:58 | 1693 | 0.9 | 386.52 |
| 15:44:59 | 1694 | 0.9 | 386.53 |
| 15:45:00 | 1693 | 1.0 | 386.55 |
| 15:45:01 | 1694 | 1.0 | 386.57 |
| 15:45:02 | 1694 | 0.9 | 386.58 |
| 15:45:03 | 1693 | 0.9 | 386.60 |
| 15:45:04 | 1694 | 0.9 | 386.61 |
| 15:45:05 | 1693 | 0.9 | 386.63 |
| 15:45:06 | 1693 | 0.9 | 386.64 |
| 15:45:07 | 1693 | 0.9 | 386.66 |
| 15:45:08 | 1693 | 0.9 | 386.68 |
| 15:45:09 | 1693 | 1.0 | 386.69 |
| 15:45:10 | 1694 | 0.9 | 386.71 |
| 15:45:11 | 1694 | 1.0 | 386.72 |
| 15:45:12 | 1694 | 0.9 | 386.74 |
| 15:45:13 | 1694 | 0.9 | 386.76 |
| 15:45:14 | 1694 | 0.9 | 386.77 |
| 15:45:15 | 1694 | 0.9 | 386.79 |
| 15:45:16 | 1694 | 0.9 | 386.80 |
| 15:45:17 | 1694 | 0.9 | 386.82 |
| 15:45:18 | 1694 | 0.9 | 386.83 |
| 15:45:19 | 1694 | 0.9 | 386.85 |
| 15:45:20 | 1694 | 0.9 | 386.87 |
| 15:45:21 | 1694 | 0.9 | 386.88 |
| 15:45:22 | 1694 | 1.0 | 386.90 |
| 15:45:23 | 1694 | 0.9 | 386.91 |
| 15:45:24 | 1694 | 0.9 | 386.93 |
| 15:45:25 | 1694 | 0.9 | 386.95 |
| 15:45:26 | 1694 | 0.9 | 386.96 |
| 15:45:27 | 1694 | 0.9 | 386.98 |
| 15:45:28 | 1694 | 0.9 | 386.99 |
| 15:45:29 | 1694 | 0.9 | 387.01 |
| 15:45:30 | 1694 | 0.9 | 387.02 |
| 15:45:31 | 1694 | 1.0 | 387.04 |
| 15:45:32 | 1694 | 0.9 | 387.06 |
| 15:45:33 | 1694 | 0.9 | 387.07 |
| 15:45:34 | 1694 | 0.9 | 387.09 |
| 15:45:35 | 1695 | 0.9 | 387.10 |
| 15:45:36 | 1695 | 0.9 | 387.12 |
| 15:45:37 | 1694 | 0.9 | 387.14 |
| 15:45:38 | 1694 | 0.9 | 387.15 |
| 15:45:39 | 1694 | 0.9 | 387.17 |
| 15:45:40 | 1694 | 0.9 | 387.18 |
| 15:45:41 | 1694 | 0.9 | 387.20 |
| 15:45:42 | 1694 | 0.9 | 387.21 |
| 15:45:43 | 1694 | 1.0 | 387.23 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:45:44 | 1694 | 0.9 | 387.25 |
| 15:45:45 | 1694 | 0.9 | 387.26 |
| 15:45:46 | 1694 | 0.9 | 387.28 |
| 15:45:47 | 1694 | 0.9 | 387.29 |
| 15:45:48 | 1694 | 0.9 | 387.31 |
| 15:45:49 | 1694 | 0.9 | 387.33 |
| 15:45:50 | 1694 | 0.9 | 387.34 |
| 15:45:51 | 1694 | 0.9 | 387.36 |
| 15:45:52 | 1694 | 0.9 | 387.37 |
| 15:45:53 | 1694 | 0.9 | 387.39 |
| 15:45:54 | 1694 | 0.9 | 387.40 |
| 15:45:55 | 1694 | 0.9 | 387.42 |
| 15:45:56 | 1694 | 0.9 | 387.44 |
| 15:45:57 | 1695 | 0.9 | 387.45 |
| 15:45:58 | 1695 | 0.9 | 387.47 |
| 15:45:59 | 1695 | 0.9 | 387.48 |
| 15:46:00 | 1695 | 0.9 | 387.50 |
| 15:46:01 | 1695 | 0.9 | 387.51 |
| 15:46:02 | 1695 | 0.9 | 387.53 |
| 15:46:03 | 1695 | 0.9 | 387.55 |
| 15:46:04 | 1695 | 1.0 | 387.56 |
| 15:46:05 | 1694 | 0.9 | 387.58 |
| 15:46:06 | 1695 | 0.9 | 387.59 |
| 15:46:07 | 1695 | 0.9 | 387.61 |
| 15:46:08 | 1695 | 0.9 | 387.63 |
| 15:46:09 | 1695 | 0.9 | 387.64 |
| 15:46:10 | 1695 | 0.9 | 387.66 |
| 15:46:11 | 1695 | 0.9 | 387.67 |
| 15:46:12 | 1695 | 0.9 | 387.69 |
| 15:46:13 | 1695 | 0.9 | 387.70 |
| 15:46:14 | 1695 | 0.9 | 387.72 |
| 15:46:15 | 1695 | 0.9 | 387.74 |
| 15:46:16 | 1695 | 0.9 | 387.75 |
| 15:46:17 | 1695 | 1.0 | 387.77 |
| 15:46:18 | 1695 | 0.9 | 387.78 |
| 15:46:19 | 1695 | 0.9 | 387.80 |
| 15:46:20 | 1695 | 0.9 | 387.82 |
| 15:46:21 | 1695 | 0.9 | 387.83 |
| 15:46:22 | 1695 | 0.9 | 387.85 |
| 15:46:23 | 1696 | 0.9 | 387.86 |
| 15:46:24 | 1696 | 0.9 | 387.88 |
| 15:46:25 | 1696 | 0.9 | 387.89 |
| 15:46:26 | 1696 | 0.9 | 387.91 |
| 15:46:27 | 1695 | 0.9 | 387.93 |
| 15:46:28 | 1696 | 0.9 | 387.94 |
| 15:46:29 | 1696 | 0.9 | 387.96 |
| 15:46:30 | 1695 | 0.9 | 387.97 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:46:31 | 1696 | 0.9 | 387.99 |
| 15:46:32 | 1696 | 0.9 | 388.01 |
| 15:46:33 | 1696 | 0.9 | 388.02 |
| 15:46:34 | 1696 | 0.9 | 388.04 |
| 15:46:35 | 1696 | 0.9 | 388.05 |
| 15:46:36 | 1696 | 0.9 | 388.07 |
| 15:46:37 | 1696 | 0.9 | 388.08 |
| 15:46:38 | 1696 | 1.0 | 388.10 |
| 15:46:39 | 1696 | 0.9 | 388.12 |
| 15:46:40 | 1696 | 0.9 | 388.13 |
| 15:46:41 | 1695 | 0.9 | 388.15 |
| 15:46:42 | 1696 | 0.9 | 388.16 |
| 15:46:43 | 1696 | 0.9 | 388.18 |
| 15:46:44 | 1696 | 0.9 | 388.20 |
| 15:46:45 | 1696 | 0.9 | 388.21 |
| 15:46:46 | 1696 | 0.9 | 388.23 |
| 15:46:47 | 1696 | 0.9 | 388.24 |
| 15:46:48 | 1696 | 0.9 | 388.26 |
| 15:46:49 | 1696 | 0.9 | 388.27 |
| 15:46:50 | 1696 | 0.9 | 388.29 |
| 15:46:51 | 1696 | 0.9 | 388.31 |
| 15:46:52 | 1696 | 0.9 | 388.32 |
| 15:46:53 | 1696 | 0.9 | 388.34 |
| 15:46:54 | 1696 | 0.9 | 388.35 |
| 15:46:55 | 1696 | 0.9 | 388.37 |
| 15:46:56 | 1696 | 0.9 | 388.38 |
| 15:46:57 | 1697 | 0.9 | 388.40 |
| 15:46:58 | 1697 | 0.9 | 388.42 |
| 15:46:59 | 1697 | 0.9 | 388.43 |
| 15:47:00 | 1697 | 0.9 | 388.45 |
| 15:47:01 | 1697 | 0.9 | 388.46 |
| 15:47:02 | 1697 | 0.9 | 388.48 |
| 15:47:03 | 1697 | 0.9 | 388.50 |
| 15:47:04 | 1696 | 0.9 | 388.51 |
| 15:47:05 | 1697 | 0.9 | 388.53 |
| 15:47:06 | 1697 | 0.9 | 388.54 |
| 15:47:07 | 1697 | 0.9 | 388.56 |
| 15:47:08 | 1697 | 0.9 | 388.57 |
| 15:47:09 | 1697 | 0.9 | 388.59 |
| 15:47:10 | 1697 | 0.9 | 388.61 |
| 15:47:11 | 1697 | 0.9 | 388.62 |
| 15:47:12 | 1697 | 0.9 | 388.64 |
| 15:47:13 | 1697 | 0.9 | 388.65 |
| 15:47:14 | 1697 | 0.9 | 388.67 |
| 15:47:15 | 1697 | 0.9 | 388.69 |
| 15:47:16 | 1697 | 0.9 | 388.70 |
| 15:47:17 | 1697 | 0.9 | 388.72 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:47:18 | 1697 | 0.9 | 388.73 |
| 15:47:19 | 1697 | 0.9 | 388.75 |
| 15:47:20 | 1697 | 0.9 | 388.76 |
| 15:47:21 | 1697 | 0.9 | 388.78 |
| 15:47:22 | 1697 | 0.9 | 388.80 |
| 15:47:23 | 1697 | 0.9 | 388.81 |
| 15:47:24 | 1697 | 0.9 | 388.83 |
| 15:47:25 | 1697 | 0.9 | 388.84 |
| 15:47:26 | 1697 | 0.9 | 388.86 |
| 15:47:27 | 1697 | 0.9 | 388.88 |
| 15:47:28 | 1697 | 0.9 | 388.89 |
| 15:47:29 | 1697 | 0.9 | 388.91 |
| 15:47:30 | 1697 | 0.9 | 388.92 |
| 15:47:31 | 1697 | 0.9 | 388.94 |
| 15:47:32 | 1698 | 0.9 | 388.95 |
| 15:47:33 | 1697 | 0.9 | 388.97 |
| 15:47:34 | 1698 | 0.9 | 388.99 |
| 15:47:35 | 1698 | 1.0 | 389.00 |
| 15:47:36 | 1698 | 0.9 | 389.02 |
| 15:47:37 | 1698 | 0.9 | 389.03 |
| 15:47:38 | 1697 | 0.9 | 389.05 |
| 15:47:39 | 1697 | 0.9 | 389.07 |
| 15:47:40 | 1697 | 0.9 | 389.08 |
| 15:47:41 | 1697 | 0.9 | 389.10 |
| 15:47:42 | 1697 | 0.9 | 389.11 |
| 15:47:43 | 1698 | 0.9 | 389.13 |
| 15:47:44 | 1698 | 0.9 | 389.14 |
| 15:47:45 | 1698 | 0.9 | 389.16 |
| 15:47:46 | 1698 | 0.9 | 389.18 |
| 15:47:47 | 1698 | 0.9 | 389.19 |
| 15:47:48 | 1698 | 0.9 | 389.21 |
| 15:47:49 | 1697 | 0.9 | 389.22 |
| 15:47:50 | 1698 | 0.9 | 389.24 |
| 15:47:51 | 1698 | 0.9 | 389.25 |
| 15:47:52 | 1698 | 0.9 | 389.27 |
| 15:47:53 | 1698 | 0.9 | 389.29 |
| 15:47:54 | 1698 | 0.9 | 389.30 |
| 15:47:55 | 1698 | 0.9 | 389.32 |
| 15:47:56 | 1698 | 1.0 | 389.33 |
| 15:47:57 | 1698 | 1.0 | 389.35 |
| 15:47:58 | 1698 | 0.9 | 389.37 |
| 15:47:59 | 1698 | 0.9 | 389.38 |
| 15:48:00 | 1698 | 0.9 | 389.40 |
| 15:48:01 | 1698 | 0.9 | 389.41 |
| 15:48:02 | 1698 | 0.9 | 389.43 |
| 15:48:03 | 1698 | 0.9 | 389.44 |
| 15:48:04 | 1698 | 0.9 | 389.46 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:48:05 | 1698 | 0.9 | 389.48 |
| 15:48:06 | 1698 | 0.9 | 389.49 |
| 15:48:07 | 1698 | 0.9 | 389.51 |
| 15:48:08 | 1698 | 0.9 | 389.52 |
| 15:48:09 | 1699 | 1.0 | 389.54 |
| 15:48:10 | 1699 | 0.9 | 389.56 |
| 15:48:11 | 1699 | 0.9 | 389.57 |
| 15:48:12 | 1699 | 0.9 | 389.59 |
| 15:48:13 | 1699 | 0.9 | 389.60 |
| 15:48:14 | 1698 | 0.9 | 389.62 |
| 15:48:15 | 1698 | 0.9 | 389.63 |
| 15:48:16 | 1698 | 0.9 | 389.65 |
| 15:48:17 | 1698 | 0.9 | 389.67 |
| 15:48:18 | 1699 | 0.9 | 389.68 |
| 15:48:19 | 1699 | 0.9 | 389.70 |
| 15:48:20 | 1699 | 0.9 | 389.71 |
| 15:48:21 | 1699 | 0.9 | 389.73 |
| 15:48:22 | 1699 | 0.9 | 389.75 |
| 15:48:23 | 1699 | 0.9 | 389.76 |
| 15:48:24 | 1699 | 0.9 | 389.78 |
| 15:48:25 | 1699 | 0.9 | 389.79 |
| 15:48:26 | 1699 | 0.9 | 389.81 |
| 15:48:27 | 1699 | 0.9 | 389.82 |
| 15:48:28 | 1699 | 0.9 | 389.84 |
| 15:48:29 | 1699 | 0.9 | 389.86 |
| 15:48:30 | 1699 | 1.0 | 389.87 |
| 15:48:31 | 1699 | 0.9 | 389.89 |
| 15:48:32 | 1699 | 0.9 | 389.90 |
| 15:48:33 | 1699 | 0.9 | 389.92 |
| 15:48:34 | 1699 | 0.9 | 389.94 |
| 15:48:35 | 1699 | 0.9 | 389.95 |
| 15:48:36 | 1699 | 0.9 | 389.97 |
| 15:48:37 | 1699 | 0.9 | 389.98 |
| 15:48:38 | 1699 | 0.9 | 390.00 |
| 15:48:39 | 1699 | 0.9 | 390.01 |
| 15:48:40 | 1699 | 0.9 | 390.03 |
| 15:48:41 | 1699 | 0.9 | 390.05 |
| 15:48:42 | 1699 | 0.9 | 390.06 |
| 15:48:43 | 1699 | 0.9 | 390.08 |
| 15:48:44 | 1699 | 0.9 | 390.09 |
| 15:48:45 | 1699 | 0.9 | 390.11 |
| 15:48:46 | 1700 | 0.9 | 390.13 |
| 15:48:47 | 1700 | 0.9 | 390.14 |
| 15:48:48 | 1700 | 0.9 | 390.16 |
| 15:48:49 | 1700 | 0.9 | 390.17 |
| 15:48:50 | 1699 | 0.9 | 390.19 |
| 15:48:51 | 1699 | 0.9 | 390.20 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:48:52 | 1699 | 0.9 | 390.22 |
| 15:48:53 | 1699 | 0.9 | 390.24 |
| 15:48:54 | 1699 | 0.9 | 390.25 |
| 15:48:55 | 1699 | 0.9 | 390.27 |
| 15:48:56 | 1700 | 0.9 | 390.28 |
| 15:48:57 | 1700 | 0.9 | 390.30 |
| 15:48:58 | 1700 | 0.9 | 390.31 |
| 15:48:59 | 1700 | 0.9 | 390.33 |
| 15:49:00 | 1700 | 0.9 | 390.35 |
| 15:49:01 | 1700 | 0.9 | 390.36 |
| 15:49:02 | 1700 | 0.9 | 390.38 |
| 15:49:03 | 1700 | 0.9 | 390.39 |
| 15:49:04 | 1700 | 1.0 | 390.41 |
| 15:49:05 | 1700 | 0.9 | 390.43 |
| 15:49:06 | 1700 | 0.9 | 390.44 |
| 15:49:07 | 1700 | 0.9 | 390.46 |
| 15:49:08 | 1700 | 0.9 | 390.47 |
| 15:49:09 | 1700 | 0.9 | 390.49 |
| 15:49:10 | 1700 | 0.9 | 390.50 |
| 15:49:11 | 1700 | 0.9 | 390.52 |
| 15:49:12 | 1700 | 0.9 | 390.54 |
| 15:49:13 | 1700 | 0.9 | 390.55 |
| 15:49:14 | 1700 | 1.0 | 390.57 |
| 15:49:15 | 1700 | 0.9 | 390.58 |
| 15:49:16 | 1700 | 1.0 | 390.60 |
| 15:49:17 | 1700 | 0.9 | 390.62 |
| 15:49:18 | 1700 | 0.9 | 390.63 |
| 15:49:19 | 1700 | 0.9 | 390.65 |
| 15:49:20 | 1700 | 0.9 | 390.66 |
| 15:49:21 | 1700 | 0.9 | 390.68 |
| 15:49:22 | 1700 | 0.9 | 390.69 |
| 15:49:23 | 1700 | 0.9 | 390.71 |
| 15:49:24 | 1700 | 0.9 | 390.73 |
| 15:49:25 | 1700 | 1.0 | 390.74 |
| 15:49:26 | 1700 | 0.9 | 390.76 |
| 15:49:27 | 1700 | 0.9 | 390.77 |
| 15:49:28 | 1700 | 0.9 | 390.79 |
| 15:49:29 | 1700 | 0.9 | 390.81 |
| 15:49:30 | 1700 | 0.9 | 390.82 |
| 15:49:31 | 1700 | 0.9 | 390.84 |
| 15:49:32 | 1700 | 0.9 | 390.85 |
| 15:49:33 | 1700 | 0.9 | 390.87 |
| 15:49:34 | 1700 | 0.9 | 390.88 |
| 15:49:35 | 1700 | 1.0 | 390.90 |
| 15:49:36 | 1700 | 0.9 | 390.92 |
| 15:49:37 | 1700 | 0.9 | 390.93 |
| 15:49:38 | 1700 | 0.9 | 390.95 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:49:39 | 1700 | 0.9 | 390.96 |
| 15:49:40 | 1700 | 0.9 | 390.98 |
| 15:49:41 | 1700 | 0.9 | 391.00 |
| 15:49:42 | 1700 | 0.9 | 391.01 |
| 15:49:43 | 1700 | 0.9 | 391.03 |
| 15:49:44 | 1700 | 0.9 | 391.04 |
| 15:49:45 | 1700 | 0.9 | 391.06 |
| 15:49:46 | 1700 | 1.0 | 391.07 |
| 15:49:47 | 1700 | 0.9 | 391.09 |
| 15:49:48 | 1700 | 1.0 | 391.11 |
| 15:49:49 | 1700 | 0.9 | 391.12 |
| 15:49:50 | 1700 | 0.9 | 391.14 |
| 15:49:51 | 1700 | 0.9 | 391.15 |
| 15:49:52 | 1700 | 0.9 | 391.17 |
| 15:49:53 | 1700 | 0.9 | 391.19 |
| 15:49:54 | 1700 | 0.9 | 391.20 |
| 15:49:55 | 1700 | 0.9 | 391.22 |
| 15:49:56 | 1700 | 0.9 | 391.23 |
| 15:49:57 | 1700 | 0.9 | 391.25 |
| 15:49:58 | 1700 | 0.9 | 391.26 |
| 15:49:59 | 1700 | 0.9 | 391.28 |
| 15:50:00 | 1700 | 0.9 | 391.30 |
| 15:50:01 | 1700 | 0.9 | 391.31 |
| 15:50:02 | 1700 | 0.9 | 391.33 |
| 15:50:03 | 1700 | 0.9 | 391.34 |
| 15:50:04 | 1700 | 0.9 | 391.36 |
| 15:50:05 | 1700 | 0.9 | 391.37 |
| 15:50:06 | 1700 | 0.9 | 391.39 |
| 15:50:07 | 1700 | 0.9 | 391.41 |
| 15:50:08 | 1700 | 0.9 | 391.42 |
| 15:50:09 | 1700 | 1.0 | 391.44 |
| 15:50:10 | 1700 | 0.9 | 391.45 |
| 15:50:11 | 1700 | 0.9 | 391.47 |
| 15:50:12 | 1700 | 0.9 | 391.49 |
| 15:50:13 | 1700 | 0.9 | 391.50 |
| 15:50:14 | 1700 | 0.9 | 391.52 |
| 15:50:15 | 1700 | 0.9 | 391.53 |
| 15:50:16 | 1700 | 0.9 | 391.55 |
| 15:50:17 | 1700 | 0.9 | 391.56 |
| 15:50:18 | 1700 | 1.0 | 391.58 |
| 15:50:19 | 1700 | 0.9 | 391.60 |
| 15:50:20 | 1700 | 0.9 | 391.61 |
| 15:50:21 | 1700 | 0.9 | 391.63 |
| 15:50:22 | 1700 | 0.9 | 391.64 |
| 15:50:23 | 1700 | 0.9 | 391.66 |
| 15:50:24 | 1700 | 0.9 | 391.68 |
| 15:50:25 | 1700 | 0.9 | 391.69 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:50:26 | 1700 | 0.9 | 391.71 |
| 15:50:27 | 1700 | 0.9 | 391.72 |
| 15:50:28 | 1700 | 0.9 | 391.74 |
| 15:50:29 | 1700 | 0.9 | 391.75 |
| 15:50:30 | 1700 | 1.0 | 391.77 |
| 15:50:31 | 1700 | 1.0 | 391.79 |
| 15:50:32 | 1701 | 1.0 | 391.80 |
| 15:50:33 | 1700 | 0.9 | 391.82 |
| 15:50:34 | 1700 | 1.0 | 391.83 |
| 15:50:35 | 1700 | 0.9 | 391.85 |
| 15:50:36 | 1700 | 0.9 | 391.87 |
| 15:50:37 | 1700 | 0.9 | 391.88 |
| 15:50:38 | 1700 | 0.9 | 391.90 |
| 15:50:39 | 1700 | 1.0 | 391.91 |
| 15:50:40 | 1700 | 0.9 | 391.93 |
| 15:50:41 | 1700 | 0.9 | 391.94 |
| 15:50:42 | 1700 | 1.0 | 391.96 |
| 15:50:43 | 1700 | 1.0 | 391.98 |
| 15:50:44 | 1700 | 1.0 | 391.99 |
| 15:50:45 | 1700 | 0.9 | 392.01 |
| 15:50:46 | 1700 | 0.9 | 392.02 |
| 15:50:47 | 1700 | 0.9 | 392.04 |
| 15:50:48 | 1700 | 1.0 | 392.06 |
| 15:50:49 | 1700 | 0.9 | 392.07 |
| 15:50:50 | 1700 | 0.9 | 392.09 |
| 15:50:51 | 1699 | 1.0 | 392.10 |
| 15:50:52 | 1699 | 0.9 | 392.12 |
| 15:50:53 | 1699 | 1.0 | 392.13 |
| 15:50:54 | 1699 | 0.9 | 392.15 |
| 15:50:55 | 1699 | 1.0 | 392.17 |
| 15:50:56 | 1699 | 1.0 | 392.18 |
| 15:50:57 | 1699 | 0.9 | 392.20 |
| 15:50:58 | 1700 | 0.9 | 392.21 |
| 15:50:59 | 1699 | 0.9 | 392.23 |
| 15:51:00 | 1699 | 0.9 | 392.25 |
| 15:51:01 | 1699 | 0.9 | 392.26 |
| 15:51:02 | 1699 | 0.9 | 392.28 |
| 15:51:03 | 1699 | 0.9 | 392.29 |
| 15:51:04 | 1699 | 1.0 | 392.31 |
| 15:51:05 | 1699 | 0.9 | 392.32 |
| 15:51:06 | 1699 | 0.9 | 392.34 |
| 15:51:07 | 1699 | 0.9 | 392.36 |
| 15:51:08 | 1699 | 0.9 | 392.37 |
| 15:51:09 | 1699 | 0.9 | 392.39 |
| 15:51:10 | 1699 | 0.9 | 392.40 |
| 15:51:11 | 1699 | 0.9 | 392.42 |
| 15:51:12 | 1699 | 0.9 | 392.44 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:51:13 | 1699 | 0.9 | 392.45 |
| 15:51:14 | 1699 | 0.9 | 392.47 |
| 15:51:15 | 1699 | 1.0 | 392.48 |
| 15:51:16 | 1699 | 1.0 | 392.50 |
| 15:51:17 | 1699 | 1.0 | 392.51 |
| 15:51:18 | 1699 | 0.9 | 392.53 |
| 15:51:19 | 1699 | 0.9 | 392.55 |
| 15:51:20 | 1699 | 0.9 | 392.56 |
| 15:51:21 | 1699 | 0.9 | 392.58 |
| 15:51:22 | 1699 | 0.9 | 392.59 |
| 15:51:23 | 1699 | 0.9 | 392.61 |
| 15:51:24 | 1699 | 0.9 | 392.63 |
| 15:51:25 | 1699 | 1.0 | 392.64 |
| 15:51:26 | 1699 | 0.9 | 392.66 |
| 15:51:27 | 1699 | 0.9 | 392.67 |
| 15:51:28 | 1699 | 0.9 | 392.69 |
| 15:51:29 | 1699 | 0.9 | 392.70 |
| 15:51:30 | 1699 | 0.9 | 392.72 |
| 15:51:31 | 1699 | 0.9 | 392.74 |
| 15:51:32 | 1699 | 0.9 | 392.75 |
| 15:51:33 | 1699 | 0.9 | 392.77 |
| 15:51:34 | 1699 | 0.9 | 392.78 |
| 15:51:35 | 1699 | 0.9 | 392.80 |
| 15:51:36 | 1699 | 0.9 | 392.82 |
| 15:51:37 | 1699 | 0.9 | 392.83 |
| 15:51:38 | 1699 | 0.9 | 392.85 |
| 15:51:39 | 1699 | 0.9 | 392.86 |
| 15:51:40 | 1699 | 1.0 | 392.88 |
| 15:51:41 | 1699 | 0.9 | 392.89 |
| 15:51:42 | 1699 | 0.9 | 392.91 |
| 15:51:43 | 1699 | 0.9 | 392.93 |
| 15:51:44 | 1699 | 0.9 | 392.94 |
| 15:51:45 | 1699 | 0.9 | 392.96 |
| 15:51:46 | 1699 | 0.9 | 392.97 |
| 15:51:47 | 1699 | 0.9 | 392.99 |
| 15:51:48 | 1699 | 0.9 | 393.00 |
| 15:51:49 | 1699 | 1.0 | 393.02 |
| 15:51:50 | 1699 | 1.0 | 393.04 |
| 15:51:51 | 1699 | 1.0 | 393.05 |
| 15:51:52 | 1699 | 0.9 | 393.07 |
| 15:51:53 | 1699 | 0.9 | 393.08 |
| 15:51:54 | 1699 | 0.9 | 393.10 |
| 15:51:55 | 1699 | 0.9 | 393.12 |
| 15:51:56 | 1699 | 0.9 | 393.13 |
| 15:51:57 | 1699 | 0.9 | 393.15 |
| 15:51:58 | 1699 | 1.0 | 393.16 |
| 15:51:59 | 1699 | 0.9 | 393.18 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:52:00 | 1699 | 0.9 | 393.19 |
| 15:52:01 | 1699 | 1.0 | 393.21 |
| 15:52:02 | 1699 | 1.0 | 393.23 |
| 15:52:03 | 1699 | 0.9 | 393.24 |
| 15:52:04 | 1699 | 0.9 | 393.26 |
| 15:52:05 | 1699 | 0.9 | 393.27 |
| 15:52:06 | 1700 | 0.9 | 393.29 |
| 15:52:07 | 1700 | 0.9 | 393.31 |
| 15:52:08 | 1700 | 0.9 | 393.32 |
| 15:52:09 | 1699 | 0.9 | 393.34 |
| 15:52:10 | 1700 | 0.9 | 393.35 |
| 15:52:11 | 1699 | 1.0 | 393.37 |
| 15:52:12 | 1699 | 1.0 | 393.38 |
| 15:52:13 | 1699 | 0.9 | 393.40 |
| 15:52:14 | 1699 | 1.0 | 393.42 |
| 15:52:15 | 1699 | 0.9 | 393.43 |
| 15:52:16 | 1699 | 0.9 | 393.45 |
| 15:52:17 | 1699 | 0.9 | 393.46 |
| 15:52:18 | 1700 | 0.9 | 393.48 |
| 15:52:19 | 1700 | 0.9 | 393.50 |
| 15:52:20 | 1700 | 0.9 | 393.51 |
| 15:52:21 | 1700 | 0.9 | 393.53 |
| 15:52:22 | 1700 | 1.0 | 393.54 |
| 15:52:23 | 1700 | 1.0 | 393.56 |
| 15:52:24 | 1700 | 0.9 | 393.57 |
| 15:52:25 | 1699 | 0.9 | 393.59 |
| 15:52:26 | 1699 | 0.9 | 393.61 |
| 15:52:27 | 1699 | 0.9 | 393.62 |
| 15:52:28 | 1699 | 0.9 | 393.64 |
| 15:52:29 | 1699 | 0.9 | 393.65 |
| 15:52:30 | 1700 | 1.0 | 393.67 |
| 15:52:31 | 1700 | 0.9 | 393.69 |
| 15:52:32 | 1700 | 1.0 | 393.70 |
| 15:52:33 | 1700 | 0.9 | 393.72 |
| 15:52:34 | 1700 | 0.9 | 393.73 |
| 15:52:35 | 1700 | 1.0 | 393.75 |
| 15:52:36 | 1700 | 0.9 | 393.76 |
| 15:52:37 | 1700 | 0.9 | 393.78 |
| 15:52:38 | 1700 | 0.9 | 393.80 |
| 15:52:39 | 1700 | 0.9 | 393.81 |
| 15:52:40 | 1700 | 0.9 | 393.83 |
| 15:52:41 | 1700 | 0.9 | 393.84 |
| 15:52:42 | 1700 | 0.9 | 393.86 |
| 15:52:43 | 1700 | 1.0 | 393.88 |
| 15:52:44 | 1700 | 1.0 | 393.89 |
| 15:52:45 | 1700 | 0.9 | 393.91 |
| 15:52:46 | 1700 | 0.9 | 393.92 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:52:47 | 1700 | 0.9 | 393.94 |
| 15:52:48 | 1700 | 0.9 | 393.95 |
| 15:52:49 | 1700 | 0.9 | 393.97 |
| 15:52:50 | 1700 | 0.9 | 393.99 |
| 15:52:51 | 1700 | 0.9 | 394.00 |
| 15:52:52 | 1700 | 0.9 | 394.02 |
| 15:52:53 | 1700 | 0.9 | 394.03 |
| 15:52:54 | 1700 | 0.9 | 394.05 |
| 15:52:55 | 1700 | 0.9 | 394.07 |
| 15:52:56 | 1700 | 1.0 | 394.08 |
| 15:52:57 | 1700 | 0.9 | 394.10 |
| 15:52:58 | 1700 | 0.9 | 394.11 |
| 15:52:59 | 1700 | 0.9 | 394.13 |
| 15:53:00 | 1700 | 0.9 | 394.14 |
| 15:53:01 | 1700 | 0.9 | 394.16 |
| 15:53:02 | 1700 | 0.9 | 394.18 |
| 15:53:03 | 1700 | 0.9 | 394.19 |
| 15:53:04 | 1700 | 0.9 | 394.21 |
| 15:53:05 | 1700 | 0.9 | 394.22 |
| 15:53:06 | 1701 | 0.9 | 394.24 |
| 15:53:07 | 1701 | 0.9 | 394.26 |
| 15:53:08 | 1701 | 0.9 | 394.27 |
| 15:53:09 | 1701 | 1.0 | 394.29 |
| 15:53:10 | 1701 | 0.9 | 394.30 |
| 15:53:11 | 1701 | 0.9 | 394.32 |
| 15:53:12 | 1701 | 0.9 | 394.33 |
| 15:53:13 | 1701 | 0.9 | 394.35 |
| 15:53:14 | 1701 | 0.9 | 394.37 |
| 15:53:15 | 1701 | 0.9 | 394.38 |
| 15:53:16 | 1701 | 0.9 | 394.40 |
| 15:53:17 | 1701 | 1.0 | 394.41 |
| 15:53:18 | 1701 | 1.0 | 394.43 |
| 15:53:19 | 1701 | 0.9 | 394.44 |
| 15:53:20 | 1701 | 0.9 | 394.46 |
| 15:53:21 | 1701 | 0.9 | 394.48 |
| 15:53:22 | 1701 | 0.9 | 394.49 |
| 15:53:23 | 1701 | 0.9 | 394.51 |
| 15:53:24 | 1701 | 0.9 | 394.52 |
| 15:53:25 | 1701 | 0.9 | 394.54 |
| 15:53:26 | 1701 | 0.9 | 394.56 |
| 15:53:27 | 1701 | 0.9 | 394.57 |
| 15:53:28 | 1701 | 0.9 | 394.59 |
| 15:53:29 | 1701 | 0.9 | 394.60 |
| 15:53:30 | 1702 | 1.0 | 394.62 |
| 15:53:31 | 1702 | 0.9 | 394.63 |
| 15:53:32 | 1702 | 0.9 | 394.65 |
| 15:53:33 | 1702 | 0.9 | 394.67 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:53:34 | 1702 | 0.9 | 394.68 |
| 15:53:35 | 1702 | 0.9 | 394.70 |
| 15:53:36 | 1702 | 0.9 | 394.71 |
| 15:53:37 | 1702 | 0.9 | 394.73 |
| 15:53:38 | 1702 | 0.9 | 394.75 |
| 15:53:39 | 1702 | 1.0 | 394.76 |
| 15:53:40 | 1702 | 1.0 | 394.78 |
| 15:53:41 | 1702 | 0.9 | 394.79 |
| 15:53:42 | 1702 | 1.0 | 394.81 |
| 15:53:43 | 1702 | 0.9 | 394.82 |
| 15:53:44 | 1702 | 0.9 | 394.84 |
| 15:53:45 | 1702 | 0.9 | 394.86 |
| 15:53:46 | 1702 | 0.9 | 394.87 |
| 15:53:47 | 1702 | 0.9 | 394.89 |
| 15:53:48 | 1702 | 0.9 | 394.90 |
| 15:53:49 | 1702 | 0.9 | 394.92 |
| 15:53:50 | 1702 | 0.9 | 394.94 |
| 15:53:51 | 1702 | 1.0 | 394.95 |
| 15:53:52 | 1702 | 0.9 | 394.97 |
| 15:53:53 | 1702 | 0.9 | 394.98 |
| 15:53:54 | 1702 | 0.9 | 395.00 |
| 15:53:55 | 1703 | 0.9 | 395.01 |
| 15:53:56 | 1703 | 0.9 | 395.03 |
| 15:53:57 | 1702 | 0.9 | 395.05 |
| 15:53:58 | 1702 | 0.9 | 395.06 |
| 15:53:59 | 1702 | 1.0 | 395.08 |
| 15:54:00 | 1702 | 0.9 | 395.09 |
| 15:54:01 | 1702 | 0.9 | 395.11 |
| 15:54:02 | 1702 | 1.0 | 395.13 |
| 15:54:03 | 1702 | 0.9 | 395.14 |
| 15:54:04 | 1703 | 0.9 | 395.16 |
| 15:54:05 | 1703 | 0.9 | 395.17 |
| 15:54:06 | 1703 | 0.9 | 395.19 |
| 15:54:07 | 1703 | 0.9 | 395.20 |
| 15:54:08 | 1703 | 0.9 | 395.22 |
| 15:54:09 | 1703 | 0.9 | 395.24 |
| 15:54:10 | 1702 | 0.9 | 395.25 |
| 15:54:11 | 1702 | 0.9 | 395.27 |
| 15:54:12 | 1703 | 1.0 | 395.28 |
| 15:54:13 | 1702 | 0.9 | 395.30 |
| 15:54:14 | 1703 | 1.0 | 395.32 |
| 15:54:15 | 1703 | 0.9 | 395.33 |
| 15:54:16 | 1703 | 0.9 | 395.35 |
| 15:54:17 | 1703 | 0.9 | 395.36 |
| 15:54:18 | 1703 | 0.9 | 395.38 |
| 15:54:19 | 1703 | 0.9 | 395.39 |
| 15:54:20 | 1703 | 0.9 | 395.41 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:54:21 | 1703 | 0.9 | 395.43 |
| 15:54:22 | 1703 | 0.9 | 395.44 |
| 15:54:23 | 1703 | 0.9 | 395.46 |
| 15:54:24 | 1703 | 0.9 | 395.47 |
| 15:54:25 | 1703 | 0.9 | 395.49 |
| 15:54:26 | 1703 | 0.9 | 395.51 |
| 15:54:27 | 1703 | 0.9 | 395.52 |
| 15:54:28 | 1703 | 0.9 | 395.54 |
| 15:54:29 | 1703 | 0.9 | 395.55 |
| 15:54:30 | 1703 | 0.9 | 395.57 |
| 15:54:31 | 1703 | 0.9 | 395.58 |
| 15:54:32 | 1703 | 0.9 | 395.60 |
| 15:54:33 | 1703 | 0.9 | 395.62 |
| 15:54:34 | 1703 | 0.9 | 395.63 |
| 15:54:35 | 1703 | 1.0 | 395.65 |
| 15:54:36 | 1703 | 0.9 | 395.66 |
| 15:54:37 | 1703 | 0.9 | 395.68 |
| 15:54:38 | 1703 | 0.9 | 395.69 |
| 15:54:39 | 1703 | 0.9 | 395.71 |
| 15:54:40 | 1703 | 0.9 | 395.73 |
| 15:54:41 | 1704 | 0.9 | 395.74 |
| 15:54:42 | 1704 | 0.9 | 395.76 |
| 15:54:43 | 1704 | 0.9 | 395.77 |
| 15:54:44 | 1704 | 0.9 | 395.79 |
| 15:54:45 | 1704 | 0.9 | 395.81 |
| 15:54:46 | 1704 | 0.9 | 395.82 |
| 15:54:47 | 1704 | 0.9 | 395.84 |
| 15:54:48 | 1704 | 1.0 | 395.85 |
| 15:54:49 | 1704 | 0.9 | 395.87 |
| 15:54:50 | 1704 | 0.9 | 395.88 |
| 15:54:51 | 1704 | 0.9 | 395.90 |
| 15:54:52 | 1704 | 0.9 | 395.92 |
| 15:54:53 | 1704 | 0.9 | 395.93 |
| 15:54:54 | 1704 | 0.9 | 395.95 |
| 15:54:55 | 1704 | 0.9 | 395.96 |
| 15:54:56 | 1704 | 0.9 | 395.98 |
| 15:54:57 | 1704 | 1.0 | 396.00 |
| 15:54:58 | 1704 | 1.0 | 396.01 |
| 15:54:59 | 1704 | 0.9 | 396.03 |
| 15:55:00 | 1704 | 0.9 | 396.04 |
| 15:55:01 | 1704 | 0.9 | 396.06 |
| 15:55:02 | 1704 | 0.9 | 396.07 |
| 15:55:03 | 1704 | 0.9 | 396.09 |
| 15:55:04 | 1704 | 0.9 | 396.11 |
| 15:55:05 | 1704 | 0.9 | 396.12 |
| 15:55:06 | 1704 | 0.9 | 396.14 |
| 15:55:07 | 1704 | 0.9 | 396.15 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:55:08 | 1704 | 0.9 | 396.17 |
| 15:55:09 | 1704 | 1.0 | 396.19 |
| 15:55:10 | 1704 | 0.9 | 396.20 |
| 15:55:11 | 1704 | 0.9 | 396.22 |
| 15:55:12 | 1704 | 0.9 | 396.23 |
| 15:55:13 | 1704 | 0.9 | 396.25 |
| 15:55:14 | 1704 | 0.9 | 396.26 |
| 15:55:15 | 1704 | 0.9 | 396.28 |
| 15:55:16 | 1704 | 0.9 | 396.30 |
| 15:55:17 | 1704 | 0.9 | 396.31 |
| 15:55:18 | 1705 | 0.9 | 396.33 |
| 15:55:19 | 1705 | 1.0 | 396.34 |
| 15:55:20 | 1704 | 0.9 | 396.36 |
| 15:55:21 | 1704 | 0.9 | 396.38 |
| 15:55:22 | 1704 | 1.0 | 396.39 |
| 15:55:23 | 1704 | 0.9 | 396.41 |
| 15:55:24 | 1704 | 0.9 | 396.42 |
| 15:55:25 | 1704 | 0.9 | 396.44 |
| 15:55:26 | 1705 | 0.9 | 396.45 |
| 15:55:27 | 1705 | 0.9 | 396.47 |
| 15:55:28 | 1705 | 0.9 | 396.49 |
| 15:55:29 | 1705 | 0.9 | 396.50 |
| 15:55:30 | 1705 | 0.9 | 396.52 |
| 15:55:31 | 1705 | 0.9 | 396.53 |
| 15:55:32 | 1705 | 0.9 | 396.55 |
| 15:55:33 | 1705 | 0.9 | 396.57 |
| 15:55:34 | 1705 | 0.9 | 396.58 |
| 15:55:35 | 1705 | 0.9 | 396.60 |
| 15:55:36 | 1705 | 0.9 | 396.61 |
| 15:55:37 | 1705 | 0.9 | 396.63 |
| 15:55:38 | 1705 | 0.9 | 396.64 |
| 15:55:39 | 1706 | 0.9 | 396.66 |
| 15:55:40 | 1706 | 0.9 | 396.68 |
| 15:55:41 | 1706 | 0.9 | 396.69 |
| 15:55:42 | 1706 | 0.9 | 396.71 |
| 15:55:43 | 1706 | 1.0 | 396.72 |
| 15:55:44 | 1705 | 1.0 | 396.74 |
| 15:55:45 | 1705 | 0.9 | 396.75 |
| 15:55:46 | 1705 | 0.9 | 396.77 |
| 15:55:47 | 1705 | 0.9 | 396.79 |
| 15:55:48 | 1705 | 0.9 | 396.80 |
| 15:55:49 | 1705 | 0.9 | 396.82 |
| 15:55:50 | 1705 | 0.9 | 396.83 |
| 15:55:51 | 1705 | 1.0 | 396.85 |
| 15:55:52 | 1705 | 0.9 | 396.87 |
| 15:55:53 | 1705 | 0.9 | 396.88 |
| 15:55:54 | 1705 | 0.9 | 396.90 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:55:55 | 1706 | 0.9 | 396.91 |
| 15:55:56 | 1705 | 0.9 | 396.93 |
| 15:55:57 | 1705 | 0.9 | 396.94 |
| 15:55:58 | 1705 | 0.9 | 396.96 |
| 15:55:59 | 1705 | 0.9 | 396.98 |
| 15:56:00 | 1705 | 0.9 | 396.99 |
| 15:56:01 | 1705 | 0.9 | 397.01 |
| 15:56:02 | 1705 | 0.9 | 397.02 |
| 15:56:03 | 1705 | 0.9 | 397.04 |
| 15:56:04 | 1706 | 1.0 | 397.06 |
| 15:56:05 | 1706 | 1.0 | 397.07 |
| 15:56:06 | 1706 | 0.9 | 397.09 |
| 15:56:07 | 1706 | 0.9 | 397.10 |
| 15:56:08 | 1706 | 0.9 | 397.12 |
| 15:56:09 | 1706 | 0.9 | 397.13 |
| 15:56:10 | 1705 | 0.9 | 397.15 |
| 15:56:11 | 1706 | 0.9 | 397.17 |
| 15:56:12 | 1706 | 0.9 | 397.18 |
| 15:56:13 | 1706 | 0.9 | 397.20 |
| 15:56:14 | 1706 | 0.9 | 397.21 |
| 15:56:15 | 1706 | 1.0 | 397.23 |
| 15:56:16 | 1706 | 0.9 | 397.25 |
| 15:56:17 | 1706 | 1.0 | 397.26 |
| 15:56:18 | 1706 | 0.9 | 397.28 |
| 15:56:19 | 1706 | 0.9 | 397.29 |
| 15:56:20 | 1706 | 0.9 | 397.31 |
| 15:56:21 | 1706 | 0.9 | 397.32 |
| 15:56:22 | 1706 | 0.9 | 397.34 |
| 15:56:23 | 1706 | 0.9 | 397.36 |
| 15:56:24 | 1706 | 0.9 | 397.37 |
| 15:56:25 | 1706 | 1.0 | 397.39 |
| 15:56:26 | 1706 | 0.9 | 397.40 |
| 15:56:27 | 1706 | 0.9 | 397.42 |
| 15:56:28 | 1706 | 0.9 | 397.44 |
| 15:56:29 | 1706 | 0.9 | 397.45 |
| 15:56:30 | 1706 | 0.9 | 397.47 |
| 15:56:31 | 1706 | 0.9 | 397.48 |
| 15:56:32 | 1706 | 0.9 | 397.50 |
| 15:56:33 | 1706 | 0.9 | 397.51 |
| 15:56:34 | 1706 | 0.9 | 397.53 |
| 15:56:35 | 1706 | 0.9 | 397.55 |
| 15:56:36 | 1706 | 0.9 | 397.56 |
| 15:56:37 | 1706 | 0.9 | 397.58 |
| 15:56:38 | 1706 | 0.9 | 397.59 |
| 15:56:39 | 1706 | 0.9 | 397.61 |
| 15:56:40 | 1706 | 1.0 | 397.63 |
| 15:56:41 | 1707 | 0.9 | 397.64 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:56:42 | 1707 | 0.9 | 397.66 |
| 15:56:43 | 1707 | 0.9 | 397.67 |
| 15:56:44 | 1707 | 0.9 | 397.69 |
| 15:56:45 | 1707 | 0.9 | 397.70 |
| 15:56:46 | 1707 | 0.9 | 397.72 |
| 15:56:47 | 1706 | 0.9 | 397.74 |
| 15:56:48 | 1706 | 0.9 | 397.75 |
| 15:56:49 | 1707 | 0.9 | 397.77 |
| 15:56:50 | 1707 | 0.9 | 397.78 |
| 15:56:51 | 1707 | 0.9 | 397.80 |
| 15:56:52 | 1707 | 0.9 | 397.81 |
| 15:56:53 | 1707 | 0.9 | 397.83 |
| 15:56:54 | 1707 | 0.9 | 397.85 |
| 15:56:55 | 1707 | 0.9 | 397.86 |
| 15:56:56 | 1707 | 0.9 | 397.88 |
| 15:56:57 | 1707 | 0.9 | 397.89 |
| 15:56:58 | 1707 | 0.9 | 397.91 |
| 15:56:59 | 1707 | 0.9 | 397.93 |
| 15:57:00 | 1707 | 0.9 | 397.94 |
| 15:57:01 | 1707 | 1.0 | 397.96 |
| 15:57:02 | 1707 | 0.9 | 397.97 |
| 15:57:03 | 1707 | 0.9 | 397.99 |
| 15:57:04 | 1707 | 0.9 | 398.00 |
| 15:57:05 | 1707 | 0.9 | 398.02 |
| 15:57:06 | 1707 | 0.9 | 398.04 |
| 15:57:07 | 1707 | 0.9 | 398.05 |
| 15:57:08 | 1707 | 0.9 | 398.07 |
| 15:57:09 | 1707 | 0.9 | 398.08 |
| 15:57:10 | 1707 | 0.9 | 398.10 |
| 15:57:11 | 1707 | 0.9 | 398.12 |
| 15:57:12 | 1708 | 0.9 | 398.13 |
| 15:57:13 | 1708 | 0.9 | 398.15 |
| 15:57:14 | 1708 | 0.9 | 398.16 |
| 15:57:15 | 1708 | 0.9 | 398.18 |
| 15:57:16 | 1708 | 0.9 | 398.19 |
| 15:57:17 | 1708 | 0.9 | 398.21 |
| 15:57:18 | 1708 | 0.9 | 398.23 |
| 15:57:19 | 1708 | 0.9 | 398.24 |
| 15:57:20 | 1708 | 0.9 | 398.26 |
| 15:57:21 | 1708 | 0.9 | 398.27 |
| 15:57:22 | 1708 | 1.0 | 398.29 |
| 15:57:23 | 1708 | 0.9 | 398.31 |
| 15:57:24 | 1708 | 0.9 | 398.32 |
| 15:57:25 | 1708 | 0.9 | 398.34 |
| 15:57:26 | 1708 | 0.9 | 398.35 |
| 15:57:27 | 1708 | 0.9 | 398.37 |
| 15:57:28 | 1708 | 0.9 | 398.38 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:57:29 | 1708 | 0.9 | 398.40 |
| 15:57:30 | 1708 | 0.9 | 398.42 |
| 15:57:31 | 1708 | 0.9 | 398.43 |
| 15:57:32 | 1708 | 0.9 | 398.45 |
| 15:57:33 | 1708 | 0.9 | 398.46 |
| 15:57:34 | 1708 | 0.9 | 398.48 |
| 15:57:35 | 1708 | 0.9 | 398.50 |
| 15:57:36 | 1708 | 0.9 | 398.51 |
| 15:57:37 | 1708 | 0.9 | 398.53 |
| 15:57:38 | 1709 | 0.9 | 398.54 |
| 15:57:39 | 1709 | 0.9 | 398.56 |
| 15:57:40 | 1709 | 0.9 | 398.57 |
| 15:57:41 | 1708 | 0.9 | 398.59 |
| 15:57:42 | 1708 | 0.9 | 398.61 |
| 15:57:43 | 1708 | 1.0 | 398.62 |
| 15:57:44 | 1708 | 1.0 | 398.64 |
| 15:57:45 | 1708 | 0.9 | 398.65 |
| 15:57:46 | 1708 | 0.9 | 398.67 |
| 15:57:47 | 1708 | 0.9 | 398.69 |
| 15:57:48 | 1709 | 0.9 | 398.70 |
| 15:57:49 | 1709 | 0.9 | 398.72 |
| 15:57:50 | 1709 | 0.9 | 398.73 |
| 15:57:51 | 1709 | 0.9 | 398.75 |
| 15:57:52 | 1709 | 0.9 | 398.76 |
| 15:57:53 | 1709 | 0.9 | 398.78 |
| 15:57:54 | 1709 | 0.9 | 398.80 |
| 15:57:55 | 1709 | 0.9 | 398.81 |
| 15:57:56 | 1709 | 1.0 | 398.83 |
| 15:57:57 | 1709 | 0.9 | 398.84 |
| 15:57:58 | 1709 | 0.9 | 398.86 |
| 15:57:59 | 1709 | 0.9 | 398.87 |
| 15:58:00 | 1709 | 0.9 | 398.89 |
| 15:58:01 | 1709 | 0.9 | 398.91 |
| 15:58:02 | 1709 | 0.9 | 398.92 |
| 15:58:03 | 1709 | 0.9 | 398.94 |
| 15:58:04 | 1709 | 0.9 | 398.95 |
| 15:58:05 | 1709 | 1.0 | 398.97 |
| 15:58:06 | 1709 | 0.9 | 398.99 |
| 15:58:07 | 1709 | 0.9 | 399.00 |
| 15:58:08 | 1709 | 0.9 | 399.02 |
| 15:58:09 | 1709 | 1.0 | 399.03 |
| 15:58:10 | 1709 | 0.9 | 399.05 |
| 15:58:11 | 1709 | 0.9 | 399.06 |
| 15:58:12 | 1709 | 0.9 | 399.08 |
| 15:58:13 | 1710 | 0.9 | 399.10 |
| 15:58:14 | 1710 | 0.9 | 399.11 |
| 15:58:15 | 1710 | 0.9 | 399.13 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:58:16 | 1710 | 0.9 | 399.14 |
| 15:58:17 | 1710 | 1.0 | 399.16 |
| 15:58:18 | 1710 | 0.9 | 399.18 |
| 15:58:19 | 1710 | 0.9 | 399.19 |
| 15:58:20 | 1709 | 0.9 | 399.21 |
| 15:58:21 | 1710 | 0.9 | 399.22 |
| 15:58:22 | 1710 | 0.9 | 399.24 |
| 15:58:23 | 1710 | 0.9 | 399.25 |
| 15:58:24 | 1710 | 0.9 | 399.27 |
| 15:58:25 | 1710 | 0.9 | 399.29 |
| 15:58:26 | 1710 | 0.9 | 399.30 |
| 15:58:27 | 1710 | 0.9 | 399.32 |
| 15:58:28 | 1710 | 0.9 | 399.33 |
| 15:58:29 | 1710 | 0.9 | 399.35 |
| 15:58:30 | 1710 | 1.0 | 399.37 |
| 15:58:31 | 1710 | 0.9 | 399.38 |
| 15:58:32 | 1710 | 0.9 | 399.40 |
| 15:58:33 | 1710 | 0.9 | 399.41 |
| 15:58:34 | 1710 | 0.9 | 399.43 |
| 15:58:35 | 1710 | 0.9 | 399.44 |
| 15:58:36 | 1711 | 0.9 | 399.46 |
| 15:58:37 | 1711 | 0.9 | 399.48 |
| 15:58:38 | 1711 | 1.0 | 399.49 |
| 15:58:39 | 1711 | 0.9 | 399.51 |
| 15:58:40 | 1711 | 1.0 | 399.52 |
| 15:58:41 | 1711 | 0.9 | 399.54 |
| 15:58:42 | 1711 | 0.9 | 399.56 |
| 15:58:43 | 1711 | 0.9 | 399.57 |
| 15:58:44 | 1711 | 0.9 | 399.59 |
| 15:58:45 | 1711 | 0.9 | 399.60 |
| 15:58:46 | 1711 | 0.9 | 399.62 |
| 15:58:47 | 1711 | 0.9 | 399.63 |
| 15:58:48 | 1711 | 0.9 | 399.65 |
| 15:58:49 | 1711 | 0.9 | 399.67 |
| 15:58:50 | 1711 | 0.9 | 399.68 |
| 15:58:51 | 1711 | 1.0 | 399.70 |
| 15:58:52 | 1711 | 0.9 | 399.71 |
| 15:58:53 | 1711 | 0.9 | 399.73 |
| 15:58:54 | 1711 | 0.9 | 399.75 |
| 15:58:55 | 1711 | 0.9 | 399.76 |
| 15:58:56 | 1711 | 0.9 | 399.78 |
| 15:58:57 | 1711 | 0.9 | 399.79 |
| 15:58:58 | 1711 | 0.9 | 399.81 |
| 15:58:59 | 1711 | 0.9 | 399.82 |
| 15:59:00 | 1711 | 0.9 | 399.84 |
| 15:59:01 | 1712 | 0.9 | 399.86 |
| 15:59:02 | 1712 | 0.9 | 399.87 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:59:03 | 1712 | 0.9 | 399.89 |
| 15:59:04 | 1711 | 0.9 | 399.90 |
| 15:59:05 | 1711 | 0.9 | 399.92 |
| 15:59:06 | 1711 | 0.9 | 399.94 |
| 15:59:07 | 1711 | 0.9 | 399.95 |
| 15:59:08 | 1711 | 0.9 | 399.97 |
| 15:59:09 | 1711 | 0.9 | 399.98 |
| 15:59:10 | 1712 | 0.9 | 400.00 |
| 15:59:11 | 1712 | 0.9 | 400.01 |
| 15:59:12 | 1712 | 1.0 | 400.03 |
| 15:59:13 | 1712 | 0.9 | 400.05 |
| 15:59:14 | 1712 | 0.9 | 400.06 |
| 15:59:15 | 1712 | 0.9 | 400.08 |
| 15:59:16 | 1712 | 0.9 | 400.09 |
| 15:59:17 | 1712 | 0.9 | 400.11 |
| 15:59:18 | 1712 | 0.9 | 400.12 |
| 15:59:19 | 1712 | 0.9 | 400.14 |
| 15:59:20 | 1712 | 0.9 | 400.16 |
| 15:59:21 | 1712 | 0.9 | 400.17 |
| 15:59:22 | 1712 | 0.9 | 400.19 |
| 15:59:23 | 1713 | 0.9 | 400.20 |
| 15:59:24 | 1713 | 0.9 | 400.22 |
| 15:59:25 | 1713 | 0.9 | 400.24 |
| 15:59:26 | 1712 | 0.9 | 400.25 |
| 15:59:27 | 1712 | 0.9 | 400.27 |
| 15:59:28 | 1713 | 0.9 | 400.28 |
| 15:59:29 | 1713 | 0.9 | 400.30 |
| 15:59:30 | 1713 | 0.9 | 400.31 |
| 15:59:31 | 1713 | 0.9 | 400.33 |
| 15:59:32 | 1713 | 0.9 | 400.35 |
| 15:59:33 | 1713 | 1.0 | 400.36 |
| 15:59:34 | 1713 | 0.9 | 400.38 |
| 15:59:35 | 1713 | 0.9 | 400.39 |
| 15:59:36 | 1713 | 0.9 | 400.41 |
| 15:59:37 | 1713 | 0.9 | 400.43 |
| 15:59:38 | 1713 | 0.9 | 400.44 |
| 15:59:39 | 1713 | 0.9 | 400.46 |
| 15:59:40 | 1713 | 0.9 | 400.47 |
| 15:59:41 | 1713 | 0.9 | 400.49 |
| 15:59:42 | 1713 | 0.9 | 400.50 |
| 15:59:43 | 1713 | 0.9 | 400.52 |
| 15:59:44 | 1713 | 0.9 | 400.54 |
| 15:59:45 | 1713 | 1.0 | 400.55 |
| 15:59:46 | 1714 | 0.9 | 400.57 |
| 15:59:47 | 1714 | 0.9 | 400.58 |
| 15:59:48 | 1714 | 1.0 | 400.60 |
| 15:59:49 | 1714 | 0.9 | 400.62 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 15:59:50 | 1714 | 0.9 | 400.63 |
| 15:59:51 | 1714 | 0.9 | 400.65 |
| 15:59:52 | 1714 | 0.9 | 400.66 |
| 15:59:53 | 1714 | 0.9 | 400.68 |
| 15:59:54 | 1714 | 0.9 | 400.69 |
| 15:59:55 | 1714 | 0.9 | 400.71 |
| 15:59:56 | 1714 | 0.9 | 400.73 |
| 15:59:57 | 1715 | 0.9 | 400.74 |
| 15:59:58 | 1715 | 0.9 | 400.76 |
| 15:59:59 | 1715 | 0.9 | 400.77 |
| 16:00:00 | 1715 | 0.9 | 400.79 |
| 16:00:01 | 1715 | 0.9 | 400.81 |
| 16:00:02 | 1715 | 0.9 | 400.82 |
| 16:00:03 | 1715 | 0.9 | 400.84 |
| 16:00:04 | 1715 | 0.9 | 400.85 |
| 16:00:05 | 1715 | 0.9 | 400.87 |
| 16:00:06 | 1715 | 0.9 | 400.88 |
| 16:00:07 | 1715 | 0.9 | 400.90 |
| 16:00:08 | 1715 | 0.9 | 400.92 |
| 16:00:09 | 1716 | 1.0 | 400.93 |
| 16:00:10 | 1716 | 0.9 | 400.95 |
| 16:00:11 | 1716 | 0.9 | 400.96 |
| 16:00:12 | 1716 | 0.9 | 400.98 |
| 16:00:13 | 1716 | 0.9 | 400.99 |
| 16:00:14 | 1716 | 0.9 | 401.01 |
| 16:00:15 | 1716 | 0.9 | 401.03 |
| 16:00:16 | 1716 | 0.9 | 401.04 |
| 16:00:17 | 1716 | 0.9 | 401.06 |
| 16:00:18 | 1716 | 0.9 | 401.07 |
| 16:00:19 | 1716 | 0.9 | 401.09 |
| 16:00:20 | 1716 | 0.9 | 401.11 |
| 16:00:21 | 1716 | 0.9 | 401.12 |
| 16:00:22 | 1716 | 0.9 | 401.14 |
| 16:00:23 | 1716 | 0.9 | 401.15 |
| 16:00:24 | 1716 | 0.9 | 401.17 |
| 16:00:25 | 1716 | 0.9 | 401.18 |
| 16:00:26 | 1716 | 0.9 | 401.20 |
| 16:00:27 | 1716 | 0.9 | 401.22 |
| 16:00:28 | 1716 | 0.9 | 401.23 |
| 16:00:29 | 1716 | 0.9 | 401.25 |
| 16:00:30 | 1716 | 0.9 | 401.26 |
| 16:00:31 | 1716 | 0.9 | 401.28 |
| 16:00:32 | 1716 | 0.9 | 401.30 |
| 16:00:33 | 1716 | 0.9 | 401.31 |
| 16:00:34 | 1717 | 0.9 | 401.33 |
| 16:00:35 | 1717 | 0.9 | 401.34 |
| 16:00:36 | 1717 | 0.9 | 401.36 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:00:37 | 1716 | 0.9 | 401.37 |
| 16:00:38 | 1716 | 0.9 | 401.39 |
| 16:00:39 | 1716 | 0.9 | 401.41 |
| 16:00:40 | 1716 | 0.9 | 401.42 |
| 16:00:41 | 1716 | 0.9 | 401.44 |
| 16:00:42 | 1716 | 0.9 | 401.45 |
| 16:00:43 | 1717 | 0.9 | 401.47 |
| 16:00:44 | 1717 | 0.9 | 401.49 |
| 16:00:45 | 1717 | 0.9 | 401.50 |
| 16:00:46 | 1717 | 0.9 | 401.52 |
| 16:00:47 | 1717 | 0.9 | 401.53 |
| 16:00:48 | 1717 | 0.9 | 401.55 |
| 16:00:49 | 1717 | 0.9 | 401.56 |
| 16:00:50 | 1717 | 0.9 | 401.58 |
| 16:00:51 | 1717 | 0.9 | 401.60 |
| 16:00:52 | 1717 | 0.9 | 401.61 |
| 16:00:53 | 1717 | 0.9 | 401.63 |
| 16:00:54 | 1717 | 0.9 | 401.64 |
| 16:00:55 | 1717 | 0.9 | 401.66 |
| 16:00:56 | 1717 | 0.9 | 401.67 |
| 16:00:57 | 1717 | 0.9 | 401.69 |
| 16:00:58 | 1717 | 0.9 | 401.71 |
| 16:00:59 | 1717 | 0.9 | 401.72 |
| 16:01:00 | 1717 | 0.9 | 401.74 |
| 16:01:01 | 1717 | 0.9 | 401.75 |
| 16:01:02 | 1717 | 0.9 | 401.77 |
| 16:01:03 | 1717 | 0.9 | 401.79 |
| 16:01:04 | 1717 | 0.9 | 401.80 |
| 16:01:05 | 1717 | 0.9 | 401.82 |
| 16:01:06 | 1717 | 0.9 | 401.83 |
| 16:01:07 | 1717 | 0.9 | 401.85 |
| 16:01:08 | 1717 | 0.9 | 401.86 |
| 16:01:09 | 1717 | 0.9 | 401.88 |
| 16:01:10 | 1717 | 0.9 | 401.90 |
| 16:01:11 | 1717 | 0.9 | 401.91 |
| 16:01:12 | 1717 | 0.9 | 401.93 |
| 16:01:13 | 1717 | 0.9 | 401.94 |
| 16:01:14 | 1717 | 0.9 | 401.96 |
| 16:01:15 | 1717 | 0.9 | 401.98 |
| 16:01:16 | 1717 | 0.9 | 401.99 |
| 16:01:17 | 1717 | 0.9 | 402.01 |
| 16:01:18 | 1717 | 0.9 | 402.02 |
| 16:01:19 | 1717 | 0.9 | 402.04 |
| 16:01:20 | 1717 | 0.9 | 402.05 |
| 16:01:21 | 1718 | 0.9 | 402.07 |
| 16:01:22 | 1718 | 0.9 | 402.09 |
| 16:01:23 | 1718 | 0.9 | 402.10 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:01:24 | 1717 | 0.9 | 402.12 |
| 16:01:25 | 1717 | 0.9 | 402.13 |
| 16:01:26 | 1717 | 0.9 | 402.15 |
| 16:01:27 | 1717 | 0.9 | 402.17 |
| 16:01:28 | 1717 | 0.9 | 402.18 |
| 16:01:29 | 1718 | 0.9 | 402.20 |
| 16:01:30 | 1718 | 0.9 | 402.21 |
| 16:01:31 | 1718 | 0.9 | 402.23 |
| 16:01:32 | 1718 | 0.9 | 402.24 |
| 16:01:33 | 1718 | 0.9 | 402.26 |
| 16:01:34 | 1718 | 0.9 | 402.28 |
| 16:01:35 | 1718 | 0.9 | 402.29 |
| 16:01:36 | 1717 | 0.9 | 402.31 |
| 16:01:37 | 1717 | 0.9 | 402.32 |
| 16:01:38 | 1717 | 0.9 | 402.34 |
| 16:01:39 | 1717 | 0.9 | 402.35 |
| 16:01:40 | 1718 | 0.9 | 402.37 |
| 16:01:41 | 1718 | 0.9 | 402.39 |
| 16:01:42 | 1718 | 0.9 | 402.40 |
| 16:01:43 | 1718 | 0.9 | 402.42 |
| 16:01:44 | 1718 | 0.9 | 402.43 |
| 16:01:45 | 1718 | 0.9 | 402.45 |
| 16:01:46 | 1718 | 0.9 | 402.47 |
| 16:01:47 | 1718 | 0.9 | 402.48 |
| 16:01:48 | 1718 | 0.9 | 402.50 |
| 16:01:49 | 1718 | 0.9 | 402.51 |
| 16:01:50 | 1718 | 0.9 | 402.53 |
| 16:01:51 | 1718 | 0.9 | 402.54 |
| 16:01:52 | 1718 | 0.9 | 402.56 |
| 16:01:53 | 1718 | 0.9 | 402.58 |
| 16:01:54 | 1718 | 0.9 | 402.59 |
| 16:01:55 | 1718 | 0.9 | 402.61 |
| 16:01:56 | 1718 | 0.9 | 402.62 |
| 16:01:57 | 1718 | 0.9 | 402.64 |
| 16:01:58 | 1718 | 0.9 | 402.66 |
| 16:01:59 | 1718 | 0.9 | 402.67 |
| 16:02:00 | 1718 | 0.9 | 402.69 |
| 16:02:01 | 1718 | 0.9 | 402.70 |
| 16:02:02 | 1718 | 0.9 | 402.72 |
| 16:02:03 | 1718 | 0.9 | 402.73 |
| 16:02:04 | 1718 | 0.9 | 402.75 |
| 16:02:05 | 1718 | 0.9 | 402.77 |
| 16:02:06 | 1718 | 0.9 | 402.78 |
| 16:02:07 | 1718 | 0.9 | 402.80 |
| 16:02:08 | 1719 | 0.9 | 402.81 |
| 16:02:09 | 1719 | 0.9 | 402.83 |
| 16:02:10 | 1718 | 0.9 | 402.85 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:02:11 | 1718 | 0.9 | 402.86 |
| 16:02:12 | 1718 | 0.9 | 402.88 |
| 16:02:13 | 1718 | 0.9 | 402.89 |
| 16:02:14 | 1718 | 0.9 | 402.91 |
| 16:02:15 | 1718 | 0.9 | 402.92 |
| 16:02:16 | 1719 | 0.9 | 402.94 |
| 16:02:17 | 1719 | 0.9 | 402.96 |
| 16:02:18 | 1719 | 0.9 | 402.97 |
| 16:02:19 | 1719 | 0.9 | 402.99 |
| 16:02:20 | 1719 | 0.9 | 403.00 |
| 16:02:21 | 1719 | 0.9 | 403.02 |
| 16:02:22 | 1719 | 0.9 | 403.03 |
| 16:02:23 | 1719 | 0.9 | 403.05 |
| 16:02:24 | 1719 | 0.9 | 403.07 |
| 16:02:25 | 1719 | 0.9 | 403.08 |
| 16:02:26 | 1719 | 0.9 | 403.10 |
| 16:02:27 | 1719 | 0.9 | 403.11 |
| 16:02:28 | 1719 | 0.9 | 403.13 |
| 16:02:29 | 1719 | 0.9 | 403.15 |
| 16:02:30 | 1719 | 0.9 | 403.16 |
| 16:02:31 | 1719 | 0.9 | 403.18 |
| 16:02:32 | 1719 | 0.9 | 403.19 |
| 16:02:33 | 1719 | 0.9 | 403.21 |
| 16:02:34 | 1719 | 0.9 | 403.22 |
| 16:02:35 | 1719 | 0.9 | 403.24 |
| 16:02:36 | 1719 | 0.9 | 403.26 |
| 16:02:37 | 1719 | 0.9 | 403.27 |
| 16:02:38 | 1719 | 0.9 | 403.29 |
| 16:02:39 | 1719 | 0.9 | 403.30 |
| 16:02:40 | 1719 | 0.9 | 403.32 |
| 16:02:41 | 1719 | 0.9 | 403.34 |
| 16:02:42 | 1719 | 0.9 | 403.35 |
| 16:02:43 | 1719 | 0.9 | 403.37 |
| 16:02:44 | 1719 | 0.9 | 403.38 |
| 16:02:45 | 1719 | 0.9 | 403.40 |
| 16:02:46 | 1719 | 0.9 | 403.41 |
| 16:02:47 | 1719 | 0.9 | 403.43 |
| 16:02:48 | 1719 | 0.9 | 403.45 |
| 16:02:49 | 1719 | 0.9 | 403.46 |
| 16:02:50 | 1719 | 0.9 | 403.48 |
| 16:02:51 | 1719 | 0.9 | 403.49 |
| 16:02:52 | 1719 | 0.9 | 403.51 |
| 16:02:53 | 1719 | 0.9 | 403.53 |
| 16:02:54 | 1719 | 0.9 | 403.54 |
| 16:02:55 | 1719 | 0.9 | 403.56 |
| 16:02:56 | 1719 | 0.9 | 403.57 |
| 16:02:57 | 1719 | 0.9 | 403.59 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:02:58 | 1719 | 0.9 | 403.60 |
| 16:02:59 | 1719 | 0.9 | 403.62 |
| 16:03:00 | 1719 | 0.9 | 403.64 |
| 16:03:01 | 1719 | 0.9 | 403.65 |
| 16:03:02 | 1719 | 0.9 | 403.67 |
| 16:03:03 | 1719 | 0.9 | 403.68 |
| 16:03:04 | 1719 | 0.9 | 403.70 |
| 16:03:05 | 1720 | 0.9 | 403.71 |
| 16:03:06 | 1719 | 0.9 | 403.73 |
| 16:03:07 | 1720 | 0.9 | 403.75 |
| 16:03:08 | 1719 | 0.9 | 403.76 |
| 16:03:09 | 1719 | 0.9 | 403.78 |
| 16:03:10 | 1719 | 0.9 | 403.79 |
| 16:03:11 | 1719 | 0.9 | 403.81 |
| 16:03:12 | 1719 | 0.9 | 403.83 |
| 16:03:13 | 1719 | 0.9 | 403.84 |
| 16:03:14 | 1719 | 0.9 | 403.86 |
| 16:03:15 | 1719 | 0.9 | 403.87 |
| 16:03:16 | 1720 | 0.9 | 403.89 |
| 16:03:17 | 1720 | 0.9 | 403.90 |
| 16:03:18 | 1720 | 0.9 | 403.92 |
| 16:03:19 | 1720 | 0.9 | 403.94 |
| 16:03:20 | 1720 | 0.9 | 403.95 |
| 16:03:21 | 1720 | 0.9 | 403.97 |
| 16:03:22 | 1720 | 0.9 | 403.98 |
| 16:03:23 | 1720 | 0.9 | 404.00 |
| 16:03:24 | 1720 | 0.9 | 404.02 |
| 16:03:25 | 1719 | 0.9 | 404.03 |
| 16:03:26 | 1720 | 0.9 | 404.05 |
| 16:03:27 | 1719 | 0.9 | 404.06 |
| 16:03:28 | 1720 | 0.9 | 404.08 |
| 16:03:29 | 1720 | 0.9 | 404.09 |
| 16:03:30 | 1720 | 0.9 | 404.11 |
| 16:03:31 | 1720 | 0.9 | 404.13 |
| 16:03:32 | 1720 | 0.9 | 404.14 |
| 16:03:33 | 1720 | 0.9 | 404.16 |
| 16:03:34 | 1720 | 0.9 | 404.17 |
| 16:03:35 | 1719 | 0.9 | 404.19 |
| 16:03:36 | 1719 | 0.9 | 404.20 |
| 16:03:37 | 1720 | 0.9 | 404.22 |
| 16:03:38 | 1720 | 0.9 | 404.24 |
| 16:03:39 | 1720 | 0.9 | 404.25 |
| 16:03:40 | 1720 | 0.9 | 404.27 |
| 16:03:41 | 1720 | 0.9 | 404.28 |
| 16:03:42 | 1720 | 0.9 | 404.30 |
| 16:03:43 | 1720 | 0.9 | 404.32 |
| 16:03:44 | 1720 | 0.9 | 404.33 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:03:45 | 1720 | 0.9 | 404.35 |
| 16:03:46 | 1720 | 0.9 | 404.36 |
| 16:03:47 | 1720 | 0.9 | 404.38 |
| 16:03:48 | 1720 | 0.9 | 404.39 |
| 16:03:49 | 1720 | 0.9 | 404.41 |
| 16:03:50 | 1720 | 0.9 | 404.43 |
| 16:03:51 | 1720 | 0.9 | 404.44 |
| 16:03:52 | 1721 | 0.9 | 404.46 |
| 16:03:53 | 1721 | 0.9 | 404.47 |
| 16:03:54 | 1721 | 0.9 | 404.49 |
| 16:03:55 | 1721 | 0.9 | 404.51 |
| 16:03:56 | 1720 | 0.9 | 404.52 |
| 16:03:57 | 1720 | 0.9 | 404.54 |
| 16:03:58 | 1720 | 0.9 | 404.55 |
| 16:03:59 | 1720 | 0.9 | 404.57 |
| 16:04:00 | 1720 | 0.9 | 404.58 |
| 16:04:01 | 1720 | 0.9 | 404.60 |
| 16:04:02 | 1720 | 0.9 | 404.62 |
| 16:04:03 | 1721 | 0.9 | 404.63 |
| 16:04:04 | 1720 | 0.9 | 404.65 |
| 16:04:05 | 1720 | 0.9 | 404.66 |
| 16:04:06 | 1720 | 0.9 | 404.68 |
| 16:04:07 | 1720 | 0.9 | 404.70 |
| 16:04:08 | 1720 | 0.9 | 404.71 |
| 16:04:09 | 1720 | 0.9 | 404.73 |
| 16:04:10 | 1720 | 0.9 | 404.74 |
| 16:04:11 | 1720 | 0.9 | 404.76 |
| 16:04:12 | 1720 | 0.9 | 404.77 |
| 16:04:13 | 1720 | 0.9 | 404.79 |
| 16:04:14 | 1720 | 0.9 | 404.81 |
| 16:04:15 | 1720 | 0.9 | 404.82 |
| 16:04:16 | 1721 | 0.9 | 404.84 |
| 16:04:17 | 1721 | 0.9 | 404.85 |
| 16:04:18 | 1721 | 0.9 | 404.87 |
| 16:04:19 | 1721 | 0.9 | 404.88 |
| 16:04:20 | 1720 | 0.9 | 404.90 |
| 16:04:21 | 1720 | 0.9 | 404.92 |
| 16:04:22 | 1720 | 0.9 | 404.93 |
| 16:04:23 | 1720 | 0.9 | 404.95 |
| 16:04:24 | 1720 | 0.9 | 404.96 |
| 16:04:25 | 1720 | 0.9 | 404.98 |
| 16:04:26 | 1721 | 0.9 | 405.00 |
| 16:04:27 | 1721 | 0.9 | 405.01 |
| 16:04:28 | 1721 | 0.9 | 405.03 |
| 16:04:29 | 1721 | 0.9 | 405.04 |
| 16:04:30 | 1721 | 0.9 | 405.06 |
| 16:04:31 | 1721 | 0.9 | 405.07 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:04:32 | 1721 | 0.9 | 405.09 |
| 16:04:33 | 1721 | 0.9 | 405.11 |
| 16:04:34 | 1721 | 0.9 | 405.12 |
| 16:04:35 | 1721 | 0.9 | 405.14 |
| 16:04:36 | 1721 | 0.9 | 405.15 |
| 16:04:37 | 1721 | 0.9 | 405.17 |
| 16:04:38 | 1721 | 0.9 | 405.19 |
| 16:04:39 | 1721 | 0.9 | 405.20 |
| 16:04:40 | 1721 | 0.9 | 405.22 |
| 16:04:41 | 1721 | 0.9 | 405.23 |
| 16:04:42 | 1721 | 0.9 | 405.25 |
| 16:04:43 | 1721 | 0.9 | 405.26 |
| 16:04:44 | 1721 | 0.9 | 405.28 |
| 16:04:45 | 1721 | 0.9 | 405.30 |
| 16:04:46 | 1721 | 0.9 | 405.31 |
| 16:04:47 | 1721 | 0.9 | 405.33 |
| 16:04:48 | 1721 | 0.9 | 405.34 |
| 16:04:49 | 1721 | 0.9 | 405.36 |
| 16:04:50 | 1721 | 0.9 | 405.38 |
| 16:04:51 | 1721 | 0.9 | 405.39 |
| 16:04:52 | 1721 | 0.9 | 405.41 |
| 16:04:53 | 1721 | 0.9 | 405.42 |
| 16:04:54 | 1721 | 0.9 | 405.44 |
| 16:04:55 | 1721 | 0.9 | 405.45 |
| 16:04:56 | 1721 | 0.9 | 405.47 |
| 16:04:57 | 1721 | 0.9 | 405.49 |
| 16:04:58 | 1721 | 0.9 | 405.50 |
| 16:04:59 | 1721 | 0.9 | 405.52 |
| 16:05:00 | 1721 | 0.9 | 405.53 |
| 16:05:01 | 1721 | 0.9 | 405.55 |
| 16:05:02 | 1721 | 0.9 | 405.56 |
| 16:05:03 | 1721 | 0.9 | 405.58 |
| 16:05:04 | 1722 | 0.9 | 405.60 |
| 16:05:05 | 1721 | 0.9 | 405.61 |
| 16:05:06 | 1721 | 0.9 | 405.63 |
| 16:05:07 | 1721 | 0.9 | 405.64 |
| 16:05:08 | 1721 | 0.9 | 405.66 |
| 16:05:09 | 1721 | 0.9 | 405.68 |
| 16:05:10 | 1721 | 0.9 | 405.69 |
| 16:05:11 | 1721 | 0.9 | 405.71 |
| 16:05:12 | 1721 | 0.9 | 405.72 |
| 16:05:13 | 1722 | 0.9 | 405.74 |
| 16:05:14 | 1722 | 0.9 | 405.75 |
| 16:05:15 | 1722 | 0.9 | 405.77 |
| 16:05:16 | 1722 | 0.9 | 405.79 |
| 16:05:17 | 1722 | 0.9 | 405.80 |
| 16:05:18 | 1721 | 0.9 | 405.82 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:05:19 | 1721 | 0.9 | 405.83 |
| 16:05:20 | 1721 | 0.9 | 405.85 |
| 16:05:21 | 1721 | 0.9 | 405.87 |
| 16:05:22 | 1722 | 0.9 | 405.88 |
| 16:05:23 | 1722 | 0.9 | 405.90 |
| 16:05:24 | 1722 | 0.9 | 405.91 |
| 16:05:25 | 1722 | 0.9 | 405.93 |
| 16:05:26 | 1722 | 0.9 | 405.94 |
| 16:05:27 | 1722 | 0.9 | 405.96 |
| 16:05:28 | 1722 | 0.9 | 405.98 |
| 16:05:29 | 1722 | 0.9 | 405.99 |
| 16:05:30 | 1722 | 0.9 | 406.01 |
| 16:05:31 | 1722 | 0.9 | 406.02 |
| 16:05:32 | 1722 | 0.9 | 406.04 |
| 16:05:33 | 1722 | 0.9 | 406.05 |
| 16:05:34 | 1722 | 0.9 | 406.07 |
| 16:05:35 | 1722 | 0.9 | 406.09 |
| 16:05:36 | 1722 | 0.9 | 406.10 |
| 16:05:37 | 1722 | 0.9 | 406.12 |
| 16:05:38 | 1722 | 0.9 | 406.13 |
| 16:05:39 | 1722 | 0.9 | 406.15 |
| 16:05:40 | 1722 | 0.9 | 406.17 |
| 16:05:41 | 1722 | 0.9 | 406.18 |
| 16:05:42 | 1722 | 0.9 | 406.20 |
| 16:05:43 | 1722 | 0.9 | 406.21 |
| 16:05:44 | 1722 | 0.9 | 406.23 |
| 16:05:45 | 1722 | 0.9 | 406.24 |
| 16:05:46 | 1722 | 0.9 | 406.26 |
| 16:05:47 | 1722 | 0.9 | 406.28 |
| 16:05:48 | 1722 | 0.9 | 406.29 |
| 16:05:49 | 1722 | 0.9 | 406.31 |
| 16:05:50 | 1722 | 0.9 | 406.32 |
| 16:05:51 | 1723 | 0.9 | 406.34 |
| 16:05:52 | 1722 | 0.9 | 406.36 |
| 16:05:53 | 1722 | 0.9 | 406.37 |
| 16:05:54 | 1722 | 0.9 | 406.39 |
| 16:05:55 | 1722 | 0.9 | 406.40 |
| 16:05:56 | 1722 | 0.9 | 406.42 |
| 16:05:57 | 1722 | 0.9 | 406.43 |
| 16:05:58 | 1722 | 0.9 | 406.45 |
| 16:05:59 | 1723 | 0.9 | 406.47 |
| 16:06:00 | 1723 | 0.9 | 406.48 |
| 16:06:01 | 1723 | 0.9 | 406.50 |
| 16:06:02 | 1723 | 0.9 | 406.51 |
| 16:06:03 | 1723 | 0.9 | 406.53 |
| 16:06:04 | 1723 | 0.9 | 406.55 |
| 16:06:05 | 1723 | 0.9 | 406.56 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:06:06 | 1723 | 0.9 | 406.58 |
| 16:06:07 | 1723 | 0.9 | 406.59 |
| 16:06:08 | 1723 | 0.9 | 406.61 |
| 16:06:09 | 1723 | 0.9 | 406.62 |
| 16:06:10 | 1723 | 0.9 | 406.64 |
| 16:06:11 | 1723 | 0.9 | 406.66 |
| 16:06:12 | 1723 | 0.9 | 406.67 |
| 16:06:13 | 1723 | 0.9 | 406.69 |
| 16:06:14 | 1723 | 0.9 | 406.70 |
| 16:06:15 | 1723 | 0.9 | 406.72 |
| 16:06:16 | 1723 | 0.9 | 406.73 |
| 16:06:17 | 1723 | 0.9 | 406.75 |
| 16:06:18 | 1723 | 0.9 | 406.77 |
| 16:06:19 | 1723 | 0.9 | 406.78 |
| 16:06:20 | 1723 | 0.9 | 406.80 |
| 16:06:21 | 1723 | 0.9 | 406.81 |
| 16:06:22 | 1723 | 0.9 | 406.83 |
| 16:06:23 | 1723 | 0.9 | 406.85 |
| 16:06:24 | 1723 | 0.9 | 406.86 |
| 16:06:25 | 1723 | 1.0 | 406.88 |
| 16:06:26 | 1723 | 0.9 | 406.89 |
| 16:06:27 | 1723 | 0.9 | 406.91 |
| 16:06:28 | 1723 | 0.9 | 406.92 |
| 16:06:29 | 1723 | 0.9 | 406.94 |
| 16:06:30 | 1723 | 0.9 | 406.96 |
| 16:06:31 | 1723 | 0.9 | 406.97 |
| 16:06:32 | 1723 | 0.9 | 406.99 |
| 16:06:33 | 1723 | 0.9 | 407.00 |
| 16:06:34 | 1723 | 0.9 | 407.02 |
| 16:06:35 | 1723 | 0.9 | 407.04 |
| 16:06:36 | 1724 | 0.9 | 407.05 |
| 16:06:37 | 1724 | 0.9 | 407.07 |
| 16:06:38 | 1723 | 0.9 | 407.08 |
| 16:06:39 | 1723 | 0.9 | 407.10 |
| 16:06:40 | 1723 | 0.9 | 407.11 |
| 16:06:41 | 1723 | 0.9 | 407.13 |
| 16:06:42 | 1723 | 0.9 | 407.15 |
| 16:06:43 | 1723 | 0.9 | 407.16 |
| 16:06:44 | 1723 | 0.9 | 407.18 |
| 16:06:45 | 1724 | 0.9 | 407.19 |
| 16:06:46 | 1724 | 1.0 | 407.21 |
| 16:06:47 | 1724 | 0.9 | 407.23 |
| 16:06:48 | 1724 | 0.9 | 407.24 |
| 16:06:49 | 1724 | 0.9 | 407.26 |
| 16:06:50 | 1724 | 0.9 | 407.27 |
| 16:06:51 | 1724 | 0.9 | 407.29 |
| 16:06:52 | 1724 | 0.9 | 407.30 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:06:53 | 1724 | 0.9 | 407.32 |
| 16:06:54 | 1724 | 0.9 | 407.34 |
| 16:06:55 | 1724 | 0.9 | 407.35 |
| 16:06:56 | 1724 | 0.9 | 407.37 |
| 16:06:57 | 1724 | 0.9 | 407.38 |
| 16:06:58 | 1724 | 0.9 | 407.40 |
| 16:06:59 | 1724 | 0.9 | 407.41 |
| 16:07:00 | 1724 | 0.9 | 407.43 |
| 16:07:01 | 1724 | 0.9 | 407.45 |
| 16:07:02 | 1724 | 0.9 | 407.46 |
| 16:07:03 | 1724 | 0.9 | 407.48 |
| 16:07:04 | 1724 | 0.9 | 407.49 |
| 16:07:05 | 1724 | 0.9 | 407.51 |
| 16:07:06 | 1724 | 0.9 | 407.53 |
| 16:07:07 | 1724 | 0.9 | 407.54 |
| 16:07:08 | 1724 | 0.9 | 407.56 |
| 16:07:09 | 1724 | 0.9 | 407.57 |
| 16:07:10 | 1724 | 0.9 | 407.59 |
| 16:07:11 | 1724 | 0.9 | 407.60 |
| 16:07:12 | 1724 | 0.9 | 407.62 |
| 16:07:13 | 1724 | 0.9 | 407.64 |
| 16:07:14 | 1724 | 0.9 | 407.65 |
| 16:07:15 | 1724 | 0.9 | 407.67 |
| 16:07:16 | 1724 | 0.9 | 407.68 |
| 16:07:17 | 1724 | 0.9 | 407.70 |
| 16:07:18 | 1724 | 0.9 | 407.72 |
| 16:07:19 | 1724 | 0.9 | 407.73 |
| 16:07:20 | 1724 | 1.0 | 407.75 |
| 16:07:21 | 1724 | 0.9 | 407.76 |
| 16:07:22 | 1725 | 0.9 | 407.78 |
| 16:07:23 | 1725 | 0.9 | 407.79 |
| 16:07:24 | 1725 | 0.9 | 407.81 |
| 16:07:25 | 1725 | 0.9 | 407.83 |
| 16:07:26 | 1725 | 0.9 | 407.84 |
| 16:07:27 | 1725 | 0.9 | 407.86 |
| 16:07:28 | 1724 | 0.9 | 407.87 |
| 16:07:29 | 1724 | 0.9 | 407.89 |
| 16:07:30 | 1725 | 0.9 | 407.91 |
| 16:07:31 | 1725 | 0.9 | 407.92 |
| 16:07:32 | 1725 | 0.9 | 407.94 |
| 16:07:33 | 1725 | 0.9 | 407.95 |
| 16:07:34 | 1725 | 0.9 | 407.97 |
| 16:07:35 | 1725 | 0.9 | 407.98 |
| 16:07:36 | 1725 | 0.9 | 408.00 |
| 16:07:37 | 1725 | 0.9 | 408.02 |
| 16:07:38 | 1725 | 0.9 | 408.03 |
| 16:07:39 | 1725 | 0.9 | 408.05 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:07:40 | 1725 | 0.9 | 408.06 |
| 16:07:41 | 1725 | 0.9 | 408.08 |
| 16:07:42 | 1725 | 0.9 | 408.09 |
| 16:07:43 | 1726 | 0.9 | 408.11 |
| 16:07:44 | 1726 | 0.9 | 408.13 |
| 16:07:45 | 1726 | 0.9 | 408.14 |
| 16:07:46 | 1726 | 0.9 | 408.16 |
| 16:07:47 | 1726 | 0.9 | 408.17 |
| 16:07:48 | 1726 | 0.9 | 408.19 |
| 16:07:49 | 1725 | 0.9 | 408.21 |
| 16:07:50 | 1725 | 0.9 | 408.22 |
| 16:07:51 | 1726 | 0.9 | 408.24 |
| 16:07:52 | 1725 | 0.9 | 408.25 |
| 16:07:53 | 1726 | 0.9 | 408.27 |
| 16:07:54 | 1725 | 0.9 | 408.28 |
| 16:07:55 | 1726 | 0.9 | 408.30 |
| 16:07:56 | 1726 | 0.9 | 408.32 |
| 16:07:57 | 1726 | 0.9 | 408.33 |
| 16:07:58 | 1726 | 0.9 | 408.35 |
| 16:07:59 | 1726 | 0.9 | 408.36 |
| 16:08:00 | 1726 | 0.9 | 408.38 |
| 16:08:01 | 1726 | 0.9 | 408.40 |
| 16:08:02 | 1726 | 0.9 | 408.41 |
| 16:08:03 | 1726 | 0.9 | 408.43 |
| 16:08:04 | 1726 | 0.9 | 408.44 |
| 16:08:05 | 1726 | 0.9 | 408.46 |
| 16:08:06 | 1726 | 0.9 | 408.47 |
| 16:08:07 | 1726 | 0.9 | 408.49 |
| 16:08:08 | 1726 | 0.9 | 408.51 |
| 16:08:09 | 1727 | 0.9 | 408.52 |
| 16:08:10 | 1726 | 0.9 | 408.54 |
| 16:08:11 | 1726 | 0.9 | 408.55 |
| 16:08:12 | 1726 | 0.9 | 408.57 |
| 16:08:13 | 1726 | 0.9 | 408.58 |
| 16:08:14 | 1726 | 0.9 | 408.60 |
| 16:08:15 | 1726 | 0.9 | 408.62 |
| 16:08:16 | 1726 | 0.9 | 408.63 |
| 16:08:17 | 1726 | 0.9 | 408.65 |
| 16:08:18 | 1726 | 0.9 | 408.66 |
| 16:08:19 | 1727 | 0.9 | 408.68 |
| 16:08:20 | 1727 | 0.9 | 408.70 |
| 16:08:21 | 1727 | 0.9 | 408.71 |
| 16:08:22 | 1726 | 0.9 | 408.73 |
| 16:08:23 | 1726 | 0.9 | 408.74 |
| 16:08:24 | 1726 | 0.9 | 408.76 |
| 16:08:25 | 1726 | 0.9 | 408.77 |
| 16:08:26 | 1726 | 0.9 | 408.79 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:08:27 | 1726 | 0.9 | 408.81 |
| 16:08:28 | 1727 | 0.9 | 408.82 |
| 16:08:29 | 1727 | 0.9 | 408.84 |
| 16:08:30 | 1727 | 0.9 | 408.85 |
| 16:08:31 | 1727 | 0.9 | 408.87 |
| 16:08:32 | 1727 | 0.9 | 408.88 |
| 16:08:33 | 1727 | 0.9 | 408.90 |
| 16:08:34 | 1727 | 0.9 | 408.92 |
| 16:08:35 | 1727 | 0.9 | 408.93 |
| 16:08:36 | 1727 | 0.9 | 408.95 |
| 16:08:37 | 1727 | 0.9 | 408.96 |
| 16:08:38 | 1727 | 0.9 | 408.98 |
| 16:08:39 | 1727 | 0.9 | 409.00 |
| 16:08:40 | 1727 | 0.9 | 409.01 |
| 16:08:41 | 1727 | 0.9 | 409.03 |
| 16:08:42 | 1727 | 0.9 | 409.04 |
| 16:08:43 | 1727 | 0.9 | 409.06 |
| 16:08:44 | 1727 | 0.9 | 409.07 |
| 16:08:45 | 1727 | 0.9 | 409.09 |
| 16:08:46 | 1727 | 0.9 | 409.11 |
| 16:08:47 | 1727 | 0.9 | 409.12 |
| 16:08:48 | 1727 | 0.9 | 409.14 |
| 16:08:49 | 1727 | 0.9 | 409.15 |
| 16:08:50 | 1727 | 0.9 | 409.17 |
| 16:08:51 | 1727 | 0.9 | 409.18 |
| 16:08:52 | 1727 | 0.9 | 409.20 |
| 16:08:53 | 1727 | 0.9 | 409.22 |
| 16:08:54 | 1727 | 0.9 | 409.23 |
| 16:08:55 | 1727 | 0.9 | 409.25 |
| 16:08:56 | 1727 | 0.9 | 409.26 |
| 16:08:57 | 1727 | 0.9 | 409.28 |
| 16:08:58 | 1727 | 0.9 | 409.29 |
| 16:08:59 | 1727 | 0.9 | 409.31 |
| 16:09:00 | 1727 | 0.9 | 409.33 |
| 16:09:01 | 1727 | 0.9 | 409.34 |
| 16:09:02 | 1727 | 0.9 | 409.36 |
| 16:09:03 | 1727 | 0.9 | 409.37 |
| 16:09:04 | 1728 | 0.9 | 409.39 |
| 16:09:05 | 1728 | 0.9 | 409.40 |
| 16:09:06 | 1727 | 0.9 | 409.42 |
| 16:09:07 | 1727 | 0.9 | 409.44 |
| 16:09:08 | 1727 | 0.9 | 409.45 |
| 16:09:09 | 1727 | 0.9 | 409.47 |
| 16:09:10 | 1727 | 0.9 | 409.48 |
| 16:09:11 | 1727 | 0.9 | 409.50 |
| 16:09:12 | 1727 | 0.9 | 409.51 |
| 16:09:13 | 1728 | 0.9 | 409.53 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:09:14 | 1727 | 0.9 | 409.55 |
| 16:09:15 | 1727 | 0.9 | 409.56 |
| 16:09:16 | 1727 | 0.9 | 409.58 |
| 16:09:17 | 1727 | 0.9 | 409.59 |
| 16:09:18 | 1727 | 0.9 | 409.61 |
| 16:09:19 | 1727 | 0.9 | 409.62 |
| 16:09:20 | 1727 | 0.9 | 409.64 |
| 16:09:21 | 1727 | 0.9 | 409.65 |
| 16:09:22 | 1727 | 0.9 | 409.67 |
| 16:09:23 | 1728 | 0.9 | 409.68 |
| 16:09:24 | 1728 | 0.9 | 409.70 |
| 16:09:25 | 1728 | 0.9 | 409.72 |
| 16:09:26 | 1728 | 0.9 | 409.73 |
| 16:09:27 | 1728 | 0.9 | 409.75 |
| 16:09:28 | 1728 | 0.9 | 409.76 |
| 16:09:29 | 1728 | 0.9 | 409.78 |
| 16:09:30 | 1728 | 0.9 | 409.79 |
| 16:09:31 | 1728 | 0.9 | 409.81 |
| 16:09:32 | 1728 | 0.9 | 409.83 |
| 16:09:33 | 1728 | 0.9 | 409.84 |
| 16:09:34 | 1728 | 0.9 | 409.86 |
| 16:09:35 | 1728 | 0.9 | 409.87 |
| 16:09:36 | 1728 | 0.9 | 409.89 |
| 16:09:37 | 1729 | 0.9 | 409.90 |
| 16:09:38 | 1728 | 0.9 | 409.92 |
| 16:09:39 | 1728 | 0.9 | 409.93 |
| 16:09:40 | 1728 | 0.9 | 409.95 |
| 16:09:41 | 1728 | 0.9 | 409.97 |
| 16:09:42 | 1728 | 0.9 | 409.98 |
| 16:09:43 | 1728 | 0.9 | 410.00 |
| 16:09:44 | 1728 | 0.9 | 410.01 |
| 16:09:45 | 1728 | 0.9 | 410.03 |
| 16:09:46 | 1728 | 0.9 | 410.04 |
| 16:09:47 | 1728 | 0.9 | 410.06 |
| 16:09:48 | 1729 | 0.9 | 410.08 |
| 16:09:49 | 1729 | 0.9 | 410.09 |
| 16:09:50 | 1729 | 0.9 | 410.11 |
| 16:09:51 | 1729 | 0.9 | 410.12 |
| 16:09:52 | 1728 | 0.9 | 410.14 |
| 16:09:53 | 1728 | 0.9 | 410.15 |
| 16:09:54 | 1728 | 0.9 | 410.17 |
| 16:09:55 | 1728 | 0.9 | 410.18 |
| 16:09:56 | 1728 | 0.9 | 410.20 |
| 16:09:57 | 1728 | 0.9 | 410.22 |
| 16:09:58 | 1728 | 0.9 | 410.23 |
| 16:09:59 | 1728 | 0.9 | 410.25 |
| 16:10:00 | 1728 | 0.9 | 410.26 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:10:01 | 1728 | 0.9 | 410.28 |
| 16:10:02 | 1728 | 0.9 | 410.29 |
| 16:10:03 | 1728 | 0.9 | 410.31 |
| 16:10:04 | 1728 | 0.9 | 410.32 |
| 16:10:05 | 1728 | 0.9 | 410.34 |
| 16:10:06 | 1728 | 0.9 | 410.35 |
| 16:10:07 | 1727 | 0.9 | 410.37 |
| 16:10:08 | 1727 | 0.9 | 410.38 |
| 16:10:09 | 1727 | 0.9 | 410.40 |
| 16:10:10 | 1727 | 0.9 | 410.41 |
| 16:10:11 | 1727 | 0.9 | 410.43 |
| 16:10:12 | 1727 | 0.9 | 410.44 |
| 16:10:13 | 1727 | 0.9 | 410.46 |
| 16:10:14 | 1727 | 0.9 | 410.47 |
| 16:10:15 | 1727 | 0.9 | 410.49 |
| 16:10:16 | 1727 | 0.9 | 410.50 |
| 16:10:17 | 1727 | 0.9 | 410.52 |
| 16:10:18 | 1726 | 0.9 | 410.53 |
| 16:10:19 | 1726 | 0.9 | 410.55 |
| 16:10:20 | 1726 | 0.9 | 410.56 |
| 16:10:21 | 1726 | 0.9 | 410.58 |
| 16:10:22 | 1726 | 0.9 | 410.59 |
| 16:10:23 | 1726 | 0.9 | 410.61 |
| 16:10:24 | 1726 | 0.9 | 410.62 |
| 16:10:25 | 1726 | 0.9 | 410.64 |
| 16:10:26 | 1726 | 0.9 | 410.65 |
| 16:10:27 | 1726 | 0.9 | 410.67 |
| 16:10:28 | 1726 | 0.9 | 410.68 |
| 16:10:29 | 1726 | 0.9 | 410.70 |
| 16:10:30 | 1726 | 0.9 | 410.71 |
| 16:10:31 | 1726 | 0.9 | 410.73 |
| 16:10:32 | 1726 | 0.9 | 410.74 |
| 16:10:33 | 1726 | 0.9 | 410.76 |
| 16:10:34 | 1726 | 0.9 | 410.77 |
| 16:10:35 | 1726 | 0.9 | 410.79 |
| 16:10:36 | 1726 | 0.9 | 410.80 |
| 16:10:37 | 1726 | 0.9 | 410.82 |
| 16:10:38 | 1726 | 0.9 | 410.83 |
| 16:10:39 | 1726 | 0.9 | 410.85 |
| 16:10:40 | 1726 | 0.9 | 410.86 |
| 16:10:41 | 1725 | 0.9 | 410.88 |
| 16:10:42 | 1725 | 0.9 | 410.89 |
| 16:10:43 | 1725 | 0.9 | 410.91 |
| 16:10:44 | 1725 | 0.9 | 410.92 |
| 16:10:45 | 1725 | 0.9 | 410.94 |
| 16:10:46 | 1725 | 0.9 | 410.96 |
| 16:10:47 | 1725 | 0.9 | 410.97 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:10:48 | 1726 | 0.9 | 410.99 |
| 16:10:49 | 1726 | 0.9 | 411.00 |
| 16:10:50 | 1725 | 0.9 | 411.02 |
| 16:10:51 | 1725 | 0.9 | 411.03 |
| 16:10:52 | 1725 | 0.9 | 411.05 |
| 16:10:53 | 1725 | 0.9 | 411.06 |
| 16:10:54 | 1726 | 0.9 | 411.08 |
| 16:10:55 | 1726 | 0.9 | 411.09 |
| 16:10:56 | 1726 | 0.9 | 411.11 |
| 16:10:57 | 1726 | 0.9 | 411.12 |
| 16:10:58 | 1726 | 0.9 | 411.14 |
| 16:10:59 | 1726 | 0.9 | 411.15 |
| 16:11:00 | 1726 | 0.9 | 411.17 |
| 16:11:01 | 1726 | 0.9 | 411.18 |
| 16:11:02 | 1725 | 0.9 | 411.20 |
| 16:11:03 | 1726 | 0.9 | 411.21 |
| 16:11:04 | 1726 | 0.9 | 411.23 |
| 16:11:05 | 1726 | 0.9 | 411.24 |
| 16:11:06 | 1726 | 0.9 | 411.26 |
| 16:11:07 | 1726 | 0.9 | 411.27 |
| 16:11:08 | 1726 | 0.9 | 411.29 |
| 16:11:09 | 1726 | 0.9 | 411.30 |
| 16:11:10 | 1726 | 0.9 | 411.32 |
| 16:11:11 | 1726 | 0.9 | 411.33 |
| 16:11:12 | 1725 | 0.9 | 411.35 |
| 16:11:13 | 1725 | 0.9 | 411.36 |
| 16:11:14 | 1725 | 0.9 | 411.38 |
| 16:11:15 | 1725 | 0.9 | 411.40 |
| 16:11:16 | 1725 | 0.9 | 411.41 |
| 16:11:17 | 1725 | 0.9 | 411.43 |
| 16:11:18 | 1725 | 0.9 | 411.44 |
| 16:11:19 | 1725 | 0.9 | 411.46 |
| 16:11:20 | 1726 | 0.9 | 411.47 |
| 16:11:21 | 1725 | 0.9 | 411.49 |
| 16:11:22 | 1725 | 0.9 | 411.50 |
| 16:11:23 | 1725 | 0.9 | 411.52 |
| 16:11:24 | 1725 | 0.9 | 411.53 |
| 16:11:25 | 1725 | 0.9 | 411.55 |
| 16:11:26 | 1724 | 0.9 | 411.56 |
| 16:11:27 | 1724 | 0.9 | 411.57 |
| 16:11:28 | 1725 | 0.9 | 411.59 |
| 16:11:29 | 1725 | 0.9 | 411.60 |
| 16:11:30 | 1725 | 0.9 | 411.62 |
| 16:11:31 | 1724 | 0.9 | 411.63 |
| 16:11:32 | 1725 | 0.9 | 411.65 |
| 16:11:33 | 1724 | 0.9 | 411.66 |
| 16:11:34 | 1724 | 0.9 | 411.68 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:11:35 | 1724 | 0.9 | 411.69 |
| 16:11:36 | 1723 | 0.8 | 411.71 |
| 16:11:37 | 1723 | 0.9 | 411.72 |
| 16:11:38 | 1721 | 0.8 | 411.74 |
| 16:11:39 | 1721 | 0.8 | 411.75 |
| 16:11:40 | 1720 | 0.8 | 411.76 |
| 16:11:41 | 1720 | 0.8 | 411.77 |
| 16:11:42 | 1719 | 0.8 | 411.79 |
| 16:11:43 | 1718 | 0.7 | 411.80 |
| 16:11:44 | 1718 | 0.7 | 411.81 |
| 16:11:45 | 1716 | 0.7 | 411.83 |
| 16:11:46 | 1716 | 0.7 | 411.84 |
| 16:11:47 | 1715 | 0.7 | 411.85 |
| 16:11:48 | 1715 | 0.6 | 411.86 |
| 16:11:49 | 1715 | 0.7 | 411.87 |
| 16:11:50 | 1713 | 0.7 | 411.88 |
| 16:11:51 | 1714 | 0.7 | 411.89 |
| 16:11:52 | 1712 | 0.7 | 411.91 |
| 16:11:53 | 1713 | 0.7 | 411.92 |
| 16:11:54 | 1713 | 0.7 | 411.93 |
| 16:11:55 | 1710 | 0.6 | 411.94 |
| 16:11:56 | 1703 | 0.4 | 411.95 |
| 16:11:57 | 1698 | 0.3 | 411.95 |
| 16:11:58 | 1697 | 0.2 | 411.95 |
| 16:11:59 | 1700 | 0.2 | 411.96 |
| 16:12:00 | 1702 | 0.1 | 411.96 |
| 16:12:01 | 1700 | 0.1 | 411.96 |
| 16:12:02 | 1695 | 0.1 | 411.96 |
| 16:12:03 | 1692 | 0.0 | 411.96 |
| 16:12:04 | 1691 | 0.0 | 411.96 |
| 16:12:05 | 1692 | 0.0 | 411.96 |
| 16:12:06 | 1692 | 0.0 | 411.96 |
| 16:12:07 | 1690 | 0.0 | 411.96 |
| 16:12:08 | 1687 | 0.0 | 411.96 |
| 16:12:09 | 1684 | 0.0 | 411.96 |
| 16:12:10 | 1683 | 0.0 | 411.96 |
| 16:12:11 | 1683 | 0.0 | 411.96 |
| 16:12:12 | 1682 | 0.0 | 411.96 |
| 16:12:13 | 1680 | 0.0 | 411.96 |
| 16:12:14 | 1677 | 0.0 | 411.96 |
| 16:12:15 | 1675 | 0.0 | 411.96 |
| 16:12:16 | 1673 | 0.0 | 411.96 |
| 16:12:17 | 1672 | 0.0 | 411.96 |
| 16:12:18 | 1671 | 0.0 | 411.96 |
| 16:12:19 | 1669 | 0.0 | 411.96 |
| 16:12:20 | 1667 | 0.0 | 411.96 |
| 16:12:21 | 1665 | 0.0 | 411.96 |

| Time (hh:mm:ss) | Treating Pressure (psi) | Slurry Rate (bpm) | Job Slurry Vol (bbl) |
|---|---|---|---|
| 16:12:22 | 1663 | 0.0 | 411.96 |
| 16:12:23 | 1662 | 0.0 | 411.96 |
| 16:12:24 | 1661 | 0.0 | 411.96 |
| 16:12:25 | 1659 | 0.0 | 411.96 |
| 16:12:26 | 1657 | 0.0 | 411.96 |
| 16:12:27 | 1656 | 0.0 | 411.96 |
| 16:12:28 | 1654 | 0.0 | 411.96 |
| 16:12:29 | 1653 | 0.0 | 411.96 |
| 16:12:30 | 1652 | 0.0 | 411.96 |
| 16:12:31 | 1650 | 0.0 | 411.96 |
| 16:12:32 | 1649 | 0.0 | 411.96 |
| 16:12:33 | 1648 | 0.0 | 411.96 |
| 16:12:34 | 1646 | 0.0 | 411.96 |
| 16:12:35 | 1645 | 0.0 | 411.96 |
| 16:12:36 | 1645 | 0.0 | 411.96 |
| 16:12:37 | 1644 | 0.0 | 411.96 |
| 16:12:38 | 1644 | 0.0 | 411.96 |
| 16:12:39 | 1643 | 0.0 | 411.96 |
| 16:12:40 | 1643 | 0.0 | 411.96 |
| 16:12:41 | 1643 | 0.0 | 411.96 |
| 16:12:42 | 1643 | 0.0 | 411.96 |
| 16:12:43 | 1642 | 0.0 | 411.96 |
| 16:12:44 | 1642 | 0.0 | 411.96 |
| 16:12:45 | 1642 | 0.0 | 411.96 |
| 16:12:46 | 1642 | 0.0 | 411.96 |
| 16:12:47 | 1642 | 0.0 | 411.96 |
| 16:12:48 | 1642 | 0.0 | 411.96 |
| 16:12:49 | 1642 | 0.0 | 411.96 |
| 16:12:50 | 1642 | 0.0 | 411.96 |
| 16:12:51 | 1642 | 0.0 | 411.96 |
| 16:12:52 | 1642 | 0.0 | 411.96 |
| 16:12:53 | 1642 | 0.0 | 411.96 |
| 16:12:54 | 1643 | 0.0 | 411.96 |
| 16:12:55 | 1643 | 0.0 | 411.96 |
| 16:12:56 | 1643 | 0.0 | 411.96 |
| 16:12:57 | 1643 | 0.0 | 411.96 |
| 16:12:58 | 1643 | 0.0 | 411.96 |
| 16:12:59 | 1643 | 0.0 | 411.96 |
| 16:13:00 | 1643 | 0.0 | 411.96 |
| 16:13:01 | 1643 | 0.0 | 411.96 |
| 16:13:02 | 1643 | 0.0 | 411.96 |
| 16:13:03 | 1643 | 0.0 | 411.96 |
| 16:13:04 | 1643 | 0.0 | 411.96 |
| 16:13:05 | 1643 | 0.0 | 411.96 |
| 16:13:06 | 1643 | 0.0 | 411.96 |
| 16:13:07 | 1643 | 0.0 | 411.96 |
| 16:13:08 | 1643 | 0.0 | 411.96 |

COPY

Form 3160-5
(April 2004)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004-0137
Expires: March 31, 2007

## SUNDRY NOTICES AND REPORTS ON WELLS

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE- Other instructions on reverse side.***

1. Type of Well: ☐ Oil Well ☑ Gas Well ☐ Other

2. Name of Operator: **BILL BARRETT CORPORATION**

3a. Address: **1099 18th Street Suite 2300 Denver CO 80202**

3b. Phone No. *(include area code)*: **303 312-8134**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*: **SWSW, 1271' FSL, 483' FWL, Section 24-T12S-R14E S.L.B.&M.**

5. Lease Serial No.: **UTU-77513**

6. If Indian, Allottee or Tribe Name: **n/a**

7. If Unit or CA/Agreement, Name and/or No.: **Prickly Pear / UTU-79487**

8. Well Name and No.: **Prickly Pear Unit Fed 12-24**

9. API Well No.: **43-007-30953**

10. Field and Pool, or Exploratory Area:

11. County or Parish, State: **Carbon County, Utah**

12. CHECK APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☑ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production (Start/Resume) | ☐ Water Shut-Off |
| ☐ Subsequent Report | ☐ Alter Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☐ Final Abandonment Notice | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☑ Other **Request to Perf the Wasatch** |
| | ☐ Change Plans | ☐ Plug and Abandon | ☐ Temporarily Abandon | |
| | ☐ Convert to Injection | ☐ Plug Back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be performed or provide the Bond No. on file with BLM/BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notices shall be filed only after all requirements, including reclamation, have been completed, and the operator has determined that the site is ready for final inspection.)

**Conditional approvals have been received from the BLM and the State of Utah, Division of Oil, Gas and Mining to convert this well to a water disposal well . Upon intial testing of the existing perf'd intervals (with poor disposal results) and after further review of the logs for this well, we would like to request to perf the Middle Wasatch following the attached procedure to conduct further disposal testing. Upon completion of the new perfs, BBC would conduct a step-rate test and file for an amended UIC permit.**

**If you should have any questions or need additional information, please contact me at 303-312-8134.**

COPY SENT TO OPERATOR
Date: 8.4.2008
Initials: KS

RECEIVED
JUL 18 2008
DIV. OF OIL, GAS & MINING

14. I hereby certify that the foregoing is true and correct
Name *(Printed/Typed)*: **Tracey Fallang** Title **Environmental/Regulatory Analyst**

Signature: Tracy Fallang Date **07/16/2008**

**THIS SPACE FOR FEDERAL OR STATE OFFICE USE**

Approved by: BRADLEY G. HILL Title ENVIRONMENTAL MANAGER Date 08-04-08

Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. Office

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

*(Instructions on page 2)*

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

**June 23, 2008**

**AFE #** **W.I. 100.0000%**

Surface Casing: 9.625", 36.00#, J-55, ST&C Set @ 1,002'

Production Casing: 5.50", 17.00#, L-80, LT&C Set @9,491'
Float collar @ 9,447'.
Cemented with 1850 sks 50/50 POZ
**Drift I.D. = 4.767". Collapse = 6,290 psi. Burst = 7,740 psi.**
**Capacity = 0.0232 BBL/Linear Ft.**

TOC: 820'

CBP @ 8,595'. CFP @ 7,675".

Bit, bit sub and partial joint of tubing twisted off while drilling up CFP.
**Top of fish @ 7,665'**

CIBP @ 7,655' with 2 sx cement on top. PBTD @ 7,648'.

| Perforations: | | | |
|---|---|---|---|
| | Price River | 7,620-7,630' | 3 JSPF |
| | Dark Canyon | 7,258-7,266' | 3 JSPF |
| | North Horn | 6,908-6,916' | 4 JSPF |
| | | 6,791-6,799' | 3 JSPF |
| | | 6,295-6,300' | 3 JSPF |

Packer: Halliburton "PLS" @ 6215'
2 3/8", 4.7#, N-80, EUE 8RD to 6,215'

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

## Workover Procedure

01 MIRU workover tools.
02 Blow down well and kill with filtered production water if needed.
03 ND tree and NU BOPs.
04 Release packer and TOOH with tubing.
05 RU E-Line and set CBP @ +/- 4,700'. Perforate interval #1 on attached table with 3 3/8" expendable guns loaded with OWEN "HERO" charges 6 JSPF @ 60° phasing. Frac interval with small frac as per Halliburton recommendation.
06 Set CFP and continue to perf and frac intervals on attached sheet.
07 Flow well to clean up.
08 PU bit and TIH with tubing. Drill out CFPs and clean out to PBTD @ 7,648'.
09 TOOH and LD bit.
10 PU Halliburton "PLS packer and TIH. Circulate annulus with packer fluid and space out tubing. Set packer @ +/- 3,400'.
11 ND BOPs and NU tree.
12 Perform MIT on casing, tubing and packer by pressure testing to 1,500 psi with DOGM witness* present.
13 RDMO workover tools.
14 Conduct step-rate test and forward information with modified UIC permit to Division Oil, Gas, and Mining and BLM.

**Bill Barrett Corporation**

**PRICKLY PEAR 12-24**
Surface Location: SWSW 24-T12S-R15E 1,271' FSL & 483' FWL
Bottom Hole Location:
API No. 43-007-30953

**TOC @ 780'**

| STAGE | FORMATION | TOP PEFORATION | BOTTOM PERFORATION | GUN LENGTH | SHOT DENSITY |
|---|---|---|---|---|---|
| 1 | Middle Wasatch | 4500 ' | 4518 ' | 18 ' | 6 JSPF @ 60° |
| 2 | Middle Wasatch | 4260 ' | 4290 ' | 30 ' | 6 JSPF @ 60° |
| 3 | Middle Wasatch | 4058 ' | 4068 ' | 10 ' | 6 JSPF @ 60° |
| | | 4038 ' | 4048 ' | 10 ' | 6 JSPF @ 60° |
| | | 4018 ' | 4028 ' | 10 ' | 6 JSPF @ 60° |
| | | 3976 ' | 3996 ' | 20 ' | 6 JSPF @ 60° |
| | | 3946 ' | 3964 ' | 18 ' | 6 JSPF @ 60° |
| 4 | Middle Wasatch | 3875 ' | 3890 ' | 15 ' | 6 JSPF @ 60° |
| | | 3838 ' | 3858 ' | 20 ' | 6 JSPF @ 60° |
| 5 | Middle Wasatch | 3798 ' | 3804 ' | 6 ' | 6 JSPF @ 60° |
| | | 3768 ' | 3776 ' | 8 ' | 6 JSPF @ 60° |
| | | 3750 ' | 3755 ' | 5 ' | 6 JSPF @ 60° |
| 6 | Middle Wasatch | 3644 ' | 3662 ' | 18 ' | 6 JSPF @ 60° |
| | | 3616 ' | 3620 ' | 4 ' | 6 JSPF @ 60° |
| | | 3606 ' | 3610 ' | 4 ' | 6 JSPF @ 60° |
| | | 3596 ' | 3600 ' | 4 ' | 6 JSPF @ 60° |
| | | 3586 ' | 3590 ' | 4 ' | 6 JSPF @ 60° |
| | | 3554 ' | 3558 ' | 4 ' | 6 JSPF @ 60° |
| | | 3544 ' | 3548 ' | 4 ' | 6 JSPF @ 60° |
| | | 3501 ' | 3505 ' | 4 ' | 6 JSPF @ 60° |
| | | 3492 ' | 3496 ' | 4 ' | 6 JSPF @ 60° |
| | | 3482 ' | 3486 ' | 4 ' | 6 JSPF @ 60° |
| | | | | | |

**** Correlated to Halliburton Dual-Spaced Neutron/Spectral Density log dated 09/26/04.**

**From:** Tracey Fallang <tfallang@billbarrettcorp.com>
**To:** Chris Kierst <chriskierst@utah.gov>
**Date:** 08/21/2008 4:24 PM
**Subject:** FW: Prickly Pear 12-24 step rate test
**Attachments:** BILL BARRETT==PRICKLY PEAR 12-24.xls

---

From: John Shepard
Sent: Thursday, March 27, 2008 2:12 PM
To: Tracey Fallang
Subject: FW: Prickly Pear 12-24 step rate test

Charts and data from the step-rate test.

---

From: Donald Kundert [mailto:Donald.Kundert@Halliburton.com]
Sent: Thursday, March 27, 2008 2:00 PM
To: John Shepard
Subject: Prickly Pear 12-24 step rate test

Pat Kundert
Halliburton - Denver
Office 303-312-8188
Cell 303-886-0839
email:donald.kundert@halliburton.com

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

**October 24, 2008**

| | | |
|---|---|---|
| **AFE #** | **W.I. 100.0000%** | |
| Surface Casing: | 9.625", 36.00#, J-55, ST&C | Set @ 1,002' |
| Production Casing: | 5.50", 17.00#, L-80, LT&C<br>Float collar @ 9,447'.<br>Cemented with 1850 sks 50/50 POZ<br>**Drift I.D. = 4.767". Collapse = 6,290 psi. Burst = 7,740 psi.**<br>**Capacity = 0.0232 BBL/Linear Ft.** | Set @9,491' |
| TOC: | 820' | |
| CBP @ 8,595'. | CFP @ 7,675". | |

Bit, bit sub and partial joint of tubing twisted off while drilling up CFP.
**Top of fish @ 7,665'**

CIBP @ 7,655' with 2 sx cement on top. PBTD @ 7,648'.

| | |
|---|---|
| Tubing: | 2 3/8", 4.7#, N-80, EUE 8RD to 3,400'. |
| Packer: | Halliburton "PLS" @ 3,400'. |

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

| | | | |
|---|---|---|---|
| **Perforations:** | Price River | 7,620-7,630' | 3 JSPF |
| | Dark Canyon | 7,258-7,266' | 3 JSPF |
| | North Horn | 6,908-6,916' | 4 JSPF |
| | | 6,791-6,799' | 3 JSPF |
| | | 6,295-6,300' | 3 JSPF |
| | Wasatch | 4,500-4,518' | 6 JSPF |
| | | 4,260-4,290' | 6 JSPF |
| | | 4,058-4,068' | 6 JSPF |
| | | 4,038-4,048' | 6 JSPF |
| | | 4,018-4,028' | 6 JSPF |
| | | 3,976-3,996' | 6 JSPF |
| | | 3,946-3,964' | 6 JSPF |
| | | 3,875-3,890' | 6 JSPF |
| | | 3,838-3,858' | 6 JSPF |
| | | 3,798-3,804' | 6 JSPF |
| | | 3,768-3,776' | 6 JSPF |
| | | 3,750-3,755' | 6 JSPF |
| | | 3,644-3,662' | 6 JSPF |
| | | 3,616-3,620' | 6 JSPF |
| | | 3,606-3,310' | 6 JSPF |
| | | 3,596-3,600' | 6 JSPF |
| | | 3,586-3,590' | 6 JSPF |
| | | 3,554-3,558' | 6 JSPF |
| | | 3,544-3,548' | 6 JSPF |
| | | 3,501-3,505' | 6 JSPF |
| | | 3,492-3,496' | 6 JSPF |
| | | 3,482-3,486' | 6 JSPF |

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

Bill Barrett Corporation has completed perforating and fracing 6 stages in the Wasatch interval on the Prickly Pear 12-24 well from 4,518' to 3,482'. Enclosed are the treatment summary sheets and the treating pressure graphs from CalFrac for each stage. After drilling out the composite frac plugs, a Halliburton "PLS" packer was run on 2.375", 4.7#, N-80, EUE 8rd tubing and set at 3,400' leaving the Price River, Dark Canyon, North Horn and Wasatch intervals open for water disposal. The tubing, packer and casing were pressure tested to 1,500 psi and the chart for the MIT is enclosed.

On each of the six stages, BBC shut down pumping after seeing an initial breakdown and recorded the instant shutdown pressure (ISIP) for each stage. BBC also recorded the final ISIP at the end of each stage. The initial and the final ISIPs along with their corresponding frac gradients are shown in the enclosed "**Prickly Pear 12-24 Disposal Well**" graph. After plotting the frac gradients for each stage, the initial ISIP on stage 2 and both the initial and final ISIPs on stages 3 and 4 appear to be abnormally low compared to the other stages. BBC then looked at the frac gradients for the Wasatch intervals on the offsetting Prickly Pear 13-17D-12-15 pad and found the following results:

| Well Name | Stage | Final Gradient psi/ft |
|---|---|---|
| Prickly Pear 12-17D | 12 | 0.960 |
| | 13 | 0.960 |
| | 14 | 0.980 |
| | 15 | 1.020 |
| | 16 | 1.080 |
| Prickly Pear 13-17D | 11 | 0.970 |
| | 12 | 0.980 |
| | 13 | 0.960 |
| Prickly Pear 14-17D | 07 | 0.920 |
| | 08 | 1.050 |
| Prickly Pear 16-18D | 10 | 1.030 |
| | 11 | 1.110 |
| | 12 | 1.210 |

The gradients on the offset wells are very similar to the final gradients on stages 1, 2, 5 and 6 of the Prickly Pear 12-24 well and would further indicate that the frac gradients seen on stages 3 and 4 may not be right.

The Wasatch interval in the Prickly Pear area is an under-pressured reservoir with a pore pressure gradient of approximately 0.38 psi/ft. BBC fraced the Wasatch intervals with a water based fluid with a hydrostatic gradient of approximately 0.44 psi/ft. Stages 3 and 4 both appear to have very high permeability as seen in the high leak-off rate after final shut-down. The shut in casing pressure on stage 3 bled off to 0 psi in 11 minutes and on stage 4 bled off to 0 psi in 3 minutes. BBC believes the high leak-off rate in these two intervals may be a factor causing us to see lower ISIPs in these two intervals than what we would expect to see. BBC would contend that in these two intervals, we either (a.) were not pumping enough rate to overcome the leak-off into the formation and did not generate a significant fracture in the formation or (b.) as we started to step down rate at the end of the jobs, the leak-off was higher than the pump rate and the fractures closed before we got to the final shutdown.

After the packer was run and the MIT was performed, BBC set up two 500 bbl frac tanks and filled them with produced water from the Prickly Pear wells. BBC injected the 1,000 bbls of produced water into the Prickly Pear well to test the viability of the newly completed interval for injection and to try to get a step-rate test to establish a maximum surface injection pressure. The water was injected at 2,700 bbl/day with 0 psi surface injection pressure. The tubing went on a vacuum immediately after shut down further confirming the high permeability in some of the Wasatch intervals. Because the Prickly Pear 12-24 well took water at 0 psi surface injection pressure, BBC was not able to obtain a step-rate test and requests that the maximum allowable surface injection pressure be determined from the frac gradients recorded on the six Wasatch fracs.

The **"Prickly Pear 12-24 Disposal Well"** graph shows the Initial and Final Gradient trendlines for the six Wasatch fracs and show an initial frac gradient of approximately 0.68 psi/ft and a final frac gradient of approximately 0.88 psi/ft. The trendlines include data from stages 3 and 4 which BBC believes are too low as we normally don't see sections within an interval that have significantly lower frac gradients than the sections above and below them. BBC would propose to use the average of the Initial and Final trendlines or 0.78 psi/ft as the starting point for maximum allowable injection pressure on the Prickly Pear 12-24 disposal well. BBC believes that the actual frac gradient in this interval is closer to 0.95 to 1.0 psi/ft and is supported by the Final frac gradients on stages 1, 2, 5 and 6 as well as on the offset wells, so using 0.78 psi/ft as a starting point will allow a significant margin for error.

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

Using the following formula, ***maximum surface injection pressure = (frac gradient – hydrostatic gradient of injected water) x depth of top interval***, and a frac gradient of 0.78 psi/ ft, maximum surface injection pressure = (0.78 psi/ft - 0.433 psi/ft) x 3500' = 1,215 psi. BBC would propose setting the initial maximum allowable surface injection pressure at **1,200 psi** with a rate of **3,000 bbl/day** on the **Prickly Pear 12-24-12-14 Disposal Well.** After BBC has been injecting into this well for a period of time, we would expect the reservoir pressure to increase along with the surface injection pressure. If the surface injection pressure starts to approach the maximum allowable pressure, BBC would perform a step-rate test on the well and submit a request for a change in maximum allowable surface treating pressure based on the results of the step-rate test.

= revisions

Form 3160-4
(April 2004)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

**BBC CONFIDENTIAL**

FORM APPROVED
OMB NO. 1004-0137
Expires: March 31, 2007

# WELL COMPLETION OR RECOMPLETION REPORT AND LOG

5. Lease Serial No. **UTU 77513**

1a. Type of Well ☐ Oil Well ☑ Gas Well ☐ Dry ☐ Other
b. Type of Completion: ☑ New Well ☐ Work Over ☐ Deepen ☐ Plug Back ☐ Diff. Resvr.,
Other

6. If Indian, Allottee or Tribe Name

7. Unit or CA Agreement Name and No. **Prickly Pear Unit**

2. Name of Operator **BILL BARRETT CORPORATION**

8. Lease Name and Well No. **Prickly Pear Unit Fed 12-24**

3. Address **1099 18th Street, Suite 2300, Denver, CO 80202**

3a. Phone No. *(include area code)* **303-312-8168**

9. AFI Well No. **4300730953**

4. Location of Well *(Report location clearly and in accordance with Federal requirements)**

At surface **SWSW, 1271' FSL, 483' FWL**

At top prod. interval reported below **same**

At total depth **same**

10. Field and Pool, or Exploratory **Prickly Pear**

11. Sec., T., R., M., on Block and Survey or Area **24-T12S-R14E**

12. County or Parish **Carbon** 13. State **UT**

| 14. Date Spudded | 15. Date T.D. Reached | 16. Date Completed | 17. Elevations (DF, RKB, RT, GL)* |
|---|---|---|---|
| 09/03/2004 | 09/26/2004 | ☐ D & A ☑ Ready to Prod. 11/18/2004 | 7795' |

| 18. Total Depth: | 19. Plug Back T.D.: | 20. Depth Bridge Plug Set: |
|---|---|---|
| MD 9496' | MD 7648' | MD 8595' |
| TVD 9496' | TVD 7648' | TVD 8595' |

21. Type Electric & Other Mechanical Logs Run (Submit copy of each)
**TRPL COMBO (GR/DSN/SDL AND HRI), DIPOLE SONIC & CBL/GR/CCL**

22. Was well cored? ☑ No ☐ Yes (Submit analysis)
Was DST run? ☑ No ☐ Yes (Submit report)
Directional Survey? ☑ No ☐ Yes (Submit copy)

23. Casing and Liner Record *(Report all strings set in well)*

| Hole Size | Size/Grade | Wt. (#/ft.) | Top (MD) | Bottom (MD) | Stage Cementer Depth | No. of Sks. & Type of Cement | Slurry Vol. (BBL) | Cement Top* | Amount Pulled |
|---|---|---|---|---|---|---|---|---|---|
| 12-1/4" | 95/8 J-55 | 36 | 0 | 1002 | | 225 HLP | 74 | Surf (CIR) | None |
| | | | | | | 190 Premag | 39 | | |
| 7-7/8" | 51/2 L80 | 17 | 0 | 9491 | | 1850 5050Poz | 491 | 740 (CBL) | None |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

24. Tubing Record

| Size | Depth Set (MD) | Packer Depth (MD) | Size | Depth Set (MD) | Packer Depth (MD) | Size | Depth Set (MD) | Packer Depth (MD) |
|---|---|---|---|---|---|---|---|---|
| 2 3/8" | 3400' | | | | | | | |

25. Producing Intervals / 26. Perforation Record

| Formation | Top | Bottom | Perforated Interval | Size | No. Holes | Perf. Status |
|---|---|---|---|---|---|---|
| A) Mesaverde | 7258' | 7630' | 9242' - 9279' | 0.41" | 24 | Closed |
| B) North Horn | 4500' | 6916' | 8620' - 8699' | 0.41" | 24 | Closed |
| C) | | | 8460' - 8572' | 0.41" | 36 | Closed |
| D) | | | 8327' - 8379' | 0.41" | 24 | Closed |

27. Acid, Fracture, Treatment, Cement Squeeze, etc.

| Depth Interval | Amount and Type of Material |
|---|---|
| 9242' - 9279' | 30# Purgel III LT 70Q CO2 foam frac: 110 tons of CO2, 58,000# 20/40 White Sand, 207 bbls |
| 8620' - 8699' | 30# Purgel III LT 70Q CO2 foam frac: 141 tons of CO2, 102,000# 20/40 White Sand, 321 bbls |
| 8460' - 8572' | 30# Purgel III LT 70Q CO2 foam frac: 105 tons of CO2, 45,600# 20/40 White Sand, 260 bbls |
| 8327' - 8379' | 30# Purgel III LT 70Q CO2 foam frac: 70 tons of CO2, 27,000# 20/40 White Sand, 223 bbls |

28. Production - Interval A

| Date First Produced | Test Date | Hours Tested | Test Production | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| 11/05/2004 | 11/21/2004 | 24 | → | 0 | 280 | 63 | | | Flowing |
| **Choke Size** | **Tbg. Press. Flwg. SI** | **Csg. Press.** | **24 Hr. Rate** | **Oil BBL** | **Gas MCF** | **Water BBL** | **Gas/Oil Ratio** | **Well Status** | |
| 32/64 | SI 75 | 350 | → | 0 | 280 | 63 | | Open | |

28a. Production - Interval B

| Date First Produced | Test Date | Hours Tested | Test Production | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| | | | → | | | | | | |
| **Choke Size** | **Tbg. Press. Flwg. SI** | **Csg. Press.** | **24 Hr. Rate** | **Oil BBL** | **Gas MCF** | **Water BBL** | **Gas/Oil Ratio** | **Well Status** | |
| | | | → | | | | | | |

*(See instructions and spaces for additional data on page 2)*

28b. Production - Interval C

| Date First Produced | Test Date | Hours Tested | Test Production → | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | |

| Choke Size | Tbg. Press. Flwg. SI | Csg. Press. | 24 Hr. Rate → | Oil BBL | Gas MCF | Water BBL | Gas/Oil Ratio | Well Status |
|---|---|---|---|---|---|---|---|---|
| | | | | | | | | |

28c. Production - Interval D

| Date First Produced | Test Date | Hours Tested | Test Production → | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | |

| Choke Size | Tbg. Press. Flwg. SI | Csg. Press. | 24 Hr. Rate → | Oil BBL | Gas MCF | Water BBL | Gas/Oil Ratio | Well Status |
|---|---|---|---|---|---|---|---|---|
| | | | | | | | | |

29. Disposition of Gas *(Sold, used for fuel, vented, etc.)*

**Sold**

30. Summary of Porous Zones (Include Aquifers):

Show all important zones of porosity and contents thereof: Cored intervals and all drill-stem tests, including depth interval tested, cushion used, time tool open, flowing and shut-in pressures and recoveries.

31. Formation (Log) Markers

| Formation | Top | Bottom | Descriptions. Contents. etc. | Name | Top Meas. Depth |
|---|---|---|---|---|---|
| | | | | **Green River (marker)** | **2102'** |
| | | | | **Base Resisti** | **2409'** |
| | | | | **Uteland Butte** | **2838'** |
| | | | | **Wasatch** | **3060'** |
| | | | | **Middle Wasatch** | **4088'** |
| | | | | **North Horn** | **5168'** |
| | | | | **Price River** | **6984'** |
| | | | | **Base UPR** | **7268'** |
| | | | | **Bluecastle** | **8288'** |
| | | | | **Sego** | **8582'** |
| | | | | **Castlegate** | **8972'** |
| | | | | **Blackhawk** | **9211'** |

32. Additional remarks (include plugging procedure):

**Copies of logs already submitted. CIBP set at 7655'. This well has been converted to a salt-water disposal well.**

33. Indicate which itmes have been attached by placing a check in the appropriate boxes:

☐ Electrical/Mechanical Logs (1 full set req'd.) ☐ Geologic Report ☐ DST Report ☐ Directional Survey
☐ Sundry Notice for plugging and cement verification ☐ Core Analysis ☐ Other:

34. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records (see attached instructions)*

Name *(please print)* **Tracey Fallang** Title **Regulatory Analyst**

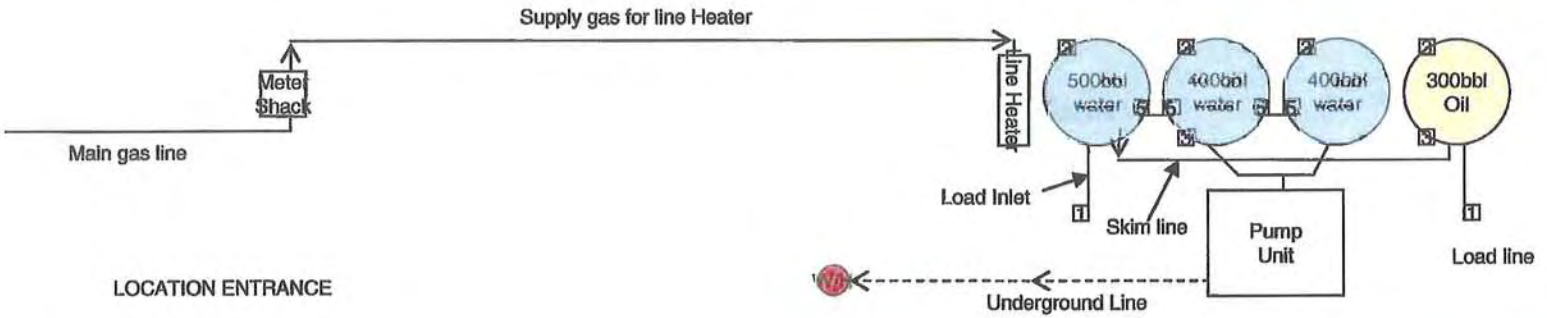
Signature **Tracey Fallang** Digitally signed by Tracey Fallang DN: CN = Tracey Fallang, C = US, O = BEC Date: 2008.11.03 14:01:23 -07'00' Date **11/03/2008** Revised

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

BBC
CONFIDENTIAL

| 27. PERFORATION RECORD (cont.) | | | | |
|---|---|---|---|---|
| INTERVAL (Top/Bot-MD) | | SIZE | NO. HOLES | PERFORATION STATUS |
| 7620' | 7630' | 0.41" | 30 | Open |
| 7258' | 7266' | 0.41" | 24 | Open |
| 6908' | 6916' | 0.41" | 32 | Open (perf only, no frac) |
| 6791' | 6799' | 0.41" | 24 | Open |
| 6295' | 6300' | 0.41" | 15 | Open (perf only, no frac) |
| 4500' | 4518' | 0.43" | 108 | Open |
| 4260' | 4290' | 0.43" | 180 | Open |
| 3946' | 4068' | 0.43" | 408 | Open |
| 3838' | 3890' | 0.43" | 210 | Open |
| 3750' | 3804' | 0.43" | 114 | Open |
| 3482' | 3620' | 0.43" | 216 | Open |

| 28. ACID, FRACTURE, TREATMENT, CEMENT SQUEEZE, ETC. (cont.) | |
|---|---|
| DEPTH INTERVAL | AMOUNT AND TYPE OF MATERIAL |
| 7620' – 7630' | 30# Purgel III LT 70Q CO2 foam frac: 138 tons of CO2, 80,000# 20/40 White Sand, 264 bbls |
| 7258' – 7266' | 30# Purgel III LT 70Q CO2 foam frac: 75 tons of CO2, 22,000# 20/40 White Sand, 176 bbls |
| 6791' – 6799' | 30# Purgel III LT 70Q CO2 foam frac: 122 tons of CO2, 78,000# 20/40 White Sand, 271 bbls |
| 4500' – 4518' | 700 bbls Dyna Flow-1; 18,000# 20/40 White Sand |
| 4260' – 4290' | 621 bbls Dyna Flow-1; 30,000# 20/40 White Sand |
| 3946' – 4068' | 1268 bbls Dyna Flow-1; 68,000# 20/40 White Sand |
| 3838' – 3890' | 615 bbls Dyna Flow-1; 35,279# 20/40 White Sand |
| 3750' – 3804' | 397 bbls Dyna Flow-1; 18,381# 20/40 White Sand |
| 3482' – 3620' | 899 bbls Dyna Flow-1; 54,000# 20/40 White Sand |




Irrigation Ditch/Pond/Stream/
Dry Drainage/Other
43' -feet away (direction indicated w/arrows)

# 12-24 Injection Well

1 - LOAD LINE
3 - DRAIN
5 - LOWER EQUALIZER

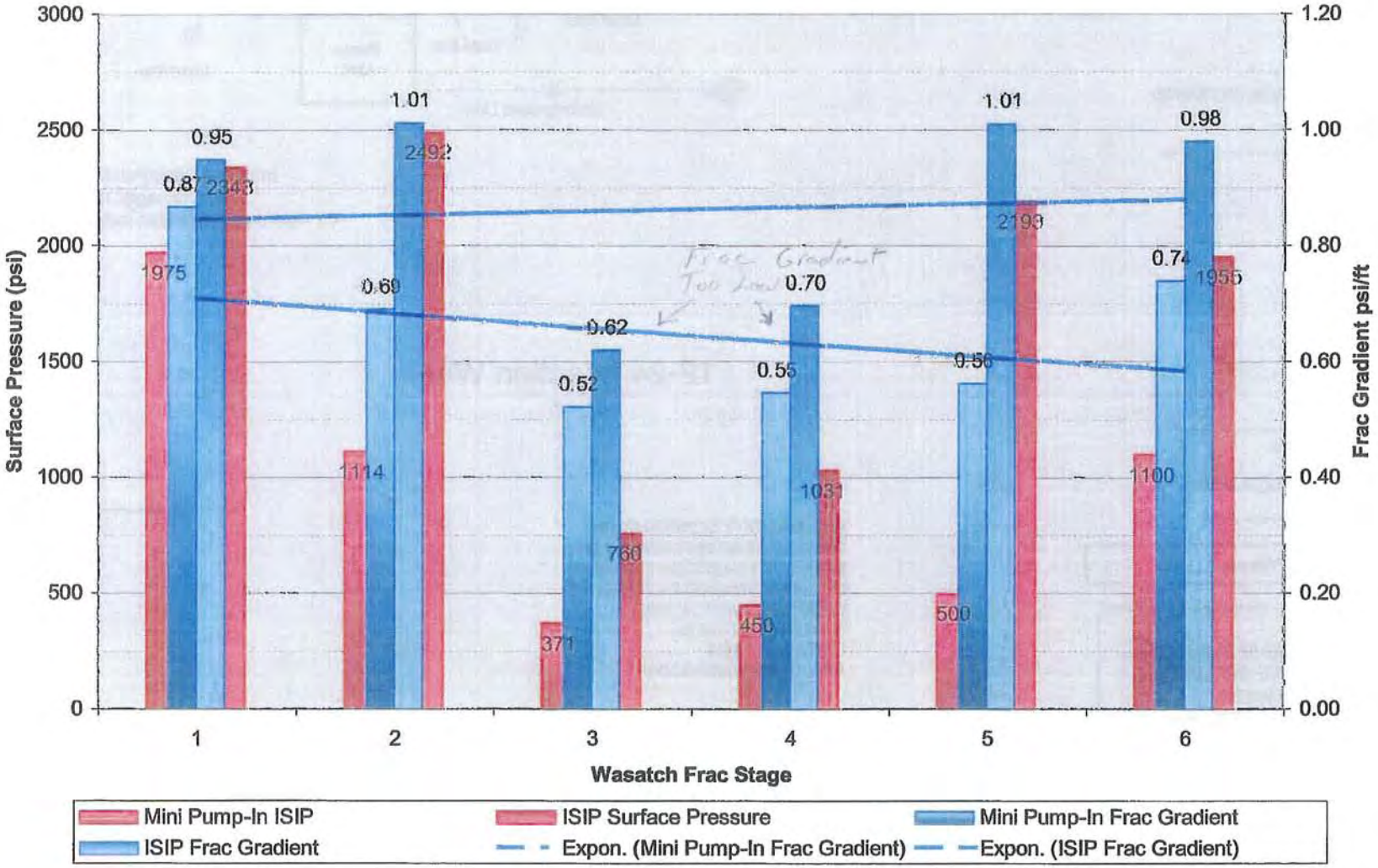
Tank Containment Volume: ___ bbls

NOTE:
THIS LEASE IS SUBJECT TO THE SITE SECURITY PLAN FOR WEST TAVAPUTS. THIS PLAN WILL BE LOCATED AT 1820 WEST HWY 40, ROOSEVELT, UT.

N

**BILL BARRETT CORPORATION**
**PRICKLY PEAR UNIT FED #12-24**
SHL:SW/4SW/4,SEC.24-T12S-R14E
BHL:SW/4SW/4,SEC.24-T12S-R14E
CARBON COUNTY, UTAH
LEASE# UTU-077513
UNIT# UTU-79487
API# 43-007-30953-00-00

## Prickly Pear 12-24 Disposal Well



BILL BARRETT
GRAPHIC CONTROLS CORPORATION
BUFFALO, NEW YORK
CHART NO. MC MP-15000
10-1-08
METER
TAKEN OFF
M
CHART PUT ON
M
LOCATION Prickly Pear
REMARKS 12-24 12-14
Jon Sidwell
B+C
6 PM

CALFRAC WELL SERVICES

# Treatment Summary

## General Info



| | | | |
|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 1), SWSW S24, T12S, R15E | Service Line: | Frac |
| Customer: | John Shepard, P.E. | Job Date: | 09/18/08 |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0188RN |
| | Denver, CO 80202 | Service Order #: | 77813 |

Time Requested: 9:00 AM

Time On: 9:00 AM

Time Off: 4:00 PM

## Wellbore Data

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 4600 | 104.6 |
| Annulus: | | | | | | | |
| | | | | | | Total | 104.6 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

## Perforations

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 4500 | 4518 | 6 |

Formation Treated
Middle Wasatch, (WW)

## Proppant Data

| | | |
|---|---|---|
| Proppant Type | 1 | 20/40 Sand |
| | 2 | |
| | 3 | |
| | 4 | |
| Total sand on location | | 225,660 lb |
| Sand pumped | | 18,000 lb |
| Sand In Formation | | 18,000 lb |
| Final Conc @ Perfs | | 0 lb/gal |

## Pump Power

| | |
|---|---|
| Available | 8000 hhp |
| Used | 1778 hhp |

## Fluid in Tanks

| | |
|---|---|
| Pre-Job | 2446 bbl |
| Post-Job | 1749 bbl |

## Flush Fluid Density

8.34 (lb/gal)

## Treatment Data

| | | |
|---|---|---|
| Max.Treating Rate | 30.2 | bbl/min |
| Max.Treating Pressure | 3176 | psi |
| Pressure Test Lines | 7500 | psi |
| Annular Relief Set | N/A | psi |
| Annulus Pressure | N/A | psi |
| Initial Well Press | 0 | psi |
| Breakdown Press | 3125 | psi |
| Average Pressure | 2411 | psi |
| Average Fluid Rate | 30.1 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 1975 | | | 2343 | psi |
| 1 Min. SIP | | | | 2054 | psi |
| 5 Min. SIP | | | | 1868 | psi |
| 10 Min. SIP | | | | 1787 | psi |
| 15 Min. SIP | | | | 1761 | psi |
| Frac Grad.: | 0.87 | 0.43 | 0.43 | 0.95 | psi/ft |

## Fluid Summary

| | | |
|---|---|---|
| Hole Fill Fluid Vol. | 3.1 | bbl |
| | | bbl |
| | | bbl |
| | | bbl |
| Pad Fluid Vol. | 388.7 | bbl |
| Proppant Fluid Vol. | 206.6 | bbl |
| Flush Fluid Vol. | 104.6 | bbl |
| Total Fluid Pumped | 699.8 | bbl |

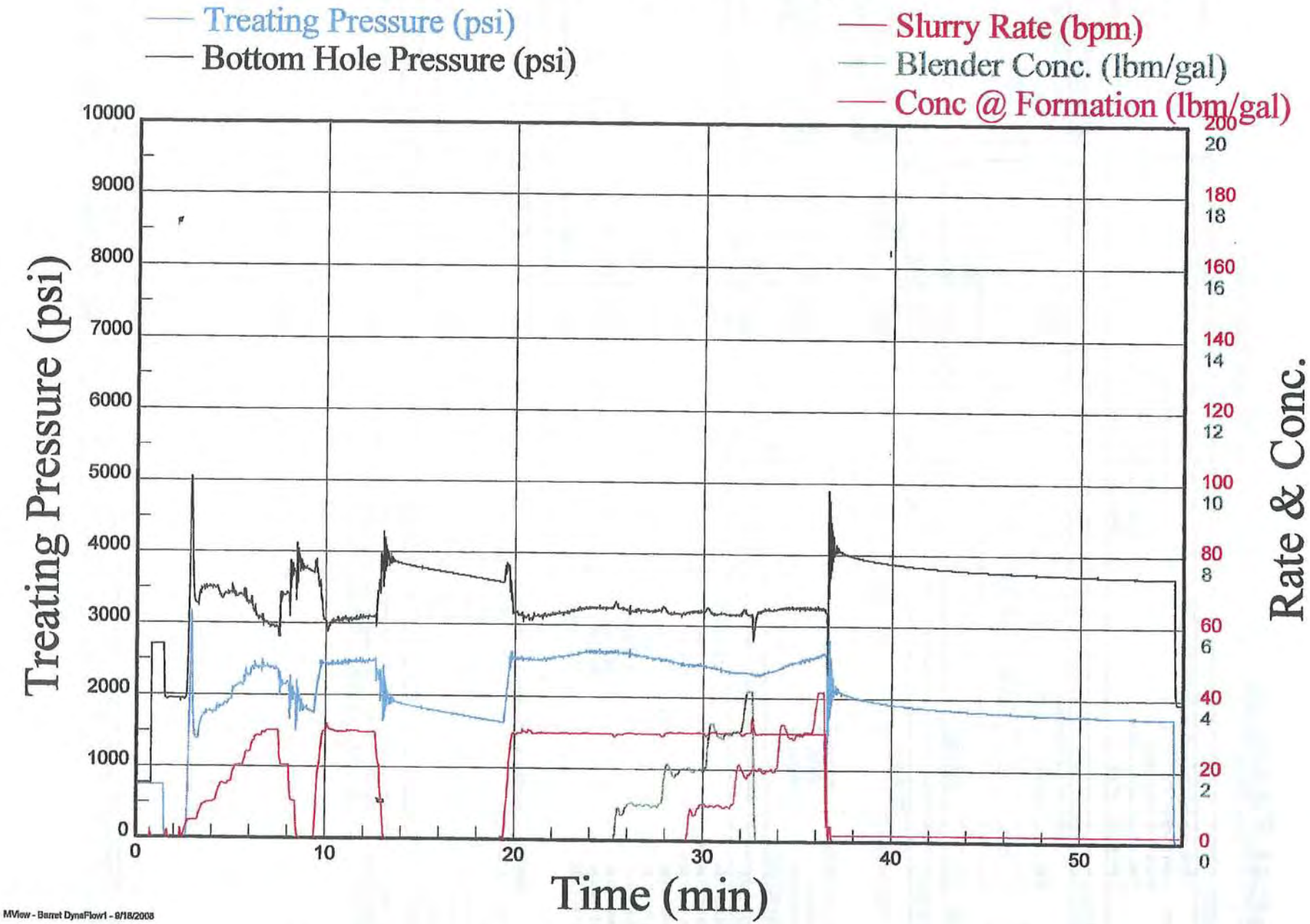
## Chemical Data

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 211 | 12 | 223 |
| DWP-202 | 40 | 10 | 50 |
| DWP-206 | 192 | 12 | 204 |
| DWP-988 | 47 | 0 | 47 |

Remarks: Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #1




MView - Barret DynaFlow1 - 9/18/2008

CALFRAC WELL SERVICES

# Treatment Summary

## General Info



| | | | |
|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 2), SWSW S24, T12S, R15E | Service Line: | Frac |
| Customer: | John Shepard, P.E. | Job Date: | 09/18/08 |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0189RN |
| | Denver, CO 80202 | Service Order #: | 77814 |

Time Requested: 4:00 PM

Time On: 4:00 PM

Time Off: 7:30 PM

## Wellbore Data

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 4260 | 99.0 |
| Annulus: | | | | | | | |
| | | | | | | Total | 99.0 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

## Perforations

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 4260 | 4290 | 6 |

Formation Treated
Middle Wasatch, (WIW)

## Proppant Data

| | | |
|---|---|---|
| Proppant Type | 1 | 20/40 Sand |
| | 2 | |
| | 3 | |
| | 4 | |
| Total sand on location | | 202,660 lb |
| Sand pumped | | 30,000 lb |
| Sand in Formation | | 30,000 lb |
| Final Conc @ Perfs | | 0 lb/gal |

## Pump Power

| | |
|---|---|
| Available | 8000 hhp |
| Used | 1752 hhp |

## Fluid in Tanks

| | |
|---|---|
| Pre-Job | 1749 bbl |
| Post-Job | 1374 bbl |

## Flush Fluid Density

8.34 (lb/gal)

## Treatment Data

| | | |
|---|---|---|
| Max.Treating Rate | 30.2 | bbl/min |
| Max.Treating Pressure | 3356 | psi |
| Pressure Test Lines | 7500 | psi |
| Annular Relief Set | N/A | psi |
| Annulus Pressure | N/A | psi |
| Initial Well Press | 1116 | psi |
| Breakdown Press | 4062 | psi |
| Average Pressure | 2379 | psi |
| Average Fluid Rate | 30.1 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 1114 | | | 2492 | psi |
| 1 Min. SIP | | | | 2257 | psi |
| 5 Min. SIP | | | | 1625 | psi |
| 10 Min. SIP | | | | 1078 | psi |
| 15 Min. SIP | | | | 614 | psi |
| Frac Grad.: | 0.70 | 0.43 | 0.43 | 1.02 | psi/ft |

## Fluid Summary

| | | |
|---|---|---|
| Pad Fluid Vol. | 220.6 | bbl |
| Proppant Fluid Vol. | 301.5 | bbl |
| Flush Fluid Vol. | 99.0 | bbl |
| Total Fluid Pumped | 621.1 | bbl |

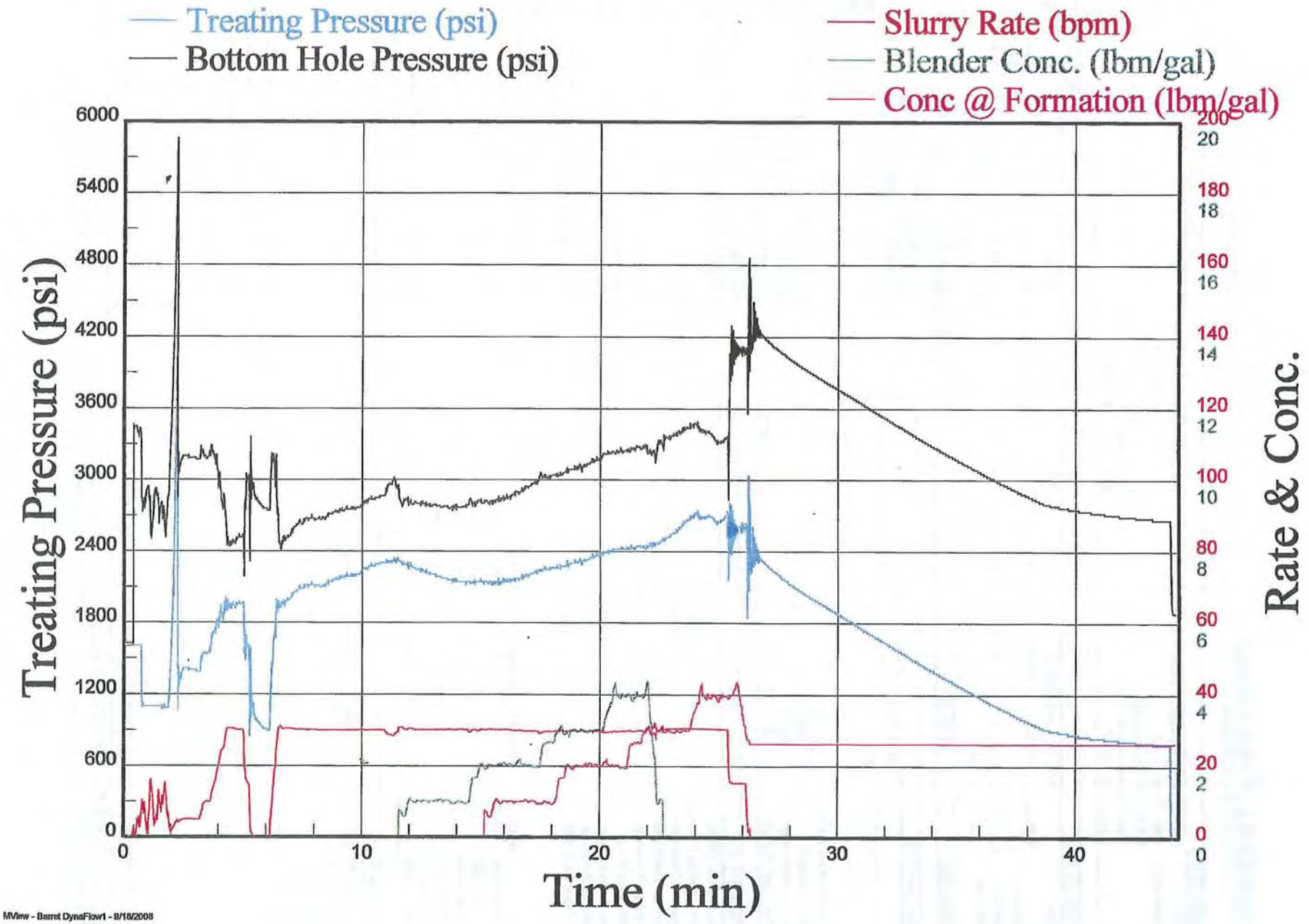
## Chemical Data

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 87 | 0 | 87 |
| DWP-202 | 37 | 0 | 37 |
| DWP-206 | 82 | 0 | 82 |
| DWP-988 | 50 | 0 | 50 |

Remarks: Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #2




MView - Barret DynaFlow1 - 8/18/2008

CALFRAC WELL SERVICES

# Treatment Summary

## General Info



Loc'n: Prickly Pear 12-24 (Stage 3), SWSW S24, T12S, R15E
Customer: John Shepard, P.E.
Bill Barrett Corporation
1099 18th StreetSuite 2300
Denver, CO 80202

Service Line: Frac
Job Date: 09/19/08
Job Type: DynaFlow-1
Program Number: FAYH0190RN
Service Order #: 77815

Time Requested: 6:30 AM
Time On: 6:30 AM
Time Off: 10:00 AM

## Wellbore Data

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 3946 | 91.7 |
| Annulus: | | | | | | | |
| | | | | | | Total | 91.7 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

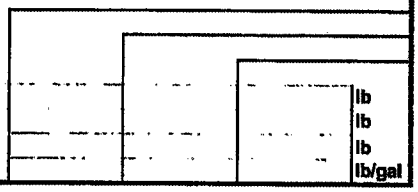
## Perforations

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 3946 | 3964 | 6 |
| 3976 | 3996 | 6 |
| 4018 | 4028 | 6 |
| 4038 | 4048 | 6 |
| 4058 | 4068 | 6 |

Formation Treated
Middle Wasatch, (WIW)

## Proppant Data

| | | |
|---|---|---|
| Proppant Type | 1 | 20/40 Sand |
| | 2 | |
| | 3 | |
| | 4 | |
| Total sand on location | | 174,520 lb |
| Sand pumped | | 88,000 lb |
| Sand in Formation | | 88,000 lb |
| Final Conc @ Perfs | | 0 lb/gal |



## Pump Power

| | |
|---|---|
| Available | 8000 hhp |
| Used | 797 hhp |

## Fluid in Tanks

| | |
|---|---|
| Pre-Job | 2410 bbl |
| Post-Job | 1314 bbl |

## Flush Fluid Density

8.34 (lb/gal)

## Treatment Data

| | | |
|---|---|---|
| Max.Treating Rate | 41 | bbl/min |
| Max.Treating Pressure | 1494 | psi |
| Pressure Test Lines | 75000 | psi |
| Annular Relief Set | N/A | psi |
| Annulus Pressure | N/A | psi |
| Initial Well Press | 0 | psi |
| Breakdown Press | 1864 | psi |
| Average Pressure | 921 | psi |
| Average Fluid Rate | 35.3 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 371 | | | 760 | psi |
| 1 Min. SIP | 0 | | | 624 | psi |
| 5 Min. SIP | | | | 308 | psi |
| 10 Min. SIP | | | | 56 | psi |
| 15 Min. SIP | | | | | psi |
| Frac Grad.: | 0.53 | 0.43 | 0.43 | 0.63 | psi/ft |

## Fluid Summary

| | | |
|---|---|---|
| Hole Fill Fluid Vol. | HF | bbl |
| | | bbl |
| | | bbl |
| | | bbl |
| Pad Fluid Vol. | 540.2 | bbl |
| Proppant Fluid Vol. | 631.6 | bbl |
| Flush Fluid Vol. | 96.0 | bbl |
| Total Fluid Pumped | 1267.8 | bbl |

Ball Sealers: Size 7/8" # 73 Weight 1.3

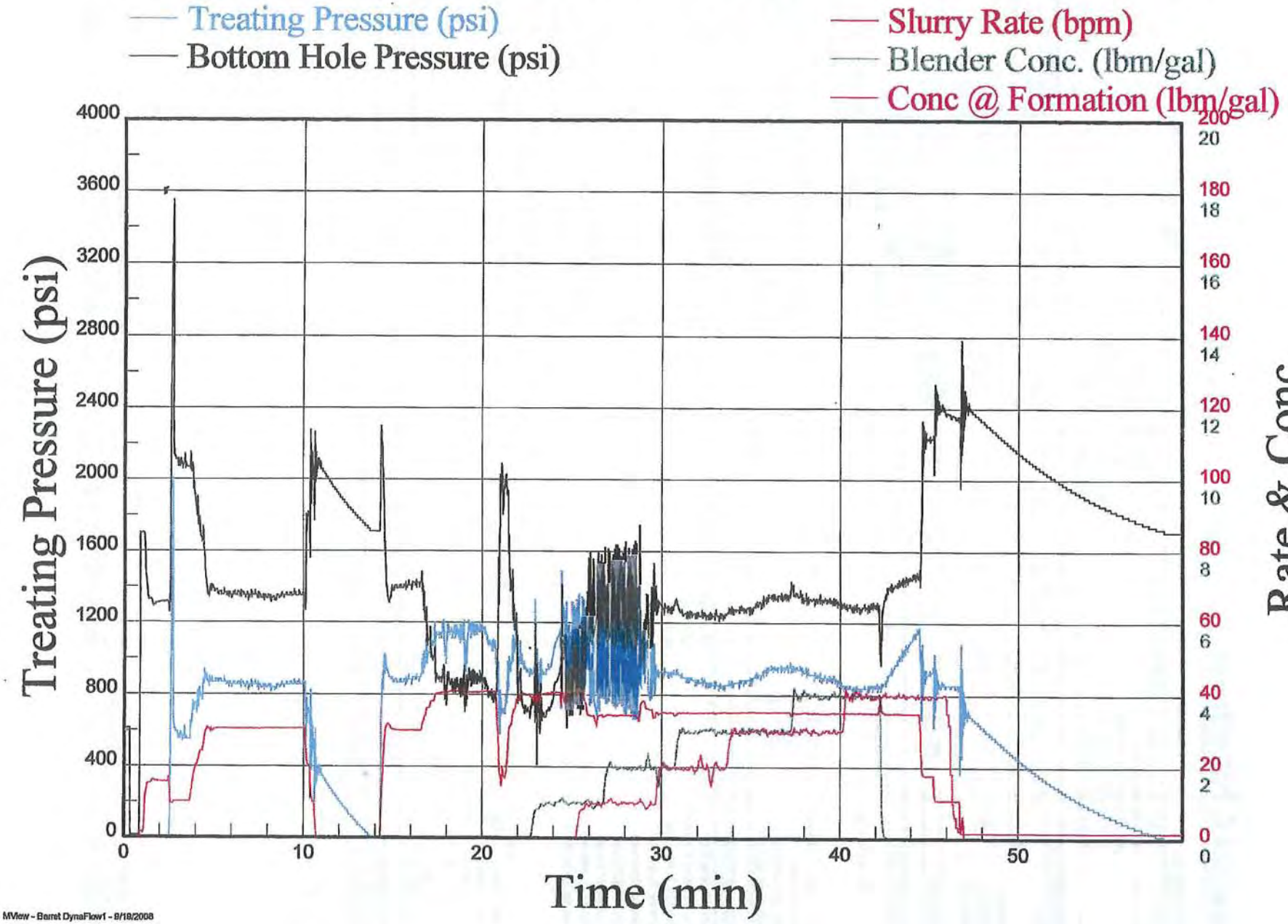
## Chemical Data

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 285 | 7 | 292 |
| DWP-202 | 83 | 4 | 87 |
| DWP-206 | 270 | 10 | 280 |
| DWP-988 | 70 | 0 | 70 |

Remarks: Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ
Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #3




MView - Barret DynaFlow1 - 8/18/2008

CALFRAC WELL SERVICES

# Treatment Summary

**General Info** — Page 1 of 2 — 240

| | | | |
|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 4), SWSW S24, T12S, R15E | Service Line: | Frac |
| Customer: | John Shepard, P.E. | Job Date: | 09/19/08 |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0191RN |
| | Denver, CO 80202 | Service Order #: | 77816 |

Time Requested: 10:00 AM
Time On: 10:00 AM
Time Off: 12:30 PM

**Wellbore Data**

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 3838 | 89.2 |
| Annulus: | | | | | | | |
| | | | | | | Total | 89.2 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

**Perforations**

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 3838 | 3858 | 6 |
| 3875 | 3890 | 6 |

Formation Treated: Middle Wasatch, (WW)

**Proppant Data**

| | 1 | 2 | 3 | 4 | |
|---|---|---|---|---|---|
| Proppant Type | 20/40 Sand | | | | |
| Total sand on location | 109,040 | | | | lb |
| Sand pumped | 35,279 | | | | lb |
| Sand in Formation | 35,279 | | | | lb |
| Final Conc @ Perfs | 0 | | | | lb/gal |

**Pump Power**

| | |
|---|---|
| Available | 8000 hhp |
| Used | 1382 hhp |

**Fluid in Tanks**

| | |
|---|---|
| Pre-Job | 2068 bbl |
| Post-Job | 1669 bbl |

**Flush Fluid Density**: 8.34 (lb/gal)

**Treatment Data**

| | | |
|---|---|---|
| Max.Treating Rate | 40.2 | bbl/min |
| Max.Treating Pressure | 2994 | psi |
| Pressure Test Lines | 7500 | psi |
| Annular Relief Set | N/A | psi |
| Annulus Pressure | N/A | psi |
| Initial Well Press | 0 | psi |
| Breakdown Press | 2924 | psi |
| Average Pressure | 1469 | psi |
| Average Fluid Rate | 38.4 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 450 | | | 1031 | psi |
| 1 Min. SIP | | | | 578 | psi |
| 5 Min. SIP | | | | 0 | psi |
| 10 Min. SIP | | | | | psi |
| 15 Min. SIP | | | | | psi |
| Frac Grad.: | 0.55 | 0.43 | 0.43 | 0.70 | psi/ft |

**Fluid Summary**

| | | |
|---|---|---|
| Hole Fill Fluid Vol. | HF | bbl |
| | | bbl |
| | | bbl |
| | | bbl |
| Pad Fluid Vol. | 190.8 | bbl |
| Proppant Fluid Vol. | 328.9 | bbl |
| Flush Fluid Vol. | 95.2 | bbl |
| Total Fluid Pumped | 614.9 | bbl |

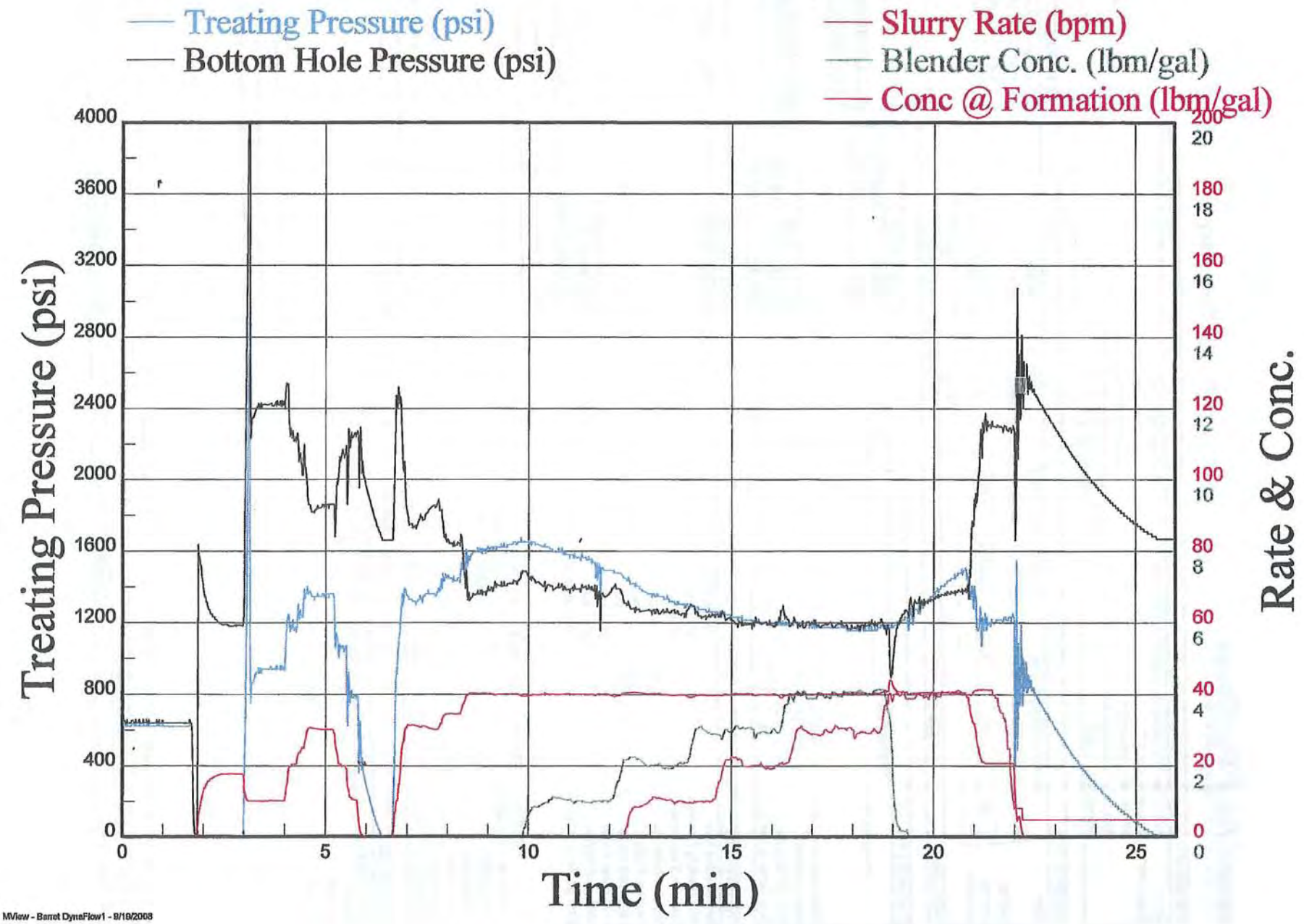
**Chemical Data**

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 124 | 0 | 124 |
| DWP-202 | 38 | 0 | 38 |
| DWP-206 | 114 | 0 | 114 |
| DWP-988 | 50 | 0 | 50 |

Remarks: Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ — Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #4




MView - Barret DynaFlow1 - 8/19/2008

CALFRAC WELL SERVICES

# Treatment Summary

## General Info



| | | | |
|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 5), SWSW S24, T12S, R15E | Service Line: | Frac |
| Customer: | John Shepard, P.E. | Job Date: | 09/19/08 |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0192RN |
| | Denver, CO 80202 | Service Order #: | 77817 |

Time Requested: 12:30 PM
Time On: 12:30 PM
Time Off: 2:30 PM

## Wellbore Data

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 3750 | 87.2 |
| Annulus: | | | | | | | |
| | | | | | | Total | 87.2 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

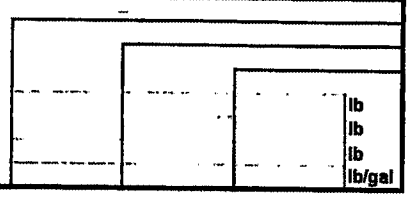
## Perforations

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 3750 | 3755 | 6 |
| 3768 | 3776 | 6 |
| 3798 | 3804 | 6 |

Formation Treated
Middle Wasatch, (WW)

## Proppant Data

| | | |
|---|---|---|
| Proppant Type | 1 | 20/40 Sand |
| | 2 | |
| | 3 | |
| | 4 | |
| Total sand on location | | 73,000 lb |
| Sand pumped | | 18,381 lb |
| Sand in Formation | | 18,381 lb |
| Final Conc @ Perfs | | 0 lb/gal |



## Pump Power

| | |
|---|---|
| Available | 8000 hhp |
| Used | 1027 hhp |

## Fluid in Tanks

| | |
|---|---|
| Pre-Job | 1947 bbl |
| Post-Job | 1560 bbl |

## Flush Fluid Density

8.34 (lb/gal)

## Treatment Data

| | | |
|---|---|---|
| Max.Treating Rate | 30.2 | bbl/min |
| Max.Treating Pressure | 2727 | psi |
| Pressure Test Lines | 7500 | psi |
| Annular Relief Set | N/A | psi |
| Annulus Pressure | N/A | psi |
| Initial Well Press | 0 | psi |
| Breakdown Press | 2116 | psi |
| Average Pressure | 1393 | psi |
| Average Fluid Rate | 30.1 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 600 | | | 2193 | psi |
| 1 Min. SIP | | | | 1819 | psi |
| 5 Min. SIP | | | | 1100 | psi |
| 10 Min. SIP | | | | 281 | psi |
| 15 Min. SIP | | | | 0 | psi |
| Frac Grad.: | 0.57 | 0.43 | 0.43 | 1.02 | psi/ft |

## Fluid Summary

| Hole Fill Fluid Vol. | HF | bbl |
|---|---|---|
| Pad Fluid Vol. | 129.7 | bbl |
| Proppant Fluid Vol. | 171.6 | bbl |
| Flush Fluid Vol. | 96.0 | bbl |
| Total Fluid Pumped | 397.2 | bbl |

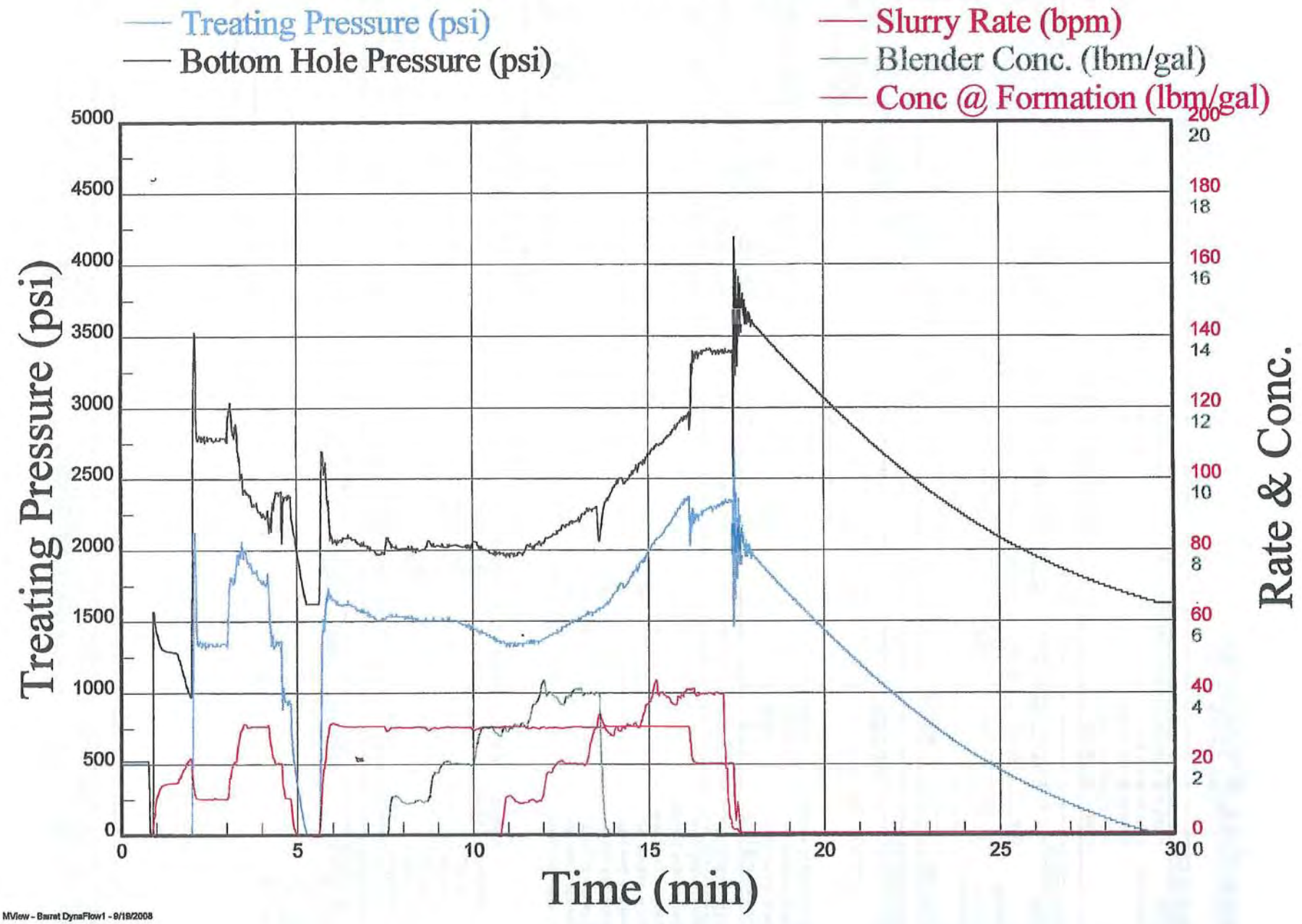
## Chemical Data

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 73 | 0 | 73 |
| DWP-202 | 18 | 0 | 18 |
| DWP-206 | 73 | 0 | 73 |
| DWP-988 | 30 | 0 | 30 |

Remarks: Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #5




MView - Barret DynaFlow1 - 9/19/2008

CALFRAC WELL SERVICES

# Treatment Summary

| General Info | | | Page 1 of 2 | 240 |
|---|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 8), SWSW S24, T12S, R15E | Service Line: | Frac | |
| Customer: | John Shepard, P.E. | Job Date: | 09/19/08 | |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 | |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0193RN | |
| | Denver, CO 80202 | Service Order #: | 77818 | |

Time Requested: 2:30 PM
Time On: 2:30 PM
Time Off: 7:00 PM

**Wellbore Data**

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 3482 | 80.9 |
| Annulus: | | | | | | | |
| | | | | | | Total | 80.9 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

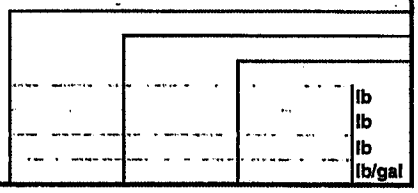
**Perforations**

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 3482 | 3486 | 6 |
| 3492 | 3496 | 6 |
| 3501 | 3505 | 6 |
| 3544 | 3548 | 6 |
| 3554 | 3558 | 6 |
| 3586 | 3590 | 6 |
| 3596 | 3600 | 6 |
| 3606 | 3610 | 6 |
| 3616 | 3620 | 6 |

Formation Treated: Middle Wasatch, (WIW)

**Proppant Data**

| | | |
|---|---|---|
| Proppant Type | 1 | 20/40 Sand |
| | 2 | |
| | 3 | |
| | 4 | |
| Total sand on location | | 54,000 lb |
| Sand pumped | | 54,000 lb |
| Sand In Formation | | 54,000 lb |
| Final Conc @ Perfs | | 0 lb/gal |



**Pump Power**

| | |
|---|---|
| Available | 8000 hhp |
| Used | 1351 hhp |

**Fluid in Tanks**

| | |
|---|---|
| Pre-Job | 1560 bbl |
| Post-Job | 921 bbl |

**Flush Fluid Density**: 8.34 (lb/gal)

**Treatment Data**

| | | |
|---|---|---|
| Max.Treating Rate | 30.1 | bbl/min |
| Max.Treating Pressure | 2611 | psi |
| Pressure Test Lines | 7500 | psi |
| Annular Relief Set | N/A | psi |
| Annulus Pressure | N/A | psi |
| Initial Well Press | 0 | psi |
| Breakdown Press | 2611 | psi |
| Average Pressure | 1837 | psi |
| Average Fluid Rate | 30.0 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 1100 | | | 1955 | psi |
| 1 Min. SIP | | | | 1786 | psi |
| 5 Min. SIP | | | | 1564 | psi |
| 10 Min. SIP | | | | 1258 | psi |
| 15 Min. SIP | | | | 969 | psi |
| Frac Grad.: | 0.75 | 0.43 | 0.43 | 0.99 | psi/ft |

**Fluid Summary**

| Hole Fill Fluid Vol. | HF | bbl |
|---|---|---|
| Pad Fluid Vol. | 262.9 | bbl |
| Proppant Fluid Vol. | 546.5 | bbl |
| Flush Fluid Vol. | 89.2 | bbl |
| Total Fluid Pumped | 898.6 | bbl |

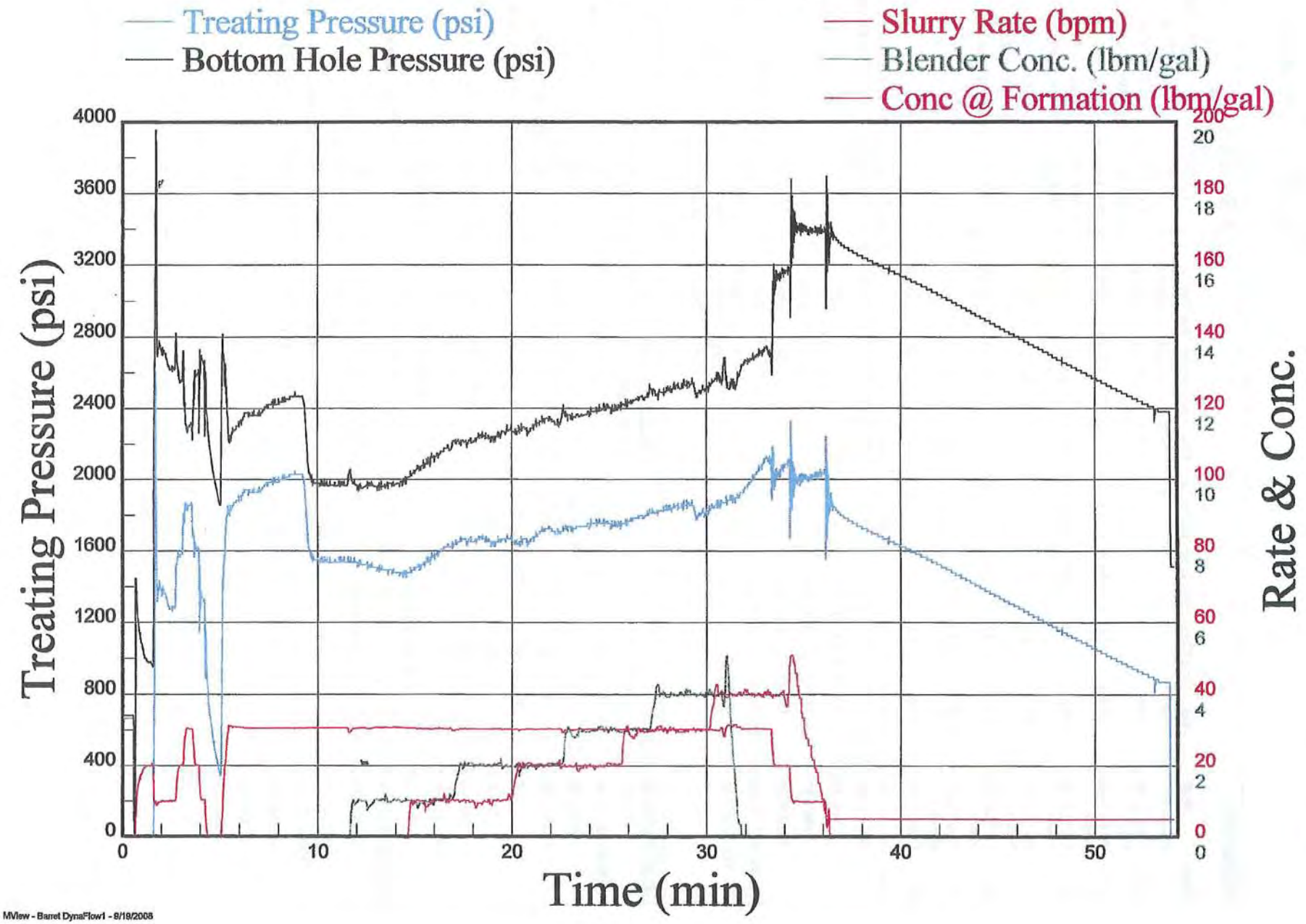
**Chemical Data**

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 131 | 0 | 131 |
| DWP-202 | 64 | 0 | 64 |
| DWP-206 | 139 | 0 | 139 |
| DWP-988 | 60 | 0 | 60 |

Remarks: Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #6




MView - Barret DynaFlow1 - 9/19/2008

| | | | | | |
|---|---|---|---|---|---|
| Tagged E.L. : | 4845.00 | FT : (>6% Porosity) | Casing ID : | 4.000 | Volume to Load Hole |
| | | | | | Pressure Test |
| Top | Bottom | JSPF / Shots / Status | Entrance Size : | | BBC Representative |
| 4808.000 | 4818.000 | 30 | 0.370 | | Russell Evans |
| | | | | | HES Representative |
| | | | | | Pat Butterfield, Technical Professional |

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1279 | 0.0 | 0 | 30.0 | 11.0 | 2994.0 | 2262.0 |
| 2 | CO2 Linear Pad | 1995 | 0.0 | 0 | 48.0 | 10.2 | 2997.0 | 2488.0 |
| 3 | 1# SLF CO2 Foam | 746 | 2.0 | 1425 | 19.0 | 11.0 | 3022.0 | 2985.0 |
| 4 | 2# SLF CO2 Foam | 1625 | 4.0 | 5964 | 45.0 | 11.8 | 2998.0 | 2807.0 |
| 5 | 3# SLF CO2 Foam | 1679 | 5.0 | 8865 | 50.0 | 12.6 | 2885.0 | 2767.0 |
| 6 | 4# SLF CO2 Foam | 2138 | 6.0 | 13746 | 66.0 | 13.2 | 2805.0 | 2713.0 |
| 7 | Overflush (50%) | 1035 | 0.0 | 0 | 25.0 | 10.1 | 2941.0 | 2604.0 |
| 8 | Flush (50%) | 1868 | 0.0 | 0 | 44.0 | 10.1 | 3056.0 | 2333.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 73.00 | 77.28 | -5.50 |
| MA-844 | 35.00 | 24.73 | 41.50 |
| AQF-2 | 40.00 | 41.44 | -3.50 |
| SP Breaker | 10.00 | 9.46 | 0.00 |
| GBW-30 | 5.00 | 6.63 | -24.50 |
| Gyptron T-2 | 101.00 | 110.00 | -8.20 |
| CO2 | 37.00 | 36.50 | 0.00 |
| CO2 | 201.65 | 198.93 | 1.40 |
| CO2 | 8469.30 | 8354.85 | 1.40 |

| | | | |
|---|---|---|---|
| Gel System : | 9218 | Tanks : | 1 |
| Pct Pad : | 38.30 | Avg Prop Conc : | 2.40 |
| Total Fluid : | 12365 | Avg Rate : | 11.4 |
| Total Slurry : | 13722 | Max Rate : | 13.2 |
| Prime-Up & Tnkbot : | 5605 | Min Rate : | 10.1 |
| Total Job Fluid : | 18000 | | |

**Proppant Summary** Total Proppant Pumped : 30000 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 30000 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.45 | | |
| Wellhead Pressure : | 2250 | @ | psi/ft |
| Broke Back : | 2490 | @ 12 | bbl/min |
| Final Injection : | 2700 | @ 10 | bbl/min |
| ISIP : | 2510.0 | @ 0.960 | psi/ft |
| 1 Min ISIP : | | @ | psi/ft |
| 4 Min ISIP : | | @ | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 2084 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 30 | bbl of : Linear Purgel III | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | | @ 0.0000 $/lb | |

**Frac Information**

Fraced well with 250 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 37 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 3022 | psi |
| Min Treat Pressure : | 2262 | psi |
| Avg Treat Pressure : | 2805 | psi |
| After Frac ISDP : | 2510 @ 0.960 | psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 11 | bbl/min |
| Flush Short With : | 44 bbl of Slick Water or | 1868 Gals |
| Total Fluid To Recover : | 325 bbl + | 75 In CSG = 400 |

Tagged E.L. : 4701.00 FT : (>6% Porosity)

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4664.000 | 4674.000 | 3 | 30 | |

Casing ID : 4.000
Entrance Size : 0.370

Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1025 | 0.0 | 0 | 24.0 | 7.0 | 2954.0 | 2184.0 |
| 2 | CO2 Linear Pad | 1973 | 0.0 | 0 | 47.0 | 10.1 | 3018.0 | 2944.0 |
| 3 | 1# SLF CO2 Foam | 747 | 2.0 | 1427 | 19.0 | 10.7 | 3048.0 | 2958.0 |
| 4 | 2# SLF CO2 Foam | 1598 | 4.0 | 5865 | 44.0 | 11.7 | 3038.0 | 2889.0 |
| 5 | 3# SLF CO2 Foam | 1672 | 5.0 | 8828 | 49.0 | 12.4 | 2916.0 | 2791.0 |
| 6 | 4# SLF CO2 Foam | 2237 | 7.0 | 15144 | 70.0 | 13.2 | 2830.0 | 2755.0 |
| 7 | Overflush (50%) | 1033 | 0.0 | 0 | 25.0 | 10.2 | 2894.0 | 2627.0 |
| 8 | Flush (50%) | 1848 | 0.0 | 0 | 44.0 | 10.0 | 2906.0 | 2301.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 62.00 | 75.83 | -18.20 |
| MA-844 | 27.00 | 24.27 | 11.30 |
| AQF-2 | 40.00 | 41.55 | -3.70 |
| SP Breaker | 8.00 | 9.25 | -13.50 |
| GBW-30 | 5.00 | 6.56 | -23.80 |
| Gyptron T-2 | 105.00 | 110.00 | -4.50 |
| CO2 | 37.00 | 35.90 | 3.10 |
| CO2 | 201.65 | 195.66 | 3.10 |
| CO2 | 8469.30 | 8217.51 | 3.10 |

Gel System : 9260 Tanks : 1
Pct Pad : 36.41 Avg Prop Conc : 2.50
Total Fluid : 12133 Avg Rate : 10.8
Total Slurry : 13548 Max Rate : 13.2
Prime-Up & Tnkbot : 5579 Min Rate : 7.0
Total Job Fluid : 18000

**Proppant Summary** Total Proppant Pumped : 31264 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 31264 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.45
Wellhead Pressure : 2184 @ psi/ft
Broke Back : 2790 @ 16 bbl/min
Final Injection : 2670 @ 10 bbl/min
ISIP : 2430.0 @ 0.960 psi/ft
1 Min ISIP : @ psi/ft
4 Min ISIP : @ psi/ft
3 Min Bleed Off :
Final ISIP : 0.0 Final ISIP MIN : 0.000
Permeability & MD-FT : 0.000 MD FT : 0.00
Shale Stress : 0.000 Reservoir Pressure : 2022
Sand Stress : 0.000
Bleed Off Ratio : 0.000
Breakdown Fluid : 24 bbl of : Linear Purgel III
# of Perfs Open : 30
Entry Points : 2
Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 245 bbl of : LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 0 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

Max Treat Pressure : 3048 psi
Min Treat Pressure : 2184 psi
Avg Treat Pressure : 2846 psi
After Frac ISDP : 2430 @ 0.960 psi/ft
Press. Increase During Frac : 0 psi
Avg Rate : 11 bbl/min
Flush Short With : 44 bbl of Slick Water or 1848 Gals
Total Fluid To Recover : 313 bbl + 73 In CSG = 386

Tagged E.L. : 4277.00 FT : (>6% Porosity)

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4122.000 | 4126.000 | 3 | 12 | |
| 4184.000 | 4188.000 | 3 | 12 | |
| 4224.000 | 4228.000 | 3 | 12 | |
| 4246.000 | 4250.000 | 3 | 12 | |

Casing ID : 4.000
Entrance Size : 0.370

Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield. Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 4850 | 0.0 | 0 | 115.0 | 17.4 | 3468.0 | 906.0 |
| 2 | CO2 Linear Pad | 4085 | 0.0 | 0 | 97.0 | 20.4 | 3816.0 | 2895.0 |
| 3 | 1# SLF CO2 Foam | 2344 | 2.0 | 4477 | 61.0 | 21.6 | 3578.0 | 3358.0 |
| 4 | 2# SLF CO2 Foam | 4832 | 4.0 | 17733 | 134.0 | 23.4 | 3518.0 | 3362.0 |
| 5 | 3# SLF CO2 Foam | 5037 | 5.0 | 26595 | 149.0 | 24.9 | 3538.0 | 3438.0 |
| 6 | 4# SLF CO2 Foam | 6116 | 7.0 | 40894 | 190.0 | 26.0 | 3525.0 | 3212.0 |
| 7 | Overflush (50%) | 1044 | 0.0 | 0 | 25.0 | 20.2 | 3547.0 | 3346.0 |
| 8 | Flush (50%) | 1650 | 0.0 | 0 | 39.0 | 20.0 | 3588.0 | 2053.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 197.00 | 203.00 | -3.00 |
| MA-844 | 65.00 | 59.92 | 8.50 |
| AQF-2 | 100.00 | 97.74 | 2.30 |
| SP Breaker | 20.00 | 22.41 | -10.80 |
| GBW-30 | 15.00 | 16.73 | -10.40 |
| Gyptron T-2 | 110.00 | 109.94 | 0.00 |
| CO2 | 71.00 | 75.00 | -5.30 |
| CO2 | 386.95 | 408.75 | -5.30 |
| CO2 | 16251.9( | 7167.50 | -5.30 |

Gel System : 23458 Tanks : 3
Pct Pad : 39.84 Avg Prop Conc : 3.40
Total Fluid : 29958 Avg Rate : 22.0
Total Slurry : 34017 Max Rate : 26.0
Prime-Up & Tnkbot : 7604 Min Rate : 17.4
Total Job Fluid : 38000

**Proppant Summary** Total Proppant Pumped : 89700 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 89700 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.45
Wellhead Pressure : 940 @ psi/ft
Broke Back : 3468 @ 20 bbl/min
Final Injection : 2840 @ 20 bbl/min
ISIP : 2262.0 @ 0.980 psi/ft
1 Min ISIP : @ psi/ft
4 Min ISIP : @ psi/ft
3 Min Bleed Off :
Final ISIP : 0.0 Final ISIP MIN : 0.000
Permeability & MD-FT : 0.000 MD FT : 0.00
Shale Stress : 0.000 Reservoir Pressure : 1813
Sand Stress : 0.000
Bleed Off Ratio : 0.000
Breakdown Fluid : 115 bbl of : Linear Purgel III
# of Perfs Open : 30
Entry Points : 2
Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 674 bbl of : LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 71 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

Max Treat Pressure : 3816 psi
Min Treat Pressure : 906 psi
Avg Treat Pressure : 3251 psi
After Frac ISDP : 2262 @ 0.980 psi/ft
Press. Increase During Frac : 0 psi
Avg Rate : 22 bbl/min
Flush Short With : 39 bbl of Slick Water or 1650 Gals
Total Fluid To Recover : 829 bbl + 66 In CSG = 895

Tagged E.L. : 3930.00 FT : (>6% Porosity)

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 3888.000 | 3903.000 | 3 | 45 | |

Casing ID : 4.000
Entrance Size : 0.370

Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1401 | 0.0 | 0 | 33.0 | 8.7 | 3909.0 | 1308.0 |
| 2 | CO2 Linear Pad | 4452 | 0.0 | 0 | 106.0 | 15.2 | 2914.0 | 1976.0 |
| 3 | 1# SLF CO2 Foam | 1757 | 2.0 | 4199 | 46.0 | 16.4 | 2865.0 | 2778.0 |
| 4 | 2# SLF CO2 Foam | 3908 | 5.0 | 17899 | 112.0 | 17.5 | 2786.0 | 2653.0 |
| 5 | 3# SLF CO2 Foam | 4057 | 7.0 | 26776 | 125.0 | 18.6 | 2765.0 | 26538.0 |
| 6 | 4# SLF CO2 Foam | 4708 | 9.0 | 40489 | 156.0 | 19.5 | 2708.0 | 2587.0 |
| 7 | Overflush (50%) | 1086 | 0.0 | 0 | 26.0 | 15.1 | 2781.0 | 2657.0 |
| 8 | Flush (50%) | 1567 | 0.0 | 0 | 37.0 | 15.0 | 2943.0 | 2204.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 163.00 | 160.55 | 1.50 |
| MA-844 | 45.00 | 45.87 | 0.00 |
| AQF-2 | 82.00 | 83.49 | -1.80 |
| SP Breaker | 20.00 | 20.28 | 0.00 |
| GBW-30 | 15.00 | 14.49 | 0.00 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 63.00 | 66.40 | -5.10 |
| CO2 | 343.35 | 361.88 | -5.10 |
| CO2 | 14420.7( | 5198.96 | -5.10 |

| | | | |
|---|---|---|---|
| Gel System : | 19968 | Tanks : | 2 |
| Pct Pad : | 35.61 | Avg Prop Conc : | 4.00 |
| Total Fluid : | 22936 | Avg Rate : | 15.9 |
| Total Slurry : | 26980 | Max Rate : | 19.5 |
| Prime-Up & Tnkbot : | 6806 | Min Rate : | 8.7 |
| Total Job Fluid : | 30000 | | |

**Proppant Summary** Total Proppant Pumped : 89363 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 89363 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.45 | | |
| Wellhead Pressure : | 1310 | @ | psi/ft |
| Broke Back : | 3909 | @ 15 | bbl/min |
| Final Injection : | 2590 | @ 15 | bbl/min |
| ISIP : | 2280.0 | @ 1.020 | psi/ft |
| 1 Min ISIP : | | @ | psi/ft |
| 4 Min ISIP : | | @ | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 1687 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 33 | bbl of : Linear Purgel III | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | | @ 0.0000 | $/lb |

**Frac Information**

Fraced well with 509 bbl of : LGC 6

| | | | |
|---|---|---|---|
| 0 | Quality N2 | 0 | SCF of nitrogen down hole |
| 70 | Quality CO2 | 63 | tons CO2 |
| | | | Total SCF N2 Pumped |
| | | | Total tons CO2 Pumped |

| | | |
|---|---|---|
| Max Treat Pressure : | 3909 | psi |
| Min Treat Pressure : | 1308 | psi |
| Avg Treat Pressure : | 4373 | psi |
| After Frac ISDP : | 2280 @ 1.020 | psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 16 | bbl/min |
| Flush Short With : | 37 bbl | of Slick Water or 1567 Gals |
| Total Fluid To Recover : | 579 bbl + | 61 In CSG = 641 |

Tagged E.L. : 3634.00 FT : (>6% Porosity)

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 3597.000 | 3607.000 | 3 | 30 | |

Casing ID : 4.000
Entrance Size : 0.370

Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1662 | 0.0 | 0 | 40.0 | 5.8 | 3561.0 | 1608.0 |
| 2 | CO2 Linear Pad | 4491 | 0.0 | 0 | 107.0 | 15.1 | 3156.0 | 2088.0 |
| 3 | 1# SLF CO2 Foam | 1749 | 2.0 | 3341 | 45.0 | 16.1 | 3051.0 | 2991.0 |
| 4 | 2# SLF CO2 Foam | 3880 | 4.0 | 14240 | 108.0 | 17.6 | 3077.0 | 2967.0 |
| 5 | 3# SLF CO2 Foam | 4024 | 5.0 | 21247 | 119.0 | 18.6 | 3165.0 | 2986.0 |
| 6 | 4# SLF CO2 Foam | 5130 | 6.0 | 32273 | 157.0 | 19.6 | 3189.0 | 3112.0 |
| 7 | Overflush (50%) | 231 | 0.0 | 0 | 6.0 | 18.4 | 3194.0 | 2956.0 |
| 8 | Flush (50%) | 1478 | 0.0 | 0 | 35.0 | 15.1 | 3050.0 | 2185.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 138.00 | 141.53 | -2.50 |
| MA-844 | 45.00 | 45.29 | 0.00 |
| AQF-2 | 80.00 | 82.22 | -2.70 |
| SP Breaker | 20.00 | 20.94 | 0.00 |
| GBW-30 | 15.00 | 15.01 | 0.00 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 63.00 | 64.00 | 0.00 |
| CO2 | 343.35 | 348.80 | -1.60 |
| CO2 | 14420.7( | 4649.60 | -1.60 |

Gel System : 19505 Tanks : 2
Pct Pad : 37.33 Avg Prop Conc : 3.30
Total Fluid : 22645 Avg Rate : 15.9
Total Slurry : 25862 Max Rate : 19.6
Prime-Up & Tnkbot : 6773 Min Rate : 5.8
Total Job Fluid : 30000

**Proppant Summary** Total Proppant Pumped : 71100 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 71100 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.45
Wellhead Pressure : 1760 @ psi/ft
Broke Back : 3561 @ 12 bbl/min
Final Injection : 2730 @ 15 bbl/min
ISIP : 2310.0 @ 1.080 psi/ft
1 Min ISIP : @ psi/ft
4 Min ISIP : @ psi/ft
3 Min Bleed Off :
Final ISIP : 0.0 Final ISIP MIN : 0.000
Permeability & MD-FT : 0.000 MD FT : 0.00
Shale Stress : 0.000 Reservoir Pressure : 1560
Sand Stress : 0.000
Bleed Off Ratio : 0.000
Breakdown Fluid : 40 bbl of : Linear Purgel III
# of Perfs Open : 30
Entry Points : 2
Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 504 bbl of LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 63 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

Max Treat Pressure : 3561 psi
Min Treat Pressure : 1608 psi
Avg Treat Pressure : 2936 psi
After Frac ISDP : 2310 @ 1.080 psi/ft
Press. Increase During Frac : 0 psi
Avg Rate : 16 bbl/min
Flush Short With : 35 bbl of Slick Water or 1478 Gals
Total Fluid To Recover : 579 bbl + 56 In CSG = 635

Tagged E.L. : 4696.00 FT : (>6% Porosity)

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4664.000 | 4669.000 | 3 | 15 | |

Casing ID : 4.000
Entrance Size : 0.370

Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1046 | 0.0 | 0 | 25.0 | 5.0 | 4694.0 | 2606.0 |
| 2 | CO2 Linear Pad | 1527 | 0.0 | 0 | 36.0 | 10.1 | 4290.0 | 2700.0 |
| 3 | 1# SLF CO2 Foam | 709 | 2.0 | 1354 | 18.0 | 10.8 | 4030.0 | 3848.0 |
| 4 | 2# SLF CO2 Foam | 1324 | 4.0 | 4859 | 37.0 | 11.7 | 3951.0 | 3580.0 |
| 5 | 3# SLF CO2 Foam | 1396 | 5.0 | 7371 | 41.0 | 12.3 | 3812.0 | 3419.0 |
| 6 | 4# SLF CO2 Foam | 1889 | 6.0 | 11416 | 57.0 | 13.2 | 3522.0 | 3311.0 |
| 7 | Overflush (50%) | 1035 | 0.0 | 0 | 25.0 | 10.3 | 3504.0 | 3195.0 |
| 8 | Flush (50%) | 1755 | 0.0 | 0 | 42.0 | 10.0 | 3568.0 | 2400.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 59.00 | 66.76 | -11.60 |
| MA-844 | 25.00 | 21.36 | 17.00 |
| AQF-2 | 38.00 | 35.75 | 6.30 |
| SP Breaker | 7.00 | 7.89 | 0.00 |
| GBW-30 | 5.00 | 5.57 | 0.00 |
| Gyptron T-2 | 90.00 | 110.00 | -18.20 |
| CO2 | 36.00 | 34.60 | 4.00 |
| CO2 | 196.20 | 188.57 | 4.00 |
| CO2 | 8240.40 | 7919.94 | 4.00 |

| | | | |
|---|---|---|---|
| Gel System : | 7880 | Tanks : | 1 |
| Pct Pad : | 36.77 | Avg Prop Conc : | 2.30 |
| Total Fluid : | 10681 | Avg Rate : | 10.5 |
| Total Slurry : | 11812 | Max Rate : | 13.2 |
| Prime-Up & Tnkbot : | 5414 | Min Rate : | 5.0 |
| Total Job Fluid : | 17000 | | |

**Proppant Summary** Total Proppant Pumped : 25000 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 25000 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.44 | | |
| Wellhead Pressure : | 2500 | @ | psi/ft |
| Broke Back : | 4694 | @ | 17 bbl/min |
| Final Injection : | 2900 | @ | 10 bbl/min |
| ISIP : | 2490.0 | @ | 0.970 psi/ft |
| 1 Min ISIP : | | @ | psi/ft |
| 4 Min ISIP : | | @ | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 2021 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 25 | bbl of : Linear Purgel III | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | | @ 0.0000 $/lb | |

**Frac Information**

Fraced well with 213 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 36 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 4694 | psi |
| Min Treat Pressure : | 2606 | psi |
| Avg Treat Pressure : | 3604 | psi |
| After Frac ISDP : | 2490 @ 0.970 | psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 10 | bbl/min |
| Flush Short With : | 42 bbl of Slick Water or | 1755 Gals |
| Total Fluid To Recover : | 279 bbl + | 73 In CSG = 352 |

Tagged E.L. : 4015.00 FT : (>6% Porosity)

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 3856.000 | 3858.000 | 3 | 6 | |
| 3873.000 | 3875.000 | 3 | 6 | |
| 3914.000 | 3916.000 | 3 | 6 | |
| 3922.000 | 3924.000 | 3 | 6 | |
| 3937.000 | 3939.000 | 3 | 6 | |
| 3964.000 | 3966.000 | 3 | 6 | |
| 3986.000 | 3988.000 | 3 | 6 | |

Casing ID : 4.000
Entrance Size : 0.370

Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 4875 | 0.0 | 0 | 116.0 | 11.1 | 3680.0 | 800.0 |
| 2 | CO2 Linear Pad | 25500 | 0.0 | 0 | 607.0 | 33.7 | 5771.0 | 2000.0 |
| 3 | 0.25# SLF CO2 Foam | 12791 | 0.0 | 4400 | 309.0 | 39.5 | 5334.0 | 4402.0 |
| 4 | 0.50# SLF CO2 Foam | 32446 | 1.0 | 22000 | 796.0 | 40.9 | 5066.0 | 4677.0 |
| 5 | 0.75# SLF CO2 Foam | 17375 | 1.0 | 18070 | 433.0 | 40.4 | 5032.0 | 4808.0 |
| 6 | 1.00# SLF CO2 Foam | 9909 | 1.0 | 13575 | 251.0 | 40.9 | 4990.0 | 4928.0 |
| 7 | 1.50# SLF CO2 Foam | 6689 | 2.0 | 13445 | 174.0 | 40.9 | 4989.0 | 4757.0 |
| 8 | 2.00# SLF CO2 Foam | 7373 | 3.0 | 18710 | 196.0 | 41.1 | 5214.0 | 4797.0 |
| 9 | Overflush (50%) | 1462 | 0.0 | 0 | 35.0 | 40.9 | 6023.0 | 5087.0 |
| 10 | Flush (50%) | 2075 | 0.0 | 0 | 49.0 | 34.4 | 6293.0 | 2300.0 |

**Additive Totals**

| Additive | Acual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| FR-56 | 55.00 | 60.25 | -8.70 |
| MA-844 | 220.00 | 240.99 | -8.70 |
| AQF-2 | 320.00 | 346.86 | -7.70 |
| Gyptron T-2 | 95.00 | 323.13 | -70.60 |
| CO2 | 198.00 | 198.80 | 0.00 |
| CO2 | 1079.10 | 1083.46 | -0.40 |
| CO2 | 45322.2( | 45505.32 | -0.40 |

Gel System : 113545 Tanks : 8
Pct Pad : 36.45 Avg Prop Conc : 0.80
Total Fluid : 120495 Avg Rate : 36.6
Total Slurry : 124576 Max Rate : 41.1
Prime-Up & Tnkbot : 17893 Min Rate : 11.1
Total Job Fluid : 139000

**Proppant Summary** Total Proppant Pumped : 90200 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 90200 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.50
Wellhead Pressure : 900 @ psi/ft
Broke Back : 3055 @ 15 bbl/min
Final Injection : 2750 @ 23 bbl/min
ISIP : 2100.0 @ 0.980 psi/ft
1 Min ISIP : @ psi/ft
4 Min ISIP : @ psi/ft
3 Min Bleed Off :
Final ISIP : 0.0 Final ISIP MIN : 0.000
Permeability & MD-FT : 0.000 MD FT : 0.00
Shale Stress : 0.000 Reservoir Pressure : 1698
Sand Stress : 0.000
Bleed Off Ratio : 0.000
Breakdown Fluid : 116 bbl of : Linear Purgel III
# of Perfs Open : 30

**Frac Information**

Fraced well with 2820 bbl of : LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 198 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

Max Treat Pressure : 6023 psi
Min Treat Pressure : 800 psi
Avg Treat Pressure : 4575 psi
After Frac ISDP : 2100 @ 0.980 psi/ft
Press. Increase During Frac : 0 psi
Avg Rate : 37 bbl/min
Flush Short With : 49 bbl of Slick Water or 2075 Gals
Total Fluid To Recover : 2985 bbl + 62 In CSG = 3047

| Tagged E.L. : | 3736.00 | FT : (>6% Porosity) | | Casing ID : | 4.000 | Volume to Load Hole |
|---|---|---|---|---|---|---|
| Top | Bottom | JSPF | Shots | Status | Entrance Size : | Pressure Test |
| 3694.000 | 3709.000 | 3 | 45 | | 0.370 | BBC Representative<br>Russell Evans<br>HES Representative<br>Pat Butterfield. Technical Professional |

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1244 | 0.0 | 0 | 30.0 | 7.6 | 4280.0 | 1454.0 |
| 2 | CO2 Linear Pad | 2644 | 0.0 | 0 | 63.0 | 11.3 | 3219.0 | 1928.0 |
| 3 | 1# SLF CO2 Foam | 1193 | 2.0 | 2200 | 31.0 | 13.8 | 2614.0 | 2458.0 |
| 4 | 2# SLF CO2 Foam | 2167 | 4.0 | 7800 | 60.0 | 14.7 | 2568.0 | 2415.0 |
| 5 | 3# SLF CO2 Foam | 2222 | 5.0 | 11500 | 65.0 | 15.5 | 2444.0 | 2378.0 |
| 6 | 4# SLF CO2 Foam | 3629 | 6.0 | 21500 | 110.0 | 16.2 | 2413.0 | 2235.0 |
| 7 | Overflush (50%) | 1101 | 0.0 | 0 | 26.0 | 12.9 | 2510.0 | 2330.0 |
| 8 | Flush (50%) | 1222 | 0.0 | 0 | 29.0 | 12.6 | 2569.0 | 1791.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 113.00 | 96.39 | 17.20 |
| MA-844 | 30.00 | 30.84 | 0.00 |
| AQF-2 | 75.00 | 54.39 | 37.90 |
| SP Breaker | 11.00 | 13.10 | -16.00 |
| GBW-30 | 8.00 | 9.46 | -15.40 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 51.00 | 52.70 | -3.20 |
| CO2 | 277.95 | 287.22 | -3.20 |
| CO2 | 11673.9( | 2063.03 | -3.20 |

| | | | |
|---|---|---|---|
| Gel System : | 12956 | Tanks : | 2 |
| Pct Pad : | 35.78 | Avg Prop Conc : | 2.80 |
| Total Fluid : | 15422 | Avg Rate : | 13.1 |
| Total Slurry : | 17368 | Max Rate : | 16.2 |
| Prime-Up & Tnkbot : | 5953 | Min Rate : | 7.6 |
| Total Job Fluid : | 22000 | | |

**Proppant Summary** Total Proppant Pumped : 43000 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 43000 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | | |
|---|---|---|---|---|
| Base Fluid : | 8.43 | | | |
| Wellhead Pressure : | 1530 | @ | | psi/ft |
| Broke Back : | 4280 | @ | 17 | bbl/min |
| Final Injection : | 2220 | @ | 13 | bbl/min |
| ISIP : | 1922.0 | @ | 0.960 | psi/ft |
| 1 Min ISIP : | | @ | | psi/ft |
| 4 Min ISIP : | | @ | | psi/ft |
| 3 Min Bleed Off : | | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | | 1603 |
| Sand Stress : | 0.000 | | | |
| Bleed Off Ratio : | 0.000 | | | |
| Breakdown Fluid : | 30 | bbl of : Linear Purgel III | | |
| # of Perfs Open : | 30 | | | |
| Entry Points : | 2 | | | |
| Total Cost : | | @ | 0.0000 | $/lb |

**Frac Information**

Fraced well with 338 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 51 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | | |
|---|---|---|---|
| Max Treat Pressure : | 4280 | psi | |
| Min Treat Pressure : | 1454 | psi | |
| Avg Treat Pressure : | 2518 | psi | |
| After Frac ISDP : | 1922 | @ 0.960 | psi/ft |
| Press. Increase During Frac : | 0 | psi | |
| Avg Rate : | 13 | bbl/min | |
| Flush Short With : | 29 | bbl of Slick Water or 1222 | Gals |
| Total Fluid To Recover : | 397 | bbl + 58 In CSG = 455 | |

Tagged E.L. : 4929.00 FT : (>6% Porosity)

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4860.000 | 4868.000 | 3 | 24 | |
| 4898.000 | 4902.000 | 3 | 12 | |

Casing ID : 4.000
Entrance Size : 0.370

Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 856 | 0.0 | 0 | 20.0 | 6.2 | 4034.0 | 2058.0 |
| 2 | CO2 Linear Pad | 2579 | 0.0 | 0 | 61.0 | 9.9 | 3014.0 | 2250.0 |
| 3 | 1# SLF CO2 Foam | 1085 | 2.0 | 2072 | 28.0 | 10.9 | 3034.0 | 2663.0 |
| 4 | 2# SLF CO2 Foam | 2278 | 4.0 | 8360 | 63.0 | 11.8 | 3019.0 | 2898.0 |
| 5 | 3# SLF CO2 Foam | 2376 | 5.0 | 12545 | 70.0 | 12.3 | 2969.0 | 2731.0 |
| 6 | 4# SLF CO2 Foam | 2966 | 6.0 | 19022 | 91.0 | 12.7 | 2909.0 | 2601.0 |
| 7 | Overflush (50%) | 1041 | 0.0 | 0 | 25.0 | 9.9 | 2984.0 | 2640.0 |
| 8 | Flush (50%) | 1920 | 0.0 | 0 | 46.0 | 10.0 | 3000.0 | 2300.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 84.00 | 94.38 | -11.00 |
| LoSurf-300 | 15.00 | 15.10 | 0.00 |
| AQF-2 | 50.00 | 54.02 | -7.40 |
| SP Breaker | 12.00 | 12.14 | 0.00 |
| GBW-30 | 8.00 | 8.72 | 0.00 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 44.00 | 44.50 | 0.00 |
| CO2 | 239.80 | 242.53 | -1.10 |
| CO2 | 10071.6( | 0186.05 | -1.10 |

Gel System : 12325 Tanks : 2
Pct Pad : 34.29 Avg Prop Conc : 2.70
Total Fluid : 15101 Avg Rate : 10.5
Total Slurry : 17001 Max Rate : 12.7
Prime-Up & Tnkbot : 5916 Min Rate : 6.2
Total Job Fluid : 22000

**Proppant Summary** Total Proppant Pumped : 42000 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 42000 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.46
Wellhead Pressure : 2061 @ psi/ft
Broke Back : 4304 @ 17 bbl/min
Final Injection : 2640 @ 10 bbl/min
ISIP : 2340.0 @ 0.920 psi/ft
1 Min ISIP : @ psi/ft
4 Min ISIP : @ psi/ft
3 Min Bleed Off :
Final ISIP : 0.0 Final ISIP MIN : 0.000
Permeability & MD-FT : 0.000 MD FT : 0.00
Shale Stress : 0.000 Reservoir Pressure : 2113
Sand Stress : 0.000
Bleed Off Ratio : 0.000
Breakdown Fluid : 20 bbl of : Linear Purgel III
# of Perfs Open : 30
Entry Points : 2
Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 314 bbl of : LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 44 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

Max Treat Pressure : 4034 psi
Min Treat Pressure : 2058 psi
Avg Treat Pressure : 2843 psi
After Frac ISDP : 2340 @ 0.920 psi/ft
Press. Increase During Frac : 0 psi
Avg Rate : 11 bbl/min
Flush Short With : 46 bbl of Slick Water or 1920 Gals
Total Fluid To Recover : 380 bbl + 77 In CSG = 457

Tagged E.L. : 4331.00 FT : (>6% Porosity)

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4147.000 | 4150.000 | 3 | 9 | |
| 4170.000 | 4173.000 | 3 | 9 | |
| 4188.000 | 4190.000 | 3 | 6 | |
| 4276.000 | 4280.000 | 3 | 12 | |
| 4301.000 | 4304.000 | 3 | 9 | |

Casing ID : 4.000
Entrance Size : 0.370

Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1565 | 0.0 | 0 | 37.0 | 9.2 | 3894.0 | 1865.0 |
| 2 | CO2 Linear Pad | 6071 | 0.0 | 0 | 145.0 | 19.9 | 4303.0 | 3121.0 |
| 3 | 1# SLF CO2 Foam | 2540 | 2.0 | 4851 | 66.0 | 21.4 | 3979.0 | 3820.0 |
| 4 | 2# SLF CO2 Foam | 5216 | 4.0 | 19143 | 145.0 | 23.3 | 4123.0 | 3799.0 |
| 5 | 3# SLF CO2 Foam | 5407 | 5.0 | 28549 | 159.0 | 24.4 | 4073.0 | 3722.0 |
| 6 | 4# SLF CO2 Foam | 9705 | 6.0 | 56557 | 292.0 | 25.6 | 3846.0 | 3732.0 |
| 7 | Overflush (50%) | 1079 | 0.0 | 0 | 26.0 | 20.3 | 3803.0 | 3549.0 |
| 8 | Flush (50%) | 1680 | 0.0 | 0 | 40.0 | 20.0 | 3845.0 | 3063.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 233.00 | 207.89 | 12.10 |
| LoSurf-300 | 40.00 | 33.26 | 20.30 |
| AQF-2 | 120.00 | 124.03 | -3.30 |
| SP Breaker | 30.00 | 30.50 | 0.00 |
| GBW-30 | 22.00 | 22.76 | 0.00 |
| Gyptron T-2 | 115.00 | 110.00 | 4.50 |
| CO2 | 94.00 | 95.10 | -1.20 |
| CO2 | 512.30 | 518.30 | -1.20 |
| CO2 | 21516.6( | 1768.39 | -1.20 |

Gel System : 30018 Tanks : 3
Pct Pad : 32.22 Avg Prop Conc : 3.30
Total Fluid : 33263 Avg Rate : 20.6
Total Slurry : 38200 Max Rate : 25.6
Prime-Up & Tnkbot : 7980 Min Rate : 9.2
Total Job Fluid : 42000

**Proppant Summary** Total Proppant Pumped : 109100 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 109100 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.46
Wellhead Pressure : 1940 @ psi/ft
Broke Back : 3616 @ 18 bbl/min
Final Injection : 3160 @ 20 bbl/min
ISIP : 2590.0 @ 1.050 psi/ft
1 Min ISIP : @ psi/ft
4 Min ISIP : @ psi/ft
3 Min Bleed Off :
Final ISIP : 0.0 Final ISIP MIN : 0.000
Permeability & MD-FT : 0.000 MD FT : 0.00
Shale Stress : 0.000 Reservoir Pressure : 1830
Sand Stress : 0.000
Bleed Off Ratio : 0.000
Breakdown Fluid : 37 bbl of : Linear Purgel III
# of Perfs Open : 30
Entry Points : 2
Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 752 bbl of : LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 94 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

Max Treat Pressure : 4303 psi
Min Treat Pressure : 1865 psi
Avg Treat Pressure : 3688 psi
After Frac ISDP : 2590 @ 1.050 psi/ft
Press. Increase During Frac : 0 psi
Avg Rate : 21 bbl/min
Flush Short With : 40 bbl of Slick Water or 1680 Gals
Total Fluid To Recover : 829 bbl + 67 In CSG = 897

Tagged E.L. : 4442.00 FT : (>6% Porosity) Casing ID : 4.892 Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Aaron Holten, Technical Professional

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4395.000 | 4415.000 | 3 | 60 | |

Entrance Size : 0.370

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1195 | 0.0 | 0 | 28.0 | 2.9 | 3201.0 | 2303.0 |
| 2 | CO2 Linear Pad | 5115 | 0.0 | 0 | 122.0 | 12.7 | 6137.0 | 2781.0 |
| 3 | 1# SLF CO2 Foam | 3197 | 2.0 | 6330 | 83.0 | 13.2 | 4547.0 | 3753.0 |
| 4 | 2# SLF CO2 Foam | 6208 | 4.0 | 24522 | 174.0 | 13.7 | 3762.0 | 3679.0 |
| 5 | 3# SLF CO2 Foam | 5229 | 6.0 | 29548 | 156.0 | 14.2 | 3698.0 | 3652.0 |
| 6 | Overflush (50%) | 0 | 0.0 | 0 | 0.0 | 0.1 | 0.0 | 0.0 |
| 8 | Flush (50%) | 2222 | 0.0 | 0 | 53.0 | 12.9 | 3673.0 | 447.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 135.00 | 144.79 | -6.80 |
| LoSurf 300 | 25.00 | 23.17 | 7.90 |
| AQF-2 | 80.00 | 85.66 | -6.60 |
| SP Breaker | 19.00 | 20.94 | -9.30 |
| GBW-30 | 12.00 | 14.64 | -18.00 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 83.00 | 86.90 | -4.50 |
| CO2 | 452.35 | 473.61 | -4.50 |
| CO2 | 18998.7( | 9891.41 | -4.50 |

Gel System : 19749 Tanks : 2
Pct Pad : 45.39 Avg Prop Conc : 2.50
Total Fluid : 23166 Avg Rate : 9.5
Total Slurry : 25899 Max Rate : 14.2
Prime-Up & Tnkbot : 6833 Min Rate : 0.1
Total Job Fluid : 30000

**Proppant Summary** Total Proppant Pumped : 60400 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 60400 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.42
Wellhead Pressure : 2450 @ psi/ft
Broke Back : 5946 @ 10 bbl/min
Final Injection : 3600 @ 25 bbl/min
ISIP : 2596.0 @ 1.030 psi/ft
1 Min ISIP : @ psi/ft
4 Min ISIP : @ psi/ft
3 Min Bleed Off :
Final ISIP : 0.0 Final ISIP MIN : 0.000
Permeability & MD-FT : 0.000 MD FT : 0.00
Shale Stress : 0.000 Reservoir Pressure : 1907
Sand Stress : 0.000
Bleed Off Ratio : 0.000
Breakdown Fluid : 28 bbl of : Linear Purgel III
# of Perfs Open : 30
Entry Points : 2
Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 499 bbl of : LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 83 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

Max Treat Pressure : 6137 psi
Min Treat Pressure : 2303 psi
Avg Treat Pressure : 3751 psi
After Frac ISDP : 2596 @ 1.030 psi/ft
Press. Increase During Frac : 0 psi
Avg Rate : 9 bbl/min
Flush Short With : 53 bbl of Slick Water or 2222 Gals
Total Fluid To Recover : 580 bbl + 103 In CSG = 683

Tagged E.L. : 4197.00 FT : (>6% Porosity)

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4126.000 | 4136.000 | 3 | 30 | Open |
| 4164.000 | 4170.000 | 3 | 18 | Open |

Casing ID : 4.892
Entrance Size : 0.370

Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Aaron Holten, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 2049 | 0.0 | 0 | 49.0 | 9.9 | 3465.0 | 851.0 |
| 2 | CO2 Linear Pad | 9026 | 0.0 | 0 | 215.0 | 15.0 | 3770.0 | 1826.0 |
| 3 | 1# SLF CO2 Foam | 5574 | 2.0 | 11037 | 145.0 | 15.8 | 3787.0 | 3654.0 |
| 4 | 2# SLF CO2 Foam | 11067 | 4.0 | 43715 | 311.0 | 16.4 | 3854.0 | 3689.0 |
| 5 | 3# SLF CO2 Foam | 9433 | 6.0 | 53349 | 282.0 | 17.0 | 3965.0 | 3675.0 |
| 6 | Overflush (50%) | 1004 | 0.0 | 0 | 24.0 | 15.2 | 3966.0 | 3562.0 |
| 8 | Flush (50%) | 1484 | 0.0 | 0 | 35.0 | 11.4 | 4043.0 | 86.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 245.00 | 247.73 | -1.10 |
| LoSurf 300 | 35.00 | 39.64 | -11.70 |
| AQF-2 | 150.00 | 147.86 | 1.40 |
| SP Breaker | 36.00 | 37.15 | -3.10 |
| GBW-30 | 23.00 | 26.06 | -11.70 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 139.00 | 143.90 | -3.40 |
| CO2 | 757.55 | 784.26 | -3.40 |
| CO2 | 31817.1( | 2938.71 | -3.40 |

Gel System : 36104 Tanks : 3
Pct Pad : 43.64 Avg Prop Conc : 2.70
Total Fluid : 39637 Avg Rate : 14.9
Total Slurry : 44528 Max Rate : 17.0
Prime-Up & Tnkbot : 8704 Min Rate : 9.9
Total Job Fluid : 49000

**Proppant Summary** Total Proppant Pumped : 108100 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 108100 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.41
Wellhead Pressure : 850 @ psi/ft
Broke Back : 3465 @ 15 bbl/min
Final Injection : 3580 @ 15 bbl/min
ISIP : 3225.0 @ 1.210 psi/ft
1 Min ISIP : @ psi/ft
4 Min ISIP : @ psi/ft
3 Min Bleed Off :
Final ISIP : 0.0 Final ISIP MIN : 0.000
Permeability & MD-FT : 0.000 MD FT : 0.00
Shale Stress : 0.000 Reservoir Pressure : 1796
Sand Stress : 0.000
Bleed Off Ratio : 0.000
Breakdown Fluid : 49 bbl of : Linear Purgel III
# of Perfs Open : 30
Entry Points : 2
Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 908 bbl of : LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 139 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

Max Treat Pressure : 3966 psi
Min Treat Pressure : 851 psi
Avg Treat Pressure : 3339 psi
After Frac ISDP : 3225 @ 1.210 psi/ft
Press. Increase During Frac : 0 psi
Avg Rate : 15 bbl/min
Flush Short With : 35 bbl of Slick Water or 1484 Gals
Total Fluid To Recover : 993 bbl + 98 In CSG = 1090

| | | | | | | | |
|---|---|---|---|---|---|---|---|
| Tagged E.L. : | 3961.00 | FT : (>6% Porosity) | | Casing ID : | 4.892 | Volume to Load Hole | |
| Top | Bottom | JSPF | Shots | Status | Entrance Size : | Pressure Test | |
| 3914.000 | 3934.000 | 3 | 60 | Open | 0.370 | BBC Representative | |
| | | | | | | Russell Evans | |
| | | | | | | HES Representative | |
| | | | | | | Aaron Holten, Technical Professional | |

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1083 | 0.0 | 0 | 26.0 | 7.0 | 3775.0 | 1949.0 |
| 2 | CO2 Linear Pad | 6354 | 0.0 | 0 | 151.0 | 15.2 | 3231.0 | 2098.0 |
| 3 | 1# SLF CO2 Foam | 3651 | 2.0 | 7229 | 95.0 | 15.7 | 3287.0 | 3158.0 |
| 4 | 2# SLF CO2 Foam | 7215 | 4.0 | 28499 | 202.0 | 16.4 | 3351.0 | 3265.0 |
| 5 | 3# SLF CO2 Foam | 7790 | 5.0 | 41772 | 230.0 | 17.0 | 3511.0 | 3310.0 |
| 8 | Flush (50%) | 1596 | 0.0 | 0 | 38.0 | 14.6 | 3570.0 | 3000.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 180.00 | 173.06 | 4.00 |
| LoSurf 300 | 30.00 | 27.69 | 8.30 |
| AQF-2 | 100.00 | 104.83 | -4.60 |
| SP Breaker | 25.00 | 26.09 | -4.20 |
| GBW-30 | 23.00 | 18.75 | 22.70 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 93.00 | 101.90 | -8.70 |
| CO2 | 506.85 | 555.36 | -8.70 |
| CO2 | 21287.7( | 3324.91 | -8.70 |

| | | | |
|---|---|---|---|
| Gel System : | 25010 | Tanks : | 2 |
| Pct Pad : | 42.49 | Avg Prop Conc : | 2.70 |
| Total Fluid : | 27689 | Avg Rate : | 14.3 |
| Total Slurry : | 31196 | Max Rate : | 17.0 |
| Prime-Up & Tnkbot : | 7346 | Min Rate : | 7.0 |
| Total Job Fluid : | 36000 | | |

**Proppant Summary** Total Proppant Pumped : 77500 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 77500 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | | |
|---|---|---|---|---|
| Base Fluid : | 8.41 | | | |
| Wellhead Pressure : | 2400 | @ | | psi/ft |
| Broke Back : | 3775 | @ | 15 | bbl/min |
| Final Injection : | 3400 | @ | 26 | bbl/min |
| ISIP : | 2635.0 | @ | 1.110 | psi/ft |
| 1 Min ISIP : | | @ | | psi/ft |
| 4 Min ISIP : | | @ | | psi/ft |
| 3 Min Bleed Off : | | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | | 1699 |
| Sand Stress : | 0.000 | | | |
| Bleed Off Ratio : | 0.000 | | | |
| Breakdown Fluid : | 26 | bbl of : Linear Purgel III | | |
| # of Perfs Open : | 30 | | | |
| Entry Points : | 2 | | | |
| Total Cost : | | @ | 0.0000 | $/lb |

**Frac Information**

Fraced well with 621 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 93 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | | |
|---|---|---|---|
| Max Treat Pressure : | 3775 | psi | |
| Min Treat Pressure : | 1949 | psi | |
| Avg Treat Pressure : | 3094 | psi | |
| After Frac ISDP : | 2635 | @ 1.110 | psi/ft |
| Press. Increase During Frac : | 0 | psi | |
| Avg Rate : | 14 | bbl/min | |
| Flush Short With : | 38 | bbl of Slick Water or | 1596 Gals |
| Total Fluid To Recover : | 685 | bbl + | 92 In CSG = 777 |

**From:** Chris Kierst
**To:** Tracey Fallang
**Date:** 09/09/2008 4:45 PM
**Subject:** Re: Prickly Pear 12-24 SWD

Hi Tracey,
You do not need to re-Notice for this procedure. You do not have to perform a Step Rate Test (SRT) for the interval specified as Interval (Stage) #1 on the Table (4,500' to 4,518' TD) attached to the Sundry Notice dated 7/16/2008. This interval will be construed by DOGM to be covered under the existing Permitted Maximum Allowable Surface Pressure (2,000 psi). However, subsequent uphole zones in the middle Wasatch Formation, as listed on the cited attached Table, that may be proposed for perforation, will require SRT. You will need to submit a new Sundry Notice requesting permission to inject into the new middle Wasatch Formation perforations as a Permit Modification. If everything is acceptable on the Sundry Notice then Brad Hill will approve it and a copy will be returned. We can provide a verbal permission to proceed after receipt and approval of the new Sundry Notice if you feel it is warranted. Otherwise, normal documentation of approval will occur within a conventional postal delivery cycle. Please contact me if you have any questions (801) 538-5337 or chriskierst@utah.gov.

>>> Tracey Fallang <tfallang@billbarrettcorp.com> 09/09/2008 11:52 AM >>>
Chris, we received the SWD permit, thank you. A couple of questions as we get closer to frac'ing that upper zone.

1) Because the original public notice dated April 23, 2007 included the Wasatch, will you need to re-notice or are we OK?
2) Once we perf and frac, what is the next process. Will we then need to complete another step-rate and provide you with those results and then amend the current permit?
3) I guess based on your answer for #2 above, how long will the approval take of the amended permit as the engineer in our office has concern about shutting the well in.

Thanks Chris!

**From:** Tracey Fallang <tfallang@billbarrettcorp.com>
**To:** Chris Kierst <chriskierst@utah.gov>
**Date:** 09/09/2008 11:53 AM
**Subject:** Prickly Pear 12-24 SWD

Chris, we received the SWD permit, thank you. A couple of questions as we get closer to frac'ing that upper zone.

1) Because the original public notice dated April 23, 2007 included the Wasatch, will you need to re-notice or are we OK?
2) Once we perf and frac, what is the next process. Will we then need to complete another step-rate and provide you with those results and then amend the current permit?
3) I guess based on your answer for #2 above, how long will the approval take of the amended permit as the engineer in our office has concern about shutting the well in.

Thanks Chris!

No SRT; we will accept existing pressure
Another sundry requesting permit mod. to inject into your table 1 zone perfs
Subsequent perfs will need an SRT

JON M. HUNTSMAN, JR.
*Governor*

GARY R. HERBERT
*Lieutenant Governor*

# State of Utah
**DEPARTMENT OF NATURAL RESOURCES**

MICHAEL R. STYLER
*Executive Director*

**Division of Oil, Gas and Mining**

JOHN R. BAZA
*Division Director*

Chris -
For the file -
-Jan

## UNDERGROUND INJECTION CONTROL PERMIT

### Cause No. UIC-338

**Operator:** Bill Barrett Corporation

**Wells:** Prickly Pear Unit Federal 12-24

**Location:** Section 24, Township 12 South, Range 14 East (SLBM)

**County:** Carbon

**API No.:** 43-007-30953

**Well Type:** Salt Water Disposal Well

**Stipulations of Permit Approval**

1. Approval for conversion to Injection Well issued on July 31, 2007
2. Maximum Allowable Surface Pressure: 2000 psi.
3. Corresponding Injection Rate: As limited by pressure.
4. Injection Interval: Perforations between 6,295' and 7,630'in the North Horn Formation, Dark Canyon Conglomerate and Price River Formation.

---

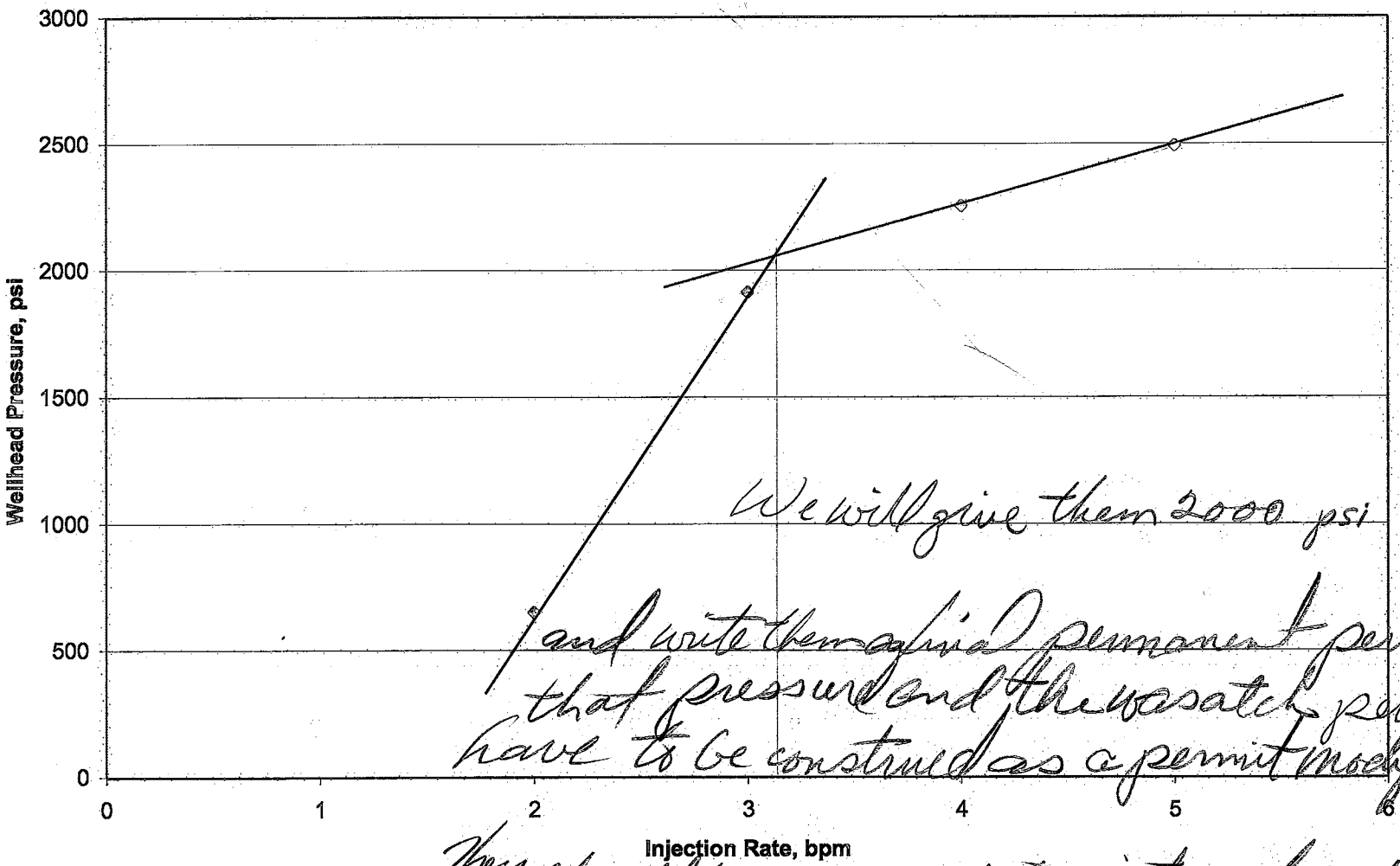
Approved by: Gil Hunt — Associate Director

8-28-08
Date

CK/js

cc: Dan Jackson, Environmental Protection Agency
Bureau of Land Management, Price
Carbon County Planning

**Prickly Pear 12-24**
**Step Rate Test August 30** 2007




We will give them 2000 psi max inj. pressure and write them a trial permanent permit with that pressure and the Wasatch perfs will have to be construed as a permit modification.

They should have had 7 data points not just 5 or 6.

**From:** Tracey Fallang <tfallang@billbarrettcorp.com>
**To:** Chris Kierst <chriskierst@utah.gov>
**Date:** 11/02/2008 2:00 PM
**Subject:** Sundry for Amendment to UIC-338
**Attachments:** SKMBT_C35108110304280.pdf

Chris, as per our last discussion on this, I am attaching the sundry to amend our UIC permit. We would like to begin using this immediately so if we could get a verbal to proceed, I'd appreciate it. A hard copy will be sent via mail.

Form 3160-5
(April 2004)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OMB No. 1004-0137
Expires: March 31, 2007

## SUNDRY NOTICES AND REPORTS ON WELLS

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE- Other instructions on reverse side.***

5. Lease Serial No.
**UTU-77513**

6. If Indian, Allottee or Tribe Name
**n/a**

7. If Unit or CA/Agreement, Name and/or No.
**Prickly Pear / UTU-79487**

8. Well Name and No.
**Prickly Pear Unit Fed 12-24**

9. API Well No.
**43-007-30953**

10. Field and Pool, or Exploratory Area

11. County or Parish, State
**Carbon County, Utah**

1. Type of Well
☐ Oil Well ☐ ☑ Gas Well ☐☐ ☐ Other

2. Name of Operator **BILL BARRETT CORPORATION**

3a. Address
**1099 18th Street Suite 2300 Denver CO 80202**

3b. Phone No. *(include area code)*
**303 312-8134**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*
**SWSW, 1271' FSL, 483' FWL, Section 24-T12S-R14E S.L.B.&M.**

Permit Modification

12. CHECK APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☑ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production (Start/Resume) | ☐ Water Shut-Off |
| ☐ Subsequent Report | ☐ Alter Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☐ Final Abandonment Notice | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☑ Other **Amendment of disposal permit and** |
| | ☐ Change Plans | ☐ Plug and Abandon | ☐ Temporarily Abandon | |
| | ☐ Convert to Injection | ☐ Plug Back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be performed or provide the Bond No. on file with BLM/BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notices shall be filed only after all requirements, including reclamation, have been completed, and the operator has determined that the site is ready for final inspection.)

**This sundy is being submitted subsequent to approval granted (BLM-7/24/08 and DOGM 8/4/08) to allow additional perfs and testing on this well for conversion in to a water disposal well. As per guidance from Chris Kierst with DOGM (copy of e-mail attached), this request is to amend the existing UIC permit (UIC-338) to begin injection into the new Middle Wasatch perforations.**

**BBC was unable to perform the step-rate test requested (details attached). BBC requests that the injection pressure be set at 1200 psi with a rate 3000 bbls/day. Also attached to this sundry is a revised completion report and site security diagram.**

**If you should have any questions or need additional information, please contact me at 303-312-8134.**

14. I hereby certify that the foregoing is true and correct
Name *(Printed/Typed)*
**Tracey Fallang** Title **Regulatory Analyst**

Signature Tracey Fallang Date **11/03/2008**

## THIS SPACE FOR FEDERAL OR STATE OFFICE USE

Approved by BRADLEY G. HILL Title ENVIRONMENTAL MANAGER Date 11-03-08

Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. Office

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

*(Instructions on page 2)*

Federal Approval of this Action is Necessary

-----Original Message-----
From: Chris Kierst [mailto:chriskierst@utah.gov]
Sent: Tuesday, September 09, 2008 4:46 PM
To: Tracey Fallang
Subject: Re: Prickly Pear 12-24 SWD

Hi Tracey,
You do not need to re-Notice for this procedure. You do not have to perform a Step Rate Test (SRT) for the interval specified as Interval (Stage) #1 on the Table (4,500' to 4,518' TD) attached to the Sundry Notice dated 7/16/2008. This interval will be construed by DOGM to be covered under the existing Permitted Maximum Allowable Surface Pressure (2,000 psi). However, subsequent uphole zones in the middle Wasatch Formation, as listed on the cited attached Table, that may be proposed for perforation, will require SRT. You will need to submit a new Sundry Notice requesting permission to inject into the new middle Wasatch Formation perforations as a Permit Modification. If everything is acceptable on the Sundry Notice then Brad Hill will approve it and a copy will be returned. We can provide a verbal permission to proceed after receipt and approval of the new Sundry Notice if you feel it is warranted. Otherwise, normal documentation of approval will occur within a conventional postal delivery cycle. Please contact me if you have any questions (801) 538-5337 or chriskierst@utah.gov.

>>> Tracey Fallang <tfallang@billbarrettcorp.com> 09/09/2008 11:52 AM >>>
Chris, we received the SWD permit, thank you. A couple of questions as we get closer to frac'ing that upper zone.

1) Because the original public notice dated April 23, 2007 included the Wasatch, will you need to re-notice or are we OK?
2) Once we perf and frac, what is the next process. Will we then need to complete another step-rate and provide you with those results and then amend the current permit?
3) I guess based on your answer for #2 above, how long will the approval take of the amended permit as the engineer in our office has concern about shutting the well in.

Thanks Chris!

Form 3160-5
(April 2004)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

COPY

FORM APPROVED
OMB No. 1004-0137
Expires: March 31, 2007

## SUNDRY NOTICES AND REPORTS ON WELLS

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160-3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE*- Other instructions on reverse side.**

1. Type of Well: ☐ Oil Well ☐ ☑ Gas Well ☐ ☐ Other

2. Name of Operator: **BILL BARRETT CORPORATION**

3a. Address: **1099 18th Street Suite 2300 Denver CO 80202**

3b. Phone No. *(include area code)*: **303 312-8134**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*

**SWSW, 1271' FSL, 483' FWL, Section 24-T12S-R14E S.L.B.&M.**

5. Lease Serial No.: **UTU-77513**

6. If Indian, Allottee or Tribe Name: **n/a**

7. If Unit or CA/Agreement, Name and/or No.: **Prickly Pear / UTU-79487**

8. Well Name and No.: **Prickly Pear Unit Fed 12-24**

9. API Well No.: **43-007-30953**

10. Field and Pool, or Exploratory Area

11. County or Parish, State: **Carbon County, Utah**

12. CHECK APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☑ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production (Start/Resume) | ☐ Water Shut-Off |
| ☐ Subsequent Report | ☐ Alter Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☐ Final Abandonment Notice | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☑ Other **Amendment of disposal permit and** |
| | ☐ Change Plans | ☐ Plug and Abandon | ☐ Temporarily Abandon | |
| | ☐ Convert to Injection | ☐ Plug Back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be performed or provide the Bond No. on file with BLM/BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notices shall be filed only after all requirements, including reclamation, have been completed, and the operator has determined that the site is ready for final inspection.)

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**BBC was unable to perform the step-rate test requested (details attached). BBC requests that the injection pressure be set at 1200 psi with a rate 3000 bbls/day. Also attached to this sundry is a revised completion report and site security diagram.**

**If you should have any questions or need additional information, please contact me at 303-312-8134.**

RECEIVED
NOV 10 2008
DIV. OF OIL, GAS & MINING

14. I hereby certify that the foregoing is true and correct
Name *(Printed/Typed)*: **Tracey Fallang** Title **Regulatory Analyst**

Signature: Tracey Fallang Date: **11/03/2008**

**THIS SPACE FOR FEDERAL OR STATE OFFICE USE**

Approved by: BRADLEY G. HILL Title: ENVIRONMENTAL MANAGER Date: 11-17-08

Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon.

Office

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*(Instructions on page 2)*

**COPY SENT TO OPERATOR**
**Date:** 11.18.2008
**Initials:** KS

-----Original Message-----
From: Chris Kierst [mailto:chriskierst@utah.gov]
Sent: Tuesday, September 09, 2008 4:46 PM
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Thanks Chris!

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

**October 24, 2008**

| | | |
|---|---|---|
| **AFE #** | **W.I. 100.0000%** | |
| Surface Casing: | 9.625", 36.00#, J-55, ST&C | Set @ 1,002' |
| Production Casing: | 5.50", 17.00#, L-80, LT&C<br>Float collar @ 9,447'.<br>Cemented with 1850 sks 50/50 POZ<br>**Drift I.D. = 4.767". Collapse = 6,290 psi. Burst = 7,740 psi.**<br>**Capacity = 0.0232 BBL/Linear Ft.** | Set @9,491' |
| TOC: | 820' | |
| CBP @ 8,595'. | CFP @ 7,675". | |

Bit, bit sub and partial joint of tubing twisted off while drilling up CFP.
**Top of fish @ 7,665'**

CIBP @ 7,655' with 2 sx cement on top. PBTD @ 7,648'.

| | |
|---|---|
| Tubing: | 2 3/8", 4.7#, N-80, EUE 8RD to 3,400'. |
| Packer: | Halliburton "PLS" @ 3,400'. |

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

| | | | |
|---|---|---|---|
| **Perforations:** | Price River | 7,620-7,630' | 3 JSPF |
| | Dark Canyon | 7,258-7,266' | 3 JSPF |
| | North Horn | 6,908-6,916' | 4 JSPF |
| | | 6,791-6,799' | 3 JSPF |
| | | 6,295-6,300' | 3 JSPF |
| | Wasatch | 4,500-4,518' | 6 JSPF |
| | | 4,260-4,290' | 6 JSPF |
| | | 4,058-4,068' | 6 JSPF |
| | | 4,038-4,048' | 6 JSPF |
| | | 4,018-4,028' | 6 JSPF |
| | | 3,976-3,996' | 6 JSPF |
| | | 3,946-3,964' | 6 JSPF |
| | | 3,875-3,890' | 6 JSPF |
| | | 3,838-3,858' | 6 JSPF |
| | | 3,798-3,804' | 6 JSPF |
| | | 3,768-3,776' | 6 JSPF |
| | | 3,750-3,755' | 6 JSPF |
| | | 3,644-3,662' | 6 JSPF |
| | | 3,616-3,620' | 6 JSPF |
| | | 3,606-3,310' | 6 JSPF |
| | | 3,596-3,600' | 6 JSPF |
| | | 3,586-3,590' | 6 JSPF |
| | | 3,554-3,558' | 6 JSPF |
| | | 3,544-3,548' | 6 JSPF |
| | | 3,501-3,505' | 6 JSPF |
| | | 3,492-3,496' | 6 JSPF |
| | | 3,482-3,486' | 6 JSPF |

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

Bill Barrett Corporation has completed perforating and fracing 6 stages in the Wasatch interval on the Prickly Pear 12-24 well from 4,518' to 3,482'. Enclosed are the treatment summary sheets and the treating pressure graphs from CalFrac for each stage. After drilling out the composite frac plugs, a Halliburton "PLS" packer was run on 2.375", 4.7#, N-80, EUE 8rd tubing and set at 3,400' leaving the Price River, Dark Canyon, North Horn and Wasatch intervals open for water disposal. The tubing, packer and casing were pressure tested to 1,500 psi and the chart for the MIT is enclosed.

On each of the six stages, BBC shut down pumping after seeing an initial breakdown and recorded the instant shutdown pressure (ISIP) for each stage. BBC also recorded the final ISIP at the end of each stage. The initial and the final ISIPs along with their corresponding frac gradients are shown in the enclosed "**Prickly Pear 12-24 Disposal Well**" graph. After plotting the frac gradients for each stage, the initial ISIP on stage 2 and both the initial and final ISIPs on stages 3 and 4 appear to be abnormally low compared to the other stages. BBC then looked at the frac gradients for the Wasatch intervals on the offsetting Prickly Pear 13-17D-12-15 pad and found the following results:

| Well Name | Stage | Final Gradient psi/ft |
|---|---|---|
| Prickly Pear 12-17D | 12 | 0.960 |
| | 13 | 0.960 |
| | 14 | 0.980 |
| | 15 | 1.020 |
| | 16 | 1.080 |
| Prickly Pear 13-17D | 11 | 0.970 |
| | 12 | 0.980 |
| | 13 | 0.960 |
| Prickly Pear 14-17D | 07 | 0.920 |
| | 08 | 1.050 |
| Prickly Pear 16-18D | 10 | 1.030 |
| | 11 | 1.110 |
| | 12 | 1.210 |

The gradients on the offset wells are very similar to the final gradients on stages 1, 2, 5 and 6 of the Prickly Pear 12-24 well and would further indicate that the frac gradients seen on stages 3 and 4 may not be right.

The Wasatch interval in the Prickly Pear area is an under-pressured reservoir with a pore pressure gradient of approximately 0.38 psi/ft. BBC fraced the Wasatch intervals with a water based fluid with a hydrostatic gradient of approximately 0.44 psi/ft. Stages 3 and 4 both appear to have very high permeability as seen in the high leak-off rate after final shut-down. The shut in casing pressure on stage 3 bled off to 0 psi in 11 minutes and on stage 4 bled off to 0 psi in 3 minutes. BBC believes the high leak-off rate in these two intervals may be a factor causing us to see lower ISIPs in these two intervals than what we would expect to see. BBC would contend that in these two intervals, we either (a.) were not pumping enough rate to overcome the leak-off into the formation and did not generate a significant fracture in the formation or (b.) as we started to step down rate at the end of the jobs, the leak-off was higher than the pump rate and the fractures closed before we got to the final shutdown.

After the packer was run and the MIT was performed, BBC set up two 500 bbl frac tanks and filled them with produced water from the Prickly Pear wells. BBC injected the 1,000 bbls of produced water into the Prickly Pear well to test the viability of the newly completed interval for injection and to try to get a step-rate test to establish a maximum surface injection pressure. The water was injected at 2,700 bbl/day with 0 psi surface injection pressure. The tubing went on a vacuum immediately after shut down further confirming the high permeability in some of the Wasatch intervals. Because the Prickly Pear 12-24 well took water at 0 psi surface injection pressure, BBC was not able to obtain a step-rate test and requests that the maximum allowable surface injection pressure be determined from the frac gradients recorded on the six Wasatch fracs.

The **"Prickly Pear 12-24 Disposal Well"** graph shows the Initial and Final Gradient trendlines for the six Wasatch fracs and show an initial frac gradient of approximately 0.68 psi/ft and a final frac gradient of approximately 0.88 psi/ft. The trendlines include data from stages 3 and 4 which BBC believes are too low as we normally don't see sections within an interval that have significantly lower frac gradients than the sections above and below them. BBC would propose to use the average of the Initial and Final trendlines or 0.78 psi/ft as the starting point for maximum allowable injection pressure on the Prickly Pear 12-24 disposal well. BBC believes that the actual frac gradient in this interval is closer to 0.95 to 1.0 psi/ft and is supported by the Final frac gradients on stages 1, 2, 5 and 6 as well as on the offset wells, so using 0.78 psi/ft as a starting point will allow a significant margin for error.

**Bill Barrett Corporation**

# PRICKLY PEAR FEDERAL 12-24-12-14

**1,271' FSL & 483' FWL**
**SW/SW SECTION 24-T12S-R14E-W26M**
**CARBON COUNTY, UTAH**
**API #43-007-30953**

Using the following formula, ***maximum surface injection pressure = (frac gradient – hydrostatic gradient of injected water) x depth of top interval***, and a frac gradient of 0.78 psi/ ft, maximum surface injection pressure = (0.78 psi/ft - 0.433 psi/ft) x 3500' = 1,215 psi. BBC would propose setting the initial maximum allowable surface injection pressure at **1,200 psi** with a rate of **3,000 bbl/day** on the **Prickly Pear 12-24-12-14 Disposal Well.** After BBC has been injecting into this well for a period of time, we would expect the reservoir pressure to increase along with the surface injection pressure. If the surface injection pressure starts to approach the maximum allowable pressure, BBC would perform a step-rate test on the well and submit a request for a change in maximum allowable surface treating pressure based on the results of the step-rate test.

=REVISIONS

Form 3160-4
(April 2004)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

**BBC CONFIDENTIAL**

FORM APPROVED
OMB NO. 1004-0137
Expires: March 31, 2007

# WELL COMPLETION OR RECOMPLETION REPORT AND LOG

5. Lease Serial No. **UTU 77513**

1a. Type of Well ☐ Oil Well ☑ Gas Well ☐ Dry ☐ Other
b. Type of Completion: ☑ New Well ☐ Work Over ☐ Deepen ☐ Plug Back ☐ Diff. Resvr,.
Other

6. If Indian, Allottee or Tribe Name

7. Unit or CA Agreement Name and No. **Prickly Pear Unit**

2. Name of Operator **BILL BARRETT CORPORATION**

8. Lease Name and Well No. **Prickly Pear Unit Fed 12-24**

3. Address **1099 18th Street, Suite 2300 Denver, CO 80202**

3a. Phone No. *(include area code)* **303-312-8168**

9. AFI Well No. **4300730953**

4. Location of Well *(Report location clearly and in accordance with Federal requirements)**

At surface **SWSW, 1271' FSL, 483' FWL**

At top prod. interval reported below **same**

At total depth **same**

10. Field and Pool, or Exploratory **Prickly Pear**

11. Sec., T., R., M., on Block and Survey or Area **24-T12S-R14E**

12. County or Parish **Carbon**

13. State **UT**

14. Date Spudded **09/03/2004**

15. Date T.D. Reached **09/26/2004**

16. Date Completed **11/18/2004** ☐ D & A ☑ Ready to Prod.

17. Elevations (DF, RKB, RT, GL)* **7795'**

18. Total Depth: MD **9496'** TVD **9496'**

19. Plug Back T.D.: MD **7648'** TVD **7648'**

20. Depth Bridge Plug Set: MD **8595'** TVD **8595'**

21. Type Electric & Other Mechanical Logs Run (Submit copy of each)
**TRPL COMBO (GR/DSN/SDL AND HRI), DIPOLE SONIC & CBL/GR/CCL**

22. Was well cored? ☑ No ☐ Yes (Submit analysis)
Was DST run? ☑ No ☐ Yes (Submit report)
Directional Survey? ☑ No ☐ Yes (Submit copy)

23. Casing and Liner Record *(Report all strings set in well)*

| Hole Size | Size/Grade | Wt. (#/ft.) | Top (MD) | Bottom (MD) | Stage Cementer Depth | No. of Sks. & Type of Cement | Slurry Vol. (BBL) | Cement Top* | Amount Pulled |
|---|---|---|---|---|---|---|---|---|---|
| **12-1/4"** | **95/8 J-55** | **36** | **0** | **1002** | | **225 HLP** | **74** | **Surf (CIR)** | **None** |
| | | | | | | **190 Premag** | **39** | | |
| **7-7/8"** | **51/2 L80** | **17** | **0** | **9491** | | **1850 5050Poz** | **491** | **740 (CBL)** | **None** |
| | | | | | | | | | |
| | | | | | | | | | |
| | | | | | | | | | |

24. Tubing Record

| Size | Depth Set (MD) | Packer Depth (MD) | Size | Depth Set (MD) | Packer Depth (MD) | Size | Depth Set (MD) | Packer Depth (MD) |
|---|---|---|---|---|---|---|---|---|
| **2 3/8"** | **3400'** | | | | | | | |

25. Producing Intervals / 26. Perforation Record

| Formation | Top | Bottom | Perforated Interval | Size | No. Holes | Perf. Status |
|---|---|---|---|---|---|---|
| A) **Mesaverde** | **7258'** | **7630'** | **9242' - 9279'** | **0.41"** | **24** | **Closed** |
| B) **North Horn** | **4500'** | **6916'** | **8620' - 8699'** | **0.41"** | **24** | **Closed** |
| C) | | | **8460' - 8572'** | **0.41"** | **36** | **Closed** |
| D) | | | **8327' - 8379'** | **0.41"** | **24** | **Closed** |

27. Acid, Fracture, Treatment, Cement Squeeze, etc.

| Depth Interval | Amount and Type of Material |
|---|---|
| **9242' - 9279'** | **30# Purgel III LT 70Q CO2 foam frac: 110 tons of CO2, 58,000# 20/40 White Sand, 207 bbls** |
| **8620' - 8699'** | **30# Purgel III LT 70Q CO2 foam frac: 141 tons of CO2, 102,000# 20/40 White Sand, 321 bbls** |
| **8460' - 8572'** | **30# Purgel III LT 70Q CO2 foam frac: 105 tons of CO2, 45,600# 20/40 White Sand, 260 bbls** |
| **8327' - 8379'** | **30# Purgel III LT 70Q CO2 foam frac: 70 tons of CO2, 27,000# 20/40 White Sand, 223 bbls** |

28. Production - Interval A

| Date First Produced | Test Date | Hours Tested | Test Production | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| **11/05/2004** | **11/21/2004** | **24** | → | **0** | **280** | **63** | | | **Flowing** |
| **Choke Size** | **Tbg. Press. Flwg. SI** | **Csg. Press.** | **24 Hr. Rate** | **Oil BBL** | **Gas MCF** | **Water BBL** | **Gas/Oil Ratio** | **Well Status** | |
| **32/64** | **75** | **350** | → | **0** | **280** | **63** | | **Open** | |

28a. Production - Interval B

| Date First Produced | Test Date | Hours Tested | Test Production | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| | | | → | | | | | | |
| **Choke Size** | **Tbg. Press. Flwg. SI** | **Csg. Press.** | **24 Hr. Rate** | **Oil BBL** | **Gas MCF** | **Water BBL** | **Gas/Oil Ratio** | **Well Status** | |
| | | | → | | | | | | |

*(See instructions and spaces for additional data on page 2)*

28b. Production - Interval C

| Date First Produced | Test Date | Hours Tested | Test Production → | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | |

| Choke Size | Tbg. Press. Flwg. SI | Csg. Press. | 24 Hr. Rate → | Oil BBL | Gas MCF | Water BBL | Gas/Oil Ratio | Well Status |
|---|---|---|---|---|---|---|---|---|
| | | | | | | | | |

28c. Production - Interval D

| Date First Produced | Test Date | Hours Tested | Test Production → | Oil BBL | Gas MCF | Water BBL | Oil Gravity Corr. API | Gas Gravity | Production Method |
|---|---|---|---|---|---|---|---|---|---|
| | | | | | | | | | |

| Choke Size | Tbg. Press. Flwg. SI | Csg. Press. | 24 Hr. Rate → | Oil BBL | Gas MCF | Water BBL | Gas/Oil Ratio | Well Status |
|---|---|---|---|---|---|---|---|---|
| | | | | | | | | |

29. Disposition of Gas *(Sold, used for fuel, vented, etc.)*

**Sold**

30. Summary of Porous Zones (Include Aquifers):

Show all important zones of porosity and contents thereof: Cored intervals and all drill-stem tests, including depth interval tested, cushion used, time tool open, flowing and shut-in pressures and recoveries.

31. Formation (Log) Markers

| Formation | Top | Bottom | Descriptions, Contents, etc. | Name | Top Meas. Depth |
|---|---|---|---|---|---|
| | | | | **Green River (marker)** | **2102'** |
| | | | | **Base Resisti** | **2409'** |
| | | | | **Uteland Butte** | **2838'** |
| | | | | **Wasatch** | **3060'** |
| | | | | **Middle Wasatch** | **4088'** |
| | | | | **North Horn** | **5168'** |
| | | | | **Price River** | **6984'** |
| | | | | **Base UPR** | **7268'** |
| | | | | **Bluecastle** | **8288'** |
| | | | | **Sego** | **8582'** |
| | | | | **Castlegate** | **8972'** |
| | | | | **Blackhawk** | **9211'** |

32. Additional remarks (include plugging procedure):

**Copies of logs already submitted. CIBP set at 7655'. This well has been converted to a salt-water disposal well.**

33. Indicate which itmes have been attached by placing a check in the appropriate boxes:

☐ Electrical/Mechanical Logs (1 full set req'd.) ☐ Geologic Report ☐ DST Report ☐ Directional Survey
☐ Sundry Notice for plugging and cement verification ☐ Core Analysis ☐ Other:

34. I hereby certify that the foregoing and attached information is complete and correct as determined from all available records (see attached instructions)*

Name *(please print)* **Tracey Fallang** Title **Regulatory Analyst**

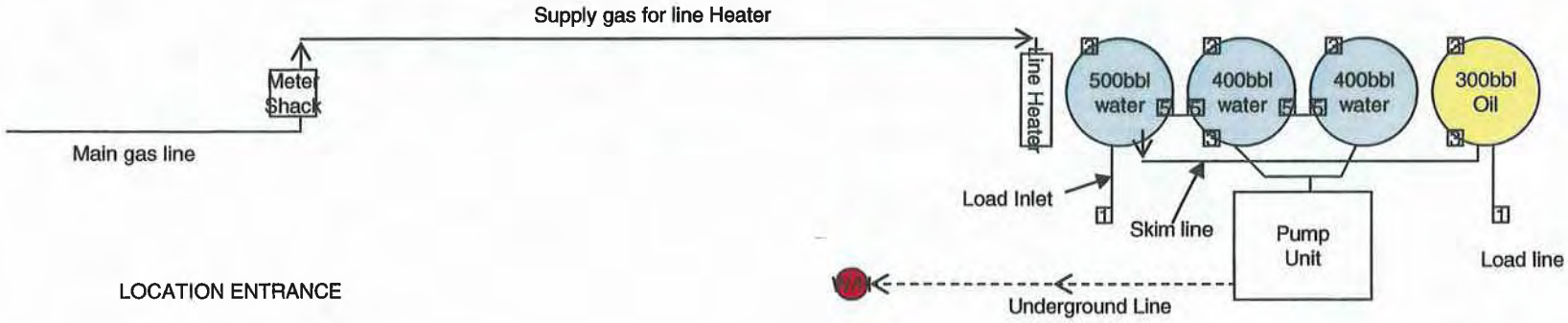
Signature **Tracey Fallang** Digitally signed by Tracey Fallang DN: CN = Tracey Fallang, C = UR, O = BBC Date: 2008.12.01 14:01:26 -07'00' Date **11/03/2008** Revised

Title 18 U.S.C Section 1001 and Title 43 U.S.C Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

BBC
CONFIDENTIAL

| 27. PERFORATION RECORD (cont.) | | | | |
|---|---|---|---|---|
| INTERVAL (Top/Bot-MD) | | SIZE | NO. HOLES | PERFORATION STATUS |
| 7620' | 7630' | 0.41" | 30 | Open |
| 7258' | 7266' | 0.41" | 24 | Open |
| 6908' | 6916' | 0.41" | 32 | Open (perf only, no frac) |
| 6791' | 6799' | 0.41" | 24 | Open |
| 6295' | 6300' | 0.41" | 15 | Open (perf only, no frac) |
| 4500' | 4518' | 0.43" | 108 | Open |
| 4260' | 4290' | 0.43" | 180 | Open |
| 3946' | 4068' | 0.43" | 408 | Open |
| 3838' | 3890' | 0.43" | 210 | Open |
| 3750' | 3804' | 0.43" | 114 | Open |
| 3482' | 3620' | 0.43" | 216 | Open |

| 28. ACID, FRACTURE, TREATMENT, CEMENT SQUEEZE, ETC. (cont.) | |
|---|---|
| DEPTH INTERVAL | AMOUNT AND TYPE OF MATERIAL |
| 7620' – 7630' | 30# Purgel III LT 70Q CO2 foam frac: 138 tons of CO2, 80,000# 20/40 White Sand, 264 bbls |
| 7258' – 7266' | 30# Purgel III LT 70Q CO2 foam frac: 75 tons of CO2, 22,000# 20/40 White Sand, 176 bbls |
| 6791' – 6799' | 30# Purgel III LT 70Q CO2 foam frac: 122 tons of CO2, 78,000# 20/40 White Sand, 271 bbls |
| 4500' – 4518' | 700 bbls Dyna Flow-1; 18,000# 20/40 White Sand |
| 4260' – 4290' | 621 bbls Dyna Flow-1; 30,000# 20/40 White Sand |
| 3946' – 4068' | 1268 bbls Dyna Flow-1; 68,000# 20/40 White Sand |
| 3838' – 3890' | 615 bbls Dyna Flow-1; 35,279# 20/40 White Sand |
| 3750' – 3804' | 397 bbls Dyna Flow-1; 18,381# 20/40 White Sand |
| 3482' – 3620' | 899 bbls Dyna Flow-1; 54,000# 20/40 White Sand |




Irrigation Ditch/Pond/Stream/
Dry Drainage/Other
43' -feet away (direction indicated w/arrows)

# 12-24 Injection Well

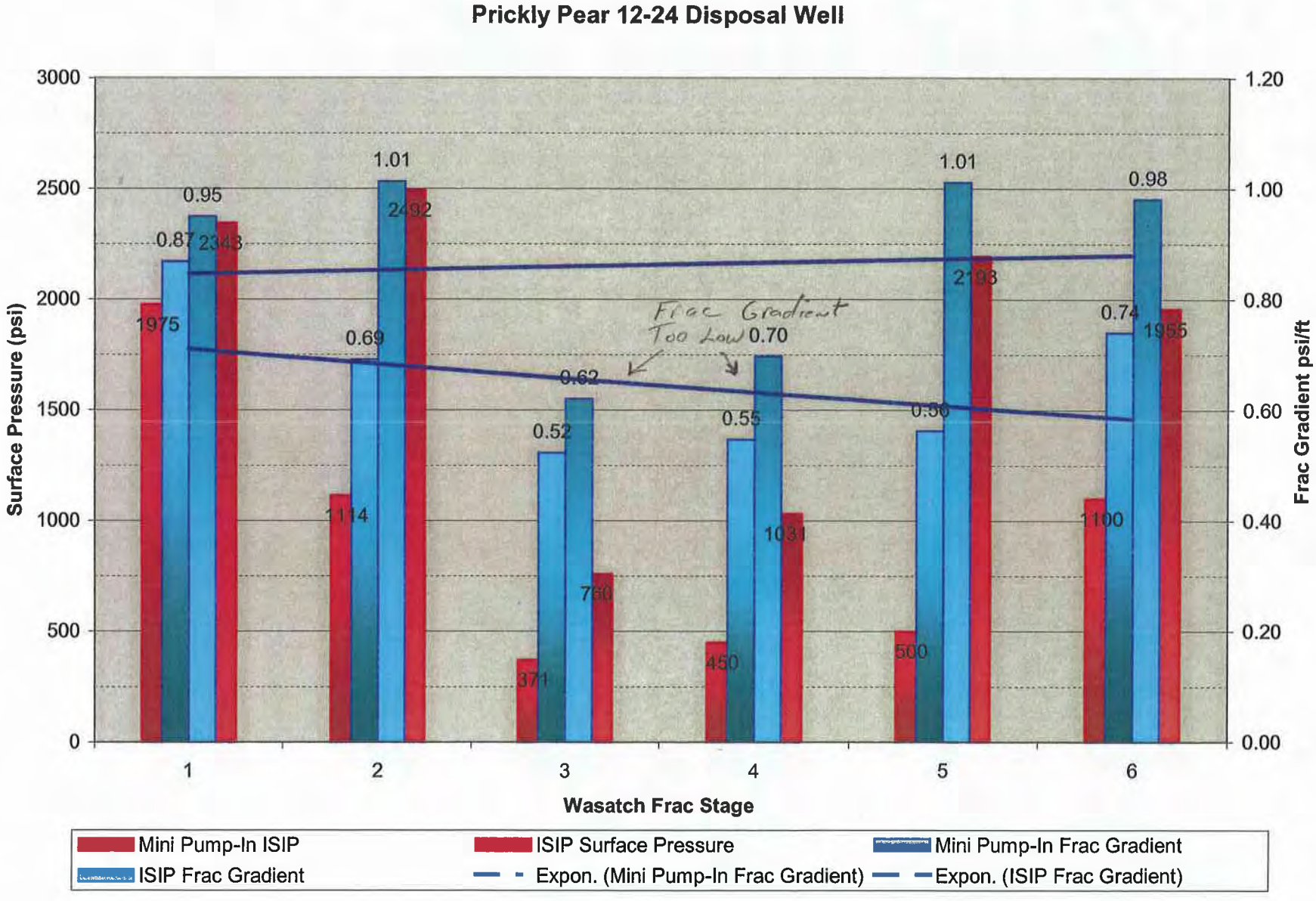
1 - LOAD LINE
3 - DRAIN
5 - LOWER EQUALIZER

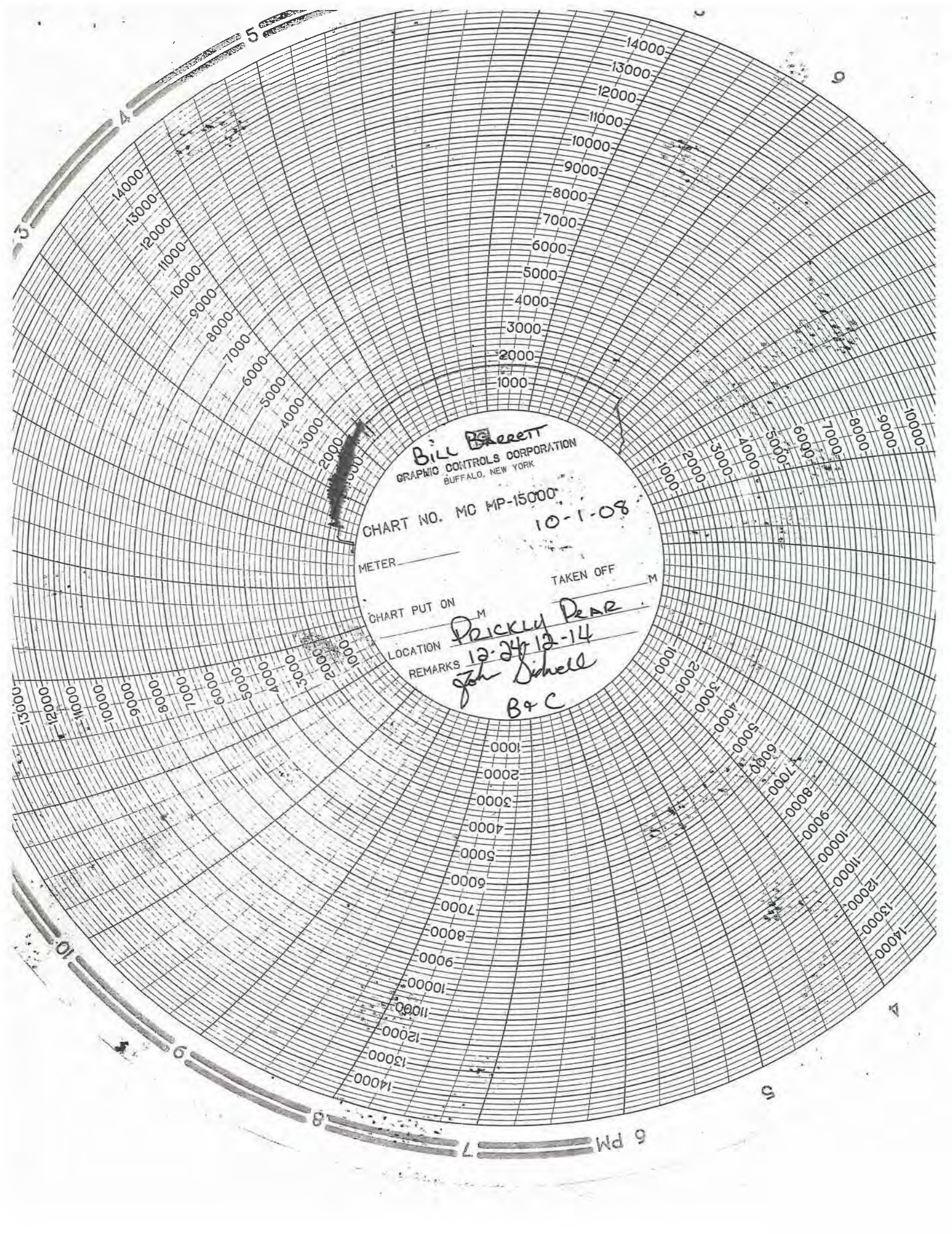
Tank Containment Volume: ___ bbls

NOTE:
THIS LEASE IS SUBJECT TO THE SITE SECURITY PLAN FOR WEST TAVAPUTS. THIS PLAN WILL BE LOCATED AT 1820 WEST HWY 40, ROOSEVELT, UT.

N

**BILL BARRETT CORPORATION**
**PRICKLY PEAR UNIT FED #12-24**
SHL:SW/4SW/4,SEC.24-T12S-R14E
BHL:SW/4SW/4,SEC.24-T12S-R14E
CARBON COUNTY, UTAH
LEASE# UTU-077513
UNIT# UTU-79487
API# 43-007-30953-00-00


Prickly Pear 12-24 Disposal Well
Surface Pressure (psi)
Frac Gradient psi/ft
Wasatch Frac Stage
Frac Gradient Too Low
3000
2500
2000
1500
1000
500
0
1.20
1.00
0.80
0.60
0.40
0.20
0.00
1
2
3
4
5
6
1975
0.87
0.95
2348
1114
0.69
1.01
2492
371
0.52
0.62
760
450
0.55
0.70
1031
500
0.56
1.01
2198
1100
0.74
0.98
1955
Mini Pump-In ISIP
ISIP Surface Pressure
Mini Pump-In Frac Gradient
ISIP Frac Gradient
Expon. (Mini Pump-In Frac Gradient)
Expon. (ISIP Frac Gradient)


BILL BARRETT
GRAPHIC CONTROLS CORPORATION
BUFFALO, NEW YORK
CHART NO. MC MP-15000
10-1-08
METER
TAKEN OFF
M
CHART PUT ON
M
LOCATION Prickly Pear
REMARKS 12-24 12-14
John Sidwell
B&C
6 PM

CALFRAC WELL SERVICES

# Treatment Summary

## General Info



| | | | |
|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 1), SWSW S24, T12S, R15E | Service Line: | Frac |
| Customer: | John Shepard, P.E. | Job Date: | 09/18/08 |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0188RN |
| | Denver, CO 80202 | Service Order #: | 77813 |

Time Requested: 9:00 AM
Time On: 9:00 AM
Time Off: 4:00 PM

## Wellbore Data

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 4500 | 104.6 |
| Annulus: | | | | | | | |
| | | | | | | Total | 104.6 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

## Perforations

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 4500 | 4518 | 6 |

Formation Treated
Middle Wasatch, (WIW)

## Proppant Data

| | 1 | 2 | 3 | 4 | |
|---|---|---|---|---|---|
| Proppant Type | 20/40 Sand | | | | |
| Total sand on location | 225,660 | | | | lb |
| Sand pumped | 18,000 | | | | lb |
| Sand in Formation | 18,000 | | | | lb |
| Final Conc @ Perfs | 0 | | | | lb/gal |

## Pump Power

| | | |
|---|---|---|
| Available | 8000 | hhp |
| Used | 1778 | hhp |

## Fluid in Tanks

| | | |
|---|---|---|
| Pre-Job | 2446 | bbl |
| Post-Job | 1749 | bbl |

## Flush Fluid Density

8.34 (lb/gal)

## Treatment Data

| | | | |
|---|---|---|---|
| Max.Treating Rate | | 30.2 | bbl/min |
| Max.Treating Pressure | | 3176 | psi |
| Pressure Test Lines | | 7500 | psi |
| Annular Relief Set | N/A | | psi |
| Annulus Pressure | N/A | | psi |
| Initial Well Press | 0 | | psi |
| Breakdown Press | | 3125 | psi |
| Average Pressure | | 2411 | psi |
| Average Fluid Rate | | 30.1 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 1975 | | | 2343 | psi |
| 1 Min. SIP | | | | 2054 | psi |
| 5 Min. SIP | | | | 1868 | psi |
| 10 Min. SIP | | | | 1787 | psi |
| 15 Min. SIP | | | | 1761 | psi |
| Frac Grad.: | 0.87 | 0.43 | 0.43 | 0.95 | psi/ft |

## Fluid Summary

| | | |
|---|---|---|
| Hole Fill Fluid Vol. | 3.1 | bbl |
| | | bbl |
| | | bbl |
| | | bbl |
| Pad Fluid Vol. | 388.7 | bbl |
| Proppant Fluid Vol. | 206.5 | bbl |
| Flush Fluid Vol. | 104.6 | bbl |
| Total Fluid Pumped | 699.8 | bbl |

## Chemical Data

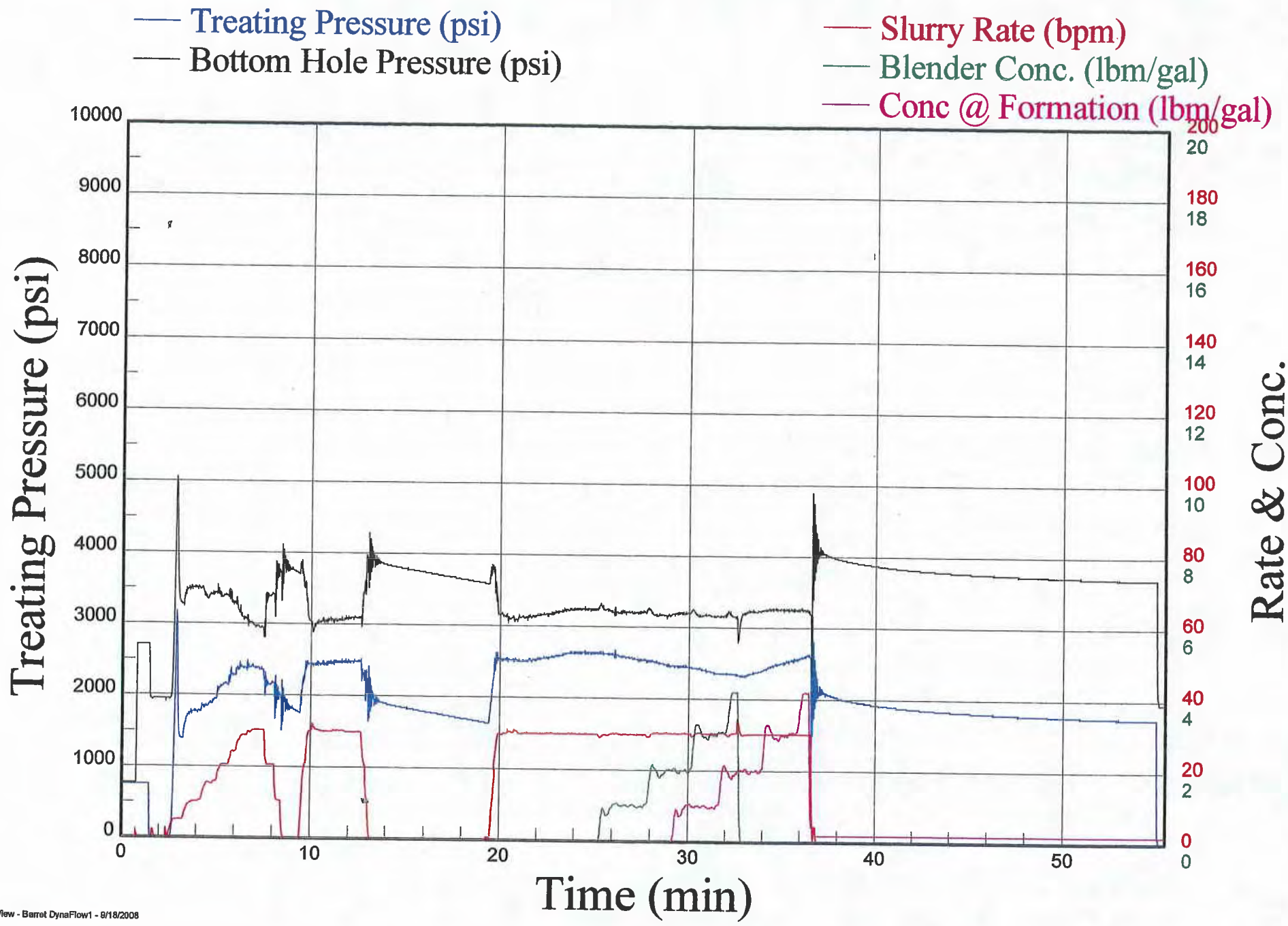
| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 211 | 12 | 223 |
| DWP-202 | 40 | 10 | 50 |
| DWP-206 | 192 | 12 | 204 |
| DWP-988 | 47 | 0 | 47 |

**Remarks:** Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ

Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #1



# Treatment Summary

## General Info



| | | | |
|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 2), SWSW S24, T12S, R15E | Service Line: | Frac |
| Customer: | John Shepard, P.E. | Job Date: | 09/18/08 |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0189RN |
| | Denver, CO 80202 | Service Order #: | 77814 |

Time Requested: 4:00 PM
Time On: 4:00 PM
Time Off: 7:30 PM

## Wellbore Data

| Type | Wellbore Configuration Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 4260 | 99.0 |
| Annulus: | | | | | | | |
| | | | | | | Total | 99.0 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

## Perforations

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 4260 | 4290 | 6 |

Formation Treated
Middle Wasatch, (WIW)

## Proppant Data

| | | | | | | |
|---|---|---|---|---|---|---|
| Proppant Type | 1 | 20/40 Sand | | | | |
| | 2 | | | | | |
| | 3 | | | | | |
| | 4 | | | | | |
| Total sand on location | | 202,660 | | | | lb |
| Sand pumped | | 30,000 | | | | lb |
| Sand in Formation | | 30,000 | | | | lb |
| Final Conc @ Perfs | | 0 | | | | lb/gal |

## Pump Power

| | | |
|---|---|---|
| Available | 8000 | hhp |
| Used | 1752 | hhp |

## Fluid in Tanks

| | | |
|---|---|---|
| Pre-Job | 1749 | bbl |
| Post-Job | 1374 | bbl |

## Flush Fluid Density

8.34 (lb/gal)

## Treatment Data

| | | | |
|---|---|---|---|
| Max.Treating Rate | | 30.2 | bbl/min |
| Max.Treating Pressure | | 3356 | psi |
| Pressure Test Lines | | 7500 | psi |
| Annular Relief Set | N/A | | psi |
| Annulus Pressure | N/A | | psi |
| Initial Well Press | | 1116 | psi |
| Breakdown Press | | 4062 | psi |
| Average Pressure | | 2379 | psi |
| Average Fluid Rate | | 30.1 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 1114 | | | 2492 | psi |
| 1 Min. SIP | | | | 2257 | psi |
| 5 Min. SIP | | | | 1625 | psi |
| 10 Min. SIP | | | | 1078 | psi |
| 15 Min. SIP | | | | 814 | psi |
| Frac Grad.: | 0.70 | 0.43 | 0.43 | 1.02 | psi/ft |

## Fluid Summary

| | | |
|---|---|---|
| Pad Fluid Vol. | 220.6 | bbl |
| Proppant Fluid Vol. | 301.5 | bbl |
| Flush Fluid Vol. | 99.0 | bbl |
| Total Fluid Pumped | 621.1 | bbl |

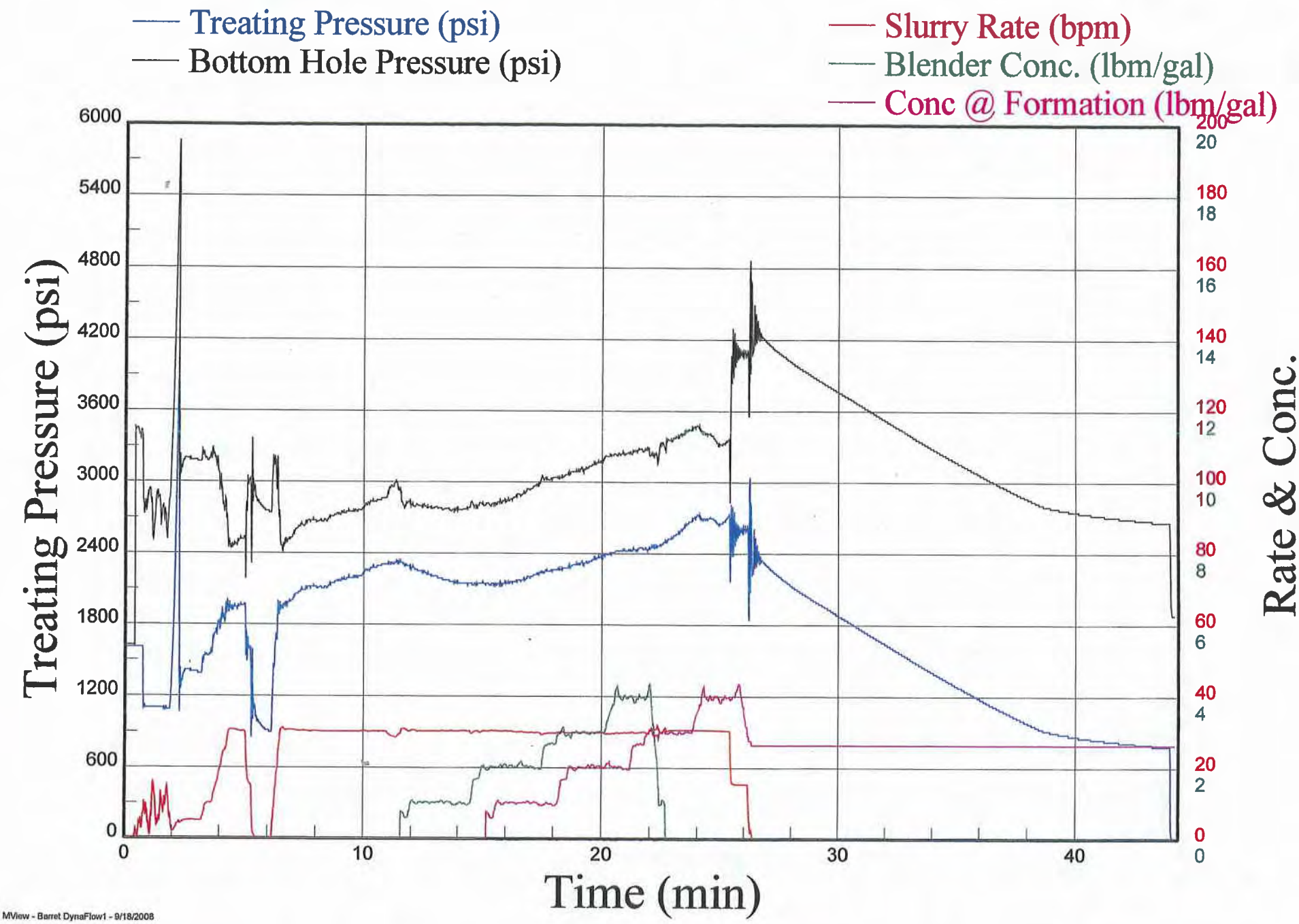
## Chemical Data

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 87 | 0 | 87 |
| DWP-202 | 37 | 0 | 37 |
| DWP-206 | 82 | 0 | 82 |
| DWP-988 | 50 | 0 | 50 |

Remarks: Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #2




MView - Barret DynaFlow1 - 9/18/2008

CALFRAC WELL SERVICES

# Treatment Summary

## General Info



Loc'n: Prickly Pear 12-24 (Stage 3), SWSW S24, T12S, R15E
Customer: John Shepard, P.E.
Bill Barrett Corporation
1099 18th StreetSuite 2300
Denver, CO 80202

Service Line: Frac
Job Date: 09/19/08
Job Type: DynaFlow-1
Program Number: FAYH0190RN
Service Order #: 77815

Time Requested: 6:30 AM
Time On: 6:30 AM
Time Off: 10:00 AM

## Wellbore Data

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 3946 | 91.7 |
| Annulus: | | | | | | | |
| | | | | | | Total | 91.7 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

## Perforations

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 3946 | 3964 | 6 |
| 3976 | 3996 | 6 |
| 4018 | 4028 | 6 |
| 4038 | 4048 | 6 |
| 4058 | 4068 | 6 |

Formation Treated: Middle Wasatch, (WIW)

## Proppant Data

| | | 1 | 2 | 3 | 4 | |
|---|---|---|---|---|---|---|
| Proppant Type | | 20/40 Sand | | | | |
| Total sand on location | 174,520 | | | | | lb |
| Sand pumped | 68,000 | | | | | lb |
| Sand in Formation | 68,000 | | | | | lb |
| Final Conc @ Perfs | 0 | | | | | lb/gal |

## Pump Power

| | | |
|---|---|---|
| Available | 8000 | hhp |
| Used | 797 | hhp |

## Fluid in Tanks

| | | |
|---|---|---|
| Pre-Job | 2410 | bbl |
| Post-Job | 1314 | bbl |

## Flush Fluid Density

8.34 (lb/gal)

## Treatment Data

| | | | |
|---|---|---|---|
| Max.Treating Rate | | 41 | bbl/min |
| Max.Treating Pressure | | 1494 | psi |
| Pressure Test Lines | | 75000 | psi |
| Annular Relief Set | N/A | | psi |
| Annulus Pressure | N/A | | psi |
| Initial Well Press | 0 | | psi |
| Breakdown Press | | 1964 | psi |
| Average Pressure | | 921 | psi |
| Average Fluid Rate | | 35.3 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 371 | | | 760 | psi |
| 1 Min. SIP | 0 | | | 624 | psi |
| 5 Min. SIP | | | | 308 | psi |
| 10 Min. SIP | | | | 56 | psi |
| 15 Min. SIP | | | | | psi |
| Frac Grad.: | 0.53 | 0.43 | 0.43 | 0.63 | psi/ft |

## Fluid Summary

| | | |
|---|---|---|
| Hole Fill Fluid Vol. | HF | bbl |
| | | bbl |
| | | bbl |
| | | bbl |
| Pad Fluid Vol. | 540.2 | bbl |
| Proppant Fluid Vol. | 631.6 | bbl |
| Flush Fluid Vol. | 96.0 | bbl |
| Total Fluid Pumped | 1267.8 | bbl |

Ball Sealers: Size 7/8" # 73 Weight 1.3

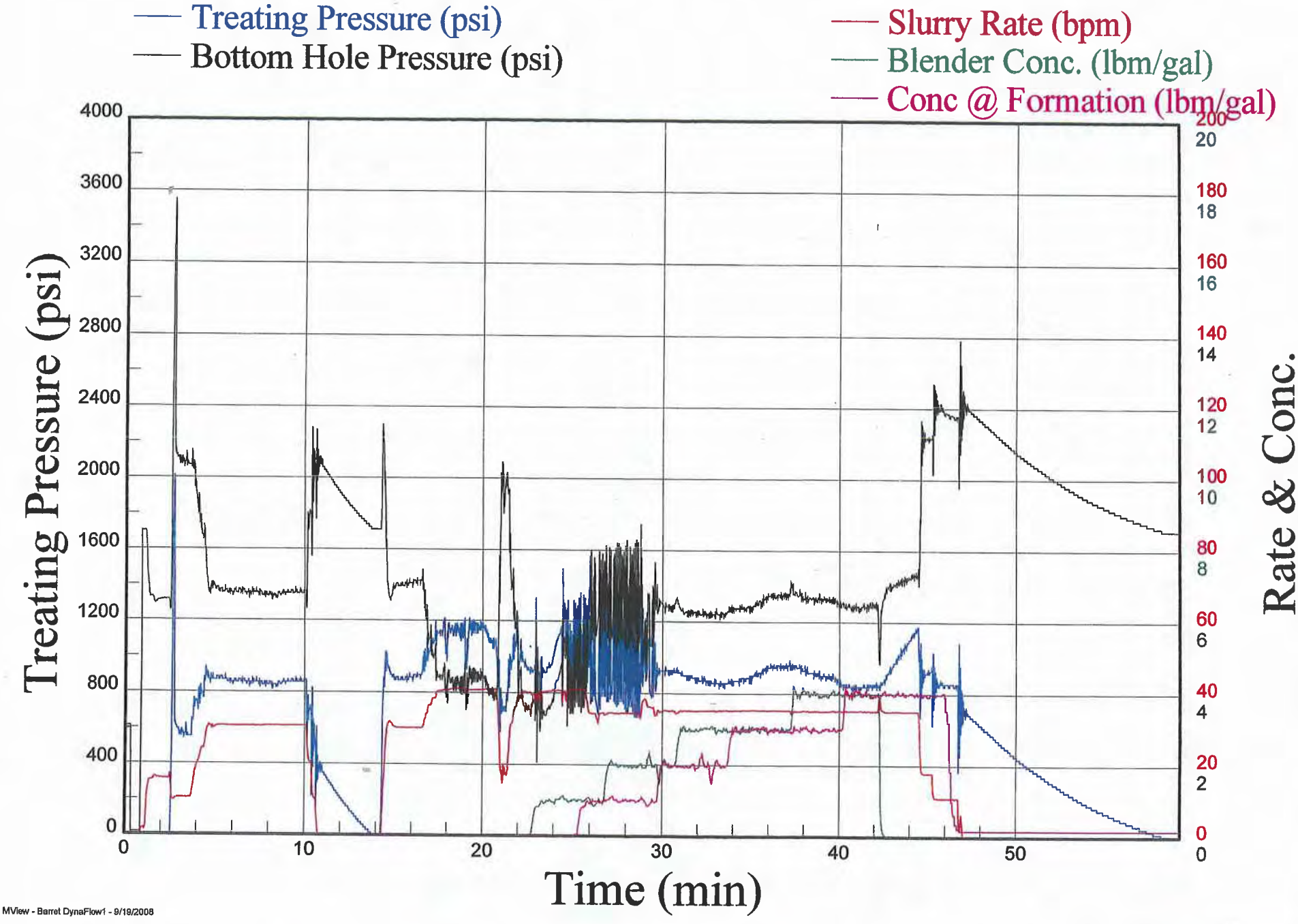
## Chemical Data

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 285 | 7 | 292 |
| DWP-202 | 83 | 4 | 87 |
| DWP-206 | 270 | 10 | 280 |
| DWP-988 | 70 | 0 | 70 |

Remarks: Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #3




MView - Barret DynaFlow1 - 9/19/2008

CALFRAC WELL SERVICES

# Treatment Summary

**General Info** — Page 1 of 2 — 240

| | | | |
|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 4), SWSW S24, T12S, R15E | Service Line: | Frac |
| Customer: | John Shepard, P.E. | Job Date: | 09/19/08 |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0191RN |
| | Denver, CO 80202 | Service Order #: | 77816 |

Time Requested: 10:00 AM
Time On: 10:00 AM
Time Off: 12:30 PM

**Wellbore Data**

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 3838 | 89.2 |
| Annulus: | | | | | | | |
| | | | | | | Total | 89.2 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

**Perforations**

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 3838 | 3858 | 6 |
| 3875 | 3890 | 6 |

Formation Treated: Middle Wasatch, (WIW)

**Proppant Data**

| | | 1 | 2 | 3 | 4 | |
|---|---|---|---|---|---|---|
| Proppant Type | | 20/40 Sand | | | | |
| Total sand on location | | 109,040 | | | | lb |
| Sand pumped | | 35,279 | | | | lb |
| Sand in Formation | | 35,279 | | | | lb |
| Final Conc @ Perfs | | 0 | | | | lb/gal |

**Pump Power**

| | | |
|---|---|---|
| Available | 8000 | hhp |
| Used | 1382 | hhp |

**Fluid in Tanks**

| | | |
|---|---|---|
| Pre-Job | 2068 | bbl |
| Post-Job | 1669 | bbl |

**Flush Fluid Density**: 8.34 (lb/gal)

**Treatment Data**

| | | | |
|---|---|---|---|
| Max.Treating Rate | | 40.2 | bbl/min |
| Max.Treating Pressure | | 2994 | psi |
| Pressure Test Lines | | 7500 | psi |
| Annular Relief Set | N/A | | psi |
| Annulus Pressure | N/A | | psi |
| Initial Well Press | 0 | | psi |
| Breakdown Press | | 2924 | psi |
| Average Pressure | | 1469 | psi |
| Average Fluid Rate | | 38.4 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 450 | | | 1031 | psi |
| 1 Min. SIP | | | | 578 | psi |
| 5 Min. SIP | | | | 0 | psi |
| 10 Min. SIP | | | | | psi |
| 15 Min. SIP | | | | | psi |
| Frac Grad.: | 0.55 | 0.43 | 0.43 | 0.70 | psi/ft |

**Fluid Summary**

| | HF | bbl |
|---|---|---|
| Hole Fill Fluid Vol. | | bbl |
| | | bbl |
| | | bbl |
| | | bbl |
| Pad Fluid Vol. | 190.8 | bbl |
| Proppant Fluid Vol. | 328.9 | bbl |
| Flush Fluid Vol. | 95.2 | bbl |
| Total Fluid Pumped | 614.9 | bbl |

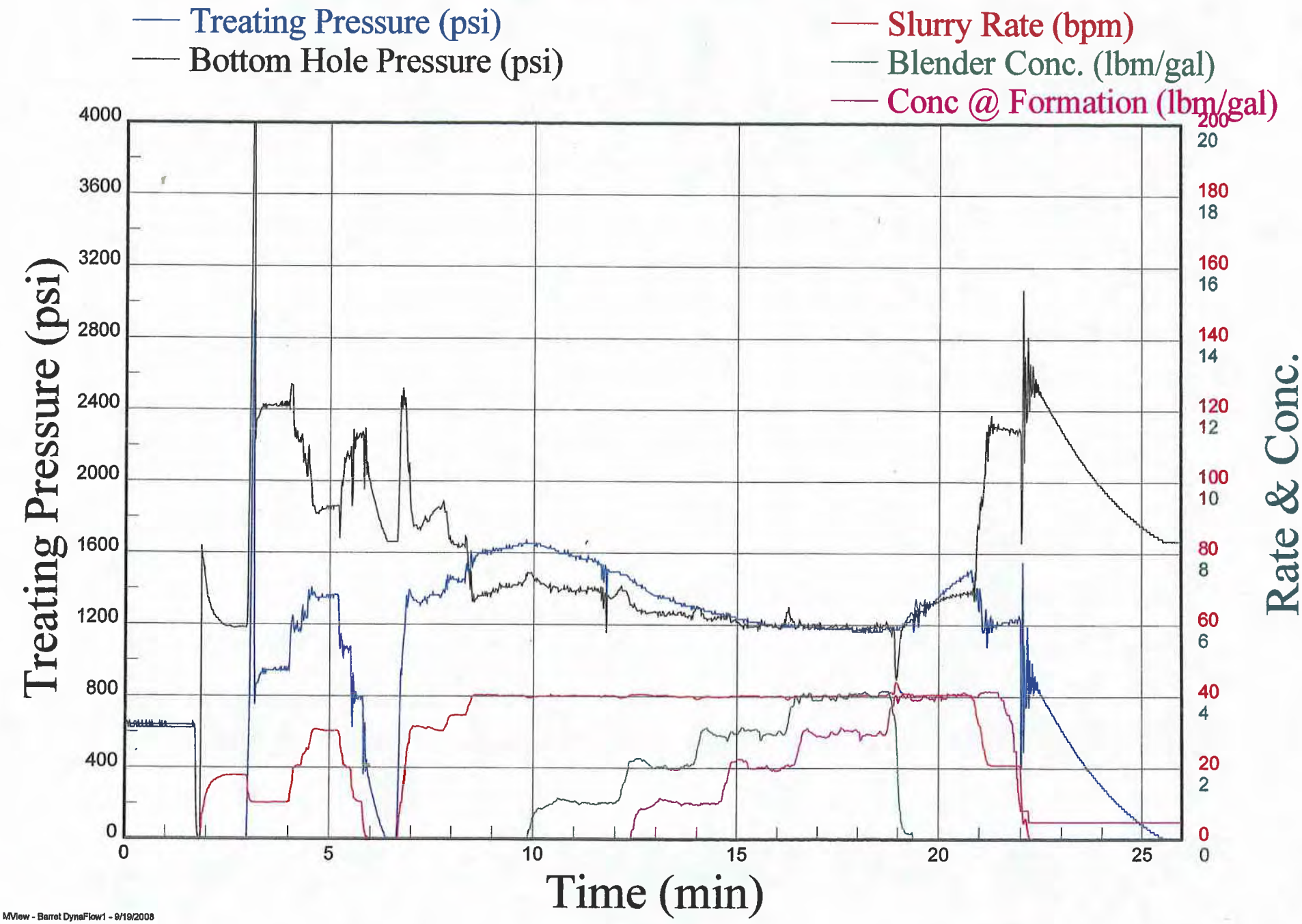
**Chemical Data**

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 124 | 0 | 124 |
| DWP-202 | 38 | 0 | 38 |
| DWP-206 | 114 | 0 | 114 |
| DWP-988 | 50 | 0 | 50 |

**Remarks:** Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ — Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #4




MView - Barret DynaFlow1 - 9/19/2008

CALFRAC WELL SERVICES

# Treatment Summary

## General Info



| | | | |
|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 5), SWSW S24, T12S, R15E | Service Line: | Frac |
| Customer: | John Shepard, P.E. | Job Date: | 09/19/08 |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0192RN |
| | Denver, CO 80202 | Service Order #: | 77817 |

Time Requested: 12:30 PM
Time On: 12:30 PM
Time Off: 2:30 PM

## Wellbore Data

| Type | Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 3750 | 87.2 |
| Annulus: | | | | | | | |
| | | | | | | Total | 87.2 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

## Perforations

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 3750 | 3755 | 6 |
| 3768 | 3776 | 6 |
| 3798 | 3804 | 6 |

Formation Treated
Middle Wasatch, (WIW)

## Proppant Data

| | 1 | 2 | 3 | 4 | |
|---|---|---|---|---|---|
| Proppant Type | 20/40 Sand | | | | |
| Total sand on location | 73,000 | | | | lb |
| Sand pumped | 18,381 | | | | lb |
| Sand in Formation | 18,381 | | | | lb |
| Final Conc @ Perfs | 0 | | | | lb/gal |

## Pump Power

| | | |
|---|---|---|
| Available | 8000 | hhp |
| Used | 1027 | hhp |

## Fluid In Tanks

| | | |
|---|---|---|
| Pre-Job | 1947 | bbl |
| Post-Job | 1560 | bbl |

## Flush Fluid Density

8.34 (lb/gal)

## Treatment Data

| | | | |
|---|---|---|---|
| Max.Treating Rate | | 30.2 | bbl/min |
| Max.Treating Pressure | | 2727 | psi |
| Pressure Test Lines | | 7500 | psi |
| Annular Relief Set | N/A | | psi |
| Annulus Pressure | N/A | | psi |
| Initial Well Press | 0 | | psi |
| Breakdown Press | | 2116 | psi |
| Average Pressure | | 1393 | psi |
| Average Fluid Rate | | 30.1 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 500 | | | 2193 | psi |
| 1 Min. SIP | | | | 1819 | psi |
| 5 Min. SIP | | | | 1100 | psi |
| 10 Min. SIP | | | | 281 | psi |
| 15 Min. SIP | | | | 0 | psi |
| Frac Grad.: | 0.57 | 0.43 | 0.43 | 1.02 | psi/ft |

## Fluid Summary

| | | |
|---|---|---|
| Hole Fill Fluid Vol. | HF | bbl |
| Pad Fluid Vol. | 129.7 | bbl |
| Proppant Fluid Vol. | 171.5 | bbl |
| Flush Fluid Vol. | 96.0 | bbl |
| Total Fluid Pumped | 397.2 | bbl |

## Chemical Data

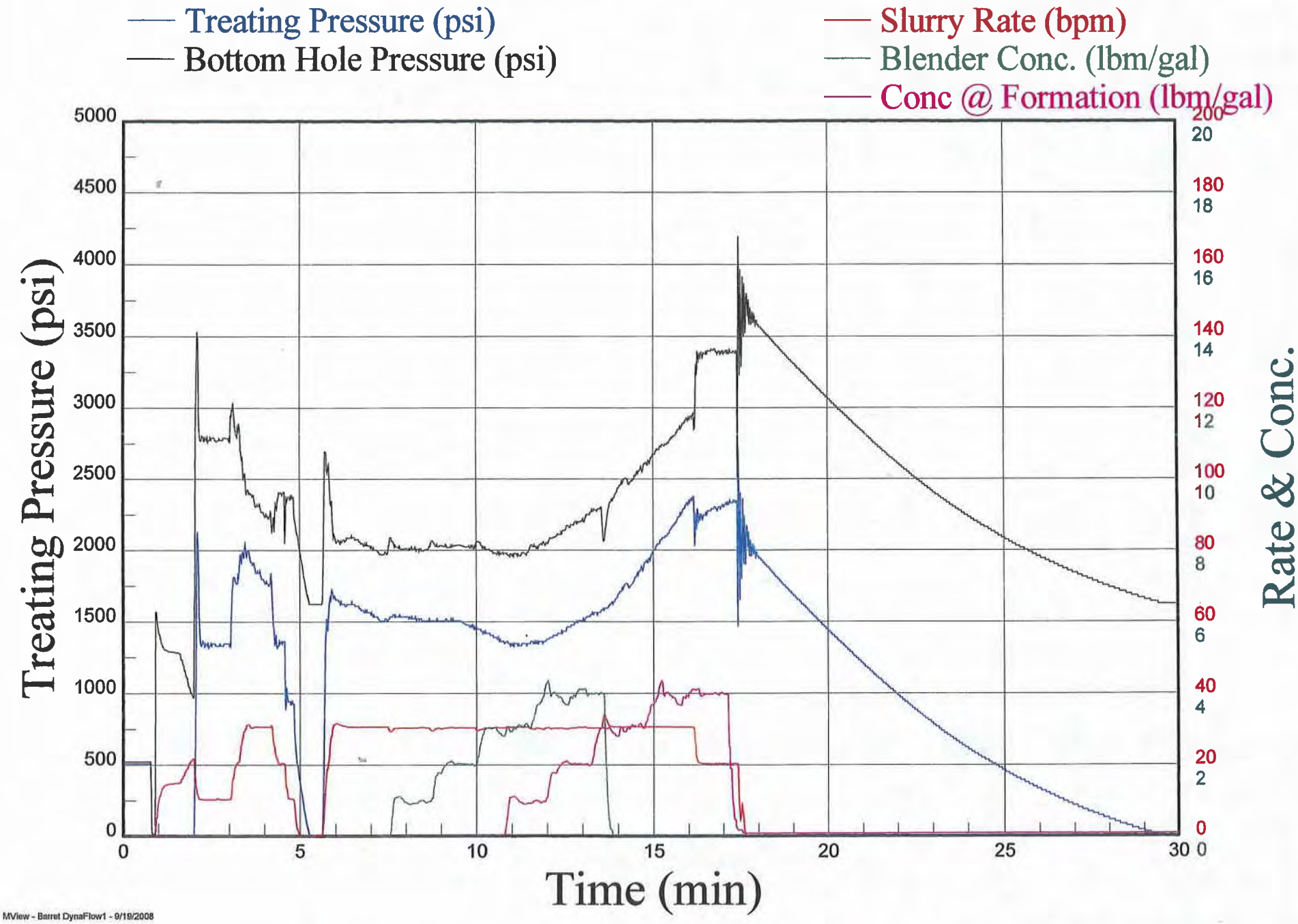
| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 73 | 0 | 73 |
| DWP-202 | 18 | 0 | 18 |
| DWP-206 | 73 | 0 | 73 |
| DWP-988 | 30 | 0 | 30 |

**Remarks:** Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ

Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #5



CALFRAC WELL SERVICES

# Treatment Summary

## General Info



| | | | |
|---|---|---|---|
| Loc'n | Prickly Pear 12-24 (Stage 6), SWSW S24, T12S, R15E | Service Line: | Frac |
| Customer: | John Shepard, P.E. | Job Date: | 09/19/08 |
| | Bill Barrett Corporation | Job Type: | DynaFlow-1 |
| | 1099 18th StreetSuite 2300 | Program Number: | FAYH0193RN |
| | Denver, CO 80202 | Service Order #: | 77818 |

Time Requested: 2:30 PM
Time On: 2:30 PM
Time Off: 7:00 PM

## Wellbore Data

| Type | Wellbore Configuration Size | Weight | Grade | Capacity (bbl/ft) | Max Pres (psi) | Depth (ft) | Volume (bbl) |
|---|---|---|---|---|---|---|---|
| Tubing: | | | | | | | |
| Casing: | 5.5 | 17 | N-80 | 0.02324 | 7740 | 3482 | 80.9 |
| Annulus: | | | | | | | |
| | | | | | | Total | 80.9 |

Packer (ft): PBTD (ft): Treating Mode: Down Casing

## Perforations

| Top (ft) | Bttm. (ft) | Shots / ft |
|---|---|---|
| 3482 | 3486 | 6 |
| 3492 | 3496 | 6 |
| 3501 | 3505 | 6 |
| 3544 | 3548 | 6 |
| 3554 | 3558 | 6 |
| 3586 | 3590 | 6 |
| 3596 | 3600 | 6 |
| 3606 | 3610 | 6 |
| 3616 | 3620 | 6 |

Formation Treated
Middle Wasatch, (WIW)

## Proppant Data

| | | | |
|---|---|---|---|
| Proppant Type | 1 20/40 Sand | | |
| | 2 | | |
| | 3 | | |
| | 4 | | |
| Total sand on location | 54,000 | | lb |
| Sand pumped | 54,000 | | lb |
| Sand in Formation | 54,000 | | lb |
| Final Conc @ Perfs | 0 | | lb/gal |

## Pump Power

| | | |
|---|---|---|
| Available | 8000 | hhp |
| Used | 1351 | hhp |

## Fluid in Tanks

| | | |
|---|---|---|
| Pre-Job | 1560 | bbl |
| Post-Job | 921 | bbl |

## Flush Fluid Density

8.34 (lb/gal)

## Treatment Data

| | | | |
|---|---|---|---|
| Max.Treating Rate | | 30.1 | bbl/min |
| Max.Treating Pressure | | 2611 | psi |
| Pressure Test Lines | | 7500 | psi |
| Annular Relief Set | N/A | | psi |
| Annulus Pressure | N/A | | psi |
| Initial Well Press | 0 | | psi |
| Breakdown Press | | 2611 | psi |
| Average Pressure | | 1837 | psi |
| Average Fluid Rate | | 30.0 | bbl/min |

| | MiniFrac | Minifrac 2 | Minifrac 3 | Treatment | |
|---|---|---|---|---|---|
| ISIP Pres. | 1100 | | | 1955 | psi |
| 1 Min. SIP | | | | 1786 | psi |
| 5 Min. SIP | | | | 1564 | psi |
| 10 Min. SIP | | | | 1258 | psi |
| 15 Min. SIP | | | | 969 | psi |
| Frac Grad.: | 0.75 | 0.43 | 0.43 | 0.99 | psi/ft |

## Fluid Summary

| | | |
|---|---|---|
| Hole Fill Fluid Vol. | HF | bbl |
| Pad Fluid Vol. | 262.9 | bbl |
| Proppant Fluid Vol. | 546.5 | bbl |
| Flush Fluid Vol. | 89.2 | bbl |
| Total Fluid Pumped | 898.6 | bbl |

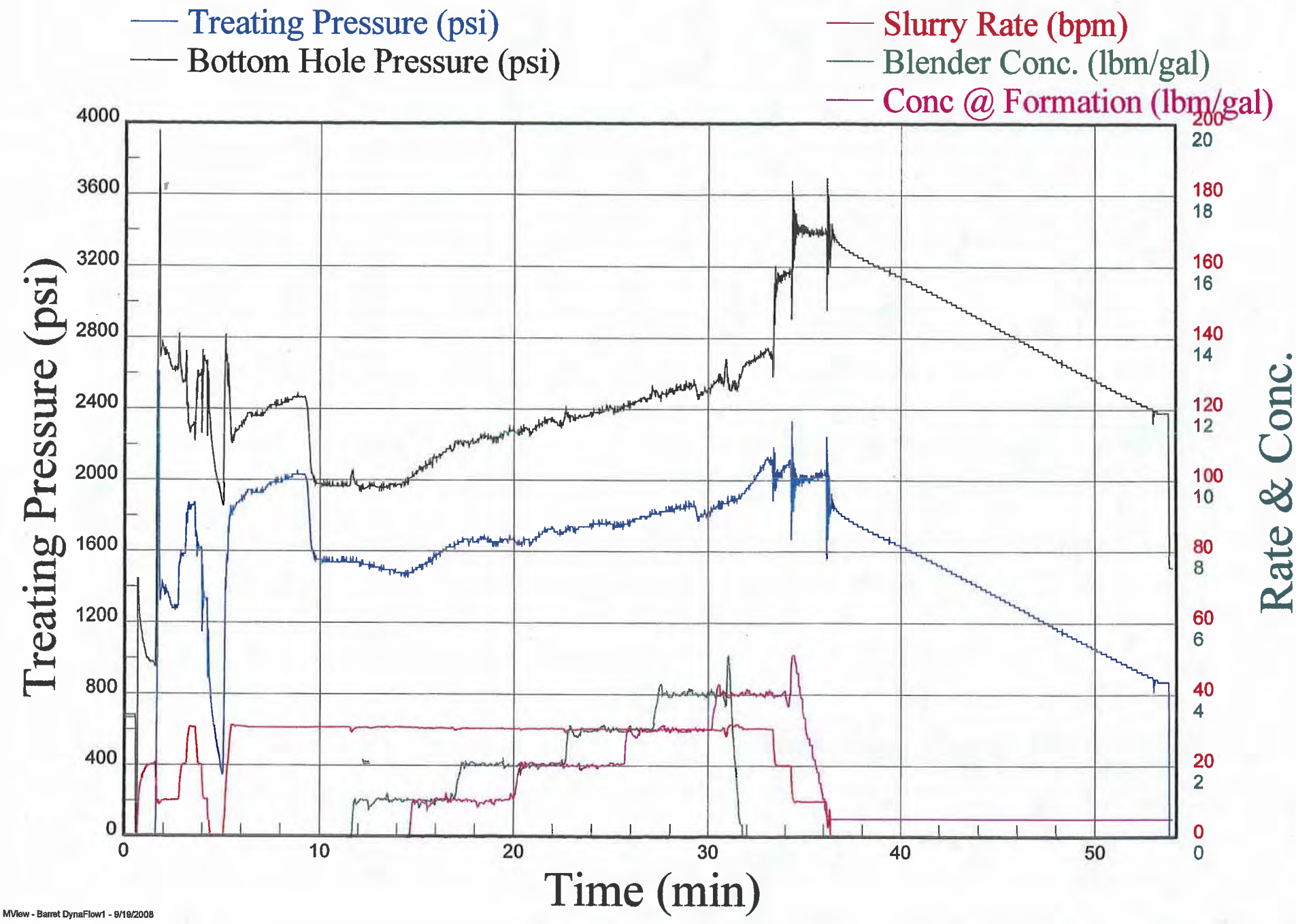
## Chemical Data

| Chemical Name | Pumped | Losses | Total (gal) |
|---|---|---|---|
| DWP-201 | 131 | 0 | 131 |
| DWP-202 | 64 | 0 | 64 |
| DWP-206 | 139 | 0 | 139 |
| DWP-988 | 60 | 0 | 60 |

Remarks: Pumped as per customer request.

Calfrac Supervisor: Jason Dusseault 540 S3 GJ Customer Representative: John Shepard, P.E.

# Surf & Bottom Hole Prickley Pear 12-24 #6




MView - Barret DynaFlow1 - 9/19/2008

# Frac Report

WELLCORE

| | |
|---|---|
| Business Unit : Operations | Bottom Hole Location : NWSW-17-12S-15E-W26M |
| Project : Uinta | API / License # : 43-007-31309 |
| Phase/Area : West Tavaputs | AFE # : 14588D |
| Well Name : Prickly Pear Fed. #12-17D-12-15 | |
| Surf. Location : SWSW-17-12S-15E-W26M | |

**Event Information**

Event Objective : Complete and equip the Prickly Pear 12-17D. Start : End : Workover # :

**Stage Information** Stage # : 12 Report 1 of 1 for Stage 12

Net Pay : 10 Report Date : 7/16/2008 1:30 PM BHST : 122 Comments :

Tagged E.L. : 4845.00 FT : (>6% Porosity) Casing ID : 4.000 Volume to Load Hole

Pressure Test

BBC Representative

Russell Evans

HES Representative

Pat Butterfield, Technical Professional

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4808.000 | 4818.000 | 3 | 30 | |

Entrance Size : 0.370

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1279 | 0.0 | 0 | 30.0 | 11.0 | 2994.0 | 2262.0 |
| 2 | CO2 Linear Pad | 1995 | 0.0 | 0 | 48.0 | 10.2 | 2997.0 | 2488.0 |
| 3 | 1# SLF CO2 Foam | 746 | 2.0 | 1425 | 19.0 | 11.0 | 3022.0 | 2985.0 |
| 4 | 2# SLF CO2 Foam | 1625 | 4.0 | 5964 | 45.0 | 11.8 | 2998.0 | 2807.0 |
| 5 | 3# SLF CO2 Foam | 1679 | 5.0 | 8865 | 50.0 | 12.6 | 2885.0 | 2767.0 |
| 6 | 4# SLF CO2 Foam | 2138 | 6.0 | 13746 | 66.0 | 13.2 | 2805.0 | 2713.0 |
| 7 | Overflush (50%) | 1035 | 0.0 | 0 | 25.0 | 10.1 | 2941.0 | 2604.0 |
| 8 | Flush (50%) | 1868 | 0.0 | 0 | 44.0 | 10.1 | 3056.0 | 2333.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 73.00 | 77.28 | -5.50 |
| MA-844 | 35.00 | 24.73 | 41.50 |
| AQF-2 | 40.00 | 41.44 | -3.50 |
| SP Breaker | 10.00 | 9.46 | 0.00 |
| GBW-30 | 5.00 | 6.63 | -24.50 |
| Gyptron T-2 | 101.00 | 110.00 | -8.20 |
| CO2 | 37.00 | 36.50 | 0.00 |
| CO2 | 201.65 | 198.93 | 1.40 |
| CO2 | 8469.30 | 8354.85 | 1.40 |

Gel System : 9218 Tanks : 1

Pct Pad : 38.30 Avg Prop Conc : 2.40

Total Fluid : 12365 Avg Rate : 11.4

Total Slurry : 13722 Max Rate : 13.2

Prime-Up & Tnkbot : 5605 Min Rate : 10.1

Total Job Fluid : 18000

**Proppant Summary** Total Proppant Pumped : 30000 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 30000 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.45

Wellhead Pressure : 2250 @ psi/ft

Broke Back : 2490 @ 12 bbl/min

Final Injection : 2700 @ 10 bbl/min

ISIP : 2510.0 @ 0.960 psi/ft

1 Min ISIP : @ psi/ft

4 Min ISIP : @ psi/ft

3 Min Bleed Off :

Final ISIP : 0.0 Final ISIP MIN : 0.000

Permeability & MD-FT : 0.000 MD FT : 0.00

Shale Stress : 0.000 Reservoir Pressure : 2084

Sand Stress : 0.000

Bleed Off Ratio : 0.000

Breakdown Fluid : 30 bbl of : Linear Purgel III

# of Perfs Open : 30

Entry Points : 2

Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 250 bbl of : LGC 6

0 Quality N2 0 SCF of nitrogen down hole

70 Quality CO2 37 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

Max Treat Pressure : 3022 psi

Min Treat Pressure : 2262 psi

Avg Treat Pressure : 2805 psi

After Frac ISDP : 2510 @ 0.960 psi/ft

Press. Increase During Frac : 0 psi

Avg Rate : 11 bbl/min

Flush Short With : 44 bbl of Slick Water or 1868 Gals

Total Fluid To Recover : 325 bbl + 75 In CSG = 400

# Frac Report

WELLCORE

| | | | |
|---|---|---|---|
| Business Unit | : Operations | Bottom Hole Location | : NWSW-17-12S-15E-W26M |
| Project | : Uinta | API / License # | : 43-007-31309 |
| Phase/Area | : West Tavaputs | AFE # | : 14588D |
| Well Name | : Prickly Pear Fed. #12-17D-12-15 | | |
| Surf. Location | : SWSW-17-12S-15E-W26M | | |

**Event Information**

Event Objective : Complete and equip the Prickly Pear 12-17D. Start : End : Workover # :

**Stage Information** Stage # : 13 Report 1 of 1 for Stage 13

Net Pay : 10 Report Date : 7/16/2008 3:15 PM BHST : 120 Comments :

Tagged E.L. : 4701.00 FT : (>6% Porosity) Casing ID : 4.000 Volume to Load Hole

Pressure Test

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 4664.000 | 4674.000 | 3 | 30 | | 0.370 |

BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1025 | 0.0 | 0 | 24.0 | 7.0 | 2954.0 | 2184.0 |
| 2 | CO2 Linear Pad | 1973 | 0.0 | 0 | 47.0 | 10.1 | 3018.0 | 2944.0 |
| 3 | 1# SLF CO2 Foam | 747 | 2.0 | 1427 | 19.0 | 10.7 | 3048.0 | 2958.0 |
| 4 | 2# SLF CO2 Foam | 1598 | 4.0 | 5865 | 44.0 | 11.7 | 3038.0 | 2889.0 |
| 5 | 3# SLF CO2 Foam | 1672 | 5.0 | 8828 | 49.0 | 12.4 | 2916.0 | 2791.0 |
| 6 | 4# SLF CO2 Foam | 2237 | 7.0 | 15144 | 70.0 | 13.2 | 2830.0 | 2755.0 |
| 7 | Overflush (50%) | 1033 | 0.0 | 0 | 25.0 | 10.2 | 2894.0 | 2627.0 |
| 8 | Flush (50%) | 1848 | 0.0 | 0 | 44.0 | 10.0 | 2906.0 | 2301.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 62.00 | 75.83 | -18.20 |
| MA-844 | 27.00 | 24.27 | 11.30 |
| AQF-2 | 40.00 | 41.55 | -3.70 |
| SP Breaker | 8.00 | 9.25 | -13.50 |
| GBW-30 | 5.00 | 6.56 | -23.80 |
| Gyptron T-2 | 105.00 | 110.00 | -4.50 |
| CO2 | 37.00 | 35.90 | 3.10 |
| CO2 | 201.65 | 195.66 | 3.10 |
| CO2 | 8469.30 | 8217.51 | 3.10 |

| | | | |
|---|---|---|---|
| Gel System : | 9260 | Tanks : | 1 |
| Pct Pad : | 36.41 | Avg Prop Conc : | 2.50 |
| Total Fluid : | 12133 | Avg Rate : | 10.8 |
| Total Slurry : | 13548 | Max Rate : | 13.2 |
| Prime-Up & Tnkbot : | 5579 | Min Rate : | 7.0 |
| Total Job Fluid : | 18000 | | |

**Proppant Summary** Total Proppant Pumped : 31264 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 31264 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.45 | | |
| Wellhead Pressure : | 2184 @ | | psi/ft |
| Broke Back : | 2790 @ | 16 | bbl/min |
| Final Injection : | 2670 @ | 10 | bbl/min |
| ISIP : | 2430.0 @ | 0.960 | psi/ft |
| 1 Min ISIP : | @ | | psi/ft |
| 4 Min ISIP : | @ | | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 2022 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 24 bbl of : Linear Purgel III | | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | @ | 0.0000 | $/lb |

**Frac Information**

Fraced well with 245 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 0 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 3048 | psi |
| Min Treat Pressure : | 2184 | psi |
| Avg Treat Pressure : | 2846 | psi |
| After Frac ISDP : | 2430 @ 0.960 | psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 11 | bbl/min |
| Flush Short With : | 44 bbl of Slick Water or 1848 | Gals |
| Total Fluid To Recover : | 313 bbl + 73 In CSG = 386 | |

# Frac Report

WELLCORE

| | | | |
|---|---|---|---|
| Business Unit | : Operations | Bottom Hole Location | : NWSW-17-12S-15E-W26M |
| Project | : Uinta | API / License # | : 43-007-31309 |
| Phase/Area | : West Tavaputs | AFE # | : 14588D |
| Well Name | : Prickly Pear Fed. #12-17D-12-15 | | |
| Surf. Location | : SWSW-17-12S-15E-W26M | | |

**Event Information**

Event Objective : Complete and equip the Prickly Pear 12-17D. Start : End : Workover # :

**Stage Information** Stage # : 14 Report 1 of 1 for Stage 14

Net Pay : 128 Report Date : 7/17/2008 7:10 AM BHST : 114 Comments :
Tagged E.L. : 4277.00 FT : (>6% Porosity) Casing ID : 4.000 Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 4122.000 | 4126.000 | 3 | 12 | | 0.370 |
| 4184.000 | 4188.000 | 3 | 12 | | |
| 4224.000 | 4228.000 | 3 | 12 | | |
| 4246.000 | 4250.000 | 3 | 12 | | |

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 4850 | 0.0 | 0 | 115.0 | 17.4 | 3468.0 | 906.0 |
| 2 | CO2 Linear Pad | 4085 | 0.0 | 0 | 97.0 | 20.4 | 3816.0 | 2895.0 |
| 3 | 1# SLF CO2 Foam | 2344 | 2.0 | 4477 | 61.0 | 21.6 | 3578.0 | 3358.0 |
| 4 | 2# SLF CO2 Foam | 4832 | 4.0 | 17733 | 134.0 | 23.4 | 3518.0 | 3362.0 |
| 5 | 3# SLF CO2 Foam | 5037 | 5.0 | 26595 | 149.0 | 24.9 | 3538.0 | 3438.0 |
| 6 | 4# SLF CO2 Foam | 6116 | 7.0 | 40894 | 190.0 | 26.0 | 3525.0 | 3212.0 |
| 7 | Overflush (50%) | 1044 | 0.0 | 0 | 25.0 | 20.2 | 3547.0 | 3346.0 |
| 8 | Flush (50%) | 1650 | 0.0 | 0 | 39.0 | 20.0 | 3588.0 | 2053.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 197.00 | 203.00 | -3.00 |
| MA-844 | 65.00 | 59.92 | 8.50 |
| AQF-2 | 100.00 | 97.74 | 2.30 |
| SP Breaker | 20.00 | 22.41 | -10.80 |
| GBW-30 | 15.00 | 16.73 | -10.40 |
| Gyptron T-2 | 110.00 | 109.94 | 0.00 |
| CO2 | 71.00 | 75.00 | -5.30 |
| CO2 | 386.95 | 408.75 | -5.30 |
| CO2 | 16251.9( | 7167.50 | -5.30 |

| | | | |
|---|---|---|---|
| Gel System : | 23458 | Tanks : | 3 |
| Pct Pad : | 39.84 | Avg Prop Conc : | 3.40 |
| Total Fluid : | 29958 | Avg Rate : | 22.0 |
| Total Slurry : | 34017 | Max Rate : | 26.0 |
| Prime-Up & Tnkbot : | 7604 | Min Rate : | 17.4 |
| Total Job Fluid : | 38000 | | |

**Proppant Summary** Total Proppant Pumped : 89700 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 89700 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.45 | | |
| Wellhead Pressure : | 940 | @ | psi/ft |
| Broke Back : | 3468 | @ 20 | bbl/min |
| Final Injection : | 2840 | @ 20 | bbl/min |
| ISIP : | 2262.0 | @ 0.980 | psi/ft |
| 1 Min ISIP : | | @ | psi/ft |
| 4 Min ISIP : | | @ | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 1813 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 115 | bbl of : Linear Purgel III | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | | @ 0.0000 | $/lb |

**Frac Information**

Fraced well with 674 bbl of : LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 71 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 3816 | psi |
| Min Treat Pressure : | 906 | psi |
| Avg Treat Pressure : | 3251 | psi |
| After Frac ISDP : | 2262 @ 0.980 | psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 22 | bbl/min |
| Flush Short With : | 39 bbl of Slick Water or 1650 | Gals |
| Total Fluid To Recover : | 829 bbl + 66 In CSG = 895 | |

# Frac Report

WELLCORE

| | | | |
|---|---|---|---|
| Business Unit | : Operations | Bottom Hole Location | : NWSW-17-12S-15E-W26M |
| Project | : Uinta | API / License # | : 43-007-31309 |
| Phase/Area | : West Tavaputs | AFE # | : 14588D |
| Well Name | : Prickly Pear Fed. #12-17D-12-15 | | |
| Surf. Location | : SWSW-17-12S-15E-W26M | | |

**Event Information**

Event Objective : Complete and equip the Prickly Pear 12-17D. Start : End : Workover # :

**Stage Information** Stage # : 15 Report 1 of 1 for Stage 15

Net Pay : 15 Report Date : 7/17/2008 8:52 AM BHST : 110 Comments :

Tagged E.L. : 3930.00 FT : (>6% Porosity) Casing ID : 4.000 Volume to Load Hole

Pressure Test

BBC Representative

Russell Evans

HES Representative

Pat Butterfield, Technical Professional

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 3888.000 | 3903.000 | 3 | 45 | | 0.370 |

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1401 | 0.0 | 0 | 33.0 | 8.7 | 3909.0 | 1308.0 |
| 2 | CO2 Linear Pad | 4452 | 0.0 | 0 | 106.0 | 15.2 | 2914.0 | 1976.0 |
| 3 | 1# SLF CO2 Foam | 1757 | 2.0 | 4199 | 46.0 | 16.4 | 2865.0 | 2778.0 |
| 4 | 2# SLF CO2 Foam | 3908 | 5.0 | 17899 | 112.0 | 17.5 | 2786.0 | 2653.0 |
| 5 | 3# SLF CO2 Foam | 4057 | 7.0 | 26776 | 125.0 | 18.6 | 2765.0 | 26538.0 |
| 6 | 4# SLF CO2 Foam | 4708 | 9.0 | 40489 | 156.0 | 19.5 | 2708.0 | 2587.0 |
| 7 | Overflush (50%) | 1086 | 0.0 | 0 | 26.0 | 15.1 | 2781.0 | 2657.0 |
| 8 | Flush (50%) | 1567 | 0.0 | 0 | 37.0 | 15.0 | 2943.0 | 2204.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 163.00 | 160.55 | 1.50 |
| MA-844 | 45.00 | 45.87 | 0.00 |
| AQF-2 | 82.00 | 83.49 | -1.80 |
| SP Breaker | 20.00 | 20.28 | 0.00 |
| GBW-30 | 15.00 | 14.49 | 0.00 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 63.00 | 66.40 | -5.10 |
| CO2 | 343.35 | 361.88 | -5.10 |
| CO2 | 14420.7( | 5198.96 | -5.10 |

| | | | |
|---|---|---|---|
| Gel System : | 19968 | Tanks : | 2 |
| Pct Pad : | 35.61 | Avg Prop Conc : | 4.00 |
| Total Fluid : | 22936 | Avg Rate : | 15.9 |
| Total Slurry : | 26980 | Max Rate : | 19.5 |
| Prime-Up & Tnkbot : | 6806 | Min Rate : | 8.7 |
| Total Job Fluid : | 30000 | | |

**Proppant Summary** Total Proppant Pumped : 89363 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 89363 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | | |
|---|---|---|---|---|
| Base Fluid : | 8.45 | | | |
| Wellhead Pressure : | 1310 | @ | | psi/ft |
| Broke Back : | 3909 | @ | 15 | bbl/min |
| Final Injection : | 2590 | @ | 15 | bbl/min |
| ISIP : | 2280.0 | @ | 1.020 | psi/ft |
| 1 Min ISIP : | | @ | | psi/ft |
| 4 Min ISIP : | | @ | | psi/ft |
| 3 Min Bleed Off : | | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | | 1687 |
| Sand Stress : | 0.000 | | | |
| Bleed Off Ratio : | 0.000 | | | |
| Breakdown Fluid : | 33 | bbl of : Linear Purgel III | | |
| # of Perfs Open : | 30 | | | |
| Entry Points : | 2 | | | |
| Total Cost : | | @ | 0.0000 | $/lb |

**Frac Information**

Fraced well with 509 bbl of : LGC 6

0 Quality N2 0 SCF of nitrogen down hole

70 Quality CO2 63 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | | |
|---|---|---|---|
| Max Treat Pressure : | 3909 | psi | |
| Min Treat Pressure : | 1308 | psi | |
| Avg Treat Pressure : | 4373 | psi | |
| After Frac ISDP : | 2280 @ | 1.020 | psi/ft |
| Press. Increase During Frac : | 0 | psi | |
| Avg Rate : | 16 | bbl/min | |
| Flush Short With : | 37 | bbl of Slick Water or | 1567 Gals |
| Total Fluid To Recover : | 579 | bbl + | 61 In CSG = 641 |

# Frac Report

WELLCORE

| | | | |
|---|---|---|---|
| Business Unit | : Operations | Bottom Hole Location | : NWSW-17-12S-15E-W26M |
| Project | : Uinta | API / License # | : 43-007-31309 |
| Phase/Area | : West Tavaputs | AFE # | : 14588D |
| Well Name | : Prickly Pear Fed. #12-17D-12-15 | | |
| Surf. Location | : SWSW-17-12S-15E-W26M | | |

**Event Information**

Event Objective : Complete and equip the Prickly Pear 12-17D. Start : End : Workover # :

**Stage Information** Stage # : 16 Report 1 of 1 for Stage 16

Net Pay : 10 Report Date : 7/17/2008 10:48 AM BHST : 106 Comments :

Tagged E.L. : 3634.00 FT : (>6% Porosity) Casing ID : 4.000 Volume to Load Hole

Pressure Test

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 3597.000 | 3607.000 | 3 | 30 | | 0.370 |

BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1662 | 0.0 | 0 | 40.0 | 5.8 | 3561.0 | 1608.0 |
| 2 | CO2 Linear Pad | 4491 | 0.0 | 0 | 107.0 | 15.1 | 3156.0 | 2088.0 |
| 3 | 1# SLF CO2 Foam | 1749 | 2.0 | 3341 | 45.0 | 16.1 | 3051.0 | 2991.0 |
| 4 | 2# SLF CO2 Foam | 3880 | 4.0 | 14240 | 108.0 | 17.6 | 3077.0 | 2967.0 |
| 5 | 3# SLF CO2 Foam | 4024 | 5.0 | 21247 | 119.0 | 18.6 | 3165.0 | 2986.0 |
| 6 | 4# SLF CO2 Foam | 5130 | 6.0 | 32273 | 157.0 | 19.6 | 3189.0 | 3112.0 |
| 7 | Overflush (50%) | 231 | 0.0 | 0 | 6.0 | 18.4 | 3194.0 | 2956.0 |
| 8 | Flush (50%) | 1478 | 0.0 | 0 | 35.0 | 15.1 | 3050.0 | 2185.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 138.00 | 141.53 | -2.50 |
| MA-844 | 45.00 | 45.29 | 0.00 |
| AQF-2 | 80.00 | 82.22 | -2.70 |
| SP Breaker | 20.00 | 20.94 | 0.00 |
| GBW-30 | 15.00 | 15.01 | 0.00 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 63.00 | 64.00 | 0.00 |
| CO2 | 343.35 | 348.80 | -1.60 |
| CO2 | 14420.7( | 4649.60 | -1.60 |

| | | | |
|---|---|---|---|
| Gel System : | 19505 | Tanks : | 2 |
| Pct Pad : | 37.33 | Avg Prop Conc : | 3.30 |
| Total Fluid : | 22645 | Avg Rate : | 15.9 |
| Total Slurry : | 25862 | Max Rate : | 19.6 |
| Prime-Up & Tnkbot : | 6773 | Min Rate : | 5.8 |
| Total Job Fluid : | 30000 | | |

**Proppant Summary** Total Proppant Pumped : 71100 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 71100 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.45 | | |
| Wellhead Pressure : | 1760 @ | | psi/ft |
| Broke Back : | 3561 @ | 12 | bbl/min |
| Final Injection : | 2730 @ | 15 | bbl/min |
| ISIP : | 2310.0 @ | 1.080 | psi/ft |
| 1 Min ISIP : | @ | | psi/ft |
| 4 Min ISIP : | @ | | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 1560 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 40 bbl of : Linear Purgel III | | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | @ | 0.0000 | $/lb |

**Frac Information**

Fraced well with 504 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 63 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 3561 | psi |
| Min Treat Pressure : | 1608 | psi |
| Avg Treat Pressure : | 2936 | psi |
| After Frac ISDP : | 2310 @ 1.080 | psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 16 | bbl/min |
| Flush Short With : | 35 bbl of Slick Water or 1478 | Gals |
| Total Fluid To Recover : | 579 bbl + 56 In CSG = 635 | |

# Frac Report

WELLCORE

| | |
|---|---|
| Business Unit : Operations | Bottom Hole Location : SWSW-17-12S-15E-W26M |
| Project : Uinta | API / License # : 43-007-31310 |
| Phase/Area : West Tavaputs | AFE # : 14587D |
| Well Name : Prickly Pear Fed. #13-17D-12-15 | |
| Surf. Location : SWSW-17-12S-15E-W26M | |

**Event Information**

Event Objective : Complete and equip the Prickly Pear 13-17. Start : End : Workover # :

**Stage Information** Stage # : 11 Report 1 of 1 for Stage 11

Net Pay : 5 Report Date : 7/11/2008 4:30 PM BHST : 120 Comments :

Tagged E.L. : 4696.00 FT : (>6% Porosity) Casing ID : 4.000 Volume to Load Hole

Pressure Test

BBC Representative

Russell Evans

HES Representative

Pat Butterfield, Technical Professional

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 4664.000 | 4669.000 | 3 | 15 | | 0.370 |

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1046 | 0.0 | 0 | 25.0 | 5.0 | 4694.0 | 2606.0 |
| 2 | CO2 Linear Pad | 1527 | 0.0 | 0 | 36.0 | 10.1 | 4290.0 | 2700.0 |
| 3 | 1# SLF CO2 Foam | 709 | 2.0 | 1354 | 18.0 | 10.8 | 4030.0 | 3848.0 |
| 4 | 2# SLF CO2 Foam | 1324 | 4.0 | 4859 | 37.0 | 11.7 | 3951.0 | 3580.0 |
| 5 | 3# SLF CO2 Foam | 1396 | 5.0 | 7371 | 41.0 | 12.3 | 3812.0 | 3419.0 |
| 6 | 4# SLF CO2 Foam | 1889 | 6.0 | 11416 | 57.0 | 13.2 | 3522.0 | 3311.0 |
| 7 | Overflush (50%) | 1035 | 0.0 | 0 | 25.0 | 10.3 | 3504.0 | 3195.0 |
| 8 | Flush (50%) | 1755 | 0.0 | 0 | 42.0 | 10.0 | 3568.0 | 2400.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 59.00 | 66.76 | -11.60 |
| MA-844 | 25.00 | 21.36 | 17.00 |
| AQF-2 | 38.00 | 35.75 | 6.30 |
| SP Breaker | 7.00 | 7.89 | 0.00 |
| GBW-30 | 5.00 | 5.57 | 0.00 |
| Gyptron T-2 | 90.00 | 110.00 | -18.20 |
| CO2 | 36.00 | 34.60 | 4.00 |
| CO2 | 196.20 | 188.57 | 4.00 |
| CO2 | 8240.40 | 7919.94 | 4.00 |

| | | | |
|---|---|---|---|
| Gel System : | 7880 | Tanks : | 1 |
| Pct Pad : | 36.77 | Avg Prop Conc : | 2.30 |
| Total Fluid : | 10681 | Avg Rate : | 10.5 |
| Total Slurry : | 11812 | Max Rate : | 13.2 |
| Prime-Up & Tnkbot : | 5414 | Min Rate : | 5.0 |
| Total Job Fluid : | 17000 | | |

**Proppant Summary** Total Proppant Pumped : 25000 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 25000 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.44 | | |
| Wellhead Pressure : | 2500 @ | | psi/ft |
| Broke Back : | 4694 @ | 17 | bbl/min |
| Final Injection : | 2900 @ | 10 | bbl/min |
| ISIP : | 2490.0 @ | 0.970 | psi/ft |
| 1 Min ISIP : | @ | | psi/ft |
| 4 Min ISIP : | @ | | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 2021 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 25 bbl | of : Linear Purgel III | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | | @ 0.0000 | $/lb |

**Frac Information**

Fraced well with 213 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 36 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 4694 | psi |
| Min Treat Pressure : | 2606 | psi |
| Avg Treat Pressure : | 3604 | psi |
| After Frac ISDP : | 2490 @ 0.970 | psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 10 | bbl/min |
| Flush Short With : | 42 bbl of Slick Water or 1755 | Gals |
| Total Fluid To Recover : | 279 bbl + 73 | In CSG = 352 |

# Frac Report

WELLCORE

| | | | |
|---|---|---|---|
| Business Unit | : Operations | Bottom Hole Location | : SWSW-17-12S-15E-W26M |
| Project | : Uinta | API / License # | : 43-007-31310 |
| Phase/Area | : West Tavaputs | AFE # | : 14587D |
| Well Name | : Prickly Pear Fed. #13-17D-12-15 | | |
| Surf. Location | : SWSW-17-12S-15E-W26M | | |

**Event Information**

Event Objective : Complete and equip the Prickly Pear 13-17. Start : End : Workover # :

**Stage Information** Stage # : 12 Report 1 of 1 for Stage 12

Net Pay : 132 Report Date : 7/12/2008 1:50 PM BHST : 111 Comments :

Tagged E.L. : 4015.00 FT : (>6% Porosity) Casing ID : 4.000 Volume to Load Hole
Pressure Test

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 3856.000 | 3858.000 | 3 | 6 | | 0.370 |
| 3873.000 | 3875.000 | 3 | 6 | | |
| 3914.000 | 3916.000 | 3 | 6 | | |
| 3922.000 | 3924.000 | 3 | 6 | | |
| 3937.000 | 3939.000 | 3 | 6 | | |
| 3964.000 | 3966.000 | 3 | 6 | | |
| 3986.000 | 3988.000 | 3 | 6 | | |

BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 4875 | 0.0 | 0 | 116.0 | 11.1 | 3680.0 | 800.0 |
| 2 | CO2 Linear Pad | 25500 | 0.0 | 0 | 607.0 | 33.7 | 5771.0 | 2000.0 |
| 3 | 0.25# SLF CO2 Foam | 12791 | 0.0 | 4400 | 309.0 | 39.5 | 5334.0 | 4402.0 |
| 4 | 0.50# SLF CO2 Foam | 32446 | 1.0 | 22000 | 796.0 | 40.9 | 5066.0 | 4677.0 |
| 5 | 0.75# SLF CO2 Foam | 17375 | 1.0 | 18070 | 433.0 | 40.4 | 5032.0 | 4808.0 |
| 6 | 1.00# SLF CO2 Foam | 9909 | 1.0 | 13575 | 251.0 | 40.9 | 4990.0 | 4928.0 |
| 7 | 1.50# SLF CO2 Foam | 6689 | 2.0 | 13445 | 174.0 | 40.9 | 4989.0 | 4757.0 |
| 8 | 2.00# SLF CO2 Foam | 7373 | 3.0 | 18710 | 196.0 | 41.1 | 5214.0 | 4797.0 |
| 9 | Overflush (50%) | 1462 | 0.0 | 0 | 35.0 | 40.9 | 6023.0 | 5087.0 |
| 10 | Flush (50%) | 2075 | 0.0 | 0 | 49.0 | 34.4 | 6293.0 | 2300.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| FR-56 | 55.00 | 60.25 | -8.70 |
| MA-844 | 220.00 | 240.99 | -8.70 |
| AQF-2 | 320.00 | 346.86 | -7.70 |
| Gyptron T-2 | 95.00 | 323.13 | -70.60 |
| CO2 | 198.00 | 198.80 | 0.00 |
| CO2 | 1079.10 | 1083.46 | -0.40 |
| CO2 | 45322.2( | 45505.32 | -0.40 |

| | | | |
|---|---|---|---|
| Gel System : | 113545 | Tanks : | 8 |
| Pct Pad : | 36.45 | Avg Prop Conc : | 0.80 |
| Total Fluid : | 120495 | Avg Rate : | 36.6 |
| Total Slurry : | 124576 | Max Rate : | 41.1 |
| Prime-Up & Tnkbot : | 17893 | Min Rate : | 11.1 |
| Total Job Fluid : | 139000 | | |

**Proppant Summary** Total Proppant Pumped : 90200 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 90200 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.50 | | |
| Wellhead Pressure : | 900 | @ | psi/ft |
| Broke Back : | 3055 | @ 15 | bbl/min |
| Final Injection : | 2750 | @ 23 | bbl/min |
| ISIP : | 2100.0 | @ 0.980 | psi/ft |
| 1 Min ISIP : | | @ | psi/ft |
| 4 Min ISIP : | | @ | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 1698 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 116 | bbl of : Linear Purgel III | |
| # of Perfs Open : | 30 | | |

**Frac Information**

Fraced well with 2820 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 198 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 6023 | psi |
| Min Treat Pressure : | 800 | psi |
| Avg Treat Pressure : | 4575 | psi |
| After Frac ISDP : | 2100 @ 0.980 | psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 37 | bbl/min |
| Flush Short With : | 49 bbl of Slick Water or | 2075 Gals |
| Total Fluid To Recover : | 2985 bbl + | 62 In CSG = 3047 |

# Frac Report

WELLCORE

| | |
|---|---|
| Business Unit : Operations | Bottom Hole Location : SWSW-17-12S-15E-W26M |
| Project : Uinta | API / License # : 43-007-31310 |
| Phase/Area : West Tavaputs | AFE # : 14587D |
| Well Name : Prickly Pear Fed. #13-17D-12-15 | |
| Surf. Location : SWSW-17-12S-15E-W26M | |

**Event Information**

Event Objective : Complete and equip the Prickly Pear 13-17. Start : End : Workover # :

**Stage Information** Stage # : 13 Report 1 of 1 for Stage 13

Net Pay : 15 Report Date : 7/12/2008 5:15 PM BHST : 108 Comments :
Tagged E.L. : 3736.00 FT : (>6% Porosity) Casing ID : 4.000 Volume to Load Hole
Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 3694.000 | 3709.000 | 3 | 45 | | 0.370 |

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1244 | 0.0 | 0 | 30.0 | 7.6 | 4280.0 | 1454.0 |
| 2 | CO2 Linear Pad | 2644 | 0.0 | 0 | 63.0 | 11.3 | 3219.0 | 1928.0 |
| 3 | 1# SLF CO2 Foam | 1193 | 2.0 | 2200 | 31.0 | 13.8 | 2614.0 | 2458.0 |
| 4 | 2# SLF CO2 Foam | 2167 | 4.0 | 7800 | 60.0 | 14.7 | 2568.0 | 2415.0 |
| 5 | 3# SLF CO2 Foam | 2222 | 5.0 | 11500 | 65.0 | 15.5 | 2444.0 | 2378.0 |
| 6 | 4# SLF CO2 Foam | 3629 | 6.0 | 21500 | 110.0 | 16.2 | 2413.0 | 2235.0 |
| 7 | Overflush (50%) | 1101 | 0.0 | 0 | 26.0 | 12.9 | 2510.0 | 2330.0 |
| 8 | Flush (50%) | 1222 | 0.0 | 0 | 29.0 | 12.6 | 2569.0 | 1791.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 113.00 | 96.39 | 17.20 |
| MA-844 | 30.00 | 30.84 | 0.00 |
| AQF-2 | 75.00 | 54.39 | 37.90 |
| SP Breaker | 11.00 | 13.10 | -16.00 |
| GBW-30 | 8.00 | 9.46 | -15.40 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 51.00 | 52.70 | -3.20 |
| CO2 | 277.95 | 287.22 | -3.20 |
| CO2 | 11673.9( | 2063.03 | -3.20 |

| | | | |
|---|---|---|---|
| Gel System : | 12956 | Tanks : | 2 |
| Pct Pad : | 35.78 | Avg Prop Conc : | 2.80 |
| Total Fluid : | 15422 | Avg Rate : | 13.1 |
| Total Slurry : | 17368 | Max Rate : | 16.2 |
| Prime-Up & Tnkbot : | 5953 | Min Rate : | 7.6 |
| Total Job Fluid : | 22000 | | |

**Proppant Summary** Total Proppant Pumped : 43000 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 43000 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.43 | | |
| Wellhead Pressure : | 1530 | @ | psi/ft |
| Broke Back : | 4280 | @ 17 | bbl/min |
| Final Injection : | 2220 | @ 13 | bbl/min |
| ISIP : | 1922.0 | @ 0.960 | psi/ft |
| 1 Min ISIP : | | @ | psi/ft |
| 4 Min ISIP : | | @ | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 1603 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 30 | bbl of : Linear Purgel III | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | | @ 0.0000 | $/lb |

**Frac Information**

Fraced well with 338 bbl of : LGC 6
0 Quality N2 0 SCF of nitrogen down hole
70 Quality CO2 51 tons CO2
Total SCF N2 Pumped
Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 4280 | psi |
| Min Treat Pressure : | 1454 | psi |
| Avg Treat Pressure : | 2518 | psi |
| After Frac ISDP : | 1922 @ | 0.960 psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 13 | bbl/min |
| Flush Short With : | 29 bbl | of Slick Water or 1222 Gals |
| Total Fluid To Recover : | 397 bbl + | 58 In CSG = 455 |

# Frac Report

WELLCORE

| | | | |
|---|---|---|---|
| Business Unit | : Operations | Bottom Hole Location | : SESW-17-12S-15E-W26M |
| Project | : Uinta | API / License # | : 43-007-3123 |
| Phase/Area | : West Tavaputs | AFE # | : 14589D |
| Well Name | : Prickly Pear Fed. #14-17D-12-15 | | |
| Surf. Location | : SWSW-17-12S-15E-W26M | | |

**Event Information**

Event Objective : Drill, complete, and equip a 7,704' Price River we  Start :  End :  Workover # :

**Stage Information**  Stage # : 7  Report 1 of 1 for Stage 7

Net Pay : 42  Report Date : 7/19/2008 3:25 PM  BHST : 123  Comments :

Tagged E.L. : 4929.00  FT : (>6% Porosity)  Casing ID : 4.000  Volume to Load Hole

Pressure Test

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 4860.000 | 4868.000 | 3 | 24 | | 0.370 |
| 4898.000 | 4902.000 | 3 | 12 | | |

BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 856 | 0.0 | 0 | 20.0 | 6.2 | 4034.0 | 2058.0 |
| 2 | CO2 Linear Pad | 2579 | 0.0 | 0 | 61.0 | 9.9 | 3014.0 | 2250.0 |
| 3 | 1# SLF CO2 Foam | 1085 | 2.0 | 2072 | 28.0 | 10.9 | 3034.0 | 2663.0 |
| 4 | 2# SLF CO2 Foam | 2278 | 4.0 | 8360 | 63.0 | 11.8 | 3019.0 | 2898.0 |
| 5 | 3# SLF CO2 Foam | 2376 | 5.0 | 12545 | 70.0 | 12.3 | 2969.0 | 2731.0 |
| 6 | 4# SLF CO2 Foam | 2966 | 6.0 | 19022 | 91.0 | 12.7 | 2909.0 | 2601.0 |
| 7 | Overflush (50%) | 1041 | 0.0 | 0 | 25.0 | 9.9 | 2984.0 | 2640.0 |
| 8 | Flush (50%) | 1920 | 0.0 | 0 | 46.0 | 10.0 | 3000.0 | 2300.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 84.00 | 94.38 | -11.00 |
| LoSurf-300 | 15.00 | 15.10 | 0.00 |
| AQF-2 | 50.00 | 54.02 | -7.40 |
| SP Breaker | 12.00 | 12.14 | 0.00 |
| GBW-30 | 8.00 | 8.72 | 0.00 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 44.00 | 44.50 | 0.00 |
| CO2 | 239.80 | 242.53 | -1.10 |
| CO2 | 10071.6( | 0186.05 | -1.10 |

| | | | |
|---|---|---|---|
| Gel System : | 12325 | Tanks : | 2 |
| Pct Pad : | 34.29 | Avg Prop Conc : | 2.70 |
| Total Fluid : | 15101 | Avg Rate : | 10.5 |
| Total Slurry : | 17001 | Max Rate : | 12.7 |
| Prime-Up & Tnkbot : | 5916 | Min Rate : | 6.2 |
| Total Job Fluid : | 22000 | | |

**Proppant Summary**  Total Proppant Pumped : 42000  Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 42000 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.46 | | |
| Wellhead Pressure : | 2061 | @ | psi/ft |
| Broke Back : | 4304 | @ 17 | bbl/min |
| Final Injection : | 2640 | @ 10 | bbl/min |
| ISIP : | 2340.0 | @ 0.920 | psi/ft |
| 1 Min ISIP : | | @ | psi/ft |
| 4 Min ISIP : | | @ | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 2113 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 20 | bbl of : Linear Purgel III | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | | @ 0.0000 | $/lb |

**Frac Information**

Fraced well with 314 bbl of : LGC 6

0 Quality N2  0 SCF of nitrogen down hole

70 Quality CO2  44 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 4034 | psi |
| Min Treat Pressure : | 2058 | psi |
| Avg Treat Pressure : | 2843 | psi |
| After Frac ISDP : | 2340 @ 0.920 | psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 11 | bbl/min |
| Flush Short With : | 46 bbl of Slick Water or 1920 | Gals |
| Total Fluid To Recover : | 380 bbl + 77 In CSG = 457 | |

# Frac Report

WELLCORE

| | | | |
|---|---|---|---|
| Business Unit | : Operations | Bottom Hole Location | : SESW-17-12S-15E-W26M |
| Project | : Uinta | API / License # | : 43-007-3123 |
| Phase/Area | : West Tavaputs | AFE # | : 14589D |
| Well Name | : Prickly Pear Fed. #14-17D-12-15 | | |
| Surf. Location | : SWSW-17-12S-15E-W26M | | |

**Event Information**

Event Objective : Drill, complete, and equip a 7,704' Price River we  Start :  End :  Workover # :

**Stage Information**  Stage # : 8  Report 1 of 1 for Stage 8

Net Pay : 157  Report Date : 7/19/2008 5:20 PM  BHST : 115  Comments :

Tagged E.L. : 4331.00  FT : (>6% Porosity)  Casing ID : 4.000  Volume to Load Hole

Entrance Size : 0.370

Pressure Test
BBC Representative
Russell Evans
HES Representative
Pat Butterfield, Technical Professional

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4147.000 | 4150.000 | 3 | 9 | |
| 4170.000 | 4173.000 | 3 | 9 | |
| 4188.000 | 4190.000 | 3 | 6 | |
| 4276.000 | 4280.000 | 3 | 12 | |
| 4301.000 | 4304.000 | 3 | 9 | |

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1565 | 0.0 | 0 | 37.0 | 9.2 | 3894.0 | 1865.0 |
| 2 | CO2 Linear Pad | 6071 | 0.0 | 0 | 145.0 | 19.9 | 4303.0 | 3121.0 |
| 3 | 1# SLF CO2 Foam | 2540 | 2.0 | 4851 | 66.0 | 21.4 | 3979.0 | 3820.0 |
| 4 | 2# SLF CO2 Foam | 5216 | 4.0 | 19143 | 145.0 | 23.3 | 4123.0 | 3799.0 |
| 5 | 3# SLF CO2 Foam | 5407 | 5.0 | 28549 | 159.0 | 24.4 | 4073.0 | 3722.0 |
| 6 | 4# SLF CO2 Foam | 9705 | 6.0 | 56557 | 292.0 | 25.6 | 3846.0 | 3732.0 |
| 7 | Overflush (50%) | 1079 | 0.0 | 0 | 26.0 | 20.3 | 3803.0 | 3549.0 |
| 8 | Flush (50%) | 1680 | 0.0 | 0 | 40.0 | 20.0 | 3845.0 | 3063.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 233.00 | 207.89 | 12.10 |
| LoSurf-300 | 40.00 | 33.26 | 20.30 |
| AQF-2 | 120.00 | 124.03 | -3.30 |
| SP Breaker | 30.00 | 30.50 | 0.00 |
| GBW-30 | 22.00 | 22.76 | 0.00 |
| Gyptron T-2 | 115.00 | 110.00 | 4.50 |
| CO2 | 94.00 | 95.10 | -1.20 |
| CO2 | 512.30 | 518.30 | -1.20 |
| CO2 | 21516.6( | 1768.39 | -1.20 |

| | | | |
|---|---|---|---|
| Gel System : | 30018 | Tanks : | 3 |
| Pct Pad : | 32.22 | Avg Prop Conc : | 3.30 |
| Total Fluid : | 33263 | Avg Rate : | 20.6 |
| Total Slurry : | 38200 | Max Rate : | 25.6 |
| Prime-Up & Tnkbot : | 7980 | Min Rate : | 9.2 |
| Total Job Fluid : | 42000 | | |

**Proppant Summary**  Total Proppant Pumped : 109100  Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 109100 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | | |
|---|---|---|---|---|
| Base Fluid : | 8.46 | | | |
| Wellhead Pressure : | 1940 | @ | | psi/ft |
| Broke Back : | 3616 | @ | 18 | bbl/min |
| Final Injection : | 3160 | @ | 20 | bbl/min |
| ISIP : | 2590.0 | @ | 1.050 | psi/ft |
| 1 Min ISIP : | | @ | | psi/ft |
| 4 Min ISIP : | | @ | | psi/ft |
| 3 Min Bleed Off : | | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | | 1830 |
| Sand Stress : | 0.000 | | | |
| Bleed Off Ratio : | 0.000 | | | |
| Breakdown Fluid : | 37 | bbl of : Linear Purgel III | | |
| # of Perfs Open : | 30 | | | |
| Entry Points : | 2 | | | |
| Total Cost : | | @ | 0.0000 | $/lb |

**Frac Information**

Fraced well with 752 bbl of : LGC 6

0 Quality N2  0 SCF of nitrogen down hole

70 Quality CO2  94 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | | |
|---|---|---|---|
| Max Treat Pressure : | 4303 | psi | |
| Min Treat Pressure : | 1865 | psi | |
| Avg Treat Pressure : | 3688 | psi | |
| After Frac ISDP : | 2590 | @ 1.050 | psi/ft |
| Press. Increase During Frac : | 0 | psi | |
| Avg Rate : | 21 | bbl/min | |
| Flush Short With : | 40 | bbl of Slick Water or | 1680 Gals |
| Total Fluid To Recover : | 829 | bbl + 67 | In CSG = 897 |

# Frac Report

WELLCORE

| | | | |
|---|---|---|---|
| Business Unit | : Operations | Bottom Hole Location | : SESE-18-12S-15E-W26M |
| Project | : Uinta | API / License # | : 43-007-31312 |
| Phase/Area | : West Tavaputs | AFE # | : 14575D |
| Well Name | : Prickly Pear Fed. #16-18D-12-15 | | |
| Surf. Location | : SWSW-17-12S-15E-W26M | | |

**Event Information**

Event Objective : Complete & equip the Prickly Pear 16-18D well. Start : End : Workover # :

**Stage Information** Stage # : 10 Report 1 of 1 for Stage 10

Net Pay : 20 Report Date : 6/30/2008 4:50 PM BHST : 117 Comments :

Tagged E.L. : 4442.00 FT : (>6% Porosity) Casing ID : 4.892 Volume to Load Hole

Pressure Test

BBC Representative

Russell Evans

HES Representative

Aaron Holten, Technical Professional

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 4395.000 | 4415.000 | 3 | 60 | | 0.370 |

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1195 | 0.0 | 0 | 28.0 | 2.9 | 3201.0 | 2303.0 |
| 2 | CO2 Linear Pad | 5115 | 0.0 | 0 | 122.0 | 12.7 | 6137.0 | 2781.0 |
| 3 | 1# SLF CO2 Foam | 3197 | 2.0 | 6330 | 83.0 | 13.2 | 4547.0 | 3753.0 |
| 4 | 2# SLF CO2 Foam | 6208 | 4.0 | 24522 | 174.0 | 13.7 | 3762.0 | 3679.0 |
| 5 | 3# SLF CO2 Foam | 5229 | 6.0 | 29548 | 156.0 | 14.2 | 3698.0 | 3652.0 |
| 6 | Overflush (50%) | 0 | 0.0 | 0 | 0.0 | 0.1 | 0.0 | 0.0 |
| 8 | Flush (50%) | 2222 | 0.0 | 0 | 53.0 | 12.9 | 3673.0 | 447.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 135.00 | 144.79 | -6.80 |
| LoSurf 300 | 25.00 | 23.17 | 7.90 |
| AQF-2 | 80.00 | 85.66 | -6.60 |
| SP Breaker | 19.00 | 20.94 | -9.30 |
| GBW-30 | 12.00 | 14.64 | -18.00 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 83.00 | 86.90 | -4.50 |
| CO2 | 452.35 | 473.61 | -4.50 |
| CO2 | 18998.7( | 9891.41 | -4.50 |

| | | | |
|---|---|---|---|
| Gel System : | 19749 | Tanks : | 2 |
| Pct Pad : | 45.39 | Avg Prop Conc : | 2.50 |
| Total Fluid : | 23166 | Avg Rate : | 9.5 |
| Total Slurry : | 25899 | Max Rate : | 14.2 |
| Prime-Up & Tnkbot : | 6833 | Min Rate : | 0.1 |
| Total Job Fluid : | 30000 | | |

**Proppant Summary** Total Proppant Pumped : 60400 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 60400 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.42 | | |
| Wellhead Pressure : | 2450 | @ | psi/ft |
| Broke Back : | 5946 | @ 10 | bbl/min |
| Final Injection : | 3600 | @ 25 | bbl/min |
| ISIP : | 2596.0 | @ 1.030 | psi/ft |
| 1 Min ISIP : | | @ | psi/ft |
| 4 Min ISIP : | | @ | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 1907 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |
| Breakdown Fluid : | 28 | bbl of : Linear Purgel III | |
| # of Perfs Open : | 30 | | |
| Entry Points : | 2 | | |
| Total Cost : | | @ 0.0000 | $/lb |

**Frac Information**

Fraced well with 499 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 83 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | |
|---|---|---|
| Max Treat Pressure : | 6137 | psi |
| Min Treat Pressure : | 2303 | psi |
| Avg Treat Pressure : | 3751 | psi |
| After Frac ISDP : | 2596 @ | 1.030 psi/ft |
| Press. Increase During Frac : | 0 | psi |
| Avg Rate : | 9 | bbl/min |
| Flush Short With : | 53 bbl of Slick Water or | 2222 Gals |
| Total Fluid To Recover : | 580 bbl + | 103 In CSG = 683 |

# Frac Report

WELLCORE

| | |
|---|---|
| Business Unit : Operations | Bottom Hole Location : SESE-18-12S-15E-W26M |
| Project : Uinta | API / License # : 43-007-31312 |
| Phase/Area : West Tavaputs | AFE # : 14575D |
| Well Name : Prickly Pear Fed. #16-18D-12-15 | |
| Surf. Location : SWSW-17-12S-15E-W26M | |

**Event Information**

Event Objective : Complete & equip the Prickly Pear 16-18D well. Start : End : Workover # :

**Stage Information** Stage # : 11 Report 1 of 1 for Stage 11

Net Pay : 44 Report Date : 7/1/2008 7:00 AM BHST : 114 Comments :

Tagged E.L. : 4197.00 FT : (>6% Porosity) Casing ID : 4.892 Volume to Load Hole

Pressure Test

Entrance Size : BBC Representative

Russell Evans

HES Representative

Aaron Holten, Technical Professional

| Top | Bottom | JSPF | Shots | Status |
|---|---|---|---|---|
| 4126.000 | 4136.000 | 3 | 30 | Open |
| 4164.000 | 4170.000 | 3 | 18 | Open |

0.370

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 2049 | 0.0 | 0 | 49.0 | 9.9 | 3465.0 | 851.0 |
| 2 | CO2 Linear Pad | 9026 | 0.0 | 0 | 215.0 | 15.0 | 3770.0 | 1826.0 |
| 3 | 1# SLF CO2 Foam | 5574 | 2.0 | 11037 | 145.0 | 15.8 | 3787.0 | 3654.0 |
| 4 | 2# SLF CO2 Foam | 11067 | 4.0 | 43715 | 311.0 | 16.4 | 3854.0 | 3689.0 |
| 5 | 3# SLF CO2 Foam | 9433 | 6.0 | 53349 | 282.0 | 17.0 | 3965.0 | 3675.0 |
| 6 | Overflush (50%) | 1004 | 0.0 | 0 | 24.0 | 15.2 | 3966.0 | 3562.0 |
| 8 | Flush (50%) | 1484 | 0.0 | 0 | 35.0 | 11.4 | 4043.0 | 86.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 245.00 | 247.73 | -1.10 |
| LoSurf 300 | 35.00 | 39.64 | -11.70 |
| AQF-2 | 150.00 | 147.86 | 1.40 |
| SP Breaker | 36.00 | 37.15 | -3.10 |
| GBW-30 | 23.00 | 26.06 | -11.70 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 139.00 | 143.90 | -3.40 |
| CO2 | 757.55 | 784.26 | -3.40 |
| CO2 | 31817.1( | 2938.71 | -3.40 |

Gel System : 36104 Tanks : 3

Pct Pad : 43.64 Avg Prop Conc : 2.70

Total Fluid : 39637 Avg Rate : 14.9

Total Slurry : 44528 Max Rate : 17.0

Prime-Up & Tnkbot : 8704 Min Rate : 9.9

Total Job Fluid : 49000

**Proppant Summary** Total Proppant Pumped : 108100 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 108100 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

Base Fluid : 8.41

Wellhead Pressure : 850 @ psi/ft

Broke Back : 3465 @ 15 bbl/min

Final Injection : 3580 @ 15 bbl/min

ISIP : 3225.0 @ 1.210 psi/ft

1 Min ISIP : @ psi/ft

4 Min ISIP : @ psi/ft

3 Min Bleed Off :

Final ISIP : 0.0 Final ISIP MIN : 0.000

Permeability & MD-FT : 0.000 MD FT : 0.00

Shale Stress : 0.000 Reservoir Pressure : 1796

Sand Stress : 0.000

Bleed Off Ratio : 0.000

Breakdown Fluid : 49 bbl of : Linear Purgel III

# of Perfs Open : 30

Entry Points : 2

Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 908 bbl of : LGC 6

0 Quality N2 0 SCF of nitrogen down hole

70 Quality CO2 139 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

Max Treat Pressure : 3966 psi

Min Treat Pressure : 851 psi

Avg Treat Pressure : 3339 psi

After Frac ISDP : 3225 @ 1.210 psi/ft

Press. Increase During Frac : 0 psi

Avg Rate : 15 bbl/min

Flush Short With : 35 bbl of Slick Water or 1484 Gals

Total Fluid To Recover : 993 bbl + 98 In CSG = 1090

# Frac Report

WELLCORE

| | |
|---|---|
| Business Unit : Operations | Bottom Hole Location : SESE-18-12S-15E-W26M |
| Project : Uinta | API / License # : 43-007-31312 |
| Phase/Area : West Tavaputs | AFE # : 14575D |
| Well Name : Prickly Pear Fed. #16-18D-12-15 | |
| Surf. Location : SWSW-17-12S-15E-W26M | |

**Event Information**

Event Objective : Complete & equip the Prickly Pear 16-18D well. Start : End : Workover # :

**Stage Information** Stage # : 12 Report 1 of 1 for Stage 12

Net Pay : 20 Report Date : 7/1/2008 7:15 AM BHST : 111 Comments :

Tagged E.L. : 3961.00 FT : (>6% Porosity) Casing ID : 4.892 Volume to Load Hole
Pressure Test

| Top | Bottom | JSPF | Shots | Status | Entrance Size : |
|---|---|---|---|---|---|
| 3914.000 | 3934.000 | 3 | 60 | Open | 0.370 |

BBC Representative
Russell Evans
HES Representative
Aaron Holten, Technical Professional

**Stage Details**

| Stage | Fluid | Vol | Prop Conc | Prop Total | Slurry Vol. | Rate | Max Press. | Min Press. |
|---|---|---|---|---|---|---|---|---|
| 1 | Pre-Pad | 1083 | 0.0 | 0 | 26.0 | 7.0 | 3775.0 | 1949.0 |
| 2 | CO2 Linear Pad | 6354 | 0.0 | 0 | 151.0 | 15.2 | 3231.0 | 2098.0 |
| 3 | 1# SLF CO2 Foam | 3651 | 2.0 | 7229 | 95.0 | 15.7 | 3287.0 | 3158.0 |
| 4 | 2# SLF CO2 Foam | 7215 | 4.0 | 28499 | 202.0 | 16.4 | 3351.0 | 3265.0 |
| 5 | 3# SLF CO2 Foam | 7790 | 5.0 | 41772 | 230.0 | 17.0 | 3511.0 | 3310.0 |
| 8 | Flush (50%) | 1596 | 0.0 | 0 | 38.0 | 14.6 | 3570.0 | 3000.0 |

**Additive Totals**

| Additive | Actual Amt | Calc. Amt | Pct Variance |
|---|---|---|---|
| LGC-6 | 180.00 | 173.06 | 4.00 |
| LoSurf 300 | 30.00 | 27.69 | 8.30 |
| AQF-2 | 100.00 | 104.83 | -4.60 |
| SP Breaker | 25.00 | 26.09 | -4.20 |
| GBW-30 | 23.00 | 18.75 | 22.70 |
| Gyptron T-2 | 110.00 | 110.00 | 0.00 |
| CO2 | 93.00 | 101.90 | -8.70 |
| CO2 | 506.85 | 555.36 | -8.70 |
| CO2 | 21287.7( | 3324.91 | -8.70 |

| | | | |
|---|---|---|---|
| Gel System : | 25010 | Tanks : | 2 |
| Pct Pad : | 42.49 | Avg Prop Conc : | 2.70 |
| Total Fluid : | 27689 | Avg Rate : | 14.3 |
| Total Slurry : | 31196 | Max Rate : | 17.0 |
| Prime-Up & Tnkbot : | 7346 | Min Rate : | 7.0 |
| Total Job Fluid : | 36000 | | |

**Proppant Summary** Total Proppant Pumped : 77500 Variance : 0.00

| % Of Job | Proppant | Mesh | Quantity | Variance |
|---|---|---|---|---|
| 0.00 | Sand | 100 | 0 | 0.00 |
| 0.00 | Sand | 16-30 | 0 | 0.00 |
| 100.00 | Sand | 20-40 | 77500 | 0.00 |
| 0.00 | PR6000 | 20-40 | 0 | 0.00 |
| 0.00 | PR6000 | 16-30 | 0 | 0.00 |
| 0.00 | THS | 20-40 | 0 | 0.00 |

**Breakdown Information**

| | | | |
|---|---|---|---|
| Base Fluid : | 8.41 | | |
| Wellhead Pressure : | 2400 | @ | psi/ft |
| Broke Back : | 3775 | @ | 15 bbl/min |
| Final Injection : | 3400 | @ | 26 bbl/min |
| ISIP : | 2635.0 | @ | 1.110 psi/ft |
| 1 Min ISIP : | | @ | psi/ft |
| 4 Min ISIP : | | @ | psi/ft |
| 3 Min Bleed Off : | | | |
| Final ISIP : | 0.0 | Final ISIP MIN : | 0.000 |
| Permeability & MD-FT : | 0.000 | MD FT : | 0.00 |
| Shale Stress : | 0.000 | Reservoir Pressure : | 1699 |
| Sand Stress : | 0.000 | | |
| Bleed Off Ratio : | 0.000 | | |

Breakdown Fluid : 26 bbl of : Linear Purgel III

# of Perfs Open : 30

Entry Points : 2

Total Cost : @ 0.0000 $/lb

**Frac Information**

Fraced well with 621 bbl of : LGC 6

0 Quality N2 — 0 SCF of nitrogen down hole

70 Quality CO2 — 93 tons CO2

Total SCF N2 Pumped

Total tons CO2 Pumped

| | | | |
|---|---|---|---|
| Max Treat Pressure : | 3775 | psi | |
| Min Treat Pressure : | 1949 | psi | |
| Avg Treat Pressure : | 3094 | psi | |
| After Frac ISDP : | 2635 @ | 1.110 | psi/ft |
| Press. Increase During Frac : | 0 | psi | |
| Avg Rate : | 14 | bbl/min | |

Flush Short With : 38 bbl of Slick Water or 1596 Gals

Total Fluid To Recover : 685 bbl + 92 In CSG = 777

COPY

Form 3160-5
(April 2004)

UNITED STATES
DEPARTMENT OF THE INTERIOR
BUREAU OF LAND MANAGEMENT

FORM APPROVED
OM B No. 1004-0137
Expires: March 31, 2007

## SUNDRY NOTICES AND REPORTS ON WELLS

***Do not use this form for proposals to drill or to re-enter an abandoned well. Use Form 3160 - 3 (APD) for such proposals.***

***SUBMIT IN TRIPLICATE*** *- Other instructions on reverse side.*

1. Type of Well
☐ Oil Well ☑ Gas Well ☐ Other

2. Name of Operator **BILL BARRETT CORPORATION**

3a. Address **1099 18th Street Suite 2300 Denver CO 80202**

3b. Phone No. *(include area code)* **303 312-8134**

4. Location of Well *(Footage, Sec., T., R., M., or Survey Description)*
**SWSW, 1271' FSL, 483' FWL, Section 24-T12S-R14E S.L.B.&M.**

5. Lease Serial No.
**UTU-77513**

6. If Indian, Allottee or Tribe Name
**n/a**

7. If Unit or CA/Agreement, Name and/or No.
**Prickly Pear / UTU-79487**

8. Well Name and No.
**Prickly Pear Unit Fed 12-24**

9. API Well No.
**43-007-30953**

10. Field and Pool, or Exploratory Area

11. County or Parish, State
**Carbon County, Utah**

12. CHECK APPROPRIATE BOX(ES) TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | | |
|---|---|---|---|---|
| ☑ Notice of Intent | ☐ Acidize | ☐ Deepen | ☐ Production (Start/Resume) | ☐ Water Shut-Off |
| ☐ Subsequent Report | ☐ Alter Casing | ☐ Fracture Treat | ☐ Reclamation | ☐ Well Integrity |
| ☐ Final Abandonment Notice | ☐ Casing Repair | ☐ New Construction | ☐ Recomplete | ☑ Other **Addition of Tanks** |
| | ☐ Change Plans | ☐ Plug and Abandon | ☐ Temporarily Abandon | |
| | ☐ Convert to Injection | ☐ Plug Back | ☐ Water Disposal | |

13. Describe Proposed or Completed Operation (clearly state all pertinent details, including estimated starting date of any proposed work and approximate duration thereof. If the proposal is to deepen directionally or recomplete horizontally, give subsurface locations and measured and true vertical depths of all pertinent markers and zones. Attach the Bond under which the work will be performed or provide the Bond No. on file with BLM/BIA. Required subsequent reports shall be filed within 30 days following completion of the involved operations. If the operation results in a multiple completion or recompletion in a new interval, a Form 3160-4 shall be filed once testing has been completed. Final Abandonment Notices shall be filed only after all requirements, including reclamation, have been completed, and the operator has determined that the site is ready for final inspection.)

**This sundry is being submitted to request that additional tanks be added to this location due to the conversion to a disposal well. A diagram indicating the proposed layout and number/size of tanks is attached. A revised site security will be submitted upon completion of the reconfiguration.**

Accepted by the
Utah Division of
Oil, Gas and Mining
For Record Only

14. I hereby certify that the foregoing is true and correct
Name *(Printed/Typed)* **Tracey Fallang** Title **Regulatory Analyst**

Signature Tracey Fallang Date **04/23/2009**

**THIS SPACE FOR FEDERAL OR STATE OFFICE USE**

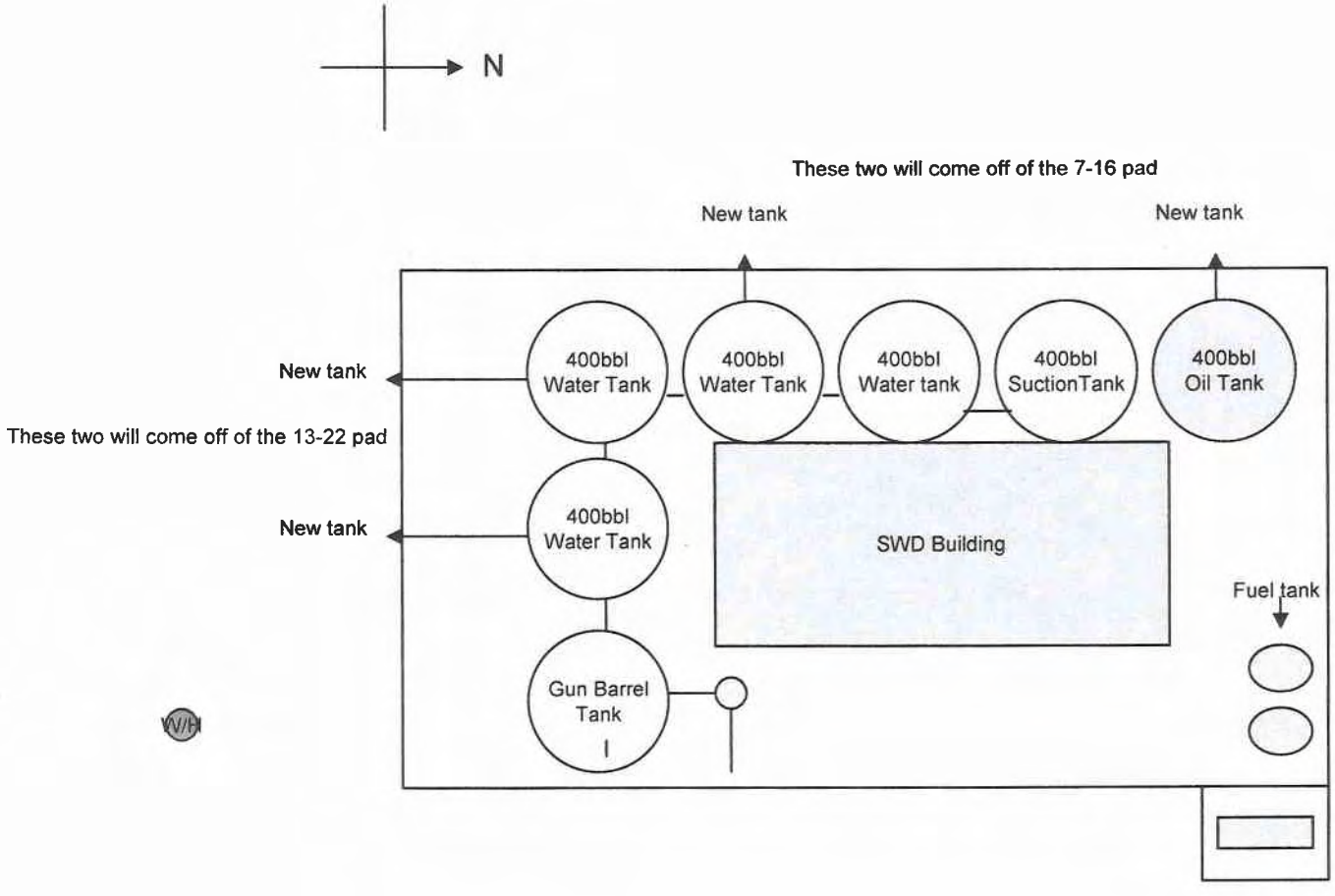
Approved by _____ Title _____ Date _____

Conditions of approval, if any, are attached. Approval of this notice does not warrant or certify that the applicant holds legal or equitable title to those rights in the subject lease which would entitle the applicant to conduct operations thereon. Office

Title 18 U.S.C. Section 1001 and Title 43 U.S.C. Section 1212, make it a crime for any person knowingly and willfully to make to any department or agency of the United States any false, fictitious or fraudulent statements or representations as to any matter within its jurisdiction.

*(Instructions on page 2)*

RECEIVED
APR 28 2009
DIV. OF OIL, GAS & MINING


N
These two will come off of the 7-16 pad
New tank
New tank
New tank
These two will come off of the 13-22 pad
New tank
400bbl Water Tank
400bbl Water Tank
400bbl Water tank
400bbl SuctionTank
400bbl Oil Tank
400bbl Water Tank
SWD Building
Fuel tank
Gun Barrel Tank
WH

# STATE OF UTAH
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS, AND MINING

FORM 9

## SUNDRY NOTICES AND REPORTS ON WELLS

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

**5.LEASE DESIGNATION AND SERIAL NUMBER:** UTU-77513

**6. IF INDIAN, ALLOTTEE OR TRIBE NAME:**

**7.UNIT or CA AGREEMENT NAME:** PRICKLY PEAR

**1. TYPE OF WELL** Water Disposal Well

**8. WELL NAME and NUMBER:** PRICKLY PEAR U FED 12-24

**2. NAME OF OPERATOR:** BILL BARRETT CORP

**9. API NUMBER:** 43007309530000

**3. ADDRESS OF OPERATOR:** 1099 18th Street Ste 2300 , Denver, CO, 80202

**PHONE NUMBER:** 303 312-8134 Ext

**9. FIELD and POOL or WILDCAT:** NINE MILE CANYON

**4. LOCATION OF WELL**
**FOOTAGES AT SURFACE:** 1271 FSL 0483 FWL
**QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN:** Qtr/Qtr: SWSW Section: 24 Township: 12.0S Range: 14.0E Meridian: S

**COUNTY:** CARBON

**STATE:** UTAH

**11.** CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☐ NOTICE OF INTENT<br>Approximate date work will start: | ☐ ACIDIZE | ☐ ALTER CASING | ☐ CASING REPAIR |
| ☑ SUBSEQUENT REPORT<br>Date of Work Completion:<br>8/13/2013 | ☐ CHANGE TO PREVIOUS PLANS | ☐ CHANGE TUBING | ☐ CHANGE WELL NAME |
| ☐ SPUD REPORT<br>Date of Spud: | ☐ CHANGE WELL STATUS | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ CONVERT WELL TYPE |
| ☐ DRILLING REPORT<br>Report Date: | ☐ DEEPEN | ☐ FRACTURE TREAT | ☐ NEW CONSTRUCTION |
| | ☐ OPERATOR CHANGE | ☐ PLUG AND ABANDON | ☐ PLUG BACK |
| | ☐ PRODUCTION START OR RESUME | ☐ RECLAMATION OF WELL SITE | ☐ RECOMPLETE DIFFERENT FORMATION |
| | ☐ REPERFORATE CURRENT FORMATION | ☐ SIDETRACK TO REPAIR WELL | ☐ TEMPORARY ABANDON |
| | ☐ TUBING REPAIR | ☐ VENT OR FLARE | ☐ WATER DISPOSAL |
| | ☐ WATER SHUTOFF | ☐ SI TA STATUS EXTENSION | ☐ APD EXTENSION |
| | ☐ WILDCAT WELL DETERMINATION | ☑ OTHER | OTHER: MIT results |

**12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.**

A MIT was conducted on the Prickly Pear Unit Federal 12-24-12-15, as required every 5 years on the annulus of the 5-1/2" casing and 2-3/8" tubing. Pressure testing the Annulus to 1,060 psig for 30 minutes. No pressure bleed off was observed and it is concluded that this wellbore and it's casing does in fact have integrity. Therefore, all underground sources of drinking water remain protected. This well has no risk to public health, safety, or environment. See attached copy of the MIT performed on 8/13/13. BBC contacted UDOGM's Dennis Ingram but he did not attend the test. Based on the results, BBC will continue to use this well as an injection well and conduct another MIT in five years.

**Accepted by the Utah Division of Oil, Gas and Mining**

**Date:** August 21, 2013

**By:**

| NAME (PLEASE PRINT) | PHONE NUMBER | TITLE |
|---|---|---|
| Brady Riley | 303 312-8115 | Permit Analyst |
| **SIGNATURE** N/A | | **DATE** 8/19/2013 |

RECEIVED: Aug. 19, 2013

Bill Barrett Corporati

# Prickly Pear 12 24 12 15 swd

Bill Barrett Corp

Delsco Northwest Inc.

PrPr 12 24 12 15
well location
West Tavaputts
Injection

Bill Barrett Corporation

# Prickly Pear 12 24 12 15 swd

## Company Information

| | |
|---|---|
| Company Name: | Bill Barrett Corp |
| Engineer: | |
| Phone: | |
| Email: | |
| Service Company: | Delsco Northwest Inc. |

## Well Information

| | |
|---|---|
| Well Name: | PrPr 12 24 12 15 |
| Well Location: | well location |
| Field / Pool: | West Tavaputts |
| Status: | Injection |

## Test Information

| | |
|---|---|
| Type of Test: | test type |
| Test Date: | 2013/08/13 11:00:00 |
| Job Number: | 1 |
| Tool Serial Number: | SH50472 |
| Tool Offset from End of Tool String: | |
| Run Depth at Tool Pressure Port: | |

## Test Results

| | |
|---|---|
| Maximum Pressure Reading: | 1632.267 |
| Maximum Temperature Reading: | 81.848 |
| Gradient Survey Information | |
| Extrapolated Pressure to MPP: | |
| Final Gradient Depth: | |

Bill Barrett Corporation

## Tool Information

| | |
|---|---|
| Tool Serial Number: | SH50472 |
| Tool Type: | |
| Calibration Date: | |
| Pressure: | |
| Pressure Rating: | |
| Temperature: | |
| Temperature Rating: | |

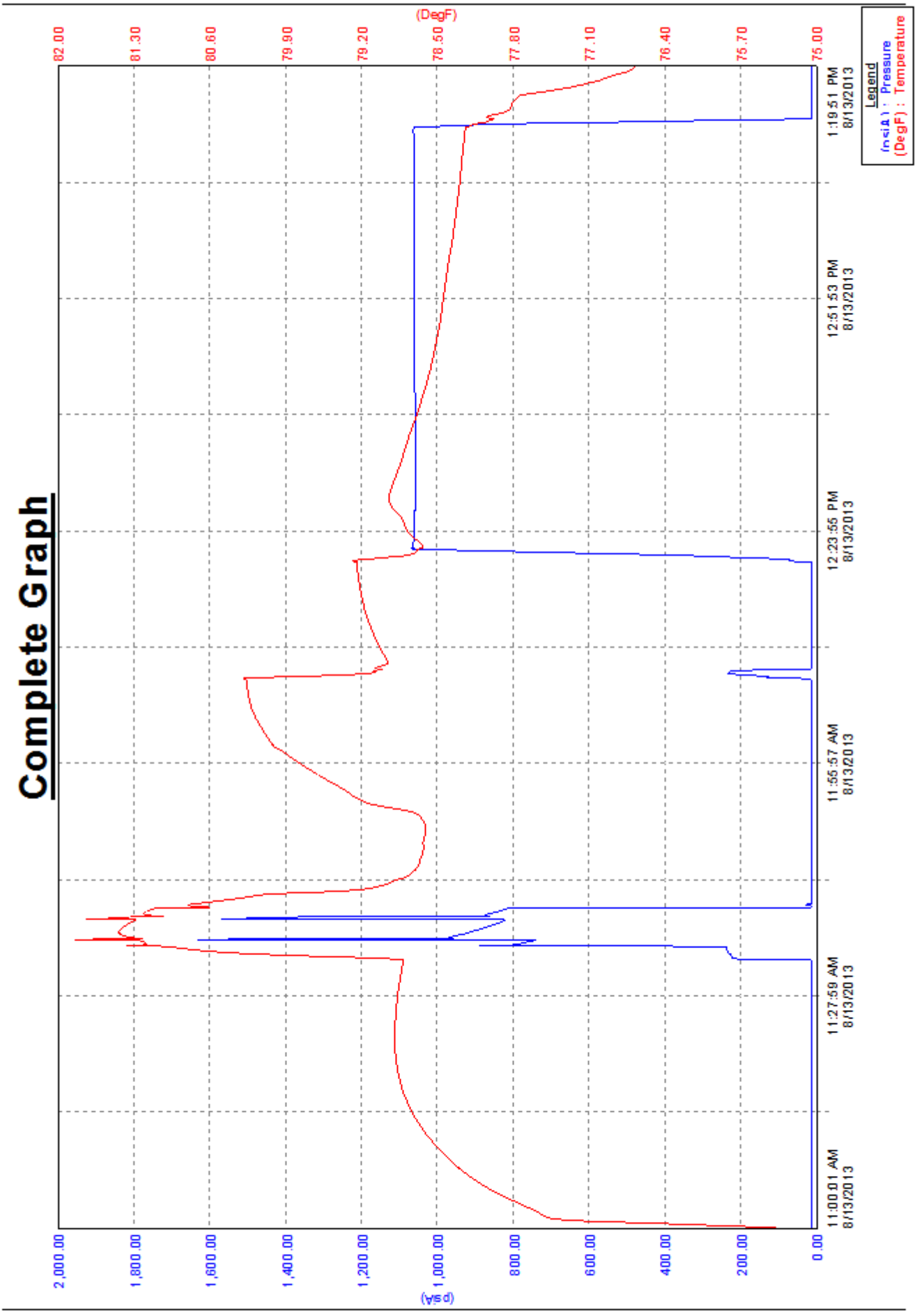
## Program Details

| Step | Sample Rate | Interval | Comments |
|---|---|---|---|
| 0 | 1 Str_sec | 32 Str_seconds | Initial sample burst |

| | |
|---|---|
| Start Time: | 2013/08/13 11:00:00 |
| End Time: | 2013/08/13 13:19:51 |
| Number of Samples: | 8391 |

## Comments

Bill Barrett Corporation




Tool Serial Number:SH50472

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:00:01 AM | 0.00028 | 14.30 | 75.19 |
| 8/13/2013 11:00:02 AM | 0.00056 | 14.30 | 75.24 |
| 8/13/2013 11:00:03 AM | 0.00083 | 14.30 | 75.29 |
| 8/13/2013 11:00:04 AM | 0.00111 | 14.30 | 75.32 |
| 8/13/2013 11:00:05 AM | 0.00139 | 14.30 | 75.35 |
| 8/13/2013 11:00:06 AM | 0.00167 | 14.30 | 75.38 |
| 8/13/2013 11:00:07 AM | 0.00194 | 14.30 | 75.41 |
| 8/13/2013 11:00:08 AM | 0.00222 | 14.30 | 75.43 |
| 8/13/2013 11:00:09 AM | 0.00250 | 14.30 | 75.46 |
| 8/13/2013 11:00:10 AM | 0.00278 | 14.30 | 75.49 |
| 8/13/2013 11:00:11 AM | 0.00306 | 14.30 | 75.52 |
| 8/13/2013 11:00:12 AM | 0.00333 | 14.30 | 75.55 |
| 8/13/2013 11:00:13 AM | 0.00361 | 14.30 | 75.58 |
| 8/13/2013 11:00:14 AM | 0.00389 | 14.30 | 75.61 |
| 8/13/2013 11:00:15 AM | 0.00417 | 14.30 | 75.65 |
| 8/13/2013 11:00:16 AM | 0.00444 | 14.30 | 75.68 |
| 8/13/2013 11:00:17 AM | 0.00472 | 14.30 | 75.71 |
| 8/13/2013 11:00:18 AM | 0.00500 | 14.30 | 75.75 |
| 8/13/2013 11:00:19 AM | 0.00528 | 14.30 | 75.78 |
| 8/13/2013 11:00:20 AM | 0.00556 | 14.30 | 75.81 |
| 8/13/2013 11:00:21 AM | 0.00583 | 14.30 | 75.85 |
| 8/13/2013 11:00:22 AM | 0.00611 | 14.30 | 75.88 |
| 8/13/2013 11:00:23 AM | 0.00639 | 14.30 | 75.91 |
| 8/13/2013 11:00:24 AM | 0.00667 | 14.30 | 75.95 |
| 8/13/2013 11:00:25 AM | 0.00694 | 14.30 | 75.98 |
| 8/13/2013 11:00:26 AM | 0.00722 | 14.30 | 76.02 |
| 8/13/2013 11:00:27 AM | 0.00750 | 14.30 | 76.05 |
| 8/13/2013 11:00:28 AM | 0.00778 | 14.30 | 76.09 |
| 8/13/2013 11:00:29 AM | 0.00806 | 14.30 | 76.12 |
| 8/13/2013 11:00:30 AM | 0.00833 | 14.30 | 76.16 |
| 8/13/2013 11:00:31 AM | 0.00861 | 14.30 | 76.19 |
| 8/13/2013 11:00:32 AM | 0.00889 | 14.30 | 76.23 |
| 8/13/2013 11:00:33 AM | 0.00917 | 14.30 | 76.26 |
| 8/13/2013 11:00:34 AM | 0.00944 | 14.30 | 76.30 |
| 8/13/2013 11:00:35 AM | 0.00972 | 14.30 | 76.33 |
| 8/13/2013 11:00:36 AM | 0.01000 | 14.30 | 76.37 |
| 8/13/2013 11:00:37 AM | 0.01028 | 14.30 | 76.41 |
| 8/13/2013 11:00:38 AM | 0.01056 | 14.30 | 76.45 |
| 8/13/2013 11:00:39 AM | 0.01083 | 14.30 | 76.48 |
| 8/13/2013 11:00:40 AM | 0.01111 | 14.30 | 76.53 |
| 8/13/2013 11:00:41 AM | 0.01139 | 14.30 | 76.57 |
| 8/13/2013 11:00:42 AM | 0.01167 | 14.30 | 76.61 |
| 8/13/2013 11:00:43 AM | 0.01194 | 14.30 | 76.65 |
| 8/13/2013 11:00:44 AM | 0.01222 | 14.30 | 76.69 |
| 8/13/2013 11:00:45 AM | 0.01250 | 14.30 | 76.74 |
| 8/13/2013 11:00:46 AM | 0.01278 | 14.30 | 76.78 |
| 8/13/2013 11:00:47 AM | 0.01306 | 14.30 | 76.82 |
| 8/13/2013 11:00:48 AM | 0.01333 | 14.30 | 76.87 |
| 8/13/2013 11:00:49 AM | 0.01361 | 14.30 | 76.91 |
| 8/13/2013 11:00:50 AM | 0.01389 | 14.30 | 76.95 |
| 8/13/2013 11:00:51 AM | 0.01417 | 14.30 | 76.99 |
| 8/13/2013 11:00:52 AM | 0.01444 | 14.30 | 77.03 |
| 8/13/2013 11:00:53 AM | 0.01472 | 14.30 | 77.06 |
| 8/13/2013 11:00:54 AM | 0.01500 | 14.30 | 77.09 |
| 8/13/2013 11:00:55 AM | 0.01528 | 14.30 | 77.13 |
| 8/13/2013 11:00:56 AM | 0.01556 | 14.30 | 77.16 |
| 8/13/2013 11:00:57 AM | 0.01583 | 14.30 | 77.18 |
| 8/13/2013 11:00:58 AM | 0.01611 | 14.30 | 77.21 |
| 8/13/2013 11:00:59 AM | 0.01639 | 14.30 | 77.23 |
| 8/13/2013 11:01:00 AM | 0.01667 | 14.30 | 77.26 |
| 8/13/2013 11:01:01 AM | 0.01694 | 14.30 | 77.28 |
| 8/13/2013 11:01:02 AM | 0.01722 | 14.30 | 77.30 |
| 8/13/2013 11:01:03 AM | 0.01750 | 14.30 | 77.31 |
| 8/13/2013 11:01:04 AM | 0.01778 | 14.30 | 77.33 |
| 8/13/2013 11:01:05 AM | 0.01806 | 14.30 | 77.35 |
| 8/13/2013 11:01:06 AM | 0.01833 | 14.30 | 77.36 |
| 8/13/2013 11:01:07 AM | 0.01861 | 14.30 | 77.37 |
| 8/13/2013 11:01:08 AM | 0.01889 | 14.30 | 77.39 |
| 8/13/2013 11:01:09 AM | 0.01917 | 14.30 | 77.40 |
| 8/13/2013 11:01:10 AM | 0.01944 | 14.30 | 77.41 |
| 8/13/2013 11:01:11 AM | 0.01972 | 14.30 | 77.42 |
| 8/13/2013 11:01:12 AM | 0.02000 | 14.30 | 77.43 |
| 8/13/2013 11:01:13 AM | 0.02028 | 14.30 | 77.44 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:01:14 AM | 0.02056 | 14.30 | 77.44 |
| 8/13/2013 11:01:15 AM | 0.02083 | 14.30 | 77.45 |
| 8/13/2013 11:01:16 AM | 0.02111 | 14.30 | 77.46 |
| 8/13/2013 11:01:17 AM | 0.02139 | 14.30 | 77.46 |
| 8/13/2013 11:01:18 AM | 0.02167 | 14.30 | 77.47 |
| 8/13/2013 11:01:19 AM | 0.02194 | 14.30 | 77.47 |
| 8/13/2013 11:01:20 AM | 0.02222 | 14.30 | 77.48 |
| 8/13/2013 11:01:21 AM | 0.02250 | 14.30 | 77.48 |
| 8/13/2013 11:01:22 AM | 0.02278 | 14.30 | 77.49 |
| 8/13/2013 11:01:23 AM | 0.02306 | 14.30 | 77.49 |
| 8/13/2013 11:01:24 AM | 0.02333 | 14.30 | 77.49 |
| 8/13/2013 11:01:25 AM | 0.02361 | 14.30 | 77.50 |
| 8/13/2013 11:01:26 AM | 0.02389 | 14.30 | 77.50 |
| 8/13/2013 11:01:27 AM | 0.02417 | 14.30 | 77.50 |
| 8/13/2013 11:01:28 AM | 0.02444 | 14.30 | 77.50 |
| 8/13/2013 11:01:29 AM | 0.02472 | 14.30 | 77.51 |
| 8/13/2013 11:01:30 AM | 0.02500 | 14.30 | 77.51 |
| 8/13/2013 11:01:31 AM | 0.02528 | 14.30 | 77.51 |
| 8/13/2013 11:01:32 AM | 0.02556 | 14.30 | 77.52 |
| 8/13/2013 11:01:33 AM | 0.02583 | 14.30 | 77.52 |
| 8/13/2013 11:01:34 AM | 0.02611 | 14.30 | 77.52 |
| 8/13/2013 11:01:35 AM | 0.02639 | 14.30 | 77.52 |
| 8/13/2013 11:01:36 AM | 0.02667 | 14.30 | 77.52 |
| 8/13/2013 11:01:37 AM | 0.02694 | 14.30 | 77.53 |
| 8/13/2013 11:01:38 AM | 0.02722 | 14.30 | 77.53 |
| 8/13/2013 11:01:39 AM | 0.02750 | 14.30 | 77.53 |
| 8/13/2013 11:01:40 AM | 0.02778 | 14.30 | 77.53 |
| 8/13/2013 11:01:41 AM | 0.02806 | 14.30 | 77.53 |
| 8/13/2013 11:01:42 AM | 0.02833 | 14.30 | 77.54 |
| 8/13/2013 11:01:43 AM | 0.02861 | 14.30 | 77.54 |
| 8/13/2013 11:01:44 AM | 0.02889 | 14.30 | 77.54 |
| 8/13/2013 11:01:45 AM | 0.02917 | 14.30 | 77.54 |
| 8/13/2013 11:01:46 AM | 0.02944 | 14.30 | 77.54 |
| 8/13/2013 11:01:47 AM | 0.02972 | 14.30 | 77.55 |
| 8/13/2013 11:01:48 AM | 0.03000 | 14.30 | 77.55 |
| 8/13/2013 11:01:49 AM | 0.03028 | 14.30 | 77.55 |
| 8/13/2013 11:01:50 AM | 0.03056 | 14.30 | 77.55 |
| 8/13/2013 11:01:51 AM | 0.03083 | 14.30 | 77.55 |
| 8/13/2013 11:01:52 AM | 0.03111 | 14.30 | 77.56 |
| 8/13/2013 11:01:53 AM | 0.03139 | 14.30 | 77.56 |
| 8/13/2013 11:01:54 AM | 0.03167 | 14.30 | 77.56 |
| 8/13/2013 11:01:55 AM | 0.03194 | 14.30 | 77.56 |
| 8/13/2013 11:01:56 AM | 0.03222 | 14.30 | 77.56 |
| 8/13/2013 11:01:57 AM | 0.03250 | 14.30 | 77.57 |
| 8/13/2013 11:01:58 AM | 0.03278 | 14.30 | 77.57 |
| 8/13/2013 11:01:59 AM | 0.03306 | 14.30 | 77.57 |
| 8/13/2013 11:02:00 AM | 0.03333 | 14.30 | 77.57 |
| 8/13/2013 11:02:01 AM | 0.03361 | 14.30 | 77.58 |
| 8/13/2013 11:02:02 AM | 0.03389 | 14.30 | 77.58 |
| 8/13/2013 11:02:03 AM | 0.03417 | 14.30 | 77.58 |
| 8/13/2013 11:02:04 AM | 0.03444 | 14.30 | 77.58 |
| 8/13/2013 11:02:05 AM | 0.03472 | 14.30 | 77.58 |
| 8/13/2013 11:02:06 AM | 0.03500 | 14.30 | 77.59 |
| 8/13/2013 11:02:07 AM | 0.03528 | 14.30 | 77.59 |
| 8/13/2013 11:02:08 AM | 0.03556 | 14.30 | 77.59 |
| 8/13/2013 11:02:09 AM | 0.03583 | 14.30 | 77.59 |
| 8/13/2013 11:02:10 AM | 0.03611 | 14.30 | 77.60 |
| 8/13/2013 11:02:11 AM | 0.03639 | 14.30 | 77.60 |
| 8/13/2013 11:02:12 AM | 0.03667 | 14.30 | 77.60 |
| 8/13/2013 11:02:13 AM | 0.03694 | 14.30 | 77.61 |
| 8/13/2013 11:02:14 AM | 0.03722 | 14.30 | 77.61 |
| 8/13/2013 11:02:15 AM | 0.03750 | 14.30 | 77.61 |
| 8/13/2013 11:02:16 AM | 0.03778 | 14.30 | 77.61 |
| 8/13/2013 11:02:17 AM | 0.03806 | 14.30 | 77.62 |
| 8/13/2013 11:02:18 AM | 0.03833 | 14.30 | 77.62 |
| 8/13/2013 11:02:19 AM | 0.03861 | 14.30 | 77.62 |
| 8/13/2013 11:02:20 AM | 0.03889 | 14.30 | 77.62 |
| 8/13/2013 11:02:21 AM | 0.03917 | 14.30 | 77.63 |
| 8/13/2013 11:02:22 AM | 0.03944 | 14.30 | 77.63 |
| 8/13/2013 11:02:23 AM | 0.03972 | 14.30 | 77.63 |
| 8/13/2013 11:02:24 AM | 0.04000 | 14.30 | 77.64 |
| 8/13/2013 11:02:25 AM | 0.04028 | 14.30 | 77.64 |
| 8/13/2013 11:02:26 AM | 0.04056 | 14.30 | 77.64 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:02:27 AM | 0.04083 | 14.30 | 77.64 |
| 8/13/2013 11:02:28 AM | 0.04111 | 14.30 | 77.65 |
| 8/13/2013 11:02:29 AM | 0.04139 | 14.30 | 77.65 |
| 8/13/2013 11:02:30 AM | 0.04167 | 14.30 | 77.65 |
| 8/13/2013 11:02:31 AM | 0.04194 | 14.30 | 77.66 |
| 8/13/2013 11:02:32 AM | 0.04222 | 14.30 | 77.66 |
| 8/13/2013 11:02:33 AM | 0.04250 | 14.30 | 77.66 |
| 8/13/2013 11:02:34 AM | 0.04278 | 14.30 | 77.66 |
| 8/13/2013 11:02:35 AM | 0.04306 | 14.30 | 77.67 |
| 8/13/2013 11:02:36 AM | 0.04333 | 14.30 | 77.67 |
| 8/13/2013 11:02:37 AM | 0.04361 | 14.30 | 77.67 |
| 8/13/2013 11:02:38 AM | 0.04389 | 14.30 | 77.68 |
| 8/13/2013 11:02:39 AM | 0.04417 | 14.30 | 77.68 |
| 8/13/2013 11:02:40 AM | 0.04444 | 14.30 | 77.68 |
| 8/13/2013 11:02:41 AM | 0.04472 | 14.30 | 77.68 |
| 8/13/2013 11:02:42 AM | 0.04500 | 14.30 | 77.69 |
| 8/13/2013 11:02:43 AM | 0.04528 | 14.30 | 77.69 |
| 8/13/2013 11:02:44 AM | 0.04556 | 14.30 | 77.69 |
| 8/13/2013 11:02:45 AM | 0.04583 | 14.30 | 77.70 |
| 8/13/2013 11:02:46 AM | 0.04611 | 14.30 | 77.70 |
| 8/13/2013 11:02:47 AM | 0.04639 | 14.30 | 77.70 |
| 8/13/2013 11:02:48 AM | 0.04667 | 14.30 | 77.70 |
| 8/13/2013 11:02:49 AM | 0.04694 | 14.30 | 77.71 |
| 8/13/2013 11:02:50 AM | 0.04722 | 14.30 | 77.71 |
| 8/13/2013 11:02:51 AM | 0.04750 | 14.30 | 77.71 |
| 8/13/2013 11:02:52 AM | 0.04778 | 14.30 | 77.72 |
| 8/13/2013 11:02:53 AM | 0.04806 | 14.30 | 77.72 |
| 8/13/2013 11:02:54 AM | 0.04833 | 14.30 | 77.72 |
| 8/13/2013 11:02:55 AM | 0.04861 | 14.30 | 77.72 |
| 8/13/2013 11:02:56 AM | 0.04889 | 14.30 | 77.73 |
| 8/13/2013 11:02:57 AM | 0.04917 | 14.30 | 77.73 |
| 8/13/2013 11:02:58 AM | 0.04944 | 14.30 | 77.73 |
| 8/13/2013 11:02:59 AM | 0.04972 | 14.30 | 77.74 |
| 8/13/2013 11:03:00 AM | 0.05000 | 14.30 | 77.74 |
| 8/13/2013 11:03:01 AM | 0.05028 | 14.30 | 77.74 |
| 8/13/2013 11:03:02 AM | 0.05056 | 14.30 | 77.75 |
| 8/13/2013 11:03:03 AM | 0.05083 | 14.30 | 77.75 |
| 8/13/2013 11:03:04 AM | 0.05111 | 14.30 | 77.75 |
| 8/13/2013 11:03:05 AM | 0.05139 | 14.30 | 77.75 |
| 8/13/2013 11:03:06 AM | 0.05167 | 14.30 | 77.76 |
| 8/13/2013 11:03:07 AM | 0.05194 | 14.30 | 77.76 |
| 8/13/2013 11:03:08 AM | 0.05222 | 14.30 | 77.76 |
| 8/13/2013 11:03:09 AM | 0.05250 | 14.30 | 77.77 |
| 8/13/2013 11:03:10 AM | 0.05278 | 14.30 | 77.77 |
| 8/13/2013 11:03:11 AM | 0.05306 | 14.30 | 77.77 |
| 8/13/2013 11:03:12 AM | 0.05333 | 14.30 | 77.77 |
| 8/13/2013 11:03:13 AM | 0.05361 | 14.30 | 77.78 |
| 8/13/2013 11:03:14 AM | 0.05389 | 14.30 | 77.78 |
| 8/13/2013 11:03:15 AM | 0.05417 | 14.30 | 77.78 |
| 8/13/2013 11:03:16 AM | 0.05444 | 14.30 | 77.78 |
| 8/13/2013 11:03:17 AM | 0.05472 | 14.30 | 77.79 |
| 8/13/2013 11:03:18 AM | 0.05500 | 14.30 | 77.79 |
| 8/13/2013 11:03:19 AM | 0.05528 | 14.30 | 77.79 |
| 8/13/2013 11:03:20 AM | 0.05556 | 14.30 | 77.80 |
| 8/13/2013 11:03:21 AM | 0.05583 | 14.30 | 77.80 |
| 8/13/2013 11:03:22 AM | 0.05611 | 14.30 | 77.80 |
| 8/13/2013 11:03:23 AM | 0.05639 | 14.30 | 77.81 |
| 8/13/2013 11:03:24 AM | 0.05667 | 14.30 | 77.81 |
| 8/13/2013 11:03:25 AM | 0.05694 | 14.30 | 77.81 |
| 8/13/2013 11:03:26 AM | 0.05722 | 14.30 | 77.81 |
| 8/13/2013 11:03:27 AM | 0.05750 | 14.30 | 77.82 |
| 8/13/2013 11:03:28 AM | 0.05778 | 14.30 | 77.82 |
| 8/13/2013 11:03:29 AM | 0.05806 | 14.30 | 77.82 |
| 8/13/2013 11:03:30 AM | 0.05833 | 14.30 | 77.83 |
| 8/13/2013 11:03:31 AM | 0.05861 | 14.30 | 77.83 |
| 8/13/2013 11:03:32 AM | 0.05889 | 14.30 | 77.83 |
| 8/13/2013 11:03:33 AM | 0.05917 | 14.30 | 77.83 |
| 8/13/2013 11:03:34 AM | 0.05944 | 14.30 | 77.84 |
| 8/13/2013 11:03:35 AM | 0.05972 | 14.30 | 77.84 |
| 8/13/2013 11:03:36 AM | 0.06000 | 14.30 | 77.84 |
| 8/13/2013 11:03:37 AM | 0.06028 | 14.30 | 77.84 |
| 8/13/2013 11:03:38 AM | 0.06056 | 14.30 | 77.85 |
| 8/13/2013 11:03:39 AM | 0.06083 | 14.30 | 77.85 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:03:40 AM | 0.06111 | 14.30 | 77.85 |
| 8/13/2013 11:03:41 AM | 0.06139 | 14.30 | 77.86 |
| 8/13/2013 11:03:42 AM | 0.06167 | 14.30 | 77.86 |
| 8/13/2013 11:03:43 AM | 0.06194 | 14.30 | 77.86 |
| 8/13/2013 11:03:44 AM | 0.06222 | 14.30 | 77.86 |
| 8/13/2013 11:03:45 AM | 0.06250 | 14.30 | 77.87 |
| 8/13/2013 11:03:46 AM | 0.06278 | 14.30 | 77.87 |
| 8/13/2013 11:03:47 AM | 0.06306 | 14.30 | 77.87 |
| 8/13/2013 11:03:48 AM | 0.06333 | 14.30 | 77.87 |
| 8/13/2013 11:03:49 AM | 0.06361 | 14.30 | 77.88 |
| 8/13/2013 11:03:50 AM | 0.06389 | 14.30 | 77.88 |
| 8/13/2013 11:03:51 AM | 0.06417 | 14.30 | 77.88 |
| 8/13/2013 11:03:52 AM | 0.06444 | 14.30 | 77.88 |
| 8/13/2013 11:03:53 AM | 0.06472 | 14.30 | 77.89 |
| 8/13/2013 11:03:54 AM | 0.06500 | 14.30 | 77.89 |
| 8/13/2013 11:03:55 AM | 0.06528 | 14.30 | 77.89 |
| 8/13/2013 11:03:56 AM | 0.06556 | 14.30 | 77.89 |
| 8/13/2013 11:03:57 AM | 0.06583 | 14.30 | 77.90 |
| 8/13/2013 11:03:58 AM | 0.06611 | 14.30 | 77.90 |
| 8/13/2013 11:03:59 AM | 0.06639 | 14.30 | 77.90 |
| 8/13/2013 11:04:00 AM | 0.06667 | 14.30 | 77.91 |
| 8/13/2013 11:04:01 AM | 0.06694 | 14.30 | 77.91 |
| 8/13/2013 11:04:02 AM | 0.06722 | 14.30 | 77.91 |
| 8/13/2013 11:04:03 AM | 0.06750 | 14.30 | 77.91 |
| 8/13/2013 11:04:04 AM | 0.06778 | 14.30 | 77.92 |
| 8/13/2013 11:04:05 AM | 0.06806 | 14.30 | 77.92 |
| 8/13/2013 11:04:06 AM | 0.06833 | 14.30 | 77.92 |
| 8/13/2013 11:04:07 AM | 0.06861 | 14.30 | 77.92 |
| 8/13/2013 11:04:08 AM | 0.06889 | 14.30 | 77.92 |
| 8/13/2013 11:04:09 AM | 0.06917 | 14.30 | 77.93 |
| 8/13/2013 11:04:10 AM | 0.06944 | 14.30 | 77.93 |
| 8/13/2013 11:04:11 AM | 0.06972 | 14.30 | 77.93 |
| 8/13/2013 11:04:12 AM | 0.07000 | 14.30 | 77.94 |
| 8/13/2013 11:04:13 AM | 0.07028 | 14.30 | 77.94 |
| 8/13/2013 11:04:14 AM | 0.07056 | 14.30 | 77.94 |
| 8/13/2013 11:04:15 AM | 0.07083 | 14.30 | 77.94 |
| 8/13/2013 11:04:16 AM | 0.07111 | 14.30 | 77.95 |
| 8/13/2013 11:04:17 AM | 0.07139 | 14.30 | 77.95 |
| 8/13/2013 11:04:18 AM | 0.07167 | 14.30 | 77.95 |
| 8/13/2013 11:04:19 AM | 0.07194 | 14.30 | 77.95 |
| 8/13/2013 11:04:20 AM | 0.07222 | 14.30 | 77.95 |
| 8/13/2013 11:04:21 AM | 0.07250 | 14.30 | 77.96 |
| 8/13/2013 11:04:22 AM | 0.07278 | 14.30 | 77.96 |
| 8/13/2013 11:04:23 AM | 0.07306 | 14.30 | 77.96 |
| 8/13/2013 11:04:24 AM | 0.07333 | 14.30 | 77.97 |
| 8/13/2013 11:04:25 AM | 0.07361 | 14.30 | 77.97 |
| 8/13/2013 11:04:26 AM | 0.07389 | 14.30 | 77.97 |
| 8/13/2013 11:04:27 AM | 0.07417 | 14.30 | 77.97 |
| 8/13/2013 11:04:28 AM | 0.07444 | 14.30 | 77.97 |
| 8/13/2013 11:04:29 AM | 0.07472 | 14.30 | 77.98 |
| 8/13/2013 11:04:30 AM | 0.07500 | 14.30 | 77.98 |
| 8/13/2013 11:04:31 AM | 0.07528 | 14.30 | 77.98 |
| 8/13/2013 11:04:32 AM | 0.07556 | 14.30 | 77.98 |
| 8/13/2013 11:04:33 AM | 0.07583 | 14.30 | 77.99 |
| 8/13/2013 11:04:34 AM | 0.07611 | 14.30 | 77.99 |
| 8/13/2013 11:04:35 AM | 0.07639 | 14.30 | 77.99 |
| 8/13/2013 11:04:36 AM | 0.07667 | 14.30 | 77.99 |
| 8/13/2013 11:04:37 AM | 0.07694 | 14.30 | 78.00 |
| 8/13/2013 11:04:38 AM | 0.07722 | 14.30 | 78.00 |
| 8/13/2013 11:04:39 AM | 0.07750 | 14.30 | 78.00 |
| 8/13/2013 11:04:40 AM | 0.07778 | 14.30 | 78.00 |
| 8/13/2013 11:04:41 AM | 0.07806 | 14.30 | 78.00 |
| 8/13/2013 11:04:42 AM | 0.07833 | 14.30 | 78.01 |
| 8/13/2013 11:04:43 AM | 0.07861 | 14.30 | 78.01 |
| 8/13/2013 11:04:44 AM | 0.07889 | 14.30 | 78.01 |
| 8/13/2013 11:04:45 AM | 0.07917 | 14.30 | 78.02 |
| 8/13/2013 11:04:46 AM | 0.07944 | 14.30 | 78.02 |
| 8/13/2013 11:04:47 AM | 0.07972 | 14.30 | 78.02 |
| 8/13/2013 11:04:48 AM | 0.08000 | 14.30 | 78.02 |
| 8/13/2013 11:04:49 AM | 0.08028 | 14.30 | 78.02 |
| 8/13/2013 11:04:50 AM | 0.08056 | 14.30 | 78.03 |
| 8/13/2013 11:04:51 AM | 0.08083 | 14.30 | 78.03 |
| 8/13/2013 11:04:52 AM | 0.08111 | 14.30 | 78.03 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:04:53 AM | 0.08139 | 14.30 | 78.03 |
| 8/13/2013 11:04:54 AM | 0.08167 | 14.30 | 78.03 |
| 8/13/2013 11:04:55 AM | 0.08194 | 14.30 | 78.04 |
| 8/13/2013 11:04:56 AM | 0.08222 | 14.30 | 78.04 |
| 8/13/2013 11:04:57 AM | 0.08250 | 14.30 | 78.04 |
| 8/13/2013 11:04:58 AM | 0.08278 | 14.30 | 78.05 |
| 8/13/2013 11:04:59 AM | 0.08306 | 14.30 | 78.05 |
| 8/13/2013 11:05:00 AM | 0.08333 | 14.30 | 78.05 |
| 8/13/2013 11:05:01 AM | 0.08361 | 14.30 | 78.05 |
| 8/13/2013 11:05:02 AM | 0.08389 | 14.30 | 78.05 |
| 8/13/2013 11:05:03 AM | 0.08417 | 14.30 | 78.06 |
| 8/13/2013 11:05:04 AM | 0.08444 | 14.30 | 78.06 |
| 8/13/2013 11:05:05 AM | 0.08472 | 14.30 | 78.06 |
| 8/13/2013 11:05:06 AM | 0.08500 | 14.30 | 78.06 |
| 8/13/2013 11:05:07 AM | 0.08528 | 14.30 | 78.06 |
| 8/13/2013 11:05:08 AM | 0.08556 | 14.30 | 78.07 |
| 8/13/2013 11:05:09 AM | 0.08583 | 14.30 | 78.07 |
| 8/13/2013 11:05:10 AM | 0.08611 | 14.30 | 78.07 |
| 8/13/2013 11:05:11 AM | 0.08639 | 14.30 | 78.07 |
| 8/13/2013 11:05:12 AM | 0.08667 | 14.30 | 78.08 |
| 8/13/2013 11:05:13 AM | 0.08694 | 14.30 | 78.08 |
| 8/13/2013 11:05:14 AM | 0.08722 | 14.30 | 78.08 |
| 8/13/2013 11:05:15 AM | 0.08750 | 14.30 | 78.08 |
| 8/13/2013 11:05:16 AM | 0.08778 | 14.30 | 78.08 |
| 8/13/2013 11:05:17 AM | 0.08806 | 14.30 | 78.09 |
| 8/13/2013 11:05:18 AM | 0.08833 | 14.30 | 78.09 |
| 8/13/2013 11:05:19 AM | 0.08861 | 14.30 | 78.09 |
| 8/13/2013 11:05:20 AM | 0.08889 | 14.30 | 78.09 |
| 8/13/2013 11:05:21 AM | 0.08917 | 14.30 | 78.09 |
| 8/13/2013 11:05:22 AM | 0.08944 | 14.30 | 78.10 |
| 8/13/2013 11:05:23 AM | 0.08972 | 14.30 | 78.10 |
| 8/13/2013 11:05:24 AM | 0.09000 | 14.30 | 78.10 |
| 8/13/2013 11:05:25 AM | 0.09028 | 14.30 | 78.10 |
| 8/13/2013 11:05:26 AM | 0.09056 | 14.30 | 78.10 |
| 8/13/2013 11:05:27 AM | 0.09083 | 14.30 | 78.11 |
| 8/13/2013 11:05:28 AM | 0.09111 | 14.30 | 78.11 |
| 8/13/2013 11:05:29 AM | 0.09139 | 14.30 | 78.11 |
| 8/13/2013 11:05:30 AM | 0.09167 | 14.30 | 78.11 |
| 8/13/2013 11:05:31 AM | 0.09194 | 14.30 | 78.11 |
| 8/13/2013 11:05:32 AM | 0.09222 | 14.30 | 78.12 |
| 8/13/2013 11:05:33 AM | 0.09250 | 14.30 | 78.12 |
| 8/13/2013 11:05:34 AM | 0.09278 | 14.30 | 78.12 |
| 8/13/2013 11:05:35 AM | 0.09306 | 14.30 | 78.12 |
| 8/13/2013 11:05:36 AM | 0.09333 | 14.30 | 78.13 |
| 8/13/2013 11:05:37 AM | 0.09361 | 14.30 | 78.13 |
| 8/13/2013 11:05:38 AM | 0.09389 | 14.30 | 78.13 |
| 8/13/2013 11:05:39 AM | 0.09417 | 14.30 | 78.13 |
| 8/13/2013 11:05:40 AM | 0.09444 | 14.30 | 78.13 |
| 8/13/2013 11:05:41 AM | 0.09472 | 14.30 | 78.14 |
| 8/13/2013 11:05:42 AM | 0.09500 | 14.30 | 78.14 |
| 8/13/2013 11:05:43 AM | 0.09528 | 14.30 | 78.14 |
| 8/13/2013 11:05:44 AM | 0.09556 | 14.30 | 78.14 |
| 8/13/2013 11:05:45 AM | 0.09583 | 14.30 | 78.14 |
| 8/13/2013 11:05:46 AM | 0.09611 | 14.30 | 78.14 |
| 8/13/2013 11:05:47 AM | 0.09639 | 14.30 | 78.15 |
| 8/13/2013 11:05:48 AM | 0.09667 | 14.30 | 78.15 |
| 8/13/2013 11:05:49 AM | 0.09694 | 14.30 | 78.15 |
| 8/13/2013 11:05:50 AM | 0.09722 | 14.30 | 78.15 |
| 8/13/2013 11:05:51 AM | 0.09750 | 14.30 | 78.15 |
| 8/13/2013 11:05:52 AM | 0.09778 | 14.30 | 78.16 |
| 8/13/2013 11:05:53 AM | 0.09806 | 14.30 | 78.16 |
| 8/13/2013 11:05:54 AM | 0.09833 | 14.30 | 78.16 |
| 8/13/2013 11:05:55 AM | 0.09861 | 14.30 | 78.16 |
| 8/13/2013 11:05:56 AM | 0.09889 | 14.30 | 78.16 |
| 8/13/2013 11:05:57 AM | 0.09917 | 14.30 | 78.17 |
| 8/13/2013 11:05:58 AM | 0.09944 | 14.30 | 78.17 |
| 8/13/2013 11:05:59 AM | 0.09972 | 14.30 | 78.17 |
| 8/13/2013 11:06:00 AM | 0.10000 | 14.30 | 78.17 |
| 8/13/2013 11:06:01 AM | 0.10028 | 14.30 | 78.17 |
| 8/13/2013 11:06:02 AM | 0.10056 | 14.30 | 78.17 |
| 8/13/2013 11:06:03 AM | 0.10083 | 14.30 | 78.18 |
| 8/13/2013 11:06:04 AM | 0.10111 | 14.30 | 78.18 |
| 8/13/2013 11:06:05 AM | 0.10139 | 14.30 | 78.18 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:06:06 AM | 0.10167 | 14.30 | 78.18 |
| 8/13/2013 11:06:07 AM | 0.10194 | 14.30 | 78.18 |
| 8/13/2013 11:06:08 AM | 0.10222 | 14.30 | 78.19 |
| 8/13/2013 11:06:09 AM | 0.10250 | 14.30 | 78.19 |
| 8/13/2013 11:06:10 AM | 0.10278 | 14.30 | 78.19 |
| 8/13/2013 11:06:11 AM | 0.10306 | 14.30 | 78.19 |
| 8/13/2013 11:06:12 AM | 0.10333 | 14.30 | 78.19 |
| 8/13/2013 11:06:13 AM | 0.10361 | 14.30 | 78.19 |
| 8/13/2013 11:06:14 AM | 0.10389 | 14.30 | 78.20 |
| 8/13/2013 11:06:15 AM | 0.10417 | 14.30 | 78.20 |
| 8/13/2013 11:06:16 AM | 0.10444 | 14.30 | 78.20 |
| 8/13/2013 11:06:17 AM | 0.10472 | 14.30 | 78.20 |
| 8/13/2013 11:06:18 AM | 0.10500 | 14.30 | 78.20 |
| 8/13/2013 11:06:19 AM | 0.10528 | 14.30 | 78.20 |
| 8/13/2013 11:06:20 AM | 0.10556 | 14.30 | 78.21 |
| 8/13/2013 11:06:21 AM | 0.10583 | 14.30 | 78.21 |
| 8/13/2013 11:06:22 AM | 0.10611 | 14.30 | 78.21 |
| 8/13/2013 11:06:23 AM | 0.10639 | 14.30 | 78.21 |
| 8/13/2013 11:06:24 AM | 0.10667 | 14.30 | 78.21 |
| 8/13/2013 11:06:25 AM | 0.10694 | 14.30 | 78.22 |
| 8/13/2013 11:06:26 AM | 0.10722 | 14.30 | 78.22 |
| 8/13/2013 11:06:27 AM | 0.10750 | 14.30 | 78.22 |
| 8/13/2013 11:06:28 AM | 0.10778 | 14.30 | 78.22 |
| 8/13/2013 11:06:29 AM | 0.10806 | 14.30 | 78.22 |
| 8/13/2013 11:06:30 AM | 0.10833 | 14.30 | 78.22 |
| 8/13/2013 11:06:31 AM | 0.10861 | 14.30 | 78.23 |
| 8/13/2013 11:06:32 AM | 0.10889 | 14.30 | 78.23 |
| 8/13/2013 11:06:33 AM | 0.10917 | 14.30 | 78.23 |
| 8/13/2013 11:06:34 AM | 0.10944 | 14.30 | 78.23 |
| 8/13/2013 11:06:35 AM | 0.10972 | 14.30 | 78.23 |
| 8/13/2013 11:06:36 AM | 0.11000 | 14.30 | 78.23 |
| 8/13/2013 11:06:37 AM | 0.11028 | 14.30 | 78.24 |
| 8/13/2013 11:06:38 AM | 0.11056 | 14.30 | 78.24 |
| 8/13/2013 11:06:39 AM | 0.11083 | 14.30 | 78.24 |
| 8/13/2013 11:06:40 AM | 0.11111 | 14.30 | 78.24 |
| 8/13/2013 11:06:41 AM | 0.11139 | 14.30 | 78.24 |
| 8/13/2013 11:06:42 AM | 0.11167 | 14.30 | 78.25 |
| 8/13/2013 11:06:43 AM | 0.11194 | 14.30 | 78.25 |
| 8/13/2013 11:06:44 AM | 0.11222 | 14.30 | 78.25 |
| 8/13/2013 11:06:45 AM | 0.11250 | 14.30 | 78.25 |
| 8/13/2013 11:06:46 AM | 0.11278 | 14.30 | 78.25 |
| 8/13/2013 11:06:47 AM | 0.11306 | 14.30 | 78.25 |
| 8/13/2013 11:06:48 AM | 0.11333 | 14.30 | 78.25 |
| 8/13/2013 11:06:49 AM | 0.11361 | 14.30 | 78.26 |
| 8/13/2013 11:06:50 AM | 0.11389 | 14.30 | 78.26 |
| 8/13/2013 11:06:51 AM | 0.11417 | 14.30 | 78.26 |
| 8/13/2013 11:06:52 AM | 0.11444 | 14.30 | 78.26 |
| 8/13/2013 11:06:53 AM | 0.11472 | 14.30 | 78.26 |
| 8/13/2013 11:06:54 AM | 0.11500 | 14.30 | 78.27 |
| 8/13/2013 11:06:55 AM | 0.11528 | 14.30 | 78.27 |
| 8/13/2013 11:06:56 AM | 0.11556 | 14.30 | 78.27 |
| 8/13/2013 11:06:57 AM | 0.11583 | 14.30 | 78.27 |
| 8/13/2013 11:06:58 AM | 0.11611 | 14.30 | 78.27 |
| 8/13/2013 11:06:59 AM | 0.11639 | 14.30 | 78.27 |
| 8/13/2013 11:07:00 AM | 0.11667 | 14.30 | 78.27 |
| 8/13/2013 11:07:01 AM | 0.11694 | 14.30 | 78.28 |
| 8/13/2013 11:07:02 AM | 0.11722 | 14.30 | 78.28 |
| 8/13/2013 11:07:03 AM | 0.11750 | 14.30 | 78.28 |
| 8/13/2013 11:07:04 AM | 0.11778 | 14.30 | 78.28 |
| 8/13/2013 11:07:05 AM | 0.11806 | 14.30 | 78.28 |
| 8/13/2013 11:07:06 AM | 0.11833 | 14.30 | 78.28 |
| 8/13/2013 11:07:07 AM | 0.11861 | 14.30 | 78.29 |
| 8/13/2013 11:07:08 AM | 0.11889 | 14.30 | 78.29 |
| 8/13/2013 11:07:09 AM | 0.11917 | 14.30 | 78.29 |
| 8/13/2013 11:07:10 AM | 0.11944 | 14.30 | 78.29 |
| 8/13/2013 11:07:11 AM | 0.11972 | 14.30 | 78.29 |
| 8/13/2013 11:07:12 AM | 0.12000 | 14.30 | 78.29 |
| 8/13/2013 11:07:13 AM | 0.12028 | 14.30 | 78.30 |
| 8/13/2013 11:07:14 AM | 0.12056 | 14.30 | 78.30 |
| 8/13/2013 11:07:15 AM | 0.12083 | 14.30 | 78.30 |
| 8/13/2013 11:07:16 AM | 0.12111 | 14.30 | 78.30 |
| 8/13/2013 11:07:17 AM | 0.12139 | 14.30 | 78.30 |
| 8/13/2013 11:07:18 AM | 0.12167 | 14.30 | 78.30 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:07:19 AM | 0.12194 | 14.30 | 78.31 |
| 8/13/2013 11:07:20 AM | 0.12222 | 14.30 | 78.31 |
| 8/13/2013 11:07:21 AM | 0.12250 | 14.30 | 78.31 |
| 8/13/2013 11:07:22 AM | 0.12278 | 14.30 | 78.31 |
| 8/13/2013 11:07:23 AM | 0.12306 | 14.30 | 78.31 |
| 8/13/2013 11:07:24 AM | 0.12333 | 14.30 | 78.31 |
| 8/13/2013 11:07:25 AM | 0.12361 | 14.30 | 78.31 |
| 8/13/2013 11:07:26 AM | 0.12389 | 14.30 | 78.31 |
| 8/13/2013 11:07:27 AM | 0.12417 | 14.30 | 78.32 |
| 8/13/2013 11:07:28 AM | 0.12444 | 14.30 | 78.32 |
| 8/13/2013 11:07:29 AM | 0.12472 | 14.30 | 78.32 |
| 8/13/2013 11:07:30 AM | 0.12500 | 14.30 | 78.32 |
| 8/13/2013 11:07:31 AM | 0.12528 | 14.30 | 78.32 |
| 8/13/2013 11:07:32 AM | 0.12556 | 14.30 | 78.32 |
| 8/13/2013 11:07:33 AM | 0.12583 | 14.30 | 78.33 |
| 8/13/2013 11:07:34 AM | 0.12611 | 14.30 | 78.33 |
| 8/13/2013 11:07:35 AM | 0.12639 | 14.30 | 78.33 |
| 8/13/2013 11:07:36 AM | 0.12667 | 14.30 | 78.33 |
| 8/13/2013 11:07:37 AM | 0.12694 | 14.30 | 78.33 |
| 8/13/2013 11:07:38 AM | 0.12722 | 14.30 | 78.33 |
| 8/13/2013 11:07:39 AM | 0.12750 | 14.30 | 78.33 |
| 8/13/2013 11:07:40 AM | 0.12778 | 14.30 | 78.34 |
| 8/13/2013 11:07:41 AM | 0.12806 | 14.30 | 78.34 |
| 8/13/2013 11:07:42 AM | 0.12833 | 14.30 | 78.34 |
| 8/13/2013 11:07:43 AM | 0.12861 | 14.30 | 78.34 |
| 8/13/2013 11:07:44 AM | 0.12889 | 14.30 | 78.34 |
| 8/13/2013 11:07:45 AM | 0.12917 | 14.30 | 78.34 |
| 8/13/2013 11:07:46 AM | 0.12944 | 14.30 | 78.34 |
| 8/13/2013 11:07:47 AM | 0.12972 | 14.30 | 78.35 |
| 8/13/2013 11:07:48 AM | 0.13000 | 14.30 | 78.35 |
| 8/13/2013 11:07:49 AM | 0.13028 | 14.30 | 78.35 |
| 8/13/2013 11:07:50 AM | 0.13056 | 14.30 | 78.35 |
| 8/13/2013 11:07:51 AM | 0.13083 | 14.30 | 78.35 |
| 8/13/2013 11:07:52 AM | 0.13111 | 14.30 | 78.35 |
| 8/13/2013 11:07:53 AM | 0.13139 | 14.30 | 78.36 |
| 8/13/2013 11:07:54 AM | 0.13167 | 14.30 | 78.36 |
| 8/13/2013 11:07:55 AM | 0.13194 | 14.30 | 78.36 |
| 8/13/2013 11:07:56 AM | 0.13222 | 14.30 | 78.36 |
| 8/13/2013 11:07:57 AM | 0.13250 | 14.30 | 78.36 |
| 8/13/2013 11:07:58 AM | 0.13278 | 14.30 | 78.36 |
| 8/13/2013 11:07:59 AM | 0.13306 | 14.30 | 78.36 |
| 8/13/2013 11:08:00 AM | 0.13333 | 14.30 | 78.36 |
| 8/13/2013 11:08:01 AM | 0.13361 | 14.30 | 78.37 |
| 8/13/2013 11:08:02 AM | 0.13389 | 14.30 | 78.37 |
| 8/13/2013 11:08:03 AM | 0.13417 | 14.30 | 78.37 |
| 8/13/2013 11:08:04 AM | 0.13444 | 14.30 | 78.37 |
| 8/13/2013 11:08:05 AM | 0.13472 | 14.30 | 78.37 |
| 8/13/2013 11:08:06 AM | 0.13500 | 14.30 | 78.37 |
| 8/13/2013 11:08:07 AM | 0.13528 | 14.30 | 78.37 |
| 8/13/2013 11:08:08 AM | 0.13556 | 14.30 | 78.38 |
| 8/13/2013 11:08:09 AM | 0.13583 | 14.30 | 78.38 |
| 8/13/2013 11:08:10 AM | 0.13611 | 14.30 | 78.38 |
| 8/13/2013 11:08:11 AM | 0.13639 | 14.30 | 78.38 |
| 8/13/2013 11:08:12 AM | 0.13667 | 14.30 | 78.38 |
| 8/13/2013 11:08:13 AM | 0.13694 | 14.30 | 78.38 |
| 8/13/2013 11:08:14 AM | 0.13722 | 14.30 | 78.38 |
| 8/13/2013 11:08:15 AM | 0.13750 | 14.30 | 78.39 |
| 8/13/2013 11:08:16 AM | 0.13778 | 14.30 | 78.39 |
| 8/13/2013 11:08:17 AM | 0.13806 | 14.30 | 78.39 |
| 8/13/2013 11:08:18 AM | 0.13833 | 14.30 | 78.39 |
| 8/13/2013 11:08:19 AM | 0.13861 | 14.30 | 78.39 |
| 8/13/2013 11:08:20 AM | 0.13889 | 14.30 | 78.39 |
| 8/13/2013 11:08:21 AM | 0.13917 | 14.30 | 78.39 |
| 8/13/2013 11:08:22 AM | 0.13944 | 14.30 | 78.39 |
| 8/13/2013 11:08:23 AM | 0.13972 | 14.30 | 78.40 |
| 8/13/2013 11:08:24 AM | 0.14000 | 14.30 | 78.40 |
| 8/13/2013 11:08:25 AM | 0.14028 | 14.30 | 78.40 |
| 8/13/2013 11:08:26 AM | 0.14056 | 14.30 | 78.40 |
| 8/13/2013 11:08:27 AM | 0.14083 | 14.30 | 78.40 |
| 8/13/2013 11:08:28 AM | 0.14111 | 14.30 | 78.40 |
| 8/13/2013 11:08:29 AM | 0.14139 | 14.30 | 78.40 |
| 8/13/2013 11:08:30 AM | 0.14167 | 14.30 | 78.41 |
| 8/13/2013 11:08:31 AM | 0.14194 | 14.30 | 78.41 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:08:32 AM | 0.14222 | 14.30 | 78.41 |
| 8/13/2013 11:08:33 AM | 0.14250 | 14.30 | 78.41 |
| 8/13/2013 11:08:34 AM | 0.14278 | 14.30 | 78.41 |
| 8/13/2013 11:08:35 AM | 0.14306 | 14.30 | 78.41 |
| 8/13/2013 11:08:36 AM | 0.14333 | 14.30 | 78.41 |
| 8/13/2013 11:08:37 AM | 0.14361 | 14.30 | 78.42 |
| 8/13/2013 11:08:38 AM | 0.14389 | 14.30 | 78.42 |
| 8/13/2013 11:08:39 AM | 0.14417 | 14.30 | 78.42 |
| 8/13/2013 11:08:40 AM | 0.14444 | 14.30 | 78.42 |
| 8/13/2013 11:08:41 AM | 0.14472 | 14.30 | 78.42 |
| 8/13/2013 11:08:42 AM | 0.14500 | 14.30 | 78.42 |
| 8/13/2013 11:08:43 AM | 0.14528 | 14.30 | 78.42 |
| 8/13/2013 11:08:44 AM | 0.14556 | 14.30 | 78.42 |
| 8/13/2013 11:08:45 AM | 0.14583 | 14.30 | 78.42 |
| 8/13/2013 11:08:46 AM | 0.14611 | 14.30 | 78.43 |
| 8/13/2013 11:08:47 AM | 0.14639 | 14.30 | 78.43 |
| 8/13/2013 11:08:48 AM | 0.14667 | 14.30 | 78.43 |
| 8/13/2013 11:08:49 AM | 0.14694 | 14.30 | 78.43 |
| 8/13/2013 11:08:50 AM | 0.14722 | 14.30 | 78.43 |
| 8/13/2013 11:08:51 AM | 0.14750 | 14.30 | 78.43 |
| 8/13/2013 11:08:52 AM | 0.14778 | 14.30 | 78.44 |
| 8/13/2013 11:08:53 AM | 0.14806 | 14.30 | 78.44 |
| 8/13/2013 11:08:54 AM | 0.14833 | 14.30 | 78.44 |
| 8/13/2013 11:08:55 AM | 0.14861 | 14.30 | 78.44 |
| 8/13/2013 11:08:56 AM | 0.14889 | 14.30 | 78.44 |
| 8/13/2013 11:08:57 AM | 0.14917 | 14.30 | 78.44 |
| 8/13/2013 11:08:58 AM | 0.14944 | 14.30 | 78.44 |
| 8/13/2013 11:08:59 AM | 0.14972 | 14.30 | 78.44 |
| 8/13/2013 11:09:00 AM | 0.15000 | 14.30 | 78.44 |
| 8/13/2013 11:09:01 AM | 0.15028 | 14.30 | 78.45 |
| 8/13/2013 11:09:02 AM | 0.15056 | 14.30 | 78.45 |
| 8/13/2013 11:09:03 AM | 0.15083 | 14.30 | 78.45 |
| 8/13/2013 11:09:04 AM | 0.15111 | 14.30 | 78.45 |
| 8/13/2013 11:09:05 AM | 0.15139 | 14.30 | 78.45 |
| 8/13/2013 11:09:06 AM | 0.15167 | 14.30 | 78.45 |
| 8/13/2013 11:09:07 AM | 0.15194 | 14.30 | 78.45 |
| 8/13/2013 11:09:08 AM | 0.15222 | 14.30 | 78.45 |
| 8/13/2013 11:09:09 AM | 0.15250 | 14.30 | 78.46 |
| 8/13/2013 11:09:10 AM | 0.15278 | 14.30 | 78.46 |
| 8/13/2013 11:09:11 AM | 0.15306 | 14.30 | 78.46 |
| 8/13/2013 11:09:12 AM | 0.15333 | 14.30 | 78.46 |
| 8/13/2013 11:09:13 AM | 0.15361 | 14.30 | 78.46 |
| 8/13/2013 11:09:14 AM | 0.15389 | 14.30 | 78.46 |
| 8/13/2013 11:09:15 AM | 0.15417 | 14.30 | 78.46 |
| 8/13/2013 11:09:16 AM | 0.15444 | 14.30 | 78.47 |
| 8/13/2013 11:09:17 AM | 0.15472 | 14.30 | 78.47 |
| 8/13/2013 11:09:18 AM | 0.15500 | 14.30 | 78.47 |
| 8/13/2013 11:09:19 AM | 0.15528 | 14.30 | 78.47 |
| 8/13/2013 11:09:20 AM | 0.15556 | 14.30 | 78.47 |
| 8/13/2013 11:09:21 AM | 0.15583 | 14.30 | 78.47 |
| 8/13/2013 11:09:22 AM | 0.15611 | 14.30 | 78.47 |
| 8/13/2013 11:09:23 AM | 0.15639 | 14.30 | 78.47 |
| 8/13/2013 11:09:24 AM | 0.15667 | 14.30 | 78.47 |
| 8/13/2013 11:09:25 AM | 0.15694 | 14.30 | 78.47 |
| 8/13/2013 11:09:26 AM | 0.15722 | 14.30 | 78.48 |
| 8/13/2013 11:09:27 AM | 0.15750 | 14.30 | 78.48 |
| 8/13/2013 11:09:28 AM | 0.15778 | 14.30 | 78.48 |
| 8/13/2013 11:09:29 AM | 0.15806 | 14.30 | 78.48 |
| 8/13/2013 11:09:30 AM | 0.15833 | 14.30 | 78.48 |
| 8/13/2013 11:09:31 AM | 0.15861 | 14.30 | 78.48 |
| 8/13/2013 11:09:32 AM | 0.15889 | 14.30 | 78.48 |
| 8/13/2013 11:09:33 AM | 0.15917 | 14.30 | 78.48 |
| 8/13/2013 11:09:34 AM | 0.15944 | 14.30 | 78.49 |
| 8/13/2013 11:09:35 AM | 0.15972 | 14.30 | 78.49 |
| 8/13/2013 11:09:36 AM | 0.16000 | 14.30 | 78.49 |
| 8/13/2013 11:09:37 AM | 0.16028 | 14.30 | 78.49 |
| 8/13/2013 11:09:38 AM | 0.16056 | 14.30 | 78.49 |
| 8/13/2013 11:09:39 AM | 0.16083 | 14.30 | 78.49 |
| 8/13/2013 11:09:40 AM | 0.16111 | 14.30 | 78.49 |
| 8/13/2013 11:09:41 AM | 0.16139 | 14.30 | 78.50 |
| 8/13/2013 11:09:42 AM | 0.16167 | 14.30 | 78.50 |
| 8/13/2013 11:09:43 AM | 0.16194 | 14.30 | 78.50 |
| 8/13/2013 11:09:44 AM | 0.16222 | 14.30 | 78.50 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:09:45 AM | 0.16250 | 14.30 | 78.50 |
| 8/13/2013 11:09:46 AM | 0.16278 | 14.30 | 78.50 |
| 8/13/2013 11:09:47 AM | 0.16306 | 14.30 | 78.50 |
| 8/13/2013 11:09:48 AM | 0.16333 | 14.30 | 78.50 |
| 8/13/2013 11:09:49 AM | 0.16361 | 14.30 | 78.50 |
| 8/13/2013 11:09:50 AM | 0.16389 | 14.30 | 78.50 |
| 8/13/2013 11:09:51 AM | 0.16417 | 14.30 | 78.51 |
| 8/13/2013 11:09:52 AM | 0.16444 | 14.30 | 78.51 |
| 8/13/2013 11:09:53 AM | 0.16472 | 14.30 | 78.51 |
| 8/13/2013 11:09:54 AM | 0.16500 | 14.30 | 78.51 |
| 8/13/2013 11:09:55 AM | 0.16528 | 14.30 | 78.51 |
| 8/13/2013 11:09:56 AM | 0.16556 | 14.30 | 78.51 |
| 8/13/2013 11:09:57 AM | 0.16583 | 14.30 | 78.51 |
| 8/13/2013 11:09:58 AM | 0.16611 | 14.30 | 78.51 |
| 8/13/2013 11:09:59 AM | 0.16639 | 14.30 | 78.52 |
| 8/13/2013 11:10:00 AM | 0.16667 | 14.30 | 78.52 |
| 8/13/2013 11:10:01 AM | 0.16694 | 14.30 | 78.52 |
| 8/13/2013 11:10:02 AM | 0.16722 | 14.30 | 78.52 |
| 8/13/2013 11:10:03 AM | 0.16750 | 14.30 | 78.52 |
| 8/13/2013 11:10:04 AM | 0.16778 | 14.30 | 78.52 |
| 8/13/2013 11:10:05 AM | 0.16806 | 14.30 | 78.52 |
| 8/13/2013 11:10:06 AM | 0.16833 | 14.30 | 78.52 |
| 8/13/2013 11:10:07 AM | 0.16861 | 14.30 | 78.52 |
| 8/13/2013 11:10:08 AM | 0.16889 | 14.30 | 78.53 |
| 8/13/2013 11:10:09 AM | 0.16917 | 14.30 | 78.53 |
| 8/13/2013 11:10:10 AM | 0.16944 | 14.30 | 78.53 |
| 8/13/2013 11:10:11 AM | 0.16972 | 14.30 | 78.53 |
| 8/13/2013 11:10:12 AM | 0.17000 | 14.30 | 78.53 |
| 8/13/2013 11:10:13 AM | 0.17028 | 14.30 | 78.53 |
| 8/13/2013 11:10:14 AM | 0.17056 | 14.30 | 78.53 |
| 8/13/2013 11:10:15 AM | 0.17083 | 14.30 | 78.53 |
| 8/13/2013 11:10:16 AM | 0.17111 | 14.30 | 78.53 |
| 8/13/2013 11:10:17 AM | 0.17139 | 14.30 | 78.53 |
| 8/13/2013 11:10:18 AM | 0.17167 | 14.30 | 78.54 |
| 8/13/2013 11:10:19 AM | 0.17194 | 14.30 | 78.54 |
| 8/13/2013 11:10:20 AM | 0.17222 | 14.30 | 78.54 |
| 8/13/2013 11:10:21 AM | 0.17250 | 14.30 | 78.54 |
| 8/13/2013 11:10:22 AM | 0.17278 | 14.30 | 78.54 |
| 8/13/2013 11:10:23 AM | 0.17306 | 14.30 | 78.54 |
| 8/13/2013 11:10:24 AM | 0.17333 | 14.30 | 78.54 |
| 8/13/2013 11:10:25 AM | 0.17361 | 14.30 | 78.54 |
| 8/13/2013 11:10:26 AM | 0.17389 | 14.30 | 78.55 |
| 8/13/2013 11:10:27 AM | 0.17417 | 14.30 | 78.55 |
| 8/13/2013 11:10:28 AM | 0.17444 | 14.30 | 78.55 |
| 8/13/2013 11:10:29 AM | 0.17472 | 14.30 | 78.55 |
| 8/13/2013 11:10:30 AM | 0.17500 | 14.30 | 78.55 |
| 8/13/2013 11:10:31 AM | 0.17528 | 14.30 | 78.55 |
| 8/13/2013 11:10:32 AM | 0.17556 | 14.30 | 78.55 |
| 8/13/2013 11:10:33 AM | 0.17583 | 14.30 | 78.55 |
| 8/13/2013 11:10:34 AM | 0.17611 | 14.30 | 78.55 |
| 8/13/2013 11:10:35 AM | 0.17639 | 14.30 | 78.55 |
| 8/13/2013 11:10:36 AM | 0.17667 | 14.30 | 78.56 |
| 8/13/2013 11:10:37 AM | 0.17694 | 14.30 | 78.56 |
| 8/13/2013 11:10:38 AM | 0.17722 | 14.30 | 78.56 |
| 8/13/2013 11:10:39 AM | 0.17750 | 14.30 | 78.56 |
| 8/13/2013 11:10:40 AM | 0.17778 | 14.30 | 78.56 |
| 8/13/2013 11:10:41 AM | 0.17806 | 14.30 | 78.56 |
| 8/13/2013 11:10:42 AM | 0.17833 | 14.30 | 78.56 |
| 8/13/2013 11:10:43 AM | 0.17861 | 14.30 | 78.56 |
| 8/13/2013 11:10:44 AM | 0.17889 | 14.30 | 78.56 |
| 8/13/2013 11:10:45 AM | 0.17917 | 14.30 | 78.56 |
| 8/13/2013 11:10:46 AM | 0.17944 | 14.30 | 78.57 |
| 8/13/2013 11:10:47 AM | 0.17972 | 14.30 | 78.57 |
| 8/13/2013 11:10:48 AM | 0.18000 | 14.30 | 78.57 |
| 8/13/2013 11:10:49 AM | 0.18028 | 14.30 | 78.57 |
| 8/13/2013 11:10:50 AM | 0.18056 | 14.30 | 78.57 |
| 8/13/2013 11:10:51 AM | 0.18083 | 14.30 | 78.57 |
| 8/13/2013 11:10:52 AM | 0.18111 | 14.30 | 78.57 |
| 8/13/2013 11:10:53 AM | 0.18139 | 14.30 | 78.57 |
| 8/13/2013 11:10:54 AM | 0.18167 | 14.30 | 78.58 |
| 8/13/2013 11:10:55 AM | 0.18194 | 14.30 | 78.58 |
| 8/13/2013 11:10:56 AM | 0.18222 | 14.30 | 78.58 |
| 8/13/2013 11:10:57 AM | 0.18250 | 14.30 | 78.58 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:10:58 AM | 0.18278 | 14.30 | 78.58 |
| 8/13/2013 11:10:59 AM | 0.18306 | 14.30 | 78.58 |
| 8/13/2013 11:11:00 AM | 0.18333 | 14.30 | 78.58 |
| 8/13/2013 11:11:01 AM | 0.18361 | 14.30 | 78.58 |
| 8/13/2013 11:11:02 AM | 0.18389 | 14.30 | 78.58 |
| 8/13/2013 11:11:03 AM | 0.18417 | 14.30 | 78.58 |
| 8/13/2013 11:11:04 AM | 0.18444 | 14.30 | 78.58 |
| 8/13/2013 11:11:05 AM | 0.18472 | 14.30 | 78.59 |
| 8/13/2013 11:11:06 AM | 0.18500 | 14.30 | 78.59 |
| 8/13/2013 11:11:07 AM | 0.18528 | 14.30 | 78.59 |
| 8/13/2013 11:11:08 AM | 0.18556 | 14.30 | 78.59 |
| 8/13/2013 11:11:09 AM | 0.18583 | 14.30 | 78.59 |
| 8/13/2013 11:11:10 AM | 0.18611 | 14.30 | 78.59 |
| 8/13/2013 11:11:11 AM | 0.18639 | 14.30 | 78.59 |
| 8/13/2013 11:11:12 AM | 0.18667 | 14.30 | 78.59 |
| 8/13/2013 11:11:13 AM | 0.18694 | 14.30 | 78.59 |
| 8/13/2013 11:11:14 AM | 0.18722 | 14.30 | 78.59 |
| 8/13/2013 11:11:15 AM | 0.18750 | 14.30 | 78.60 |
| 8/13/2013 11:11:16 AM | 0.18778 | 14.30 | 78.60 |
| 8/13/2013 11:11:17 AM | 0.18806 | 14.30 | 78.60 |
| 8/13/2013 11:11:18 AM | 0.18833 | 14.30 | 78.60 |
| 8/13/2013 11:11:19 AM | 0.18861 | 14.30 | 78.60 |
| 8/13/2013 11:11:20 AM | 0.18889 | 14.30 | 78.60 |
| 8/13/2013 11:11:21 AM | 0.18917 | 14.30 | 78.60 |
| 8/13/2013 11:11:22 AM | 0.18944 | 14.30 | 78.60 |
| 8/13/2013 11:11:23 AM | 0.18972 | 14.30 | 78.60 |
| 8/13/2013 11:11:24 AM | 0.19000 | 14.30 | 78.61 |
| 8/13/2013 11:11:25 AM | 0.19028 | 14.30 | 78.61 |
| 8/13/2013 11:11:26 AM | 0.19056 | 14.30 | 78.61 |
| 8/13/2013 11:11:27 AM | 0.19083 | 14.30 | 78.61 |
| 8/13/2013 11:11:28 AM | 0.19111 | 14.30 | 78.61 |
| 8/13/2013 11:11:29 AM | 0.19139 | 14.30 | 78.61 |
| 8/13/2013 11:11:30 AM | 0.19167 | 14.30 | 78.61 |
| 8/13/2013 11:11:31 AM | 0.19194 | 14.30 | 78.61 |
| 8/13/2013 11:11:32 AM | 0.19222 | 14.30 | 78.61 |
| 8/13/2013 11:11:33 AM | 0.19250 | 14.30 | 78.61 |
| 8/13/2013 11:11:34 AM | 0.19278 | 14.30 | 78.61 |
| 8/13/2013 11:11:35 AM | 0.19306 | 14.30 | 78.62 |
| 8/13/2013 11:11:36 AM | 0.19333 | 14.30 | 78.62 |
| 8/13/2013 11:11:37 AM | 0.19361 | 14.30 | 78.62 |
| 8/13/2013 11:11:38 AM | 0.19389 | 14.30 | 78.62 |
| 8/13/2013 11:11:39 AM | 0.19417 | 14.30 | 78.62 |
| 8/13/2013 11:11:40 AM | 0.19444 | 14.30 | 78.62 |
| 8/13/2013 11:11:41 AM | 0.19472 | 14.30 | 78.62 |
| 8/13/2013 11:11:42 AM | 0.19500 | 14.30 | 78.62 |
| 8/13/2013 11:11:43 AM | 0.19528 | 14.30 | 78.62 |
| 8/13/2013 11:11:44 AM | 0.19556 | 14.30 | 78.62 |
| 8/13/2013 11:11:45 AM | 0.19583 | 14.30 | 78.63 |
| 8/13/2013 11:11:46 AM | 0.19611 | 14.30 | 78.63 |
| 8/13/2013 11:11:47 AM | 0.19639 | 14.30 | 78.63 |
| 8/13/2013 11:11:48 AM | 0.19667 | 14.30 | 78.63 |
| 8/13/2013 11:11:49 AM | 0.19694 | 14.30 | 78.63 |
| 8/13/2013 11:11:50 AM | 0.19722 | 14.30 | 78.63 |
| 8/13/2013 11:11:51 AM | 0.19750 | 14.30 | 78.63 |
| 8/13/2013 11:11:52 AM | 0.19778 | 14.30 | 78.63 |
| 8/13/2013 11:11:53 AM | 0.19806 | 14.30 | 78.63 |
| 8/13/2013 11:11:54 AM | 0.19833 | 14.30 | 78.63 |
| 8/13/2013 11:11:55 AM | 0.19861 | 14.30 | 78.63 |
| 8/13/2013 11:11:56 AM | 0.19889 | 14.30 | 78.64 |
| 8/13/2013 11:11:57 AM | 0.19917 | 14.30 | 78.64 |
| 8/13/2013 11:11:58 AM | 0.19944 | 14.30 | 78.64 |
| 8/13/2013 11:11:59 AM | 0.19972 | 14.30 | 78.64 |
| 8/13/2013 11:12:00 AM | 0.20000 | 14.30 | 78.64 |
| 8/13/2013 11:12:01 AM | 0.20028 | 14.30 | 78.64 |
| 8/13/2013 11:12:02 AM | 0.20056 | 14.30 | 78.64 |
| 8/13/2013 11:12:03 AM | 0.20083 | 14.30 | 78.64 |
| 8/13/2013 11:12:04 AM | 0.20111 | 14.30 | 78.64 |
| 8/13/2013 11:12:05 AM | 0.20139 | 14.30 | 78.64 |
| 8/13/2013 11:12:06 AM | 0.20167 | 14.30 | 78.64 |
| 8/13/2013 11:12:07 AM | 0.20194 | 14.30 | 78.64 |
| 8/13/2013 11:12:08 AM | 0.20222 | 14.30 | 78.64 |
| 8/13/2013 11:12:09 AM | 0.20250 | 14.30 | 78.65 |
| 8/13/2013 11:12:10 AM | 0.20278 | 14.30 | 78.65 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:12:11 AM | 0.20306 | 14.30 | 78.65 |
| 8/13/2013 11:12:12 AM | 0.20333 | 14.30 | 78.65 |
| 8/13/2013 11:12:13 AM | 0.20361 | 14.30 | 78.65 |
| 8/13/2013 11:12:14 AM | 0.20389 | 14.30 | 78.65 |
| 8/13/2013 11:12:15 AM | 0.20417 | 14.30 | 78.65 |
| 8/13/2013 11:12:16 AM | 0.20444 | 14.30 | 78.65 |
| 8/13/2013 11:12:17 AM | 0.20472 | 14.30 | 78.65 |
| 8/13/2013 11:12:18 AM | 0.20500 | 14.30 | 78.66 |
| 8/13/2013 11:12:19 AM | 0.20528 | 14.30 | 78.66 |
| 8/13/2013 11:12:20 AM | 0.20556 | 14.30 | 78.66 |
| 8/13/2013 11:12:21 AM | 0.20583 | 14.30 | 78.66 |
| 8/13/2013 11:12:22 AM | 0.20611 | 14.30 | 78.66 |
| 8/13/2013 11:12:23 AM | 0.20639 | 14.30 | 78.66 |
| 8/13/2013 11:12:24 AM | 0.20667 | 14.30 | 78.66 |
| 8/13/2013 11:12:25 AM | 0.20694 | 14.30 | 78.66 |
| 8/13/2013 11:12:26 AM | 0.20722 | 14.30 | 78.66 |
| 8/13/2013 11:12:27 AM | 0.20750 | 14.30 | 78.66 |
| 8/13/2013 11:12:28 AM | 0.20778 | 14.30 | 78.66 |
| 8/13/2013 11:12:29 AM | 0.20806 | 14.30 | 78.66 |
| 8/13/2013 11:12:30 AM | 0.20833 | 14.30 | 78.67 |
| 8/13/2013 11:12:31 AM | 0.20861 | 14.30 | 78.67 |
| 8/13/2013 11:12:32 AM | 0.20889 | 14.30 | 78.67 |
| 8/13/2013 11:12:33 AM | 0.20917 | 14.30 | 78.67 |
| 8/13/2013 11:12:34 AM | 0.20944 | 14.30 | 78.67 |
| 8/13/2013 11:12:35 AM | 0.20972 | 14.30 | 78.67 |
| 8/13/2013 11:12:36 AM | 0.21000 | 14.30 | 78.67 |
| 8/13/2013 11:12:37 AM | 0.21028 | 14.30 | 78.67 |
| 8/13/2013 11:12:38 AM | 0.21056 | 14.30 | 78.67 |
| 8/13/2013 11:12:39 AM | 0.21083 | 14.30 | 78.67 |
| 8/13/2013 11:12:40 AM | 0.21111 | 14.30 | 78.67 |
| 8/13/2013 11:12:41 AM | 0.21139 | 14.30 | 78.67 |
| 8/13/2013 11:12:42 AM | 0.21167 | 14.30 | 78.67 |
| 8/13/2013 11:12:43 AM | 0.21194 | 14.30 | 78.68 |
| 8/13/2013 11:12:44 AM | 0.21222 | 14.30 | 78.68 |
| 8/13/2013 11:12:45 AM | 0.21250 | 14.30 | 78.68 |
| 8/13/2013 11:12:46 AM | 0.21278 | 14.30 | 78.68 |
| 8/13/2013 11:12:47 AM | 0.21306 | 14.30 | 78.68 |
| 8/13/2013 11:12:48 AM | 0.21333 | 14.30 | 78.68 |
| 8/13/2013 11:12:49 AM | 0.21361 | 14.30 | 78.68 |
| 8/13/2013 11:12:50 AM | 0.21389 | 14.30 | 78.68 |
| 8/13/2013 11:12:51 AM | 0.21417 | 14.30 | 78.68 |
| 8/13/2013 11:12:52 AM | 0.21444 | 14.30 | 78.68 |
| 8/13/2013 11:12:53 AM | 0.21472 | 14.30 | 78.68 |
| 8/13/2013 11:12:54 AM | 0.21500 | 14.30 | 78.69 |
| 8/13/2013 11:12:55 AM | 0.21528 | 14.30 | 78.69 |
| 8/13/2013 11:12:56 AM | 0.21556 | 14.30 | 78.69 |
| 8/13/2013 11:12:57 AM | 0.21583 | 14.30 | 78.69 |
| 8/13/2013 11:12:58 AM | 0.21611 | 14.30 | 78.69 |
| 8/13/2013 11:12:59 AM | 0.21639 | 14.30 | 78.69 |
| 8/13/2013 11:13:00 AM | 0.21667 | 14.30 | 78.69 |
| 8/13/2013 11:13:01 AM | 0.21694 | 14.30 | 78.69 |
| 8/13/2013 11:13:02 AM | 0.21722 | 14.30 | 78.69 |
| 8/13/2013 11:13:03 AM | 0.21750 | 14.30 | 78.69 |
| 8/13/2013 11:13:04 AM | 0.21778 | 14.30 | 78.69 |
| 8/13/2013 11:13:05 AM | 0.21806 | 14.30 | 78.69 |
| 8/13/2013 11:13:06 AM | 0.21833 | 14.30 | 78.69 |
| 8/13/2013 11:13:07 AM | 0.21861 | 14.30 | 78.70 |
| 8/13/2013 11:13:08 AM | 0.21889 | 14.30 | 78.70 |
| 8/13/2013 11:13:09 AM | 0.21917 | 14.30 | 78.70 |
| 8/13/2013 11:13:10 AM | 0.21944 | 14.30 | 78.70 |
| 8/13/2013 11:13:11 AM | 0.21972 | 14.30 | 78.70 |
| 8/13/2013 11:13:12 AM | 0.22000 | 14.30 | 78.70 |
| 8/13/2013 11:13:13 AM | 0.22028 | 14.30 | 78.70 |
| 8/13/2013 11:13:14 AM | 0.22056 | 14.30 | 78.70 |
| 8/13/2013 11:13:15 AM | 0.22083 | 14.30 | 78.70 |
| 8/13/2013 11:13:16 AM | 0.22111 | 14.30 | 78.70 |
| 8/13/2013 11:13:17 AM | 0.22139 | 14.30 | 78.70 |
| 8/13/2013 11:13:18 AM | 0.22167 | 14.30 | 78.70 |
| 8/13/2013 11:13:19 AM | 0.22194 | 14.30 | 78.70 |
| 8/13/2013 11:13:20 AM | 0.22222 | 14.30 | 78.70 |
| 8/13/2013 11:13:21 AM | 0.22250 | 14.30 | 78.71 |
| 8/13/2013 11:13:22 AM | 0.22278 | 14.30 | 78.71 |
| 8/13/2013 11:13:23 AM | 0.22306 | 14.30 | 78.71 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:13:24 AM | 0.22333 | 14.30 | 78.71 |
| 8/13/2013 11:13:25 AM | 0.22361 | 14.30 | 78.71 |
| 8/13/2013 11:13:26 AM | 0.22389 | 14.30 | 78.71 |
| 8/13/2013 11:13:27 AM | 0.22417 | 14.30 | 78.71 |
| 8/13/2013 11:13:28 AM | 0.22444 | 14.30 | 78.71 |
| 8/13/2013 11:13:29 AM | 0.22472 | 14.30 | 78.71 |
| 8/13/2013 11:13:30 AM | 0.22500 | 14.30 | 78.71 |
| 8/13/2013 11:13:31 AM | 0.22528 | 14.30 | 78.71 |
| 8/13/2013 11:13:32 AM | 0.22556 | 14.30 | 78.71 |
| 8/13/2013 11:13:33 AM | 0.22583 | 14.30 | 78.72 |
| 8/13/2013 11:13:34 AM | 0.22611 | 14.30 | 78.72 |
| 8/13/2013 11:13:35 AM | 0.22639 | 14.30 | 78.72 |
| 8/13/2013 11:13:36 AM | 0.22667 | 14.30 | 78.72 |
| 8/13/2013 11:13:37 AM | 0.22694 | 14.30 | 78.72 |
| 8/13/2013 11:13:38 AM | 0.22722 | 14.30 | 78.72 |
| 8/13/2013 11:13:39 AM | 0.22750 | 14.30 | 78.72 |
| 8/13/2013 11:13:40 AM | 0.22778 | 14.30 | 78.72 |
| 8/13/2013 11:13:41 AM | 0.22806 | 14.30 | 78.72 |
| 8/13/2013 11:13:42 AM | 0.22833 | 14.30 | 78.72 |
| 8/13/2013 11:13:43 AM | 0.22861 | 14.30 | 78.72 |
| 8/13/2013 11:13:44 AM | 0.22889 | 14.30 | 78.72 |
| 8/13/2013 11:13:45 AM | 0.22917 | 14.30 | 78.72 |
| 8/13/2013 11:13:46 AM | 0.22944 | 14.30 | 78.72 |
| 8/13/2013 11:13:47 AM | 0.22972 | 14.30 | 78.72 |
| 8/13/2013 11:13:48 AM | 0.23000 | 14.30 | 78.73 |
| 8/13/2013 11:13:49 AM | 0.23028 | 14.30 | 78.73 |
| 8/13/2013 11:13:50 AM | 0.23056 | 14.30 | 78.73 |
| 8/13/2013 11:13:51 AM | 0.23083 | 14.30 | 78.73 |
| 8/13/2013 11:13:52 AM | 0.23111 | 14.30 | 78.73 |
| 8/13/2013 11:13:53 AM | 0.23139 | 14.30 | 78.73 |
| 8/13/2013 11:13:54 AM | 0.23167 | 14.30 | 78.73 |
| 8/13/2013 11:13:55 AM | 0.23194 | 14.30 | 78.73 |
| 8/13/2013 11:13:56 AM | 0.23222 | 14.30 | 78.73 |
| 8/13/2013 11:13:57 AM | 0.23250 | 14.30 | 78.73 |
| 8/13/2013 11:13:58 AM | 0.23278 | 14.30 | 78.73 |
| 8/13/2013 11:13:59 AM | 0.23306 | 14.30 | 78.73 |
| 8/13/2013 11:14:00 AM | 0.23333 | 14.30 | 78.73 |
| 8/13/2013 11:14:01 AM | 0.23361 | 14.30 | 78.73 |
| 8/13/2013 11:14:02 AM | 0.23389 | 14.30 | 78.74 |
| 8/13/2013 11:14:03 AM | 0.23417 | 14.30 | 78.74 |
| 8/13/2013 11:14:04 AM | 0.23444 | 14.30 | 78.74 |
| 8/13/2013 11:14:05 AM | 0.23472 | 14.30 | 78.74 |
| 8/13/2013 11:14:06 AM | 0.23500 | 14.30 | 78.74 |
| 8/13/2013 11:14:07 AM | 0.23528 | 14.30 | 78.74 |
| 8/13/2013 11:14:08 AM | 0.23556 | 14.30 | 78.74 |
| 8/13/2013 11:14:09 AM | 0.23583 | 14.30 | 78.74 |
| 8/13/2013 11:14:10 AM | 0.23611 | 14.30 | 78.74 |
| 8/13/2013 11:14:11 AM | 0.23639 | 14.30 | 78.74 |
| 8/13/2013 11:14:12 AM | 0.23667 | 14.30 | 78.74 |
| 8/13/2013 11:14:13 AM | 0.23694 | 14.30 | 78.74 |
| 8/13/2013 11:14:14 AM | 0.23722 | 14.30 | 78.74 |
| 8/13/2013 11:14:15 AM | 0.23750 | 14.30 | 78.74 |
| 8/13/2013 11:14:16 AM | 0.23778 | 14.30 | 78.75 |
| 8/13/2013 11:14:17 AM | 0.23806 | 14.30 | 78.75 |
| 8/13/2013 11:14:18 AM | 0.23833 | 14.30 | 78.75 |
| 8/13/2013 11:14:19 AM | 0.23861 | 14.30 | 78.75 |
| 8/13/2013 11:14:20 AM | 0.23889 | 14.30 | 78.75 |
| 8/13/2013 11:14:21 AM | 0.23917 | 14.30 | 78.75 |
| 8/13/2013 11:14:22 AM | 0.23944 | 14.30 | 78.75 |
| 8/13/2013 11:14:23 AM | 0.23972 | 14.30 | 78.75 |
| 8/13/2013 11:14:24 AM | 0.24000 | 14.30 | 78.75 |
| 8/13/2013 11:14:25 AM | 0.24028 | 14.30 | 78.75 |
| 8/13/2013 11:14:26 AM | 0.24056 | 14.30 | 78.75 |
| 8/13/2013 11:14:27 AM | 0.24083 | 14.30 | 78.75 |
| 8/13/2013 11:14:28 AM | 0.24111 | 14.30 | 78.75 |
| 8/13/2013 11:14:29 AM | 0.24139 | 14.30 | 78.75 |
| 8/13/2013 11:14:30 AM | 0.24167 | 14.30 | 78.75 |
| 8/13/2013 11:14:31 AM | 0.24194 | 14.30 | 78.75 |
| 8/13/2013 11:14:32 AM | 0.24222 | 14.30 | 78.75 |
| 8/13/2013 11:14:33 AM | 0.24250 | 14.30 | 78.76 |
| 8/13/2013 11:14:34 AM | 0.24278 | 14.30 | 78.76 |
| 8/13/2013 11:14:35 AM | 0.24306 | 14.30 | 78.76 |
| 8/13/2013 11:14:36 AM | 0.24333 | 14.30 | 78.76 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:14:37 AM | 0.24361 | 14.30 | 78.76 |
| 8/13/2013 11:14:38 AM | 0.24389 | 14.30 | 78.76 |
| 8/13/2013 11:14:39 AM | 0.24417 | 14.30 | 78.76 |
| 8/13/2013 11:14:40 AM | 0.24444 | 14.30 | 78.76 |
| 8/13/2013 11:14:41 AM | 0.24472 | 14.30 | 78.76 |
| 8/13/2013 11:14:42 AM | 0.24500 | 14.30 | 78.76 |
| 8/13/2013 11:14:43 AM | 0.24528 | 14.30 | 78.76 |
| 8/13/2013 11:14:44 AM | 0.24556 | 14.30 | 78.76 |
| 8/13/2013 11:14:45 AM | 0.24583 | 14.30 | 78.76 |
| 8/13/2013 11:14:46 AM | 0.24611 | 14.30 | 78.76 |
| 8/13/2013 11:14:47 AM | 0.24639 | 14.30 | 78.76 |
| 8/13/2013 11:14:48 AM | 0.24667 | 14.30 | 78.76 |
| 8/13/2013 11:14:49 AM | 0.24694 | 14.30 | 78.77 |
| 8/13/2013 11:14:50 AM | 0.24722 | 14.30 | 78.77 |
| 8/13/2013 11:14:51 AM | 0.24750 | 14.30 | 78.77 |
| 8/13/2013 11:14:52 AM | 0.24778 | 14.30 | 78.77 |
| 8/13/2013 11:14:53 AM | 0.24806 | 14.30 | 78.77 |
| 8/13/2013 11:14:54 AM | 0.24833 | 14.30 | 78.77 |
| 8/13/2013 11:14:55 AM | 0.24861 | 14.30 | 78.77 |
| 8/13/2013 11:14:56 AM | 0.24889 | 14.30 | 78.77 |
| 8/13/2013 11:14:57 AM | 0.24917 | 14.30 | 78.77 |
| 8/13/2013 11:14:58 AM | 0.24944 | 14.30 | 78.77 |
| 8/13/2013 11:14:59 AM | 0.24972 | 14.30 | 78.77 |
| 8/13/2013 11:15:00 AM | 0.25000 | 14.30 | 78.77 |
| 8/13/2013 11:15:01 AM | 0.25028 | 14.30 | 78.77 |
| 8/13/2013 11:15:02 AM | 0.25056 | 14.30 | 78.77 |
| 8/13/2013 11:15:03 AM | 0.25083 | 14.30 | 78.77 |
| 8/13/2013 11:15:04 AM | 0.25111 | 14.30 | 78.77 |
| 8/13/2013 11:15:05 AM | 0.25139 | 14.30 | 78.77 |
| 8/13/2013 11:15:06 AM | 0.25167 | 14.30 | 78.78 |
| 8/13/2013 11:15:07 AM | 0.25194 | 14.30 | 78.78 |
| 8/13/2013 11:15:08 AM | 0.25222 | 14.30 | 78.78 |
| 8/13/2013 11:15:09 AM | 0.25250 | 14.30 | 78.78 |
| 8/13/2013 11:15:10 AM | 0.25278 | 14.30 | 78.78 |
| 8/13/2013 11:15:11 AM | 0.25306 | 14.30 | 78.78 |
| 8/13/2013 11:15:12 AM | 0.25333 | 14.30 | 78.78 |
| 8/13/2013 11:15:13 AM | 0.25361 | 14.30 | 78.78 |
| 8/13/2013 11:15:14 AM | 0.25389 | 14.30 | 78.78 |
| 8/13/2013 11:15:15 AM | 0.25417 | 14.30 | 78.78 |
| 8/13/2013 11:15:16 AM | 0.25444 | 14.30 | 78.78 |
| 8/13/2013 11:15:17 AM | 0.25472 | 14.30 | 78.78 |
| 8/13/2013 11:15:18 AM | 0.25500 | 14.30 | 78.78 |
| 8/13/2013 11:15:19 AM | 0.25528 | 14.30 | 78.78 |
| 8/13/2013 11:15:20 AM | 0.25556 | 14.30 | 78.78 |
| 8/13/2013 11:15:21 AM | 0.25583 | 14.30 | 78.78 |
| 8/13/2013 11:15:22 AM | 0.25611 | 14.30 | 78.78 |
| 8/13/2013 11:15:23 AM | 0.25639 | 14.30 | 78.78 |
| 8/13/2013 11:15:24 AM | 0.25667 | 14.30 | 78.78 |
| 8/13/2013 11:15:25 AM | 0.25694 | 14.30 | 78.78 |
| 8/13/2013 11:15:26 AM | 0.25722 | 14.30 | 78.78 |
| 8/13/2013 11:15:27 AM | 0.25750 | 14.30 | 78.79 |
| 8/13/2013 11:15:28 AM | 0.25778 | 14.30 | 78.79 |
| 8/13/2013 11:15:29 AM | 0.25806 | 14.30 | 78.79 |
| 8/13/2013 11:15:30 AM | 0.25833 | 14.30 | 78.79 |
| 8/13/2013 11:15:31 AM | 0.25861 | 14.30 | 78.79 |
| 8/13/2013 11:15:32 AM | 0.25889 | 14.30 | 78.79 |
| 8/13/2013 11:15:33 AM | 0.25917 | 14.30 | 78.79 |
| 8/13/2013 11:15:34 AM | 0.25944 | 14.30 | 78.79 |
| 8/13/2013 11:15:35 AM | 0.25972 | 14.30 | 78.79 |
| 8/13/2013 11:15:36 AM | 0.26000 | 14.30 | 78.79 |
| 8/13/2013 11:15:37 AM | 0.26028 | 14.30 | 78.79 |
| 8/13/2013 11:15:38 AM | 0.26056 | 14.30 | 78.79 |
| 8/13/2013 11:15:39 AM | 0.26083 | 14.30 | 78.79 |
| 8/13/2013 11:15:40 AM | 0.26111 | 14.30 | 78.79 |
| 8/13/2013 11:15:41 AM | 0.26139 | 14.30 | 78.79 |
| 8/13/2013 11:15:42 AM | 0.26167 | 14.30 | 78.80 |
| 8/13/2013 11:15:43 AM | 0.26194 | 14.30 | 78.80 |
| 8/13/2013 11:15:44 AM | 0.26222 | 14.30 | 78.80 |
| 8/13/2013 11:15:45 AM | 0.26250 | 14.30 | 78.80 |
| 8/13/2013 11:15:46 AM | 0.26278 | 14.30 | 78.80 |
| 8/13/2013 11:15:47 AM | 0.26306 | 14.30 | 78.80 |
| 8/13/2013 11:15:48 AM | 0.26333 | 14.30 | 78.80 |
| 8/13/2013 11:15:49 AM | 0.26361 | 14.30 | 78.80 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:15:50 AM | 0.26389 | 14.30 | 78.80 |
| 8/13/2013 11:15:51 AM | 0.26417 | 14.30 | 78.80 |
| 8/13/2013 11:15:52 AM | 0.26444 | 14.30 | 78.80 |
| 8/13/2013 11:15:53 AM | 0.26472 | 14.30 | 78.80 |
| 8/13/2013 11:15:54 AM | 0.26500 | 14.30 | 78.80 |
| 8/13/2013 11:15:55 AM | 0.26528 | 14.30 | 78.80 |
| 8/13/2013 11:15:56 AM | 0.26556 | 14.30 | 78.80 |
| 8/13/2013 11:15:57 AM | 0.26583 | 14.30 | 78.80 |
| 8/13/2013 11:15:58 AM | 0.26611 | 14.30 | 78.80 |
| 8/13/2013 11:15:59 AM | 0.26639 | 14.30 | 78.80 |
| 8/13/2013 11:16:00 AM | 0.26667 | 14.30 | 78.80 |
| 8/13/2013 11:16:01 AM | 0.26694 | 14.30 | 78.80 |
| 8/13/2013 11:16:02 AM | 0.26722 | 14.30 | 78.80 |
| 8/13/2013 11:16:03 AM | 0.26750 | 14.30 | 78.80 |
| 8/13/2013 11:16:04 AM | 0.26778 | 14.30 | 78.80 |
| 8/13/2013 11:16:05 AM | 0.26806 | 14.30 | 78.81 |
| 8/13/2013 11:16:06 AM | 0.26833 | 14.30 | 78.81 |
| 8/13/2013 11:16:07 AM | 0.26861 | 14.30 | 78.81 |
| 8/13/2013 11:16:08 AM | 0.26889 | 14.30 | 78.81 |
| 8/13/2013 11:16:09 AM | 0.26917 | 14.30 | 78.81 |
| 8/13/2013 11:16:10 AM | 0.26944 | 14.30 | 78.81 |
| 8/13/2013 11:16:11 AM | 0.26972 | 14.30 | 78.81 |
| 8/13/2013 11:16:12 AM | 0.27000 | 14.30 | 78.81 |
| 8/13/2013 11:16:13 AM | 0.27028 | 14.30 | 78.81 |
| 8/13/2013 11:16:14 AM | 0.27056 | 14.30 | 78.81 |
| 8/13/2013 11:16:15 AM | 0.27083 | 14.30 | 78.81 |
| 8/13/2013 11:16:16 AM | 0.27111 | 14.30 | 78.81 |
| 8/13/2013 11:16:17 AM | 0.27139 | 14.30 | 78.81 |
| 8/13/2013 11:16:18 AM | 0.27167 | 14.30 | 78.81 |
| 8/13/2013 11:16:19 AM | 0.27194 | 14.30 | 78.81 |
| 8/13/2013 11:16:20 AM | 0.27222 | 14.30 | 78.81 |
| 8/13/2013 11:16:21 AM | 0.27250 | 14.30 | 78.81 |
| 8/13/2013 11:16:22 AM | 0.27278 | 14.30 | 78.81 |
| 8/13/2013 11:16:23 AM | 0.27306 | 14.30 | 78.81 |
| 8/13/2013 11:16:24 AM | 0.27333 | 14.30 | 78.81 |
| 8/13/2013 11:16:25 AM | 0.27361 | 14.30 | 78.81 |
| 8/13/2013 11:16:26 AM | 0.27389 | 14.30 | 78.81 |
| 8/13/2013 11:16:27 AM | 0.27417 | 14.30 | 78.81 |
| 8/13/2013 11:16:28 AM | 0.27444 | 14.30 | 78.81 |
| 8/13/2013 11:16:29 AM | 0.27472 | 14.30 | 78.81 |
| 8/13/2013 11:16:30 AM | 0.27500 | 14.30 | 78.82 |
| 8/13/2013 11:16:31 AM | 0.27528 | 14.30 | 78.82 |
| 8/13/2013 11:16:32 AM | 0.27556 | 14.30 | 78.82 |
| 8/13/2013 11:16:33 AM | 0.27583 | 14.30 | 78.82 |
| 8/13/2013 11:16:34 AM | 0.27611 | 14.30 | 78.82 |
| 8/13/2013 11:16:35 AM | 0.27639 | 14.30 | 78.82 |
| 8/13/2013 11:16:36 AM | 0.27667 | 14.30 | 78.82 |
| 8/13/2013 11:16:37 AM | 0.27694 | 14.30 | 78.82 |
| 8/13/2013 11:16:38 AM | 0.27722 | 14.30 | 78.82 |
| 8/13/2013 11:16:39 AM | 0.27750 | 14.30 | 78.82 |
| 8/13/2013 11:16:40 AM | 0.27778 | 14.30 | 78.82 |
| 8/13/2013 11:16:41 AM | 0.27806 | 14.30 | 78.82 |
| 8/13/2013 11:16:42 AM | 0.27833 | 14.30 | 78.82 |
| 8/13/2013 11:16:43 AM | 0.27861 | 14.30 | 78.82 |
| 8/13/2013 11:16:44 AM | 0.27889 | 14.30 | 78.82 |
| 8/13/2013 11:16:45 AM | 0.27917 | 14.30 | 78.82 |
| 8/13/2013 11:16:46 AM | 0.27944 | 14.30 | 78.82 |
| 8/13/2013 11:16:47 AM | 0.27972 | 14.30 | 78.82 |
| 8/13/2013 11:16:48 AM | 0.28000 | 14.30 | 78.82 |
| 8/13/2013 11:16:49 AM | 0.28028 | 14.30 | 78.83 |
| 8/13/2013 11:16:50 AM | 0.28056 | 14.30 | 78.83 |
| 8/13/2013 11:16:51 AM | 0.28083 | 14.30 | 78.83 |
| 8/13/2013 11:16:52 AM | 0.28111 | 14.30 | 78.83 |
| 8/13/2013 11:16:53 AM | 0.28139 | 14.30 | 78.83 |
| 8/13/2013 11:16:54 AM | 0.28167 | 14.30 | 78.83 |
| 8/13/2013 11:16:55 AM | 0.28194 | 14.30 | 78.83 |
| 8/13/2013 11:16:56 AM | 0.28222 | 14.30 | 78.83 |
| 8/13/2013 11:16:57 AM | 0.28250 | 14.30 | 78.83 |
| 8/13/2013 11:16:58 AM | 0.28278 | 14.30 | 78.83 |
| 8/13/2013 11:16:59 AM | 0.28306 | 14.30 | 78.83 |
| 8/13/2013 11:17:00 AM | 0.28333 | 14.30 | 78.83 |
| 8/13/2013 11:17:01 AM | 0.28361 | 14.30 | 78.83 |
| 8/13/2013 11:17:02 AM | 0.28389 | 14.30 | 78.83 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:17:03 AM | 0.28417 | 14.30 | 78.83 |
| 8/13/2013 11:17:04 AM | 0.28444 | 14.30 | 78.83 |
| 8/13/2013 11:17:05 AM | 0.28472 | 14.30 | 78.83 |
| 8/13/2013 11:17:06 AM | 0.28500 | 14.30 | 78.83 |
| 8/13/2013 11:17:07 AM | 0.28528 | 14.30 | 78.83 |
| 8/13/2013 11:17:08 AM | 0.28556 | 14.30 | 78.83 |
| 8/13/2013 11:17:09 AM | 0.28583 | 14.30 | 78.83 |
| 8/13/2013 11:17:10 AM | 0.28611 | 14.30 | 78.83 |
| 8/13/2013 11:17:11 AM | 0.28639 | 14.30 | 78.83 |
| 8/13/2013 11:17:12 AM | 0.28667 | 14.30 | 78.83 |
| 8/13/2013 11:17:13 AM | 0.28694 | 14.30 | 78.83 |
| 8/13/2013 11:17:14 AM | 0.28722 | 14.30 | 78.83 |
| 8/13/2013 11:17:15 AM | 0.28750 | 14.30 | 78.83 |
| 8/13/2013 11:17:16 AM | 0.28778 | 14.30 | 78.83 |
| 8/13/2013 11:17:17 AM | 0.28806 | 14.30 | 78.83 |
| 8/13/2013 11:17:18 AM | 0.28833 | 14.30 | 78.83 |
| 8/13/2013 11:17:19 AM | 0.28861 | 14.30 | 78.84 |
| 8/13/2013 11:17:20 AM | 0.28889 | 14.30 | 78.84 |
| 8/13/2013 11:17:21 AM | 0.28917 | 14.30 | 78.84 |
| 8/13/2013 11:17:22 AM | 0.28944 | 14.30 | 78.84 |
| 8/13/2013 11:17:23 AM | 0.28972 | 14.30 | 78.84 |
| 8/13/2013 11:17:24 AM | 0.29000 | 14.30 | 78.84 |
| 8/13/2013 11:17:25 AM | 0.29028 | 14.30 | 78.84 |
| 8/13/2013 11:17:26 AM | 0.29056 | 14.30 | 78.84 |
| 8/13/2013 11:17:27 AM | 0.29083 | 14.30 | 78.84 |
| 8/13/2013 11:17:28 AM | 0.29111 | 14.30 | 78.84 |
| 8/13/2013 11:17:29 AM | 0.29139 | 14.30 | 78.84 |
| 8/13/2013 11:17:30 AM | 0.29167 | 14.30 | 78.84 |
| 8/13/2013 11:17:31 AM | 0.29194 | 14.30 | 78.84 |
| 8/13/2013 11:17:32 AM | 0.29222 | 14.30 | 78.84 |
| 8/13/2013 11:17:33 AM | 0.29250 | 14.30 | 78.84 |
| 8/13/2013 11:17:34 AM | 0.29278 | 14.30 | 78.84 |
| 8/13/2013 11:17:35 AM | 0.29306 | 14.30 | 78.84 |
| 8/13/2013 11:17:36 AM | 0.29333 | 14.30 | 78.84 |
| 8/13/2013 11:17:37 AM | 0.29361 | 14.30 | 78.84 |
| 8/13/2013 11:17:38 AM | 0.29389 | 14.30 | 78.84 |
| 8/13/2013 11:17:39 AM | 0.29417 | 14.30 | 78.84 |
| 8/13/2013 11:17:40 AM | 0.29444 | 14.30 | 78.84 |
| 8/13/2013 11:17:41 AM | 0.29472 | 14.30 | 78.84 |
| 8/13/2013 11:17:42 AM | 0.29500 | 14.30 | 78.84 |
| 8/13/2013 11:17:43 AM | 0.29528 | 14.30 | 78.84 |
| 8/13/2013 11:17:44 AM | 0.29556 | 14.30 | 78.84 |
| 8/13/2013 11:17:45 AM | 0.29583 | 14.30 | 78.84 |
| 8/13/2013 11:17:46 AM | 0.29611 | 14.30 | 78.84 |
| 8/13/2013 11:17:47 AM | 0.29639 | 14.30 | 78.85 |
| 8/13/2013 11:17:48 AM | 0.29667 | 14.30 | 78.85 |
| 8/13/2013 11:17:49 AM | 0.29694 | 14.30 | 78.85 |
| 8/13/2013 11:17:50 AM | 0.29722 | 14.30 | 78.85 |
| 8/13/2013 11:17:51 AM | 0.29750 | 14.30 | 78.85 |
| 8/13/2013 11:17:52 AM | 0.29778 | 14.30 | 78.85 |
| 8/13/2013 11:17:53 AM | 0.29806 | 14.30 | 78.85 |
| 8/13/2013 11:17:54 AM | 0.29833 | 14.30 | 78.85 |
| 8/13/2013 11:17:55 AM | 0.29861 | 14.30 | 78.85 |
| 8/13/2013 11:17:56 AM | 0.29889 | 14.30 | 78.85 |
| 8/13/2013 11:17:57 AM | 0.29917 | 14.30 | 78.85 |
| 8/13/2013 11:17:58 AM | 0.29944 | 14.30 | 78.85 |
| 8/13/2013 11:17:59 AM | 0.29972 | 14.30 | 78.85 |
| 8/13/2013 11:18:00 AM | 0.30000 | 14.30 | 78.85 |
| 8/13/2013 11:18:01 AM | 0.30028 | 14.30 | 78.85 |
| 8/13/2013 11:18:02 AM | 0.30056 | 14.30 | 78.85 |
| 8/13/2013 11:18:03 AM | 0.30083 | 14.30 | 78.85 |
| 8/13/2013 11:18:04 AM | 0.30111 | 14.30 | 78.85 |
| 8/13/2013 11:18:05 AM | 0.30139 | 14.30 | 78.85 |
| 8/13/2013 11:18:06 AM | 0.30167 | 14.30 | 78.85 |
| 8/13/2013 11:18:07 AM | 0.30194 | 14.30 | 78.85 |
| 8/13/2013 11:18:08 AM | 0.30222 | 14.30 | 78.85 |
| 8/13/2013 11:18:09 AM | 0.30250 | 14.30 | 78.85 |
| 8/13/2013 11:18:10 AM | 0.30278 | 14.30 | 78.85 |
| 8/13/2013 11:18:11 AM | 0.30306 | 14.30 | 78.85 |
| 8/13/2013 11:18:12 AM | 0.30333 | 14.30 | 78.85 |
| 8/13/2013 11:18:13 AM | 0.30361 | 14.30 | 78.86 |
| 8/13/2013 11:18:14 AM | 0.30389 | 14.30 | 78.86 |
| 8/13/2013 11:18:15 AM | 0.30417 | 14.30 | 78.86 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:18:16 AM | 0.30444 | 14.30 | 78.86 |
| 8/13/2013 11:18:17 AM | 0.30472 | 14.30 | 78.86 |
| 8/13/2013 11:18:18 AM | 0.30500 | 14.30 | 78.86 |
| 8/13/2013 11:18:19 AM | 0.30528 | 14.30 | 78.86 |
| 8/13/2013 11:18:20 AM | 0.30556 | 14.30 | 78.86 |
| 8/13/2013 11:18:21 AM | 0.30583 | 14.30 | 78.86 |
| 8/13/2013 11:18:22 AM | 0.30611 | 14.30 | 78.86 |
| 8/13/2013 11:18:23 AM | 0.30639 | 14.30 | 78.86 |
| 8/13/2013 11:18:24 AM | 0.30667 | 14.30 | 78.86 |
| 8/13/2013 11:18:25 AM | 0.30694 | 14.30 | 78.86 |
| 8/13/2013 11:18:26 AM | 0.30722 | 14.30 | 78.86 |
| 8/13/2013 11:18:27 AM | 0.30750 | 14.30 | 78.86 |
| 8/13/2013 11:18:28 AM | 0.30778 | 14.30 | 78.86 |
| 8/13/2013 11:18:29 AM | 0.30806 | 14.30 | 78.86 |
| 8/13/2013 11:18:30 AM | 0.30833 | 14.30 | 78.86 |
| 8/13/2013 11:18:31 AM | 0.30861 | 14.30 | 78.86 |
| 8/13/2013 11:18:32 AM | 0.30889 | 14.30 | 78.86 |
| 8/13/2013 11:18:33 AM | 0.30917 | 14.30 | 78.86 |
| 8/13/2013 11:18:34 AM | 0.30944 | 14.30 | 78.86 |
| 8/13/2013 11:18:35 AM | 0.30972 | 14.30 | 78.86 |
| 8/13/2013 11:18:36 AM | 0.31000 | 14.30 | 78.86 |
| 8/13/2013 11:18:37 AM | 0.31028 | 14.30 | 78.86 |
| 8/13/2013 11:18:38 AM | 0.31056 | 14.30 | 78.86 |
| 8/13/2013 11:18:39 AM | 0.31083 | 14.30 | 78.86 |
| 8/13/2013 11:18:40 AM | 0.31111 | 14.30 | 78.86 |
| 8/13/2013 11:18:41 AM | 0.31139 | 14.30 | 78.86 |
| 8/13/2013 11:18:42 AM | 0.31167 | 14.30 | 78.86 |
| 8/13/2013 11:18:43 AM | 0.31194 | 14.30 | 78.86 |
| 8/13/2013 11:18:44 AM | 0.31222 | 14.30 | 78.86 |
| 8/13/2013 11:18:45 AM | 0.31250 | 14.30 | 78.86 |
| 8/13/2013 11:18:46 AM | 0.31278 | 14.30 | 78.86 |
| 8/13/2013 11:18:47 AM | 0.31306 | 14.30 | 78.86 |
| 8/13/2013 11:18:48 AM | 0.31333 | 14.30 | 78.86 |
| 8/13/2013 11:18:49 AM | 0.31361 | 14.30 | 78.86 |
| 8/13/2013 11:18:50 AM | 0.31389 | 14.30 | 78.86 |
| 8/13/2013 11:18:51 AM | 0.31417 | 14.30 | 78.86 |
| 8/13/2013 11:18:52 AM | 0.31444 | 14.30 | 78.87 |
| 8/13/2013 11:18:53 AM | 0.31472 | 14.30 | 78.87 |
| 8/13/2013 11:18:54 AM | 0.31500 | 14.30 | 78.87 |
| 8/13/2013 11:18:55 AM | 0.31528 | 14.30 | 78.87 |
| 8/13/2013 11:18:56 AM | 0.31556 | 14.30 | 78.87 |
| 8/13/2013 11:18:57 AM | 0.31583 | 14.30 | 78.87 |
| 8/13/2013 11:18:58 AM | 0.31611 | 14.30 | 78.87 |
| 8/13/2013 11:18:59 AM | 0.31639 | 14.30 | 78.87 |
| 8/13/2013 11:19:00 AM | 0.31667 | 14.30 | 78.87 |
| 8/13/2013 11:19:01 AM | 0.31694 | 14.30 | 78.87 |
| 8/13/2013 11:19:02 AM | 0.31722 | 14.30 | 78.87 |
| 8/13/2013 11:19:03 AM | 0.31750 | 14.30 | 78.87 |
| 8/13/2013 11:19:04 AM | 0.31778 | 14.30 | 78.87 |
| 8/13/2013 11:19:05 AM | 0.31806 | 14.30 | 78.87 |
| 8/13/2013 11:19:06 AM | 0.31833 | 14.30 | 78.87 |
| 8/13/2013 11:19:07 AM | 0.31861 | 14.30 | 78.87 |
| 8/13/2013 11:19:08 AM | 0.31889 | 14.30 | 78.87 |
| 8/13/2013 11:19:09 AM | 0.31917 | 14.30 | 78.87 |
| 8/13/2013 11:19:10 AM | 0.31944 | 14.30 | 78.87 |
| 8/13/2013 11:19:11 AM | 0.31972 | 14.30 | 78.87 |
| 8/13/2013 11:19:12 AM | 0.32000 | 14.30 | 78.87 |
| 8/13/2013 11:19:13 AM | 0.32028 | 14.30 | 78.87 |
| 8/13/2013 11:19:14 AM | 0.32056 | 14.30 | 78.87 |
| 8/13/2013 11:19:15 AM | 0.32083 | 14.30 | 78.87 |
| 8/13/2013 11:19:16 AM | 0.32111 | 14.30 | 78.87 |
| 8/13/2013 11:19:17 AM | 0.32139 | 14.30 | 78.87 |
| 8/13/2013 11:19:18 AM | 0.32167 | 14.30 | 78.87 |
| 8/13/2013 11:19:19 AM | 0.32194 | 14.30 | 78.87 |
| 8/13/2013 11:19:20 AM | 0.32222 | 14.30 | 78.87 |
| 8/13/2013 11:19:21 AM | 0.32250 | 14.30 | 78.87 |
| 8/13/2013 11:19:22 AM | 0.32278 | 14.30 | 78.87 |
| 8/13/2013 11:19:23 AM | 0.32306 | 14.30 | 78.87 |
| 8/13/2013 11:19:24 AM | 0.32333 | 14.30 | 78.87 |
| 8/13/2013 11:19:25 AM | 0.32361 | 14.30 | 78.87 |
| 8/13/2013 11:19:26 AM | 0.32389 | 14.30 | 78.87 |
| 8/13/2013 11:19:27 AM | 0.32417 | 14.30 | 78.87 |
| 8/13/2013 11:19:28 AM | 0.32444 | 14.30 | 78.87 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:19:29 AM | 0.32472 | 14.30 | 78.87 |
| 8/13/2013 11:19:30 AM | 0.32500 | 14.30 | 78.87 |
| 8/13/2013 11:19:31 AM | 0.32528 | 14.30 | 78.87 |
| 8/13/2013 11:19:32 AM | 0.32556 | 14.30 | 78.87 |
| 8/13/2013 11:19:33 AM | 0.32583 | 14.30 | 78.87 |
| 8/13/2013 11:19:34 AM | 0.32611 | 14.30 | 78.87 |
| 8/13/2013 11:19:35 AM | 0.32639 | 14.30 | 78.88 |
| 8/13/2013 11:19:36 AM | 0.32667 | 14.30 | 78.88 |
| 8/13/2013 11:19:37 AM | 0.32694 | 14.30 | 78.88 |
| 8/13/2013 11:19:38 AM | 0.32722 | 14.30 | 78.88 |
| 8/13/2013 11:19:39 AM | 0.32750 | 14.30 | 78.88 |
| 8/13/2013 11:19:40 AM | 0.32778 | 14.30 | 78.88 |
| 8/13/2013 11:19:41 AM | 0.32806 | 14.30 | 78.88 |
| 8/13/2013 11:19:42 AM | 0.32833 | 14.30 | 78.88 |
| 8/13/2013 11:19:43 AM | 0.32861 | 14.30 | 78.88 |
| 8/13/2013 11:19:44 AM | 0.32889 | 14.30 | 78.88 |
| 8/13/2013 11:19:45 AM | 0.32917 | 14.30 | 78.88 |
| 8/13/2013 11:19:46 AM | 0.32944 | 14.30 | 78.88 |
| 8/13/2013 11:19:47 AM | 0.32972 | 14.30 | 78.88 |
| 8/13/2013 11:19:48 AM | 0.33000 | 14.30 | 78.88 |
| 8/13/2013 11:19:49 AM | 0.33028 | 14.30 | 78.88 |
| 8/13/2013 11:19:50 AM | 0.33056 | 14.30 | 78.88 |
| 8/13/2013 11:19:51 AM | 0.33083 | 14.30 | 78.88 |
| 8/13/2013 11:19:52 AM | 0.33111 | 14.30 | 78.88 |
| 8/13/2013 11:19:53 AM | 0.33139 | 14.30 | 78.88 |
| 8/13/2013 11:19:54 AM | 0.33167 | 14.30 | 78.88 |
| 8/13/2013 11:19:55 AM | 0.33194 | 14.30 | 78.88 |
| 8/13/2013 11:19:56 AM | 0.33222 | 14.30 | 78.88 |
| 8/13/2013 11:19:57 AM | 0.33250 | 14.30 | 78.88 |
| 8/13/2013 11:19:58 AM | 0.33278 | 14.30 | 78.88 |
| 8/13/2013 11:19:59 AM | 0.33306 | 14.30 | 78.88 |
| 8/13/2013 11:20:00 AM | 0.33333 | 14.30 | 78.88 |
| 8/13/2013 11:20:01 AM | 0.33361 | 14.30 | 78.88 |
| 8/13/2013 11:20:02 AM | 0.33389 | 14.30 | 78.88 |
| 8/13/2013 11:20:03 AM | 0.33417 | 14.30 | 78.88 |
| 8/13/2013 11:20:04 AM | 0.33444 | 14.30 | 78.88 |
| 8/13/2013 11:20:05 AM | 0.33472 | 14.30 | 78.88 |
| 8/13/2013 11:20:06 AM | 0.33500 | 14.30 | 78.88 |
| 8/13/2013 11:20:07 AM | 0.33528 | 14.30 | 78.88 |
| 8/13/2013 11:20:08 AM | 0.33556 | 14.30 | 78.88 |
| 8/13/2013 11:20:09 AM | 0.33583 | 14.30 | 78.88 |
| 8/13/2013 11:20:10 AM | 0.33611 | 14.30 | 78.88 |
| 8/13/2013 11:20:11 AM | 0.33639 | 14.30 | 78.88 |
| 8/13/2013 11:20:12 AM | 0.33667 | 14.30 | 78.88 |
| 8/13/2013 11:20:13 AM | 0.33694 | 14.30 | 78.88 |
| 8/13/2013 11:20:14 AM | 0.33722 | 14.30 | 78.88 |
| 8/13/2013 11:20:15 AM | 0.33750 | 14.30 | 78.88 |
| 8/13/2013 11:20:16 AM | 0.33778 | 14.30 | 78.88 |
| 8/13/2013 11:20:17 AM | 0.33806 | 14.30 | 78.88 |
| 8/13/2013 11:20:18 AM | 0.33833 | 14.30 | 78.88 |
| 8/13/2013 11:20:19 AM | 0.33861 | 14.30 | 78.88 |
| 8/13/2013 11:20:20 AM | 0.33889 | 14.30 | 78.88 |
| 8/13/2013 11:20:21 AM | 0.33917 | 14.30 | 78.88 |
| 8/13/2013 11:20:22 AM | 0.33944 | 14.30 | 78.88 |
| 8/13/2013 11:20:23 AM | 0.33972 | 14.30 | 78.88 |
| 8/13/2013 11:20:24 AM | 0.34000 | 14.30 | 78.88 |
| 8/13/2013 11:20:25 AM | 0.34028 | 14.30 | 78.88 |
| 8/13/2013 11:20:26 AM | 0.34056 | 14.30 | 78.88 |
| 8/13/2013 11:20:27 AM | 0.34083 | 14.30 | 78.88 |
| 8/13/2013 11:20:28 AM | 0.34111 | 14.30 | 78.88 |
| 8/13/2013 11:20:29 AM | 0.34139 | 14.30 | 78.89 |
| 8/13/2013 11:20:30 AM | 0.34167 | 14.30 | 78.89 |
| 8/13/2013 11:20:31 AM | 0.34194 | 14.30 | 78.89 |
| 8/13/2013 11:20:32 AM | 0.34222 | 14.30 | 78.89 |
| 8/13/2013 11:20:33 AM | 0.34250 | 14.30 | 78.89 |
| 8/13/2013 11:20:34 AM | 0.34278 | 14.30 | 78.89 |
| 8/13/2013 11:20:35 AM | 0.34306 | 14.30 | 78.89 |
| 8/13/2013 11:20:36 AM | 0.34333 | 14.30 | 78.89 |
| 8/13/2013 11:20:37 AM | 0.34361 | 14.30 | 78.89 |
| 8/13/2013 11:20:38 AM | 0.34389 | 14.30 | 78.89 |
| 8/13/2013 11:20:39 AM | 0.34417 | 14.30 | 78.89 |
| 8/13/2013 11:20:40 AM | 0.34444 | 14.30 | 78.89 |
| 8/13/2013 11:20:41 AM | 0.34472 | 14.30 | 78.89 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:20:42 AM | 0.34500 | 14.30 | 78.89 |
| 8/13/2013 11:20:43 AM | 0.34528 | 14.30 | 78.89 |
| 8/13/2013 11:20:44 AM | 0.34556 | 14.30 | 78.89 |
| 8/13/2013 11:20:45 AM | 0.34583 | 14.30 | 78.89 |
| 8/13/2013 11:20:46 AM | 0.34611 | 14.30 | 78.89 |
| 8/13/2013 11:20:47 AM | 0.34639 | 14.30 | 78.89 |
| 8/13/2013 11:20:48 AM | 0.34667 | 14.30 | 78.89 |
| 8/13/2013 11:20:49 AM | 0.34694 | 14.30 | 78.89 |
| 8/13/2013 11:20:50 AM | 0.34722 | 14.30 | 78.89 |
| 8/13/2013 11:20:51 AM | 0.34750 | 14.30 | 78.89 |
| 8/13/2013 11:20:52 AM | 0.34778 | 14.30 | 78.89 |
| 8/13/2013 11:20:53 AM | 0.34806 | 14.30 | 78.89 |
| 8/13/2013 11:20:54 AM | 0.34833 | 14.30 | 78.89 |
| 8/13/2013 11:20:55 AM | 0.34861 | 14.30 | 78.89 |
| 8/13/2013 11:20:56 AM | 0.34889 | 14.30 | 78.89 |
| 8/13/2013 11:20:57 AM | 0.34917 | 14.30 | 78.89 |
| 8/13/2013 11:20:58 AM | 0.34944 | 14.30 | 78.89 |
| 8/13/2013 11:20:59 AM | 0.34972 | 14.30 | 78.89 |
| 8/13/2013 11:21:00 AM | 0.35000 | 14.30 | 78.89 |
| 8/13/2013 11:21:01 AM | 0.35028 | 14.30 | 78.89 |
| 8/13/2013 11:21:02 AM | 0.35056 | 14.30 | 78.89 |
| 8/13/2013 11:21:03 AM | 0.35083 | 14.30 | 78.89 |
| 8/13/2013 11:21:04 AM | 0.35111 | 14.30 | 78.89 |
| 8/13/2013 11:21:05 AM | 0.35139 | 14.30 | 78.89 |
| 8/13/2013 11:21:06 AM | 0.35167 | 14.30 | 78.89 |
| 8/13/2013 11:21:07 AM | 0.35194 | 14.30 | 78.89 |
| 8/13/2013 11:21:08 AM | 0.35222 | 14.30 | 78.89 |
| 8/13/2013 11:21:09 AM | 0.35250 | 14.30 | 78.89 |
| 8/13/2013 11:21:10 AM | 0.35278 | 14.30 | 78.89 |
| 8/13/2013 11:21:11 AM | 0.35306 | 14.30 | 78.89 |
| 8/13/2013 11:21:12 AM | 0.35333 | 14.30 | 78.89 |
| 8/13/2013 11:21:13 AM | 0.35361 | 14.30 | 78.89 |
| 8/13/2013 11:21:14 AM | 0.35389 | 14.30 | 78.89 |
| 8/13/2013 11:21:15 AM | 0.35417 | 14.30 | 78.89 |
| 8/13/2013 11:21:16 AM | 0.35444 | 14.30 | 78.89 |
| 8/13/2013 11:21:17 AM | 0.35472 | 14.30 | 78.89 |
| 8/13/2013 11:21:18 AM | 0.35500 | 14.30 | 78.89 |
| 8/13/2013 11:21:19 AM | 0.35528 | 14.30 | 78.89 |
| 8/13/2013 11:21:20 AM | 0.35556 | 14.30 | 78.89 |
| 8/13/2013 11:21:21 AM | 0.35583 | 14.30 | 78.89 |
| 8/13/2013 11:21:22 AM | 0.35611 | 14.30 | 78.89 |
| 8/13/2013 11:21:23 AM | 0.35639 | 14.30 | 78.89 |
| 8/13/2013 11:21:24 AM | 0.35667 | 14.30 | 78.89 |
| 8/13/2013 11:21:25 AM | 0.35694 | 14.30 | 78.89 |
| 8/13/2013 11:21:26 AM | 0.35722 | 14.30 | 78.89 |
| 8/13/2013 11:21:27 AM | 0.35750 | 14.30 | 78.89 |
| 8/13/2013 11:21:28 AM | 0.35778 | 14.30 | 78.89 |
| 8/13/2013 11:21:29 AM | 0.35806 | 14.30 | 78.89 |
| 8/13/2013 11:21:30 AM | 0.35833 | 14.30 | 78.89 |
| 8/13/2013 11:21:31 AM | 0.35861 | 14.30 | 78.89 |
| 8/13/2013 11:21:32 AM | 0.35889 | 14.30 | 78.89 |
| 8/13/2013 11:21:33 AM | 0.35917 | 14.30 | 78.89 |
| 8/13/2013 11:21:34 AM | 0.35944 | 14.30 | 78.89 |
| 8/13/2013 11:21:35 AM | 0.35972 | 14.30 | 78.89 |
| 8/13/2013 11:21:36 AM | 0.36000 | 14.30 | 78.89 |
| 8/13/2013 11:21:37 AM | 0.36028 | 14.30 | 78.89 |
| 8/13/2013 11:21:38 AM | 0.36056 | 14.30 | 78.89 |
| 8/13/2013 11:21:39 AM | 0.36083 | 14.30 | 78.89 |
| 8/13/2013 11:21:40 AM | 0.36111 | 14.30 | 78.89 |
| 8/13/2013 11:21:41 AM | 0.36139 | 14.30 | 78.89 |
| 8/13/2013 11:21:42 AM | 0.36167 | 14.30 | 78.89 |
| 8/13/2013 11:21:43 AM | 0.36194 | 14.30 | 78.89 |
| 8/13/2013 11:21:44 AM | 0.36222 | 14.30 | 78.89 |
| 8/13/2013 11:21:45 AM | 0.36250 | 14.30 | 78.89 |
| 8/13/2013 11:21:46 AM | 0.36278 | 14.30 | 78.89 |
| 8/13/2013 11:21:47 AM | 0.36306 | 14.30 | 78.89 |
| 8/13/2013 11:21:48 AM | 0.36333 | 14.30 | 78.89 |
| 8/13/2013 11:21:49 AM | 0.36361 | 14.30 | 78.89 |
| 8/13/2013 11:21:50 AM | 0.36389 | 14.30 | 78.89 |
| 8/13/2013 11:21:51 AM | 0.36417 | 14.30 | 78.89 |
| 8/13/2013 11:21:52 AM | 0.36444 | 14.30 | 78.89 |
| 8/13/2013 11:21:53 AM | 0.36472 | 14.30 | 78.89 |
| 8/13/2013 11:21:54 AM | 0.36500 | 14.30 | 78.89 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:21:55 AM | 0.36528 | 14.30 | 78.89 |
| 8/13/2013 11:21:56 AM | 0.36556 | 14.30 | 78.89 |
| 8/13/2013 11:21:57 AM | 0.36583 | 14.30 | 78.89 |
| 8/13/2013 11:21:58 AM | 0.36611 | 14.30 | 78.89 |
| 8/13/2013 11:21:59 AM | 0.36639 | 14.30 | 78.89 |
| 8/13/2013 11:22:00 AM | 0.36667 | 14.30 | 78.89 |
| 8/13/2013 11:22:01 AM | 0.36694 | 14.30 | 78.89 |
| 8/13/2013 11:22:02 AM | 0.36722 | 14.30 | 78.89 |
| 8/13/2013 11:22:03 AM | 0.36750 | 14.30 | 78.89 |
| 8/13/2013 11:22:04 AM | 0.36778 | 14.30 | 78.89 |
| 8/13/2013 11:22:05 AM | 0.36806 | 14.30 | 78.89 |
| 8/13/2013 11:22:06 AM | 0.36833 | 14.30 | 78.89 |
| 8/13/2013 11:22:07 AM | 0.36861 | 14.30 | 78.89 |
| 8/13/2013 11:22:08 AM | 0.36889 | 14.30 | 78.89 |
| 8/13/2013 11:22:09 AM | 0.36917 | 14.30 | 78.89 |
| 8/13/2013 11:22:10 AM | 0.36944 | 14.30 | 78.89 |
| 8/13/2013 11:22:11 AM | 0.36972 | 14.30 | 78.89 |
| 8/13/2013 11:22:12 AM | 0.37000 | 14.30 | 78.89 |
| 8/13/2013 11:22:13 AM | 0.37028 | 14.30 | 78.89 |
| 8/13/2013 11:22:14 AM | 0.37056 | 14.30 | 78.89 |
| 8/13/2013 11:22:15 AM | 0.37083 | 14.30 | 78.89 |
| 8/13/2013 11:22:16 AM | 0.37111 | 14.30 | 78.89 |
| 8/13/2013 11:22:17 AM | 0.37139 | 14.30 | 78.89 |
| 8/13/2013 11:22:18 AM | 0.37167 | 14.30 | 78.89 |
| 8/13/2013 11:22:19 AM | 0.37194 | 14.30 | 78.89 |
| 8/13/2013 11:22:20 AM | 0.37222 | 14.30 | 78.89 |
| 8/13/2013 11:22:21 AM | 0.37250 | 14.30 | 78.89 |
| 8/13/2013 11:22:22 AM | 0.37278 | 14.30 | 78.89 |
| 8/13/2013 11:22:23 AM | 0.37306 | 14.30 | 78.89 |
| 8/13/2013 11:22:24 AM | 0.37333 | 14.30 | 78.89 |
| 8/13/2013 11:22:25 AM | 0.37361 | 14.30 | 78.89 |
| 8/13/2013 11:22:26 AM | 0.37389 | 14.30 | 78.89 |
| 8/13/2013 11:22:27 AM | 0.37417 | 14.30 | 78.89 |
| 8/13/2013 11:22:28 AM | 0.37444 | 14.30 | 78.89 |
| 8/13/2013 11:22:29 AM | 0.37472 | 14.30 | 78.89 |
| 8/13/2013 11:22:30 AM | 0.37500 | 14.30 | 78.89 |
| 8/13/2013 11:22:31 AM | 0.37528 | 14.30 | 78.89 |
| 8/13/2013 11:22:32 AM | 0.37556 | 14.30 | 78.89 |
| 8/13/2013 11:22:33 AM | 0.37583 | 14.30 | 78.89 |
| 8/13/2013 11:22:34 AM | 0.37611 | 14.30 | 78.89 |
| 8/13/2013 11:22:35 AM | 0.37639 | 14.30 | 78.89 |
| 8/13/2013 11:22:36 AM | 0.37667 | 14.30 | 78.89 |
| 8/13/2013 11:22:37 AM | 0.37694 | 14.30 | 78.89 |
| 8/13/2013 11:22:38 AM | 0.37722 | 14.30 | 78.89 |
| 8/13/2013 11:22:39 AM | 0.37750 | 14.30 | 78.89 |
| 8/13/2013 11:22:40 AM | 0.37778 | 14.30 | 78.89 |
| 8/13/2013 11:22:41 AM | 0.37806 | 14.30 | 78.89 |
| 8/13/2013 11:22:42 AM | 0.37833 | 14.30 | 78.89 |
| 8/13/2013 11:22:43 AM | 0.37861 | 14.30 | 78.89 |
| 8/13/2013 11:22:44 AM | 0.37889 | 14.30 | 78.89 |
| 8/13/2013 11:22:45 AM | 0.37917 | 14.30 | 78.89 |
| 8/13/2013 11:22:46 AM | 0.37944 | 14.30 | 78.89 |
| 8/13/2013 11:22:47 AM | 0.37972 | 14.30 | 78.89 |
| 8/13/2013 11:22:48 AM | 0.38000 | 14.30 | 78.89 |
| 8/13/2013 11:22:49 AM | 0.38028 | 14.30 | 78.89 |
| 8/13/2013 11:22:50 AM | 0.38056 | 14.30 | 78.89 |
| 8/13/2013 11:22:51 AM | 0.38083 | 14.30 | 78.89 |
| 8/13/2013 11:22:52 AM | 0.38111 | 14.30 | 78.89 |
| 8/13/2013 11:22:53 AM | 0.38139 | 14.30 | 78.89 |
| 8/13/2013 11:22:54 AM | 0.38167 | 14.30 | 78.89 |
| 8/13/2013 11:22:55 AM | 0.38194 | 14.30 | 78.89 |
| 8/13/2013 11:22:56 AM | 0.38222 | 14.30 | 78.89 |
| 8/13/2013 11:22:57 AM | 0.38250 | 14.30 | 78.89 |
| 8/13/2013 11:22:58 AM | 0.38278 | 14.30 | 78.89 |
| 8/13/2013 11:22:59 AM | 0.38306 | 14.30 | 78.89 |
| 8/13/2013 11:23:00 AM | 0.38333 | 14.30 | 78.89 |
| 8/13/2013 11:23:01 AM | 0.38361 | 14.30 | 78.89 |
| 8/13/2013 11:23:02 AM | 0.38389 | 14.30 | 78.89 |
| 8/13/2013 11:23:03 AM | 0.38417 | 14.30 | 78.89 |
| 8/13/2013 11:23:04 AM | 0.38444 | 14.30 | 78.89 |
| 8/13/2013 11:23:05 AM | 0.38472 | 14.30 | 78.89 |
| 8/13/2013 11:23:06 AM | 0.38500 | 14.30 | 78.89 |
| 8/13/2013 11:23:07 AM | 0.38528 | 14.30 | 78.89 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:23:08 AM | 0.38556 | 14.30 | 78.89 |
| 8/13/2013 11:23:09 AM | 0.38583 | 14.30 | 78.89 |
| 8/13/2013 11:23:10 AM | 0.38611 | 14.30 | 78.89 |
| 8/13/2013 11:23:11 AM | 0.38639 | 14.30 | 78.89 |
| 8/13/2013 11:23:12 AM | 0.38667 | 14.30 | 78.89 |
| 8/13/2013 11:23:13 AM | 0.38694 | 14.30 | 78.89 |
| 8/13/2013 11:23:14 AM | 0.38722 | 14.30 | 78.89 |
| 8/13/2013 11:23:15 AM | 0.38750 | 14.30 | 78.89 |
| 8/13/2013 11:23:16 AM | 0.38778 | 14.30 | 78.89 |
| 8/13/2013 11:23:17 AM | 0.38806 | 14.30 | 78.89 |
| 8/13/2013 11:23:18 AM | 0.38833 | 14.30 | 78.89 |
| 8/13/2013 11:23:19 AM | 0.38861 | 14.30 | 78.89 |
| 8/13/2013 11:23:20 AM | 0.38889 | 14.30 | 78.89 |
| 8/13/2013 11:23:21 AM | 0.38917 | 14.30 | 78.89 |
| 8/13/2013 11:23:22 AM | 0.38944 | 14.30 | 78.89 |
| 8/13/2013 11:23:23 AM | 0.38972 | 14.30 | 78.89 |
| 8/13/2013 11:23:24 AM | 0.39000 | 14.30 | 78.89 |
| 8/13/2013 11:23:25 AM | 0.39028 | 14.30 | 78.89 |
| 8/13/2013 11:23:26 AM | 0.39056 | 14.30 | 78.89 |
| 8/13/2013 11:23:27 AM | 0.39083 | 14.30 | 78.89 |
| 8/13/2013 11:23:28 AM | 0.39111 | 14.30 | 78.89 |
| 8/13/2013 11:23:29 AM | 0.39139 | 14.30 | 78.89 |
| 8/13/2013 11:23:30 AM | 0.39167 | 14.30 | 78.89 |
| 8/13/2013 11:23:31 AM | 0.39194 | 14.30 | 78.89 |
| 8/13/2013 11:23:32 AM | 0.39222 | 14.30 | 78.89 |
| 8/13/2013 11:23:33 AM | 0.39250 | 14.30 | 78.89 |
| 8/13/2013 11:23:34 AM | 0.39278 | 14.30 | 78.89 |
| 8/13/2013 11:23:35 AM | 0.39306 | 14.30 | 78.89 |
| 8/13/2013 11:23:36 AM | 0.39333 | 14.30 | 78.89 |
| 8/13/2013 11:23:37 AM | 0.39361 | 14.30 | 78.89 |
| 8/13/2013 11:23:38 AM | 0.39389 | 14.30 | 78.89 |
| 8/13/2013 11:23:39 AM | 0.39417 | 14.30 | 78.89 |
| 8/13/2013 11:23:40 AM | 0.39444 | 14.30 | 78.89 |
| 8/13/2013 11:23:41 AM | 0.39472 | 14.30 | 78.89 |
| 8/13/2013 11:23:42 AM | 0.39500 | 14.30 | 78.89 |
| 8/13/2013 11:23:43 AM | 0.39528 | 14.30 | 78.89 |
| 8/13/2013 11:23:44 AM | 0.39556 | 14.30 | 78.89 |
| 8/13/2013 11:23:45 AM | 0.39583 | 14.30 | 78.89 |
| 8/13/2013 11:23:46 AM | 0.39611 | 14.30 | 78.89 |
| 8/13/2013 11:23:47 AM | 0.39639 | 14.30 | 78.89 |
| 8/13/2013 11:23:48 AM | 0.39667 | 14.30 | 78.89 |
| 8/13/2013 11:23:49 AM | 0.39694 | 14.30 | 78.89 |
| 8/13/2013 11:23:50 AM | 0.39722 | 14.30 | 78.89 |
| 8/13/2013 11:23:51 AM | 0.39750 | 14.30 | 78.89 |
| 8/13/2013 11:23:52 AM | 0.39778 | 14.30 | 78.89 |
| 8/13/2013 11:23:53 AM | 0.39806 | 14.30 | 78.89 |
| 8/13/2013 11:23:54 AM | 0.39833 | 14.30 | 78.89 |
| 8/13/2013 11:23:55 AM | 0.39861 | 14.30 | 78.89 |
| 8/13/2013 11:23:56 AM | 0.39889 | 14.30 | 78.89 |
| 8/13/2013 11:23:57 AM | 0.39917 | 14.30 | 78.89 |
| 8/13/2013 11:23:58 AM | 0.39944 | 14.30 | 78.89 |
| 8/13/2013 11:23:59 AM | 0.39972 | 14.30 | 78.89 |
| 8/13/2013 11:24:00 AM | 0.40000 | 14.30 | 78.89 |
| 8/13/2013 11:24:01 AM | 0.40028 | 14.30 | 78.89 |
| 8/13/2013 11:24:02 AM | 0.40056 | 14.30 | 78.89 |
| 8/13/2013 11:24:03 AM | 0.40083 | 14.30 | 78.89 |
| 8/13/2013 11:24:04 AM | 0.40111 | 14.30 | 78.89 |
| 8/13/2013 11:24:05 AM | 0.40139 | 14.30 | 78.89 |
| 8/13/2013 11:24:06 AM | 0.40167 | 14.30 | 78.89 |
| 8/13/2013 11:24:07 AM | 0.40194 | 14.30 | 78.89 |
| 8/13/2013 11:24:08 AM | 0.40222 | 14.30 | 78.89 |
| 8/13/2013 11:24:09 AM | 0.40250 | 14.30 | 78.89 |
| 8/13/2013 11:24:10 AM | 0.40278 | 14.30 | 78.89 |
| 8/13/2013 11:24:11 AM | 0.40306 | 14.30 | 78.89 |
| 8/13/2013 11:24:12 AM | 0.40333 | 14.30 | 78.89 |
| 8/13/2013 11:24:13 AM | 0.40361 | 14.30 | 78.89 |
| 8/13/2013 11:24:14 AM | 0.40389 | 14.30 | 78.89 |
| 8/13/2013 11:24:15 AM | 0.40417 | 14.30 | 78.89 |
| 8/13/2013 11:24:16 AM | 0.40444 | 14.30 | 78.89 |
| 8/13/2013 11:24:17 AM | 0.40472 | 14.30 | 78.89 |
| 8/13/2013 11:24:18 AM | 0.40500 | 14.30 | 78.89 |
| 8/13/2013 11:24:19 AM | 0.40528 | 14.30 | 78.89 |
| 8/13/2013 11:24:20 AM | 0.40556 | 14.30 | 78.89 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:24:21 AM | 0.40583 | 14.30 | 78.89 |
| 8/13/2013 11:24:22 AM | 0.40611 | 14.30 | 78.89 |
| 8/13/2013 11:24:23 AM | 0.40639 | 14.30 | 78.89 |
| 8/13/2013 11:24:24 AM | 0.40667 | 14.30 | 78.89 |
| 8/13/2013 11:24:25 AM | 0.40694 | 14.30 | 78.89 |
| 8/13/2013 11:24:26 AM | 0.40722 | 14.30 | 78.89 |
| 8/13/2013 11:24:27 AM | 0.40750 | 14.30 | 78.89 |
| 8/13/2013 11:24:28 AM | 0.40778 | 14.30 | 78.89 |
| 8/13/2013 11:24:29 AM | 0.40806 | 14.30 | 78.89 |
| 8/13/2013 11:24:30 AM | 0.40833 | 14.30 | 78.89 |
| 8/13/2013 11:24:31 AM | 0.40861 | 14.30 | 78.89 |
| 8/13/2013 11:24:32 AM | 0.40889 | 14.30 | 78.89 |
| 8/13/2013 11:24:33 AM | 0.40917 | 14.30 | 78.89 |
| 8/13/2013 11:24:34 AM | 0.40944 | 14.30 | 78.89 |
| 8/13/2013 11:24:35 AM | 0.40972 | 14.30 | 78.89 |
| 8/13/2013 11:24:36 AM | 0.41000 | 14.30 | 78.89 |
| 8/13/2013 11:24:37 AM | 0.41028 | 14.30 | 78.89 |
| 8/13/2013 11:24:38 AM | 0.41056 | 14.30 | 78.89 |
| 8/13/2013 11:24:39 AM | 0.41083 | 14.30 | 78.89 |
| 8/13/2013 11:24:40 AM | 0.41111 | 14.30 | 78.89 |
| 8/13/2013 11:24:41 AM | 0.41139 | 14.30 | 78.89 |
| 8/13/2013 11:24:42 AM | 0.41167 | 14.30 | 78.89 |
| 8/13/2013 11:24:43 AM | 0.41194 | 14.30 | 78.89 |
| 8/13/2013 11:24:44 AM | 0.41222 | 14.30 | 78.89 |
| 8/13/2013 11:24:45 AM | 0.41250 | 14.30 | 78.89 |
| 8/13/2013 11:24:46 AM | 0.41278 | 14.30 | 78.89 |
| 8/13/2013 11:24:47 AM | 0.41306 | 14.30 | 78.89 |
| 8/13/2013 11:24:48 AM | 0.41333 | 14.30 | 78.89 |
| 8/13/2013 11:24:49 AM | 0.41361 | 14.30 | 78.89 |
| 8/13/2013 11:24:50 AM | 0.41389 | 14.30 | 78.89 |
| 8/13/2013 11:24:51 AM | 0.41417 | 14.30 | 78.89 |
| 8/13/2013 11:24:52 AM | 0.41444 | 14.30 | 78.89 |
| 8/13/2013 11:24:53 AM | 0.41472 | 14.30 | 78.89 |
| 8/13/2013 11:24:54 AM | 0.41500 | 14.30 | 78.89 |
| 8/13/2013 11:24:55 AM | 0.41528 | 14.30 | 78.89 |
| 8/13/2013 11:24:56 AM | 0.41556 | 14.30 | 78.89 |
| 8/13/2013 11:24:57 AM | 0.41583 | 14.30 | 78.89 |
| 8/13/2013 11:24:58 AM | 0.41611 | 14.30 | 78.89 |
| 8/13/2013 11:24:59 AM | 0.41639 | 14.30 | 78.89 |
| 8/13/2013 11:25:00 AM | 0.41667 | 14.30 | 78.89 |
| 8/13/2013 11:25:01 AM | 0.41694 | 14.30 | 78.89 |
| 8/13/2013 11:25:02 AM | 0.41722 | 14.30 | 78.89 |
| 8/13/2013 11:25:03 AM | 0.41750 | 14.30 | 78.89 |
| 8/13/2013 11:25:04 AM | 0.41778 | 14.30 | 78.89 |
| 8/13/2013 11:25:05 AM | 0.41806 | 14.30 | 78.89 |
| 8/13/2013 11:25:06 AM | 0.41833 | 14.30 | 78.89 |
| 8/13/2013 11:25:07 AM | 0.41861 | 14.30 | 78.89 |
| 8/13/2013 11:25:08 AM | 0.41889 | 14.30 | 78.89 |
| 8/13/2013 11:25:09 AM | 0.41917 | 14.30 | 78.89 |
| 8/13/2013 11:25:10 AM | 0.41944 | 14.30 | 78.89 |
| 8/13/2013 11:25:11 AM | 0.41972 | 14.30 | 78.89 |
| 8/13/2013 11:25:12 AM | 0.42000 | 14.30 | 78.89 |
| 8/13/2013 11:25:13 AM | 0.42028 | 14.30 | 78.89 |
| 8/13/2013 11:25:14 AM | 0.42056 | 14.30 | 78.89 |
| 8/13/2013 11:25:15 AM | 0.42083 | 14.30 | 78.89 |
| 8/13/2013 11:25:16 AM | 0.42111 | 14.30 | 78.89 |
| 8/13/2013 11:25:17 AM | 0.42139 | 14.30 | 78.89 |
| 8/13/2013 11:25:18 AM | 0.42167 | 14.30 | 78.89 |
| 8/13/2013 11:25:19 AM | 0.42194 | 14.30 | 78.89 |
| 8/13/2013 11:25:20 AM | 0.42222 | 14.30 | 78.89 |
| 8/13/2013 11:25:21 AM | 0.42250 | 14.30 | 78.89 |
| 8/13/2013 11:25:22 AM | 0.42278 | 14.30 | 78.89 |
| 8/13/2013 11:25:23 AM | 0.42306 | 14.30 | 78.89 |
| 8/13/2013 11:25:24 AM | 0.42333 | 14.30 | 78.89 |
| 8/13/2013 11:25:25 AM | 0.42361 | 14.30 | 78.89 |
| 8/13/2013 11:25:26 AM | 0.42389 | 14.30 | 78.89 |
| 8/13/2013 11:25:27 AM | 0.42417 | 14.30 | 78.89 |
| 8/13/2013 11:25:28 AM | 0.42444 | 14.30 | 78.89 |
| 8/13/2013 11:25:29 AM | 0.42472 | 14.30 | 78.89 |
| 8/13/2013 11:25:30 AM | 0.42500 | 14.30 | 78.89 |
| 8/13/2013 11:25:31 AM | 0.42528 | 14.30 | 78.89 |
| 8/13/2013 11:25:32 AM | 0.42556 | 14.30 | 78.89 |
| 8/13/2013 11:25:33 AM | 0.42583 | 14.30 | 78.89 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:25:34 AM | 0.42611 | 14.30 | 78.89 |
| 8/13/2013 11:25:35 AM | 0.42639 | 14.30 | 78.89 |
| 8/13/2013 11:25:36 AM | 0.42667 | 14.30 | 78.89 |
| 8/13/2013 11:25:37 AM | 0.42694 | 14.30 | 78.89 |
| 8/13/2013 11:25:38 AM | 0.42722 | 14.30 | 78.89 |
| 8/13/2013 11:25:39 AM | 0.42750 | 14.30 | 78.89 |
| 8/13/2013 11:25:40 AM | 0.42778 | 14.30 | 78.89 |
| 8/13/2013 11:25:41 AM | 0.42806 | 14.30 | 78.89 |
| 8/13/2013 11:25:42 AM | 0.42833 | 14.30 | 78.89 |
| 8/13/2013 11:25:43 AM | 0.42861 | 14.30 | 78.89 |
| 8/13/2013 11:25:44 AM | 0.42889 | 14.30 | 78.89 |
| 8/13/2013 11:25:45 AM | 0.42917 | 14.30 | 78.89 |
| 8/13/2013 11:25:46 AM | 0.42944 | 14.30 | 78.89 |
| 8/13/2013 11:25:47 AM | 0.42972 | 14.30 | 78.89 |
| 8/13/2013 11:25:48 AM | 0.43000 | 14.30 | 78.89 |
| 8/13/2013 11:25:49 AM | 0.43028 | 14.30 | 78.89 |
| 8/13/2013 11:25:50 AM | 0.43056 | 14.30 | 78.89 |
| 8/13/2013 11:25:51 AM | 0.43083 | 14.30 | 78.89 |
| 8/13/2013 11:25:52 AM | 0.43111 | 14.30 | 78.89 |
| 8/13/2013 11:25:53 AM | 0.43139 | 14.30 | 78.89 |
| 8/13/2013 11:25:54 AM | 0.43167 | 14.30 | 78.89 |
| 8/13/2013 11:25:55 AM | 0.43194 | 14.30 | 78.89 |
| 8/13/2013 11:25:56 AM | 0.43222 | 14.30 | 78.89 |
| 8/13/2013 11:25:57 AM | 0.43250 | 14.30 | 78.88 |
| 8/13/2013 11:25:58 AM | 0.43278 | 14.30 | 78.88 |
| 8/13/2013 11:25:59 AM | 0.43306 | 14.30 | 78.88 |
| 8/13/2013 11:26:00 AM | 0.43333 | 14.30 | 78.88 |
| 8/13/2013 11:26:01 AM | 0.43361 | 14.30 | 78.88 |
| 8/13/2013 11:26:02 AM | 0.43389 | 14.30 | 78.88 |
| 8/13/2013 11:26:03 AM | 0.43417 | 14.30 | 78.88 |
| 8/13/2013 11:26:04 AM | 0.43444 | 14.30 | 78.88 |
| 8/13/2013 11:26:05 AM | 0.43472 | 14.30 | 78.88 |
| 8/13/2013 11:26:06 AM | 0.43500 | 14.30 | 78.88 |
| 8/13/2013 11:26:07 AM | 0.43528 | 14.30 | 78.88 |
| 8/13/2013 11:26:08 AM | 0.43556 | 14.30 | 78.88 |
| 8/13/2013 11:26:09 AM | 0.43583 | 14.30 | 78.88 |
| 8/13/2013 11:26:10 AM | 0.43611 | 14.30 | 78.88 |
| 8/13/2013 11:26:11 AM | 0.43639 | 14.30 | 78.88 |
| 8/13/2013 11:26:12 AM | 0.43667 | 14.30 | 78.88 |
| 8/13/2013 11:26:13 AM | 0.43694 | 14.30 | 78.88 |
| 8/13/2013 11:26:14 AM | 0.43722 | 14.30 | 78.88 |
| 8/13/2013 11:26:15 AM | 0.43750 | 14.30 | 78.88 |
| 8/13/2013 11:26:16 AM | 0.43778 | 14.30 | 78.88 |
| 8/13/2013 11:26:17 AM | 0.43806 | 14.30 | 78.88 |
| 8/13/2013 11:26:18 AM | 0.43833 | 14.30 | 78.88 |
| 8/13/2013 11:26:19 AM | 0.43861 | 14.30 | 78.88 |
| 8/13/2013 11:26:20 AM | 0.43889 | 14.30 | 78.88 |
| 8/13/2013 11:26:21 AM | 0.43917 | 14.30 | 78.88 |
| 8/13/2013 11:26:22 AM | 0.43944 | 14.30 | 78.88 |
| 8/13/2013 11:26:23 AM | 0.43972 | 14.30 | 78.88 |
| 8/13/2013 11:26:24 AM | 0.44000 | 14.30 | 78.88 |
| 8/13/2013 11:26:25 AM | 0.44028 | 14.30 | 78.88 |
| 8/13/2013 11:26:26 AM | 0.44056 | 14.30 | 78.88 |
| 8/13/2013 11:26:27 AM | 0.44083 | 14.30 | 78.88 |
| 8/13/2013 11:26:28 AM | 0.44111 | 14.30 | 78.88 |
| 8/13/2013 11:26:29 AM | 0.44139 | 14.30 | 78.88 |
| 8/13/2013 11:26:30 AM | 0.44167 | 14.30 | 78.88 |
| 8/13/2013 11:26:31 AM | 0.44194 | 14.30 | 78.88 |
| 8/13/2013 11:26:32 AM | 0.44222 | 14.30 | 78.88 |
| 8/13/2013 11:26:33 AM | 0.44250 | 14.30 | 78.88 |
| 8/13/2013 11:26:34 AM | 0.44278 | 14.30 | 78.88 |
| 8/13/2013 11:26:35 AM | 0.44306 | 14.30 | 78.88 |
| 8/13/2013 11:26:36 AM | 0.44333 | 14.30 | 78.88 |
| 8/13/2013 11:26:37 AM | 0.44361 | 14.30 | 78.88 |
| 8/13/2013 11:26:38 AM | 0.44389 | 14.30 | 78.88 |
| 8/13/2013 11:26:39 AM | 0.44417 | 14.30 | 78.88 |
| 8/13/2013 11:26:40 AM | 0.44444 | 14.30 | 78.88 |
| 8/13/2013 11:26:41 AM | 0.44472 | 14.30 | 78.88 |
| 8/13/2013 11:26:42 AM | 0.44500 | 14.30 | 78.88 |
| 8/13/2013 11:26:43 AM | 0.44528 | 14.30 | 78.88 |
| 8/13/2013 11:26:44 AM | 0.44556 | 14.30 | 78.88 |
| 8/13/2013 11:26:45 AM | 0.44583 | 14.30 | 78.88 |
| 8/13/2013 11:26:46 AM | 0.44611 | 14.30 | 78.88 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:26:47 AM | 0.44639 | 14.30 | 78.88 |
| 8/13/2013 11:26:48 AM | 0.44667 | 14.30 | 78.88 |
| 8/13/2013 11:26:49 AM | 0.44694 | 14.30 | 78.88 |
| 8/13/2013 11:26:50 AM | 0.44722 | 14.30 | 78.88 |
| 8/13/2013 11:26:51 AM | 0.44750 | 14.30 | 78.88 |
| 8/13/2013 11:26:52 AM | 0.44778 | 14.30 | 78.88 |
| 8/13/2013 11:26:53 AM | 0.44806 | 14.30 | 78.88 |
| 8/13/2013 11:26:54 AM | 0.44833 | 14.30 | 78.88 |
| 8/13/2013 11:26:55 AM | 0.44861 | 14.30 | 78.88 |
| 8/13/2013 11:26:56 AM | 0.44889 | 14.30 | 78.88 |
| 8/13/2013 11:26:57 AM | 0.44917 | 14.30 | 78.88 |
| 8/13/2013 11:26:58 AM | 0.44944 | 14.30 | 78.88 |
| 8/13/2013 11:26:59 AM | 0.44972 | 14.30 | 78.88 |
| 8/13/2013 11:27:00 AM | 0.45000 | 14.30 | 78.88 |
| 8/13/2013 11:27:01 AM | 0.45028 | 14.30 | 78.88 |
| 8/13/2013 11:27:02 AM | 0.45056 | 14.30 | 78.88 |
| 8/13/2013 11:27:03 AM | 0.45083 | 14.30 | 78.88 |
| 8/13/2013 11:27:04 AM | 0.45111 | 14.30 | 78.88 |
| 8/13/2013 11:27:05 AM | 0.45139 | 14.30 | 78.88 |
| 8/13/2013 11:27:06 AM | 0.45167 | 14.30 | 78.88 |
| 8/13/2013 11:27:07 AM | 0.45194 | 14.30 | 78.88 |
| 8/13/2013 11:27:08 AM | 0.45222 | 14.30 | 78.88 |
| 8/13/2013 11:27:09 AM | 0.45250 | 14.30 | 78.88 |
| 8/13/2013 11:27:10 AM | 0.45278 | 14.30 | 78.88 |
| 8/13/2013 11:27:11 AM | 0.45306 | 14.30 | 78.88 |
| 8/13/2013 11:27:12 AM | 0.45333 | 14.30 | 78.88 |
| 8/13/2013 11:27:13 AM | 0.45361 | 14.30 | 78.88 |
| 8/13/2013 11:27:14 AM | 0.45389 | 14.30 | 78.88 |
| 8/13/2013 11:27:15 AM | 0.45417 | 14.30 | 78.88 |
| 8/13/2013 11:27:16 AM | 0.45444 | 14.30 | 78.88 |
| 8/13/2013 11:27:17 AM | 0.45472 | 14.30 | 78.87 |
| 8/13/2013 11:27:18 AM | 0.45500 | 14.30 | 78.87 |
| 8/13/2013 11:27:19 AM | 0.45528 | 14.30 | 78.87 |
| 8/13/2013 11:27:20 AM | 0.45556 | 14.30 | 78.87 |
| 8/13/2013 11:27:21 AM | 0.45583 | 14.30 | 78.87 |
| 8/13/2013 11:27:22 AM | 0.45611 | 14.30 | 78.87 |
| 8/13/2013 11:27:23 AM | 0.45639 | 14.30 | 78.87 |
| 8/13/2013 11:27:24 AM | 0.45667 | 14.30 | 78.87 |
| 8/13/2013 11:27:25 AM | 0.45694 | 14.30 | 78.87 |
| 8/13/2013 11:27:26 AM | 0.45722 | 14.30 | 78.87 |
| 8/13/2013 11:27:27 AM | 0.45750 | 14.30 | 78.87 |
| 8/13/2013 11:27:28 AM | 0.45778 | 14.30 | 78.87 |
| 8/13/2013 11:27:29 AM | 0.45806 | 14.30 | 78.87 |
| 8/13/2013 11:27:30 AM | 0.45833 | 14.30 | 78.87 |
| 8/13/2013 11:27:31 AM | 0.45861 | 14.30 | 78.87 |
| 8/13/2013 11:27:32 AM | 0.45889 | 14.30 | 78.87 |
| 8/13/2013 11:27:33 AM | 0.45917 | 14.30 | 78.87 |
| 8/13/2013 11:27:34 AM | 0.45944 | 14.30 | 78.87 |
| 8/13/2013 11:27:35 AM | 0.45972 | 14.30 | 78.87 |
| 8/13/2013 11:27:36 AM | 0.46000 | 14.30 | 78.87 |
| 8/13/2013 11:27:37 AM | 0.46028 | 14.30 | 78.87 |
| 8/13/2013 11:27:38 AM | 0.46056 | 14.30 | 78.87 |
| 8/13/2013 11:27:39 AM | 0.46083 | 14.30 | 78.87 |
| 8/13/2013 11:27:40 AM | 0.46111 | 14.30 | 78.87 |
| 8/13/2013 11:27:41 AM | 0.46139 | 14.30 | 78.87 |
| 8/13/2013 11:27:42 AM | 0.46167 | 14.30 | 78.87 |
| 8/13/2013 11:27:43 AM | 0.46194 | 14.30 | 78.87 |
| 8/13/2013 11:27:44 AM | 0.46222 | 14.30 | 78.87 |
| 8/13/2013 11:27:45 AM | 0.46250 | 14.30 | 78.87 |
| 8/13/2013 11:27:46 AM | 0.46278 | 14.30 | 78.87 |
| 8/13/2013 11:27:47 AM | 0.46306 | 14.30 | 78.87 |
| 8/13/2013 11:27:48 AM | 0.46333 | 14.30 | 78.87 |
| 8/13/2013 11:27:49 AM | 0.46361 | 14.30 | 78.87 |
| 8/13/2013 11:27:50 AM | 0.46389 | 14.30 | 78.87 |
| 8/13/2013 11:27:51 AM | 0.46417 | 14.30 | 78.87 |
| 8/13/2013 11:27:52 AM | 0.46444 | 14.30 | 78.87 |
| 8/13/2013 11:27:53 AM | 0.46472 | 14.30 | 78.87 |
| 8/13/2013 11:27:54 AM | 0.46500 | 14.30 | 78.87 |
| 8/13/2013 11:27:55 AM | 0.46528 | 14.30 | 78.87 |
| 8/13/2013 11:27:56 AM | 0.46556 | 14.30 | 78.87 |
| 8/13/2013 11:27:57 AM | 0.46583 | 14.30 | 78.87 |
| 8/13/2013 11:27:58 AM | 0.46611 | 14.30 | 78.87 |
| 8/13/2013 11:27:59 AM | 0.46639 | 14.30 | 78.87 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:28:00 AM | 0.46667 | 14.30 | 78.87 |
| 8/13/2013 11:28:01 AM | 0.46694 | 14.30 | 78.87 |
| 8/13/2013 11:28:02 AM | 0.46722 | 14.30 | 78.87 |
| 8/13/2013 11:28:03 AM | 0.46750 | 14.30 | 78.87 |
| 8/13/2013 11:28:04 AM | 0.46778 | 14.30 | 78.87 |
| 8/13/2013 11:28:05 AM | 0.46806 | 14.30 | 78.87 |
| 8/13/2013 11:28:06 AM | 0.46833 | 14.30 | 78.87 |
| 8/13/2013 11:28:07 AM | 0.46861 | 14.30 | 78.87 |
| 8/13/2013 11:28:08 AM | 0.46889 | 14.30 | 78.87 |
| 8/13/2013 11:28:09 AM | 0.46917 | 14.30 | 78.87 |
| 8/13/2013 11:28:10 AM | 0.46944 | 14.30 | 78.87 |
| 8/13/2013 11:28:11 AM | 0.46972 | 14.30 | 78.87 |
| 8/13/2013 11:28:12 AM | 0.47000 | 14.30 | 78.87 |
| 8/13/2013 11:28:13 AM | 0.47028 | 14.30 | 78.86 |
| 8/13/2013 11:28:14 AM | 0.47056 | 14.30 | 78.86 |
| 8/13/2013 11:28:15 AM | 0.47083 | 14.30 | 78.86 |
| 8/13/2013 11:28:16 AM | 0.47111 | 14.30 | 78.86 |
| 8/13/2013 11:28:17 AM | 0.47139 | 14.30 | 78.86 |
| 8/13/2013 11:28:18 AM | 0.47167 | 14.30 | 78.86 |
| 8/13/2013 11:28:19 AM | 0.47194 | 14.30 | 78.86 |
| 8/13/2013 11:28:20 AM | 0.47222 | 14.30 | 78.86 |
| 8/13/2013 11:28:21 AM | 0.47250 | 14.30 | 78.86 |
| 8/13/2013 11:28:22 AM | 0.47278 | 14.30 | 78.86 |
| 8/13/2013 11:28:23 AM | 0.47306 | 14.30 | 78.86 |
| 8/13/2013 11:28:24 AM | 0.47333 | 14.30 | 78.86 |
| 8/13/2013 11:28:25 AM | 0.47361 | 14.30 | 78.86 |
| 8/13/2013 11:28:26 AM | 0.47389 | 14.30 | 78.86 |
| 8/13/2013 11:28:27 AM | 0.47417 | 14.30 | 78.86 |
| 8/13/2013 11:28:28 AM | 0.47444 | 14.30 | 78.86 |
| 8/13/2013 11:28:29 AM | 0.47472 | 14.30 | 78.86 |
| 8/13/2013 11:28:30 AM | 0.47500 | 14.30 | 78.86 |
| 8/13/2013 11:28:31 AM | 0.47528 | 14.30 | 78.86 |
| 8/13/2013 11:28:32 AM | 0.47556 | 14.30 | 78.86 |
| 8/13/2013 11:28:33 AM | 0.47583 | 14.30 | 78.86 |
| 8/13/2013 11:28:34 AM | 0.47611 | 14.30 | 78.86 |
| 8/13/2013 11:28:35 AM | 0.47639 | 14.30 | 78.86 |
| 8/13/2013 11:28:36 AM | 0.47667 | 14.30 | 78.86 |
| 8/13/2013 11:28:37 AM | 0.47694 | 14.30 | 78.86 |
| 8/13/2013 11:28:38 AM | 0.47722 | 14.30 | 78.86 |
| 8/13/2013 11:28:39 AM | 0.47750 | 14.30 | 78.86 |
| 8/13/2013 11:28:40 AM | 0.47778 | 14.30 | 78.86 |
| 8/13/2013 11:28:41 AM | 0.47806 | 14.30 | 78.86 |
| 8/13/2013 11:28:42 AM | 0.47833 | 14.30 | 78.86 |
| 8/13/2013 11:28:43 AM | 0.47861 | 14.30 | 78.86 |
| 8/13/2013 11:28:44 AM | 0.47889 | 14.30 | 78.86 |
| 8/13/2013 11:28:45 AM | 0.47917 | 14.30 | 78.86 |
| 8/13/2013 11:28:46 AM | 0.47944 | 14.30 | 78.86 |
| 8/13/2013 11:28:47 AM | 0.47972 | 14.30 | 78.86 |
| 8/13/2013 11:28:48 AM | 0.48000 | 14.30 | 78.86 |
| 8/13/2013 11:28:49 AM | 0.48028 | 14.30 | 78.86 |
| 8/13/2013 11:28:50 AM | 0.48056 | 14.30 | 78.86 |
| 8/13/2013 11:28:51 AM | 0.48083 | 14.30 | 78.86 |
| 8/13/2013 11:28:52 AM | 0.48111 | 14.30 | 78.86 |
| 8/13/2013 11:28:53 AM | 0.48139 | 14.30 | 78.86 |
| 8/13/2013 11:28:54 AM | 0.48167 | 14.30 | 78.86 |
| 8/13/2013 11:28:55 AM | 0.48194 | 14.30 | 78.86 |
| 8/13/2013 11:28:56 AM | 0.48222 | 14.30 | 78.86 |
| 8/13/2013 11:28:57 AM | 0.48250 | 14.30 | 78.86 |
| 8/13/2013 11:28:58 AM | 0.48278 | 14.30 | 78.86 |
| 8/13/2013 11:28:59 AM | 0.48306 | 14.30 | 78.86 |
| 8/13/2013 11:29:00 AM | 0.48333 | 14.30 | 78.86 |
| 8/13/2013 11:29:01 AM | 0.48361 | 14.30 | 78.86 |
| 8/13/2013 11:29:02 AM | 0.48389 | 14.30 | 78.86 |
| 8/13/2013 11:29:03 AM | 0.48417 | 14.30 | 78.86 |
| 8/13/2013 11:29:04 AM | 0.48444 | 14.30 | 78.86 |
| 8/13/2013 11:29:05 AM | 0.48472 | 14.30 | 78.86 |
| 8/13/2013 11:29:06 AM | 0.48500 | 14.30 | 78.86 |
| 8/13/2013 11:29:07 AM | 0.48528 | 14.30 | 78.86 |
| 8/13/2013 11:29:08 AM | 0.48556 | 14.30 | 78.86 |
| 8/13/2013 11:29:09 AM | 0.48583 | 14.30 | 78.85 |
| 8/13/2013 11:29:10 AM | 0.48611 | 14.30 | 78.85 |
| 8/13/2013 11:29:11 AM | 0.48639 | 14.30 | 78.85 |
| 8/13/2013 11:29:12 AM | 0.48667 | 14.30 | 78.85 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:29:13 AM | 0.48694 | 14.30 | 78.85 |
| 8/13/2013 11:29:14 AM | 0.48722 | 14.30 | 78.85 |
| 8/13/2013 11:29:15 AM | 0.48750 | 14.30 | 78.85 |
| 8/13/2013 11:29:16 AM | 0.48778 | 14.30 | 78.85 |
| 8/13/2013 11:29:17 AM | 0.48806 | 14.30 | 78.85 |
| 8/13/2013 11:29:18 AM | 0.48833 | 14.30 | 78.85 |
| 8/13/2013 11:29:19 AM | 0.48861 | 14.30 | 78.85 |
| 8/13/2013 11:29:20 AM | 0.48889 | 14.30 | 78.85 |
| 8/13/2013 11:29:21 AM | 0.48917 | 14.30 | 78.85 |
| 8/13/2013 11:29:22 AM | 0.48944 | 14.30 | 78.85 |
| 8/13/2013 11:29:23 AM | 0.48972 | 14.30 | 78.85 |
| 8/13/2013 11:29:24 AM | 0.49000 | 14.30 | 78.85 |
| 8/13/2013 11:29:25 AM | 0.49028 | 14.30 | 78.85 |
| 8/13/2013 11:29:26 AM | 0.49056 | 14.30 | 78.85 |
| 8/13/2013 11:29:27 AM | 0.49083 | 14.30 | 78.85 |
| 8/13/2013 11:29:28 AM | 0.49111 | 14.30 | 78.85 |
| 8/13/2013 11:29:29 AM | 0.49139 | 14.30 | 78.85 |
| 8/13/2013 11:29:30 AM | 0.49167 | 14.30 | 78.85 |
| 8/13/2013 11:29:31 AM | 0.49194 | 14.30 | 78.85 |
| 8/13/2013 11:29:32 AM | 0.49222 | 14.30 | 78.85 |
| 8/13/2013 11:29:33 AM | 0.49250 | 14.30 | 78.85 |
| 8/13/2013 11:29:34 AM | 0.49278 | 14.30 | 78.85 |
| 8/13/2013 11:29:35 AM | 0.49306 | 14.30 | 78.85 |
| 8/13/2013 11:29:36 AM | 0.49333 | 14.30 | 78.85 |
| 8/13/2013 11:29:37 AM | 0.49361 | 14.30 | 78.85 |
| 8/13/2013 11:29:38 AM | 0.49389 | 14.30 | 78.85 |
| 8/13/2013 11:29:39 AM | 0.49417 | 14.30 | 78.85 |
| 8/13/2013 11:29:40 AM | 0.49444 | 14.30 | 78.85 |
| 8/13/2013 11:29:41 AM | 0.49472 | 14.30 | 78.85 |
| 8/13/2013 11:29:42 AM | 0.49500 | 14.30 | 78.85 |
| 8/13/2013 11:29:43 AM | 0.49528 | 14.30 | 78.85 |
| 8/13/2013 11:29:44 AM | 0.49556 | 14.30 | 78.85 |
| 8/13/2013 11:29:45 AM | 0.49583 | 14.30 | 78.85 |
| 8/13/2013 11:29:46 AM | 0.49611 | 14.30 | 78.85 |
| 8/13/2013 11:29:47 AM | 0.49639 | 14.30 | 78.85 |
| 8/13/2013 11:29:48 AM | 0.49667 | 14.30 | 78.85 |
| 8/13/2013 11:29:49 AM | 0.49694 | 14.30 | 78.85 |
| 8/13/2013 11:29:50 AM | 0.49722 | 14.30 | 78.85 |
| 8/13/2013 11:29:51 AM | 0.49750 | 14.30 | 78.85 |
| 8/13/2013 11:29:52 AM | 0.49778 | 14.30 | 78.85 |
| 8/13/2013 11:29:53 AM | 0.49806 | 14.30 | 78.85 |
| 8/13/2013 11:29:54 AM | 0.49833 | 14.30 | 78.85 |
| 8/13/2013 11:29:55 AM | 0.49861 | 14.30 | 78.84 |
| 8/13/2013 11:29:56 AM | 0.49889 | 14.30 | 78.84 |
| 8/13/2013 11:29:57 AM | 0.49917 | 14.30 | 78.84 |
| 8/13/2013 11:29:58 AM | 0.49944 | 14.30 | 78.84 |
| 8/13/2013 11:29:59 AM | 0.49972 | 14.30 | 78.84 |
| 8/13/2013 11:30:00 AM | 0.50000 | 14.30 | 78.84 |
| 8/13/2013 11:30:01 AM | 0.50028 | 14.30 | 78.84 |
| 8/13/2013 11:30:02 AM | 0.50056 | 14.30 | 78.84 |
| 8/13/2013 11:30:03 AM | 0.50083 | 14.30 | 78.84 |
| 8/13/2013 11:30:04 AM | 0.50111 | 14.30 | 78.84 |
| 8/13/2013 11:30:05 AM | 0.50139 | 14.30 | 78.84 |
| 8/13/2013 11:30:06 AM | 0.50167 | 14.30 | 78.84 |
| 8/13/2013 11:30:07 AM | 0.50194 | 14.30 | 78.84 |
| 8/13/2013 11:30:08 AM | 0.50222 | 14.30 | 78.84 |
| 8/13/2013 11:30:09 AM | 0.50250 | 14.30 | 78.84 |
| 8/13/2013 11:30:10 AM | 0.50278 | 14.30 | 78.84 |
| 8/13/2013 11:30:11 AM | 0.50306 | 14.30 | 78.84 |
| 8/13/2013 11:30:12 AM | 0.50333 | 14.30 | 78.84 |
| 8/13/2013 11:30:13 AM | 0.50361 | 14.30 | 78.84 |
| 8/13/2013 11:30:14 AM | 0.50389 | 14.30 | 78.84 |
| 8/13/2013 11:30:15 AM | 0.50417 | 14.30 | 78.84 |
| 8/13/2013 11:30:16 AM | 0.50444 | 14.30 | 78.84 |
| 8/13/2013 11:30:17 AM | 0.50472 | 14.30 | 78.84 |
| 8/13/2013 11:30:18 AM | 0.50500 | 14.30 | 78.84 |
| 8/13/2013 11:30:19 AM | 0.50528 | 14.30 | 78.84 |
| 8/13/2013 11:30:20 AM | 0.50556 | 14.30 | 78.84 |
| 8/13/2013 11:30:21 AM | 0.50583 | 14.30 | 78.84 |
| 8/13/2013 11:30:22 AM | 0.50611 | 14.30 | 78.84 |
| 8/13/2013 11:30:23 AM | 0.50639 | 14.30 | 78.84 |
| 8/13/2013 11:30:24 AM | 0.50667 | 14.30 | 78.84 |
| 8/13/2013 11:30:25 AM | 0.50694 | 14.30 | 78.84 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:30:26 AM | 0.50722 | 14.30 | 78.84 |
| 8/13/2013 11:30:27 AM | 0.50750 | 14.30 | 78.84 |
| 8/13/2013 11:30:28 AM | 0.50778 | 14.30 | 78.84 |
| 8/13/2013 11:30:29 AM | 0.50806 | 14.30 | 78.84 |
| 8/13/2013 11:30:30 AM | 0.50833 | 14.30 | 78.84 |
| 8/13/2013 11:30:31 AM | 0.50861 | 14.30 | 78.84 |
| 8/13/2013 11:30:32 AM | 0.50889 | 14.30 | 78.84 |
| 8/13/2013 11:30:33 AM | 0.50917 | 14.30 | 78.84 |
| 8/13/2013 11:30:34 AM | 0.50944 | 14.30 | 78.84 |
| 8/13/2013 11:30:35 AM | 0.50972 | 14.30 | 78.84 |
| 8/13/2013 11:30:36 AM | 0.51000 | 14.30 | 78.84 |
| 8/13/2013 11:30:37 AM | 0.51028 | 14.30 | 78.84 |
| 8/13/2013 11:30:38 AM | 0.51056 | 14.30 | 78.84 |
| 8/13/2013 11:30:39 AM | 0.51083 | 14.30 | 78.84 |
| 8/13/2013 11:30:40 AM | 0.51111 | 14.30 | 78.84 |
| 8/13/2013 11:30:41 AM | 0.51139 | 14.30 | 78.84 |
| 8/13/2013 11:30:42 AM | 0.51167 | 14.30 | 78.84 |
| 8/13/2013 11:30:43 AM | 0.51194 | 14.30 | 78.84 |
| 8/13/2013 11:30:44 AM | 0.51222 | 14.30 | 78.84 |
| 8/13/2013 11:30:45 AM | 0.51250 | 14.30 | 78.84 |
| 8/13/2013 11:30:46 AM | 0.51278 | 14.30 | 78.84 |
| 8/13/2013 11:30:47 AM | 0.51306 | 14.30 | 78.84 |
| 8/13/2013 11:30:48 AM | 0.51333 | 14.30 | 78.84 |
| 8/13/2013 11:30:49 AM | 0.51361 | 14.30 | 78.83 |
| 8/13/2013 11:30:50 AM | 0.51389 | 14.30 | 78.83 |
| 8/13/2013 11:30:51 AM | 0.51417 | 14.30 | 78.83 |
| 8/13/2013 11:30:52 AM | 0.51444 | 14.30 | 78.83 |
| 8/13/2013 11:30:53 AM | 0.51472 | 14.30 | 78.83 |
| 8/13/2013 11:30:54 AM | 0.51500 | 14.30 | 78.83 |
| 8/13/2013 11:30:55 AM | 0.51528 | 14.30 | 78.83 |
| 8/13/2013 11:30:56 AM | 0.51556 | 14.30 | 78.83 |
| 8/13/2013 11:30:57 AM | 0.51583 | 14.30 | 78.83 |
| 8/13/2013 11:30:58 AM | 0.51611 | 14.30 | 78.83 |
| 8/13/2013 11:30:59 AM | 0.51639 | 14.30 | 78.83 |
| 8/13/2013 11:31:00 AM | 0.51667 | 14.30 | 78.83 |
| 8/13/2013 11:31:01 AM | 0.51694 | 14.30 | 78.83 |
| 8/13/2013 11:31:02 AM | 0.51722 | 14.30 | 78.83 |
| 8/13/2013 11:31:03 AM | 0.51750 | 14.30 | 78.83 |
| 8/13/2013 11:31:04 AM | 0.51778 | 14.30 | 78.83 |
| 8/13/2013 11:31:05 AM | 0.51806 | 14.30 | 78.83 |
| 8/13/2013 11:31:06 AM | 0.51833 | 14.30 | 78.83 |
| 8/13/2013 11:31:07 AM | 0.51861 | 14.30 | 78.83 |
| 8/13/2013 11:31:08 AM | 0.51889 | 14.30 | 78.83 |
| 8/13/2013 11:31:09 AM | 0.51917 | 14.30 | 78.83 |
| 8/13/2013 11:31:10 AM | 0.51944 | 14.30 | 78.83 |
| 8/13/2013 11:31:11 AM | 0.51972 | 14.30 | 78.83 |
| 8/13/2013 11:31:12 AM | 0.52000 | 14.30 | 78.83 |
| 8/13/2013 11:31:13 AM | 0.52028 | 14.30 | 78.83 |
| 8/13/2013 11:31:14 AM | 0.52056 | 14.30 | 78.83 |
| 8/13/2013 11:31:15 AM | 0.52083 | 14.30 | 78.83 |
| 8/13/2013 11:31:16 AM | 0.52111 | 14.30 | 78.83 |
| 8/13/2013 11:31:17 AM | 0.52139 | 14.30 | 78.83 |
| 8/13/2013 11:31:18 AM | 0.52167 | 14.30 | 78.83 |
| 8/13/2013 11:31:19 AM | 0.52194 | 14.30 | 78.83 |
| 8/13/2013 11:31:20 AM | 0.52222 | 14.30 | 78.83 |
| 8/13/2013 11:31:21 AM | 0.52250 | 14.30 | 78.83 |
| 8/13/2013 11:31:22 AM | 0.52278 | 14.30 | 78.83 |
| 8/13/2013 11:31:23 AM | 0.52306 | 14.30 | 78.83 |
| 8/13/2013 11:31:24 AM | 0.52333 | 14.30 | 78.83 |
| 8/13/2013 11:31:25 AM | 0.52361 | 14.30 | 78.83 |
| 8/13/2013 11:31:26 AM | 0.52389 | 14.30 | 78.83 |
| 8/13/2013 11:31:27 AM | 0.52417 | 14.30 | 78.83 |
| 8/13/2013 11:31:28 AM | 0.52444 | 14.30 | 78.83 |
| 8/13/2013 11:31:29 AM | 0.52472 | 14.30 | 78.83 |
| 8/13/2013 11:31:30 AM | 0.52500 | 14.30 | 78.83 |
| 8/13/2013 11:31:31 AM | 0.52528 | 14.30 | 78.83 |
| 8/13/2013 11:31:32 AM | 0.52556 | 14.30 | 78.83 |
| 8/13/2013 11:31:33 AM | 0.52583 | 14.30 | 78.83 |
| 8/13/2013 11:31:34 AM | 0.52611 | 14.30 | 78.82 |
| 8/13/2013 11:31:35 AM | 0.52639 | 14.30 | 78.82 |
| 8/13/2013 11:31:36 AM | 0.52667 | 14.30 | 78.82 |
| 8/13/2013 11:31:37 AM | 0.52694 | 14.30 | 78.82 |
| 8/13/2013 11:31:38 AM | 0.52722 | 14.30 | 78.82 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:31:39 AM | 0.52750 | 14.30 | 78.82 |
| 8/13/2013 11:31:40 AM | 0.52778 | 14.30 | 78.82 |
| 8/13/2013 11:31:41 AM | 0.52806 | 14.30 | 78.82 |
| 8/13/2013 11:31:42 AM | 0.52833 | 14.30 | 78.82 |
| 8/13/2013 11:31:43 AM | 0.52861 | 14.30 | 78.82 |
| 8/13/2013 11:31:44 AM | 0.52889 | 14.30 | 78.82 |
| 8/13/2013 11:31:45 AM | 0.52917 | 14.30 | 78.82 |
| 8/13/2013 11:31:46 AM | 0.52944 | 14.30 | 78.82 |
| 8/13/2013 11:31:47 AM | 0.52972 | 14.30 | 78.82 |
| 8/13/2013 11:31:48 AM | 0.53000 | 14.30 | 78.82 |
| 8/13/2013 11:31:49 AM | 0.53028 | 14.30 | 78.82 |
| 8/13/2013 11:31:50 AM | 0.53056 | 14.30 | 78.82 |
| 8/13/2013 11:31:51 AM | 0.53083 | 14.30 | 78.82 |
| 8/13/2013 11:31:52 AM | 0.53111 | 14.30 | 78.82 |
| 8/13/2013 11:31:53 AM | 0.53139 | 14.30 | 78.82 |
| 8/13/2013 11:31:54 AM | 0.53167 | 14.30 | 78.82 |
| 8/13/2013 11:31:55 AM | 0.53194 | 14.30 | 78.82 |
| 8/13/2013 11:31:56 AM | 0.53222 | 14.30 | 78.82 |
| 8/13/2013 11:31:57 AM | 0.53250 | 14.30 | 78.82 |
| 8/13/2013 11:31:58 AM | 0.53278 | 14.30 | 78.82 |
| 8/13/2013 11:31:59 AM | 0.53306 | 14.30 | 78.82 |
| 8/13/2013 11:32:00 AM | 0.53333 | 14.30 | 78.82 |
| 8/13/2013 11:32:01 AM | 0.53361 | 14.30 | 78.82 |
| 8/13/2013 11:32:02 AM | 0.53389 | 14.30 | 78.82 |
| 8/13/2013 11:32:03 AM | 0.53417 | 14.30 | 78.82 |
| 8/13/2013 11:32:04 AM | 0.53444 | 14.30 | 78.82 |
| 8/13/2013 11:32:05 AM | 0.53472 | 14.30 | 78.82 |
| 8/13/2013 11:32:06 AM | 0.53500 | 14.30 | 78.82 |
| 8/13/2013 11:32:07 AM | 0.53528 | 14.30 | 78.82 |
| 8/13/2013 11:32:08 AM | 0.53556 | 14.30 | 78.82 |
| 8/13/2013 11:32:09 AM | 0.53583 | 14.30 | 78.82 |
| 8/13/2013 11:32:10 AM | 0.53611 | 14.30 | 78.81 |
| 8/13/2013 11:32:11 AM | 0.53639 | 14.30 | 78.81 |
| 8/13/2013 11:32:12 AM | 0.53667 | 14.32 | 78.82 |
| 8/13/2013 11:32:13 AM | 0.53694 | 14.33 | 78.81 |
| 8/13/2013 11:32:14 AM | 0.53722 | 14.38 | 78.81 |
| 8/13/2013 11:32:15 AM | 0.53750 | 14.45 | 78.81 |
| 8/13/2013 11:32:16 AM | 0.53778 | 14.55 | 78.81 |
| 8/13/2013 11:32:17 AM | 0.53806 | 14.65 | 78.81 |
| 8/13/2013 11:32:18 AM | 0.53833 | 14.78 | 78.81 |
| 8/13/2013 11:32:19 AM | 0.53861 | 14.88 | 78.82 |
| 8/13/2013 11:32:20 AM | 0.53889 | 33.11 | 78.83 |
| 8/13/2013 11:32:21 AM | 0.53917 | 155.65 | 78.91 |
| 8/13/2013 11:32:22 AM | 0.53944 | 161.85 | 78.91 |
| 8/13/2013 11:32:23 AM | 0.53972 | 164.47 | 78.90 |
| 8/13/2013 11:32:24 AM | 0.54000 | 169.71 | 78.91 |
| 8/13/2013 11:32:25 AM | 0.54028 | 176.88 | 78.91 |
| 8/13/2013 11:32:26 AM | 0.54056 | 185.43 | 78.92 |
| 8/13/2013 11:32:27 AM | 0.54083 | 200.72 | 78.93 |
| 8/13/2013 11:32:28 AM | 0.54111 | 213.56 | 78.94 |
| 8/13/2013 11:32:29 AM | 0.54139 | 212.73 | 78.96 |
| 8/13/2013 11:32:30 AM | 0.54167 | 213.76 | 78.97 |
| 8/13/2013 11:32:31 AM | 0.54194 | 214.72 | 79.00 |
| 8/13/2013 11:32:32 AM | 0.54222 | 216.69 | 79.03 |
| 8/13/2013 11:32:33 AM | 0.54250 | 218.66 | 79.06 |
| 8/13/2013 11:32:34 AM | 0.54278 | 220.44 | 79.10 |
| 8/13/2013 11:32:35 AM | 0.54306 | 220.85 | 79.14 |
| 8/13/2013 11:32:36 AM | 0.54333 | 221.70 | 79.18 |
| 8/13/2013 11:32:37 AM | 0.54361 | 222.75 | 79.22 |
| 8/13/2013 11:32:38 AM | 0.54389 | 223.08 | 79.26 |
| 8/13/2013 11:32:39 AM | 0.54417 | 223.23 | 79.31 |
| 8/13/2013 11:32:40 AM | 0.54444 | 223.44 | 79.35 |
| 8/13/2013 11:32:41 AM | 0.54472 | 223.65 | 79.39 |
| 8/13/2013 11:32:42 AM | 0.54500 | 224.17 | 79.44 |
| 8/13/2013 11:32:43 AM | 0.54528 | 224.42 | 79.48 |
| 8/13/2013 11:32:44 AM | 0.54556 | 224.55 | 79.52 |
| 8/13/2013 11:32:45 AM | 0.54583 | 224.81 | 79.57 |
| 8/13/2013 11:32:46 AM | 0.54611 | 225.04 | 79.61 |
| 8/13/2013 11:32:47 AM | 0.54639 | 225.26 | 79.65 |
| 8/13/2013 11:32:48 AM | 0.54667 | 225.49 | 79.69 |
| 8/13/2013 11:32:49 AM | 0.54694 | 225.70 | 79.73 |
| 8/13/2013 11:32:50 AM | 0.54722 | 225.91 | 79.77 |
| 8/13/2013 11:32:51 AM | 0.54750 | 226.10 | 79.81 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:32:52 AM | 0.54778 | 226.32 | 79.84 |
| 8/13/2013 11:32:53 AM | 0.54806 | 226.44 | 79.88 |
| 8/13/2013 11:32:54 AM | 0.54833 | 226.58 | 79.92 |
| 8/13/2013 11:32:55 AM | 0.54861 | 226.70 | 79.95 |
| 8/13/2013 11:32:56 AM | 0.54889 | 226.81 | 79.98 |
| 8/13/2013 11:32:57 AM | 0.54917 | 226.88 | 80.02 |
| 8/13/2013 11:32:58 AM | 0.54944 | 226.93 | 80.05 |
| 8/13/2013 11:32:59 AM | 0.54972 | 226.99 | 80.08 |
| 8/13/2013 11:33:00 AM | 0.55000 | 227.13 | 80.11 |
| 8/13/2013 11:33:01 AM | 0.55028 | 227.19 | 80.14 |
| 8/13/2013 11:33:02 AM | 0.55056 | 227.17 | 80.17 |
| 8/13/2013 11:33:03 AM | 0.55083 | 227.12 | 80.20 |
| 8/13/2013 11:33:04 AM | 0.55111 | 227.24 | 80.23 |
| 8/13/2013 11:33:05 AM | 0.55139 | 227.23 | 80.26 |
| 8/13/2013 11:33:06 AM | 0.55167 | 227.31 | 80.28 |
| 8/13/2013 11:33:07 AM | 0.55194 | 229.27 | 80.31 |
| 8/13/2013 11:33:08 AM | 0.55222 | 230.52 | 80.33 |
| 8/13/2013 11:33:09 AM | 0.55250 | 231.56 | 80.36 |
| 8/13/2013 11:33:10 AM | 0.55278 | 232.19 | 80.38 |
| 8/13/2013 11:33:11 AM | 0.55306 | 232.32 | 80.40 |
| 8/13/2013 11:33:12 AM | 0.55333 | 232.63 | 80.43 |
| 8/13/2013 11:33:13 AM | 0.55361 | 232.80 | 80.45 |
| 8/13/2013 11:33:14 AM | 0.55389 | 233.04 | 80.47 |
| 8/13/2013 11:33:15 AM | 0.55417 | 233.35 | 80.49 |
| 8/13/2013 11:33:16 AM | 0.55444 | 233.53 | 80.50 |
| 8/13/2013 11:33:17 AM | 0.55472 | 233.76 | 80.52 |
| 8/13/2013 11:33:18 AM | 0.55500 | 233.97 | 80.54 |
| 8/13/2013 11:33:19 AM | 0.55528 | 234.18 | 80.56 |
| 8/13/2013 11:33:20 AM | 0.55556 | 234.38 | 80.57 |
| 8/13/2013 11:33:21 AM | 0.55583 | 234.63 | 80.59 |
| 8/13/2013 11:33:22 AM | 0.55611 | 234.86 | 80.61 |
| 8/13/2013 11:33:23 AM | 0.55639 | 235.09 | 80.62 |
| 8/13/2013 11:33:24 AM | 0.55667 | 235.33 | 80.64 |
| 8/13/2013 11:33:25 AM | 0.55694 | 235.57 | 80.65 |
| 8/13/2013 11:33:26 AM | 0.55722 | 235.80 | 80.67 |
| 8/13/2013 11:33:27 AM | 0.55750 | 236.02 | 80.68 |
| 8/13/2013 11:33:28 AM | 0.55778 | 236.24 | 80.69 |
| 8/13/2013 11:33:29 AM | 0.55806 | 236.45 | 80.71 |
| 8/13/2013 11:33:30 AM | 0.55833 | 236.61 | 80.72 |
| 8/13/2013 11:33:31 AM | 0.55861 | 236.77 | 80.73 |
| 8/13/2013 11:33:32 AM | 0.55889 | 236.93 | 80.75 |
| 8/13/2013 11:33:33 AM | 0.55917 | 237.06 | 80.76 |
| 8/13/2013 11:33:34 AM | 0.55944 | 237.19 | 80.77 |
| 8/13/2013 11:33:35 AM | 0.55972 | 237.31 | 80.78 |
| 8/13/2013 11:33:36 AM | 0.56000 | 237.41 | 80.79 |
| 8/13/2013 11:33:37 AM | 0.56028 | 237.51 | 80.80 |
| 8/13/2013 11:33:38 AM | 0.56056 | 237.59 | 80.81 |
| 8/13/2013 11:33:39 AM | 0.56083 | 237.66 | 80.82 |
| 8/13/2013 11:33:40 AM | 0.56111 | 237.73 | 80.83 |
| 8/13/2013 11:33:41 AM | 0.56139 | 237.79 | 80.84 |
| 8/13/2013 11:33:42 AM | 0.56167 | 237.85 | 80.85 |
| 8/13/2013 11:33:43 AM | 0.56194 | 237.89 | 80.86 |
| 8/13/2013 11:33:44 AM | 0.56222 | 237.93 | 80.86 |
| 8/13/2013 11:33:45 AM | 0.56250 | 237.97 | 80.87 |
| 8/13/2013 11:33:46 AM | 0.56278 | 238.01 | 80.88 |
| 8/13/2013 11:33:47 AM | 0.56306 | 238.05 | 80.89 |
| 8/13/2013 11:33:48 AM | 0.56333 | 238.09 | 80.90 |
| 8/13/2013 11:33:49 AM | 0.56361 | 238.13 | 80.90 |
| 8/13/2013 11:33:50 AM | 0.56389 | 238.30 | 80.91 |
| 8/13/2013 11:33:51 AM | 0.56417 | 238.26 | 80.92 |
| 8/13/2013 11:33:52 AM | 0.56444 | 238.26 | 80.93 |
| 8/13/2013 11:33:53 AM | 0.56472 | 238.63 | 80.94 |
| 8/13/2013 11:33:54 AM | 0.56500 | 238.60 | 80.94 |
| 8/13/2013 11:33:55 AM | 0.56528 | 238.59 | 80.95 |
| 8/13/2013 11:33:56 AM | 0.56556 | 238.78 | 80.95 |
| 8/13/2013 11:33:57 AM | 0.56583 | 239.05 | 80.96 |
| 8/13/2013 11:33:58 AM | 0.56611 | 377.37 | 81.05 |
| 8/13/2013 11:33:59 AM | 0.56639 | 646.62 | 81.28 |
| 8/13/2013 11:34:00 AM | 0.56667 | 889.10 | 81.38 |
| 8/13/2013 11:34:01 AM | 0.56694 | 857.52 | 81.34 |
| 8/13/2013 11:34:02 AM | 0.56722 | 840.37 | 81.32 |
| 8/13/2013 11:34:03 AM | 0.56750 | 829.65 | 81.30 |
| 8/13/2013 11:34:04 AM | 0.56778 | 822.17 | 81.28 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:34:05 AM | 0.56806 | 816.52 | 81.26 |
| 8/13/2013 11:34:06 AM | 0.56833 | 812.06 | 81.24 |
| 8/13/2013 11:34:07 AM | 0.56861 | 808.34 | 81.23 |
| 8/13/2013 11:34:08 AM | 0.56889 | 805.10 | 81.22 |
| 8/13/2013 11:34:09 AM | 0.56917 | 802.18 | 81.21 |
| 8/13/2013 11:34:10 AM | 0.56944 | 799.60 | 81.20 |
| 8/13/2013 11:34:11 AM | 0.56972 | 797.10 | 81.20 |
| 8/13/2013 11:34:12 AM | 0.57000 | 794.83 | 81.20 |
| 8/13/2013 11:34:13 AM | 0.57028 | 792.57 | 81.19 |
| 8/13/2013 11:34:14 AM | 0.57056 | 790.37 | 81.19 |
| 8/13/2013 11:34:15 AM | 0.57083 | 788.22 | 81.19 |
| 8/13/2013 11:34:16 AM | 0.57111 | 786.12 | 81.19 |
| 8/13/2013 11:34:17 AM | 0.57139 | 784.10 | 81.19 |
| 8/13/2013 11:34:18 AM | 0.57167 | 782.08 | 81.19 |
| 8/13/2013 11:34:19 AM | 0.57194 | 780.10 | 81.19 |
| 8/13/2013 11:34:20 AM | 0.57222 | 778.09 | 81.19 |
| 8/13/2013 11:34:21 AM | 0.57250 | 776.16 | 81.19 |
| 8/13/2013 11:34:22 AM | 0.57278 | 774.21 | 81.19 |
| 8/13/2013 11:34:23 AM | 0.57306 | 772.34 | 81.20 |
| 8/13/2013 11:34:24 AM | 0.57333 | 770.53 | 81.20 |
| 8/13/2013 11:34:25 AM | 0.57361 | 768.68 | 81.20 |
| 8/13/2013 11:34:26 AM | 0.57389 | 766.91 | 81.21 |
| 8/13/2013 11:34:27 AM | 0.57417 | 765.18 | 81.21 |
| 8/13/2013 11:34:28 AM | 0.57444 | 763.46 | 81.21 |
| 8/13/2013 11:34:29 AM | 0.57472 | 761.76 | 81.21 |
| 8/13/2013 11:34:30 AM | 0.57500 | 760.00 | 81.22 |
| 8/13/2013 11:34:31 AM | 0.57528 | 758.36 | 81.22 |
| 8/13/2013 11:34:32 AM | 0.57556 | 756.66 | 81.23 |
| 8/13/2013 11:34:33 AM | 0.57583 | 755.08 | 81.23 |
| 8/13/2013 11:34:34 AM | 0.57611 | 753.50 | 81.23 |
| 8/13/2013 11:34:35 AM | 0.57639 | 752.00 | 81.24 |
| 8/13/2013 11:34:36 AM | 0.57667 | 750.49 | 81.24 |
| 8/13/2013 11:34:37 AM | 0.57694 | 749.00 | 81.25 |
| 8/13/2013 11:34:38 AM | 0.57722 | 747.62 | 81.25 |
| 8/13/2013 11:34:39 AM | 0.57750 | 746.07 | 81.25 |
| 8/13/2013 11:34:40 AM | 0.57778 | 744.69 | 81.26 |
| 8/13/2013 11:34:41 AM | 0.57806 | 743.29 | 81.26 |
| 8/13/2013 11:34:42 AM | 0.57833 | 741.93 | 81.26 |
| 8/13/2013 11:34:43 AM | 0.57861 | 865.37 | 81.34 |
| 8/13/2013 11:34:44 AM | 0.57889 | 1632.27 | 81.85 |
| 8/13/2013 11:34:45 AM | 0.57917 | 1600.40 | 81.79 |
| 8/13/2013 11:34:46 AM | 0.57944 | 1581.55 | 81.76 |
| 8/13/2013 11:34:47 AM | 0.57972 | 1568.02 | 81.73 |
| 8/13/2013 11:34:48 AM | 0.58000 | 1557.89 | 81.69 |
| 8/13/2013 11:34:49 AM | 0.58028 | 1549.54 | 81.67 |
| 8/13/2013 11:34:50 AM | 0.58056 | 1542.41 | 81.64 |
| 8/13/2013 11:34:51 AM | 0.58083 | 1535.74 | 81.62 |
| 8/13/2013 11:34:52 AM | 0.58111 | 969.35 | 81.22 |
| 8/13/2013 11:34:53 AM | 0.58139 | 966.45 | 81.24 |
| 8/13/2013 11:34:54 AM | 0.58167 | 972.90 | 81.25 |
| 8/13/2013 11:34:55 AM | 0.58194 | 974.32 | 81.26 |
| 8/13/2013 11:34:56 AM | 0.58222 | 974.63 | 81.27 |
| 8/13/2013 11:34:57 AM | 0.58250 | 974.20 | 81.28 |
| 8/13/2013 11:34:58 AM | 0.58278 | 973.47 | 81.30 |
| 8/13/2013 11:34:59 AM | 0.58306 | 972.48 | 81.31 |
| 8/13/2013 11:35:00 AM | 0.58333 | 971.13 | 81.31 |
| 8/13/2013 11:35:01 AM | 0.58361 | 969.97 | 81.33 |
| 8/13/2013 11:35:02 AM | 0.58389 | 968.83 | 81.33 |
| 8/13/2013 11:35:03 AM | 0.58417 | 967.46 | 81.34 |
| 8/13/2013 11:35:04 AM | 0.58444 | 966.07 | 81.35 |
| 8/13/2013 11:35:05 AM | 0.58472 | 964.59 | 81.36 |
| 8/13/2013 11:35:06 AM | 0.58500 | 963.08 | 81.36 |
| 8/13/2013 11:35:07 AM | 0.58528 | 961.58 | 81.37 |
| 8/13/2013 11:35:08 AM | 0.58556 | 960.03 | 81.37 |
| 8/13/2013 11:35:09 AM | 0.58583 | 958.46 | 81.38 |
| 8/13/2013 11:35:10 AM | 0.58611 | 956.88 | 81.39 |
| 8/13/2013 11:35:11 AM | 0.58639 | 955.39 | 81.39 |
| 8/13/2013 11:35:12 AM | 0.58667 | 953.82 | 81.39 |
| 8/13/2013 11:35:13 AM | 0.58694 | 952.25 | 81.40 |
| 8/13/2013 11:35:14 AM | 0.58722 | 950.65 | 81.40 |
| 8/13/2013 11:35:15 AM | 0.58750 | 949.12 | 81.40 |
| 8/13/2013 11:35:16 AM | 0.58778 | 947.60 | 81.41 |
| 8/13/2013 11:35:17 AM | 0.58806 | 945.99 | 81.41 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:35:18 AM | 0.58833 | 944.43 | 81.41 |
| 8/13/2013 11:35:19 AM | 0.58861 | 942.87 | 81.42 |
| 8/13/2013 11:35:20 AM | 0.58889 | 941.38 | 81.42 |
| 8/13/2013 11:35:21 AM | 0.58917 | 939.81 | 81.42 |
| 8/13/2013 11:35:22 AM | 0.58944 | 938.35 | 81.42 |
| 8/13/2013 11:35:23 AM | 0.58972 | 936.79 | 81.42 |
| 8/13/2013 11:35:24 AM | 0.59000 | 935.39 | 81.43 |
| 8/13/2013 11:35:25 AM | 0.59028 | 933.97 | 81.43 |
| 8/13/2013 11:35:26 AM | 0.59056 | 932.59 | 81.43 |
| 8/13/2013 11:35:27 AM | 0.59083 | 931.22 | 81.43 |
| 8/13/2013 11:35:28 AM | 0.59111 | 929.87 | 81.43 |
| 8/13/2013 11:35:29 AM | 0.59139 | 928.53 | 81.43 |
| 8/13/2013 11:35:30 AM | 0.59167 | 927.15 | 81.43 |
| 8/13/2013 11:35:31 AM | 0.59194 | 925.80 | 81.44 |
| 8/13/2013 11:35:32 AM | 0.59222 | 924.49 | 81.44 |
| 8/13/2013 11:35:33 AM | 0.59250 | 923.17 | 81.44 |
| 8/13/2013 11:35:34 AM | 0.59278 | 921.86 | 81.44 |
| 8/13/2013 11:35:35 AM | 0.59306 | 920.52 | 81.44 |
| 8/13/2013 11:35:36 AM | 0.59333 | 919.16 | 81.44 |
| 8/13/2013 11:35:37 AM | 0.59361 | 917.85 | 81.44 |
| 8/13/2013 11:35:38 AM | 0.59389 | 916.58 | 81.44 |
| 8/13/2013 11:35:39 AM | 0.59417 | 915.25 | 81.44 |
| 8/13/2013 11:35:40 AM | 0.59444 | 914.00 | 81.44 |
| 8/13/2013 11:35:41 AM | 0.59472 | 912.77 | 81.44 |
| 8/13/2013 11:35:42 AM | 0.59500 | 911.56 | 81.44 |
| 8/13/2013 11:35:43 AM | 0.59528 | 910.33 | 81.44 |
| 8/13/2013 11:35:44 AM | 0.59556 | 909.12 | 81.44 |
| 8/13/2013 11:35:45 AM | 0.59583 | 907.92 | 81.44 |
| 8/13/2013 11:35:46 AM | 0.59611 | 906.73 | 81.44 |
| 8/13/2013 11:35:47 AM | 0.59639 | 905.55 | 81.44 |
| 8/13/2013 11:35:48 AM | 0.59667 | 904.34 | 81.44 |
| 8/13/2013 11:35:49 AM | 0.59694 | 903.16 | 81.44 |
| 8/13/2013 11:35:50 AM | 0.59722 | 902.00 | 81.43 |
| 8/13/2013 11:35:51 AM | 0.59750 | 900.84 | 81.43 |
| 8/13/2013 11:35:52 AM | 0.59778 | 899.65 | 81.43 |
| 8/13/2013 11:35:53 AM | 0.59806 | 898.44 | 81.43 |
| 8/13/2013 11:35:54 AM | 0.59833 | 897.22 | 81.43 |
| 8/13/2013 11:35:55 AM | 0.59861 | 896.08 | 81.43 |
| 8/13/2013 11:35:56 AM | 0.59889 | 894.87 | 81.43 |
| 8/13/2013 11:35:57 AM | 0.59917 | 893.69 | 81.43 |
| 8/13/2013 11:35:58 AM | 0.59944 | 892.50 | 81.43 |
| 8/13/2013 11:35:59 AM | 0.59972 | 891.31 | 81.42 |
| 8/13/2013 11:36:00 AM | 0.60000 | 890.17 | 81.42 |
| 8/13/2013 11:36:01 AM | 0.60028 | 888.99 | 81.42 |
| 8/13/2013 11:36:02 AM | 0.60056 | 887.77 | 81.42 |
| 8/13/2013 11:36:03 AM | 0.60083 | 886.61 | 81.42 |
| 8/13/2013 11:36:04 AM | 0.60111 | 885.42 | 81.42 |
| 8/13/2013 11:36:05 AM | 0.60139 | 884.24 | 81.42 |
| 8/13/2013 11:36:06 AM | 0.60167 | 883.10 | 81.42 |
| 8/13/2013 11:36:07 AM | 0.60194 | 881.93 | 81.42 |
| 8/13/2013 11:36:08 AM | 0.60222 | 880.77 | 81.41 |
| 8/13/2013 11:36:09 AM | 0.60250 | 879.64 | 81.41 |
| 8/13/2013 11:36:10 AM | 0.60278 | 878.52 | 81.41 |
| 8/13/2013 11:36:11 AM | 0.60306 | 877.37 | 81.41 |
| 8/13/2013 11:36:12 AM | 0.60333 | 876.25 | 81.41 |
| 8/13/2013 11:36:13 AM | 0.60361 | 875.10 | 81.41 |
| 8/13/2013 11:36:14 AM | 0.60389 | 873.98 | 81.40 |
| 8/13/2013 11:36:15 AM | 0.60417 | 872.84 | 81.40 |
| 8/13/2013 11:36:16 AM | 0.60444 | 871.74 | 81.40 |
| 8/13/2013 11:36:17 AM | 0.60472 | 870.60 | 81.40 |
| 8/13/2013 11:36:18 AM | 0.60500 | 869.48 | 81.40 |
| 8/13/2013 11:36:19 AM | 0.60528 | 868.35 | 81.40 |
| 8/13/2013 11:36:20 AM | 0.60556 | 867.24 | 81.39 |
| 8/13/2013 11:36:21 AM | 0.60583 | 866.15 | 81.39 |
| 8/13/2013 11:36:22 AM | 0.60611 | 865.03 | 81.39 |
| 8/13/2013 11:36:23 AM | 0.60639 | 863.95 | 81.39 |
| 8/13/2013 11:36:24 AM | 0.60667 | 862.87 | 81.39 |
| 8/13/2013 11:36:25 AM | 0.60694 | 861.75 | 81.39 |
| 8/13/2013 11:36:26 AM | 0.60722 | 860.65 | 81.38 |
| 8/13/2013 11:36:27 AM | 0.60750 | 859.63 | 81.38 |
| 8/13/2013 11:36:28 AM | 0.60778 | 858.62 | 81.38 |
| 8/13/2013 11:36:29 AM | 0.60806 | 857.57 | 81.38 |
| 8/13/2013 11:36:30 AM | 0.60833 | 856.53 | 81.38 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:36:31 AM | 0.60861 | 855.52 | 81.37 |
| 8/13/2013 11:36:32 AM | 0.60889 | 854.45 | 81.37 |
| 8/13/2013 11:36:33 AM | 0.60917 | 853.46 | 81.37 |
| 8/13/2013 11:36:34 AM | 0.60944 | 852.42 | 81.36 |
| 8/13/2013 11:36:35 AM | 0.60972 | 851.40 | 81.36 |
| 8/13/2013 11:36:36 AM | 0.61000 | 850.36 | 81.36 |
| 8/13/2013 11:36:37 AM | 0.61028 | 849.34 | 81.36 |
| 8/13/2013 11:36:38 AM | 0.61056 | 848.29 | 81.36 |
| 8/13/2013 11:36:39 AM | 0.61083 | 847.27 | 81.36 |
| 8/13/2013 11:36:40 AM | 0.61111 | 846.22 | 81.35 |
| 8/13/2013 11:36:41 AM | 0.61139 | 845.21 | 81.35 |
| 8/13/2013 11:36:42 AM | 0.61167 | 844.25 | 81.35 |
| 8/13/2013 11:36:43 AM | 0.61194 | 843.26 | 81.34 |
| 8/13/2013 11:36:44 AM | 0.61222 | 842.31 | 81.34 |
| 8/13/2013 11:36:45 AM | 0.61250 | 841.34 | 81.34 |
| 8/13/2013 11:36:46 AM | 0.61278 | 840.37 | 81.34 |
| 8/13/2013 11:36:47 AM | 0.61306 | 839.40 | 81.33 |
| 8/13/2013 11:36:48 AM | 0.61333 | 838.40 | 81.33 |
| 8/13/2013 11:36:49 AM | 0.61361 | 837.42 | 81.33 |
| 8/13/2013 11:36:50 AM | 0.61389 | 836.42 | 81.33 |
| 8/13/2013 11:36:51 AM | 0.61417 | 835.41 | 81.32 |
| 8/13/2013 11:36:52 AM | 0.61444 | 834.52 | 81.32 |
| 8/13/2013 11:36:53 AM | 0.61472 | 833.57 | 81.32 |
| 8/13/2013 11:36:54 AM | 0.61500 | 832.61 | 81.32 |
| 8/13/2013 11:36:55 AM | 0.61528 | 831.67 | 81.31 |
| 8/13/2013 11:36:56 AM | 0.61556 | 830.75 | 81.31 |
| 8/13/2013 11:36:57 AM | 0.61583 | 829.79 | 81.31 |
| 8/13/2013 11:36:58 AM | 0.61611 | 828.84 | 81.31 |
| 8/13/2013 11:36:59 AM | 0.61639 | 827.87 | 81.30 |
| 8/13/2013 11:37:00 AM | 0.61667 | 826.99 | 81.30 |
| 8/13/2013 11:37:01 AM | 0.61694 | 826.08 | 81.30 |
| 8/13/2013 11:37:02 AM | 0.61722 | 825.17 | 81.30 |
| 8/13/2013 11:37:03 AM | 0.61750 | 824.26 | 81.29 |
| 8/13/2013 11:37:04 AM | 0.61778 | 823.33 | 81.29 |
| 8/13/2013 11:37:05 AM | 0.61806 | 822.31 | 81.29 |
| 8/13/2013 11:37:06 AM | 0.61833 | 821.43 | 81.28 |
| 8/13/2013 11:37:07 AM | 0.61861 | 820.55 | 81.28 |
| 8/13/2013 11:37:08 AM | 0.61889 | 819.76 | 81.28 |
| 8/13/2013 11:37:09 AM | 0.61917 | 819.38 | 81.28 |
| 8/13/2013 11:37:10 AM | 0.61944 | 822.62 | 81.28 |
| 8/13/2013 11:37:11 AM | 0.61972 | 834.65 | 81.28 |
| 8/13/2013 11:37:12 AM | 0.62000 | 846.65 | 81.39 |
| 8/13/2013 11:37:13 AM | 0.62028 | 1570.98 | 81.75 |
| 8/13/2013 11:37:14 AM | 0.62056 | 1552.17 | 81.70 |
| 8/13/2013 11:37:15 AM | 0.62083 | 1539.63 | 81.67 |
| 8/13/2013 11:37:16 AM | 0.62111 | 1530.15 | 81.64 |
| 8/13/2013 11:37:17 AM | 0.62139 | 1522.55 | 81.61 |
| 8/13/2013 11:37:18 AM | 0.62167 | 1516.02 | 81.58 |
| 8/13/2013 11:37:19 AM | 0.62194 | 1510.20 | 81.55 |
| 8/13/2013 11:37:20 AM | 0.62222 | 1498.69 | 81.52 |
| 8/13/2013 11:37:21 AM | 0.62250 | 1493.15 | 81.50 |
| 8/13/2013 11:37:22 AM | 0.62278 | 1488.03 | 81.48 |
| 8/13/2013 11:37:23 AM | 0.62306 | 1482.82 | 81.47 |
| 8/13/2013 11:37:24 AM | 0.62333 | 1478.33 | 81.45 |
| 8/13/2013 11:37:25 AM | 0.62361 | 1472.83 | 81.44 |
| 8/13/2013 11:37:26 AM | 0.62389 | 1468.80 | 81.43 |
| 8/13/2013 11:37:27 AM | 0.62417 | 1463.56 | 81.41 |
| 8/13/2013 11:37:28 AM | 0.62444 | 1458.16 | 81.41 |
| 8/13/2013 11:37:29 AM | 0.62472 | 1370.90 | 81.34 |
| 8/13/2013 11:37:30 AM | 0.62500 | 1368.36 | 81.34 |
| 8/13/2013 11:37:31 AM | 0.62528 | 1259.77 | 81.27 |
| 8/13/2013 11:37:32 AM | 0.62556 | 1232.23 | 81.22 |
| 8/13/2013 11:37:33 AM | 0.62583 | 900.03 | 81.03 |
| 8/13/2013 11:37:34 AM | 0.62611 | 860.83 | 81.04 |
| 8/13/2013 11:37:35 AM | 0.62639 | 870.87 | 81.06 |
| 8/13/2013 11:37:36 AM | 0.62667 | 874.27 | 81.08 |
| 8/13/2013 11:37:37 AM | 0.62694 | 876.04 | 81.10 |
| 8/13/2013 11:37:38 AM | 0.62722 | 876.73 | 81.11 |
| 8/13/2013 11:37:39 AM | 0.62750 | 877.07 | 81.13 |
| 8/13/2013 11:37:40 AM | 0.62778 | 876.67 | 81.14 |
| 8/13/2013 11:37:41 AM | 0.62806 | 875.89 | 81.16 |
| 8/13/2013 11:37:42 AM | 0.62833 | 875.05 | 81.16 |
| 8/13/2013 11:37:43 AM | 0.62861 | 874.05 | 81.17 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:37:44 AM | 0.62889 | 872.97 | 81.18 |
| 8/13/2013 11:37:45 AM | 0.62917 | 871.85 | 81.19 |
| 8/13/2013 11:37:46 AM | 0.62944 | 870.66 | 81.19 |
| 8/13/2013 11:37:47 AM | 0.62972 | 869.43 | 81.20 |
| 8/13/2013 11:37:48 AM | 0.63000 | 868.26 | 81.20 |
| 8/13/2013 11:37:49 AM | 0.63028 | 867.08 | 81.21 |
| 8/13/2013 11:37:50 AM | 0.63056 | 865.91 | 81.21 |
| 8/13/2013 11:37:51 AM | 0.63083 | 864.73 | 81.21 |
| 8/13/2013 11:37:52 AM | 0.63111 | 863.24 | 81.21 |
| 8/13/2013 11:37:53 AM | 0.63139 | 861.27 | 81.21 |
| 8/13/2013 11:37:54 AM | 0.63167 | 859.82 | 81.21 |
| 8/13/2013 11:37:55 AM | 0.63194 | 858.35 | 81.21 |
| 8/13/2013 11:37:56 AM | 0.63222 | 857.03 | 81.21 |
| 8/13/2013 11:37:57 AM | 0.63250 | 855.68 | 81.21 |
| 8/13/2013 11:37:58 AM | 0.63278 | 854.39 | 81.21 |
| 8/13/2013 11:37:59 AM | 0.63306 | 853.13 | 81.21 |
| 8/13/2013 11:38:00 AM | 0.63333 | 851.81 | 81.21 |
| 8/13/2013 11:38:01 AM | 0.63361 | 850.58 | 81.21 |
| 8/13/2013 11:38:02 AM | 0.63389 | 849.27 | 81.20 |
| 8/13/2013 11:38:03 AM | 0.63417 | 848.02 | 81.20 |
| 8/13/2013 11:38:04 AM | 0.63444 | 846.77 | 81.20 |
| 8/13/2013 11:38:05 AM | 0.63472 | 845.56 | 81.20 |
| 8/13/2013 11:38:06 AM | 0.63500 | 844.34 | 81.20 |
| 8/13/2013 11:38:07 AM | 0.63528 | 843.10 | 81.20 |
| 8/13/2013 11:38:08 AM | 0.63556 | 841.91 | 81.19 |
| 8/13/2013 11:38:09 AM | 0.63583 | 840.68 | 81.19 |
| 8/13/2013 11:38:10 AM | 0.63611 | 839.48 | 81.19 |
| 8/13/2013 11:38:11 AM | 0.63639 | 838.26 | 81.19 |
| 8/13/2013 11:38:12 AM | 0.63667 | 837.05 | 81.18 |
| 8/13/2013 11:38:13 AM | 0.63694 | 835.86 | 81.18 |
| 8/13/2013 11:38:14 AM | 0.63722 | 834.66 | 81.18 |
| 8/13/2013 11:38:15 AM | 0.63750 | 833.43 | 81.17 |
| 8/13/2013 11:38:16 AM | 0.63778 | 832.18 | 81.17 |
| 8/13/2013 11:38:17 AM | 0.63806 | 830.95 | 81.17 |
| 8/13/2013 11:38:18 AM | 0.63833 | 829.73 | 81.16 |
| 8/13/2013 11:38:19 AM | 0.63861 | 828.47 | 81.16 |
| 8/13/2013 11:38:20 AM | 0.63889 | 827.27 | 81.16 |
| 8/13/2013 11:38:21 AM | 0.63917 | 826.02 | 81.15 |
| 8/13/2013 11:38:22 AM | 0.63944 | 824.86 | 81.15 |
| 8/13/2013 11:38:23 AM | 0.63972 | 823.71 | 81.15 |
| 8/13/2013 11:38:24 AM | 0.64000 | 822.54 | 81.14 |
| 8/13/2013 11:38:25 AM | 0.64028 | 821.37 | 81.14 |
| 8/13/2013 11:38:26 AM | 0.64056 | 820.25 | 81.14 |
| 8/13/2013 11:38:27 AM | 0.64083 | 819.19 | 81.13 |
| 8/13/2013 11:38:28 AM | 0.64111 | 818.17 | 81.13 |
| 8/13/2013 11:38:29 AM | 0.64139 | 817.15 | 81.12 |
| 8/13/2013 11:38:30 AM | 0.64167 | 816.09 | 81.12 |
| 8/13/2013 11:38:31 AM | 0.64194 | 815.04 | 81.12 |
| 8/13/2013 11:38:32 AM | 0.64222 | 813.92 | 81.11 |
| 8/13/2013 11:38:33 AM | 0.64250 | 812.78 | 81.11 |
| 8/13/2013 11:38:34 AM | 0.64278 | 811.65 | 81.11 |
| 8/13/2013 11:38:35 AM | 0.64306 | 810.46 | 81.11 |
| 8/13/2013 11:38:36 AM | 0.64333 | 809.27 | 81.10 |
| 8/13/2013 11:38:37 AM | 0.64361 | 804.00 | 81.09 |
| 8/13/2013 11:38:38 AM | 0.64389 | 113.39 | 80.62 |
| 8/13/2013 11:38:39 AM | 0.64417 | 23.17 | 80.60 |
| 8/13/2013 11:38:40 AM | 0.64444 | 14.84 | 80.61 |
| 8/13/2013 11:38:41 AM | 0.64472 | 14.69 | 80.63 |
| 8/13/2013 11:38:42 AM | 0.64500 | 14.56 | 80.66 |
| 8/13/2013 11:38:43 AM | 0.64528 | 14.46 | 80.68 |
| 8/13/2013 11:38:44 AM | 0.64556 | 14.38 | 80.70 |
| 8/13/2013 11:38:45 AM | 0.64583 | 14.33 | 80.72 |
| 8/13/2013 11:38:46 AM | 0.64611 | 14.33 | 80.74 |
| 8/13/2013 11:38:47 AM | 0.64639 | 14.33 | 80.75 |
| 8/13/2013 11:38:48 AM | 0.64667 | 14.31 | 80.75 |
| 8/13/2013 11:38:49 AM | 0.64694 | 14.33 | 80.77 |
| 8/13/2013 11:38:50 AM | 0.64722 | 14.38 | 80.78 |
| 8/13/2013 11:38:51 AM | 0.64750 | 14.44 | 80.79 |
| 8/13/2013 11:38:52 AM | 0.64778 | 14.53 | 80.79 |
| 8/13/2013 11:38:53 AM | 0.64806 | 14.64 | 80.80 |
| 8/13/2013 11:38:54 AM | 0.64833 | 14.75 | 80.80 |
| 8/13/2013 11:38:55 AM | 0.64861 | 14.86 | 80.80 |
| 8/13/2013 11:38:56 AM | 0.64889 | 15.34 | 80.80 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:38:57 AM | 0.64917 | 29.60 | 80.81 |
| 8/13/2013 11:38:58 AM | 0.64944 | 28.11 | 80.80 |
| 8/13/2013 11:38:59 AM | 0.64972 | 26.61 | 80.79 |
| 8/13/2013 11:39:00 AM | 0.65000 | 27.64 | 80.79 |
| 8/13/2013 11:39:01 AM | 0.65028 | 26.56 | 80.78 |
| 8/13/2013 11:39:02 AM | 0.65056 | 15.15 | 80.77 |
| 8/13/2013 11:39:03 AM | 0.65083 | 14.83 | 80.76 |
| 8/13/2013 11:39:04 AM | 0.65111 | 14.73 | 80.75 |
| 8/13/2013 11:39:05 AM | 0.65139 | 14.62 | 80.73 |
| 8/13/2013 11:39:06 AM | 0.65167 | 14.53 | 80.73 |
| 8/13/2013 11:39:07 AM | 0.65194 | 14.45 | 80.72 |
| 8/13/2013 11:39:08 AM | 0.65222 | 14.37 | 80.70 |
| 8/13/2013 11:39:09 AM | 0.65250 | 14.33 | 80.69 |
| 8/13/2013 11:39:10 AM | 0.65278 | 14.30 | 80.68 |
| 8/13/2013 11:39:11 AM | 0.65306 | 14.30 | 80.67 |
| 8/13/2013 11:39:12 AM | 0.65333 | 14.30 | 80.66 |
| 8/13/2013 11:39:13 AM | 0.65361 | 14.30 | 80.65 |
| 8/13/2013 11:39:14 AM | 0.65389 | 14.30 | 80.64 |
| 8/13/2013 11:39:15 AM | 0.65417 | 14.30 | 80.63 |
| 8/13/2013 11:39:16 AM | 0.65444 | 14.30 | 80.62 |
| 8/13/2013 11:39:17 AM | 0.65472 | 14.30 | 80.61 |
| 8/13/2013 11:39:18 AM | 0.65500 | 14.30 | 80.60 |
| 8/13/2013 11:39:19 AM | 0.65528 | 14.30 | 80.59 |
| 8/13/2013 11:39:20 AM | 0.65556 | 14.30 | 80.58 |
| 8/13/2013 11:39:21 AM | 0.65583 | 14.30 | 80.57 |
| 8/13/2013 11:39:22 AM | 0.65611 | 14.30 | 80.56 |
| 8/13/2013 11:39:23 AM | 0.65639 | 14.30 | 80.55 |
| 8/13/2013 11:39:24 AM | 0.65667 | 14.30 | 80.54 |
| 8/13/2013 11:39:25 AM | 0.65694 | 14.30 | 80.53 |
| 8/13/2013 11:39:26 AM | 0.65722 | 14.30 | 80.52 |
| 8/13/2013 11:39:27 AM | 0.65750 | 14.30 | 80.51 |
| 8/13/2013 11:39:28 AM | 0.65778 | 14.30 | 80.50 |
| 8/13/2013 11:39:29 AM | 0.65806 | 14.30 | 80.49 |
| 8/13/2013 11:39:30 AM | 0.65833 | 14.30 | 80.48 |
| 8/13/2013 11:39:31 AM | 0.65861 | 14.30 | 80.47 |
| 8/13/2013 11:39:32 AM | 0.65889 | 14.30 | 80.46 |
| 8/13/2013 11:39:33 AM | 0.65917 | 14.30 | 80.45 |
| 8/13/2013 11:39:34 AM | 0.65944 | 14.30 | 80.44 |
| 8/13/2013 11:39:35 AM | 0.65972 | 14.30 | 80.43 |
| 8/13/2013 11:39:36 AM | 0.66000 | 14.30 | 80.42 |
| 8/13/2013 11:39:37 AM | 0.66028 | 14.30 | 80.41 |
| 8/13/2013 11:39:38 AM | 0.66056 | 14.30 | 80.40 |
| 8/13/2013 11:39:39 AM | 0.66083 | 14.30 | 80.39 |
| 8/13/2013 11:39:40 AM | 0.66111 | 14.30 | 80.38 |
| 8/13/2013 11:39:41 AM | 0.66139 | 14.30 | 80.37 |
| 8/13/2013 11:39:42 AM | 0.66167 | 14.30 | 80.36 |
| 8/13/2013 11:39:43 AM | 0.66194 | 14.30 | 80.35 |
| 8/13/2013 11:39:44 AM | 0.66222 | 14.30 | 80.34 |
| 8/13/2013 11:39:45 AM | 0.66250 | 14.30 | 80.33 |
| 8/13/2013 11:39:46 AM | 0.66278 | 14.30 | 80.32 |
| 8/13/2013 11:39:47 AM | 0.66306 | 14.30 | 80.31 |
| 8/13/2013 11:39:48 AM | 0.66333 | 14.30 | 80.30 |
| 8/13/2013 11:39:49 AM | 0.66361 | 14.30 | 80.29 |
| 8/13/2013 11:39:50 AM | 0.66389 | 14.30 | 80.28 |
| 8/13/2013 11:39:51 AM | 0.66417 | 14.30 | 80.28 |
| 8/13/2013 11:39:52 AM | 0.66444 | 14.30 | 80.27 |
| 8/13/2013 11:39:53 AM | 0.66472 | 14.30 | 80.26 |
| 8/13/2013 11:39:54 AM | 0.66500 | 14.30 | 80.25 |
| 8/13/2013 11:39:55 AM | 0.66528 | 14.30 | 80.24 |
| 8/13/2013 11:39:56 AM | 0.66556 | 14.30 | 80.23 |
| 8/13/2013 11:39:57 AM | 0.66583 | 14.30 | 80.23 |
| 8/13/2013 11:39:58 AM | 0.66611 | 14.30 | 80.22 |
| 8/13/2013 11:39:59 AM | 0.66639 | 14.29 | 80.21 |
| 8/13/2013 11:40:00 AM | 0.66667 | 14.28 | 80.20 |
| 8/13/2013 11:40:01 AM | 0.66694 | 14.26 | 80.19 |
| 8/13/2013 11:40:02 AM | 0.66722 | 14.24 | 80.19 |
| 8/13/2013 11:40:03 AM | 0.66750 | 14.20 | 80.18 |
| 8/13/2013 11:40:04 AM | 0.66778 | 14.15 | 80.17 |
| 8/13/2013 11:40:05 AM | 0.66806 | 14.10 | 80.16 |
| 8/13/2013 11:40:06 AM | 0.66833 | 14.04 | 80.16 |
| 8/13/2013 11:40:07 AM | 0.66861 | 13.97 | 80.15 |
| 8/13/2013 11:40:08 AM | 0.66889 | 13.90 | 80.14 |
| 8/13/2013 11:40:09 AM | 0.66917 | 13.84 | 80.13 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:40:10 AM | 0.66944 | 13.79 | 80.12 |
| 8/13/2013 11:40:11 AM | 0.66972 | 13.74 | 80.11 |
| 8/13/2013 11:40:12 AM | 0.67000 | 13.71 | 80.09 |
| 8/13/2013 11:40:13 AM | 0.67028 | 13.68 | 80.08 |
| 8/13/2013 11:40:14 AM | 0.67056 | 13.66 | 80.06 |
| 8/13/2013 11:40:15 AM | 0.67083 | 13.65 | 80.04 |
| 8/13/2013 11:40:16 AM | 0.67111 | 13.65 | 80.02 |
| 8/13/2013 11:40:17 AM | 0.67139 | 13.66 | 80.00 |
| 8/13/2013 11:40:18 AM | 0.67167 | 13.66 | 79.97 |
| 8/13/2013 11:40:19 AM | 0.67194 | 13.67 | 79.94 |
| 8/13/2013 11:40:20 AM | 0.67222 | 13.67 | 79.91 |
| 8/13/2013 11:40:21 AM | 0.67250 | 13.68 | 79.88 |
| 8/13/2013 11:40:22 AM | 0.67278 | 13.68 | 79.85 |
| 8/13/2013 11:40:23 AM | 0.67306 | 13.69 | 79.81 |
| 8/13/2013 11:40:24 AM | 0.67333 | 13.69 | 79.78 |
| 8/13/2013 11:40:25 AM | 0.67361 | 13.70 | 79.75 |
| 8/13/2013 11:40:26 AM | 0.67389 | 13.70 | 79.71 |
| 8/13/2013 11:40:27 AM | 0.67417 | 13.71 | 79.68 |
| 8/13/2013 11:40:28 AM | 0.67444 | 13.71 | 79.64 |
| 8/13/2013 11:40:29 AM | 0.67472 | 13.72 | 79.61 |
| 8/13/2013 11:40:30 AM | 0.67500 | 13.72 | 79.58 |
| 8/13/2013 11:40:31 AM | 0.67528 | 13.73 | 79.55 |
| 8/13/2013 11:40:32 AM | 0.67556 | 13.73 | 79.52 |
| 8/13/2013 11:40:33 AM | 0.67583 | 13.74 | 79.49 |
| 8/13/2013 11:40:34 AM | 0.67611 | 13.75 | 79.47 |
| 8/13/2013 11:40:35 AM | 0.67639 | 13.76 | 79.44 |
| 8/13/2013 11:40:36 AM | 0.67667 | 13.77 | 79.42 |
| 8/13/2013 11:40:37 AM | 0.67694 | 13.78 | 79.39 |
| 8/13/2013 11:40:38 AM | 0.67722 | 13.79 | 79.37 |
| 8/13/2013 11:40:39 AM | 0.67750 | 13.80 | 79.35 |
| 8/13/2013 11:40:40 AM | 0.67778 | 13.81 | 79.33 |
| 8/13/2013 11:40:41 AM | 0.67806 | 13.82 | 79.31 |
| 8/13/2013 11:40:42 AM | 0.67833 | 13.82 | 79.30 |
| 8/13/2013 11:40:43 AM | 0.67861 | 13.83 | 79.28 |
| 8/13/2013 11:40:44 AM | 0.67889 | 13.83 | 79.27 |
| 8/13/2013 11:40:45 AM | 0.67917 | 13.83 | 79.25 |
| 8/13/2013 11:40:46 AM | 0.67944 | 13.83 | 79.24 |
| 8/13/2013 11:40:47 AM | 0.67972 | 13.83 | 79.22 |
| 8/13/2013 11:40:48 AM | 0.68000 | 13.83 | 79.21 |
| 8/13/2013 11:40:49 AM | 0.68028 | 13.84 | 79.20 |
| 8/13/2013 11:40:50 AM | 0.68056 | 13.84 | 79.19 |
| 8/13/2013 11:40:51 AM | 0.68083 | 13.84 | 79.18 |
| 8/13/2013 11:40:52 AM | 0.68111 | 13.85 | 79.17 |
| 8/13/2013 11:40:53 AM | 0.68139 | 13.85 | 79.16 |
| 8/13/2013 11:40:54 AM | 0.68167 | 13.86 | 79.15 |
| 8/13/2013 11:40:55 AM | 0.68194 | 13.87 | 79.14 |
| 8/13/2013 11:40:56 AM | 0.68222 | 13.87 | 79.13 |
| 8/13/2013 11:40:57 AM | 0.68250 | 13.88 | 79.12 |
| 8/13/2013 11:40:58 AM | 0.68278 | 13.88 | 79.12 |
| 8/13/2013 11:40:59 AM | 0.68306 | 13.89 | 79.11 |
| 8/13/2013 11:41:00 AM | 0.68333 | 13.89 | 79.10 |
| 8/13/2013 11:41:01 AM | 0.68361 | 13.89 | 79.09 |
| 8/13/2013 11:41:02 AM | 0.68389 | 13.90 | 79.09 |
| 8/13/2013 11:41:03 AM | 0.68417 | 13.90 | 79.08 |
| 8/13/2013 11:41:04 AM | 0.68444 | 13.91 | 79.08 |
| 8/13/2013 11:41:05 AM | 0.68472 | 13.91 | 79.07 |
| 8/13/2013 11:41:06 AM | 0.68500 | 13.92 | 79.06 |
| 8/13/2013 11:41:07 AM | 0.68528 | 13.93 | 79.06 |
| 8/13/2013 11:41:08 AM | 0.68556 | 13.93 | 79.05 |
| 8/13/2013 11:41:09 AM | 0.68583 | 13.94 | 79.05 |
| 8/13/2013 11:41:10 AM | 0.68611 | 13.95 | 79.04 |
| 8/13/2013 11:41:11 AM | 0.68639 | 13.95 | 79.04 |
| 8/13/2013 11:41:12 AM | 0.68667 | 13.95 | 79.03 |
| 8/13/2013 11:41:13 AM | 0.68694 | 13.96 | 79.03 |
| 8/13/2013 11:41:14 AM | 0.68722 | 13.96 | 79.02 |
| 8/13/2013 11:41:15 AM | 0.68750 | 13.96 | 79.02 |
| 8/13/2013 11:41:16 AM | 0.68778 | 13.96 | 79.02 |
| 8/13/2013 11:41:17 AM | 0.68806 | 13.96 | 79.01 |
| 8/13/2013 11:41:18 AM | 0.68833 | 13.96 | 79.01 |
| 8/13/2013 11:41:19 AM | 0.68861 | 13.96 | 79.00 |
| 8/13/2013 11:41:20 AM | 0.68889 | 13.97 | 79.00 |
| 8/13/2013 11:41:21 AM | 0.68917 | 13.97 | 78.99 |
| 8/13/2013 11:41:22 AM | 0.68944 | 13.97 | 78.99 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:41:23 AM | 0.68972 | 13.97 | 78.99 |
| 8/13/2013 11:41:24 AM | 0.69000 | 13.98 | 78.98 |
| 8/13/2013 11:41:25 AM | 0.69028 | 13.98 | 78.98 |
| 8/13/2013 11:41:26 AM | 0.69056 | 13.98 | 78.98 |
| 8/13/2013 11:41:27 AM | 0.69083 | 13.98 | 78.97 |
| 8/13/2013 11:41:28 AM | 0.69111 | 13.99 | 78.97 |
| 8/13/2013 11:41:29 AM | 0.69139 | 13.99 | 78.97 |
| 8/13/2013 11:41:30 AM | 0.69167 | 13.99 | 78.96 |
| 8/13/2013 11:41:31 AM | 0.69194 | 14.00 | 78.96 |
| 8/13/2013 11:41:32 AM | 0.69222 | 14.00 | 78.95 |
| 8/13/2013 11:41:33 AM | 0.69250 | 14.01 | 78.95 |
| 8/13/2013 11:41:34 AM | 0.69278 | 14.01 | 78.95 |
| 8/13/2013 11:41:35 AM | 0.69306 | 14.02 | 78.94 |
| 8/13/2013 11:41:36 AM | 0.69333 | 14.02 | 78.94 |
| 8/13/2013 11:41:37 AM | 0.69361 | 14.02 | 78.94 |
| 8/13/2013 11:41:38 AM | 0.69389 | 14.03 | 78.93 |
| 8/13/2013 11:41:39 AM | 0.69417 | 14.03 | 78.93 |
| 8/13/2013 11:41:40 AM | 0.69444 | 14.04 | 78.93 |
| 8/13/2013 11:41:41 AM | 0.69472 | 14.04 | 78.92 |
| 8/13/2013 11:41:42 AM | 0.69500 | 14.05 | 78.92 |
| 8/13/2013 11:41:43 AM | 0.69528 | 14.06 | 78.92 |
| 8/13/2013 11:41:44 AM | 0.69556 | 14.07 | 78.91 |
| 8/13/2013 11:41:45 AM | 0.69583 | 14.08 | 78.91 |
| 8/13/2013 11:41:46 AM | 0.69611 | 14.10 | 78.91 |
| 8/13/2013 11:41:47 AM | 0.69639 | 14.12 | 78.91 |
| 8/13/2013 11:41:48 AM | 0.69667 | 14.14 | 78.90 |
| 8/13/2013 11:41:49 AM | 0.69694 | 14.16 | 78.90 |
| 8/13/2013 11:41:50 AM | 0.69722 | 14.19 | 78.90 |
| 8/13/2013 11:41:51 AM | 0.69750 | 14.21 | 78.90 |
| 8/13/2013 11:41:52 AM | 0.69778 | 14.23 | 78.89 |
| 8/13/2013 11:41:53 AM | 0.69806 | 14.25 | 78.89 |
| 8/13/2013 11:41:54 AM | 0.69833 | 14.26 | 78.89 |
| 8/13/2013 11:41:55 AM | 0.69861 | 14.28 | 78.89 |
| 8/13/2013 11:41:56 AM | 0.69889 | 14.28 | 78.88 |
| 8/13/2013 11:41:57 AM | 0.69917 | 14.29 | 78.88 |
| 8/13/2013 11:41:58 AM | 0.69944 | 14.30 | 78.88 |
| 8/13/2013 11:41:59 AM | 0.69972 | 14.30 | 78.87 |
| 8/13/2013 11:42:00 AM | 0.70000 | 14.30 | 78.87 |
| 8/13/2013 11:42:01 AM | 0.70028 | 14.30 | 78.86 |
| 8/13/2013 11:42:02 AM | 0.70056 | 14.30 | 78.86 |
| 8/13/2013 11:42:03 AM | 0.70083 | 14.30 | 78.85 |
| 8/13/2013 11:42:04 AM | 0.70111 | 14.30 | 78.85 |
| 8/13/2013 11:42:05 AM | 0.70139 | 14.30 | 78.84 |
| 8/13/2013 11:42:06 AM | 0.70167 | 14.30 | 78.84 |
| 8/13/2013 11:42:07 AM | 0.70194 | 14.30 | 78.83 |
| 8/13/2013 11:42:08 AM | 0.70222 | 14.30 | 78.83 |
| 8/13/2013 11:42:09 AM | 0.70250 | 14.30 | 78.82 |
| 8/13/2013 11:42:10 AM | 0.70278 | 14.30 | 78.82 |
| 8/13/2013 11:42:11 AM | 0.70306 | 14.30 | 78.81 |
| 8/13/2013 11:42:12 AM | 0.70333 | 14.30 | 78.81 |
| 8/13/2013 11:42:13 AM | 0.70361 | 14.30 | 78.81 |
| 8/13/2013 11:42:14 AM | 0.70389 | 14.30 | 78.80 |
| 8/13/2013 11:42:15 AM | 0.70417 | 14.30 | 78.80 |
| 8/13/2013 11:42:16 AM | 0.70444 | 14.30 | 78.80 |
| 8/13/2013 11:42:17 AM | 0.70472 | 14.30 | 78.80 |
| 8/13/2013 11:42:18 AM | 0.70500 | 14.30 | 78.79 |
| 8/13/2013 11:42:19 AM | 0.70528 | 14.30 | 78.79 |
| 8/13/2013 11:42:20 AM | 0.70556 | 14.30 | 78.79 |
| 8/13/2013 11:42:21 AM | 0.70583 | 14.30 | 78.79 |
| 8/13/2013 11:42:22 AM | 0.70611 | 14.30 | 78.78 |
| 8/13/2013 11:42:23 AM | 0.70639 | 14.30 | 78.78 |
| 8/13/2013 11:42:24 AM | 0.70667 | 14.30 | 78.78 |
| 8/13/2013 11:42:25 AM | 0.70694 | 14.30 | 78.78 |
| 8/13/2013 11:42:26 AM | 0.70722 | 14.30 | 78.78 |
| 8/13/2013 11:42:27 AM | 0.70750 | 14.30 | 78.78 |
| 8/13/2013 11:42:28 AM | 0.70778 | 14.30 | 78.77 |
| 8/13/2013 11:42:29 AM | 0.70806 | 14.30 | 78.77 |
| 8/13/2013 11:42:30 AM | 0.70833 | 14.30 | 78.77 |
| 8/13/2013 11:42:31 AM | 0.70861 | 14.30 | 78.77 |
| 8/13/2013 11:42:32 AM | 0.70889 | 14.30 | 78.77 |
| 8/13/2013 11:42:33 AM | 0.70917 | 14.30 | 78.76 |
| 8/13/2013 11:42:34 AM | 0.70944 | 14.30 | 78.76 |
| 8/13/2013 11:42:35 AM | 0.70972 | 14.30 | 78.76 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:42:36 AM | 0.71000 | 14.30 | 78.76 |
| 8/13/2013 11:42:37 AM | 0.71028 | 14.30 | 78.76 |
| 8/13/2013 11:42:38 AM | 0.71056 | 14.30 | 78.75 |
| 8/13/2013 11:42:39 AM | 0.71083 | 14.30 | 78.75 |
| 8/13/2013 11:42:40 AM | 0.71111 | 14.30 | 78.75 |
| 8/13/2013 11:42:41 AM | 0.71139 | 14.30 | 78.75 |
| 8/13/2013 11:42:42 AM | 0.71167 | 14.30 | 78.75 |
| 8/13/2013 11:42:43 AM | 0.71194 | 14.30 | 78.75 |
| 8/13/2013 11:42:44 AM | 0.71222 | 14.30 | 78.75 |
| 8/13/2013 11:42:45 AM | 0.71250 | 14.30 | 78.74 |
| 8/13/2013 11:42:46 AM | 0.71278 | 14.30 | 78.74 |
| 8/13/2013 11:42:47 AM | 0.71306 | 14.30 | 78.74 |
| 8/13/2013 11:42:48 AM | 0.71333 | 14.30 | 78.74 |
| 8/13/2013 11:42:49 AM | 0.71361 | 14.30 | 78.74 |
| 8/13/2013 11:42:50 AM | 0.71389 | 14.30 | 78.74 |
| 8/13/2013 11:42:51 AM | 0.71417 | 14.30 | 78.73 |
| 8/13/2013 11:42:52 AM | 0.71444 | 14.30 | 78.73 |
| 8/13/2013 11:42:53 AM | 0.71472 | 14.30 | 78.73 |
| 8/13/2013 11:42:54 AM | 0.71500 | 14.30 | 78.73 |
| 8/13/2013 11:42:55 AM | 0.71528 | 14.30 | 78.73 |
| 8/13/2013 11:42:56 AM | 0.71556 | 14.30 | 78.73 |
| 8/13/2013 11:42:57 AM | 0.71583 | 14.30 | 78.72 |
| 8/13/2013 11:42:58 AM | 0.71611 | 14.30 | 78.72 |
| 8/13/2013 11:42:59 AM | 0.71639 | 14.30 | 78.72 |
| 8/13/2013 11:43:00 AM | 0.71667 | 14.30 | 78.72 |
| 8/13/2013 11:43:01 AM | 0.71694 | 14.30 | 78.72 |
| 8/13/2013 11:43:02 AM | 0.71722 | 14.30 | 78.72 |
| 8/13/2013 11:43:03 AM | 0.71750 | 14.30 | 78.71 |
| 8/13/2013 11:43:04 AM | 0.71778 | 14.30 | 78.71 |
| 8/13/2013 11:43:05 AM | 0.71806 | 14.30 | 78.71 |
| 8/13/2013 11:43:06 AM | 0.71833 | 14.30 | 78.71 |
| 8/13/2013 11:43:07 AM | 0.71861 | 14.30 | 78.71 |
| 8/13/2013 11:43:08 AM | 0.71889 | 14.30 | 78.71 |
| 8/13/2013 11:43:09 AM | 0.71917 | 14.30 | 78.70 |
| 8/13/2013 11:43:10 AM | 0.71944 | 14.30 | 78.70 |
| 8/13/2013 11:43:11 AM | 0.71972 | 14.30 | 78.70 |
| 8/13/2013 11:43:12 AM | 0.72000 | 14.30 | 78.70 |
| 8/13/2013 11:43:13 AM | 0.72028 | 14.30 | 78.70 |
| 8/13/2013 11:43:14 AM | 0.72056 | 14.30 | 78.70 |
| 8/13/2013 11:43:15 AM | 0.72083 | 14.30 | 78.70 |
| 8/13/2013 11:43:16 AM | 0.72111 | 14.30 | 78.70 |
| 8/13/2013 11:43:17 AM | 0.72139 | 14.30 | 78.70 |
| 8/13/2013 11:43:18 AM | 0.72167 | 14.30 | 78.69 |
| 8/13/2013 11:43:19 AM | 0.72194 | 14.30 | 78.69 |
| 8/13/2013 11:43:20 AM | 0.72222 | 14.30 | 78.69 |
| 8/13/2013 11:43:21 AM | 0.72250 | 14.30 | 78.69 |
| 8/13/2013 11:43:22 AM | 0.72278 | 14.30 | 78.69 |
| 8/13/2013 11:43:23 AM | 0.72306 | 14.30 | 78.69 |
| 8/13/2013 11:43:24 AM | 0.72333 | 14.30 | 78.69 |
| 8/13/2013 11:43:25 AM | 0.72361 | 14.30 | 78.69 |
| 8/13/2013 11:43:26 AM | 0.72389 | 14.30 | 78.69 |
| 8/13/2013 11:43:27 AM | 0.72417 | 14.30 | 78.69 |
| 8/13/2013 11:43:28 AM | 0.72444 | 14.30 | 78.69 |
| 8/13/2013 11:43:29 AM | 0.72472 | 14.30 | 78.69 |
| 8/13/2013 11:43:30 AM | 0.72500 | 14.30 | 78.69 |
| 8/13/2013 11:43:31 AM | 0.72528 | 14.30 | 78.69 |
| 8/13/2013 11:43:32 AM | 0.72556 | 14.30 | 78.68 |
| 8/13/2013 11:43:33 AM | 0.72583 | 14.30 | 78.68 |
| 8/13/2013 11:43:34 AM | 0.72611 | 14.30 | 78.68 |
| 8/13/2013 11:43:35 AM | 0.72639 | 14.30 | 78.68 |
| 8/13/2013 11:43:36 AM | 0.72667 | 14.30 | 78.68 |
| 8/13/2013 11:43:37 AM | 0.72694 | 14.30 | 78.68 |
| 8/13/2013 11:43:38 AM | 0.72722 | 14.30 | 78.68 |
| 8/13/2013 11:43:39 AM | 0.72750 | 14.30 | 78.68 |
| 8/13/2013 11:43:40 AM | 0.72778 | 14.30 | 78.68 |
| 8/13/2013 11:43:41 AM | 0.72806 | 14.30 | 78.68 |
| 8/13/2013 11:43:42 AM | 0.72833 | 14.30 | 78.67 |
| 8/13/2013 11:43:43 AM | 0.72861 | 14.30 | 78.67 |
| 8/13/2013 11:43:44 AM | 0.72889 | 14.30 | 78.67 |
| 8/13/2013 11:43:45 AM | 0.72917 | 14.30 | 78.67 |
| 8/13/2013 11:43:46 AM | 0.72944 | 14.30 | 78.67 |
| 8/13/2013 11:43:47 AM | 0.72972 | 14.30 | 78.67 |
| 8/13/2013 11:43:48 AM | 0.73000 | 14.30 | 78.67 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:43:49 AM | 0.73028 | 14.30 | 78.67 |
| 8/13/2013 11:43:50 AM | 0.73056 | 14.30 | 78.67 |
| 8/13/2013 11:43:51 AM | 0.73083 | 14.30 | 78.67 |
| 8/13/2013 11:43:52 AM | 0.73111 | 14.30 | 78.67 |
| 8/13/2013 11:43:53 AM | 0.73139 | 14.30 | 78.67 |
| 8/13/2013 11:43:54 AM | 0.73167 | 14.30 | 78.67 |
| 8/13/2013 11:43:55 AM | 0.73194 | 14.30 | 78.67 |
| 8/13/2013 11:43:56 AM | 0.73222 | 14.30 | 78.67 |
| 8/13/2013 11:43:57 AM | 0.73250 | 14.30 | 78.67 |
| 8/13/2013 11:43:58 AM | 0.73278 | 14.30 | 78.67 |
| 8/13/2013 11:43:59 AM | 0.73306 | 14.30 | 78.67 |
| 8/13/2013 11:44:00 AM | 0.73333 | 14.30 | 78.67 |
| 8/13/2013 11:44:01 AM | 0.73361 | 14.30 | 78.67 |
| 8/13/2013 11:44:02 AM | 0.73389 | 14.30 | 78.67 |
| 8/13/2013 11:44:03 AM | 0.73417 | 14.30 | 78.67 |
| 8/13/2013 11:44:04 AM | 0.73444 | 14.30 | 78.67 |
| 8/13/2013 11:44:05 AM | 0.73472 | 14.30 | 78.67 |
| 8/13/2013 11:44:06 AM | 0.73500 | 14.30 | 78.67 |
| 8/13/2013 11:44:07 AM | 0.73528 | 14.30 | 78.67 |
| 8/13/2013 11:44:08 AM | 0.73556 | 14.30 | 78.67 |
| 8/13/2013 11:44:09 AM | 0.73583 | 14.30 | 78.67 |
| 8/13/2013 11:44:10 AM | 0.73611 | 14.30 | 78.67 |
| 8/13/2013 11:44:11 AM | 0.73639 | 14.30 | 78.66 |
| 8/13/2013 11:44:12 AM | 0.73667 | 14.30 | 78.66 |
| 8/13/2013 11:44:13 AM | 0.73694 | 14.30 | 78.66 |
| 8/13/2013 11:44:14 AM | 0.73722 | 14.30 | 78.66 |
| 8/13/2013 11:44:15 AM | 0.73750 | 14.30 | 78.66 |
| 8/13/2013 11:44:16 AM | 0.73778 | 14.30 | 78.66 |
| 8/13/2013 11:44:17 AM | 0.73806 | 14.30 | 78.66 |
| 8/13/2013 11:44:18 AM | 0.73833 | 14.30 | 78.66 |
| 8/13/2013 11:44:19 AM | 0.73861 | 14.30 | 78.66 |
| 8/13/2013 11:44:20 AM | 0.73889 | 14.30 | 78.66 |
| 8/13/2013 11:44:21 AM | 0.73917 | 14.30 | 78.66 |
| 8/13/2013 11:44:22 AM | 0.73944 | 14.30 | 78.66 |
| 8/13/2013 11:44:23 AM | 0.73972 | 14.30 | 78.66 |
| 8/13/2013 11:44:24 AM | 0.74000 | 14.30 | 78.66 |
| 8/13/2013 11:44:25 AM | 0.74028 | 14.30 | 78.66 |
| 8/13/2013 11:44:26 AM | 0.74056 | 14.30 | 78.66 |
| 8/13/2013 11:44:27 AM | 0.74083 | 14.30 | 78.66 |
| 8/13/2013 11:44:28 AM | 0.74111 | 14.30 | 78.66 |
| 8/13/2013 11:44:29 AM | 0.74139 | 14.30 | 78.66 |
| 8/13/2013 11:44:30 AM | 0.74167 | 14.30 | 78.66 |
| 8/13/2013 11:44:31 AM | 0.74194 | 14.30 | 78.65 |
| 8/13/2013 11:44:32 AM | 0.74222 | 14.30 | 78.65 |
| 8/13/2013 11:44:33 AM | 0.74250 | 14.30 | 78.65 |
| 8/13/2013 11:44:34 AM | 0.74278 | 14.30 | 78.65 |
| 8/13/2013 11:44:35 AM | 0.74306 | 14.30 | 78.65 |
| 8/13/2013 11:44:36 AM | 0.74333 | 14.30 | 78.65 |
| 8/13/2013 11:44:37 AM | 0.74361 | 14.30 | 78.65 |
| 8/13/2013 11:44:38 AM | 0.74389 | 14.30 | 78.65 |
| 8/13/2013 11:44:39 AM | 0.74417 | 14.30 | 78.65 |
| 8/13/2013 11:44:40 AM | 0.74444 | 14.30 | 78.65 |
| 8/13/2013 11:44:41 AM | 0.74472 | 14.30 | 78.65 |
| 8/13/2013 11:44:42 AM | 0.74500 | 14.30 | 78.65 |
| 8/13/2013 11:44:43 AM | 0.74528 | 14.30 | 78.65 |
| 8/13/2013 11:44:44 AM | 0.74556 | 14.30 | 78.65 |
| 8/13/2013 11:44:45 AM | 0.74583 | 14.30 | 78.65 |
| 8/13/2013 11:44:46 AM | 0.74611 | 14.30 | 78.65 |
| 8/13/2013 11:44:47 AM | 0.74639 | 14.30 | 78.65 |
| 8/13/2013 11:44:48 AM | 0.74667 | 14.30 | 78.65 |
| 8/13/2013 11:44:49 AM | 0.74694 | 14.30 | 78.64 |
| 8/13/2013 11:44:50 AM | 0.74722 | 14.30 | 78.64 |
| 8/13/2013 11:44:51 AM | 0.74750 | 14.30 | 78.64 |
| 8/13/2013 11:44:52 AM | 0.74778 | 14.30 | 78.64 |
| 8/13/2013 11:44:53 AM | 0.74806 | 14.30 | 78.64 |
| 8/13/2013 11:44:54 AM | 0.74833 | 14.30 | 78.64 |
| 8/13/2013 11:44:55 AM | 0.74861 | 14.30 | 78.64 |
| 8/13/2013 11:44:56 AM | 0.74889 | 14.30 | 78.64 |
| 8/13/2013 11:44:57 AM | 0.74917 | 14.30 | 78.64 |
| 8/13/2013 11:44:58 AM | 0.74944 | 14.30 | 78.64 |
| 8/13/2013 11:44:59 AM | 0.74972 | 14.30 | 78.64 |
| 8/13/2013 11:45:00 AM | 0.75000 | 14.30 | 78.64 |
| 8/13/2013 11:45:01 AM | 0.75028 | 14.30 | 78.64 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:45:02 AM | 0.75056 | 14.30 | 78.64 |
| 8/13/2013 11:45:03 AM | 0.75083 | 14.30 | 78.64 |
| 8/13/2013 11:45:04 AM | 0.75111 | 14.30 | 78.64 |
| 8/13/2013 11:45:05 AM | 0.75139 | 14.30 | 78.64 |
| 8/13/2013 11:45:06 AM | 0.75167 | 14.30 | 78.64 |
| 8/13/2013 11:45:07 AM | 0.75194 | 14.30 | 78.64 |
| 8/13/2013 11:45:08 AM | 0.75222 | 14.30 | 78.64 |
| 8/13/2013 11:45:09 AM | 0.75250 | 14.30 | 78.64 |
| 8/13/2013 11:45:10 AM | 0.75278 | 14.30 | 78.64 |
| 8/13/2013 11:45:11 AM | 0.75306 | 14.30 | 78.64 |
| 8/13/2013 11:45:12 AM | 0.75333 | 14.30 | 78.64 |
| 8/13/2013 11:45:13 AM | 0.75361 | 14.30 | 78.64 |
| 8/13/2013 11:45:14 AM | 0.75389 | 14.30 | 78.64 |
| 8/13/2013 11:45:15 AM | 0.75417 | 14.30 | 78.64 |
| 8/13/2013 11:45:16 AM | 0.75444 | 14.30 | 78.64 |
| 8/13/2013 11:45:17 AM | 0.75472 | 14.30 | 78.64 |
| 8/13/2013 11:45:18 AM | 0.75500 | 14.30 | 78.64 |
| 8/13/2013 11:45:19 AM | 0.75528 | 14.30 | 78.63 |
| 8/13/2013 11:45:20 AM | 0.75556 | 14.30 | 78.63 |
| 8/13/2013 11:45:21 AM | 0.75583 | 14.30 | 78.63 |
| 8/13/2013 11:45:22 AM | 0.75611 | 14.30 | 78.63 |
| 8/13/2013 11:45:23 AM | 0.75639 | 14.30 | 78.63 |
| 8/13/2013 11:45:24 AM | 0.75667 | 14.30 | 78.63 |
| 8/13/2013 11:45:25 AM | 0.75694 | 14.30 | 78.63 |
| 8/13/2013 11:45:26 AM | 0.75722 | 14.30 | 78.63 |
| 8/13/2013 11:45:27 AM | 0.75750 | 14.30 | 78.63 |
| 8/13/2013 11:45:28 AM | 0.75778 | 14.30 | 78.63 |
| 8/13/2013 11:45:29 AM | 0.75806 | 14.30 | 78.63 |
| 8/13/2013 11:45:30 AM | 0.75833 | 14.30 | 78.63 |
| 8/13/2013 11:45:31 AM | 0.75861 | 14.30 | 78.63 |
| 8/13/2013 11:45:32 AM | 0.75889 | 14.30 | 78.63 |
| 8/13/2013 11:45:33 AM | 0.75917 | 14.30 | 78.63 |
| 8/13/2013 11:45:34 AM | 0.75944 | 14.30 | 78.63 |
| 8/13/2013 11:45:35 AM | 0.75972 | 14.30 | 78.63 |
| 8/13/2013 11:45:36 AM | 0.76000 | 14.30 | 78.63 |
| 8/13/2013 11:45:37 AM | 0.76028 | 14.30 | 78.63 |
| 8/13/2013 11:45:38 AM | 0.76056 | 14.30 | 78.63 |
| 8/13/2013 11:45:39 AM | 0.76083 | 14.30 | 78.63 |
| 8/13/2013 11:45:40 AM | 0.76111 | 14.30 | 78.63 |
| 8/13/2013 11:45:41 AM | 0.76139 | 14.30 | 78.63 |
| 8/13/2013 11:45:42 AM | 0.76167 | 14.30 | 78.63 |
| 8/13/2013 11:45:43 AM | 0.76194 | 14.30 | 78.63 |
| 8/13/2013 11:45:44 AM | 0.76222 | 14.30 | 78.63 |
| 8/13/2013 11:45:45 AM | 0.76250 | 14.30 | 78.63 |
| 8/13/2013 11:45:46 AM | 0.76278 | 14.30 | 78.63 |
| 8/13/2013 11:45:47 AM | 0.76306 | 14.30 | 78.63 |
| 8/13/2013 11:45:48 AM | 0.76333 | 14.30 | 78.63 |
| 8/13/2013 11:45:49 AM | 0.76361 | 14.30 | 78.63 |
| 8/13/2013 11:45:50 AM | 0.76389 | 14.30 | 78.63 |
| 8/13/2013 11:45:51 AM | 0.76417 | 14.30 | 78.63 |
| 8/13/2013 11:45:52 AM | 0.76444 | 14.30 | 78.63 |
| 8/13/2013 11:45:53 AM | 0.76472 | 14.30 | 78.63 |
| 8/13/2013 11:45:54 AM | 0.76500 | 14.30 | 78.63 |
| 8/13/2013 11:45:55 AM | 0.76528 | 14.30 | 78.63 |
| 8/13/2013 11:45:56 AM | 0.76556 | 14.30 | 78.63 |
| 8/13/2013 11:45:57 AM | 0.76583 | 14.30 | 78.63 |
| 8/13/2013 11:45:58 AM | 0.76611 | 14.30 | 78.63 |
| 8/13/2013 11:45:59 AM | 0.76639 | 14.30 | 78.63 |
| 8/13/2013 11:46:00 AM | 0.76667 | 14.30 | 78.63 |
| 8/13/2013 11:46:01 AM | 0.76694 | 14.30 | 78.63 |
| 8/13/2013 11:46:02 AM | 0.76722 | 14.30 | 78.63 |
| 8/13/2013 11:46:03 AM | 0.76750 | 14.30 | 78.63 |
| 8/13/2013 11:46:04 AM | 0.76778 | 14.30 | 78.63 |
| 8/13/2013 11:46:05 AM | 0.76806 | 14.30 | 78.63 |
| 8/13/2013 11:46:06 AM | 0.76833 | 14.30 | 78.63 |
| 8/13/2013 11:46:07 AM | 0.76861 | 14.30 | 78.63 |
| 8/13/2013 11:46:08 AM | 0.76889 | 14.30 | 78.63 |
| 8/13/2013 11:46:09 AM | 0.76917 | 14.30 | 78.63 |
| 8/13/2013 11:46:10 AM | 0.76944 | 14.30 | 78.63 |
| 8/13/2013 11:46:11 AM | 0.76972 | 14.30 | 78.63 |
| 8/13/2013 11:46:12 AM | 0.77000 | 14.30 | 78.63 |
| 8/13/2013 11:46:13 AM | 0.77028 | 14.30 | 78.63 |
| 8/13/2013 11:46:14 AM | 0.77056 | 14.30 | 78.63 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:46:15 AM | 0.77083 | 14.30 | 78.63 |
| 8/13/2013 11:46:16 AM | 0.77111 | 14.30 | 78.63 |
| 8/13/2013 11:46:17 AM | 0.77139 | 14.30 | 78.63 |
| 8/13/2013 11:46:18 AM | 0.77167 | 14.30 | 78.63 |
| 8/13/2013 11:46:19 AM | 0.77194 | 14.30 | 78.63 |
| 8/13/2013 11:46:20 AM | 0.77222 | 14.30 | 78.63 |
| 8/13/2013 11:46:21 AM | 0.77250 | 14.30 | 78.63 |
| 8/13/2013 11:46:22 AM | 0.77278 | 14.30 | 78.63 |
| 8/13/2013 11:46:23 AM | 0.77306 | 14.30 | 78.63 |
| 8/13/2013 11:46:24 AM | 0.77333 | 14.30 | 78.63 |
| 8/13/2013 11:46:25 AM | 0.77361 | 14.30 | 78.63 |
| 8/13/2013 11:46:26 AM | 0.77389 | 14.30 | 78.63 |
| 8/13/2013 11:46:27 AM | 0.77417 | 14.30 | 78.63 |
| 8/13/2013 11:46:28 AM | 0.77444 | 14.30 | 78.63 |
| 8/13/2013 11:46:29 AM | 0.77472 | 14.30 | 78.63 |
| 8/13/2013 11:46:30 AM | 0.77500 | 14.30 | 78.63 |
| 8/13/2013 11:46:31 AM | 0.77528 | 14.30 | 78.63 |
| 8/13/2013 11:46:32 AM | 0.77556 | 14.30 | 78.63 |
| 8/13/2013 11:46:33 AM | 0.77583 | 14.30 | 78.63 |
| 8/13/2013 11:46:34 AM | 0.77611 | 14.30 | 78.63 |
| 8/13/2013 11:46:35 AM | 0.77639 | 14.30 | 78.63 |
| 8/13/2013 11:46:36 AM | 0.77667 | 14.30 | 78.63 |
| 8/13/2013 11:46:37 AM | 0.77694 | 14.30 | 78.63 |
| 8/13/2013 11:46:38 AM | 0.77722 | 14.30 | 78.63 |
| 8/13/2013 11:46:39 AM | 0.77750 | 14.30 | 78.63 |
| 8/13/2013 11:46:40 AM | 0.77778 | 14.30 | 78.63 |
| 8/13/2013 11:46:41 AM | 0.77806 | 14.30 | 78.63 |
| 8/13/2013 11:46:42 AM | 0.77833 | 14.30 | 78.63 |
| 8/13/2013 11:46:43 AM | 0.77861 | 14.30 | 78.63 |
| 8/13/2013 11:46:44 AM | 0.77889 | 14.30 | 78.63 |
| 8/13/2013 11:46:45 AM | 0.77917 | 14.30 | 78.62 |
| 8/13/2013 11:46:46 AM | 0.77944 | 14.30 | 78.63 |
| 8/13/2013 11:46:47 AM | 0.77972 | 14.30 | 78.63 |
| 8/13/2013 11:46:48 AM | 0.78000 | 14.30 | 78.63 |
| 8/13/2013 11:46:49 AM | 0.78028 | 14.30 | 78.63 |
| 8/13/2013 11:46:50 AM | 0.78056 | 14.30 | 78.63 |
| 8/13/2013 11:46:51 AM | 0.78083 | 14.30 | 78.63 |
| 8/13/2013 11:46:52 AM | 0.78111 | 14.30 | 78.62 |
| 8/13/2013 11:46:53 AM | 0.78139 | 14.30 | 78.62 |
| 8/13/2013 11:46:54 AM | 0.78167 | 14.30 | 78.62 |
| 8/13/2013 11:46:55 AM | 0.78194 | 14.30 | 78.62 |
| 8/13/2013 11:46:56 AM | 0.78222 | 14.30 | 78.62 |
| 8/13/2013 11:46:57 AM | 0.78250 | 14.30 | 78.62 |
| 8/13/2013 11:46:58 AM | 0.78278 | 14.30 | 78.62 |
| 8/13/2013 11:46:59 AM | 0.78306 | 14.30 | 78.62 |
| 8/13/2013 11:47:00 AM | 0.78333 | 14.30 | 78.62 |
| 8/13/2013 11:47:01 AM | 0.78361 | 14.30 | 78.62 |
| 8/13/2013 11:47:02 AM | 0.78389 | 14.30 | 78.62 |
| 8/13/2013 11:47:03 AM | 0.78417 | 14.30 | 78.62 |
| 8/13/2013 11:47:04 AM | 0.78444 | 14.30 | 78.62 |
| 8/13/2013 11:47:05 AM | 0.78472 | 14.30 | 78.62 |
| 8/13/2013 11:47:06 AM | 0.78500 | 14.30 | 78.62 |
| 8/13/2013 11:47:07 AM | 0.78528 | 14.30 | 78.62 |
| 8/13/2013 11:47:08 AM | 0.78556 | 14.30 | 78.62 |
| 8/13/2013 11:47:09 AM | 0.78583 | 14.30 | 78.62 |
| 8/13/2013 11:47:10 AM | 0.78611 | 14.30 | 78.62 |
| 8/13/2013 11:47:11 AM | 0.78639 | 14.30 | 78.62 |
| 8/13/2013 11:47:12 AM | 0.78667 | 14.30 | 78.62 |
| 8/13/2013 11:47:13 AM | 0.78694 | 14.30 | 78.62 |
| 8/13/2013 11:47:14 AM | 0.78722 | 14.30 | 78.62 |
| 8/13/2013 11:47:15 AM | 0.78750 | 14.30 | 78.62 |
| 8/13/2013 11:47:16 AM | 0.78778 | 14.30 | 78.62 |
| 8/13/2013 11:47:17 AM | 0.78806 | 14.30 | 78.62 |
| 8/13/2013 11:47:18 AM | 0.78833 | 14.30 | 78.62 |
| 8/13/2013 11:47:19 AM | 0.78861 | 14.30 | 78.62 |
| 8/13/2013 11:47:20 AM | 0.78889 | 14.30 | 78.62 |
| 8/13/2013 11:47:21 AM | 0.78917 | 14.30 | 78.62 |
| 8/13/2013 11:47:22 AM | 0.78944 | 14.30 | 78.61 |
| 8/13/2013 11:47:23 AM | 0.78972 | 14.30 | 78.61 |
| 8/13/2013 11:47:24 AM | 0.79000 | 14.30 | 78.61 |
| 8/13/2013 11:47:25 AM | 0.79028 | 14.30 | 78.61 |
| 8/13/2013 11:47:26 AM | 0.79056 | 14.30 | 78.61 |
| 8/13/2013 11:47:27 AM | 0.79083 | 14.30 | 78.61 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:47:28 AM | 0.79111 | 14.30 | 78.61 |
| 8/13/2013 11:47:29 AM | 0.79139 | 14.30 | 78.61 |
| 8/13/2013 11:47:30 AM | 0.79167 | 14.30 | 78.61 |
| 8/13/2013 11:47:31 AM | 0.79194 | 14.30 | 78.61 |
| 8/13/2013 11:47:32 AM | 0.79222 | 14.30 | 78.61 |
| 8/13/2013 11:47:33 AM | 0.79250 | 14.30 | 78.61 |
| 8/13/2013 11:47:34 AM | 0.79278 | 14.30 | 78.61 |
| 8/13/2013 11:47:35 AM | 0.79306 | 14.30 | 78.61 |
| 8/13/2013 11:47:36 AM | 0.79333 | 14.30 | 78.61 |
| 8/13/2013 11:47:37 AM | 0.79361 | 14.30 | 78.61 |
| 8/13/2013 11:47:38 AM | 0.79389 | 14.30 | 78.61 |
| 8/13/2013 11:47:39 AM | 0.79417 | 14.30 | 78.61 |
| 8/13/2013 11:47:40 AM | 0.79444 | 14.30 | 78.61 |
| 8/13/2013 11:47:41 AM | 0.79472 | 14.30 | 78.61 |
| 8/13/2013 11:47:42 AM | 0.79500 | 14.30 | 78.61 |
| 8/13/2013 11:47:43 AM | 0.79528 | 14.30 | 78.61 |
| 8/13/2013 11:47:44 AM | 0.79556 | 14.30 | 78.61 |
| 8/13/2013 11:47:45 AM | 0.79583 | 14.30 | 78.61 |
| 8/13/2013 11:47:46 AM | 0.79611 | 14.30 | 78.61 |
| 8/13/2013 11:47:47 AM | 0.79639 | 14.30 | 78.61 |
| 8/13/2013 11:47:48 AM | 0.79667 | 14.30 | 78.61 |
| 8/13/2013 11:47:49 AM | 0.79694 | 14.30 | 78.61 |
| 8/13/2013 11:47:50 AM | 0.79722 | 14.30 | 78.61 |
| 8/13/2013 11:47:51 AM | 0.79750 | 14.30 | 78.61 |
| 8/13/2013 11:47:52 AM | 0.79778 | 14.30 | 78.61 |
| 8/13/2013 11:47:53 AM | 0.79806 | 14.30 | 78.61 |
| 8/13/2013 11:47:54 AM | 0.79833 | 14.30 | 78.61 |
| 8/13/2013 11:47:55 AM | 0.79861 | 14.30 | 78.61 |
| 8/13/2013 11:47:56 AM | 0.79889 | 14.30 | 78.61 |
| 8/13/2013 11:47:57 AM | 0.79917 | 14.30 | 78.61 |
| 8/13/2013 11:47:58 AM | 0.79944 | 14.30 | 78.61 |
| 8/13/2013 11:47:59 AM | 0.79972 | 14.30 | 78.61 |
| 8/13/2013 11:48:00 AM | 0.80000 | 14.30 | 78.61 |
| 8/13/2013 11:48:01 AM | 0.80028 | 14.30 | 78.61 |
| 8/13/2013 11:48:02 AM | 0.80056 | 14.30 | 78.61 |
| 8/13/2013 11:48:03 AM | 0.80083 | 14.30 | 78.61 |
| 8/13/2013 11:48:04 AM | 0.80111 | 14.30 | 78.61 |
| 8/13/2013 11:48:05 AM | 0.80139 | 14.30 | 78.61 |
| 8/13/2013 11:48:06 AM | 0.80167 | 14.30 | 78.61 |
| 8/13/2013 11:48:07 AM | 0.80194 | 14.30 | 78.61 |
| 8/13/2013 11:48:08 AM | 0.80222 | 14.30 | 78.61 |
| 8/13/2013 11:48:09 AM | 0.80250 | 14.30 | 78.61 |
| 8/13/2013 11:48:10 AM | 0.80278 | 14.30 | 78.61 |
| 8/13/2013 11:48:11 AM | 0.80306 | 14.30 | 78.61 |
| 8/13/2013 11:48:12 AM | 0.80333 | 14.30 | 78.61 |
| 8/13/2013 11:48:13 AM | 0.80361 | 14.30 | 78.61 |
| 8/13/2013 11:48:14 AM | 0.80389 | 14.30 | 78.61 |
| 8/13/2013 11:48:15 AM | 0.80417 | 14.30 | 78.61 |
| 8/13/2013 11:48:16 AM | 0.80444 | 14.30 | 78.61 |
| 8/13/2013 11:48:17 AM | 0.80472 | 14.30 | 78.61 |
| 8/13/2013 11:48:18 AM | 0.80500 | 14.30 | 78.61 |
| 8/13/2013 11:48:19 AM | 0.80528 | 14.30 | 78.61 |
| 8/13/2013 11:48:20 AM | 0.80556 | 14.30 | 78.61 |
| 8/13/2013 11:48:21 AM | 0.80583 | 14.30 | 78.61 |
| 8/13/2013 11:48:22 AM | 0.80611 | 14.30 | 78.61 |
| 8/13/2013 11:48:23 AM | 0.80639 | 14.30 | 78.61 |
| 8/13/2013 11:48:24 AM | 0.80667 | 14.30 | 78.61 |
| 8/13/2013 11:48:25 AM | 0.80694 | 14.30 | 78.61 |
| 8/13/2013 11:48:26 AM | 0.80722 | 14.30 | 78.61 |
| 8/13/2013 11:48:27 AM | 0.80750 | 14.30 | 78.61 |
| 8/13/2013 11:48:28 AM | 0.80778 | 14.30 | 78.61 |
| 8/13/2013 11:48:29 AM | 0.80806 | 14.30 | 78.61 |
| 8/13/2013 11:48:30 AM | 0.80833 | 14.30 | 78.61 |
| 8/13/2013 11:48:31 AM | 0.80861 | 14.30 | 78.61 |
| 8/13/2013 11:48:32 AM | 0.80889 | 14.30 | 78.61 |
| 8/13/2013 11:48:33 AM | 0.80917 | 14.30 | 78.61 |
| 8/13/2013 11:48:34 AM | 0.80944 | 14.30 | 78.61 |
| 8/13/2013 11:48:35 AM | 0.80972 | 14.30 | 78.61 |
| 8/13/2013 11:48:36 AM | 0.81000 | 14.30 | 78.61 |
| 8/13/2013 11:48:37 AM | 0.81028 | 14.30 | 78.61 |
| 8/13/2013 11:48:38 AM | 0.81056 | 14.30 | 78.61 |
| 8/13/2013 11:48:39 AM | 0.81083 | 14.30 | 78.61 |
| 8/13/2013 11:48:40 AM | 0.81111 | 14.30 | 78.61 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:48:41 AM | 0.81139 | 14.30 | 78.62 |
| 8/13/2013 11:48:42 AM | 0.81167 | 14.30 | 78.62 |
| 8/13/2013 11:48:43 AM | 0.81194 | 14.30 | 78.62 |
| 8/13/2013 11:48:44 AM | 0.81222 | 14.30 | 78.62 |
| 8/13/2013 11:48:45 AM | 0.81250 | 14.30 | 78.62 |
| 8/13/2013 11:48:46 AM | 0.81278 | 14.30 | 78.62 |
| 8/13/2013 11:48:47 AM | 0.81306 | 14.30 | 78.62 |
| 8/13/2013 11:48:48 AM | 0.81333 | 14.30 | 78.62 |
| 8/13/2013 11:48:49 AM | 0.81361 | 14.30 | 78.62 |
| 8/13/2013 11:48:50 AM | 0.81389 | 14.30 | 78.62 |
| 8/13/2013 11:48:51 AM | 0.81417 | 14.30 | 78.62 |
| 8/13/2013 11:48:52 AM | 0.81444 | 14.30 | 78.62 |
| 8/13/2013 11:48:53 AM | 0.81472 | 14.30 | 78.62 |
| 8/13/2013 11:48:54 AM | 0.81500 | 14.30 | 78.62 |
| 8/13/2013 11:48:55 AM | 0.81528 | 14.30 | 78.63 |
| 8/13/2013 11:48:56 AM | 0.81556 | 14.30 | 78.63 |
| 8/13/2013 11:48:57 AM | 0.81583 | 14.30 | 78.63 |
| 8/13/2013 11:48:58 AM | 0.81611 | 14.30 | 78.63 |
| 8/13/2013 11:48:59 AM | 0.81639 | 14.30 | 78.63 |
| 8/13/2013 11:49:00 AM | 0.81667 | 14.30 | 78.63 |
| 8/13/2013 11:49:01 AM | 0.81694 | 14.30 | 78.63 |
| 8/13/2013 11:49:02 AM | 0.81722 | 14.30 | 78.63 |
| 8/13/2013 11:49:03 AM | 0.81750 | 14.30 | 78.63 |
| 8/13/2013 11:49:04 AM | 0.81778 | 14.30 | 78.63 |
| 8/13/2013 11:49:05 AM | 0.81806 | 14.30 | 78.64 |
| 8/13/2013 11:49:06 AM | 0.81833 | 14.30 | 78.64 |
| 8/13/2013 11:49:07 AM | 0.81861 | 14.30 | 78.64 |
| 8/13/2013 11:49:08 AM | 0.81889 | 14.30 | 78.64 |
| 8/13/2013 11:49:09 AM | 0.81917 | 14.30 | 78.64 |
| 8/13/2013 11:49:10 AM | 0.81944 | 14.30 | 78.64 |
| 8/13/2013 11:49:11 AM | 0.81972 | 14.30 | 78.64 |
| 8/13/2013 11:49:12 AM | 0.82000 | 14.30 | 78.64 |
| 8/13/2013 11:49:13 AM | 0.82028 | 14.30 | 78.64 |
| 8/13/2013 11:49:14 AM | 0.82056 | 14.30 | 78.64 |
| 8/13/2013 11:49:15 AM | 0.82083 | 14.30 | 78.64 |
| 8/13/2013 11:49:16 AM | 0.82111 | 14.30 | 78.64 |
| 8/13/2013 11:49:17 AM | 0.82139 | 14.30 | 78.64 |
| 8/13/2013 11:49:18 AM | 0.82167 | 14.30 | 78.65 |
| 8/13/2013 11:49:19 AM | 0.82194 | 14.30 | 78.65 |
| 8/13/2013 11:49:20 AM | 0.82222 | 14.30 | 78.65 |
| 8/13/2013 11:49:21 AM | 0.82250 | 14.30 | 78.65 |
| 8/13/2013 11:49:22 AM | 0.82278 | 14.30 | 78.65 |
| 8/13/2013 11:49:23 AM | 0.82306 | 14.30 | 78.65 |
| 8/13/2013 11:49:24 AM | 0.82333 | 14.30 | 78.65 |
| 8/13/2013 11:49:25 AM | 0.82361 | 14.30 | 78.65 |
| 8/13/2013 11:49:26 AM | 0.82389 | 14.30 | 78.65 |
| 8/13/2013 11:49:27 AM | 0.82417 | 14.30 | 78.66 |
| 8/13/2013 11:49:28 AM | 0.82444 | 14.30 | 78.66 |
| 8/13/2013 11:49:29 AM | 0.82472 | 14.30 | 78.66 |
| 8/13/2013 11:49:30 AM | 0.82500 | 14.30 | 78.66 |
| 8/13/2013 11:49:31 AM | 0.82528 | 14.30 | 78.66 |
| 8/13/2013 11:49:32 AM | 0.82556 | 14.30 | 78.66 |
| 8/13/2013 11:49:33 AM | 0.82583 | 14.30 | 78.66 |
| 8/13/2013 11:49:34 AM | 0.82611 | 14.30 | 78.66 |
| 8/13/2013 11:49:35 AM | 0.82639 | 14.30 | 78.66 |
| 8/13/2013 11:49:36 AM | 0.82667 | 14.30 | 78.66 |
| 8/13/2013 11:49:37 AM | 0.82694 | 14.30 | 78.67 |
| 8/13/2013 11:49:38 AM | 0.82722 | 14.30 | 78.67 |
| 8/13/2013 11:49:39 AM | 0.82750 | 14.30 | 78.67 |
| 8/13/2013 11:49:40 AM | 0.82778 | 14.30 | 78.67 |
| 8/13/2013 11:49:41 AM | 0.82806 | 14.30 | 78.67 |
| 8/13/2013 11:49:42 AM | 0.82833 | 14.30 | 78.67 |
| 8/13/2013 11:49:43 AM | 0.82861 | 14.30 | 78.67 |
| 8/13/2013 11:49:44 AM | 0.82889 | 14.30 | 78.67 |
| 8/13/2013 11:49:45 AM | 0.82917 | 14.30 | 78.68 |
| 8/13/2013 11:49:46 AM | 0.82944 | 14.30 | 78.68 |
| 8/13/2013 11:49:47 AM | 0.82972 | 14.30 | 78.68 |
| 8/13/2013 11:49:48 AM | 0.83000 | 14.30 | 78.68 |
| 8/13/2013 11:49:49 AM | 0.83028 | 14.30 | 78.68 |
| 8/13/2013 11:49:50 AM | 0.83056 | 14.30 | 78.69 |
| 8/13/2013 11:49:51 AM | 0.83083 | 14.30 | 78.69 |
| 8/13/2013 11:49:52 AM | 0.83111 | 14.30 | 78.69 |
| 8/13/2013 11:49:53 AM | 0.83139 | 14.30 | 78.69 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:49:54 AM | 0.83167 | 14.30 | 78.69 |
| 8/13/2013 11:49:55 AM | 0.83194 | 14.30 | 78.69 |
| 8/13/2013 11:49:56 AM | 0.83222 | 14.30 | 78.70 |
| 8/13/2013 11:49:57 AM | 0.83250 | 14.30 | 78.70 |
| 8/13/2013 11:49:58 AM | 0.83278 | 14.30 | 78.70 |
| 8/13/2013 11:49:59 AM | 0.83306 | 14.30 | 78.70 |
| 8/13/2013 11:50:00 AM | 0.83333 | 14.30 | 78.71 |
| 8/13/2013 11:50:01 AM | 0.83361 | 14.30 | 78.71 |
| 8/13/2013 11:50:02 AM | 0.83389 | 14.30 | 78.71 |
| 8/13/2013 11:50:03 AM | 0.83417 | 14.30 | 78.72 |
| 8/13/2013 11:50:04 AM | 0.83444 | 14.30 | 78.72 |
| 8/13/2013 11:50:05 AM | 0.83472 | 14.30 | 78.72 |
| 8/13/2013 11:50:06 AM | 0.83500 | 14.30 | 78.73 |
| 8/13/2013 11:50:07 AM | 0.83528 | 14.30 | 78.73 |
| 8/13/2013 11:50:08 AM | 0.83556 | 14.30 | 78.74 |
| 8/13/2013 11:50:09 AM | 0.83583 | 14.30 | 78.74 |
| 8/13/2013 11:50:10 AM | 0.83611 | 14.30 | 78.75 |
| 8/13/2013 11:50:11 AM | 0.83639 | 14.30 | 78.75 |
| 8/13/2013 11:50:12 AM | 0.83667 | 14.30 | 78.76 |
| 8/13/2013 11:50:13 AM | 0.83694 | 14.30 | 78.76 |
| 8/13/2013 11:50:14 AM | 0.83722 | 14.30 | 78.77 |
| 8/13/2013 11:50:15 AM | 0.83750 | 14.30 | 78.78 |
| 8/13/2013 11:50:16 AM | 0.83778 | 14.30 | 78.78 |
| 8/13/2013 11:50:17 AM | 0.83806 | 14.30 | 78.79 |
| 8/13/2013 11:50:18 AM | 0.83833 | 14.30 | 78.79 |
| 8/13/2013 11:50:19 AM | 0.83861 | 14.30 | 78.80 |
| 8/13/2013 11:50:20 AM | 0.83889 | 14.30 | 78.81 |
| 8/13/2013 11:50:21 AM | 0.83917 | 14.30 | 78.81 |
| 8/13/2013 11:50:22 AM | 0.83944 | 14.30 | 78.82 |
| 8/13/2013 11:50:23 AM | 0.83972 | 14.30 | 78.83 |
| 8/13/2013 11:50:24 AM | 0.84000 | 14.30 | 78.84 |
| 8/13/2013 11:50:25 AM | 0.84028 | 14.30 | 78.84 |
| 8/13/2013 11:50:26 AM | 0.84056 | 14.30 | 78.85 |
| 8/13/2013 11:50:27 AM | 0.84083 | 14.30 | 78.86 |
| 8/13/2013 11:50:28 AM | 0.84111 | 14.30 | 78.87 |
| 8/13/2013 11:50:29 AM | 0.84139 | 14.30 | 78.87 |
| 8/13/2013 11:50:30 AM | 0.84167 | 14.30 | 78.88 |
| 8/13/2013 11:50:31 AM | 0.84194 | 14.30 | 78.89 |
| 8/13/2013 11:50:32 AM | 0.84222 | 14.30 | 78.90 |
| 8/13/2013 11:50:33 AM | 0.84250 | 14.30 | 78.90 |
| 8/13/2013 11:50:34 AM | 0.84278 | 14.30 | 78.91 |
| 8/13/2013 11:50:35 AM | 0.84306 | 14.30 | 78.92 |
| 8/13/2013 11:50:36 AM | 0.84333 | 14.30 | 78.92 |
| 8/13/2013 11:50:37 AM | 0.84361 | 14.30 | 78.93 |
| 8/13/2013 11:50:38 AM | 0.84389 | 14.30 | 78.94 |
| 8/13/2013 11:50:39 AM | 0.84417 | 14.30 | 78.95 |
| 8/13/2013 11:50:40 AM | 0.84444 | 14.30 | 78.95 |
| 8/13/2013 11:50:41 AM | 0.84472 | 14.30 | 78.96 |
| 8/13/2013 11:50:42 AM | 0.84500 | 14.30 | 78.97 |
| 8/13/2013 11:50:43 AM | 0.84528 | 14.30 | 78.98 |
| 8/13/2013 11:50:44 AM | 0.84556 | 14.30 | 78.98 |
| 8/13/2013 11:50:45 AM | 0.84583 | 14.30 | 78.99 |
| 8/13/2013 11:50:46 AM | 0.84611 | 14.30 | 79.00 |
| 8/13/2013 11:50:47 AM | 0.84639 | 14.30 | 79.00 |
| 8/13/2013 11:50:48 AM | 0.84667 | 14.30 | 79.01 |
| 8/13/2013 11:50:49 AM | 0.84694 | 14.30 | 79.02 |
| 8/13/2013 11:50:50 AM | 0.84722 | 14.30 | 79.03 |
| 8/13/2013 11:50:51 AM | 0.84750 | 14.30 | 79.03 |
| 8/13/2013 11:50:52 AM | 0.84778 | 14.30 | 79.04 |
| 8/13/2013 11:50:53 AM | 0.84806 | 14.30 | 79.05 |
| 8/13/2013 11:50:54 AM | 0.84833 | 14.30 | 79.05 |
| 8/13/2013 11:50:55 AM | 0.84861 | 14.30 | 79.06 |
| 8/13/2013 11:50:56 AM | 0.84889 | 14.30 | 79.06 |
| 8/13/2013 11:50:57 AM | 0.84917 | 14.30 | 79.07 |
| 8/13/2013 11:50:58 AM | 0.84944 | 14.30 | 79.08 |
| 8/13/2013 11:50:59 AM | 0.84972 | 14.30 | 79.08 |
| 8/13/2013 11:51:00 AM | 0.85000 | 14.30 | 79.09 |
| 8/13/2013 11:51:01 AM | 0.85028 | 14.30 | 79.09 |
| 8/13/2013 11:51:02 AM | 0.85056 | 14.30 | 79.10 |
| 8/13/2013 11:51:03 AM | 0.85083 | 14.30 | 79.11 |
| 8/13/2013 11:51:04 AM | 0.85111 | 14.30 | 79.11 |
| 8/13/2013 11:51:05 AM | 0.85139 | 14.30 | 79.11 |
| 8/13/2013 11:51:06 AM | 0.85167 | 14.30 | 79.12 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:51:07 AM | 0.85194 | 14.30 | 79.13 |
| 8/13/2013 11:51:08 AM | 0.85222 | 14.30 | 79.13 |
| 8/13/2013 11:51:09 AM | 0.85250 | 14.30 | 79.13 |
| 8/13/2013 11:51:10 AM | 0.85278 | 14.30 | 79.14 |
| 8/13/2013 11:51:11 AM | 0.85306 | 14.30 | 79.14 |
| 8/13/2013 11:51:12 AM | 0.85333 | 14.30 | 79.15 |
| 8/13/2013 11:51:13 AM | 0.85361 | 14.30 | 79.15 |
| 8/13/2013 11:51:14 AM | 0.85389 | 14.30 | 79.16 |
| 8/13/2013 11:51:15 AM | 0.85417 | 14.30 | 79.16 |
| 8/13/2013 11:51:16 AM | 0.85444 | 14.30 | 79.16 |
| 8/13/2013 11:51:17 AM | 0.85472 | 14.30 | 79.17 |
| 8/13/2013 11:51:18 AM | 0.85500 | 14.30 | 79.17 |
| 8/13/2013 11:51:19 AM | 0.85528 | 14.30 | 79.17 |
| 8/13/2013 11:51:20 AM | 0.85556 | 14.30 | 79.17 |
| 8/13/2013 11:51:21 AM | 0.85583 | 14.30 | 79.18 |
| 8/13/2013 11:51:22 AM | 0.85611 | 14.30 | 79.18 |
| 8/13/2013 11:51:23 AM | 0.85639 | 14.30 | 79.19 |
| 8/13/2013 11:51:24 AM | 0.85667 | 14.30 | 79.19 |
| 8/13/2013 11:51:25 AM | 0.85694 | 14.30 | 79.19 |
| 8/13/2013 11:51:26 AM | 0.85722 | 14.30 | 79.19 |
| 8/13/2013 11:51:27 AM | 0.85750 | 14.30 | 79.20 |
| 8/13/2013 11:51:28 AM | 0.85778 | 14.30 | 79.20 |
| 8/13/2013 11:51:29 AM | 0.85806 | 14.30 | 79.20 |
| 8/13/2013 11:51:30 AM | 0.85833 | 14.30 | 79.20 |
| 8/13/2013 11:51:31 AM | 0.85861 | 14.30 | 79.21 |
| 8/13/2013 11:51:32 AM | 0.85889 | 14.30 | 79.21 |
| 8/13/2013 11:51:33 AM | 0.85917 | 14.30 | 79.21 |
| 8/13/2013 11:51:34 AM | 0.85944 | 14.30 | 79.22 |
| 8/13/2013 11:51:35 AM | 0.85972 | 14.30 | 79.22 |
| 8/13/2013 11:51:36 AM | 0.86000 | 14.30 | 79.22 |
| 8/13/2013 11:51:37 AM | 0.86028 | 14.30 | 79.22 |
| 8/13/2013 11:51:38 AM | 0.86056 | 14.30 | 79.22 |
| 8/13/2013 11:51:39 AM | 0.86083 | 14.30 | 79.23 |
| 8/13/2013 11:51:40 AM | 0.86111 | 14.30 | 79.23 |
| 8/13/2013 11:51:41 AM | 0.86139 | 14.30 | 79.23 |
| 8/13/2013 11:51:42 AM | 0.86167 | 14.30 | 79.23 |
| 8/13/2013 11:51:43 AM | 0.86194 | 14.30 | 79.23 |
| 8/13/2013 11:51:44 AM | 0.86222 | 14.30 | 79.24 |
| 8/13/2013 11:51:45 AM | 0.86250 | 14.30 | 79.24 |
| 8/13/2013 11:51:46 AM | 0.86278 | 14.30 | 79.24 |
| 8/13/2013 11:51:47 AM | 0.86306 | 14.30 | 79.24 |
| 8/13/2013 11:51:48 AM | 0.86333 | 14.30 | 79.25 |
| 8/13/2013 11:51:49 AM | 0.86361 | 14.30 | 79.25 |
| 8/13/2013 11:51:50 AM | 0.86389 | 14.30 | 79.25 |
| 8/13/2013 11:51:51 AM | 0.86417 | 14.30 | 79.25 |
| 8/13/2013 11:51:52 AM | 0.86444 | 14.30 | 79.25 |
| 8/13/2013 11:51:53 AM | 0.86472 | 14.30 | 79.26 |
| 8/13/2013 11:51:54 AM | 0.86500 | 14.30 | 79.26 |
| 8/13/2013 11:51:55 AM | 0.86528 | 14.30 | 79.26 |
| 8/13/2013 11:51:56 AM | 0.86556 | 14.30 | 79.26 |
| 8/13/2013 11:51:57 AM | 0.86583 | 14.30 | 79.27 |
| 8/13/2013 11:51:58 AM | 0.86611 | 14.30 | 79.27 |
| 8/13/2013 11:51:59 AM | 0.86639 | 14.30 | 79.27 |
| 8/13/2013 11:52:00 AM | 0.86667 | 14.30 | 79.27 |
| 8/13/2013 11:52:01 AM | 0.86694 | 14.30 | 79.27 |
| 8/13/2013 11:52:02 AM | 0.86722 | 14.30 | 79.28 |
| 8/13/2013 11:52:03 AM | 0.86750 | 14.30 | 79.28 |
| 8/13/2013 11:52:04 AM | 0.86778 | 14.30 | 79.28 |
| 8/13/2013 11:52:05 AM | 0.86806 | 14.30 | 79.28 |
| 8/13/2013 11:52:06 AM | 0.86833 | 14.30 | 79.28 |
| 8/13/2013 11:52:07 AM | 0.86861 | 14.30 | 79.28 |
| 8/13/2013 11:52:08 AM | 0.86889 | 14.30 | 79.29 |
| 8/13/2013 11:52:09 AM | 0.86917 | 14.30 | 79.29 |
| 8/13/2013 11:52:10 AM | 0.86944 | 14.30 | 79.29 |
| 8/13/2013 11:52:11 AM | 0.86972 | 14.30 | 79.29 |
| 8/13/2013 11:52:12 AM | 0.87000 | 14.30 | 79.29 |
| 8/13/2013 11:52:13 AM | 0.87028 | 14.30 | 79.30 |
| 8/13/2013 11:52:14 AM | 0.87056 | 14.30 | 79.30 |
| 8/13/2013 11:52:15 AM | 0.87083 | 14.30 | 79.30 |
| 8/13/2013 11:52:16 AM | 0.87111 | 14.30 | 79.30 |
| 8/13/2013 11:52:17 AM | 0.87139 | 14.30 | 79.30 |
| 8/13/2013 11:52:18 AM | 0.87167 | 14.30 | 79.31 |
| 8/13/2013 11:52:19 AM | 0.87194 | 14.30 | 79.31 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:52:20 AM | 0.87222 | 14.30 | 79.31 |
| 8/13/2013 11:52:21 AM | 0.87250 | 14.30 | 79.31 |
| 8/13/2013 11:52:22 AM | 0.87278 | 14.30 | 79.31 |
| 8/13/2013 11:52:23 AM | 0.87306 | 14.30 | 79.31 |
| 8/13/2013 11:52:24 AM | 0.87333 | 14.30 | 79.32 |
| 8/13/2013 11:52:25 AM | 0.87361 | 14.30 | 79.32 |
| 8/13/2013 11:52:26 AM | 0.87389 | 14.30 | 79.32 |
| 8/13/2013 11:52:27 AM | 0.87417 | 14.30 | 79.32 |
| 8/13/2013 11:52:28 AM | 0.87444 | 14.30 | 79.32 |
| 8/13/2013 11:52:29 AM | 0.87472 | 14.30 | 79.33 |
| 8/13/2013 11:52:30 AM | 0.87500 | 14.30 | 79.33 |
| 8/13/2013 11:52:31 AM | 0.87528 | 14.30 | 79.33 |
| 8/13/2013 11:52:32 AM | 0.87556 | 14.30 | 79.33 |
| 8/13/2013 11:52:33 AM | 0.87583 | 14.30 | 79.33 |
| 8/13/2013 11:52:34 AM | 0.87611 | 14.30 | 79.34 |
| 8/13/2013 11:52:35 AM | 0.87639 | 14.30 | 79.34 |
| 8/13/2013 11:52:36 AM | 0.87667 | 14.30 | 79.34 |
| 8/13/2013 11:52:37 AM | 0.87694 | 14.30 | 79.34 |
| 8/13/2013 11:52:38 AM | 0.87722 | 14.30 | 79.34 |
| 8/13/2013 11:52:39 AM | 0.87750 | 14.30 | 79.34 |
| 8/13/2013 11:52:40 AM | 0.87778 | 14.30 | 79.35 |
| 8/13/2013 11:52:41 AM | 0.87806 | 14.30 | 79.35 |
| 8/13/2013 11:52:42 AM | 0.87833 | 14.30 | 79.35 |
| 8/13/2013 11:52:43 AM | 0.87861 | 14.30 | 79.35 |
| 8/13/2013 11:52:44 AM | 0.87889 | 14.30 | 79.36 |
| 8/13/2013 11:52:45 AM | 0.87917 | 14.30 | 79.36 |
| 8/13/2013 11:52:46 AM | 0.87944 | 14.30 | 79.36 |
| 8/13/2013 11:52:47 AM | 0.87972 | 14.30 | 79.36 |
| 8/13/2013 11:52:48 AM | 0.88000 | 14.30 | 79.36 |
| 8/13/2013 11:52:49 AM | 0.88028 | 14.30 | 79.37 |
| 8/13/2013 11:52:50 AM | 0.88056 | 14.30 | 79.37 |
| 8/13/2013 11:52:51 AM | 0.88083 | 14.30 | 79.37 |
| 8/13/2013 11:52:52 AM | 0.88111 | 14.30 | 79.37 |
| 8/13/2013 11:52:53 AM | 0.88139 | 14.30 | 79.37 |
| 8/13/2013 11:52:54 AM | 0.88167 | 14.30 | 79.38 |
| 8/13/2013 11:52:55 AM | 0.88194 | 14.30 | 79.38 |
| 8/13/2013 11:52:56 AM | 0.88222 | 14.30 | 79.38 |
| 8/13/2013 11:52:57 AM | 0.88250 | 14.30 | 79.38 |
| 8/13/2013 11:52:58 AM | 0.88278 | 14.30 | 79.38 |
| 8/13/2013 11:52:59 AM | 0.88306 | 14.30 | 79.39 |
| 8/13/2013 11:53:00 AM | 0.88333 | 14.30 | 79.39 |
| 8/13/2013 11:53:01 AM | 0.88361 | 14.30 | 79.39 |
| 8/13/2013 11:53:02 AM | 0.88389 | 14.30 | 79.39 |
| 8/13/2013 11:53:03 AM | 0.88417 | 14.30 | 79.39 |
| 8/13/2013 11:53:04 AM | 0.88444 | 14.30 | 79.40 |
| 8/13/2013 11:53:05 AM | 0.88472 | 14.30 | 79.40 |
| 8/13/2013 11:53:06 AM | 0.88500 | 14.30 | 79.40 |
| 8/13/2013 11:53:07 AM | 0.88528 | 14.30 | 79.40 |
| 8/13/2013 11:53:08 AM | 0.88556 | 14.30 | 79.41 |
| 8/13/2013 11:53:09 AM | 0.88583 | 14.30 | 79.41 |
| 8/13/2013 11:53:10 AM | 0.88611 | 14.30 | 79.41 |
| 8/13/2013 11:53:11 AM | 0.88639 | 14.30 | 79.41 |
| 8/13/2013 11:53:12 AM | 0.88667 | 14.30 | 79.41 |
| 8/13/2013 11:53:13 AM | 0.88694 | 14.30 | 79.42 |
| 8/13/2013 11:53:14 AM | 0.88722 | 14.30 | 79.42 |
| 8/13/2013 11:53:15 AM | 0.88750 | 14.30 | 79.42 |
| 8/13/2013 11:53:16 AM | 0.88778 | 14.30 | 79.42 |
| 8/13/2013 11:53:17 AM | 0.88806 | 14.30 | 79.43 |
| 8/13/2013 11:53:18 AM | 0.88833 | 14.30 | 79.43 |
| 8/13/2013 11:53:19 AM | 0.88861 | 14.30 | 79.43 |
| 8/13/2013 11:53:20 AM | 0.88889 | 14.30 | 79.43 |
| 8/13/2013 11:53:21 AM | 0.88917 | 14.30 | 79.44 |
| 8/13/2013 11:53:22 AM | 0.88944 | 14.30 | 79.44 |
| 8/13/2013 11:53:23 AM | 0.88972 | 14.30 | 79.44 |
| 8/13/2013 11:53:24 AM | 0.89000 | 14.30 | 79.44 |
| 8/13/2013 11:53:25 AM | 0.89028 | 14.30 | 79.44 |
| 8/13/2013 11:53:26 AM | 0.89056 | 14.30 | 79.45 |
| 8/13/2013 11:53:27 AM | 0.89083 | 14.30 | 79.45 |
| 8/13/2013 11:53:28 AM | 0.89111 | 14.30 | 79.45 |
| 8/13/2013 11:53:29 AM | 0.89139 | 14.30 | 79.45 |
| 8/13/2013 11:53:30 AM | 0.89167 | 14.30 | 79.46 |
| 8/13/2013 11:53:31 AM | 0.89194 | 14.30 | 79.46 |
| 8/13/2013 11:53:32 AM | 0.89222 | 14.30 | 79.46 |

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| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:53:33 AM | 0.89250 | 14.30 | 79.46 |
| 8/13/2013 11:53:34 AM | 0.89278 | 14.30 | 79.46 |
| 8/13/2013 11:53:35 AM | 0.89306 | 14.30 | 79.47 |
| 8/13/2013 11:53:36 AM | 0.89333 | 14.30 | 79.47 |
| 8/13/2013 11:53:37 AM | 0.89361 | 14.30 | 79.47 |
| 8/13/2013 11:53:38 AM | 0.89389 | 14.30 | 79.47 |
| 8/13/2013 11:53:39 AM | 0.89417 | 14.30 | 79.47 |
| 8/13/2013 11:53:40 AM | 0.89444 | 14.30 | 79.48 |
| 8/13/2013 11:53:41 AM | 0.89472 | 14.30 | 79.48 |
| 8/13/2013 11:53:42 AM | 0.89500 | 14.30 | 79.48 |
| 8/13/2013 11:53:43 AM | 0.89528 | 14.30 | 79.48 |
| 8/13/2013 11:53:44 AM | 0.89556 | 14.30 | 79.49 |
| 8/13/2013 11:53:45 AM | 0.89583 | 14.30 | 79.49 |
| 8/13/2013 11:53:46 AM | 0.89611 | 14.30 | 79.49 |
| 8/13/2013 11:53:47 AM | 0.89639 | 14.30 | 79.49 |
| 8/13/2013 11:53:48 AM | 0.89667 | 14.30 | 79.50 |
| 8/13/2013 11:53:49 AM | 0.89694 | 14.30 | 79.50 |
| 8/13/2013 11:53:50 AM | 0.89722 | 14.30 | 79.50 |
| 8/13/2013 11:53:51 AM | 0.89750 | 14.30 | 79.50 |
| 8/13/2013 11:53:52 AM | 0.89778 | 14.30 | 79.50 |
| 8/13/2013 11:53:53 AM | 0.89806 | 14.30 | 79.51 |
| 8/13/2013 11:53:54 AM | 0.89833 | 14.30 | 79.51 |
| 8/13/2013 11:53:55 AM | 0.89861 | 14.30 | 79.51 |
| 8/13/2013 11:53:56 AM | 0.89889 | 14.30 | 79.51 |
| 8/13/2013 11:53:57 AM | 0.89917 | 14.30 | 79.52 |
| 8/13/2013 11:53:58 AM | 0.89944 | 14.30 | 79.52 |
| 8/13/2013 11:53:59 AM | 0.89972 | 14.30 | 79.52 |
| 8/13/2013 11:54:00 AM | 0.90000 | 14.30 | 79.52 |
| 8/13/2013 11:54:01 AM | 0.90028 | 14.30 | 79.53 |
| 8/13/2013 11:54:02 AM | 0.90056 | 14.30 | 79.53 |
| 8/13/2013 11:54:03 AM | 0.90083 | 14.30 | 79.53 |
| 8/13/2013 11:54:04 AM | 0.90111 | 14.30 | 79.53 |
| 8/13/2013 11:54:05 AM | 0.90139 | 14.30 | 79.53 |
| 8/13/2013 11:54:06 AM | 0.90167 | 14.30 | 79.54 |
| 8/13/2013 11:54:07 AM | 0.90194 | 14.30 | 79.54 |
| 8/13/2013 11:54:08 AM | 0.90222 | 14.30 | 79.54 |
| 8/13/2013 11:54:09 AM | 0.90250 | 14.30 | 79.54 |
| 8/13/2013 11:54:10 AM | 0.90278 | 14.30 | 79.55 |
| 8/13/2013 11:54:11 AM | 0.90306 | 14.30 | 79.55 |
| 8/13/2013 11:54:12 AM | 0.90333 | 14.30 | 79.55 |
| 8/13/2013 11:54:13 AM | 0.90361 | 14.30 | 79.55 |
| 8/13/2013 11:54:14 AM | 0.90389 | 14.30 | 79.55 |
| 8/13/2013 11:54:15 AM | 0.90417 | 14.30 | 79.56 |
| 8/13/2013 11:54:16 AM | 0.90444 | 14.30 | 79.56 |
| 8/13/2013 11:54:17 AM | 0.90472 | 14.30 | 79.56 |
| 8/13/2013 11:54:18 AM | 0.90500 | 14.30 | 79.56 |
| 8/13/2013 11:54:19 AM | 0.90528 | 14.30 | 79.56 |
| 8/13/2013 11:54:20 AM | 0.90556 | 14.30 | 79.57 |
| 8/13/2013 11:54:21 AM | 0.90583 | 14.30 | 79.57 |
| 8/13/2013 11:54:22 AM | 0.90611 | 14.30 | 79.57 |
| 8/13/2013 11:54:23 AM | 0.90639 | 14.30 | 79.57 |
| 8/13/2013 11:54:24 AM | 0.90667 | 14.30 | 79.58 |
| 8/13/2013 11:54:25 AM | 0.90694 | 14.30 | 79.58 |
| 8/13/2013 11:54:26 AM | 0.90722 | 14.30 | 79.58 |
| 8/13/2013 11:54:27 AM | 0.90750 | 14.30 | 79.58 |
| 8/13/2013 11:54:28 AM | 0.90778 | 14.30 | 79.58 |
| 8/13/2013 11:54:29 AM | 0.90806 | 14.30 | 79.59 |
| 8/13/2013 11:54:30 AM | 0.90833 | 14.30 | 79.59 |
| 8/13/2013 11:54:31 AM | 0.90861 | 14.30 | 79.59 |
| 8/13/2013 11:54:32 AM | 0.90889 | 14.30 | 79.59 |
| 8/13/2013 11:54:33 AM | 0.90917 | 14.30 | 79.60 |
| 8/13/2013 11:54:34 AM | 0.90944 | 14.30 | 79.60 |
| 8/13/2013 11:54:35 AM | 0.90972 | 14.30 | 79.60 |
| 8/13/2013 11:54:36 AM | 0.91000 | 14.30 | 79.60 |
| 8/13/2013 11:54:37 AM | 0.91028 | 14.30 | 79.61 |
| 8/13/2013 11:54:38 AM | 0.91056 | 14.30 | 79.61 |
| 8/13/2013 11:54:39 AM | 0.91083 | 14.30 | 79.61 |
| 8/13/2013 11:54:40 AM | 0.91111 | 14.30 | 79.61 |
| 8/13/2013 11:54:41 AM | 0.91139 | 14.30 | 79.61 |
| 8/13/2013 11:54:42 AM | 0.91167 | 14.30 | 79.62 |
| 8/13/2013 11:54:43 AM | 0.91194 | 14.30 | 79.62 |
| 8/13/2013 11:54:44 AM | 0.91222 | 14.30 | 79.62 |
| 8/13/2013 11:54:45 AM | 0.91250 | 14.30 | 79.62 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:54:46 AM | 0.91278 | 14.30 | 79.63 |
| 8/13/2013 11:54:47 AM | 0.91306 | 14.30 | 79.63 |
| 8/13/2013 11:54:48 AM | 0.91333 | 14.30 | 79.63 |
| 8/13/2013 11:54:49 AM | 0.91361 | 14.30 | 79.63 |
| 8/13/2013 11:54:50 AM | 0.91389 | 14.30 | 79.63 |
| 8/13/2013 11:54:51 AM | 0.91417 | 14.30 | 79.64 |
| 8/13/2013 11:54:52 AM | 0.91444 | 14.30 | 79.64 |
| 8/13/2013 11:54:53 AM | 0.91472 | 14.30 | 79.64 |
| 8/13/2013 11:54:54 AM | 0.91500 | 14.30 | 79.64 |
| 8/13/2013 11:54:55 AM | 0.91528 | 14.30 | 79.64 |
| 8/13/2013 11:54:56 AM | 0.91556 | 14.30 | 79.65 |
| 8/13/2013 11:54:57 AM | 0.91583 | 14.30 | 79.65 |
| 8/13/2013 11:54:58 AM | 0.91611 | 14.30 | 79.65 |
| 8/13/2013 11:54:59 AM | 0.91639 | 14.30 | 79.65 |
| 8/13/2013 11:55:00 AM | 0.91667 | 14.30 | 79.65 |
| 8/13/2013 11:55:01 AM | 0.91694 | 14.30 | 79.66 |
| 8/13/2013 11:55:02 AM | 0.91722 | 14.30 | 79.66 |
| 8/13/2013 11:55:03 AM | 0.91750 | 14.30 | 79.66 |
| 8/13/2013 11:55:04 AM | 0.91778 | 14.30 | 79.66 |
| 8/13/2013 11:55:05 AM | 0.91806 | 14.30 | 79.66 |
| 8/13/2013 11:55:06 AM | 0.91833 | 14.30 | 79.67 |
| 8/13/2013 11:55:07 AM | 0.91861 | 14.30 | 79.67 |
| 8/13/2013 11:55:08 AM | 0.91889 | 14.30 | 79.67 |
| 8/13/2013 11:55:09 AM | 0.91917 | 14.30 | 79.67 |
| 8/13/2013 11:55:10 AM | 0.91944 | 14.30 | 79.67 |
| 8/13/2013 11:55:11 AM | 0.91972 | 14.30 | 79.68 |
| 8/13/2013 11:55:12 AM | 0.92000 | 14.30 | 79.68 |
| 8/13/2013 11:55:13 AM | 0.92028 | 14.30 | 79.68 |
| 8/13/2013 11:55:14 AM | 0.92056 | 14.30 | 79.68 |
| 8/13/2013 11:55:15 AM | 0.92083 | 14.30 | 79.69 |
| 8/13/2013 11:55:16 AM | 0.92111 | 14.30 | 79.69 |
| 8/13/2013 11:55:17 AM | 0.92139 | 14.30 | 79.69 |
| 8/13/2013 11:55:18 AM | 0.92167 | 14.30 | 79.69 |
| 8/13/2013 11:55:19 AM | 0.92194 | 14.30 | 79.69 |
| 8/13/2013 11:55:20 AM | 0.92222 | 14.30 | 79.69 |
| 8/13/2013 11:55:21 AM | 0.92250 | 14.30 | 79.70 |
| 8/13/2013 11:55:22 AM | 0.92278 | 14.30 | 79.70 |
| 8/13/2013 11:55:23 AM | 0.92306 | 14.30 | 79.70 |
| 8/13/2013 11:55:24 AM | 0.92333 | 14.30 | 79.70 |
| 8/13/2013 11:55:25 AM | 0.92361 | 14.30 | 79.70 |
| 8/13/2013 11:55:26 AM | 0.92389 | 14.30 | 79.71 |
| 8/13/2013 11:55:27 AM | 0.92417 | 14.30 | 79.71 |
| 8/13/2013 11:55:28 AM | 0.92444 | 14.30 | 79.71 |
| 8/13/2013 11:55:29 AM | 0.92472 | 14.30 | 79.71 |
| 8/13/2013 11:55:30 AM | 0.92500 | 14.30 | 79.72 |
| 8/13/2013 11:55:31 AM | 0.92528 | 14.30 | 79.72 |
| 8/13/2013 11:55:32 AM | 0.92556 | 14.30 | 79.72 |
| 8/13/2013 11:55:33 AM | 0.92583 | 14.30 | 79.72 |
| 8/13/2013 11:55:34 AM | 0.92611 | 14.30 | 79.72 |
| 8/13/2013 11:55:35 AM | 0.92639 | 14.30 | 79.73 |
| 8/13/2013 11:55:36 AM | 0.92667 | 14.30 | 79.73 |
| 8/13/2013 11:55:37 AM | 0.92694 | 14.30 | 79.73 |
| 8/13/2013 11:55:38 AM | 0.92722 | 14.30 | 79.73 |
| 8/13/2013 11:55:39 AM | 0.92750 | 14.30 | 79.73 |
| 8/13/2013 11:55:40 AM | 0.92778 | 14.30 | 79.73 |
| 8/13/2013 11:55:41 AM | 0.92806 | 14.30 | 79.74 |
| 8/13/2013 11:55:42 AM | 0.92833 | 14.30 | 79.74 |
| 8/13/2013 11:55:43 AM | 0.92861 | 14.30 | 79.74 |
| 8/13/2013 11:55:44 AM | 0.92889 | 14.30 | 79.74 |
| 8/13/2013 11:55:45 AM | 0.92917 | 14.30 | 79.75 |
| 8/13/2013 11:55:46 AM | 0.92944 | 14.30 | 79.75 |
| 8/13/2013 11:55:47 AM | 0.92972 | 14.30 | 79.75 |
| 8/13/2013 11:55:48 AM | 0.93000 | 14.30 | 79.75 |
| 8/13/2013 11:55:49 AM | 0.93028 | 14.30 | 79.75 |
| 8/13/2013 11:55:50 AM | 0.93056 | 14.30 | 79.76 |
| 8/13/2013 11:55:51 AM | 0.93083 | 14.30 | 79.76 |
| 8/13/2013 11:55:52 AM | 0.93111 | 14.30 | 79.76 |
| 8/13/2013 11:55:53 AM | 0.93139 | 14.30 | 79.76 |
| 8/13/2013 11:55:54 AM | 0.93167 | 14.30 | 79.76 |
| 8/13/2013 11:55:55 AM | 0.93194 | 14.30 | 79.77 |
| 8/13/2013 11:55:56 AM | 0.93222 | 14.30 | 79.77 |
| 8/13/2013 11:55:57 AM | 0.93250 | 14.30 | 79.77 |
| 8/13/2013 11:55:58 AM | 0.93278 | 14.30 | 79.77 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:55:59 AM | 0.93306 | 14.30 | 79.77 |
| 8/13/2013 11:56:00 AM | 0.93333 | 14.30 | 79.78 |
| 8/13/2013 11:56:01 AM | 0.93361 | 14.30 | 79.78 |
| 8/13/2013 11:56:02 AM | 0.93389 | 14.30 | 79.78 |
| 8/13/2013 11:56:03 AM | 0.93417 | 14.30 | 79.78 |
| 8/13/2013 11:56:04 AM | 0.93444 | 14.30 | 79.78 |
| 8/13/2013 11:56:05 AM | 0.93472 | 14.30 | 79.78 |
| 8/13/2013 11:56:06 AM | 0.93500 | 14.30 | 79.79 |
| 8/13/2013 11:56:07 AM | 0.93528 | 14.30 | 79.79 |
| 8/13/2013 11:56:08 AM | 0.93556 | 14.30 | 79.79 |
| 8/13/2013 11:56:09 AM | 0.93583 | 14.30 | 79.79 |
| 8/13/2013 11:56:10 AM | 0.93611 | 14.30 | 79.79 |
| 8/13/2013 11:56:11 AM | 0.93639 | 14.30 | 79.80 |
| 8/13/2013 11:56:12 AM | 0.93667 | 14.30 | 79.80 |
| 8/13/2013 11:56:13 AM | 0.93694 | 14.30 | 79.80 |
| 8/13/2013 11:56:14 AM | 0.93722 | 14.30 | 79.80 |
| 8/13/2013 11:56:15 AM | 0.93750 | 14.30 | 79.80 |
| 8/13/2013 11:56:16 AM | 0.93778 | 14.30 | 79.81 |
| 8/13/2013 11:56:17 AM | 0.93806 | 14.30 | 79.81 |
| 8/13/2013 11:56:18 AM | 0.93833 | 14.30 | 79.81 |
| 8/13/2013 11:56:19 AM | 0.93861 | 14.30 | 79.81 |
| 8/13/2013 11:56:20 AM | 0.93889 | 14.30 | 79.81 |
| 8/13/2013 11:56:21 AM | 0.93917 | 14.30 | 79.81 |
| 8/13/2013 11:56:22 AM | 0.93944 | 14.30 | 79.82 |
| 8/13/2013 11:56:23 AM | 0.93972 | 14.30 | 79.82 |
| 8/13/2013 11:56:24 AM | 0.94000 | 14.30 | 79.82 |
| 8/13/2013 11:56:25 AM | 0.94028 | 14.30 | 79.82 |
| 8/13/2013 11:56:26 AM | 0.94056 | 14.30 | 79.82 |
| 8/13/2013 11:56:27 AM | 0.94083 | 14.30 | 79.83 |
| 8/13/2013 11:56:28 AM | 0.94111 | 14.30 | 79.83 |
| 8/13/2013 11:56:29 AM | 0.94139 | 14.30 | 79.83 |
| 8/13/2013 11:56:30 AM | 0.94167 | 14.30 | 79.83 |
| 8/13/2013 11:56:31 AM | 0.94194 | 14.30 | 79.83 |
| 8/13/2013 11:56:32 AM | 0.94222 | 14.30 | 79.83 |
| 8/13/2013 11:56:33 AM | 0.94250 | 14.30 | 79.84 |
| 8/13/2013 11:56:34 AM | 0.94278 | 14.30 | 79.84 |
| 8/13/2013 11:56:35 AM | 0.94306 | 14.30 | 79.84 |
| 8/13/2013 11:56:36 AM | 0.94333 | 14.30 | 79.84 |
| 8/13/2013 11:56:37 AM | 0.94361 | 14.30 | 79.84 |
| 8/13/2013 11:56:38 AM | 0.94389 | 14.30 | 79.84 |
| 8/13/2013 11:56:39 AM | 0.94417 | 14.30 | 79.85 |
| 8/13/2013 11:56:40 AM | 0.94444 | 14.30 | 79.85 |
| 8/13/2013 11:56:41 AM | 0.94472 | 14.30 | 79.85 |
| 8/13/2013 11:56:42 AM | 0.94500 | 14.30 | 79.85 |
| 8/13/2013 11:56:43 AM | 0.94528 | 14.30 | 79.86 |
| 8/13/2013 11:56:44 AM | 0.94556 | 14.30 | 79.86 |
| 8/13/2013 11:56:45 AM | 0.94583 | 14.30 | 79.86 |
| 8/13/2013 11:56:46 AM | 0.94611 | 14.30 | 79.86 |
| 8/13/2013 11:56:47 AM | 0.94639 | 14.30 | 79.86 |
| 8/13/2013 11:56:48 AM | 0.94667 | 14.30 | 79.86 |
| 8/13/2013 11:56:49 AM | 0.94694 | 14.30 | 79.87 |
| 8/13/2013 11:56:50 AM | 0.94722 | 14.30 | 79.87 |
| 8/13/2013 11:56:51 AM | 0.94750 | 14.30 | 79.87 |
| 8/13/2013 11:56:52 AM | 0.94778 | 14.30 | 79.87 |
| 8/13/2013 11:56:53 AM | 0.94806 | 14.30 | 79.87 |
| 8/13/2013 11:56:54 AM | 0.94833 | 14.30 | 79.87 |
| 8/13/2013 11:56:55 AM | 0.94861 | 14.30 | 79.88 |
| 8/13/2013 11:56:56 AM | 0.94889 | 14.30 | 79.88 |
| 8/13/2013 11:56:57 AM | 0.94917 | 14.30 | 79.88 |
| 8/13/2013 11:56:58 AM | 0.94944 | 14.30 | 79.88 |
| 8/13/2013 11:56:59 AM | 0.94972 | 14.30 | 79.88 |
| 8/13/2013 11:57:00 AM | 0.95000 | 14.30 | 79.88 |
| 8/13/2013 11:57:01 AM | 0.95028 | 14.30 | 79.89 |
| 8/13/2013 11:57:02 AM | 0.95056 | 14.30 | 79.89 |
| 8/13/2013 11:57:03 AM | 0.95083 | 14.30 | 79.89 |
| 8/13/2013 11:57:04 AM | 0.95111 | 14.30 | 79.89 |
| 8/13/2013 11:57:05 AM | 0.95139 | 14.30 | 79.89 |
| 8/13/2013 11:57:06 AM | 0.95167 | 14.30 | 79.89 |
| 8/13/2013 11:57:07 AM | 0.95194 | 14.30 | 79.90 |
| 8/13/2013 11:57:08 AM | 0.95222 | 14.30 | 79.90 |
| 8/13/2013 11:57:09 AM | 0.95250 | 14.30 | 79.90 |
| 8/13/2013 11:57:10 AM | 0.95278 | 14.30 | 79.90 |
| 8/13/2013 11:57:11 AM | 0.95306 | 14.30 | 79.90 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:57:12 AM | 0.96333 | 14.30 | 79.91 |
| 8/13/2013 11:57:13 AM | 0.96361 | 14.30 | 79.91 |
| 8/13/2013 11:57:14 AM | 0.96389 | 14.30 | 79.91 |
| 8/13/2013 11:57:15 AM | 0.96417 | 14.30 | 79.91 |
| 8/13/2013 11:57:16 AM | 0.96444 | 14.30 | 79.91 |
| 8/13/2013 11:57:17 AM | 0.96472 | 14.30 | 79.91 |
| 8/13/2013 11:57:18 AM | 0.96500 | 14.30 | 79.92 |
| 8/13/2013 11:57:19 AM | 0.96528 | 14.30 | 79.92 |
| 8/13/2013 11:57:20 AM | 0.96556 | 14.30 | 79.92 |
| 8/13/2013 11:57:21 AM | 0.96583 | 14.30 | 79.92 |
| 8/13/2013 11:57:22 AM | 0.96611 | 14.30 | 79.92 |
| 8/13/2013 11:57:23 AM | 0.96639 | 14.30 | 79.92 |
| 8/13/2013 11:57:24 AM | 0.96667 | 14.30 | 79.93 |
| 8/13/2013 11:57:25 AM | 0.96694 | 14.30 | 79.93 |
| 8/13/2013 11:57:26 AM | 0.96722 | 14.30 | 79.93 |
| 8/13/2013 11:57:27 AM | 0.96750 | 14.30 | 79.93 |
| 8/13/2013 11:57:28 AM | 0.96778 | 14.30 | 79.93 |
| 8/13/2013 11:57:29 AM | 0.96806 | 14.30 | 79.94 |
| 8/13/2013 11:57:30 AM | 0.96833 | 14.30 | 79.94 |
| 8/13/2013 11:57:31 AM | 0.96861 | 14.30 | 79.94 |
| 8/13/2013 11:57:32 AM | 0.96889 | 14.30 | 79.94 |
| 8/13/2013 11:57:33 AM | 0.96917 | 14.30 | 79.95 |
| 8/13/2013 11:57:34 AM | 0.96944 | 14.30 | 79.95 |
| 8/13/2013 11:57:35 AM | 0.96972 | 14.30 | 79.95 |
| 8/13/2013 11:57:36 AM | 0.97000 | 14.30 | 79.96 |
| 8/13/2013 11:57:37 AM | 0.97028 | 14.30 | 79.96 |
| 8/13/2013 11:57:38 AM | 0.97056 | 14.30 | 79.96 |
| 8/13/2013 11:57:39 AM | 0.97083 | 14.30 | 79.97 |
| 8/13/2013 11:57:40 AM | 0.97111 | 14.30 | 79.97 |
| 8/13/2013 11:57:41 AM | 0.97139 | 14.30 | 79.97 |
| 8/13/2013 11:57:42 AM | 0.97167 | 14.30 | 79.97 |
| 8/13/2013 11:57:43 AM | 0.97194 | 14.30 | 79.98 |
| 8/13/2013 11:57:44 AM | 0.97222 | 14.30 | 79.98 |
| 8/13/2013 11:57:45 AM | 0.97250 | 14.30 | 79.98 |
| 8/13/2013 11:57:46 AM | 0.97278 | 14.30 | 79.98 |
| 8/13/2013 11:57:47 AM | 0.97306 | 14.30 | 79.99 |
| 8/13/2013 11:57:48 AM | 0.97333 | 14.30 | 79.99 |
| 8/13/2013 11:57:49 AM | 0.97361 | 14.30 | 79.99 |
| 8/13/2013 11:57:50 AM | 0.97389 | 14.30 | 79.99 |
| 8/13/2013 11:57:51 AM | 0.97417 | 14.30 | 80.00 |
| 8/13/2013 11:57:52 AM | 0.97444 | 14.30 | 80.00 |
| 8/13/2013 11:57:53 AM | 0.97472 | 14.30 | 80.00 |
| 8/13/2013 11:57:54 AM | 0.97500 | 14.30 | 80.00 |
| 8/13/2013 11:57:55 AM | 0.97528 | 14.30 | 80.00 |
| 8/13/2013 11:57:56 AM | 0.97556 | 14.30 | 80.00 |
| 8/13/2013 11:57:57 AM | 0.97583 | 14.30 | 80.00 |
| 8/13/2013 11:57:58 AM | 0.97611 | 14.30 | 80.01 |
| 8/13/2013 11:57:59 AM | 0.97639 | 14.30 | 80.01 |
| 8/13/2013 11:58:00 AM | 0.97667 | 14.30 | 80.01 |
| 8/13/2013 11:58:01 AM | 0.97694 | 14.30 | 80.01 |
| 8/13/2013 11:58:02 AM | 0.97722 | 14.30 | 80.01 |
| 8/13/2013 11:58:03 AM | 0.97750 | 14.30 | 80.01 |
| 8/13/2013 11:58:04 AM | 0.97778 | 14.30 | 80.01 |
| 8/13/2013 11:58:05 AM | 0.97806 | 14.30 | 80.02 |
| 8/13/2013 11:58:06 AM | 0.97833 | 14.30 | 80.02 |
| 8/13/2013 11:58:07 AM | 0.97861 | 14.30 | 80.02 |
| 8/13/2013 11:58:08 AM | 0.97889 | 14.30 | 80.02 |
| 8/13/2013 11:58:09 AM | 0.97917 | 14.30 | 80.02 |
| 8/13/2013 11:58:10 AM | 0.97944 | 14.30 | 80.02 |
| 8/13/2013 11:58:11 AM | 0.97972 | 14.30 | 80.02 |
| 8/13/2013 11:58:12 AM | 0.98000 | 14.30 | 80.02 |
| 8/13/2013 11:58:13 AM | 0.98028 | 14.30 | 80.02 |
| 8/13/2013 11:58:14 AM | 0.98056 | 14.30 | 80.02 |
| 8/13/2013 11:58:15 AM | 0.98083 | 14.30 | 80.03 |
| 8/13/2013 11:58:16 AM | 0.98111 | 14.30 | 80.03 |
| 8/13/2013 11:58:17 AM | 0.98139 | 14.30 | 80.03 |
| 8/13/2013 11:58:18 AM | 0.98167 | 14.30 | 80.03 |
| 8/13/2013 11:58:19 AM | 0.98194 | 14.30 | 80.03 |
| 8/13/2013 11:58:20 AM | 0.98222 | 14.30 | 80.03 |
| 8/13/2013 11:58:21 AM | 0.98250 | 14.30 | 80.03 |
| 8/13/2013 11:58:22 AM | 0.98278 | 14.30 | 80.03 |
| 8/13/2013 11:58:23 AM | 0.98306 | 14.30 | 80.03 |
| 8/13/2013 11:58:24 AM | 0.98333 | 14.30 | 80.03 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:58:25 AM | 0.97361 | 14.30 | 80.03 |
| 8/13/2013 11:58:26 AM | 0.97389 | 14.30 | 80.04 |
| 8/13/2013 11:58:27 AM | 0.97417 | 14.30 | 80.04 |
| 8/13/2013 11:58:28 AM | 0.97444 | 14.30 | 80.04 |
| 8/13/2013 11:58:29 AM | 0.97472 | 14.30 | 80.04 |
| 8/13/2013 11:58:30 AM | 0.97500 | 14.30 | 80.04 |
| 8/13/2013 11:58:31 AM | 0.97528 | 14.30 | 80.04 |
| 8/13/2013 11:58:32 AM | 0.97556 | 14.30 | 80.04 |
| 8/13/2013 11:58:33 AM | 0.97583 | 14.30 | 80.04 |
| 8/13/2013 11:58:34 AM | 0.97611 | 14.30 | 80.04 |
| 8/13/2013 11:58:35 AM | 0.97639 | 14.30 | 80.04 |
| 8/13/2013 11:58:36 AM | 0.97667 | 14.30 | 80.04 |
| 8/13/2013 11:58:37 AM | 0.97694 | 14.30 | 80.05 |
| 8/13/2013 11:58:38 AM | 0.97722 | 14.30 | 80.05 |
| 8/13/2013 11:58:39 AM | 0.97750 | 14.30 | 80.05 |
| 8/13/2013 11:58:40 AM | 0.97778 | 14.30 | 80.05 |
| 8/13/2013 11:58:41 AM | 0.97806 | 14.30 | 80.05 |
| 8/13/2013 11:58:42 AM | 0.97833 | 14.30 | 80.05 |
| 8/13/2013 11:58:43 AM | 0.97861 | 14.30 | 80.05 |
| 8/13/2013 11:58:44 AM | 0.97889 | 14.30 | 80.05 |
| 8/13/2013 11:58:45 AM | 0.97917 | 14.30 | 80.05 |
| 8/13/2013 11:58:46 AM | 0.97944 | 14.30 | 80.05 |
| 8/13/2013 11:58:47 AM | 0.97972 | 14.30 | 80.05 |
| 8/13/2013 11:58:48 AM | 0.98000 | 14.30 | 80.06 |
| 8/13/2013 11:58:49 AM | 0.98028 | 14.30 | 80.06 |
| 8/13/2013 11:58:50 AM | 0.98056 | 14.30 | 80.06 |
| 8/13/2013 11:58:51 AM | 0.98083 | 14.30 | 80.06 |
| 8/13/2013 11:58:52 AM | 0.98111 | 14.30 | 80.06 |
| 8/13/2013 11:58:53 AM | 0.98139 | 14.30 | 80.06 |
| 8/13/2013 11:58:54 AM | 0.98167 | 14.30 | 80.06 |
| 8/13/2013 11:58:55 AM | 0.98194 | 14.30 | 80.06 |
| 8/13/2013 11:58:56 AM | 0.98222 | 14.30 | 80.06 |
| 8/13/2013 11:58:57 AM | 0.98250 | 14.30 | 80.06 |
| 8/13/2013 11:58:58 AM | 0.98278 | 14.30 | 80.06 |
| 8/13/2013 11:58:59 AM | 0.98306 | 14.30 | 80.06 |
| 8/13/2013 11:59:00 AM | 0.98333 | 14.30 | 80.06 |
| 8/13/2013 11:59:01 AM | 0.98361 | 14.30 | 80.06 |
| 8/13/2013 11:59:02 AM | 0.98389 | 14.30 | 80.07 |
| 8/13/2013 11:59:03 AM | 0.98417 | 14.30 | 80.07 |
| 8/13/2013 11:59:04 AM | 0.98444 | 14.30 | 80.07 |
| 8/13/2013 11:59:05 AM | 0.98472 | 14.30 | 80.07 |
| 8/13/2013 11:59:06 AM | 0.98500 | 14.30 | 80.07 |
| 8/13/2013 11:59:07 AM | 0.98528 | 14.30 | 80.07 |
| 8/13/2013 11:59:08 AM | 0.98556 | 14.30 | 80.07 |
| 8/13/2013 11:59:09 AM | 0.98583 | 14.30 | 80.07 |
| 8/13/2013 11:59:10 AM | 0.98611 | 14.30 | 80.07 |
| 8/13/2013 11:59:11 AM | 0.98639 | 14.30 | 80.07 |
| 8/13/2013 11:59:12 AM | 0.98667 | 14.30 | 80.07 |
| 8/13/2013 11:59:13 AM | 0.98694 | 14.30 | 80.07 |
| 8/13/2013 11:59:14 AM | 0.98722 | 14.30 | 80.08 |
| 8/13/2013 11:59:15 AM | 0.98750 | 14.30 | 80.08 |
| 8/13/2013 11:59:16 AM | 0.98778 | 14.30 | 80.08 |
| 8/13/2013 11:59:17 AM | 0.98806 | 14.30 | 80.08 |
| 8/13/2013 11:59:18 AM | 0.98833 | 14.30 | 80.08 |
| 8/13/2013 11:59:19 AM | 0.98861 | 14.30 | 80.08 |
| 8/13/2013 11:59:20 AM | 0.98889 | 14.30 | 80.08 |
| 8/13/2013 11:59:21 AM | 0.98917 | 14.30 | 80.08 |
| 8/13/2013 11:59:22 AM | 0.98944 | 14.30 | 80.08 |
| 8/13/2013 11:59:23 AM | 0.98972 | 14.30 | 80.08 |
| 8/13/2013 11:59:24 AM | 0.99000 | 14.30 | 80.08 |
| 8/13/2013 11:59:25 AM | 0.99028 | 14.30 | 80.08 |
| 8/13/2013 11:59:26 AM | 0.99056 | 14.30 | 80.08 |
| 8/13/2013 11:59:27 AM | 0.99083 | 14.30 | 80.09 |
| 8/13/2013 11:59:28 AM | 0.99111 | 14.30 | 80.09 |
| 8/13/2013 11:59:29 AM | 0.99139 | 14.30 | 80.09 |
| 8/13/2013 11:59:30 AM | 0.99167 | 14.30 | 80.09 |
| 8/13/2013 11:59:31 AM | 0.99194 | 14.30 | 80.09 |
| 8/13/2013 11:59:32 AM | 0.99222 | 14.30 | 80.09 |
| 8/13/2013 11:59:33 AM | 0.99250 | 14.30 | 80.09 |
| 8/13/2013 11:59:34 AM | 0.99278 | 14.30 | 80.09 |
| 8/13/2013 11:59:35 AM | 0.99306 | 14.30 | 80.09 |
| 8/13/2013 11:59:36 AM | 0.99333 | 14.30 | 80.09 |
| 8/13/2013 11:59:37 AM | 0.99361 | 14.30 | 80.09 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 11:59:38 AM | 0.99389 | 14.30 | 80.09 |
| 8/13/2013 11:59:39 AM | 0.99417 | 14.30 | 80.10 |
| 8/13/2013 11:59:40 AM | 0.99444 | 14.30 | 80.10 |
| 8/13/2013 11:59:41 AM | 0.99472 | 14.30 | 80.10 |
| 8/13/2013 11:59:42 AM | 0.99500 | 14.30 | 80.10 |
| 8/13/2013 11:59:43 AM | 0.99528 | 14.30 | 80.10 |
| 8/13/2013 11:59:44 AM | 0.99556 | 14.30 | 80.10 |
| 8/13/2013 11:59:45 AM | 0.99583 | 14.30 | 80.10 |
| 8/13/2013 11:59:46 AM | 0.99611 | 14.30 | 80.10 |
| 8/13/2013 11:59:47 AM | 0.99639 | 14.30 | 80.10 |
| 8/13/2013 11:59:48 AM | 0.99667 | 14.30 | 80.10 |
| 8/13/2013 11:59:49 AM | 0.99694 | 14.30 | 80.10 |
| 8/13/2013 11:59:50 AM | 0.99722 | 14.30 | 80.11 |
| 8/13/2013 11:59:51 AM | 0.99750 | 14.30 | 80.11 |
| 8/13/2013 11:59:52 AM | 0.99778 | 14.30 | 80.11 |
| 8/13/2013 11:59:53 AM | 0.99806 | 14.30 | 80.11 |
| 8/13/2013 11:59:54 AM | 0.99833 | 14.30 | 80.11 |
| 8/13/2013 11:59:55 AM | 0.99861 | 14.30 | 80.11 |
| 8/13/2013 11:59:56 AM | 0.99889 | 14.30 | 80.11 |
| 8/13/2013 11:59:57 AM | 0.99917 | 14.30 | 80.11 |
| 8/13/2013 11:59:58 AM | 0.99944 | 14.30 | 80.11 |
| 8/13/2013 11:59:59 AM | 0.99972 | 14.30 | 80.11 |
| 8/13/2013 12:00:00 PM | 1.00000 | 14.30 | 80.11 |
| 8/13/2013 12:00:01 PM | 1.00028 | 14.30 | 80.11 |
| 8/13/2013 12:00:02 PM | 1.00056 | 14.30 | 80.11 |
| 8/13/2013 12:00:03 PM | 1.00083 | 14.30 | 80.11 |
| 8/13/2013 12:00:04 PM | 1.00111 | 14.30 | 80.12 |
| 8/13/2013 12:00:05 PM | 1.00139 | 14.30 | 80.12 |
| 8/13/2013 12:00:06 PM | 1.00167 | 14.30 | 80.12 |
| 8/13/2013 12:00:07 PM | 1.00194 | 14.30 | 80.12 |
| 8/13/2013 12:00:08 PM | 1.00222 | 14.30 | 80.12 |
| 8/13/2013 12:00:09 PM | 1.00250 | 14.30 | 80.12 |
| 8/13/2013 12:00:10 PM | 1.00278 | 14.30 | 80.12 |
| 8/13/2013 12:00:11 PM | 1.00306 | 14.30 | 80.12 |
| 8/13/2013 12:00:12 PM | 1.00333 | 14.30 | 80.12 |
| 8/13/2013 12:00:13 PM | 1.00361 | 14.30 | 80.12 |
| 8/13/2013 12:00:14 PM | 1.00389 | 14.30 | 80.12 |
| 8/13/2013 12:00:15 PM | 1.00417 | 14.30 | 80.13 |
| 8/13/2013 12:00:16 PM | 1.00444 | 14.30 | 80.13 |
| 8/13/2013 12:00:17 PM | 1.00472 | 14.30 | 80.13 |
| 8/13/2013 12:00:18 PM | 1.00500 | 14.30 | 80.13 |
| 8/13/2013 12:00:19 PM | 1.00528 | 14.30 | 80.13 |
| 8/13/2013 12:00:20 PM | 1.00556 | 14.30 | 80.13 |
| 8/13/2013 12:00:21 PM | 1.00583 | 14.30 | 80.13 |
| 8/13/2013 12:00:22 PM | 1.00611 | 14.30 | 80.13 |
| 8/13/2013 12:00:23 PM | 1.00639 | 14.30 | 80.13 |
| 8/13/2013 12:00:24 PM | 1.00667 | 14.30 | 80.13 |
| 8/13/2013 12:00:25 PM | 1.00694 | 14.30 | 80.13 |
| 8/13/2013 12:00:26 PM | 1.00722 | 14.30 | 80.13 |
| 8/13/2013 12:00:27 PM | 1.00750 | 14.30 | 80.13 |
| 8/13/2013 12:00:28 PM | 1.00778 | 14.30 | 80.14 |
| 8/13/2013 12:00:29 PM | 1.00806 | 14.30 | 80.14 |
| 8/13/2013 12:00:30 PM | 1.00833 | 14.30 | 80.14 |
| 8/13/2013 12:00:31 PM | 1.00861 | 14.30 | 80.14 |
| 8/13/2013 12:00:32 PM | 1.00889 | 14.30 | 80.14 |
| 8/13/2013 12:00:33 PM | 1.00917 | 14.30 | 80.14 |
| 8/13/2013 12:00:34 PM | 1.00944 | 14.30 | 80.14 |
| 8/13/2013 12:00:35 PM | 1.00972 | 14.30 | 80.14 |
| 8/13/2013 12:00:36 PM | 1.01000 | 14.30 | 80.14 |
| 8/13/2013 12:00:37 PM | 1.01028 | 14.30 | 80.14 |
| 8/13/2013 12:00:38 PM | 1.01056 | 14.30 | 80.14 |
| 8/13/2013 12:00:39 PM | 1.01083 | 14.30 | 80.14 |
| 8/13/2013 12:00:40 PM | 1.01111 | 14.30 | 80.14 |
| 8/13/2013 12:00:41 PM | 1.01139 | 14.30 | 80.14 |
| 8/13/2013 12:00:42 PM | 1.01167 | 14.30 | 80.15 |
| 8/13/2013 12:00:43 PM | 1.01194 | 14.30 | 80.15 |
| 8/13/2013 12:00:44 PM | 1.01222 | 14.30 | 80.15 |
| 8/13/2013 12:00:45 PM | 1.01250 | 14.30 | 80.15 |
| 8/13/2013 12:00:46 PM | 1.01278 | 14.30 | 80.15 |
| 8/13/2013 12:00:47 PM | 1.01306 | 14.30 | 80.15 |
| 8/13/2013 12:00:48 PM | 1.01333 | 14.30 | 80.15 |
| 8/13/2013 12:00:49 PM | 1.01361 | 14.30 | 80.15 |
| 8/13/2013 12:00:50 PM | 1.01389 | 14.30 | 80.15 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:00:51 PM | 1.01417 | 14.30 | 80.15 |
| 8/13/2013 12:00:52 PM | 1.01444 | 14.30 | 80.15 |
| 8/13/2013 12:00:53 PM | 1.01472 | 14.30 | 80.15 |
| 8/13/2013 12:00:54 PM | 1.01500 | 14.30 | 80.16 |
| 8/13/2013 12:00:55 PM | 1.01528 | 14.30 | 80.16 |
| 8/13/2013 12:00:56 PM | 1.01556 | 14.30 | 80.16 |
| 8/13/2013 12:00:57 PM | 1.01583 | 14.30 | 80.16 |
| 8/13/2013 12:00:58 PM | 1.01611 | 14.30 | 80.16 |
| 8/13/2013 12:00:59 PM | 1.01639 | 14.30 | 80.16 |
| 8/13/2013 12:01:00 PM | 1.01667 | 14.30 | 80.16 |
| 8/13/2013 12:01:01 PM | 1.01694 | 14.30 | 80.16 |
| 8/13/2013 12:01:02 PM | 1.01722 | 14.30 | 80.16 |
| 8/13/2013 12:01:03 PM | 1.01750 | 14.30 | 80.16 |
| 8/13/2013 12:01:04 PM | 1.01778 | 14.30 | 80.16 |
| 8/13/2013 12:01:05 PM | 1.01806 | 14.30 | 80.16 |
| 8/13/2013 12:01:06 PM | 1.01833 | 14.30 | 80.16 |
| 8/13/2013 12:01:07 PM | 1.01861 | 14.30 | 80.16 |
| 8/13/2013 12:01:08 PM | 1.01889 | 14.30 | 80.17 |
| 8/13/2013 12:01:09 PM | 1.01917 | 14.30 | 80.17 |
| 8/13/2013 12:01:10 PM | 1.01944 | 14.30 | 80.17 |
| 8/13/2013 12:01:11 PM | 1.01972 | 14.30 | 80.17 |
| 8/13/2013 12:01:12 PM | 1.02000 | 14.30 | 80.17 |
| 8/13/2013 12:01:13 PM | 1.02028 | 14.30 | 80.17 |
| 8/13/2013 12:01:14 PM | 1.02056 | 14.30 | 80.17 |
| 8/13/2013 12:01:15 PM | 1.02083 | 14.30 | 80.17 |
| 8/13/2013 12:01:16 PM | 1.02111 | 14.30 | 80.17 |
| 8/13/2013 12:01:17 PM | 1.02139 | 14.30 | 80.17 |
| 8/13/2013 12:01:18 PM | 1.02167 | 14.30 | 80.17 |
| 8/13/2013 12:01:19 PM | 1.02194 | 14.30 | 80.17 |
| 8/13/2013 12:01:20 PM | 1.02222 | 14.30 | 80.17 |
| 8/13/2013 12:01:21 PM | 1.02250 | 14.30 | 80.17 |
| 8/13/2013 12:01:22 PM | 1.02278 | 14.30 | 80.17 |
| 8/13/2013 12:01:23 PM | 1.02306 | 14.30 | 80.17 |
| 8/13/2013 12:01:24 PM | 1.02333 | 14.30 | 80.18 |
| 8/13/2013 12:01:25 PM | 1.02361 | 14.30 | 80.18 |
| 8/13/2013 12:01:26 PM | 1.02389 | 14.30 | 80.18 |
| 8/13/2013 12:01:27 PM | 1.02417 | 14.30 | 80.18 |
| 8/13/2013 12:01:28 PM | 1.02444 | 14.30 | 80.18 |
| 8/13/2013 12:01:29 PM | 1.02472 | 14.30 | 80.18 |
| 8/13/2013 12:01:30 PM | 1.02500 | 14.30 | 80.18 |
| 8/13/2013 12:01:31 PM | 1.02528 | 14.30 | 80.18 |
| 8/13/2013 12:01:32 PM | 1.02556 | 14.30 | 80.18 |
| 8/13/2013 12:01:33 PM | 1.02583 | 14.30 | 80.18 |
| 8/13/2013 12:01:34 PM | 1.02611 | 14.30 | 80.18 |
| 8/13/2013 12:01:35 PM | 1.02639 | 14.30 | 80.18 |
| 8/13/2013 12:01:36 PM | 1.02667 | 14.30 | 80.18 |
| 8/13/2013 12:01:37 PM | 1.02694 | 14.30 | 80.18 |
| 8/13/2013 12:01:38 PM | 1.02722 | 14.30 | 80.18 |
| 8/13/2013 12:01:39 PM | 1.02750 | 14.30 | 80.19 |
| 8/13/2013 12:01:40 PM | 1.02778 | 14.30 | 80.19 |
| 8/13/2013 12:01:41 PM | 1.02806 | 14.30 | 80.19 |
| 8/13/2013 12:01:42 PM | 1.02833 | 14.30 | 80.19 |
| 8/13/2013 12:01:43 PM | 1.02861 | 14.30 | 80.19 |
| 8/13/2013 12:01:44 PM | 1.02889 | 14.30 | 80.19 |
| 8/13/2013 12:01:45 PM | 1.02917 | 14.30 | 80.19 |
| 8/13/2013 12:01:46 PM | 1.02944 | 14.30 | 80.19 |
| 8/13/2013 12:01:47 PM | 1.02972 | 14.30 | 80.19 |
| 8/13/2013 12:01:48 PM | 1.03000 | 14.30 | 80.19 |
| 8/13/2013 12:01:49 PM | 1.03028 | 14.30 | 80.19 |
| 8/13/2013 12:01:50 PM | 1.03056 | 14.30 | 80.19 |
| 8/13/2013 12:01:51 PM | 1.03083 | 14.30 | 80.19 |
| 8/13/2013 12:01:52 PM | 1.03111 | 14.30 | 80.19 |
| 8/13/2013 12:01:53 PM | 1.03139 | 14.30 | 80.19 |
| 8/13/2013 12:01:54 PM | 1.03167 | 14.30 | 80.19 |
| 8/13/2013 12:01:55 PM | 1.03194 | 14.30 | 80.19 |
| 8/13/2013 12:01:56 PM | 1.03222 | 14.30 | 80.19 |
| 8/13/2013 12:01:57 PM | 1.03250 | 14.30 | 80.20 |
| 8/13/2013 12:01:58 PM | 1.03278 | 14.30 | 80.20 |
| 8/13/2013 12:01:59 PM | 1.03306 | 14.30 | 80.20 |
| 8/13/2013 12:02:00 PM | 1.03333 | 14.30 | 80.20 |
| 8/13/2013 12:02:01 PM | 1.03361 | 14.30 | 80.20 |
| 8/13/2013 12:02:02 PM | 1.03389 | 14.30 | 80.20 |
| 8/13/2013 12:02:03 PM | 1.03417 | 14.30 | 80.20 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:02:04 PM | 1.03444 | 14.30 | 80.20 |
| 8/13/2013 12:02:05 PM | 1.03472 | 14.30 | 80.20 |
| 8/13/2013 12:02:06 PM | 1.03500 | 14.30 | 80.20 |
| 8/13/2013 12:02:07 PM | 1.03528 | 14.30 | 80.20 |
| 8/13/2013 12:02:08 PM | 1.03556 | 14.30 | 80.20 |
| 8/13/2013 12:02:09 PM | 1.03583 | 14.30 | 80.20 |
| 8/13/2013 12:02:10 PM | 1.03611 | 14.30 | 80.20 |
| 8/13/2013 12:02:11 PM | 1.03639 | 14.30 | 80.20 |
| 8/13/2013 12:02:12 PM | 1.03667 | 14.30 | 80.20 |
| 8/13/2013 12:02:13 PM | 1.03694 | 14.30 | 80.20 |
| 8/13/2013 12:02:14 PM | 1.03722 | 14.30 | 80.20 |
| 8/13/2013 12:02:15 PM | 1.03750 | 14.30 | 80.20 |
| 8/13/2013 12:02:16 PM | 1.03778 | 14.30 | 80.21 |
| 8/13/2013 12:02:17 PM | 1.03806 | 14.30 | 80.21 |
| 8/13/2013 12:02:18 PM | 1.03833 | 14.30 | 80.21 |
| 8/13/2013 12:02:19 PM | 1.03861 | 14.30 | 80.21 |
| 8/13/2013 12:02:20 PM | 1.03889 | 14.30 | 80.21 |
| 8/13/2013 12:02:21 PM | 1.03917 | 14.30 | 80.21 |
| 8/13/2013 12:02:22 PM | 1.03944 | 14.30 | 80.21 |
| 8/13/2013 12:02:23 PM | 1.03972 | 14.30 | 80.21 |
| 8/13/2013 12:02:24 PM | 1.04000 | 14.30 | 80.21 |
| 8/13/2013 12:02:25 PM | 1.04028 | 14.30 | 80.21 |
| 8/13/2013 12:02:26 PM | 1.04056 | 14.30 | 80.21 |
| 8/13/2013 12:02:27 PM | 1.04083 | 14.30 | 80.21 |
| 8/13/2013 12:02:28 PM | 1.04111 | 14.30 | 80.21 |
| 8/13/2013 12:02:29 PM | 1.04139 | 14.30 | 80.21 |
| 8/13/2013 12:02:30 PM | 1.04167 | 14.30 | 80.21 |
| 8/13/2013 12:02:31 PM | 1.04194 | 14.30 | 80.21 |
| 8/13/2013 12:02:32 PM | 1.04222 | 14.30 | 80.21 |
| 8/13/2013 12:02:33 PM | 1.04250 | 14.30 | 80.21 |
| 8/13/2013 12:02:34 PM | 1.04278 | 14.30 | 80.21 |
| 8/13/2013 12:02:35 PM | 1.04306 | 14.30 | 80.22 |
| 8/13/2013 12:02:36 PM | 1.04333 | 14.30 | 80.22 |
| 8/13/2013 12:02:37 PM | 1.04361 | 14.30 | 80.22 |
| 8/13/2013 12:02:38 PM | 1.04389 | 14.30 | 80.22 |
| 8/13/2013 12:02:39 PM | 1.04417 | 14.30 | 80.22 |
| 8/13/2013 12:02:40 PM | 1.04444 | 14.30 | 80.22 |
| 8/13/2013 12:02:41 PM | 1.04472 | 14.30 | 80.22 |
| 8/13/2013 12:02:42 PM | 1.04500 | 14.30 | 80.22 |
| 8/13/2013 12:02:43 PM | 1.04528 | 14.30 | 80.22 |
| 8/13/2013 12:02:44 PM | 1.04556 | 14.30 | 80.22 |
| 8/13/2013 12:02:45 PM | 1.04583 | 14.30 | 80.22 |
| 8/13/2013 12:02:46 PM | 1.04611 | 14.30 | 80.22 |
| 8/13/2013 12:02:47 PM | 1.04639 | 14.30 | 80.22 |
| 8/13/2013 12:02:48 PM | 1.04667 | 14.30 | 80.22 |
| 8/13/2013 12:02:49 PM | 1.04694 | 14.30 | 80.22 |
| 8/13/2013 12:02:50 PM | 1.04722 | 14.30 | 80.22 |
| 8/13/2013 12:02:51 PM | 1.04750 | 14.30 | 80.22 |
| 8/13/2013 12:02:52 PM | 1.04778 | 14.30 | 80.22 |
| 8/13/2013 12:02:53 PM | 1.04806 | 14.30 | 80.22 |
| 8/13/2013 12:02:54 PM | 1.04833 | 14.30 | 80.22 |
| 8/13/2013 12:02:55 PM | 1.04861 | 14.30 | 80.22 |
| 8/13/2013 12:02:56 PM | 1.04889 | 14.30 | 80.22 |
| 8/13/2013 12:02:57 PM | 1.04917 | 14.30 | 80.22 |
| 8/13/2013 12:02:58 PM | 1.04944 | 14.30 | 80.22 |
| 8/13/2013 12:02:59 PM | 1.04972 | 14.30 | 80.22 |
| 8/13/2013 12:03:00 PM | 1.05000 | 14.30 | 80.22 |
| 8/13/2013 12:03:01 PM | 1.05028 | 14.30 | 80.22 |
| 8/13/2013 12:03:02 PM | 1.05056 | 14.30 | 80.23 |
| 8/13/2013 12:03:03 PM | 1.05083 | 14.30 | 80.23 |
| 8/13/2013 12:03:04 PM | 1.05111 | 14.30 | 80.23 |
| 8/13/2013 12:03:05 PM | 1.05139 | 14.30 | 80.23 |
| 8/13/2013 12:03:06 PM | 1.05167 | 14.30 | 80.23 |
| 8/13/2013 12:03:07 PM | 1.05194 | 14.30 | 80.23 |
| 8/13/2013 12:03:08 PM | 1.05222 | 14.30 | 80.23 |
| 8/13/2013 12:03:09 PM | 1.05250 | 14.30 | 80.23 |
| 8/13/2013 12:03:10 PM | 1.05278 | 14.30 | 80.23 |
| 8/13/2013 12:03:11 PM | 1.05306 | 14.30 | 80.23 |
| 8/13/2013 12:03:12 PM | 1.05333 | 14.30 | 80.23 |
| 8/13/2013 12:03:13 PM | 1.05361 | 14.30 | 80.23 |
| 8/13/2013 12:03:14 PM | 1.05389 | 14.30 | 80.23 |
| 8/13/2013 12:03:15 PM | 1.05417 | 14.30 | 80.23 |
| 8/13/2013 12:03:16 PM | 1.05444 | 14.30 | 80.23 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:03:17 PM | 1.05472 | 14.30 | 80.23 |
| 8/13/2013 12:03:18 PM | 1.05500 | 14.30 | 80.23 |
| 8/13/2013 12:03:19 PM | 1.05528 | 14.30 | 80.23 |
| 8/13/2013 12:03:20 PM | 1.05556 | 14.30 | 80.23 |
| 8/13/2013 12:03:21 PM | 1.05583 | 14.30 | 80.23 |
| 8/13/2013 12:03:22 PM | 1.05611 | 14.30 | 80.23 |
| 8/13/2013 12:03:23 PM | 1.05639 | 14.30 | 80.23 |
| 8/13/2013 12:03:24 PM | 1.05667 | 14.30 | 80.23 |
| 8/13/2013 12:03:25 PM | 1.05694 | 14.30 | 80.23 |
| 8/13/2013 12:03:26 PM | 1.05722 | 14.30 | 80.23 |
| 8/13/2013 12:03:27 PM | 1.05750 | 14.30 | 80.23 |
| 8/13/2013 12:03:28 PM | 1.05778 | 14.30 | 80.23 |
| 8/13/2013 12:03:29 PM | 1.05806 | 14.30 | 80.23 |
| 8/13/2013 12:03:30 PM | 1.05833 | 14.30 | 80.24 |
| 8/13/2013 12:03:31 PM | 1.05861 | 14.30 | 80.24 |
| 8/13/2013 12:03:32 PM | 1.05889 | 14.30 | 80.24 |
| 8/13/2013 12:03:33 PM | 1.05917 | 14.30 | 80.24 |
| 8/13/2013 12:03:34 PM | 1.05944 | 14.30 | 80.24 |
| 8/13/2013 12:03:35 PM | 1.05972 | 14.30 | 80.24 |
| 8/13/2013 12:03:36 PM | 1.06000 | 14.30 | 80.24 |
| 8/13/2013 12:03:37 PM | 1.06028 | 14.30 | 80.24 |
| 8/13/2013 12:03:38 PM | 1.06056 | 14.30 | 80.24 |
| 8/13/2013 12:03:39 PM | 1.06083 | 14.30 | 80.24 |
| 8/13/2013 12:03:40 PM | 1.06111 | 14.30 | 80.24 |
| 8/13/2013 12:03:41 PM | 1.06139 | 14.30 | 80.24 |
| 8/13/2013 12:03:42 PM | 1.06167 | 14.30 | 80.24 |
| 8/13/2013 12:03:43 PM | 1.06194 | 14.30 | 80.24 |
| 8/13/2013 12:03:44 PM | 1.06222 | 14.30 | 80.24 |
| 8/13/2013 12:03:45 PM | 1.06250 | 14.30 | 80.24 |
| 8/13/2013 12:03:46 PM | 1.06278 | 14.30 | 80.24 |
| 8/13/2013 12:03:47 PM | 1.06306 | 14.30 | 80.24 |
| 8/13/2013 12:03:48 PM | 1.06333 | 14.30 | 80.24 |
| 8/13/2013 12:03:49 PM | 1.06361 | 14.30 | 80.24 |
| 8/13/2013 12:03:50 PM | 1.06389 | 14.30 | 80.24 |
| 8/13/2013 12:03:51 PM | 1.06417 | 14.30 | 80.24 |
| 8/13/2013 12:03:52 PM | 1.06444 | 14.30 | 80.24 |
| 8/13/2013 12:03:53 PM | 1.06472 | 14.30 | 80.24 |
| 8/13/2013 12:03:54 PM | 1.06500 | 14.30 | 80.24 |
| 8/13/2013 12:03:55 PM | 1.06528 | 14.30 | 80.24 |
| 8/13/2013 12:03:56 PM | 1.06556 | 14.30 | 80.24 |
| 8/13/2013 12:03:57 PM | 1.06583 | 14.30 | 80.24 |
| 8/13/2013 12:03:58 PM | 1.06611 | 14.30 | 80.24 |
| 8/13/2013 12:03:59 PM | 1.06639 | 14.30 | 80.24 |
| 8/13/2013 12:04:00 PM | 1.06667 | 14.30 | 80.24 |
| 8/13/2013 12:04:01 PM | 1.06694 | 14.30 | 80.24 |
| 8/13/2013 12:04:02 PM | 1.06722 | 14.30 | 80.25 |
| 8/13/2013 12:04:03 PM | 1.06750 | 14.30 | 80.25 |
| 8/13/2013 12:04:04 PM | 1.06778 | 14.30 | 80.25 |
| 8/13/2013 12:04:05 PM | 1.06806 | 14.30 | 80.25 |
| 8/13/2013 12:04:06 PM | 1.06833 | 14.30 | 80.25 |
| 8/13/2013 12:04:07 PM | 1.06861 | 14.30 | 80.25 |
| 8/13/2013 12:04:08 PM | 1.06889 | 14.30 | 80.25 |
| 8/13/2013 12:04:09 PM | 1.06917 | 14.30 | 80.25 |
| 8/13/2013 12:04:10 PM | 1.06944 | 14.30 | 80.25 |
| 8/13/2013 12:04:11 PM | 1.06972 | 14.30 | 80.25 |
| 8/13/2013 12:04:12 PM | 1.07000 | 14.30 | 80.25 |
| 8/13/2013 12:04:13 PM | 1.07028 | 14.30 | 80.25 |
| 8/13/2013 12:04:14 PM | 1.07056 | 14.30 | 80.25 |
| 8/13/2013 12:04:15 PM | 1.07083 | 14.30 | 80.25 |
| 8/13/2013 12:04:16 PM | 1.07111 | 14.30 | 80.25 |
| 8/13/2013 12:04:17 PM | 1.07139 | 14.30 | 80.25 |
| 8/13/2013 12:04:18 PM | 1.07167 | 14.30 | 80.25 |
| 8/13/2013 12:04:19 PM | 1.07194 | 14.30 | 80.25 |
| 8/13/2013 12:04:20 PM | 1.07222 | 14.30 | 80.25 |
| 8/13/2013 12:04:21 PM | 1.07250 | 14.30 | 80.25 |
| 8/13/2013 12:04:22 PM | 1.07278 | 14.30 | 80.25 |
| 8/13/2013 12:04:23 PM | 1.07306 | 14.30 | 80.25 |
| 8/13/2013 12:04:24 PM | 1.07333 | 14.30 | 80.25 |
| 8/13/2013 12:04:25 PM | 1.07361 | 14.30 | 80.25 |
| 8/13/2013 12:04:26 PM | 1.07389 | 14.30 | 80.25 |
| 8/13/2013 12:04:27 PM | 1.07417 | 14.30 | 80.25 |
| 8/13/2013 12:04:28 PM | 1.07444 | 14.30 | 80.25 |
| 8/13/2013 12:04:29 PM | 1.07472 | 14.30 | 80.25 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:04:30 PM | 1.07500 | 14.30 | 80.25 |
| 8/13/2013 12:04:31 PM | 1.07528 | 14.30 | 80.25 |
| 8/13/2013 12:04:32 PM | 1.07556 | 14.30 | 80.25 |
| 8/13/2013 12:04:33 PM | 1.07583 | 14.30 | 80.25 |
| 8/13/2013 12:04:34 PM | 1.07611 | 14.30 | 80.25 |
| 8/13/2013 12:04:35 PM | 1.07639 | 14.30 | 80.25 |
| 8/13/2013 12:04:36 PM | 1.07667 | 14.30 | 80.25 |
| 8/13/2013 12:04:37 PM | 1.07694 | 14.30 | 80.25 |
| 8/13/2013 12:04:38 PM | 1.07722 | 14.30 | 80.25 |
| 8/13/2013 12:04:39 PM | 1.07750 | 14.30 | 80.25 |
| 8/13/2013 12:04:40 PM | 1.07778 | 14.30 | 80.25 |
| 8/13/2013 12:04:41 PM | 1.07806 | 14.30 | 80.25 |
| 8/13/2013 12:04:42 PM | 1.07833 | 14.30 | 80.25 |
| 8/13/2013 12:04:43 PM | 1.07861 | 14.30 | 80.25 |
| 8/13/2013 12:04:44 PM | 1.07889 | 14.30 | 80.25 |
| 8/13/2013 12:04:45 PM | 1.07917 | 14.30 | 80.25 |
| 8/13/2013 12:04:46 PM | 1.07944 | 14.30 | 80.25 |
| 8/13/2013 12:04:47 PM | 1.07972 | 14.30 | 80.25 |
| 8/13/2013 12:04:48 PM | 1.08000 | 14.30 | 80.25 |
| 8/13/2013 12:04:49 PM | 1.08028 | 14.30 | 80.25 |
| 8/13/2013 12:04:50 PM | 1.08056 | 14.30 | 80.25 |
| 8/13/2013 12:04:51 PM | 1.08083 | 14.30 | 80.25 |
| 8/13/2013 12:04:52 PM | 1.08111 | 14.30 | 80.25 |
| 8/13/2013 12:04:53 PM | 1.08139 | 14.30 | 80.25 |
| 8/13/2013 12:04:54 PM | 1.08167 | 14.30 | 80.25 |
| 8/13/2013 12:04:55 PM | 1.08194 | 14.30 | 80.25 |
| 8/13/2013 12:04:56 PM | 1.08222 | 14.30 | 80.25 |
| 8/13/2013 12:04:57 PM | 1.08250 | 14.30 | 80.25 |
| 8/13/2013 12:04:58 PM | 1.08278 | 14.30 | 80.25 |
| 8/13/2013 12:04:59 PM | 1.08306 | 14.30 | 80.25 |
| 8/13/2013 12:05:00 PM | 1.08333 | 14.30 | 80.25 |
| 8/13/2013 12:05:01 PM | 1.08361 | 14.30 | 80.25 |
| 8/13/2013 12:05:02 PM | 1.08389 | 14.30 | 80.25 |
| 8/13/2013 12:05:03 PM | 1.08417 | 14.30 | 80.25 |
| 8/13/2013 12:05:04 PM | 1.08444 | 14.30 | 80.25 |
| 8/13/2013 12:05:05 PM | 1.08472 | 14.30 | 80.25 |
| 8/13/2013 12:05:06 PM | 1.08500 | 14.30 | 80.25 |
| 8/13/2013 12:05:07 PM | 1.08528 | 14.30 | 80.25 |
| 8/13/2013 12:05:08 PM | 1.08556 | 14.30 | 80.25 |
| 8/13/2013 12:05:09 PM | 1.08583 | 14.30 | 80.25 |
| 8/13/2013 12:05:10 PM | 1.08611 | 14.30 | 80.25 |
| 8/13/2013 12:05:11 PM | 1.08639 | 14.30 | 80.25 |
| 8/13/2013 12:05:12 PM | 1.08667 | 14.30 | 80.25 |
| 8/13/2013 12:05:13 PM | 1.08694 | 14.30 | 80.25 |
| 8/13/2013 12:05:14 PM | 1.08722 | 14.30 | 80.26 |
| 8/13/2013 12:05:15 PM | 1.08750 | 14.30 | 80.26 |
| 8/13/2013 12:05:16 PM | 1.08778 | 14.30 | 80.26 |
| 8/13/2013 12:05:17 PM | 1.08806 | 14.30 | 80.26 |
| 8/13/2013 12:05:18 PM | 1.08833 | 14.30 | 80.26 |
| 8/13/2013 12:05:19 PM | 1.08861 | 14.30 | 80.26 |
| 8/13/2013 12:05:20 PM | 1.08889 | 14.30 | 80.26 |
| 8/13/2013 12:05:21 PM | 1.08917 | 14.30 | 80.26 |
| 8/13/2013 12:05:22 PM | 1.08944 | 14.30 | 80.26 |
| 8/13/2013 12:05:23 PM | 1.08972 | 14.30 | 80.26 |
| 8/13/2013 12:05:24 PM | 1.09000 | 14.30 | 80.26 |
| 8/13/2013 12:05:25 PM | 1.09028 | 14.30 | 80.26 |
| 8/13/2013 12:05:26 PM | 1.09056 | 14.30 | 80.26 |
| 8/13/2013 12:05:27 PM | 1.09083 | 14.30 | 80.26 |
| 8/13/2013 12:05:28 PM | 1.09111 | 14.30 | 80.26 |
| 8/13/2013 12:05:29 PM | 1.09139 | 14.30 | 80.26 |
| 8/13/2013 12:05:30 PM | 1.09167 | 14.30 | 80.26 |
| 8/13/2013 12:05:31 PM | 1.09194 | 14.30 | 80.26 |
| 8/13/2013 12:05:32 PM | 1.09222 | 14.30 | 80.26 |
| 8/13/2013 12:05:33 PM | 1.09250 | 14.30 | 80.26 |
| 8/13/2013 12:05:34 PM | 1.09278 | 14.30 | 80.26 |
| 8/13/2013 12:05:35 PM | 1.09306 | 14.30 | 80.26 |
| 8/13/2013 12:05:36 PM | 1.09333 | 14.30 | 80.26 |
| 8/13/2013 12:05:37 PM | 1.09361 | 14.30 | 80.26 |
| 8/13/2013 12:05:38 PM | 1.09389 | 14.30 | 80.26 |
| 8/13/2013 12:05:39 PM | 1.09417 | 14.30 | 80.26 |
| 8/13/2013 12:05:40 PM | 1.09444 | 14.30 | 80.26 |
| 8/13/2013 12:05:41 PM | 1.09472 | 14.30 | 80.26 |
| 8/13/2013 12:05:42 PM | 1.09500 | 14.30 | 80.26 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:05:43 PM | 1.09528 | 14.30 | 80.26 |
| 8/13/2013 12:05:44 PM | 1.09556 | 14.30 | 80.26 |
| 8/13/2013 12:05:45 PM | 1.09583 | 14.30 | 80.26 |
| 8/13/2013 12:05:46 PM | 1.09611 | 14.30 | 80.26 |
| 8/13/2013 12:05:47 PM | 1.09639 | 14.30 | 80.26 |
| 8/13/2013 12:05:48 PM | 1.09667 | 14.30 | 80.26 |
| 8/13/2013 12:05:49 PM | 1.09694 | 14.30 | 80.26 |
| 8/13/2013 12:05:50 PM | 1.09722 | 14.30 | 80.26 |
| 8/13/2013 12:05:51 PM | 1.09750 | 14.30 | 80.26 |
| 8/13/2013 12:05:52 PM | 1.09778 | 14.30 | 80.26 |
| 8/13/2013 12:05:53 PM | 1.09806 | 14.30 | 80.26 |
| 8/13/2013 12:05:54 PM | 1.09833 | 14.30 | 80.26 |
| 8/13/2013 12:05:55 PM | 1.09861 | 14.30 | 80.26 |
| 8/13/2013 12:05:56 PM | 1.09889 | 14.30 | 80.26 |
| 8/13/2013 12:05:57 PM | 1.09917 | 14.31 | 80.26 |
| 8/13/2013 12:05:58 PM | 1.09944 | 14.35 | 80.27 |
| 8/13/2013 12:05:59 PM | 1.09972 | 14.35 | 80.27 |
| 8/13/2013 12:06:00 PM | 1.10000 | 14.37 | 80.27 |
| 8/13/2013 12:06:01 PM | 1.10028 | 14.40 | 80.27 |
| 8/13/2013 12:06:02 PM | 1.10056 | 14.45 | 80.27 |
| 8/13/2013 12:06:03 PM | 1.10083 | 14.54 | 80.27 |
| 8/13/2013 12:06:04 PM | 1.10111 | 14.69 | 80.27 |
| 8/13/2013 12:06:05 PM | 1.10139 | 15.08 | 80.27 |
| 8/13/2013 12:06:06 PM | 1.10167 | 16.41 | 80.27 |
| 8/13/2013 12:06:07 PM | 1.10194 | 20.75 | 80.27 |
| 8/13/2013 12:06:08 PM | 1.10222 | 27.26 | 80.28 |
| 8/13/2013 12:06:09 PM | 1.10250 | 34.50 | 80.28 |
| 8/13/2013 12:06:10 PM | 1.10278 | 42.08 | 80.29 |
| 8/13/2013 12:06:11 PM | 1.10306 | 52.07 | 80.29 |
| 8/13/2013 12:06:12 PM | 1.10333 | 63.47 | 80.29 |
| 8/13/2013 12:06:13 PM | 1.10361 | 76.39 | 80.28 |
| 8/13/2013 12:06:14 PM | 1.10389 | 90.49 | 80.27 |
| 8/13/2013 12:06:15 PM | 1.10417 | 105.56 | 80.26 |
| 8/13/2013 12:06:16 PM | 1.10444 | 119.92 | 80.24 |
| 8/13/2013 12:06:17 PM | 1.10472 | 131.21 | 80.21 |
| 8/13/2013 12:06:18 PM | 1.10500 | 130.78 | 80.16 |
| 8/13/2013 12:06:19 PM | 1.10528 | 132.05 | 80.11 |
| 8/13/2013 12:06:20 PM | 1.10556 | 127.58 | 80.06 |
| 8/13/2013 12:06:21 PM | 1.10583 | 131.50 | 80.01 |
| 8/13/2013 12:06:22 PM | 1.10611 | 126.86 | 79.95 |
| 8/13/2013 12:06:23 PM | 1.10639 | 133.66 | 79.91 |
| 8/13/2013 12:06:24 PM | 1.10667 | 130.59 | 79.85 |
| 8/13/2013 12:06:25 PM | 1.10694 | 137.90 | 79.80 |
| 8/13/2013 12:06:26 PM | 1.10722 | 139.22 | 79.75 |
| 8/13/2013 12:06:27 PM | 1.10750 | 144.41 | 79.71 |
| 8/13/2013 12:06:28 PM | 1.10778 | 147.75 | 79.66 |
| 8/13/2013 12:06:29 PM | 1.10806 | 151.85 | 79.62 |
| 8/13/2013 12:06:30 PM | 1.10833 | 156.58 | 79.58 |
| 8/13/2013 12:06:31 PM | 1.10861 | 159.15 | 79.54 |
| 8/13/2013 12:06:32 PM | 1.10889 | 164.90 | 79.51 |
| 8/13/2013 12:06:33 PM | 1.10917 | 167.64 | 79.47 |
| 8/13/2013 12:06:34 PM | 1.10944 | 174.52 | 79.44 |
| 8/13/2013 12:06:35 PM | 1.10972 | 178.78 | 79.41 |
| 8/13/2013 12:06:36 PM | 1.11000 | 186.52 | 79.38 |
| 8/13/2013 12:06:37 PM | 1.11028 | 191.54 | 79.35 |
| 8/13/2013 12:06:38 PM | 1.11056 | 197.91 | 79.33 |
| 8/13/2013 12:06:39 PM | 1.11083 | 203.71 | 79.30 |
| 8/13/2013 12:06:40 PM | 1.11111 | 209.06 | 79.28 |
| 8/13/2013 12:06:41 PM | 1.11139 | 215.94 | 79.26 |
| 8/13/2013 12:06:42 PM | 1.11167 | 219.88 | 79.24 |
| 8/13/2013 12:06:43 PM | 1.11194 | 227.94 | 79.22 |
| 8/13/2013 12:06:44 PM | 1.11222 | 230.74 | 79.20 |
| 8/13/2013 12:06:45 PM | 1.11250 | 233.34 | 79.19 |
| 8/13/2013 12:06:46 PM | 1.11278 | 229.49 | 79.17 |
| 8/13/2013 12:06:47 PM | 1.11306 | 232.74 | 79.16 |
| 8/13/2013 12:06:48 PM | 1.11333 | 228.91 | 79.14 |
| 8/13/2013 12:06:49 PM | 1.11361 | 232.51 | 79.13 |
| 8/13/2013 12:06:50 PM | 1.11389 | 229.25 | 79.12 |
| 8/13/2013 12:06:51 PM | 1.11417 | 230.73 | 79.11 |
| 8/13/2013 12:06:52 PM | 1.11444 | 229.54 | 79.11 |
| 8/13/2013 12:06:53 PM | 1.11472 | 229.35 | 79.10 |
| 8/13/2013 12:06:54 PM | 1.11500 | 229.25 | 79.09 |
| 8/13/2013 12:06:55 PM | 1.11528 | 228.17 | 79.09 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:06:56 PM | 1.11556 | 229.11 | 79.08 |
| 8/13/2013 12:06:57 PM | 1.11583 | 227.72 | 79.08 |
| 8/13/2013 12:06:58 PM | 1.11611 | 228.58 | 79.08 |
| 8/13/2013 12:06:59 PM | 1.11639 | 227.35 | 79.08 |
| 8/13/2013 12:07:00 PM | 1.11667 | 227.80 | 79.08 |
| 8/13/2013 12:07:01 PM | 1.11694 | 227.27 | 79.08 |
| 8/13/2013 12:07:02 PM | 1.11722 | 227.01 | 79.08 |
| 8/13/2013 12:07:03 PM | 1.11750 | 227.15 | 79.08 |
| 8/13/2013 12:07:04 PM | 1.11778 | 226.26 | 79.08 |
| 8/13/2013 12:07:05 PM | 1.11806 | 227.12 | 79.08 |
| 8/13/2013 12:07:06 PM | 1.11833 | 225.61 | 79.08 |
| 8/13/2013 12:07:07 PM | 1.11861 | 226.47 | 79.09 |
| 8/13/2013 12:07:08 PM | 1.11889 | 224.15 | 79.08 |
| 8/13/2013 12:07:09 PM | 1.11917 | 225.77 | 79.09 |
| 8/13/2013 12:07:10 PM | 1.11944 | 200.24 | 79.08 |
| 8/13/2013 12:07:11 PM | 1.11972 | 168.15 | 79.05 |
| 8/13/2013 12:07:12 PM | 1.12000 | 121.03 | 79.03 |
| 8/13/2013 12:07:13 PM | 1.12028 | 90.55 | 79.02 |
| 8/13/2013 12:07:14 PM | 1.12056 | 68.64 | 79.02 |
| 8/13/2013 12:07:15 PM | 1.12083 | 55.93 | 79.02 |
| 8/13/2013 12:07:16 PM | 1.12111 | 47.01 | 79.02 |
| 8/13/2013 12:07:17 PM | 1.12139 | 33.01 | 79.03 |
| 8/13/2013 12:07:18 PM | 1.12167 | 24.37 | 79.03 |
| 8/13/2013 12:07:19 PM | 1.12194 | 17.75 | 79.04 |
| 8/13/2013 12:07:20 PM | 1.12222 | 15.66 | 79.04 |
| 8/13/2013 12:07:21 PM | 1.12250 | 14.72 | 79.05 |
| 8/13/2013 12:07:22 PM | 1.12278 | 14.50 | 79.06 |
| 8/13/2013 12:07:23 PM | 1.12306 | 14.44 | 79.06 |
| 8/13/2013 12:07:24 PM | 1.12333 | 14.39 | 79.07 |
| 8/13/2013 12:07:25 PM | 1.12361 | 14.38 | 79.07 |
| 8/13/2013 12:07:26 PM | 1.12389 | 14.35 | 79.07 |
| 8/13/2013 12:07:27 PM | 1.12417 | 14.35 | 79.07 |
| 8/13/2013 12:07:28 PM | 1.12444 | 14.32 | 79.06 |
| 8/13/2013 12:07:29 PM | 1.12472 | 14.30 | 79.06 |
| 8/13/2013 12:07:30 PM | 1.12500 | 14.30 | 79.06 |
| 8/13/2013 12:07:31 PM | 1.12528 | 14.30 | 79.06 |
| 8/13/2013 12:07:32 PM | 1.12556 | 14.30 | 79.06 |
| 8/13/2013 12:07:33 PM | 1.12583 | 14.29 | 79.05 |
| 8/13/2013 12:07:34 PM | 1.12611 | 14.29 | 79.05 |
| 8/13/2013 12:07:35 PM | 1.12639 | 14.29 | 79.05 |
| 8/13/2013 12:07:36 PM | 1.12667 | 14.29 | 79.04 |
| 8/13/2013 12:07:37 PM | 1.12694 | 14.29 | 79.03 |
| 8/13/2013 12:07:38 PM | 1.12722 | 14.29 | 79.03 |
| 8/13/2013 12:07:39 PM | 1.12750 | 14.29 | 79.03 |
| 8/13/2013 12:07:40 PM | 1.12778 | 14.29 | 79.02 |
| 8/13/2013 12:07:41 PM | 1.12806 | 14.29 | 79.02 |
| 8/13/2013 12:07:42 PM | 1.12833 | 14.29 | 79.01 |
| 8/13/2013 12:07:43 PM | 1.12861 | 14.29 | 79.01 |
| 8/13/2013 12:07:44 PM | 1.12889 | 14.29 | 79.00 |
| 8/13/2013 12:07:45 PM | 1.12917 | 14.29 | 79.00 |
| 8/13/2013 12:07:46 PM | 1.12944 | 14.29 | 78.99 |
| 8/13/2013 12:07:47 PM | 1.12972 | 14.29 | 78.99 |
| 8/13/2013 12:07:48 PM | 1.13000 | 14.29 | 78.98 |
| 8/13/2013 12:07:49 PM | 1.13028 | 14.29 | 78.98 |
| 8/13/2013 12:07:50 PM | 1.13056 | 14.29 | 78.98 |
| 8/13/2013 12:07:51 PM | 1.13083 | 14.30 | 78.98 |
| 8/13/2013 12:07:52 PM | 1.13111 | 14.30 | 78.97 |
| 8/13/2013 12:07:53 PM | 1.13139 | 14.30 | 78.97 |
| 8/13/2013 12:07:54 PM | 1.13167 | 14.30 | 78.97 |
| 8/13/2013 12:07:55 PM | 1.13194 | 14.30 | 78.97 |
| 8/13/2013 12:07:56 PM | 1.13222 | 14.30 | 78.97 |
| 8/13/2013 12:07:57 PM | 1.13250 | 14.30 | 78.96 |
| 8/13/2013 12:07:58 PM | 1.13278 | 14.30 | 78.96 |
| 8/13/2013 12:07:59 PM | 1.13306 | 14.30 | 78.96 |
| 8/13/2013 12:08:00 PM | 1.13333 | 14.30 | 78.96 |
| 8/13/2013 12:08:01 PM | 1.13361 | 14.30 | 78.96 |
| 8/13/2013 12:08:02 PM | 1.13389 | 14.30 | 78.96 |
| 8/13/2013 12:08:03 PM | 1.13417 | 14.30 | 78.96 |
| 8/13/2013 12:08:04 PM | 1.13444 | 14.30 | 78.96 |
| 8/13/2013 12:08:05 PM | 1.13472 | 14.30 | 78.96 |
| 8/13/2013 12:08:06 PM | 1.13500 | 14.30 | 78.96 |
| 8/13/2013 12:08:07 PM | 1.13528 | 14.30 | 78.96 |
| 8/13/2013 12:08:08 PM | 1.13556 | 14.30 | 78.96 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:08:09 PM | 1.13583 | 14.30 | 78.96 |
| 8/13/2013 12:08:10 PM | 1.13611 | 14.30 | 78.96 |
| 8/13/2013 12:08:11 PM | 1.13639 | 14.30 | 78.96 |
| 8/13/2013 12:08:12 PM | 1.13667 | 14.30 | 78.96 |
| 8/13/2013 12:08:13 PM | 1.13694 | 14.30 | 78.96 |
| 8/13/2013 12:08:14 PM | 1.13722 | 14.30 | 78.96 |
| 8/13/2013 12:08:15 PM | 1.13750 | 14.30 | 78.96 |
| 8/13/2013 12:08:16 PM | 1.13778 | 14.30 | 78.96 |
| 8/13/2013 12:08:17 PM | 1.13806 | 14.30 | 78.96 |
| 8/13/2013 12:08:18 PM | 1.13833 | 14.30 | 78.96 |
| 8/13/2013 12:08:19 PM | 1.13861 | 14.30 | 78.96 |
| 8/13/2013 12:08:20 PM | 1.13889 | 14.30 | 78.96 |
| 8/13/2013 12:08:21 PM | 1.13917 | 14.30 | 78.96 |
| 8/13/2013 12:08:22 PM | 1.13944 | 14.30 | 78.97 |
| 8/13/2013 12:08:23 PM | 1.13972 | 14.30 | 78.97 |
| 8/13/2013 12:08:24 PM | 1.14000 | 14.30 | 78.97 |
| 8/13/2013 12:08:25 PM | 1.14028 | 14.30 | 78.97 |
| 8/13/2013 12:08:26 PM | 1.14056 | 14.30 | 78.97 |
| 8/13/2013 12:08:27 PM | 1.14083 | 14.30 | 78.97 |
| 8/13/2013 12:08:28 PM | 1.14111 | 14.30 | 78.97 |
| 8/13/2013 12:08:29 PM | 1.14139 | 14.30 | 78.97 |
| 8/13/2013 12:08:30 PM | 1.14167 | 14.30 | 78.97 |
| 8/13/2013 12:08:31 PM | 1.14194 | 14.30 | 78.97 |
| 8/13/2013 12:08:32 PM | 1.14222 | 14.30 | 78.97 |
| 8/13/2013 12:08:33 PM | 1.14250 | 14.30 | 78.97 |
| 8/13/2013 12:08:34 PM | 1.14278 | 14.30 | 78.97 |
| 8/13/2013 12:08:35 PM | 1.14306 | 14.30 | 78.98 |
| 8/13/2013 12:08:36 PM | 1.14333 | 14.30 | 78.98 |
| 8/13/2013 12:08:37 PM | 1.14361 | 14.30 | 78.98 |
| 8/13/2013 12:08:38 PM | 1.14389 | 14.30 | 78.98 |
| 8/13/2013 12:08:39 PM | 1.14417 | 14.30 | 78.98 |
| 8/13/2013 12:08:40 PM | 1.14444 | 14.30 | 78.98 |
| 8/13/2013 12:08:41 PM | 1.14472 | 14.30 | 78.98 |
| 8/13/2013 12:08:42 PM | 1.14500 | 14.30 | 78.98 |
| 8/13/2013 12:08:43 PM | 1.14528 | 14.30 | 78.98 |
| 8/13/2013 12:08:44 PM | 1.14556 | 14.30 | 78.98 |
| 8/13/2013 12:08:45 PM | 1.14583 | 14.30 | 78.98 |
| 8/13/2013 12:08:46 PM | 1.14611 | 14.30 | 78.98 |
| 8/13/2013 12:08:47 PM | 1.14639 | 14.30 | 78.98 |
| 8/13/2013 12:08:48 PM | 1.14667 | 14.30 | 78.98 |
| 8/13/2013 12:08:49 PM | 1.14694 | 14.30 | 78.99 |
| 8/13/2013 12:08:50 PM | 1.14722 | 14.30 | 78.99 |
| 8/13/2013 12:08:51 PM | 1.14750 | 14.30 | 78.99 |
| 8/13/2013 12:08:52 PM | 1.14778 | 14.30 | 78.99 |
| 8/13/2013 12:08:53 PM | 1.14806 | 14.30 | 78.99 |
| 8/13/2013 12:08:54 PM | 1.14833 | 14.30 | 78.99 |
| 8/13/2013 12:08:55 PM | 1.14861 | 14.30 | 78.99 |
| 8/13/2013 12:08:56 PM | 1.14889 | 14.30 | 78.99 |
| 8/13/2013 12:08:57 PM | 1.14917 | 14.30 | 78.99 |
| 8/13/2013 12:08:58 PM | 1.14944 | 14.30 | 78.99 |
| 8/13/2013 12:08:59 PM | 1.14972 | 14.30 | 78.99 |
| 8/13/2013 12:09:00 PM | 1.15000 | 14.30 | 79.00 |
| 8/13/2013 12:09:01 PM | 1.15028 | 14.30 | 79.00 |
| 8/13/2013 12:09:02 PM | 1.15056 | 14.30 | 79.00 |
| 8/13/2013 12:09:03 PM | 1.15083 | 14.30 | 79.00 |
| 8/13/2013 12:09:04 PM | 1.15111 | 14.30 | 79.00 |
| 8/13/2013 12:09:05 PM | 1.15139 | 14.30 | 79.00 |
| 8/13/2013 12:09:06 PM | 1.15167 | 14.30 | 79.00 |
| 8/13/2013 12:09:07 PM | 1.15194 | 14.30 | 79.00 |
| 8/13/2013 12:09:08 PM | 1.15222 | 14.30 | 79.00 |
| 8/13/2013 12:09:09 PM | 1.15250 | 14.30 | 79.00 |
| 8/13/2013 12:09:10 PM | 1.15278 | 14.30 | 79.00 |
| 8/13/2013 12:09:11 PM | 1.15306 | 14.30 | 79.00 |
| 8/13/2013 12:09:12 PM | 1.15333 | 14.30 | 79.00 |
| 8/13/2013 12:09:13 PM | 1.15361 | 14.30 | 79.00 |
| 8/13/2013 12:09:14 PM | 1.15389 | 14.30 | 79.01 |
| 8/13/2013 12:09:15 PM | 1.15417 | 14.30 | 79.01 |
| 8/13/2013 12:09:16 PM | 1.15444 | 14.30 | 79.01 |
| 8/13/2013 12:09:17 PM | 1.15472 | 14.30 | 79.01 |
| 8/13/2013 12:09:18 PM | 1.15500 | 14.30 | 79.01 |
| 8/13/2013 12:09:19 PM | 1.15528 | 14.30 | 79.01 |
| 8/13/2013 12:09:20 PM | 1.15556 | 14.30 | 79.01 |
| 8/13/2013 12:09:21 PM | 1.15583 | 14.30 | 79.01 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:09:22 PM | 1.15611 | 14.30 | 79.01 |
| 8/13/2013 12:09:23 PM | 1.15639 | 14.30 | 79.01 |
| 8/13/2013 12:09:24 PM | 1.15667 | 14.30 | 79.01 |
| 8/13/2013 12:09:25 PM | 1.15694 | 14.30 | 79.01 |
| 8/13/2013 12:09:26 PM | 1.15722 | 14.30 | 79.01 |
| 8/13/2013 12:09:27 PM | 1.15750 | 14.30 | 79.02 |
| 8/13/2013 12:09:28 PM | 1.15778 | 14.30 | 79.02 |
| 8/13/2013 12:09:29 PM | 1.15806 | 14.30 | 79.02 |
| 8/13/2013 12:09:30 PM | 1.15833 | 14.30 | 79.02 |
| 8/13/2013 12:09:31 PM | 1.15861 | 14.30 | 79.02 |
| 8/13/2013 12:09:32 PM | 1.15889 | 14.30 | 79.02 |
| 8/13/2013 12:09:33 PM | 1.15917 | 14.30 | 79.02 |
| 8/13/2013 12:09:34 PM | 1.15944 | 14.30 | 79.02 |
| 8/13/2013 12:09:35 PM | 1.15972 | 14.30 | 79.02 |
| 8/13/2013 12:09:36 PM | 1.16000 | 14.30 | 79.02 |
| 8/13/2013 12:09:37 PM | 1.16028 | 14.30 | 79.02 |
| 8/13/2013 12:09:38 PM | 1.16056 | 14.30 | 79.02 |
| 8/13/2013 12:09:39 PM | 1.16083 | 14.30 | 79.02 |
| 8/13/2013 12:09:40 PM | 1.16111 | 14.30 | 79.02 |
| 8/13/2013 12:09:41 PM | 1.16139 | 14.30 | 79.03 |
| 8/13/2013 12:09:42 PM | 1.16167 | 14.30 | 79.03 |
| 8/13/2013 12:09:43 PM | 1.16194 | 14.30 | 79.03 |
| 8/13/2013 12:09:44 PM | 1.16222 | 14.30 | 79.03 |
| 8/13/2013 12:09:45 PM | 1.16250 | 14.30 | 79.03 |
| 8/13/2013 12:09:46 PM | 1.16278 | 14.30 | 79.03 |
| 8/13/2013 12:09:47 PM | 1.16306 | 14.30 | 79.03 |
| 8/13/2013 12:09:48 PM | 1.16333 | 14.30 | 79.03 |
| 8/13/2013 12:09:49 PM | 1.16361 | 14.30 | 79.03 |
| 8/13/2013 12:09:50 PM | 1.16389 | 14.30 | 79.03 |
| 8/13/2013 12:09:51 PM | 1.16417 | 14.30 | 79.03 |
| 8/13/2013 12:09:52 PM | 1.16444 | 14.30 | 79.03 |
| 8/13/2013 12:09:53 PM | 1.16472 | 14.30 | 79.03 |
| 8/13/2013 12:09:54 PM | 1.16500 | 14.30 | 79.03 |
| 8/13/2013 12:09:55 PM | 1.16528 | 14.30 | 79.03 |
| 8/13/2013 12:09:56 PM | 1.16556 | 14.30 | 79.03 |
| 8/13/2013 12:09:57 PM | 1.16583 | 14.30 | 79.03 |
| 8/13/2013 12:09:58 PM | 1.16611 | 14.30 | 79.04 |
| 8/13/2013 12:09:59 PM | 1.16639 | 14.30 | 79.04 |
| 8/13/2013 12:10:00 PM | 1.16667 | 14.30 | 79.04 |
| 8/13/2013 12:10:01 PM | 1.16694 | 14.30 | 79.04 |
| 8/13/2013 12:10:02 PM | 1.16722 | 14.30 | 79.04 |
| 8/13/2013 12:10:03 PM | 1.16750 | 14.30 | 79.04 |
| 8/13/2013 12:10:04 PM | 1.16778 | 14.30 | 79.04 |
| 8/13/2013 12:10:05 PM | 1.16806 | 14.30 | 79.04 |
| 8/13/2013 12:10:06 PM | 1.16833 | 14.30 | 79.04 |
| 8/13/2013 12:10:07 PM | 1.16861 | 14.30 | 79.04 |
| 8/13/2013 12:10:08 PM | 1.16889 | 14.30 | 79.04 |
| 8/13/2013 12:10:09 PM | 1.16917 | 14.30 | 79.04 |
| 8/13/2013 12:10:10 PM | 1.16944 | 14.30 | 79.04 |
| 8/13/2013 12:10:11 PM | 1.16972 | 14.30 | 79.04 |
| 8/13/2013 12:10:12 PM | 1.17000 | 14.30 | 79.05 |
| 8/13/2013 12:10:13 PM | 1.17028 | 14.30 | 79.05 |
| 8/13/2013 12:10:14 PM | 1.17056 | 14.30 | 79.05 |
| 8/13/2013 12:10:15 PM | 1.17083 | 14.30 | 79.05 |
| 8/13/2013 12:10:16 PM | 1.17111 | 14.30 | 79.05 |
| 8/13/2013 12:10:17 PM | 1.17139 | 14.30 | 79.05 |
| 8/13/2013 12:10:18 PM | 1.17167 | 14.30 | 79.05 |
| 8/13/2013 12:10:19 PM | 1.17194 | 14.30 | 79.05 |
| 8/13/2013 12:10:20 PM | 1.17222 | 14.30 | 79.05 |
| 8/13/2013 12:10:21 PM | 1.17250 | 14.30 | 79.05 |
| 8/13/2013 12:10:22 PM | 1.17278 | 14.30 | 79.05 |
| 8/13/2013 12:10:23 PM | 1.17306 | 14.30 | 79.05 |
| 8/13/2013 12:10:24 PM | 1.17333 | 14.30 | 79.05 |
| 8/13/2013 12:10:25 PM | 1.17361 | 14.30 | 79.05 |
| 8/13/2013 12:10:26 PM | 1.17389 | 14.30 | 79.05 |
| 8/13/2013 12:10:27 PM | 1.17417 | 14.30 | 79.05 |
| 8/13/2013 12:10:28 PM | 1.17444 | 14.30 | 79.05 |
| 8/13/2013 12:10:29 PM | 1.17472 | 14.30 | 79.06 |
| 8/13/2013 12:10:30 PM | 1.17500 | 14.30 | 79.06 |
| 8/13/2013 12:10:31 PM | 1.17528 | 14.30 | 79.06 |
| 8/13/2013 12:10:32 PM | 1.17556 | 14.30 | 79.06 |
| 8/13/2013 12:10:33 PM | 1.17583 | 14.30 | 79.06 |
| 8/13/2013 12:10:34 PM | 1.17611 | 14.30 | 79.06 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:10:35 PM | 1.17639 | 14.30 | 79.06 |
| 8/13/2013 12:10:36 PM | 1.17667 | 14.30 | 79.06 |
| 8/13/2013 12:10:37 PM | 1.17694 | 14.30 | 79.06 |
| 8/13/2013 12:10:38 PM | 1.17722 | 14.30 | 79.06 |
| 8/13/2013 12:10:39 PM | 1.17750 | 14.30 | 79.06 |
| 8/13/2013 12:10:40 PM | 1.17778 | 14.30 | 79.06 |
| 8/13/2013 12:10:41 PM | 1.17806 | 14.30 | 79.06 |
| 8/13/2013 12:10:42 PM | 1.17833 | 14.30 | 79.06 |
| 8/13/2013 12:10:43 PM | 1.17861 | 14.30 | 79.06 |
| 8/13/2013 12:10:44 PM | 1.17889 | 14.30 | 79.06 |
| 8/13/2013 12:10:45 PM | 1.17917 | 14.30 | 79.06 |
| 8/13/2013 12:10:46 PM | 1.17944 | 14.30 | 79.06 |
| 8/13/2013 12:10:47 PM | 1.17972 | 14.30 | 79.06 |
| 8/13/2013 12:10:48 PM | 1.18000 | 14.30 | 79.07 |
| 8/13/2013 12:10:49 PM | 1.18028 | 14.30 | 79.07 |
| 8/13/2013 12:10:50 PM | 1.18056 | 14.30 | 79.07 |
| 8/13/2013 12:10:51 PM | 1.18083 | 14.30 | 79.07 |
| 8/13/2013 12:10:52 PM | 1.18111 | 14.30 | 79.07 |
| 8/13/2013 12:10:53 PM | 1.18139 | 14.30 | 79.07 |
| 8/13/2013 12:10:54 PM | 1.18167 | 14.30 | 79.07 |
| 8/13/2013 12:10:55 PM | 1.18194 | 14.30 | 79.07 |
| 8/13/2013 12:10:56 PM | 1.18222 | 14.30 | 79.07 |
| 8/13/2013 12:10:57 PM | 1.18250 | 14.30 | 79.07 |
| 8/13/2013 12:10:58 PM | 1.18278 | 14.30 | 79.07 |
| 8/13/2013 12:10:59 PM | 1.18306 | 14.30 | 79.07 |
| 8/13/2013 12:11:00 PM | 1.18333 | 14.30 | 79.07 |
| 8/13/2013 12:11:01 PM | 1.18361 | 14.30 | 79.08 |
| 8/13/2013 12:11:02 PM | 1.18389 | 14.30 | 79.08 |
| 8/13/2013 12:11:03 PM | 1.18417 | 14.30 | 79.08 |
| 8/13/2013 12:11:04 PM | 1.18444 | 14.30 | 79.08 |
| 8/13/2013 12:11:05 PM | 1.18472 | 14.30 | 79.08 |
| 8/13/2013 12:11:06 PM | 1.18500 | 14.30 | 79.08 |
| 8/13/2013 12:11:07 PM | 1.18528 | 14.30 | 79.08 |
| 8/13/2013 12:11:08 PM | 1.18556 | 14.30 | 79.08 |
| 8/13/2013 12:11:09 PM | 1.18583 | 14.30 | 79.08 |
| 8/13/2013 12:11:10 PM | 1.18611 | 14.30 | 79.08 |
| 8/13/2013 12:11:11 PM | 1.18639 | 14.30 | 79.08 |
| 8/13/2013 12:11:12 PM | 1.18667 | 14.30 | 79.08 |
| 8/13/2013 12:11:13 PM | 1.18694 | 14.30 | 79.08 |
| 8/13/2013 12:11:14 PM | 1.18722 | 14.30 | 79.08 |
| 8/13/2013 12:11:15 PM | 1.18750 | 14.30 | 79.08 |
| 8/13/2013 12:11:16 PM | 1.18778 | 14.30 | 79.08 |
| 8/13/2013 12:11:17 PM | 1.18806 | 14.30 | 79.08 |
| 8/13/2013 12:11:18 PM | 1.18833 | 14.30 | 79.08 |
| 8/13/2013 12:11:19 PM | 1.18861 | 14.30 | 79.08 |
| 8/13/2013 12:11:20 PM | 1.18889 | 14.30 | 79.09 |
| 8/13/2013 12:11:21 PM | 1.18917 | 14.30 | 79.09 |
| 8/13/2013 12:11:22 PM | 1.18944 | 14.30 | 79.09 |
| 8/13/2013 12:11:23 PM | 1.18972 | 14.30 | 79.09 |
| 8/13/2013 12:11:24 PM | 1.19000 | 14.30 | 79.09 |
| 8/13/2013 12:11:25 PM | 1.19028 | 14.30 | 79.09 |
| 8/13/2013 12:11:26 PM | 1.19056 | 14.30 | 79.09 |
| 8/13/2013 12:11:27 PM | 1.19083 | 14.30 | 79.09 |
| 8/13/2013 12:11:28 PM | 1.19111 | 14.30 | 79.09 |
| 8/13/2013 12:11:29 PM | 1.19139 | 14.30 | 79.09 |
| 8/13/2013 12:11:30 PM | 1.19167 | 14.30 | 79.09 |
| 8/13/2013 12:11:31 PM | 1.19194 | 14.30 | 79.09 |
| 8/13/2013 12:11:32 PM | 1.19222 | 14.30 | 79.09 |
| 8/13/2013 12:11:33 PM | 1.19250 | 14.30 | 79.09 |
| 8/13/2013 12:11:34 PM | 1.19278 | 14.30 | 79.09 |
| 8/13/2013 12:11:35 PM | 1.19306 | 14.30 | 79.09 |
| 8/13/2013 12:11:36 PM | 1.19333 | 14.30 | 79.09 |
| 8/13/2013 12:11:37 PM | 1.19361 | 14.30 | 79.09 |
| 8/13/2013 12:11:38 PM | 1.19389 | 14.30 | 79.10 |
| 8/13/2013 12:11:39 PM | 1.19417 | 14.30 | 79.10 |
| 8/13/2013 12:11:40 PM | 1.19444 | 14.30 | 79.10 |
| 8/13/2013 12:11:41 PM | 1.19472 | 14.30 | 79.10 |
| 8/13/2013 12:11:42 PM | 1.19500 | 14.30 | 79.10 |
| 8/13/2013 12:11:43 PM | 1.19528 | 14.30 | 79.10 |
| 8/13/2013 12:11:44 PM | 1.19556 | 14.30 | 79.10 |
| 8/13/2013 12:11:45 PM | 1.19583 | 14.30 | 79.10 |
| 8/13/2013 12:11:46 PM | 1.19611 | 14.30 | 79.10 |
| 8/13/2013 12:11:47 PM | 1.19639 | 14.30 | 79.10 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:11:48 PM | 1.19667 | 14.30 | 79.10 |
| 8/13/2013 12:11:49 PM | 1.19694 | 14.30 | 79.10 |
| 8/13/2013 12:11:50 PM | 1.19722 | 14.30 | 79.10 |
| 8/13/2013 12:11:51 PM | 1.19750 | 14.30 | 79.10 |
| 8/13/2013 12:11:52 PM | 1.19778 | 14.30 | 79.10 |
| 8/13/2013 12:11:53 PM | 1.19806 | 14.30 | 79.10 |
| 8/13/2013 12:11:54 PM | 1.19833 | 14.30 | 79.10 |
| 8/13/2013 12:11:55 PM | 1.19861 | 14.30 | 79.10 |
| 8/13/2013 12:11:56 PM | 1.19889 | 14.30 | 79.11 |
| 8/13/2013 12:11:57 PM | 1.19917 | 14.30 | 79.11 |
| 8/13/2013 12:11:58 PM | 1.19944 | 14.30 | 79.11 |
| 8/13/2013 12:11:59 PM | 1.19972 | 14.30 | 79.11 |
| 8/13/2013 12:12:00 PM | 1.20000 | 14.30 | 79.11 |
| 8/13/2013 12:12:01 PM | 1.20028 | 14.30 | 79.11 |
| 8/13/2013 12:12:02 PM | 1.20056 | 14.30 | 79.11 |
| 8/13/2013 12:12:03 PM | 1.20083 | 14.30 | 79.11 |
| 8/13/2013 12:12:04 PM | 1.20111 | 14.30 | 79.11 |
| 8/13/2013 12:12:05 PM | 1.20139 | 14.30 | 79.11 |
| 8/13/2013 12:12:06 PM | 1.20167 | 14.30 | 79.11 |
| 8/13/2013 12:12:07 PM | 1.20194 | 14.30 | 79.11 |
| 8/13/2013 12:12:08 PM | 1.20222 | 14.30 | 79.11 |
| 8/13/2013 12:12:09 PM | 1.20250 | 14.30 | 79.11 |
| 8/13/2013 12:12:10 PM | 1.20278 | 14.30 | 79.11 |
| 8/13/2013 12:12:11 PM | 1.20306 | 14.30 | 79.11 |
| 8/13/2013 12:12:12 PM | 1.20333 | 14.30 | 79.11 |
| 8/13/2013 12:12:13 PM | 1.20361 | 14.30 | 79.11 |
| 8/13/2013 12:12:14 PM | 1.20389 | 14.30 | 79.11 |
| 8/13/2013 12:12:15 PM | 1.20417 | 14.30 | 79.11 |
| 8/13/2013 12:12:16 PM | 1.20444 | 14.30 | 79.11 |
| 8/13/2013 12:12:17 PM | 1.20472 | 14.30 | 79.11 |
| 8/13/2013 12:12:18 PM | 1.20500 | 14.30 | 79.12 |
| 8/13/2013 12:12:19 PM | 1.20528 | 14.30 | 79.12 |
| 8/13/2013 12:12:20 PM | 1.20556 | 14.30 | 79.12 |
| 8/13/2013 12:12:21 PM | 1.20583 | 14.30 | 79.12 |
| 8/13/2013 12:12:22 PM | 1.20611 | 14.30 | 79.12 |
| 8/13/2013 12:12:23 PM | 1.20639 | 14.30 | 79.12 |
| 8/13/2013 12:12:24 PM | 1.20667 | 14.30 | 79.12 |
| 8/13/2013 12:12:25 PM | 1.20694 | 14.30 | 79.12 |
| 8/13/2013 12:12:26 PM | 1.20722 | 14.30 | 79.12 |
| 8/13/2013 12:12:27 PM | 1.20750 | 14.30 | 79.12 |
| 8/13/2013 12:12:28 PM | 1.20778 | 14.30 | 79.12 |
| 8/13/2013 12:12:29 PM | 1.20806 | 14.30 | 79.12 |
| 8/13/2013 12:12:30 PM | 1.20833 | 14.30 | 79.12 |
| 8/13/2013 12:12:31 PM | 1.20861 | 14.30 | 79.12 |
| 8/13/2013 12:12:32 PM | 1.20889 | 14.30 | 79.12 |
| 8/13/2013 12:12:33 PM | 1.20917 | 14.30 | 79.12 |
| 8/13/2013 12:12:34 PM | 1.20944 | 14.30 | 79.12 |
| 8/13/2013 12:12:35 PM | 1.20972 | 14.30 | 79.12 |
| 8/13/2013 12:12:36 PM | 1.21000 | 14.30 | 79.12 |
| 8/13/2013 12:12:37 PM | 1.21028 | 14.30 | 79.12 |
| 8/13/2013 12:12:38 PM | 1.21056 | 14.30 | 79.13 |
| 8/13/2013 12:12:39 PM | 1.21083 | 14.30 | 79.13 |
| 8/13/2013 12:12:40 PM | 1.21111 | 14.30 | 79.13 |
| 8/13/2013 12:12:41 PM | 1.21139 | 14.30 | 79.13 |
| 8/13/2013 12:12:42 PM | 1.21167 | 14.30 | 79.13 |
| 8/13/2013 12:12:43 PM | 1.21194 | 14.30 | 79.13 |
| 8/13/2013 12:12:44 PM | 1.21222 | 14.30 | 79.13 |
| 8/13/2013 12:12:45 PM | 1.21250 | 14.30 | 79.13 |
| 8/13/2013 12:12:46 PM | 1.21278 | 14.30 | 79.13 |
| 8/13/2013 12:12:47 PM | 1.21306 | 14.30 | 79.13 |
| 8/13/2013 12:12:48 PM | 1.21333 | 14.30 | 79.13 |
| 8/13/2013 12:12:49 PM | 1.21361 | 14.30 | 79.13 |
| 8/13/2013 12:12:50 PM | 1.21389 | 14.30 | 79.13 |
| 8/13/2013 12:12:51 PM | 1.21417 | 14.30 | 79.13 |
| 8/13/2013 12:12:52 PM | 1.21444 | 14.30 | 79.13 |
| 8/13/2013 12:12:53 PM | 1.21472 | 14.30 | 79.13 |
| 8/13/2013 12:12:54 PM | 1.21500 | 14.30 | 79.13 |
| 8/13/2013 12:12:55 PM | 1.21528 | 14.30 | 79.13 |
| 8/13/2013 12:12:56 PM | 1.21556 | 14.30 | 79.13 |
| 8/13/2013 12:12:57 PM | 1.21583 | 14.30 | 79.13 |
| 8/13/2013 12:12:58 PM | 1.21611 | 14.30 | 79.13 |
| 8/13/2013 12:12:59 PM | 1.21639 | 14.30 | 79.13 |
| 8/13/2013 12:13:00 PM | 1.21667 | 14.30 | 79.14 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:13:01 PM | 1.21694 | 14.30 | 79.14 |
| 8/13/2013 12:13:02 PM | 1.21722 | 14.30 | 79.14 |
| 8/13/2013 12:13:03 PM | 1.21750 | 14.30 | 79.14 |
| 8/13/2013 12:13:04 PM | 1.21778 | 14.30 | 79.14 |
| 8/13/2013 12:13:05 PM | 1.21806 | 14.30 | 79.14 |
| 8/13/2013 12:13:06 PM | 1.21833 | 14.30 | 79.14 |
| 8/13/2013 12:13:07 PM | 1.21861 | 14.30 | 79.14 |
| 8/13/2013 12:13:08 PM | 1.21889 | 14.30 | 79.14 |
| 8/13/2013 12:13:09 PM | 1.21917 | 14.30 | 79.14 |
| 8/13/2013 12:13:10 PM | 1.21944 | 14.30 | 79.14 |
| 8/13/2013 12:13:11 PM | 1.21972 | 14.30 | 79.14 |
| 8/13/2013 12:13:12 PM | 1.22000 | 14.30 | 79.14 |
| 8/13/2013 12:13:13 PM | 1.22028 | 14.30 | 79.14 |
| 8/13/2013 12:13:14 PM | 1.22056 | 14.30 | 79.14 |
| 8/13/2013 12:13:15 PM | 1.22083 | 14.30 | 79.14 |
| 8/13/2013 12:13:16 PM | 1.22111 | 14.30 | 79.14 |
| 8/13/2013 12:13:17 PM | 1.22139 | 14.30 | 79.14 |
| 8/13/2013 12:13:18 PM | 1.22167 | 14.30 | 79.14 |
| 8/13/2013 12:13:19 PM | 1.22194 | 14.30 | 79.14 |
| 8/13/2013 12:13:20 PM | 1.22222 | 14.30 | 79.14 |
| 8/13/2013 12:13:21 PM | 1.22250 | 14.30 | 79.14 |
| 8/13/2013 12:13:22 PM | 1.22278 | 14.30 | 79.14 |
| 8/13/2013 12:13:23 PM | 1.22306 | 14.30 | 79.14 |
| 8/13/2013 12:13:24 PM | 1.22333 | 14.30 | 79.15 |
| 8/13/2013 12:13:25 PM | 1.22361 | 14.30 | 79.15 |
| 8/13/2013 12:13:26 PM | 1.22389 | 14.30 | 79.15 |
| 8/13/2013 12:13:27 PM | 1.22417 | 14.30 | 79.15 |
| 8/13/2013 12:13:28 PM | 1.22444 | 14.30 | 79.15 |
| 8/13/2013 12:13:29 PM | 1.22472 | 14.30 | 79.15 |
| 8/13/2013 12:13:30 PM | 1.22500 | 14.30 | 79.15 |
| 8/13/2013 12:13:31 PM | 1.22528 | 14.30 | 79.15 |
| 8/13/2013 12:13:32 PM | 1.22556 | 14.30 | 79.15 |
| 8/13/2013 12:13:33 PM | 1.22583 | 14.30 | 79.15 |
| 8/13/2013 12:13:34 PM | 1.22611 | 14.30 | 79.15 |
| 8/13/2013 12:13:35 PM | 1.22639 | 14.30 | 79.15 |
| 8/13/2013 12:13:36 PM | 1.22667 | 14.30 | 79.15 |
| 8/13/2013 12:13:37 PM | 1.22694 | 14.30 | 79.15 |
| 8/13/2013 12:13:38 PM | 1.22722 | 14.30 | 79.15 |
| 8/13/2013 12:13:39 PM | 1.22750 | 14.30 | 79.15 |
| 8/13/2013 12:13:40 PM | 1.22778 | 14.30 | 79.15 |
| 8/13/2013 12:13:41 PM | 1.22806 | 14.30 | 79.15 |
| 8/13/2013 12:13:42 PM | 1.22833 | 14.30 | 79.15 |
| 8/13/2013 12:13:43 PM | 1.22861 | 14.30 | 79.15 |
| 8/13/2013 12:13:44 PM | 1.22889 | 14.30 | 79.15 |
| 8/13/2013 12:13:45 PM | 1.22917 | 14.30 | 79.15 |
| 8/13/2013 12:13:46 PM | 1.22944 | 14.30 | 79.15 |
| 8/13/2013 12:13:47 PM | 1.22972 | 14.30 | 79.16 |
| 8/13/2013 12:13:48 PM | 1.23000 | 14.30 | 79.16 |
| 8/13/2013 12:13:49 PM | 1.23028 | 14.30 | 79.16 |
| 8/13/2013 12:13:50 PM | 1.23056 | 14.30 | 79.16 |
| 8/13/2013 12:13:51 PM | 1.23083 | 14.30 | 79.16 |
| 8/13/2013 12:13:52 PM | 1.23111 | 14.30 | 79.16 |
| 8/13/2013 12:13:53 PM | 1.23139 | 14.30 | 79.16 |
| 8/13/2013 12:13:54 PM | 1.23167 | 14.30 | 79.16 |
| 8/13/2013 12:13:55 PM | 1.23194 | 14.30 | 79.16 |
| 8/13/2013 12:13:56 PM | 1.23222 | 14.30 | 79.16 |
| 8/13/2013 12:13:57 PM | 1.23250 | 14.30 | 79.16 |
| 8/13/2013 12:13:58 PM | 1.23278 | 14.30 | 79.16 |
| 8/13/2013 12:13:59 PM | 1.23306 | 14.30 | 79.16 |
| 8/13/2013 12:14:00 PM | 1.23333 | 14.30 | 79.16 |
| 8/13/2013 12:14:01 PM | 1.23361 | 14.30 | 79.16 |
| 8/13/2013 12:14:02 PM | 1.23389 | 14.30 | 79.16 |
| 8/13/2013 12:14:03 PM | 1.23417 | 14.30 | 79.16 |
| 8/13/2013 12:14:04 PM | 1.23444 | 14.30 | 79.16 |
| 8/13/2013 12:14:05 PM | 1.23472 | 14.30 | 79.16 |
| 8/13/2013 12:14:06 PM | 1.23500 | 14.30 | 79.16 |
| 8/13/2013 12:14:07 PM | 1.23528 | 14.30 | 79.16 |
| 8/13/2013 12:14:08 PM | 1.23556 | 14.30 | 79.16 |
| 8/13/2013 12:14:09 PM | 1.23583 | 14.30 | 79.16 |
| 8/13/2013 12:14:10 PM | 1.23611 | 14.30 | 79.16 |
| 8/13/2013 12:14:11 PM | 1.23639 | 14.30 | 79.16 |
| 8/13/2013 12:14:12 PM | 1.23667 | 14.30 | 79.16 |
| 8/13/2013 12:14:13 PM | 1.23694 | 14.30 | 79.17 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:14:14 PM | 1.23722 | 14.30 | 79.17 |
| 8/13/2013 12:14:15 PM | 1.23750 | 14.30 | 79.17 |
| 8/13/2013 12:14:16 PM | 1.23778 | 14.30 | 79.17 |
| 8/13/2013 12:14:17 PM | 1.23806 | 14.30 | 79.17 |
| 8/13/2013 12:14:18 PM | 1.23833 | 14.30 | 79.17 |
| 8/13/2013 12:14:19 PM | 1.23861 | 14.30 | 79.17 |
| 8/13/2013 12:14:20 PM | 1.23889 | 14.30 | 79.17 |
| 8/13/2013 12:14:21 PM | 1.23917 | 14.30 | 79.17 |
| 8/13/2013 12:14:22 PM | 1.23944 | 14.30 | 79.17 |
| 8/13/2013 12:14:23 PM | 1.23972 | 14.30 | 79.17 |
| 8/13/2013 12:14:24 PM | 1.24000 | 14.30 | 79.17 |
| 8/13/2013 12:14:25 PM | 1.24028 | 14.30 | 79.17 |
| 8/13/2013 12:14:26 PM | 1.24056 | 14.30 | 79.17 |
| 8/13/2013 12:14:27 PM | 1.24083 | 14.30 | 79.17 |
| 8/13/2013 12:14:28 PM | 1.24111 | 14.30 | 79.17 |
| 8/13/2013 12:14:29 PM | 1.24139 | 14.30 | 79.17 |
| 8/13/2013 12:14:30 PM | 1.24167 | 14.30 | 79.17 |
| 8/13/2013 12:14:31 PM | 1.24194 | 14.30 | 79.17 |
| 8/13/2013 12:14:32 PM | 1.24222 | 14.30 | 79.17 |
| 8/13/2013 12:14:33 PM | 1.24250 | 14.30 | 79.17 |
| 8/13/2013 12:14:34 PM | 1.24278 | 14.30 | 79.17 |
| 8/13/2013 12:14:35 PM | 1.24306 | 14.30 | 79.17 |
| 8/13/2013 12:14:36 PM | 1.24333 | 14.30 | 79.17 |
| 8/13/2013 12:14:37 PM | 1.24361 | 14.30 | 79.17 |
| 8/13/2013 12:14:38 PM | 1.24389 | 14.30 | 79.17 |
| 8/13/2013 12:14:39 PM | 1.24417 | 14.30 | 79.17 |
| 8/13/2013 12:14:40 PM | 1.24444 | 14.30 | 79.17 |
| 8/13/2013 12:14:41 PM | 1.24472 | 14.30 | 79.17 |
| 8/13/2013 12:14:42 PM | 1.24500 | 14.30 | 79.17 |
| 8/13/2013 12:14:43 PM | 1.24528 | 14.30 | 79.17 |
| 8/13/2013 12:14:44 PM | 1.24556 | 14.30 | 79.18 |
| 8/13/2013 12:14:45 PM | 1.24583 | 14.30 | 79.18 |
| 8/13/2013 12:14:46 PM | 1.24611 | 14.30 | 79.18 |
| 8/13/2013 12:14:47 PM | 1.24639 | 14.30 | 79.18 |
| 8/13/2013 12:14:48 PM | 1.24667 | 14.30 | 79.18 |
| 8/13/2013 12:14:49 PM | 1.24694 | 14.30 | 79.18 |
| 8/13/2013 12:14:50 PM | 1.24722 | 14.30 | 79.18 |
| 8/13/2013 12:14:51 PM | 1.24750 | 14.30 | 79.18 |
| 8/13/2013 12:14:52 PM | 1.24778 | 14.30 | 79.18 |
| 8/13/2013 12:14:53 PM | 1.24806 | 14.30 | 79.18 |
| 8/13/2013 12:14:54 PM | 1.24833 | 14.30 | 79.18 |
| 8/13/2013 12:14:55 PM | 1.24861 | 14.30 | 79.18 |
| 8/13/2013 12:14:56 PM | 1.24889 | 14.30 | 79.18 |
| 8/13/2013 12:14:57 PM | 1.24917 | 14.30 | 79.18 |
| 8/13/2013 12:14:58 PM | 1.24944 | 14.30 | 79.18 |
| 8/13/2013 12:14:59 PM | 1.24972 | 14.30 | 79.18 |
| 8/13/2013 12:15:00 PM | 1.25000 | 14.30 | 79.18 |
| 8/13/2013 12:15:01 PM | 1.25028 | 14.30 | 79.18 |
| 8/13/2013 12:15:02 PM | 1.25056 | 14.30 | 79.18 |
| 8/13/2013 12:15:03 PM | 1.25083 | 14.30 | 79.18 |
| 8/13/2013 12:15:04 PM | 1.25111 | 14.30 | 79.18 |
| 8/13/2013 12:15:05 PM | 1.25139 | 14.30 | 79.18 |
| 8/13/2013 12:15:06 PM | 1.25167 | 14.30 | 79.18 |
| 8/13/2013 12:15:07 PM | 1.25194 | 14.30 | 79.18 |
| 8/13/2013 12:15:08 PM | 1.25222 | 14.30 | 79.18 |
| 8/13/2013 12:15:09 PM | 1.25250 | 14.30 | 79.18 |
| 8/13/2013 12:15:10 PM | 1.25278 | 14.30 | 79.18 |
| 8/13/2013 12:15:11 PM | 1.25306 | 14.30 | 79.18 |
| 8/13/2013 12:15:12 PM | 1.25333 | 14.30 | 79.19 |
| 8/13/2013 12:15:13 PM | 1.25361 | 14.30 | 79.19 |
| 8/13/2013 12:15:14 PM | 1.25389 | 14.30 | 79.19 |
| 8/13/2013 12:15:15 PM | 1.25417 | 14.30 | 79.19 |
| 8/13/2013 12:15:16 PM | 1.25444 | 14.30 | 79.19 |
| 8/13/2013 12:15:17 PM | 1.25472 | 14.30 | 79.19 |
| 8/13/2013 12:15:18 PM | 1.25500 | 14.30 | 79.19 |
| 8/13/2013 12:15:19 PM | 1.25528 | 14.30 | 79.19 |
| 8/13/2013 12:15:20 PM | 1.25556 | 14.30 | 79.19 |
| 8/13/2013 12:15:21 PM | 1.25583 | 14.30 | 79.19 |
| 8/13/2013 12:15:22 PM | 1.25611 | 14.30 | 79.19 |
| 8/13/2013 12:15:23 PM | 1.25639 | 14.30 | 79.19 |
| 8/13/2013 12:15:24 PM | 1.25667 | 14.30 | 79.19 |
| 8/13/2013 12:15:25 PM | 1.25694 | 14.30 | 79.19 |
| 8/13/2013 12:15:26 PM | 1.25722 | 14.30 | 79.19 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:15:27 PM | 1.25750 | 14.30 | 79.19 |
| 8/13/2013 12:15:28 PM | 1.25778 | 14.30 | 79.19 |
| 8/13/2013 12:15:29 PM | 1.25806 | 14.30 | 79.19 |
| 8/13/2013 12:15:30 PM | 1.25833 | 14.30 | 79.19 |
| 8/13/2013 12:15:31 PM | 1.25861 | 14.30 | 79.19 |
| 8/13/2013 12:15:32 PM | 1.25889 | 14.30 | 79.19 |
| 8/13/2013 12:15:33 PM | 1.25917 | 14.30 | 79.19 |
| 8/13/2013 12:15:34 PM | 1.25944 | 14.30 | 79.19 |
| 8/13/2013 12:15:35 PM | 1.25972 | 14.30 | 79.19 |
| 8/13/2013 12:15:36 PM | 1.26000 | 14.30 | 79.19 |
| 8/13/2013 12:15:37 PM | 1.26028 | 14.30 | 79.19 |
| 8/13/2013 12:15:38 PM | 1.26056 | 14.30 | 79.19 |
| 8/13/2013 12:15:39 PM | 1.26083 | 14.30 | 79.19 |
| 8/13/2013 12:15:40 PM | 1.26111 | 14.30 | 79.19 |
| 8/13/2013 12:15:41 PM | 1.26139 | 14.30 | 79.19 |
| 8/13/2013 12:15:42 PM | 1.26167 | 14.30 | 79.19 |
| 8/13/2013 12:15:43 PM | 1.26194 | 14.30 | 79.19 |
| 8/13/2013 12:15:44 PM | 1.26222 | 14.30 | 79.19 |
| 8/13/2013 12:15:45 PM | 1.26250 | 14.30 | 79.19 |
| 8/13/2013 12:15:46 PM | 1.26278 | 14.30 | 79.19 |
| 8/13/2013 12:15:47 PM | 1.26306 | 14.30 | 79.19 |
| 8/13/2013 12:15:48 PM | 1.26333 | 14.30 | 79.19 |
| 8/13/2013 12:15:49 PM | 1.26361 | 14.30 | 79.19 |
| 8/13/2013 12:15:50 PM | 1.26389 | 14.30 | 79.20 |
| 8/13/2013 12:15:51 PM | 1.26417 | 14.30 | 79.20 |
| 8/13/2013 12:15:52 PM | 1.26444 | 14.30 | 79.20 |
| 8/13/2013 12:15:53 PM | 1.26472 | 14.30 | 79.20 |
| 8/13/2013 12:15:54 PM | 1.26500 | 14.30 | 79.20 |
| 8/13/2013 12:15:55 PM | 1.26528 | 14.30 | 79.20 |
| 8/13/2013 12:15:56 PM | 1.26556 | 14.30 | 79.20 |
| 8/13/2013 12:15:57 PM | 1.26583 | 14.30 | 79.20 |
| 8/13/2013 12:15:58 PM | 1.26611 | 14.30 | 79.20 |
| 8/13/2013 12:15:59 PM | 1.26639 | 14.30 | 79.20 |
| 8/13/2013 12:16:00 PM | 1.26667 | 14.30 | 79.20 |
| 8/13/2013 12:16:01 PM | 1.26694 | 14.30 | 79.20 |
| 8/13/2013 12:16:02 PM | 1.26722 | 14.30 | 79.20 |
| 8/13/2013 12:16:03 PM | 1.26750 | 14.30 | 79.20 |
| 8/13/2013 12:16:04 PM | 1.26778 | 14.30 | 79.20 |
| 8/13/2013 12:16:05 PM | 1.26806 | 14.30 | 79.20 |
| 8/13/2013 12:16:06 PM | 1.26833 | 14.30 | 79.20 |
| 8/13/2013 12:16:07 PM | 1.26861 | 14.30 | 79.20 |
| 8/13/2013 12:16:08 PM | 1.26889 | 14.30 | 79.20 |
| 8/13/2013 12:16:09 PM | 1.26917 | 14.30 | 79.20 |
| 8/13/2013 12:16:10 PM | 1.26944 | 14.30 | 79.20 |
| 8/13/2013 12:16:11 PM | 1.26972 | 14.30 | 79.20 |
| 8/13/2013 12:16:12 PM | 1.27000 | 14.30 | 79.20 |
| 8/13/2013 12:16:13 PM | 1.27028 | 14.30 | 79.20 |
| 8/13/2013 12:16:14 PM | 1.27056 | 14.30 | 79.20 |
| 8/13/2013 12:16:15 PM | 1.27083 | 14.30 | 79.20 |
| 8/13/2013 12:16:16 PM | 1.27111 | 14.30 | 79.20 |
| 8/13/2013 12:16:17 PM | 1.27139 | 14.30 | 79.20 |
| 8/13/2013 12:16:18 PM | 1.27167 | 14.30 | 79.20 |
| 8/13/2013 12:16:19 PM | 1.27194 | 14.30 | 79.20 |
| 8/13/2013 12:16:20 PM | 1.27222 | 14.30 | 79.20 |
| 8/13/2013 12:16:21 PM | 1.27250 | 14.30 | 79.20 |
| 8/13/2013 12:16:22 PM | 1.27278 | 14.30 | 79.20 |
| 8/13/2013 12:16:23 PM | 1.27306 | 14.30 | 79.20 |
| 8/13/2013 12:16:24 PM | 1.27333 | 14.30 | 79.20 |
| 8/13/2013 12:16:25 PM | 1.27361 | 14.30 | 79.20 |
| 8/13/2013 12:16:26 PM | 1.27389 | 14.30 | 79.20 |
| 8/13/2013 12:16:27 PM | 1.27417 | 14.30 | 79.20 |
| 8/13/2013 12:16:28 PM | 1.27444 | 14.30 | 79.20 |
| 8/13/2013 12:16:29 PM | 1.27472 | 14.30 | 79.21 |
| 8/13/2013 12:16:30 PM | 1.27500 | 14.30 | 79.21 |
| 8/13/2013 12:16:31 PM | 1.27528 | 14.30 | 79.21 |
| 8/13/2013 12:16:32 PM | 1.27556 | 14.30 | 79.21 |
| 8/13/2013 12:16:33 PM | 1.27583 | 14.30 | 79.21 |
| 8/13/2013 12:16:34 PM | 1.27611 | 14.30 | 79.21 |
| 8/13/2013 12:16:35 PM | 1.27639 | 14.30 | 79.21 |
| 8/13/2013 12:16:36 PM | 1.27667 | 14.30 | 79.21 |
| 8/13/2013 12:16:37 PM | 1.27694 | 14.30 | 79.21 |
| 8/13/2013 12:16:38 PM | 1.27722 | 14.30 | 79.21 |
| 8/13/2013 12:16:39 PM | 1.27750 | 14.30 | 79.21 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:16:40 PM | 1.27778 | 14.30 | 79.21 |
| 8/13/2013 12:16:41 PM | 1.27806 | 14.30 | 79.21 |
| 8/13/2013 12:16:42 PM | 1.27833 | 14.30 | 79.21 |
| 8/13/2013 12:16:43 PM | 1.27861 | 14.30 | 79.21 |
| 8/13/2013 12:16:44 PM | 1.27889 | 14.30 | 79.21 |
| 8/13/2013 12:16:45 PM | 1.27917 | 14.30 | 79.21 |
| 8/13/2013 12:16:46 PM | 1.27944 | 14.30 | 79.21 |
| 8/13/2013 12:16:47 PM | 1.27972 | 14.30 | 79.21 |
| 8/13/2013 12:16:48 PM | 1.28000 | 14.30 | 79.21 |
| 8/13/2013 12:16:49 PM | 1.28028 | 14.30 | 79.21 |
| 8/13/2013 12:16:50 PM | 1.28056 | 14.30 | 79.21 |
| 8/13/2013 12:16:51 PM | 1.28083 | 14.30 | 79.21 |
| 8/13/2013 12:16:52 PM | 1.28111 | 14.30 | 79.21 |
| 8/13/2013 12:16:53 PM | 1.28139 | 14.30 | 79.21 |
| 8/13/2013 12:16:54 PM | 1.28167 | 14.30 | 79.21 |
| 8/13/2013 12:16:55 PM | 1.28194 | 14.30 | 79.21 |
| 8/13/2013 12:16:56 PM | 1.28222 | 14.30 | 79.21 |
| 8/13/2013 12:16:57 PM | 1.28250 | 14.30 | 79.21 |
| 8/13/2013 12:16:58 PM | 1.28278 | 14.30 | 79.21 |
| 8/13/2013 12:16:59 PM | 1.28306 | 14.30 | 79.21 |
| 8/13/2013 12:17:00 PM | 1.28333 | 14.30 | 79.21 |
| 8/13/2013 12:17:01 PM | 1.28361 | 14.30 | 79.21 |
| 8/13/2013 12:17:02 PM | 1.28389 | 14.30 | 79.21 |
| 8/13/2013 12:17:03 PM | 1.28417 | 14.30 | 79.21 |
| 8/13/2013 12:17:04 PM | 1.28444 | 14.30 | 79.21 |
| 8/13/2013 12:17:05 PM | 1.28472 | 14.30 | 79.21 |
| 8/13/2013 12:17:06 PM | 1.28500 | 14.30 | 79.22 |
| 8/13/2013 12:17:07 PM | 1.28528 | 14.30 | 79.22 |
| 8/13/2013 12:17:08 PM | 1.28556 | 14.30 | 79.22 |
| 8/13/2013 12:17:09 PM | 1.28583 | 14.30 | 79.22 |
| 8/13/2013 12:17:10 PM | 1.28611 | 14.30 | 79.22 |
| 8/13/2013 12:17:11 PM | 1.28639 | 14.30 | 79.22 |
| 8/13/2013 12:17:12 PM | 1.28667 | 14.30 | 79.22 |
| 8/13/2013 12:17:13 PM | 1.28694 | 14.30 | 79.22 |
| 8/13/2013 12:17:14 PM | 1.28722 | 14.30 | 79.22 |
| 8/13/2013 12:17:15 PM | 1.28750 | 14.30 | 79.22 |
| 8/13/2013 12:17:16 PM | 1.28778 | 14.30 | 79.22 |
| 8/13/2013 12:17:17 PM | 1.28806 | 14.30 | 79.22 |
| 8/13/2013 12:17:18 PM | 1.28833 | 14.30 | 79.22 |
| 8/13/2013 12:17:19 PM | 1.28861 | 14.30 | 79.22 |
| 8/13/2013 12:17:20 PM | 1.28889 | 14.30 | 79.22 |
| 8/13/2013 12:17:21 PM | 1.28917 | 14.30 | 79.22 |
| 8/13/2013 12:17:22 PM | 1.28944 | 14.30 | 79.22 |
| 8/13/2013 12:17:23 PM | 1.28972 | 14.30 | 79.22 |
| 8/13/2013 12:17:24 PM | 1.29000 | 14.30 | 79.22 |
| 8/13/2013 12:17:25 PM | 1.29028 | 14.30 | 79.22 |
| 8/13/2013 12:17:26 PM | 1.29056 | 14.30 | 79.22 |
| 8/13/2013 12:17:27 PM | 1.29083 | 14.30 | 79.22 |
| 8/13/2013 12:17:28 PM | 1.29111 | 14.30 | 79.22 |
| 8/13/2013 12:17:29 PM | 1.29139 | 14.30 | 79.22 |
| 8/13/2013 12:17:30 PM | 1.29167 | 14.30 | 79.22 |
| 8/13/2013 12:17:31 PM | 1.29194 | 14.30 | 79.22 |
| 8/13/2013 12:17:32 PM | 1.29222 | 14.30 | 79.22 |
| 8/13/2013 12:17:33 PM | 1.29250 | 14.30 | 79.22 |
| 8/13/2013 12:17:34 PM | 1.29278 | 14.30 | 79.22 |
| 8/13/2013 12:17:35 PM | 1.29306 | 14.30 | 79.22 |
| 8/13/2013 12:17:36 PM | 1.29333 | 14.30 | 79.22 |
| 8/13/2013 12:17:37 PM | 1.29361 | 14.30 | 79.22 |
| 8/13/2013 12:17:38 PM | 1.29389 | 14.30 | 79.22 |
| 8/13/2013 12:17:39 PM | 1.29417 | 14.30 | 79.22 |
| 8/13/2013 12:17:40 PM | 1.29444 | 14.30 | 79.22 |
| 8/13/2013 12:17:41 PM | 1.29472 | 14.30 | 79.22 |
| 8/13/2013 12:17:42 PM | 1.29500 | 14.30 | 79.22 |
| 8/13/2013 12:17:43 PM | 1.29528 | 14.30 | 79.22 |
| 8/13/2013 12:17:44 PM | 1.29556 | 14.30 | 79.22 |
| 8/13/2013 12:17:45 PM | 1.29583 | 14.30 | 79.22 |
| 8/13/2013 12:17:46 PM | 1.29611 | 14.30 | 79.22 |
| 8/13/2013 12:17:47 PM | 1.29639 | 14.30 | 79.22 |
| 8/13/2013 12:17:48 PM | 1.29667 | 14.30 | 79.22 |
| 8/13/2013 12:17:49 PM | 1.29694 | 14.30 | 79.22 |
| 8/13/2013 12:17:50 PM | 1.29722 | 14.30 | 79.22 |
| 8/13/2013 12:17:51 PM | 1.29750 | 14.30 | 79.22 |
| 8/13/2013 12:17:52 PM | 1.29778 | 14.30 | 79.22 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:17:53 PM | 1.29806 | 14.30 | 79.22 |
| 8/13/2013 12:17:54 PM | 1.29833 | 14.30 | 79.22 |
| 8/13/2013 12:17:55 PM | 1.29861 | 14.30 | 79.22 |
| 8/13/2013 12:17:56 PM | 1.29889 | 14.30 | 79.22 |
| 8/13/2013 12:17:57 PM | 1.29917 | 14.30 | 79.22 |
| 8/13/2013 12:17:58 PM | 1.29944 | 14.30 | 79.23 |
| 8/13/2013 12:17:59 PM | 1.29972 | 14.30 | 79.23 |
| 8/13/2013 12:18:00 PM | 1.30000 | 14.30 | 79.23 |
| 8/13/2013 12:18:01 PM | 1.30028 | 14.30 | 79.23 |
| 8/13/2013 12:18:02 PM | 1.30056 | 14.30 | 79.23 |
| 8/13/2013 12:18:03 PM | 1.30083 | 14.30 | 79.23 |
| 8/13/2013 12:18:04 PM | 1.30111 | 14.30 | 79.23 |
| 8/13/2013 12:18:05 PM | 1.30139 | 14.30 | 79.23 |
| 8/13/2013 12:18:06 PM | 1.30167 | 14.30 | 79.23 |
| 8/13/2013 12:18:07 PM | 1.30194 | 14.30 | 79.23 |
| 8/13/2013 12:18:08 PM | 1.30222 | 14.30 | 79.23 |
| 8/13/2013 12:18:09 PM | 1.30250 | 14.30 | 79.23 |
| 8/13/2013 12:18:10 PM | 1.30278 | 14.30 | 79.23 |
| 8/13/2013 12:18:11 PM | 1.30306 | 14.30 | 79.23 |
| 8/13/2013 12:18:12 PM | 1.30333 | 14.30 | 79.23 |
| 8/13/2013 12:18:13 PM | 1.30361 | 14.30 | 79.23 |
| 8/13/2013 12:18:14 PM | 1.30389 | 14.30 | 79.23 |
| 8/13/2013 12:18:15 PM | 1.30417 | 14.30 | 79.23 |
| 8/13/2013 12:18:16 PM | 1.30444 | 14.30 | 79.23 |
| 8/13/2013 12:18:17 PM | 1.30472 | 14.30 | 79.23 |
| 8/13/2013 12:18:18 PM | 1.30500 | 14.30 | 79.23 |
| 8/13/2013 12:18:19 PM | 1.30528 | 14.30 | 79.23 |
| 8/13/2013 12:18:20 PM | 1.30556 | 14.30 | 79.23 |
| 8/13/2013 12:18:21 PM | 1.30583 | 14.30 | 79.23 |
| 8/13/2013 12:18:22 PM | 1.30611 | 14.30 | 79.23 |
| 8/13/2013 12:18:23 PM | 1.30639 | 14.30 | 79.23 |
| 8/13/2013 12:18:24 PM | 1.30667 | 14.30 | 79.23 |
| 8/13/2013 12:18:25 PM | 1.30694 | 14.30 | 79.23 |
| 8/13/2013 12:18:26 PM | 1.30722 | 14.30 | 79.23 |
| 8/13/2013 12:18:27 PM | 1.30750 | 14.30 | 79.23 |
| 8/13/2013 12:18:28 PM | 1.30778 | 14.30 | 79.23 |
| 8/13/2013 12:18:29 PM | 1.30806 | 14.30 | 79.23 |
| 8/13/2013 12:18:30 PM | 1.30833 | 14.30 | 79.23 |
| 8/13/2013 12:18:31 PM | 1.30861 | 14.30 | 79.23 |
| 8/13/2013 12:18:32 PM | 1.30889 | 14.30 | 79.23 |
| 8/13/2013 12:18:33 PM | 1.30917 | 14.30 | 79.23 |
| 8/13/2013 12:18:34 PM | 1.30944 | 14.30 | 79.23 |
| 8/13/2013 12:18:35 PM | 1.30972 | 14.30 | 79.23 |
| 8/13/2013 12:18:36 PM | 1.31000 | 14.30 | 79.23 |
| 8/13/2013 12:18:37 PM | 1.31028 | 14.30 | 79.23 |
| 8/13/2013 12:18:38 PM | 1.31056 | 14.30 | 79.23 |
| 8/13/2013 12:18:39 PM | 1.31083 | 14.30 | 79.23 |
| 8/13/2013 12:18:40 PM | 1.31111 | 14.30 | 79.23 |
| 8/13/2013 12:18:41 PM | 1.31139 | 14.30 | 79.23 |
| 8/13/2013 12:18:42 PM | 1.31167 | 14.30 | 79.23 |
| 8/13/2013 12:18:43 PM | 1.31194 | 14.30 | 79.23 |
| 8/13/2013 12:18:44 PM | 1.31222 | 14.30 | 79.23 |
| 8/13/2013 12:18:45 PM | 1.31250 | 14.30 | 79.23 |
| 8/13/2013 12:18:46 PM | 1.31278 | 14.30 | 79.23 |
| 8/13/2013 12:18:47 PM | 1.31306 | 14.30 | 79.23 |
| 8/13/2013 12:18:48 PM | 1.31333 | 14.30 | 79.23 |
| 8/13/2013 12:18:49 PM | 1.31361 | 14.30 | 79.23 |
| 8/13/2013 12:18:50 PM | 1.31389 | 14.30 | 79.23 |
| 8/13/2013 12:18:51 PM | 1.31417 | 14.30 | 79.23 |
| 8/13/2013 12:18:52 PM | 1.31444 | 14.30 | 79.23 |
| 8/13/2013 12:18:53 PM | 1.31472 | 14.30 | 79.23 |
| 8/13/2013 12:18:54 PM | 1.31500 | 14.30 | 79.23 |
| 8/13/2013 12:18:55 PM | 1.31528 | 14.30 | 79.23 |
| 8/13/2013 12:18:56 PM | 1.31556 | 14.30 | 79.23 |
| 8/13/2013 12:18:57 PM | 1.31583 | 14.30 | 79.24 |
| 8/13/2013 12:18:58 PM | 1.31611 | 14.30 | 79.24 |
| 8/13/2013 12:18:59 PM | 1.31639 | 14.30 | 79.24 |
| 8/13/2013 12:19:00 PM | 1.31667 | 14.30 | 79.24 |
| 8/13/2013 12:19:01 PM | 1.31694 | 14.30 | 79.24 |
| 8/13/2013 12:19:02 PM | 1.31722 | 14.30 | 79.24 |
| 8/13/2013 12:19:03 PM | 1.31750 | 14.30 | 79.24 |
| 8/13/2013 12:19:04 PM | 1.31778 | 14.30 | 79.24 |
| 8/13/2013 12:19:05 PM | 1.31806 | 14.30 | 79.24 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:19:06 PM | 1.31833 | 14.30 | 79.24 |
| 8/13/2013 12:19:07 PM | 1.31861 | 14.30 | 79.24 |
| 8/13/2013 12:19:08 PM | 1.31889 | 14.30 | 79.24 |
| 8/13/2013 12:19:09 PM | 1.31917 | 14.30 | 79.24 |
| 8/13/2013 12:19:10 PM | 1.31944 | 14.30 | 79.24 |
| 8/13/2013 12:19:11 PM | 1.31972 | 14.30 | 79.24 |
| 8/13/2013 12:19:12 PM | 1.32000 | 14.30 | 79.24 |
| 8/13/2013 12:19:13 PM | 1.32028 | 14.30 | 79.24 |
| 8/13/2013 12:19:14 PM | 1.32056 | 14.30 | 79.24 |
| 8/13/2013 12:19:15 PM | 1.32083 | 14.30 | 79.24 |
| 8/13/2013 12:19:16 PM | 1.32111 | 14.30 | 79.24 |
| 8/13/2013 12:19:17 PM | 1.32139 | 14.30 | 79.24 |
| 8/13/2013 12:19:18 PM | 1.32167 | 14.30 | 79.24 |
| 8/13/2013 12:19:19 PM | 1.32194 | 14.30 | 79.24 |
| 8/13/2013 12:19:20 PM | 1.32222 | 14.30 | 79.24 |
| 8/13/2013 12:19:21 PM | 1.32250 | 14.30 | 79.24 |
| 8/13/2013 12:19:22 PM | 1.32278 | 14.30 | 79.24 |
| 8/13/2013 12:19:23 PM | 1.32306 | 14.30 | 79.24 |
| 8/13/2013 12:19:24 PM | 1.32333 | 14.30 | 79.24 |
| 8/13/2013 12:19:25 PM | 1.32361 | 14.30 | 79.24 |
| 8/13/2013 12:19:26 PM | 1.32389 | 14.30 | 79.24 |
| 8/13/2013 12:19:27 PM | 1.32417 | 14.30 | 79.24 |
| 8/13/2013 12:19:28 PM | 1.32444 | 14.30 | 79.24 |
| 8/13/2013 12:19:29 PM | 1.32472 | 14.30 | 79.24 |
| 8/13/2013 12:19:30 PM | 1.32500 | 14.30 | 79.24 |
| 8/13/2013 12:19:31 PM | 1.32528 | 14.30 | 79.24 |
| 8/13/2013 12:19:32 PM | 1.32556 | 14.30 | 79.24 |
| 8/13/2013 12:19:33 PM | 1.32583 | 14.30 | 79.24 |
| 8/13/2013 12:19:34 PM | 1.32611 | 14.30 | 79.24 |
| 8/13/2013 12:19:35 PM | 1.32639 | 14.30 | 79.24 |
| 8/13/2013 12:19:36 PM | 1.32667 | 14.30 | 79.24 |
| 8/13/2013 12:19:37 PM | 1.32694 | 14.30 | 79.24 |
| 8/13/2013 12:19:38 PM | 1.32722 | 14.30 | 79.24 |
| 8/13/2013 12:19:39 PM | 1.32750 | 14.30 | 79.24 |
| 8/13/2013 12:19:40 PM | 1.32778 | 14.30 | 79.24 |
| 8/13/2013 12:19:41 PM | 1.32806 | 14.30 | 79.24 |
| 8/13/2013 12:19:42 PM | 1.32833 | 14.30 | 79.24 |
| 8/13/2013 12:19:43 PM | 1.32861 | 14.30 | 79.24 |
| 8/13/2013 12:19:44 PM | 1.32889 | 14.30 | 79.24 |
| 8/13/2013 12:19:45 PM | 1.32917 | 14.30 | 79.24 |
| 8/13/2013 12:19:46 PM | 1.32944 | 14.30 | 79.24 |
| 8/13/2013 12:19:47 PM | 1.32972 | 14.30 | 79.24 |
| 8/13/2013 12:19:48 PM | 1.33000 | 14.30 | 79.24 |
| 8/13/2013 12:19:49 PM | 1.33028 | 14.30 | 79.24 |
| 8/13/2013 12:19:50 PM | 1.33056 | 14.30 | 79.24 |
| 8/13/2013 12:19:51 PM | 1.33083 | 14.30 | 79.24 |
| 8/13/2013 12:19:52 PM | 1.33111 | 14.30 | 79.24 |
| 8/13/2013 12:19:53 PM | 1.33139 | 14.30 | 79.24 |
| 8/13/2013 12:19:54 PM | 1.33167 | 14.30 | 79.24 |
| 8/13/2013 12:19:55 PM | 1.33194 | 14.30 | 79.24 |
| 8/13/2013 12:19:56 PM | 1.33222 | 14.30 | 79.24 |
| 8/13/2013 12:19:57 PM | 1.33250 | 14.30 | 79.24 |
| 8/13/2013 12:19:58 PM | 1.33278 | 14.30 | 79.24 |
| 8/13/2013 12:19:59 PM | 1.33306 | 14.30 | 79.24 |
| 8/13/2013 12:20:00 PM | 1.33333 | 14.30 | 79.24 |
| 8/13/2013 12:20:01 PM | 1.33361 | 14.30 | 79.24 |
| 8/13/2013 12:20:02 PM | 1.33389 | 14.30 | 79.24 |
| 8/13/2013 12:20:03 PM | 1.33417 | 14.30 | 79.24 |
| 8/13/2013 12:20:04 PM | 1.33444 | 14.30 | 79.24 |
| 8/13/2013 12:20:05 PM | 1.33472 | 14.33 | 79.24 |
| 8/13/2013 12:20:06 PM | 1.33500 | 14.34 | 79.24 |
| 8/13/2013 12:20:07 PM | 1.33528 | 14.37 | 79.24 |
| 8/13/2013 12:20:08 PM | 1.33556 | 14.39 | 79.24 |
| 8/13/2013 12:20:09 PM | 1.33583 | 14.44 | 79.24 |
| 8/13/2013 12:20:10 PM | 1.33611 | 14.52 | 79.24 |
| 8/13/2013 12:20:11 PM | 1.33639 | 14.62 | 79.25 |
| 8/13/2013 12:20:12 PM | 1.33667 | 14.80 | 79.25 |
| 8/13/2013 12:20:13 PM | 1.33694 | 17.84 | 79.25 |
| 8/13/2013 12:20:14 PM | 1.33722 | 29.98 | 79.26 |
| 8/13/2013 12:20:15 PM | 1.33750 | 41.83 | 79.26 |
| 8/13/2013 12:20:16 PM | 1.33778 | 58.03 | 79.27 |
| 8/13/2013 12:20:17 PM | 1.33806 | 68.83 | 79.28 |
| 8/13/2013 12:20:18 PM | 1.33833 | 71.80 | 79.28 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:20:19 PM | 1.33861 | 70.03 | 79.28 |
| 8/13/2013 12:20:20 PM | 1.33889 | 68.68 | 79.28 |
| 8/13/2013 12:20:21 PM | 1.33917 | 71.41 | 79.28 |
| 8/13/2013 12:20:22 PM | 1.33944 | 67.10 | 79.27 |
| 8/13/2013 12:20:23 PM | 1.33972 | 72.09 | 79.26 |
| 8/13/2013 12:20:24 PM | 1.34000 | 68.25 | 79.25 |
| 8/13/2013 12:20:25 PM | 1.34028 | 73.06 | 79.24 |
| 8/13/2013 12:20:26 PM | 1.34056 | 70.26 | 79.23 |
| 8/13/2013 12:20:27 PM | 1.34083 | 73.16 | 79.22 |
| 8/13/2013 12:20:28 PM | 1.34111 | 71.87 | 79.20 |
| 8/13/2013 12:20:29 PM | 1.34139 | 74.18 | 79.19 |
| 8/13/2013 12:20:30 PM | 1.34167 | 78.12 | 79.17 |
| 8/13/2013 12:20:31 PM | 1.34194 | 82.50 | 79.16 |
| 8/13/2013 12:20:32 PM | 1.34222 | 91.33 | 79.14 |
| 8/13/2013 12:20:33 PM | 1.34250 | 97.37 | 79.13 |
| 8/13/2013 12:20:34 PM | 1.34278 | 107.35 | 79.12 |
| 8/13/2013 12:20:35 PM | 1.34306 | 116.26 | 79.10 |
| 8/13/2013 12:20:36 PM | 1.34333 | 124.98 | 79.09 |
| 8/13/2013 12:20:37 PM | 1.34361 | 136.76 | 79.08 |
| 8/13/2013 12:20:38 PM | 1.34389 | 142.50 | 79.06 |
| 8/13/2013 12:20:39 PM | 1.34417 | 155.93 | 79.05 |
| 8/13/2013 12:20:40 PM | 1.34444 | 162.81 | 79.03 |
| 8/13/2013 12:20:41 PM | 1.34472 | 175.59 | 79.02 |
| 8/13/2013 12:20:42 PM | 1.34500 | 185.75 | 79.01 |
| 8/13/2013 12:20:43 PM | 1.34528 | 194.99 | 79.00 |
| 8/13/2013 12:20:44 PM | 1.34556 | 207.50 | 78.98 |
| 8/13/2013 12:20:45 PM | 1.34583 | 215.68 | 78.97 |
| 8/13/2013 12:20:46 PM | 1.34611 | 227.72 | 78.96 |
| 8/13/2013 12:20:47 PM | 1.34639 | 237.95 | 78.94 |
| 8/13/2013 12:20:48 PM | 1.34667 | 246.91 | 78.93 |
| 8/13/2013 12:20:49 PM | 1.34694 | 258.27 | 78.92 |
| 8/13/2013 12:20:50 PM | 1.34722 | 266.39 | 78.90 |
| 8/13/2013 12:20:51 PM | 1.34750 | 276.19 | 78.88 |
| 8/13/2013 12:20:52 PM | 1.34778 | 286.38 | 78.87 |
| 8/13/2013 12:20:53 PM | 1.34806 | 294.75 | 78.86 |
| 8/13/2013 12:20:54 PM | 1.34833 | 305.27 | 78.84 |
| 8/13/2013 12:20:55 PM | 1.34861 | 315.92 | 78.83 |
| 8/13/2013 12:20:56 PM | 1.34889 | 325.70 | 78.82 |
| 8/13/2013 12:20:57 PM | 1.34917 | 337.72 | 78.81 |
| 8/13/2013 12:20:58 PM | 1.34944 | 349.07 | 78.80 |
| 8/13/2013 12:20:59 PM | 1.34972 | 360.95 | 78.79 |
| 8/13/2013 12:21:00 PM | 1.35000 | 374.33 | 78.78 |
| 8/13/2013 12:21:01 PM | 1.35028 | 388.42 | 78.77 |
| 8/13/2013 12:21:02 PM | 1.35056 | 404.81 | 78.77 |
| 8/13/2013 12:21:03 PM | 1.35083 | 417.85 | 78.76 |
| 8/13/2013 12:21:04 PM | 1.35111 | 436.04 | 78.75 |
| 8/13/2013 12:21:05 PM | 1.35139 | 450.20 | 78.75 |
| 8/13/2013 12:21:06 PM | 1.35167 | 467.72 | 78.74 |
| 8/13/2013 12:21:07 PM | 1.35194 | 485.41 | 78.74 |
| 8/13/2013 12:21:08 PM | 1.35222 | 499.62 | 78.73 |
| 8/13/2013 12:21:09 PM | 1.35250 | 518.56 | 78.73 |
| 8/13/2013 12:21:10 PM | 1.35278 | 533.98 | 78.73 |
| 8/13/2013 12:21:11 PM | 1.35306 | 549.42 | 78.72 |
| 8/13/2013 12:21:12 PM | 1.35333 | 568.83 | 78.72 |
| 8/13/2013 12:21:13 PM | 1.35361 | 581.66 | 78.72 |
| 8/13/2013 12:21:14 PM | 1.35389 | 598.94 | 78.71 |
| 8/13/2013 12:21:15 PM | 1.35417 | 618.57 | 78.71 |
| 8/13/2013 12:21:16 PM | 1.35444 | 632.46 | 78.71 |
| 8/13/2013 12:21:17 PM | 1.35472 | 648.71 | 78.71 |
| 8/13/2013 12:21:18 PM | 1.35500 | 666.51 | 78.70 |
| 8/13/2013 12:21:19 PM | 1.35528 | 681.86 | 78.70 |
| 8/13/2013 12:21:20 PM | 1.35556 | 698.33 | 78.70 |
| 8/13/2013 12:21:21 PM | 1.35583 | 715.50 | 78.70 |
| 8/13/2013 12:21:22 PM | 1.35611 | 730.00 | 78.70 |
| 8/13/2013 12:21:23 PM | 1.35639 | 747.48 | 78.70 |
| 8/13/2013 12:21:24 PM | 1.35667 | 763.13 | 78.69 |
| 8/13/2013 12:21:25 PM | 1.35694 | 778.80 | 78.69 |
| 8/13/2013 12:21:26 PM | 1.35722 | 795.85 | 78.69 |
| 8/13/2013 12:21:27 PM | 1.35750 | 810.65 | 78.69 |
| 8/13/2013 12:21:28 PM | 1.35778 | 827.07 | 78.69 |
| 8/13/2013 12:21:29 PM | 1.35806 | 843.30 | 78.69 |
| 8/13/2013 12:21:30 PM | 1.35833 | 857.63 | 78.69 |
| 8/13/2013 12:21:31 PM | 1.35861 | 873.41 | 78.69 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:21:32 PM | 1.35889 | 889.49 | 78.69 |
| 8/13/2013 12:21:33 PM | 1.35917 | 903.87 | 78.69 |
| 8/13/2013 12:21:34 PM | 1.35944 | 919.26 | 78.69 |
| 8/13/2013 12:21:35 PM | 1.35972 | 934.48 | 78.69 |
| 8/13/2013 12:21:36 PM | 1.36000 | 948.37 | 78.69 |
| 8/13/2013 12:21:37 PM | 1.36028 | 964.82 | 78.69 |
| 8/13/2013 12:21:38 PM | 1.36056 | 978.67 | 78.69 |
| 8/13/2013 12:21:39 PM | 1.36083 | 993.91 | 78.69 |
| 8/13/2013 12:21:40 PM | 1.36111 | 1008.77 | 78.69 |
| 8/13/2013 12:21:41 PM | 1.36139 | 1022.50 | 78.69 |
| 8/13/2013 12:21:42 PM | 1.36167 | 1036.80 | 78.69 |
| 8/13/2013 12:21:43 PM | 1.36194 | 1051.52 | 78.70 |
| 8/13/2013 12:21:44 PM | 1.36222 | 1063.18 | 78.69 |
| 8/13/2013 12:21:45 PM | 1.36250 | 1067.90 | 78.69 |
| 8/13/2013 12:21:46 PM | 1.36278 | 1060.87 | 78.68 |
| 8/13/2013 12:21:47 PM | 1.36306 | 1071.50 | 78.67 |
| 8/13/2013 12:21:48 PM | 1.36333 | 1066.43 | 78.67 |
| 8/13/2013 12:21:49 PM | 1.36361 | 1061.14 | 78.66 |
| 8/13/2013 12:21:50 PM | 1.36389 | 1070.39 | 78.66 |
| 8/13/2013 12:21:51 PM | 1.36417 | 1064.86 | 78.65 |
| 8/13/2013 12:21:52 PM | 1.36444 | 1061.89 | 78.65 |
| 8/13/2013 12:21:53 PM | 1.36472 | 1068.53 | 78.65 |
| 8/13/2013 12:21:54 PM | 1.36500 | 1064.39 | 78.64 |
| 8/13/2013 12:21:55 PM | 1.36528 | 1062.68 | 78.64 |
| 8/13/2013 12:21:56 PM | 1.36556 | 1067.62 | 78.64 |
| 8/13/2013 12:21:57 PM | 1.36583 | 1063.98 | 78.64 |
| 8/13/2013 12:21:58 PM | 1.36611 | 1063.67 | 78.64 |
| 8/13/2013 12:21:59 PM | 1.36639 | 1066.58 | 78.64 |
| 8/13/2013 12:22:00 PM | 1.36667 | 1063.70 | 78.64 |
| 8/13/2013 12:22:01 PM | 1.36694 | 1064.38 | 78.63 |
| 8/13/2013 12:22:02 PM | 1.36722 | 1065.42 | 78.64 |
| 8/13/2013 12:22:03 PM | 1.36750 | 1063.50 | 78.63 |
| 8/13/2013 12:22:04 PM | 1.36778 | 1064.75 | 78.63 |
| 8/13/2013 12:22:05 PM | 1.36806 | 1064.55 | 78.64 |
| 8/13/2013 12:22:06 PM | 1.36833 | 1063.54 | 78.64 |
| 8/13/2013 12:22:07 PM | 1.36861 | 1064.76 | 78.64 |
| 8/13/2013 12:22:08 PM | 1.36889 | 1064.33 | 78.64 |
| 8/13/2013 12:22:09 PM | 1.36917 | 1063.73 | 78.64 |
| 8/13/2013 12:22:10 PM | 1.36944 | 1064.81 | 78.64 |
| 8/13/2013 12:22:11 PM | 1.36972 | 1064.19 | 78.64 |
| 8/13/2013 12:22:12 PM | 1.37000 | 1063.80 | 78.64 |
| 8/13/2013 12:22:13 PM | 1.37028 | 1064.59 | 78.64 |
| 8/13/2013 12:22:14 PM | 1.37056 | 1063.91 | 78.64 |
| 8/13/2013 12:22:15 PM | 1.37083 | 1063.76 | 78.65 |
| 8/13/2013 12:22:16 PM | 1.37111 | 1064.19 | 78.65 |
| 8/13/2013 12:22:17 PM | 1.37139 | 1063.61 | 78.65 |
| 8/13/2013 12:22:18 PM | 1.37167 | 1063.70 | 78.65 |
| 8/13/2013 12:22:19 PM | 1.37194 | 1063.75 | 78.65 |
| 8/13/2013 12:22:20 PM | 1.37222 | 1063.42 | 78.65 |
| 8/13/2013 12:22:21 PM | 1.37250 | 1063.62 | 78.65 |
| 8/13/2013 12:22:22 PM | 1.37278 | 1063.57 | 78.66 |
| 8/13/2013 12:22:23 PM | 1.37306 | 1063.38 | 78.66 |
| 8/13/2013 12:22:24 PM | 1.37333 | 1063.48 | 78.66 |
| 8/13/2013 12:22:25 PM | 1.37361 | 1063.43 | 78.66 |
| 8/13/2013 12:22:26 PM | 1.37389 | 1063.38 | 78.66 |
| 8/13/2013 12:22:27 PM | 1.37417 | 1063.35 | 78.66 |
| 8/13/2013 12:22:28 PM | 1.37444 | 1063.30 | 78.66 |
| 8/13/2013 12:22:29 PM | 1.37472 | 1063.26 | 78.66 |
| 8/13/2013 12:22:30 PM | 1.37500 | 1063.23 | 78.67 |
| 8/13/2013 12:22:31 PM | 1.37528 | 1063.18 | 78.67 |
| 8/13/2013 12:22:32 PM | 1.37556 | 1063.14 | 78.67 |
| 8/13/2013 12:22:33 PM | 1.37583 | 1063.11 | 78.67 |
| 8/13/2013 12:22:34 PM | 1.37611 | 1063.06 | 78.67 |
| 8/13/2013 12:22:35 PM | 1.37639 | 1063.02 | 78.67 |
| 8/13/2013 12:22:36 PM | 1.37667 | 1062.98 | 78.67 |
| 8/13/2013 12:22:37 PM | 1.37694 | 1062.94 | 78.67 |
| 8/13/2013 12:22:38 PM | 1.37722 | 1062.90 | 78.68 |
| 8/13/2013 12:22:39 PM | 1.37750 | 1062.87 | 78.68 |
| 8/13/2013 12:22:40 PM | 1.37778 | 1062.83 | 78.68 |
| 8/13/2013 12:22:41 PM | 1.37806 | 1062.79 | 78.68 |
| 8/13/2013 12:22:42 PM | 1.37833 | 1062.76 | 78.68 |
| 8/13/2013 12:22:43 PM | 1.37861 | 1062.72 | 78.68 |
| 8/13/2013 12:22:44 PM | 1.37889 | 1062.68 | 78.68 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:22:45 PM | 1.37917 | 1062.65 | 78.69 |
| 8/13/2013 12:22:46 PM | 1.37944 | 1062.62 | 78.69 |
| 8/13/2013 12:22:47 PM | 1.37972 | 1062.59 | 78.69 |
| 8/13/2013 12:22:48 PM | 1.38000 | 1062.55 | 78.69 |
| 8/13/2013 12:22:49 PM | 1.38028 | 1062.52 | 78.69 |
| 8/13/2013 12:22:50 PM | 1.38056 | 1062.48 | 78.69 |
| 8/13/2013 12:22:51 PM | 1.38083 | 1062.45 | 78.69 |
| 8/13/2013 12:22:52 PM | 1.38111 | 1062.42 | 78.70 |
| 8/13/2013 12:22:53 PM | 1.38139 | 1062.38 | 78.70 |
| 8/13/2013 12:22:54 PM | 1.38167 | 1062.35 | 78.70 |
| 8/13/2013 12:22:55 PM | 1.38194 | 1062.32 | 78.70 |
| 8/13/2013 12:22:56 PM | 1.38222 | 1062.29 | 78.70 |
| 8/13/2013 12:22:57 PM | 1.38250 | 1062.25 | 78.70 |
| 8/13/2013 12:22:58 PM | 1.38278 | 1062.22 | 78.70 |
| 8/13/2013 12:22:59 PM | 1.38306 | 1062.19 | 78.71 |
| 8/13/2013 12:23:00 PM | 1.38333 | 1062.16 | 78.71 |
| 8/13/2013 12:23:01 PM | 1.38361 | 1062.13 | 78.71 |
| 8/13/2013 12:23:02 PM | 1.38389 | 1062.10 | 78.71 |
| 8/13/2013 12:23:03 PM | 1.38417 | 1062.07 | 78.71 |
| 8/13/2013 12:23:04 PM | 1.38444 | 1062.04 | 78.72 |
| 8/13/2013 12:23:05 PM | 1.38472 | 1062.01 | 78.72 |
| 8/13/2013 12:23:06 PM | 1.38500 | 1061.98 | 78.72 |
| 8/13/2013 12:23:07 PM | 1.38528 | 1061.95 | 78.72 |
| 8/13/2013 12:23:08 PM | 1.38556 | 1061.92 | 78.72 |
| 8/13/2013 12:23:09 PM | 1.38583 | 1061.89 | 78.72 |
| 8/13/2013 12:23:10 PM | 1.38611 | 1061.86 | 78.72 |
| 8/13/2013 12:23:11 PM | 1.38639 | 1061.83 | 78.72 |
| 8/13/2013 12:23:12 PM | 1.38667 | 1061.80 | 78.73 |
| 8/13/2013 12:23:13 PM | 1.38694 | 1061.78 | 78.73 |
| 8/13/2013 12:23:14 PM | 1.38722 | 1061.74 | 78.73 |
| 8/13/2013 12:23:15 PM | 1.38750 | 1061.72 | 78.73 |
| 8/13/2013 12:23:16 PM | 1.38778 | 1061.69 | 78.73 |
| 8/13/2013 12:23:17 PM | 1.38806 | 1061.66 | 78.73 |
| 8/13/2013 12:23:18 PM | 1.38833 | 1061.64 | 78.74 |
| 8/13/2013 12:23:19 PM | 1.38861 | 1061.61 | 78.74 |
| 8/13/2013 12:23:20 PM | 1.38889 | 1061.59 | 78.74 |
| 8/13/2013 12:23:21 PM | 1.38917 | 1061.56 | 78.74 |
| 8/13/2013 12:23:22 PM | 1.38944 | 1061.54 | 78.74 |
| 8/13/2013 12:23:23 PM | 1.38972 | 1061.51 | 78.74 |
| 8/13/2013 12:23:24 PM | 1.39000 | 1061.49 | 78.74 |
| 8/13/2013 12:23:25 PM | 1.39028 | 1061.46 | 78.75 |
| 8/13/2013 12:23:26 PM | 1.39056 | 1061.44 | 78.75 |
| 8/13/2013 12:23:27 PM | 1.39083 | 1061.41 | 78.75 |
| 8/13/2013 12:23:28 PM | 1.39111 | 1061.38 | 78.75 |
| 8/13/2013 12:23:29 PM | 1.39139 | 1061.36 | 78.75 |
| 8/13/2013 12:23:30 PM | 1.39167 | 1061.33 | 78.75 |
| 8/13/2013 12:23:31 PM | 1.39194 | 1061.31 | 78.75 |
| 8/13/2013 12:23:32 PM | 1.39222 | 1061.28 | 78.75 |
| 8/13/2013 12:23:33 PM | 1.39250 | 1061.25 | 78.75 |
| 8/13/2013 12:23:34 PM | 1.39278 | 1061.22 | 78.76 |
| 8/13/2013 12:23:35 PM | 1.39306 | 1061.19 | 78.76 |
| 8/13/2013 12:23:36 PM | 1.39333 | 1061.16 | 78.76 |
| 8/13/2013 12:23:37 PM | 1.39361 | 1061.14 | 78.76 |
| 8/13/2013 12:23:38 PM | 1.39389 | 1061.11 | 78.76 |
| 8/13/2013 12:23:39 PM | 1.39417 | 1061.08 | 78.76 |
| 8/13/2013 12:23:40 PM | 1.39444 | 1061.05 | 78.76 |
| 8/13/2013 12:23:41 PM | 1.39472 | 1061.03 | 78.76 |
| 8/13/2013 12:23:42 PM | 1.39500 | 1061.00 | 78.77 |
| 8/13/2013 12:23:43 PM | 1.39528 | 1060.98 | 78.77 |
| 8/13/2013 12:23:44 PM | 1.39556 | 1060.95 | 78.77 |
| 8/13/2013 12:23:45 PM | 1.39583 | 1060.93 | 78.77 |
| 8/13/2013 12:23:46 PM | 1.39611 | 1060.91 | 78.77 |
| 8/13/2013 12:23:47 PM | 1.39639 | 1060.89 | 78.77 |
| 8/13/2013 12:23:48 PM | 1.39667 | 1060.86 | 78.77 |
| 8/13/2013 12:23:49 PM | 1.39694 | 1060.84 | 78.77 |
| 8/13/2013 12:23:50 PM | 1.39722 | 1060.82 | 78.77 |
| 8/13/2013 12:23:51 PM | 1.39750 | 1060.80 | 78.77 |
| 8/13/2013 12:23:52 PM | 1.39778 | 1060.78 | 78.77 |
| 8/13/2013 12:23:53 PM | 1.39806 | 1060.76 | 78.77 |
| 8/13/2013 12:23:54 PM | 1.39833 | 1060.73 | 78.78 |
| 8/13/2013 12:23:55 PM | 1.39861 | 1060.71 | 78.78 |
| 8/13/2013 12:23:56 PM | 1.39889 | 1060.68 | 78.78 |
| 8/13/2013 12:23:57 PM | 1.39917 | 1060.66 | 78.78 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:23:58 PM | 1.39944 | 1060.64 | 78.78 |
| 8/13/2013 12:23:59 PM | 1.39972 | 1060.62 | 78.78 |
| 8/13/2013 12:24:00 PM | 1.40000 | 1060.59 | 78.78 |
| 8/13/2013 12:24:01 PM | 1.40028 | 1060.57 | 78.78 |
| 8/13/2013 12:24:02 PM | 1.40056 | 1060.55 | 78.78 |
| 8/13/2013 12:24:03 PM | 1.40083 | 1060.53 | 78.78 |
| 8/13/2013 12:24:04 PM | 1.40111 | 1060.51 | 78.78 |
| 8/13/2013 12:24:05 PM | 1.40139 | 1060.49 | 78.78 |
| 8/13/2013 12:24:06 PM | 1.40167 | 1060.47 | 78.78 |
| 8/13/2013 12:24:07 PM | 1.40194 | 1060.45 | 78.79 |
| 8/13/2013 12:24:08 PM | 1.40222 | 1060.42 | 78.79 |
| 8/13/2013 12:24:09 PM | 1.40250 | 1060.40 | 78.79 |
| 8/13/2013 12:24:10 PM | 1.40278 | 1060.38 | 78.79 |
| 8/13/2013 12:24:11 PM | 1.40306 | 1060.36 | 78.79 |
| 8/13/2013 12:24:12 PM | 1.40333 | 1060.34 | 78.79 |
| 8/13/2013 12:24:13 PM | 1.40361 | 1060.32 | 78.79 |
| 8/13/2013 12:24:14 PM | 1.40389 | 1060.30 | 78.79 |
| 8/13/2013 12:24:15 PM | 1.40417 | 1060.28 | 78.79 |
| 8/13/2013 12:24:16 PM | 1.40444 | 1060.26 | 78.79 |
| 8/13/2013 12:24:17 PM | 1.40472 | 1060.24 | 78.79 |
| 8/13/2013 12:24:18 PM | 1.40500 | 1060.22 | 78.79 |
| 8/13/2013 12:24:19 PM | 1.40528 | 1060.21 | 78.79 |
| 8/13/2013 12:24:20 PM | 1.40556 | 1060.19 | 78.79 |
| 8/13/2013 12:24:21 PM | 1.40583 | 1060.18 | 78.80 |
| 8/13/2013 12:24:22 PM | 1.40611 | 1060.16 | 78.80 |
| 8/13/2013 12:24:23 PM | 1.40639 | 1060.14 | 78.80 |
| 8/13/2013 12:24:24 PM | 1.40667 | 1060.13 | 78.80 |
| 8/13/2013 12:24:25 PM | 1.40694 | 1060.12 | 78.80 |
| 8/13/2013 12:24:26 PM | 1.40722 | 1060.10 | 78.80 |
| 8/13/2013 12:24:27 PM | 1.40750 | 1060.09 | 78.80 |
| 8/13/2013 12:24:28 PM | 1.40778 | 1060.07 | 78.80 |
| 8/13/2013 12:24:29 PM | 1.40806 | 1060.06 | 78.80 |
| 8/13/2013 12:24:30 PM | 1.40833 | 1060.04 | 78.80 |
| 8/13/2013 12:24:31 PM | 1.40861 | 1060.03 | 78.80 |
| 8/13/2013 12:24:32 PM | 1.40889 | 1060.01 | 78.80 |
| 8/13/2013 12:24:33 PM | 1.40917 | 1060.00 | 78.80 |
| 8/13/2013 12:24:34 PM | 1.40944 | 1059.99 | 78.80 |
| 8/13/2013 12:24:35 PM | 1.40972 | 1059.97 | 78.80 |
| 8/13/2013 12:24:36 PM | 1.41000 | 1059.96 | 78.80 |
| 8/13/2013 12:24:37 PM | 1.41028 | 1059.95 | 78.80 |
| 8/13/2013 12:24:38 PM | 1.41056 | 1059.94 | 78.80 |
| 8/13/2013 12:24:39 PM | 1.41083 | 1059.93 | 78.80 |
| 8/13/2013 12:24:40 PM | 1.41111 | 1059.92 | 78.80 |
| 8/13/2013 12:24:41 PM | 1.41139 | 1059.91 | 78.81 |
| 8/13/2013 12:24:42 PM | 1.41167 | 1059.90 | 78.81 |
| 8/13/2013 12:24:43 PM | 1.41194 | 1059.89 | 78.81 |
| 8/13/2013 12:24:44 PM | 1.41222 | 1059.88 | 78.81 |
| 8/13/2013 12:24:45 PM | 1.41250 | 1059.88 | 78.81 |
| 8/13/2013 12:24:46 PM | 1.41278 | 1059.87 | 78.81 |
| 8/13/2013 12:24:47 PM | 1.41306 | 1059.86 | 78.81 |
| 8/13/2013 12:24:48 PM | 1.41333 | 1059.86 | 78.81 |
| 8/13/2013 12:24:49 PM | 1.41361 | 1059.85 | 78.81 |
| 8/13/2013 12:24:50 PM | 1.41389 | 1059.84 | 78.81 |
| 8/13/2013 12:24:51 PM | 1.41417 | 1059.83 | 78.81 |
| 8/13/2013 12:24:52 PM | 1.41444 | 1059.82 | 78.81 |
| 8/13/2013 12:24:53 PM | 1.41472 | 1059.82 | 78.81 |
| 8/13/2013 12:24:54 PM | 1.41500 | 1059.81 | 78.81 |
| 8/13/2013 12:24:55 PM | 1.41528 | 1059.80 | 78.81 |
| 8/13/2013 12:24:56 PM | 1.41556 | 1059.80 | 78.81 |
| 8/13/2013 12:24:57 PM | 1.41583 | 1059.79 | 78.81 |
| 8/13/2013 12:24:58 PM | 1.41611 | 1059.78 | 78.81 |
| 8/13/2013 12:24:59 PM | 1.41639 | 1059.78 | 78.81 |
| 8/13/2013 12:25:00 PM | 1.41667 | 1059.77 | 78.81 |
| 8/13/2013 12:25:01 PM | 1.41694 | 1059.77 | 78.81 |
| 8/13/2013 12:25:02 PM | 1.41722 | 1059.76 | 78.81 |
| 8/13/2013 12:25:03 PM | 1.41750 | 1059.75 | 78.81 |
| 8/13/2013 12:25:04 PM | 1.41778 | 1059.75 | 78.81 |
| 8/13/2013 12:25:05 PM | 1.41806 | 1059.74 | 78.81 |
| 8/13/2013 12:25:06 PM | 1.41833 | 1059.73 | 78.81 |
| 8/13/2013 12:25:07 PM | 1.41861 | 1059.73 | 78.82 |
| 8/13/2013 12:25:08 PM | 1.41889 | 1059.72 | 78.82 |
| 8/13/2013 12:25:09 PM | 1.41917 | 1059.71 | 78.82 |
| 8/13/2013 12:25:10 PM | 1.41944 | 1059.70 | 78.82 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:25:11 PM | 1.41972 | 1059.70 | 78.82 |
| 8/13/2013 12:25:12 PM | 1.42000 | 1059.69 | 78.82 |
| 8/13/2013 12:25:13 PM | 1.42028 | 1059.68 | 78.82 |
| 8/13/2013 12:25:14 PM | 1.42056 | 1059.67 | 78.82 |
| 8/13/2013 12:25:15 PM | 1.42083 | 1059.66 | 78.82 |
| 8/13/2013 12:25:16 PM | 1.42111 | 1059.66 | 78.82 |
| 8/13/2013 12:25:17 PM | 1.42139 | 1059.65 | 78.82 |
| 8/13/2013 12:25:18 PM | 1.42167 | 1059.64 | 78.82 |
| 8/13/2013 12:25:19 PM | 1.42194 | 1059.64 | 78.82 |
| 8/13/2013 12:25:20 PM | 1.42222 | 1059.63 | 78.82 |
| 8/13/2013 12:25:21 PM | 1.42250 | 1059.63 | 78.83 |
| 8/13/2013 12:25:22 PM | 1.42278 | 1059.62 | 78.83 |
| 8/13/2013 12:25:23 PM | 1.42306 | 1059.62 | 78.83 |
| 8/13/2013 12:25:24 PM | 1.42333 | 1059.61 | 78.83 |
| 8/13/2013 12:25:25 PM | 1.42361 | 1059.61 | 78.83 |
| 8/13/2013 12:25:26 PM | 1.42389 | 1059.60 | 78.83 |
| 8/13/2013 12:25:27 PM | 1.42417 | 1059.60 | 78.83 |
| 8/13/2013 12:25:28 PM | 1.42444 | 1059.59 | 78.83 |
| 8/13/2013 12:25:29 PM | 1.42472 | 1059.59 | 78.83 |
| 8/13/2013 12:25:30 PM | 1.42500 | 1059.58 | 78.83 |
| 8/13/2013 12:25:31 PM | 1.42528 | 1059.57 | 78.83 |
| 8/13/2013 12:25:32 PM | 1.42556 | 1059.56 | 78.84 |
| 8/13/2013 12:25:33 PM | 1.42583 | 1059.56 | 78.84 |
| 8/13/2013 12:25:34 PM | 1.42611 | 1059.55 | 78.84 |
| 8/13/2013 12:25:35 PM | 1.42639 | 1059.54 | 78.84 |
| 8/13/2013 12:25:36 PM | 1.42667 | 1059.53 | 78.84 |
| 8/13/2013 12:25:37 PM | 1.42694 | 1059.52 | 78.84 |
| 8/13/2013 12:25:38 PM | 1.42722 | 1059.52 | 78.84 |
| 8/13/2013 12:25:39 PM | 1.42750 | 1059.51 | 78.84 |
| 8/13/2013 12:25:40 PM | 1.42778 | 1059.50 | 78.84 |
| 8/13/2013 12:25:41 PM | 1.42806 | 1059.49 | 78.85 |
| 8/13/2013 12:25:42 PM | 1.42833 | 1059.49 | 78.85 |
| 8/13/2013 12:25:43 PM | 1.42861 | 1059.48 | 78.85 |
| 8/13/2013 12:25:44 PM | 1.42889 | 1059.47 | 78.85 |
| 8/13/2013 12:25:45 PM | 1.42917 | 1059.47 | 78.85 |
| 8/13/2013 12:25:46 PM | 1.42944 | 1059.46 | 78.85 |
| 8/13/2013 12:25:47 PM | 1.42972 | 1059.46 | 78.85 |
| 8/13/2013 12:25:48 PM | 1.43000 | 1059.45 | 78.86 |
| 8/13/2013 12:25:49 PM | 1.43028 | 1059.45 | 78.86 |
| 8/13/2013 12:25:50 PM | 1.43056 | 1059.44 | 78.86 |
| 8/13/2013 12:25:51 PM | 1.43083 | 1059.44 | 78.86 |
| 8/13/2013 12:25:52 PM | 1.43111 | 1059.44 | 78.86 |
| 8/13/2013 12:25:53 PM | 1.43139 | 1059.43 | 78.86 |
| 8/13/2013 12:25:54 PM | 1.43167 | 1059.43 | 78.86 |
| 8/13/2013 12:25:55 PM | 1.43194 | 1059.42 | 78.86 |
| 8/13/2013 12:25:56 PM | 1.43222 | 1059.42 | 78.86 |
| 8/13/2013 12:25:57 PM | 1.43250 | 1059.41 | 78.87 |
| 8/13/2013 12:25:58 PM | 1.43278 | 1059.41 | 78.87 |
| 8/13/2013 12:25:59 PM | 1.43306 | 1059.40 | 78.87 |
| 8/13/2013 12:26:00 PM | 1.43333 | 1059.39 | 78.87 |
| 8/13/2013 12:26:01 PM | 1.43361 | 1059.39 | 78.87 |
| 8/13/2013 12:26:02 PM | 1.43389 | 1059.38 | 78.87 |
| 8/13/2013 12:26:03 PM | 1.43417 | 1059.38 | 78.87 |
| 8/13/2013 12:26:04 PM | 1.43444 | 1059.37 | 78.88 |
| 8/13/2013 12:26:05 PM | 1.43472 | 1059.37 | 78.88 |
| 8/13/2013 12:26:06 PM | 1.43500 | 1059.36 | 78.88 |
| 8/13/2013 12:26:07 PM | 1.43528 | 1059.36 | 78.88 |
| 8/13/2013 12:26:08 PM | 1.43556 | 1059.36 | 78.88 |
| 8/13/2013 12:26:09 PM | 1.43583 | 1059.35 | 78.88 |
| 8/13/2013 12:26:10 PM | 1.43611 | 1059.35 | 78.88 |
| 8/13/2013 12:26:11 PM | 1.43639 | 1059.34 | 78.88 |
| 8/13/2013 12:26:12 PM | 1.43667 | 1059.33 | 78.89 |
| 8/13/2013 12:26:13 PM | 1.43694 | 1059.33 | 78.89 |
| 8/13/2013 12:26:14 PM | 1.43722 | 1059.32 | 78.89 |
| 8/13/2013 12:26:15 PM | 1.43750 | 1059.32 | 78.89 |
| 8/13/2013 12:26:16 PM | 1.43778 | 1059.32 | 78.89 |
| 8/13/2013 12:26:17 PM | 1.43806 | 1059.31 | 78.89 |
| 8/13/2013 12:26:18 PM | 1.43833 | 1059.31 | 78.89 |
| 8/13/2013 12:26:19 PM | 1.43861 | 1059.30 | 78.89 |
| 8/13/2013 12:26:20 PM | 1.43889 | 1059.30 | 78.89 |
| 8/13/2013 12:26:21 PM | 1.43917 | 1059.29 | 78.90 |
| 8/13/2013 12:26:22 PM | 1.43944 | 1059.29 | 78.90 |
| 8/13/2013 12:26:23 PM | 1.43972 | 1059.28 | 78.90 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:26:24 PM | 1.44000 | 1059.28 | 78.90 |
| 8/13/2013 12:26:25 PM | 1.44028 | 1059.28 | 78.90 |
| 8/13/2013 12:26:26 PM | 1.44056 | 1059.27 | 78.90 |
| 8/13/2013 12:26:27 PM | 1.44083 | 1059.27 | 78.90 |
| 8/13/2013 12:26:28 PM | 1.44111 | 1059.27 | 78.90 |
| 8/13/2013 12:26:29 PM | 1.44139 | 1059.26 | 78.91 |
| 8/13/2013 12:26:30 PM | 1.44167 | 1059.26 | 78.91 |
| 8/13/2013 12:26:31 PM | 1.44194 | 1059.25 | 78.91 |
| 8/13/2013 12:26:32 PM | 1.44222 | 1059.25 | 78.91 |
| 8/13/2013 12:26:33 PM | 1.44250 | 1059.24 | 78.91 |
| 8/13/2013 12:26:34 PM | 1.44278 | 1059.24 | 78.91 |
| 8/13/2013 12:26:35 PM | 1.44306 | 1059.23 | 78.91 |
| 8/13/2013 12:26:36 PM | 1.44333 | 1059.23 | 78.91 |
| 8/13/2013 12:26:37 PM | 1.44361 | 1059.23 | 78.91 |
| 8/13/2013 12:26:38 PM | 1.44389 | 1059.22 | 78.92 |
| 8/13/2013 12:26:39 PM | 1.44417 | 1059.22 | 78.92 |
| 8/13/2013 12:26:40 PM | 1.44444 | 1059.21 | 78.92 |
| 8/13/2013 12:26:41 PM | 1.44472 | 1059.21 | 78.92 |
| 8/13/2013 12:26:42 PM | 1.44500 | 1059.21 | 78.92 |
| 8/13/2013 12:26:43 PM | 1.44528 | 1059.21 | 78.92 |
| 8/13/2013 12:26:44 PM | 1.44556 | 1059.20 | 78.92 |
| 8/13/2013 12:26:45 PM | 1.44583 | 1059.20 | 78.92 |
| 8/13/2013 12:26:46 PM | 1.44611 | 1059.20 | 78.92 |
| 8/13/2013 12:26:47 PM | 1.44639 | 1059.19 | 78.92 |
| 8/13/2013 12:26:48 PM | 1.44667 | 1059.19 | 78.92 |
| 8/13/2013 12:26:49 PM | 1.44694 | 1059.19 | 78.92 |
| 8/13/2013 12:26:50 PM | 1.44722 | 1059.19 | 78.92 |
| 8/13/2013 12:26:51 PM | 1.44750 | 1059.18 | 78.93 |
| 8/13/2013 12:26:52 PM | 1.44778 | 1059.18 | 78.93 |
| 8/13/2013 12:26:53 PM | 1.44806 | 1059.17 | 78.93 |
| 8/13/2013 12:26:54 PM | 1.44833 | 1059.17 | 78.93 |
| 8/13/2013 12:26:55 PM | 1.44861 | 1059.17 | 78.93 |
| 8/13/2013 12:26:56 PM | 1.44889 | 1059.16 | 78.93 |
| 8/13/2013 12:26:57 PM | 1.44917 | 1059.16 | 78.93 |
| 8/13/2013 12:26:58 PM | 1.44944 | 1059.16 | 78.93 |
| 8/13/2013 12:26:59 PM | 1.44972 | 1059.16 | 78.93 |
| 8/13/2013 12:27:00 PM | 1.45000 | 1059.15 | 78.93 |
| 8/13/2013 12:27:01 PM | 1.45028 | 1059.15 | 78.93 |
| 8/13/2013 12:27:02 PM | 1.45056 | 1059.15 | 78.93 |
| 8/13/2013 12:27:03 PM | 1.45083 | 1059.15 | 78.93 |
| 8/13/2013 12:27:04 PM | 1.45111 | 1059.14 | 78.93 |
| 8/13/2013 12:27:05 PM | 1.45139 | 1059.14 | 78.94 |
| 8/13/2013 12:27:06 PM | 1.45167 | 1059.14 | 78.94 |
| 8/13/2013 12:27:07 PM | 1.45194 | 1059.13 | 78.94 |
| 8/13/2013 12:27:08 PM | 1.45222 | 1059.13 | 78.94 |
| 8/13/2013 12:27:09 PM | 1.45250 | 1059.13 | 78.94 |
| 8/13/2013 12:27:10 PM | 1.45278 | 1059.12 | 78.94 |
| 8/13/2013 12:27:11 PM | 1.45306 | 1059.12 | 78.94 |
| 8/13/2013 12:27:12 PM | 1.45333 | 1059.12 | 78.94 |
| 8/13/2013 12:27:13 PM | 1.45361 | 1059.11 | 78.94 |
| 8/13/2013 12:27:14 PM | 1.45389 | 1059.11 | 78.94 |
| 8/13/2013 12:27:15 PM | 1.45417 | 1059.11 | 78.94 |
| 8/13/2013 12:27:16 PM | 1.45444 | 1059.10 | 78.94 |
| 8/13/2013 12:27:17 PM | 1.45472 | 1059.10 | 78.94 |
| 8/13/2013 12:27:18 PM | 1.45500 | 1059.10 | 78.94 |
| 8/13/2013 12:27:19 PM | 1.45528 | 1059.09 | 78.94 |
| 8/13/2013 12:27:20 PM | 1.45556 | 1059.09 | 78.94 |
| 8/13/2013 12:27:21 PM | 1.45583 | 1059.09 | 78.94 |
| 8/13/2013 12:27:22 PM | 1.45611 | 1059.08 | 78.94 |
| 8/13/2013 12:27:23 PM | 1.45639 | 1059.08 | 78.94 |
| 8/13/2013 12:27:24 PM | 1.45667 | 1059.08 | 78.94 |
| 8/13/2013 12:27:25 PM | 1.45694 | 1059.08 | 78.94 |
| 8/13/2013 12:27:26 PM | 1.45722 | 1059.08 | 78.94 |
| 8/13/2013 12:27:27 PM | 1.45750 | 1059.07 | 78.94 |
| 8/13/2013 12:27:28 PM | 1.45778 | 1059.07 | 78.94 |
| 8/13/2013 12:27:29 PM | 1.45806 | 1059.07 | 78.94 |
| 8/13/2013 12:27:30 PM | 1.45833 | 1059.07 | 78.94 |
| 8/13/2013 12:27:31 PM | 1.45861 | 1059.06 | 78.94 |
| 8/13/2013 12:27:32 PM | 1.45889 | 1059.06 | 78.94 |
| 8/13/2013 12:27:33 PM | 1.45917 | 1059.06 | 78.94 |
| 8/13/2013 12:27:34 PM | 1.45944 | 1059.05 | 78.94 |
| 8/13/2013 12:27:35 PM | 1.45972 | 1059.05 | 78.94 |
| 8/13/2013 12:27:36 PM | 1.46000 | 1059.05 | 78.94 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:27:37 PM | 1.46028 | 1059.05 | 78.94 |
| 8/13/2013 12:27:38 PM | 1.46056 | 1059.05 | 78.94 |
| 8/13/2013 12:27:39 PM | 1.46083 | 1059.04 | 78.94 |
| 8/13/2013 12:27:40 PM | 1.46111 | 1059.04 | 78.94 |
| 8/13/2013 12:27:41 PM | 1.46139 | 1059.04 | 78.94 |
| 8/13/2013 12:27:42 PM | 1.46167 | 1059.04 | 78.94 |
| 8/13/2013 12:27:43 PM | 1.46194 | 1059.03 | 78.94 |
| 8/13/2013 12:27:44 PM | 1.46222 | 1059.03 | 78.94 |
| 8/13/2013 12:27:45 PM | 1.46250 | 1059.03 | 78.94 |
| 8/13/2013 12:27:46 PM | 1.46278 | 1059.02 | 78.94 |
| 8/13/2013 12:27:47 PM | 1.46306 | 1059.02 | 78.94 |
| 8/13/2013 12:27:48 PM | 1.46333 | 1059.02 | 78.94 |
| 8/13/2013 12:27:49 PM | 1.46361 | 1059.01 | 78.94 |
| 8/13/2013 12:27:50 PM | 1.46389 | 1059.01 | 78.94 |
| 8/13/2013 12:27:51 PM | 1.46417 | 1059.01 | 78.94 |
| 8/13/2013 12:27:52 PM | 1.46444 | 1059.00 | 78.94 |
| 8/13/2013 12:27:53 PM | 1.46472 | 1059.00 | 78.94 |
| 8/13/2013 12:27:54 PM | 1.46500 | 1058.99 | 78.94 |
| 8/13/2013 12:27:55 PM | 1.46528 | 1058.99 | 78.94 |
| 8/13/2013 12:27:56 PM | 1.46556 | 1058.99 | 78.94 |
| 8/13/2013 12:27:57 PM | 1.46583 | 1058.98 | 78.94 |
| 8/13/2013 12:27:58 PM | 1.46611 | 1058.98 | 78.94 |
| 8/13/2013 12:27:59 PM | 1.46639 | 1058.98 | 78.94 |
| 8/13/2013 12:28:00 PM | 1.46667 | 1058.98 | 78.94 |
| 8/13/2013 12:28:01 PM | 1.46694 | 1058.98 | 78.94 |
| 8/13/2013 12:28:02 PM | 1.46722 | 1058.98 | 78.94 |
| 8/13/2013 12:28:03 PM | 1.46750 | 1058.97 | 78.94 |
| 8/13/2013 12:28:04 PM | 1.46778 | 1058.97 | 78.94 |
| 8/13/2013 12:28:05 PM | 1.46806 | 1058.97 | 78.94 |
| 8/13/2013 12:28:06 PM | 1.46833 | 1058.97 | 78.94 |
| 8/13/2013 12:28:07 PM | 1.46861 | 1058.97 | 78.94 |
| 8/13/2013 12:28:08 PM | 1.46889 | 1058.97 | 78.94 |
| 8/13/2013 12:28:09 PM | 1.46917 | 1058.97 | 78.94 |
| 8/13/2013 12:28:10 PM | 1.46944 | 1058.96 | 78.94 |
| 8/13/2013 12:28:11 PM | 1.46972 | 1058.96 | 78.94 |
| 8/13/2013 12:28:12 PM | 1.47000 | 1058.96 | 78.94 |
| 8/13/2013 12:28:13 PM | 1.47028 | 1058.95 | 78.94 |
| 8/13/2013 12:28:14 PM | 1.47056 | 1058.95 | 78.94 |
| 8/13/2013 12:28:15 PM | 1.47083 | 1058.95 | 78.94 |
| 8/13/2013 12:28:16 PM | 1.47111 | 1058.95 | 78.94 |
| 8/13/2013 12:28:17 PM | 1.47139 | 1058.94 | 78.94 |
| 8/13/2013 12:28:18 PM | 1.47167 | 1058.94 | 78.94 |
| 8/13/2013 12:28:19 PM | 1.47194 | 1058.94 | 78.94 |
| 8/13/2013 12:28:20 PM | 1.47222 | 1058.94 | 78.94 |
| 8/13/2013 12:28:21 PM | 1.47250 | 1058.94 | 78.94 |
| 8/13/2013 12:28:22 PM | 1.47278 | 1058.94 | 78.94 |
| 8/13/2013 12:28:23 PM | 1.47306 | 1058.93 | 78.94 |
| 8/13/2013 12:28:24 PM | 1.47333 | 1058.93 | 78.94 |
| 8/13/2013 12:28:25 PM | 1.47361 | 1058.93 | 78.94 |
| 8/13/2013 12:28:26 PM | 1.47389 | 1058.93 | 78.94 |
| 8/13/2013 12:28:27 PM | 1.47417 | 1058.93 | 78.94 |
| 8/13/2013 12:28:28 PM | 1.47444 | 1058.92 | 78.94 |
| 8/13/2013 12:28:29 PM | 1.47472 | 1058.92 | 78.94 |
| 8/13/2013 12:28:30 PM | 1.47500 | 1058.92 | 78.94 |
| 8/13/2013 12:28:31 PM | 1.47528 | 1058.92 | 78.94 |
| 8/13/2013 12:28:32 PM | 1.47556 | 1058.92 | 78.94 |
| 8/13/2013 12:28:33 PM | 1.47583 | 1058.92 | 78.94 |
| 8/13/2013 12:28:34 PM | 1.47611 | 1058.91 | 78.94 |
| 8/13/2013 12:28:35 PM | 1.47639 | 1058.91 | 78.94 |
| 8/13/2013 12:28:36 PM | 1.47667 | 1058.91 | 78.94 |
| 8/13/2013 12:28:37 PM | 1.47694 | 1058.90 | 78.94 |
| 8/13/2013 12:28:38 PM | 1.47722 | 1058.90 | 78.94 |
| 8/13/2013 12:28:39 PM | 1.47750 | 1058.90 | 78.94 |
| 8/13/2013 12:28:40 PM | 1.47778 | 1058.90 | 78.94 |
| 8/13/2013 12:28:41 PM | 1.47806 | 1058.89 | 78.94 |
| 8/13/2013 12:28:42 PM | 1.47833 | 1058.89 | 78.94 |
| 8/13/2013 12:28:43 PM | 1.47861 | 1058.89 | 78.93 |
| 8/13/2013 12:28:44 PM | 1.47889 | 1058.89 | 78.93 |
| 8/13/2013 12:28:45 PM | 1.47917 | 1058.89 | 78.93 |
| 8/13/2013 12:28:46 PM | 1.47944 | 1058.89 | 78.93 |
| 8/13/2013 12:28:47 PM | 1.47972 | 1058.89 | 78.93 |
| 8/13/2013 12:28:48 PM | 1.48000 | 1058.89 | 78.93 |
| 8/13/2013 12:28:49 PM | 1.48028 | 1058.88 | 78.93 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:28:50 PM | 1.48056 | 1058.88 | 78.93 |
| 8/13/2013 12:28:51 PM | 1.48083 | 1058.88 | 78.93 |
| 8/13/2013 12:28:52 PM | 1.48111 | 1058.88 | 78.93 |
| 8/13/2013 12:28:53 PM | 1.48139 | 1058.88 | 78.93 |
| 8/13/2013 12:28:54 PM | 1.48167 | 1058.87 | 78.93 |
| 8/13/2013 12:28:55 PM | 1.48194 | 1058.87 | 78.93 |
| 8/13/2013 12:28:56 PM | 1.48222 | 1058.87 | 78.93 |
| 8/13/2013 12:28:57 PM | 1.48250 | 1058.87 | 78.93 |
| 8/13/2013 12:28:58 PM | 1.48278 | 1058.87 | 78.93 |
| 8/13/2013 12:28:59 PM | 1.48306 | 1058.87 | 78.93 |
| 8/13/2013 12:29:00 PM | 1.48333 | 1058.87 | 78.93 |
| 8/13/2013 12:29:01 PM | 1.48361 | 1058.87 | 78.93 |
| 8/13/2013 12:29:02 PM | 1.48389 | 1058.87 | 78.93 |
| 8/13/2013 12:29:03 PM | 1.48417 | 1058.87 | 78.93 |
| 8/13/2013 12:29:04 PM | 1.48444 | 1058.87 | 78.93 |
| 8/13/2013 12:29:05 PM | 1.48472 | 1058.87 | 78.93 |
| 8/13/2013 12:29:06 PM | 1.48500 | 1058.87 | 78.92 |
| 8/13/2013 12:29:07 PM | 1.48528 | 1058.86 | 78.92 |
| 8/13/2013 12:29:08 PM | 1.48556 | 1058.86 | 78.92 |
| 8/13/2013 12:29:09 PM | 1.48583 | 1058.86 | 78.92 |
| 8/13/2013 12:29:10 PM | 1.48611 | 1058.86 | 78.92 |
| 8/13/2013 12:29:11 PM | 1.48639 | 1058.86 | 78.92 |
| 8/13/2013 12:29:12 PM | 1.48667 | 1058.85 | 78.92 |
| 8/13/2013 12:29:13 PM | 1.48694 | 1058.85 | 78.92 |
| 8/13/2013 12:29:14 PM | 1.48722 | 1058.85 | 78.92 |
| 8/13/2013 12:29:15 PM | 1.48750 | 1058.85 | 78.92 |
| 8/13/2013 12:29:16 PM | 1.48778 | 1058.85 | 78.92 |
| 8/13/2013 12:29:17 PM | 1.48806 | 1058.85 | 78.92 |
| 8/13/2013 12:29:18 PM | 1.48833 | 1058.85 | 78.92 |
| 8/13/2013 12:29:19 PM | 1.48861 | 1058.85 | 78.92 |
| 8/13/2013 12:29:20 PM | 1.48889 | 1058.85 | 78.92 |
| 8/13/2013 12:29:21 PM | 1.48917 | 1058.85 | 78.92 |
| 8/13/2013 12:29:22 PM | 1.48944 | 1058.85 | 78.92 |
| 8/13/2013 12:29:23 PM | 1.48972 | 1058.84 | 78.92 |
| 8/13/2013 12:29:24 PM | 1.49000 | 1058.84 | 78.92 |
| 8/13/2013 12:29:25 PM | 1.49028 | 1058.84 | 78.92 |
| 8/13/2013 12:29:26 PM | 1.49056 | 1058.84 | 78.92 |
| 8/13/2013 12:29:27 PM | 1.49083 | 1058.84 | 78.92 |
| 8/13/2013 12:29:28 PM | 1.49111 | 1058.84 | 78.92 |
| 8/13/2013 12:29:29 PM | 1.49139 | 1058.84 | 78.91 |
| 8/13/2013 12:29:30 PM | 1.49167 | 1058.84 | 78.91 |
| 8/13/2013 12:29:31 PM | 1.49194 | 1058.84 | 78.91 |
| 8/13/2013 12:29:32 PM | 1.49222 | 1058.84 | 78.91 |
| 8/13/2013 12:29:33 PM | 1.49250 | 1058.84 | 78.91 |
| 8/13/2013 12:29:34 PM | 1.49278 | 1058.84 | 78.91 |
| 8/13/2013 12:29:35 PM | 1.49306 | 1058.83 | 78.91 |
| 8/13/2013 12:29:36 PM | 1.49333 | 1058.83 | 78.91 |
| 8/13/2013 12:29:37 PM | 1.49361 | 1058.83 | 78.91 |
| 8/13/2013 12:29:38 PM | 1.49389 | 1058.83 | 78.91 |
| 8/13/2013 12:29:39 PM | 1.49417 | 1058.83 | 78.91 |
| 8/13/2013 12:29:40 PM | 1.49444 | 1058.83 | 78.91 |
| 8/13/2013 12:29:41 PM | 1.49472 | 1058.83 | 78.91 |
| 8/13/2013 12:29:42 PM | 1.49500 | 1058.83 | 78.91 |
| 8/13/2013 12:29:43 PM | 1.49528 | 1058.83 | 78.91 |
| 8/13/2013 12:29:44 PM | 1.49556 | 1058.83 | 78.91 |
| 8/13/2013 12:29:45 PM | 1.49583 | 1058.83 | 78.91 |
| 8/13/2013 12:29:46 PM | 1.49611 | 1058.83 | 78.91 |
| 8/13/2013 12:29:47 PM | 1.49639 | 1058.83 | 78.91 |
| 8/13/2013 12:29:48 PM | 1.49667 | 1058.83 | 78.91 |
| 8/13/2013 12:29:49 PM | 1.49694 | 1058.83 | 78.91 |
| 8/13/2013 12:29:50 PM | 1.49722 | 1058.83 | 78.91 |
| 8/13/2013 12:29:51 PM | 1.49750 | 1058.82 | 78.90 |
| 8/13/2013 12:29:52 PM | 1.49778 | 1058.82 | 78.90 |
| 8/13/2013 12:29:53 PM | 1.49806 | 1058.82 | 78.90 |
| 8/13/2013 12:29:54 PM | 1.49833 | 1058.82 | 78.90 |
| 8/13/2013 12:29:55 PM | 1.49861 | 1058.82 | 78.90 |
| 8/13/2013 12:29:56 PM | 1.49889 | 1058.82 | 78.90 |
| 8/13/2013 12:29:57 PM | 1.49917 | 1058.82 | 78.90 |
| 8/13/2013 12:29:58 PM | 1.49944 | 1058.82 | 78.90 |
| 8/13/2013 12:29:59 PM | 1.49972 | 1058.82 | 78.90 |
| 8/13/2013 12:30:00 PM | 1.50000 | 1058.82 | 78.90 |
| 8/13/2013 12:30:01 PM | 1.50028 | 1058.82 | 78.90 |
| 8/13/2013 12:30:02 PM | 1.50056 | 1058.82 | 78.90 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:30:03 PM | 1.50083 | 1058.82 | 78.90 |
| 8/13/2013 12:30:04 PM | 1.50111 | 1058.82 | 78.90 |
| 8/13/2013 12:30:05 PM | 1.50139 | 1058.82 | 78.90 |
| 8/13/2013 12:30:06 PM | 1.50167 | 1058.82 | 78.90 |
| 8/13/2013 12:30:07 PM | 1.50194 | 1058.82 | 78.90 |
| 8/13/2013 12:30:08 PM | 1.50222 | 1058.82 | 78.90 |
| 8/13/2013 12:30:09 PM | 1.50250 | 1058.81 | 78.89 |
| 8/13/2013 12:30:10 PM | 1.50278 | 1058.81 | 78.89 |
| 8/13/2013 12:30:11 PM | 1.50306 | 1058.81 | 78.89 |
| 8/13/2013 12:30:12 PM | 1.50333 | 1058.81 | 78.89 |
| 8/13/2013 12:30:13 PM | 1.50361 | 1058.81 | 78.89 |
| 8/13/2013 12:30:14 PM | 1.50389 | 1058.81 | 78.89 |
| 8/13/2013 12:30:15 PM | 1.50417 | 1058.81 | 78.89 |
| 8/13/2013 12:30:16 PM | 1.50444 | 1058.81 | 78.89 |
| 8/13/2013 12:30:17 PM | 1.50472 | 1058.81 | 78.89 |
| 8/13/2013 12:30:18 PM | 1.50500 | 1058.81 | 78.89 |
| 8/13/2013 12:30:19 PM | 1.50528 | 1058.81 | 78.89 |
| 8/13/2013 12:30:20 PM | 1.50556 | 1058.81 | 78.89 |
| 8/13/2013 12:30:21 PM | 1.50583 | 1058.82 | 78.89 |
| 8/13/2013 12:30:22 PM | 1.50611 | 1058.82 | 78.89 |
| 8/13/2013 12:30:23 PM | 1.50639 | 1058.82 | 78.89 |
| 8/13/2013 12:30:24 PM | 1.50667 | 1058.82 | 78.89 |
| 8/13/2013 12:30:25 PM | 1.50694 | 1058.82 | 78.89 |
| 8/13/2013 12:30:26 PM | 1.50722 | 1058.82 | 78.89 |
| 8/13/2013 12:30:27 PM | 1.50750 | 1058.82 | 78.89 |
| 8/13/2013 12:30:28 PM | 1.50778 | 1058.82 | 78.89 |
| 8/13/2013 12:30:29 PM | 1.50806 | 1058.82 | 78.89 |
| 8/13/2013 12:30:30 PM | 1.50833 | 1058.82 | 78.89 |
| 8/13/2013 12:30:31 PM | 1.50861 | 1058.82 | 78.89 |
| 8/13/2013 12:30:32 PM | 1.50889 | 1058.82 | 78.89 |
| 8/13/2013 12:30:33 PM | 1.50917 | 1058.81 | 78.88 |
| 8/13/2013 12:30:34 PM | 1.50944 | 1058.81 | 78.88 |
| 8/13/2013 12:30:35 PM | 1.50972 | 1058.81 | 78.88 |
| 8/13/2013 12:30:36 PM | 1.51000 | 1058.81 | 78.88 |
| 8/13/2013 12:30:37 PM | 1.51028 | 1058.81 | 78.88 |
| 8/13/2013 12:30:38 PM | 1.51056 | 1058.81 | 78.88 |
| 8/13/2013 12:30:39 PM | 1.51083 | 1058.81 | 78.88 |
| 8/13/2013 12:30:40 PM | 1.51111 | 1058.81 | 78.88 |
| 8/13/2013 12:30:41 PM | 1.51139 | 1058.81 | 78.88 |
| 8/13/2013 12:30:42 PM | 1.51167 | 1058.81 | 78.88 |
| 8/13/2013 12:30:43 PM | 1.51194 | 1058.81 | 78.88 |
| 8/13/2013 12:30:44 PM | 1.51222 | 1058.81 | 78.88 |
| 8/13/2013 12:30:45 PM | 1.51250 | 1058.81 | 78.88 |
| 8/13/2013 12:30:46 PM | 1.51278 | 1058.81 | 78.88 |
| 8/13/2013 12:30:47 PM | 1.51306 | 1058.81 | 78.88 |
| 8/13/2013 12:30:48 PM | 1.51333 | 1058.81 | 78.88 |
| 8/13/2013 12:30:49 PM | 1.51361 | 1058.81 | 78.88 |
| 8/13/2013 12:30:50 PM | 1.51389 | 1058.81 | 78.88 |
| 8/13/2013 12:30:51 PM | 1.51417 | 1058.80 | 78.87 |
| 8/13/2013 12:30:52 PM | 1.51444 | 1058.80 | 78.87 |
| 8/13/2013 12:30:53 PM | 1.51472 | 1058.80 | 78.87 |
| 8/13/2013 12:30:54 PM | 1.51500 | 1058.80 | 78.87 |
| 8/13/2013 12:30:55 PM | 1.51528 | 1058.80 | 78.87 |
| 8/13/2013 12:30:56 PM | 1.51556 | 1058.80 | 78.87 |
| 8/13/2013 12:30:57 PM | 1.51583 | 1058.80 | 78.87 |
| 8/13/2013 12:30:58 PM | 1.51611 | 1058.80 | 78.87 |
| 8/13/2013 12:30:59 PM | 1.51639 | 1058.80 | 78.87 |
| 8/13/2013 12:31:00 PM | 1.51667 | 1058.80 | 78.87 |
| 8/13/2013 12:31:01 PM | 1.51694 | 1058.80 | 78.87 |
| 8/13/2013 12:31:02 PM | 1.51722 | 1058.80 | 78.87 |
| 8/13/2013 12:31:03 PM | 1.51750 | 1058.80 | 78.87 |
| 8/13/2013 12:31:04 PM | 1.51778 | 1058.80 | 78.87 |
| 8/13/2013 12:31:05 PM | 1.51806 | 1058.80 | 78.87 |
| 8/13/2013 12:31:06 PM | 1.51833 | 1058.79 | 78.87 |
| 8/13/2013 12:31:07 PM | 1.51861 | 1058.79 | 78.87 |
| 8/13/2013 12:31:08 PM | 1.51889 | 1058.79 | 78.87 |
| 8/13/2013 12:31:09 PM | 1.51917 | 1058.79 | 78.87 |
| 8/13/2013 12:31:10 PM | 1.51944 | 1058.80 | 78.87 |
| 8/13/2013 12:31:11 PM | 1.51972 | 1058.80 | 78.86 |
| 8/13/2013 12:31:12 PM | 1.52000 | 1058.80 | 78.86 |
| 8/13/2013 12:31:13 PM | 1.52028 | 1058.80 | 78.86 |
| 8/13/2013 12:31:14 PM | 1.52056 | 1058.80 | 78.86 |
| 8/13/2013 12:31:15 PM | 1.52083 | 1058.80 | 78.86 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:31:16 PM | 1.52111 | 1058.80 | 78.86 |
| 8/13/2013 12:31:17 PM | 1.52139 | 1058.80 | 78.86 |
| 8/13/2013 12:31:18 PM | 1.52167 | 1058.80 | 78.86 |
| 8/13/2013 12:31:19 PM | 1.52194 | 1058.80 | 78.86 |
| 8/13/2013 12:31:20 PM | 1.52222 | 1058.80 | 78.86 |
| 8/13/2013 12:31:21 PM | 1.52250 | 1058.80 | 78.86 |
| 8/13/2013 12:31:22 PM | 1.52278 | 1058.80 | 78.86 |
| 8/13/2013 12:31:23 PM | 1.52306 | 1058.81 | 78.86 |
| 8/13/2013 12:31:24 PM | 1.52333 | 1058.81 | 78.86 |
| 8/13/2013 12:31:25 PM | 1.52361 | 1058.81 | 78.86 |
| 8/13/2013 12:31:26 PM | 1.52389 | 1058.81 | 78.86 |
| 8/13/2013 12:31:27 PM | 1.52417 | 1058.81 | 78.86 |
| 8/13/2013 12:31:28 PM | 1.52444 | 1058.81 | 78.86 |
| 8/13/2013 12:31:29 PM | 1.52472 | 1058.81 | 78.86 |
| 8/13/2013 12:31:30 PM | 1.52500 | 1058.81 | 78.86 |
| 8/13/2013 12:31:31 PM | 1.52528 | 1058.81 | 78.86 |
| 8/13/2013 12:31:32 PM | 1.52556 | 1058.81 | 78.86 |
| 8/13/2013 12:31:33 PM | 1.52583 | 1058.81 | 78.86 |
| 8/13/2013 12:31:34 PM | 1.52611 | 1058.81 | 78.86 |
| 8/13/2013 12:31:35 PM | 1.52639 | 1058.81 | 78.85 |
| 8/13/2013 12:31:36 PM | 1.52667 | 1058.81 | 78.85 |
| 8/13/2013 12:31:37 PM | 1.52694 | 1058.81 | 78.85 |
| 8/13/2013 12:31:38 PM | 1.52722 | 1058.81 | 78.85 |
| 8/13/2013 12:31:39 PM | 1.52750 | 1058.81 | 78.85 |
| 8/13/2013 12:31:40 PM | 1.52778 | 1058.81 | 78.85 |
| 8/13/2013 12:31:41 PM | 1.52806 | 1058.81 | 78.85 |
| 8/13/2013 12:31:42 PM | 1.52833 | 1058.80 | 78.85 |
| 8/13/2013 12:31:43 PM | 1.52861 | 1058.80 | 78.85 |
| 8/13/2013 12:31:44 PM | 1.52889 | 1058.80 | 78.85 |
| 8/13/2013 12:31:45 PM | 1.52917 | 1058.80 | 78.85 |
| 8/13/2013 12:31:46 PM | 1.52944 | 1058.80 | 78.85 |
| 8/13/2013 12:31:47 PM | 1.52972 | 1058.80 | 78.85 |
| 8/13/2013 12:31:48 PM | 1.53000 | 1058.80 | 78.85 |
| 8/13/2013 12:31:49 PM | 1.53028 | 1058.80 | 78.85 |
| 8/13/2013 12:31:50 PM | 1.53056 | 1058.80 | 78.85 |
| 8/13/2013 12:31:51 PM | 1.53083 | 1058.80 | 78.85 |
| 8/13/2013 12:31:52 PM | 1.53111 | 1058.80 | 78.85 |
| 8/13/2013 12:31:53 PM | 1.53139 | 1058.80 | 78.84 |
| 8/13/2013 12:31:54 PM | 1.53167 | 1058.80 | 78.84 |
| 8/13/2013 12:31:55 PM | 1.53194 | 1058.80 | 78.84 |
| 8/13/2013 12:31:56 PM | 1.53222 | 1058.80 | 78.84 |
| 8/13/2013 12:31:57 PM | 1.53250 | 1058.80 | 78.84 |
| 8/13/2013 12:31:58 PM | 1.53278 | 1058.80 | 78.84 |
| 8/13/2013 12:31:59 PM | 1.53306 | 1058.80 | 78.84 |
| 8/13/2013 12:32:00 PM | 1.53333 | 1058.80 | 78.84 |
| 8/13/2013 12:32:01 PM | 1.53361 | 1058.80 | 78.84 |
| 8/13/2013 12:32:02 PM | 1.53389 | 1058.80 | 78.84 |
| 8/13/2013 12:32:03 PM | 1.53417 | 1058.80 | 78.84 |
| 8/13/2013 12:32:04 PM | 1.53444 | 1058.80 | 78.84 |
| 8/13/2013 12:32:05 PM | 1.53472 | 1058.80 | 78.84 |
| 8/13/2013 12:32:06 PM | 1.53500 | 1058.80 | 78.84 |
| 8/13/2013 12:32:07 PM | 1.53528 | 1058.80 | 78.84 |
| 8/13/2013 12:32:08 PM | 1.53556 | 1058.81 | 78.84 |
| 8/13/2013 12:32:09 PM | 1.53583 | 1058.81 | 78.84 |
| 8/13/2013 12:32:10 PM | 1.53611 | 1058.81 | 78.84 |
| 8/13/2013 12:32:11 PM | 1.53639 | 1058.81 | 78.84 |
| 8/13/2013 12:32:12 PM | 1.53667 | 1058.81 | 78.84 |
| 8/13/2013 12:32:13 PM | 1.53694 | 1058.81 | 78.84 |
| 8/13/2013 12:32:14 PM | 1.53722 | 1058.81 | 78.83 |
| 8/13/2013 12:32:15 PM | 1.53750 | 1058.81 | 78.83 |
| 8/13/2013 12:32:16 PM | 1.53778 | 1058.81 | 78.83 |
| 8/13/2013 12:32:17 PM | 1.53806 | 1058.81 | 78.83 |
| 8/13/2013 12:32:18 PM | 1.53833 | 1058.81 | 78.83 |
| 8/13/2013 12:32:19 PM | 1.53861 | 1058.81 | 78.83 |
| 8/13/2013 12:32:20 PM | 1.53889 | 1058.81 | 78.83 |
| 8/13/2013 12:32:21 PM | 1.53917 | 1058.81 | 78.83 |
| 8/13/2013 12:32:22 PM | 1.53944 | 1058.81 | 78.83 |
| 8/13/2013 12:32:23 PM | 1.53972 | 1058.81 | 78.83 |
| 8/13/2013 12:32:24 PM | 1.54000 | 1058.81 | 78.83 |
| 8/13/2013 12:32:25 PM | 1.54028 | 1058.81 | 78.83 |
| 8/13/2013 12:32:26 PM | 1.54056 | 1058.81 | 78.83 |
| 8/13/2013 12:32:27 PM | 1.54083 | 1058.81 | 78.83 |
| 8/13/2013 12:32:28 PM | 1.54111 | 1058.81 | 78.83 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:32:29 PM | 1.54139 | 1058.81 | 78.83 |
| 8/13/2013 12:32:30 PM | 1.54167 | 1058.81 | 78.83 |
| 8/13/2013 12:32:31 PM | 1.54194 | 1058.81 | 78.83 |
| 8/13/2013 12:32:32 PM | 1.54222 | 1058.81 | 78.83 |
| 8/13/2013 12:32:33 PM | 1.54250 | 1058.81 | 78.83 |
| 8/13/2013 12:32:34 PM | 1.54278 | 1058.81 | 78.83 |
| 8/13/2013 12:32:35 PM | 1.54306 | 1058.82 | 78.83 |
| 8/13/2013 12:32:36 PM | 1.54333 | 1058.82 | 78.83 |
| 8/13/2013 12:32:37 PM | 1.54361 | 1058.82 | 78.83 |
| 8/13/2013 12:32:38 PM | 1.54389 | 1058.82 | 78.83 |
| 8/13/2013 12:32:39 PM | 1.54417 | 1058.82 | 78.83 |
| 8/13/2013 12:32:40 PM | 1.54444 | 1058.82 | 78.83 |
| 8/13/2013 12:32:41 PM | 1.54472 | 1058.82 | 78.83 |
| 8/13/2013 12:32:42 PM | 1.54500 | 1058.82 | 78.82 |
| 8/13/2013 12:32:43 PM | 1.54528 | 1058.82 | 78.82 |
| 8/13/2013 12:32:44 PM | 1.54556 | 1058.82 | 78.82 |
| 8/13/2013 12:32:45 PM | 1.54583 | 1058.82 | 78.82 |
| 8/13/2013 12:32:46 PM | 1.54611 | 1058.82 | 78.82 |
| 8/13/2013 12:32:47 PM | 1.54639 | 1058.82 | 78.82 |
| 8/13/2013 12:32:48 PM | 1.54667 | 1058.82 | 78.82 |
| 8/13/2013 12:32:49 PM | 1.54694 | 1058.82 | 78.82 |
| 8/13/2013 12:32:50 PM | 1.54722 | 1058.83 | 78.82 |
| 8/13/2013 12:32:51 PM | 1.54750 | 1058.83 | 78.82 |
| 8/13/2013 12:32:52 PM | 1.54778 | 1058.83 | 78.82 |
| 8/13/2013 12:32:53 PM | 1.54806 | 1058.83 | 78.82 |
| 8/13/2013 12:32:54 PM | 1.54833 | 1058.83 | 78.82 |
| 8/13/2013 12:32:55 PM | 1.54861 | 1058.83 | 78.82 |
| 8/13/2013 12:32:56 PM | 1.54889 | 1058.83 | 78.82 |
| 8/13/2013 12:32:57 PM | 1.54917 | 1058.83 | 78.82 |
| 8/13/2013 12:32:58 PM | 1.54944 | 1058.84 | 78.82 |
| 8/13/2013 12:32:59 PM | 1.54972 | 1058.84 | 78.82 |
| 8/13/2013 12:33:00 PM | 1.55000 | 1058.84 | 78.82 |
| 8/13/2013 12:33:01 PM | 1.55028 | 1058.84 | 78.82 |
| 8/13/2013 12:33:02 PM | 1.55056 | 1058.84 | 78.82 |
| 8/13/2013 12:33:03 PM | 1.55083 | 1058.85 | 78.82 |
| 8/13/2013 12:33:04 PM | 1.55111 | 1058.85 | 78.82 |
| 8/13/2013 12:33:05 PM | 1.55139 | 1058.85 | 78.82 |
| 8/13/2013 12:33:06 PM | 1.55167 | 1058.85 | 78.81 |
| 8/13/2013 12:33:07 PM | 1.55194 | 1058.85 | 78.81 |
| 8/13/2013 12:33:08 PM | 1.55222 | 1058.85 | 78.81 |
| 8/13/2013 12:33:09 PM | 1.55250 | 1058.85 | 78.81 |
| 8/13/2013 12:33:10 PM | 1.55278 | 1058.85 | 78.81 |
| 8/13/2013 12:33:11 PM | 1.55306 | 1058.85 | 78.81 |
| 8/13/2013 12:33:12 PM | 1.55333 | 1058.85 | 78.81 |
| 8/13/2013 12:33:13 PM | 1.55361 | 1058.84 | 78.81 |
| 8/13/2013 12:33:14 PM | 1.55389 | 1058.84 | 78.81 |
| 8/13/2013 12:33:15 PM | 1.55417 | 1058.84 | 78.81 |
| 8/13/2013 12:33:16 PM | 1.55444 | 1058.84 | 78.81 |
| 8/13/2013 12:33:17 PM | 1.55472 | 1058.84 | 78.81 |
| 8/13/2013 12:33:18 PM | 1.55500 | 1058.84 | 78.81 |
| 8/13/2013 12:33:19 PM | 1.55528 | 1058.84 | 78.81 |
| 8/13/2013 12:33:20 PM | 1.55556 | 1058.84 | 78.81 |
| 8/13/2013 12:33:21 PM | 1.55583 | 1058.84 | 78.81 |
| 8/13/2013 12:33:22 PM | 1.55611 | 1058.85 | 78.81 |
| 8/13/2013 12:33:23 PM | 1.55639 | 1058.85 | 78.81 |
| 8/13/2013 12:33:24 PM | 1.55667 | 1058.85 | 78.81 |
| 8/13/2013 12:33:25 PM | 1.55694 | 1058.85 | 78.81 |
| 8/13/2013 12:33:26 PM | 1.55722 | 1058.85 | 78.81 |
| 8/13/2013 12:33:27 PM | 1.55750 | 1058.85 | 78.81 |
| 8/13/2013 12:33:28 PM | 1.55778 | 1058.85 | 78.81 |
| 8/13/2013 12:33:29 PM | 1.55806 | 1058.85 | 78.81 |
| 8/13/2013 12:33:30 PM | 1.55833 | 1058.85 | 78.81 |
| 8/13/2013 12:33:31 PM | 1.55861 | 1058.85 | 78.81 |
| 8/13/2013 12:33:32 PM | 1.55889 | 1058.85 | 78.81 |
| 8/13/2013 12:33:33 PM | 1.55917 | 1058.85 | 78.81 |
| 8/13/2013 12:33:34 PM | 1.55944 | 1058.86 | 78.81 |
| 8/13/2013 12:33:35 PM | 1.55972 | 1058.86 | 78.81 |
| 8/13/2013 12:33:36 PM | 1.56000 | 1058.86 | 78.80 |
| 8/13/2013 12:33:37 PM | 1.56028 | 1058.86 | 78.80 |
| 8/13/2013 12:33:38 PM | 1.56056 | 1058.86 | 78.80 |
| 8/13/2013 12:33:39 PM | 1.56083 | 1058.86 | 78.80 |
| 8/13/2013 12:33:40 PM | 1.56111 | 1058.86 | 78.80 |
| 8/13/2013 12:33:41 PM | 1.56139 | 1058.86 | 78.80 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:33:42 PM | 1.56167 | 1058.86 | 78.80 |
| 8/13/2013 12:33:43 PM | 1.56194 | 1058.86 | 78.80 |
| 8/13/2013 12:33:44 PM | 1.56222 | 1058.86 | 78.80 |
| 8/13/2013 12:33:45 PM | 1.56250 | 1058.86 | 78.80 |
| 8/13/2013 12:33:46 PM | 1.56278 | 1058.87 | 78.80 |
| 8/13/2013 12:33:47 PM | 1.56306 | 1058.87 | 78.80 |
| 8/13/2013 12:33:48 PM | 1.56333 | 1058.87 | 78.80 |
| 8/13/2013 12:33:49 PM | 1.56361 | 1058.87 | 78.80 |
| 8/13/2013 12:33:50 PM | 1.56389 | 1058.87 | 78.80 |
| 8/13/2013 12:33:51 PM | 1.56417 | 1058.87 | 78.80 |
| 8/13/2013 12:33:52 PM | 1.56444 | 1058.87 | 78.80 |
| 8/13/2013 12:33:53 PM | 1.56472 | 1058.87 | 78.80 |
| 8/13/2013 12:33:54 PM | 1.56500 | 1058.87 | 78.80 |
| 8/13/2013 12:33:55 PM | 1.56528 | 1058.87 | 78.80 |
| 8/13/2013 12:33:56 PM | 1.56556 | 1058.87 | 78.80 |
| 8/13/2013 12:33:57 PM | 1.56583 | 1058.87 | 78.80 |
| 8/13/2013 12:33:58 PM | 1.56611 | 1058.87 | 78.80 |
| 8/13/2013 12:33:59 PM | 1.56639 | 1058.87 | 78.80 |
| 8/13/2013 12:34:00 PM | 1.56667 | 1058.87 | 78.79 |
| 8/13/2013 12:34:01 PM | 1.56694 | 1058.87 | 78.79 |
| 8/13/2013 12:34:02 PM | 1.56722 | 1058.87 | 78.79 |
| 8/13/2013 12:34:03 PM | 1.56750 | 1058.87 | 78.79 |
| 8/13/2013 12:34:04 PM | 1.56778 | 1058.87 | 78.79 |
| 8/13/2013 12:34:05 PM | 1.56806 | 1058.87 | 78.79 |
| 8/13/2013 12:34:06 PM | 1.56833 | 1058.88 | 78.79 |
| 8/13/2013 12:34:07 PM | 1.56861 | 1058.88 | 78.79 |
| 8/13/2013 12:34:08 PM | 1.56889 | 1058.88 | 78.79 |
| 8/13/2013 12:34:09 PM | 1.56917 | 1058.88 | 78.79 |
| 8/13/2013 12:34:10 PM | 1.56944 | 1058.88 | 78.79 |
| 8/13/2013 12:34:11 PM | 1.56972 | 1058.88 | 78.79 |
| 8/13/2013 12:34:12 PM | 1.57000 | 1058.88 | 78.79 |
| 8/13/2013 12:34:13 PM | 1.57028 | 1058.88 | 78.79 |
| 8/13/2013 12:34:14 PM | 1.57056 | 1058.88 | 78.79 |
| 8/13/2013 12:34:15 PM | 1.57083 | 1058.88 | 78.79 |
| 8/13/2013 12:34:16 PM | 1.57111 | 1058.88 | 78.79 |
| 8/13/2013 12:34:17 PM | 1.57139 | 1058.88 | 78.79 |
| 8/13/2013 12:34:18 PM | 1.57167 | 1058.89 | 78.79 |
| 8/13/2013 12:34:19 PM | 1.57194 | 1058.89 | 78.79 |
| 8/13/2013 12:34:20 PM | 1.57222 | 1058.89 | 78.79 |
| 8/13/2013 12:34:21 PM | 1.57250 | 1058.89 | 78.79 |
| 8/13/2013 12:34:22 PM | 1.57278 | 1058.89 | 78.79 |
| 8/13/2013 12:34:23 PM | 1.57306 | 1058.88 | 78.78 |
| 8/13/2013 12:34:24 PM | 1.57333 | 1058.88 | 78.78 |
| 8/13/2013 12:34:25 PM | 1.57361 | 1058.88 | 78.78 |
| 8/13/2013 12:34:26 PM | 1.57389 | 1058.88 | 78.78 |
| 8/13/2013 12:34:27 PM | 1.57417 | 1058.88 | 78.78 |
| 8/13/2013 12:34:28 PM | 1.57444 | 1058.88 | 78.78 |
| 8/13/2013 12:34:29 PM | 1.57472 | 1058.88 | 78.78 |
| 8/13/2013 12:34:30 PM | 1.57500 | 1058.88 | 78.78 |
| 8/13/2013 12:34:31 PM | 1.57528 | 1058.88 | 78.78 |
| 8/13/2013 12:34:32 PM | 1.57556 | 1058.88 | 78.78 |
| 8/13/2013 12:34:33 PM | 1.57583 | 1058.88 | 78.78 |
| 8/13/2013 12:34:34 PM | 1.57611 | 1058.88 | 78.78 |
| 8/13/2013 12:34:35 PM | 1.57639 | 1058.88 | 78.78 |
| 8/13/2013 12:34:36 PM | 1.57667 | 1058.88 | 78.78 |
| 8/13/2013 12:34:37 PM | 1.57694 | 1058.89 | 78.78 |
| 8/13/2013 12:34:38 PM | 1.57722 | 1058.89 | 78.78 |
| 8/13/2013 12:34:39 PM | 1.57750 | 1058.89 | 78.78 |
| 8/13/2013 12:34:40 PM | 1.57778 | 1058.89 | 78.78 |
| 8/13/2013 12:34:41 PM | 1.57806 | 1058.89 | 78.78 |
| 8/13/2013 12:34:42 PM | 1.57833 | 1058.89 | 78.78 |
| 8/13/2013 12:34:43 PM | 1.57861 | 1058.89 | 78.78 |
| 8/13/2013 12:34:44 PM | 1.57889 | 1058.89 | 78.78 |
| 8/13/2013 12:34:45 PM | 1.57917 | 1058.89 | 78.78 |
| 8/13/2013 12:34:46 PM | 1.57944 | 1058.89 | 78.78 |
| 8/13/2013 12:34:47 PM | 1.57972 | 1058.89 | 78.78 |
| 8/13/2013 12:34:48 PM | 1.58000 | 1058.89 | 78.78 |
| 8/13/2013 12:34:49 PM | 1.58028 | 1058.89 | 78.77 |
| 8/13/2013 12:34:50 PM | 1.58056 | 1058.89 | 78.77 |
| 8/13/2013 12:34:51 PM | 1.58083 | 1058.89 | 78.77 |
| 8/13/2013 12:34:52 PM | 1.58111 | 1058.90 | 78.77 |
| 8/13/2013 12:34:53 PM | 1.58139 | 1058.90 | 78.77 |
| 8/13/2013 12:34:54 PM | 1.58167 | 1058.90 | 78.77 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:34:55 PM | 1.58194 | 1058.90 | 78.77 |
| 8/13/2013 12:34:56 PM | 1.58222 | 1058.90 | 78.77 |
| 8/13/2013 12:34:57 PM | 1.58250 | 1058.91 | 78.77 |
| 8/13/2013 12:34:58 PM | 1.58278 | 1058.91 | 78.77 |
| 8/13/2013 12:34:59 PM | 1.58306 | 1058.91 | 78.77 |
| 8/13/2013 12:35:00 PM | 1.58333 | 1058.91 | 78.77 |
| 8/13/2013 12:35:01 PM | 1.58361 | 1058.91 | 78.77 |
| 8/13/2013 12:35:02 PM | 1.58389 | 1058.90 | 78.77 |
| 8/13/2013 12:35:03 PM | 1.58417 | 1058.90 | 78.77 |
| 8/13/2013 12:35:04 PM | 1.58444 | 1058.90 | 78.77 |
| 8/13/2013 12:35:05 PM | 1.58472 | 1058.90 | 78.77 |
| 8/13/2013 12:35:06 PM | 1.58500 | 1058.90 | 78.77 |
| 8/13/2013 12:35:07 PM | 1.58528 | 1058.90 | 78.77 |
| 8/13/2013 12:35:08 PM | 1.58556 | 1058.90 | 78.77 |
| 8/13/2013 12:35:09 PM | 1.58583 | 1058.91 | 78.77 |
| 8/13/2013 12:35:10 PM | 1.58611 | 1058.91 | 78.76 |
| 8/13/2013 12:35:11 PM | 1.58639 | 1058.91 | 78.76 |
| 8/13/2013 12:35:12 PM | 1.58667 | 1058.91 | 78.76 |
| 8/13/2013 12:35:13 PM | 1.58694 | 1058.92 | 78.76 |
| 8/13/2013 12:35:14 PM | 1.58722 | 1058.92 | 78.76 |
| 8/13/2013 12:35:15 PM | 1.58750 | 1058.92 | 78.76 |
| 8/13/2013 12:35:16 PM | 1.58778 | 1058.92 | 78.76 |
| 8/13/2013 12:35:17 PM | 1.58806 | 1058.92 | 78.76 |
| 8/13/2013 12:35:18 PM | 1.58833 | 1058.92 | 78.76 |
| 8/13/2013 12:35:19 PM | 1.58861 | 1058.93 | 78.76 |
| 8/13/2013 12:35:20 PM | 1.58889 | 1058.93 | 78.76 |
| 8/13/2013 12:35:21 PM | 1.58917 | 1058.93 | 78.76 |
| 8/13/2013 12:35:22 PM | 1.58944 | 1058.93 | 78.76 |
| 8/13/2013 12:35:23 PM | 1.58972 | 1058.93 | 78.76 |
| 8/13/2013 12:35:24 PM | 1.59000 | 1058.93 | 78.76 |
| 8/13/2013 12:35:25 PM | 1.59028 | 1058.93 | 78.76 |
| 8/13/2013 12:35:26 PM | 1.59056 | 1058.94 | 78.76 |
| 8/13/2013 12:35:27 PM | 1.59083 | 1058.94 | 78.76 |
| 8/13/2013 12:35:28 PM | 1.59111 | 1058.94 | 78.76 |
| 8/13/2013 12:35:29 PM | 1.59139 | 1058.94 | 78.76 |
| 8/13/2013 12:35:30 PM | 1.59167 | 1058.94 | 78.76 |
| 8/13/2013 12:35:31 PM | 1.59194 | 1058.94 | 78.76 |
| 8/13/2013 12:35:32 PM | 1.59222 | 1058.94 | 78.76 |
| 8/13/2013 12:35:33 PM | 1.59250 | 1058.94 | 78.76 |
| 8/13/2013 12:35:34 PM | 1.59278 | 1058.94 | 78.76 |
| 8/13/2013 12:35:35 PM | 1.59306 | 1058.94 | 78.75 |
| 8/13/2013 12:35:36 PM | 1.59333 | 1058.94 | 78.75 |
| 8/13/2013 12:35:37 PM | 1.59361 | 1058.94 | 78.75 |
| 8/13/2013 12:35:38 PM | 1.59389 | 1058.94 | 78.75 |
| 8/13/2013 12:35:39 PM | 1.59417 | 1058.94 | 78.75 |
| 8/13/2013 12:35:40 PM | 1.59444 | 1058.94 | 78.75 |
| 8/13/2013 12:35:41 PM | 1.59472 | 1058.94 | 78.75 |
| 8/13/2013 12:35:42 PM | 1.59500 | 1058.95 | 78.75 |
| 8/13/2013 12:35:43 PM | 1.59528 | 1058.95 | 78.75 |
| 8/13/2013 12:35:44 PM | 1.59556 | 1058.95 | 78.75 |
| 8/13/2013 12:35:45 PM | 1.59583 | 1058.95 | 78.75 |
| 8/13/2013 12:35:46 PM | 1.59611 | 1058.95 | 78.75 |
| 8/13/2013 12:35:47 PM | 1.59639 | 1058.95 | 78.75 |
| 8/13/2013 12:35:48 PM | 1.59667 | 1058.95 | 78.75 |
| 8/13/2013 12:35:49 PM | 1.59694 | 1058.95 | 78.75 |
| 8/13/2013 12:35:50 PM | 1.59722 | 1058.95 | 78.75 |
| 8/13/2013 12:35:51 PM | 1.59750 | 1058.95 | 78.75 |
| 8/13/2013 12:35:52 PM | 1.59778 | 1058.95 | 78.75 |
| 8/13/2013 12:35:53 PM | 1.59806 | 1058.95 | 78.75 |
| 8/13/2013 12:35:54 PM | 1.59833 | 1058.95 | 78.75 |
| 8/13/2013 12:35:55 PM | 1.59861 | 1058.95 | 78.75 |
| 8/13/2013 12:35:56 PM | 1.59889 | 1058.96 | 78.75 |
| 8/13/2013 12:35:57 PM | 1.59917 | 1058.96 | 78.75 |
| 8/13/2013 12:35:58 PM | 1.59944 | 1058.96 | 78.75 |
| 8/13/2013 12:35:59 PM | 1.59972 | 1058.96 | 78.75 |
| 8/13/2013 12:36:00 PM | 1.60000 | 1058.97 | 78.75 |
| 8/13/2013 12:36:01 PM | 1.60028 | 1058.97 | 78.74 |
| 8/13/2013 12:36:02 PM | 1.60056 | 1058.97 | 78.74 |
| 8/13/2013 12:36:03 PM | 1.60083 | 1058.97 | 78.74 |
| 8/13/2013 12:36:04 PM | 1.60111 | 1058.97 | 78.74 |
| 8/13/2013 12:36:05 PM | 1.60139 | 1058.97 | 78.74 |
| 8/13/2013 12:36:06 PM | 1.60167 | 1058.97 | 78.74 |
| 8/13/2013 12:36:07 PM | 1.60194 | 1058.97 | 78.74 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:36:08 PM | 1.60222 | 1058.96 | 78.74 |
| 8/13/2013 12:36:09 PM | 1.60250 | 1058.96 | 78.74 |
| 8/13/2013 12:36:10 PM | 1.60278 | 1058.96 | 78.74 |
| 8/13/2013 12:36:11 PM | 1.60306 | 1058.96 | 78.74 |
| 8/13/2013 12:36:12 PM | 1.60333 | 1058.96 | 78.74 |
| 8/13/2013 12:36:13 PM | 1.60361 | 1058.96 | 78.74 |
| 8/13/2013 12:36:14 PM | 1.60389 | 1058.96 | 78.74 |
| 8/13/2013 12:36:15 PM | 1.60417 | 1058.96 | 78.74 |
| 8/13/2013 12:36:16 PM | 1.60444 | 1058.97 | 78.74 |
| 8/13/2013 12:36:17 PM | 1.60472 | 1058.97 | 78.74 |
| 8/13/2013 12:36:18 PM | 1.60500 | 1058.97 | 78.74 |
| 8/13/2013 12:36:19 PM | 1.60528 | 1058.97 | 78.74 |
| 8/13/2013 12:36:20 PM | 1.60556 | 1058.97 | 78.74 |
| 8/13/2013 12:36:21 PM | 1.60583 | 1058.97 | 78.73 |
| 8/13/2013 12:36:22 PM | 1.60611 | 1058.97 | 78.73 |
| 8/13/2013 12:36:23 PM | 1.60639 | 1058.97 | 78.73 |
| 8/13/2013 12:36:24 PM | 1.60667 | 1058.97 | 78.73 |
| 8/13/2013 12:36:25 PM | 1.60694 | 1058.97 | 78.73 |
| 8/13/2013 12:36:26 PM | 1.60722 | 1058.97 | 78.73 |
| 8/13/2013 12:36:27 PM | 1.60750 | 1058.97 | 78.73 |
| 8/13/2013 12:36:28 PM | 1.60778 | 1058.98 | 78.73 |
| 8/13/2013 12:36:29 PM | 1.60806 | 1058.97 | 78.73 |
| 8/13/2013 12:36:30 PM | 1.60833 | 1058.97 | 78.73 |
| 8/13/2013 12:36:31 PM | 1.60861 | 1058.98 | 78.73 |
| 8/13/2013 12:36:32 PM | 1.60889 | 1058.98 | 78.73 |
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| 8/13/2013 12:36:34 PM | 1.60944 | 1058.98 | 78.73 |
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| 8/13/2013 12:36:40 PM | 1.61111 | 1058.98 | 78.73 |
| 8/13/2013 12:36:41 PM | 1.61139 | 1058.98 | 78.73 |
| 8/13/2013 12:36:42 PM | 1.61167 | 1058.99 | 78.73 |
| 8/13/2013 12:36:43 PM | 1.61194 | 1058.99 | 78.72 |
| 8/13/2013 12:36:44 PM | 1.61222 | 1058.99 | 78.72 |
| 8/13/2013 12:36:45 PM | 1.61250 | 1058.99 | 78.72 |
| 8/13/2013 12:36:46 PM | 1.61278 | 1058.99 | 78.72 |
| 8/13/2013 12:36:47 PM | 1.61306 | 1059.00 | 78.72 |
| 8/13/2013 12:36:48 PM | 1.61333 | 1059.00 | 78.72 |
| 8/13/2013 12:36:49 PM | 1.61361 | 1059.00 | 78.72 |
| 8/13/2013 12:36:50 PM | 1.61389 | 1059.00 | 78.72 |
| 8/13/2013 12:36:51 PM | 1.61417 | 1059.00 | 78.72 |
| 8/13/2013 12:36:52 PM | 1.61444 | 1059.00 | 78.72 |
| 8/13/2013 12:36:53 PM | 1.61472 | 1059.00 | 78.72 |
| 8/13/2013 12:36:54 PM | 1.61500 | 1059.00 | 78.72 |
| 8/13/2013 12:36:55 PM | 1.61528 | 1059.00 | 78.72 |
| 8/13/2013 12:36:56 PM | 1.61556 | 1059.00 | 78.72 |
| 8/13/2013 12:36:57 PM | 1.61583 | 1059.01 | 78.72 |
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| 8/13/2013 12:36:59 PM | 1.61639 | 1059.01 | 78.72 |
| 8/13/2013 12:37:00 PM | 1.61667 | 1059.01 | 78.72 |
| 8/13/2013 12:37:01 PM | 1.61694 | 1059.01 | 78.72 |
| 8/13/2013 12:37:02 PM | 1.61722 | 1059.01 | 78.72 |
| 8/13/2013 12:37:03 PM | 1.61750 | 1059.01 | 78.72 |
| 8/13/2013 12:37:04 PM | 1.61778 | 1059.01 | 78.71 |
| 8/13/2013 12:37:05 PM | 1.61806 | 1059.02 | 78.71 |
| 8/13/2013 12:37:06 PM | 1.61833 | 1059.02 | 78.71 |
| 8/13/2013 12:37:07 PM | 1.61861 | 1059.02 | 78.71 |
| 8/13/2013 12:37:08 PM | 1.61889 | 1059.02 | 78.71 |
| 8/13/2013 12:37:09 PM | 1.61917 | 1059.02 | 78.71 |
| 8/13/2013 12:37:10 PM | 1.61944 | 1059.02 | 78.71 |
| 8/13/2013 12:37:11 PM | 1.61972 | 1059.02 | 78.71 |
| 8/13/2013 12:37:12 PM | 1.62000 | 1059.02 | 78.71 |
| 8/13/2013 12:37:13 PM | 1.62028 | 1059.01 | 78.71 |
| 8/13/2013 12:37:14 PM | 1.62056 | 1059.01 | 78.71 |
| 8/13/2013 12:37:15 PM | 1.62083 | 1059.01 | 78.71 |
| 8/13/2013 12:37:16 PM | 1.62111 | 1059.01 | 78.71 |
| 8/13/2013 12:37:17 PM | 1.62139 | 1059.01 | 78.71 |
| 8/13/2013 12:37:18 PM | 1.62167 | 1059.02 | 78.71 |
| 8/13/2013 12:37:19 PM | 1.62194 | 1059.02 | 78.71 |
| 8/13/2013 12:37:20 PM | 1.62222 | 1059.02 | 78.71 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:37:21 PM | 1.62250 | 1059.02 | 78.71 |
| 8/13/2013 12:37:22 PM | 1.62278 | 1059.02 | 78.70 |
| 8/13/2013 12:37:23 PM | 1.62306 | 1059.02 | 78.70 |
| 8/13/2013 12:37:24 PM | 1.62333 | 1059.03 | 78.70 |
| 8/13/2013 12:37:25 PM | 1.62361 | 1059.03 | 78.70 |
| 8/13/2013 12:37:26 PM | 1.62389 | 1059.03 | 78.70 |
| 8/13/2013 12:37:27 PM | 1.62417 | 1059.03 | 78.70 |
| 8/13/2013 12:37:28 PM | 1.62444 | 1059.03 | 78.70 |
| 8/13/2013 12:37:29 PM | 1.62472 | 1059.03 | 78.70 |
| 8/13/2013 12:37:30 PM | 1.62500 | 1059.03 | 78.70 |
| 8/13/2013 12:37:31 PM | 1.62528 | 1059.03 | 78.70 |
| 8/13/2013 12:37:32 PM | 1.62556 | 1059.03 | 78.70 |
| 8/13/2013 12:37:33 PM | 1.62583 | 1059.03 | 78.70 |
| 8/13/2013 12:37:34 PM | 1.62611 | 1059.03 | 78.70 |
| 8/13/2013 12:37:35 PM | 1.62639 | 1059.03 | 78.70 |
| 8/13/2013 12:37:36 PM | 1.62667 | 1059.03 | 78.70 |
| 8/13/2013 12:37:37 PM | 1.62694 | 1059.03 | 78.70 |
| 8/13/2013 12:37:38 PM | 1.62722 | 1059.03 | 78.70 |
| 8/13/2013 12:37:39 PM | 1.62750 | 1059.03 | 78.70 |
| 8/13/2013 12:37:40 PM | 1.62778 | 1059.03 | 78.70 |
| 8/13/2013 12:37:41 PM | 1.62806 | 1059.03 | 78.70 |
| 8/13/2013 12:37:42 PM | 1.62833 | 1059.03 | 78.70 |
| 8/13/2013 12:37:43 PM | 1.62861 | 1059.03 | 78.69 |
| 8/13/2013 12:37:44 PM | 1.62889 | 1059.03 | 78.69 |
| 8/13/2013 12:37:45 PM | 1.62917 | 1059.03 | 78.69 |
| 8/13/2013 12:37:46 PM | 1.62944 | 1059.04 | 78.69 |
| 8/13/2013 12:37:47 PM | 1.62972 | 1059.04 | 78.69 |
| 8/13/2013 12:37:48 PM | 1.63000 | 1059.04 | 78.69 |
| 8/13/2013 12:37:49 PM | 1.63028 | 1059.04 | 78.69 |
| 8/13/2013 12:37:50 PM | 1.63056 | 1059.04 | 78.69 |
| 8/13/2013 12:37:51 PM | 1.63083 | 1059.04 | 78.69 |
| 8/13/2013 12:37:52 PM | 1.63111 | 1059.04 | 78.69 |
| 8/13/2013 12:37:53 PM | 1.63139 | 1059.04 | 78.69 |
| 8/13/2013 12:37:54 PM | 1.63167 | 1059.04 | 78.69 |
| 8/13/2013 12:37:55 PM | 1.63194 | 1059.05 | 78.69 |
| 8/13/2013 12:37:56 PM | 1.63222 | 1059.04 | 78.69 |
| 8/13/2013 12:37:57 PM | 1.63250 | 1059.05 | 78.69 |
| 8/13/2013 12:37:58 PM | 1.63278 | 1059.04 | 78.69 |
| 8/13/2013 12:37:59 PM | 1.63306 | 1059.04 | 78.69 |
| 8/13/2013 12:38:00 PM | 1.63333 | 1059.04 | 78.69 |
| 8/13/2013 12:38:01 PM | 1.63361 | 1059.04 | 78.69 |
| 8/13/2013 12:38:02 PM | 1.63389 | 1059.04 | 78.69 |
| 8/13/2013 12:38:03 PM | 1.63417 | 1059.04 | 78.69 |
| 8/13/2013 12:38:04 PM | 1.63444 | 1059.05 | 78.69 |
| 8/13/2013 12:38:05 PM | 1.63472 | 1059.05 | 78.69 |
| 8/13/2013 12:38:06 PM | 1.63500 | 1059.05 | 78.69 |
| 8/13/2013 12:38:07 PM | 1.63528 | 1059.05 | 78.69 |
| 8/13/2013 12:38:08 PM | 1.63556 | 1059.05 | 78.68 |
| 8/13/2013 12:38:09 PM | 1.63583 | 1059.05 | 78.68 |
| 8/13/2013 12:38:10 PM | 1.63611 | 1059.05 | 78.68 |
| 8/13/2013 12:38:11 PM | 1.63639 | 1059.05 | 78.68 |
| 8/13/2013 12:38:12 PM | 1.63667 | 1059.05 | 78.68 |
| 8/13/2013 12:38:13 PM | 1.63694 | 1059.05 | 78.68 |
| 8/13/2013 12:38:14 PM | 1.63722 | 1059.06 | 78.68 |
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| 8/13/2013 12:38:18 PM | 1.63833 | 1059.06 | 78.68 |
| 8/13/2013 12:38:19 PM | 1.63861 | 1059.06 | 78.68 |
| 8/13/2013 12:38:20 PM | 1.63889 | 1059.07 | 78.68 |
| 8/13/2013 12:38:21 PM | 1.63917 | 1059.07 | 78.68 |
| 8/13/2013 12:38:22 PM | 1.63944 | 1059.07 | 78.68 |
| 8/13/2013 12:38:23 PM | 1.63972 | 1059.07 | 78.68 |
| 8/13/2013 12:38:24 PM | 1.64000 | 1059.07 | 78.68 |
| 8/13/2013 12:38:25 PM | 1.64028 | 1059.07 | 78.68 |
| 8/13/2013 12:38:26 PM | 1.64056 | 1059.07 | 78.68 |
| 8/13/2013 12:38:27 PM | 1.64083 | 1059.07 | 78.68 |
| 8/13/2013 12:38:28 PM | 1.64111 | 1059.08 | 78.68 |
| 8/13/2013 12:38:29 PM | 1.64139 | 1059.08 | 78.67 |
| 8/13/2013 12:38:30 PM | 1.64167 | 1059.08 | 78.67 |
| 8/13/2013 12:38:31 PM | 1.64194 | 1059.08 | 78.67 |
| 8/13/2013 12:38:32 PM | 1.64222 | 1059.08 | 78.67 |
| 8/13/2013 12:38:33 PM | 1.64250 | 1059.09 | 78.67 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:38:34 PM | 1.64278 | 1059.09 | 78.67 |
| 8/13/2013 12:38:35 PM | 1.64306 | 1059.09 | 78.67 |
| 8/13/2013 12:38:36 PM | 1.64333 | 1059.09 | 78.67 |
| 8/13/2013 12:38:37 PM | 1.64361 | 1059.09 | 78.67 |
| 8/13/2013 12:38:38 PM | 1.64389 | 1059.09 | 78.67 |
| 8/13/2013 12:38:39 PM | 1.64417 | 1059.09 | 78.67 |
| 8/13/2013 12:38:40 PM | 1.64444 | 1059.09 | 78.67 |
| 8/13/2013 12:38:41 PM | 1.64472 | 1059.09 | 78.67 |
| 8/13/2013 12:38:42 PM | 1.64500 | 1059.09 | 78.67 |
| 8/13/2013 12:38:43 PM | 1.64528 | 1059.09 | 78.67 |
| 8/13/2013 12:38:44 PM | 1.64556 | 1059.09 | 78.67 |
| 8/13/2013 12:38:45 PM | 1.64583 | 1059.09 | 78.67 |
| 8/13/2013 12:38:46 PM | 1.64611 | 1059.09 | 78.67 |
| 8/13/2013 12:38:47 PM | 1.64639 | 1059.09 | 78.67 |
| 8/13/2013 12:38:48 PM | 1.64667 | 1059.09 | 78.67 |
| 8/13/2013 12:38:49 PM | 1.64694 | 1059.09 | 78.67 |
| 8/13/2013 12:38:50 PM | 1.64722 | 1059.09 | 78.67 |
| 8/13/2013 12:38:51 PM | 1.64750 | 1059.10 | 78.67 |
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| 8/13/2013 12:38:53 PM | 1.64806 | 1059.10 | 78.67 |
| 8/13/2013 12:38:54 PM | 1.64833 | 1059.10 | 78.67 |
| 8/13/2013 12:38:55 PM | 1.64861 | 1059.10 | 78.67 |
| 8/13/2013 12:38:56 PM | 1.64889 | 1059.11 | 78.67 |
| 8/13/2013 12:38:57 PM | 1.64917 | 1059.11 | 78.66 |
| 8/13/2013 12:38:58 PM | 1.64944 | 1059.11 | 78.66 |
| 8/13/2013 12:38:59 PM | 1.64972 | 1059.11 | 78.66 |
| 8/13/2013 12:39:00 PM | 1.65000 | 1059.11 | 78.66 |
| 8/13/2013 12:39:01 PM | 1.65028 | 1059.11 | 78.66 |
| 8/13/2013 12:39:02 PM | 1.65056 | 1059.12 | 78.66 |
| 8/13/2013 12:39:03 PM | 1.65083 | 1059.12 | 78.66 |
| 8/13/2013 12:39:04 PM | 1.65111 | 1059.12 | 78.66 |
| 8/13/2013 12:39:05 PM | 1.65139 | 1059.12 | 78.66 |
| 8/13/2013 12:39:06 PM | 1.65167 | 1059.12 | 78.66 |
| 8/13/2013 12:39:07 PM | 1.65194 | 1059.12 | 78.66 |
| 8/13/2013 12:39:08 PM | 1.65222 | 1059.12 | 78.66 |
| 8/13/2013 12:39:09 PM | 1.65250 | 1059.13 | 78.66 |
| 8/13/2013 12:39:10 PM | 1.65278 | 1059.13 | 78.66 |
| 8/13/2013 12:39:11 PM | 1.65306 | 1059.13 | 78.66 |
| 8/13/2013 12:39:12 PM | 1.65333 | 1059.13 | 78.66 |
| 8/13/2013 12:39:13 PM | 1.65361 | 1059.13 | 78.66 |
| 8/13/2013 12:39:14 PM | 1.65389 | 1059.14 | 78.66 |
| 8/13/2013 12:39:15 PM | 1.65417 | 1059.14 | 78.66 |
| 8/13/2013 12:39:16 PM | 1.65444 | 1059.14 | 78.66 |
| 8/13/2013 12:39:17 PM | 1.65472 | 1059.14 | 78.66 |
| 8/13/2013 12:39:18 PM | 1.65500 | 1059.14 | 78.66 |
| 8/13/2013 12:39:19 PM | 1.65528 | 1059.15 | 78.66 |
| 8/13/2013 12:39:20 PM | 1.65556 | 1059.15 | 78.65 |
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| 8/13/2013 12:39:23 PM | 1.65639 | 1059.15 | 78.65 |
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| 8/13/2013 12:39:25 PM | 1.65694 | 1059.16 | 78.65 |
| 8/13/2013 12:39:26 PM | 1.65722 | 1059.16 | 78.65 |
| 8/13/2013 12:39:27 PM | 1.65750 | 1059.16 | 78.65 |
| 8/13/2013 12:39:28 PM | 1.65778 | 1059.16 | 78.65 |
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| 8/13/2013 12:39:33 PM | 1.65917 | 1059.16 | 78.65 |
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| 8/13/2013 12:39:35 PM | 1.65972 | 1059.16 | 78.65 |
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| 8/13/2013 12:39:40 PM | 1.66111 | 1059.17 | 78.65 |
| 8/13/2013 12:39:41 PM | 1.66139 | 1059.18 | 78.65 |
| 8/13/2013 12:39:42 PM | 1.66167 | 1059.18 | 78.65 |
| 8/13/2013 12:39:43 PM | 1.66194 | 1059.18 | 78.65 |
| 8/13/2013 12:39:44 PM | 1.66222 | 1059.18 | 78.64 |
| 8/13/2013 12:39:45 PM | 1.66250 | 1059.19 | 78.64 |
| 8/13/2013 12:39:46 PM | 1.66278 | 1059.19 | 78.64 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:39:47 PM | 1.66306 | 1059.19 | 78.64 |
| 8/13/2013 12:39:48 PM | 1.66333 | 1059.19 | 78.64 |
| 8/13/2013 12:39:49 PM | 1.66361 | 1059.19 | 78.64 |
| 8/13/2013 12:39:50 PM | 1.66389 | 1059.20 | 78.64 |
| 8/13/2013 12:39:51 PM | 1.66417 | 1059.20 | 78.64 |
| 8/13/2013 12:39:52 PM | 1.66444 | 1059.20 | 78.64 |
| 8/13/2013 12:39:53 PM | 1.66472 | 1059.20 | 78.64 |
| 8/13/2013 12:39:54 PM | 1.66500 | 1059.21 | 78.64 |
| 8/13/2013 12:39:55 PM | 1.66528 | 1059.21 | 78.64 |
| 8/13/2013 12:39:56 PM | 1.66556 | 1059.21 | 78.64 |
| 8/13/2013 12:39:57 PM | 1.66583 | 1059.21 | 78.64 |
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| 8/13/2013 12:39:59 PM | 1.66639 | 1059.22 | 78.64 |
| 8/13/2013 12:40:00 PM | 1.66667 | 1059.22 | 78.64 |
| 8/13/2013 12:40:01 PM | 1.66694 | 1059.22 | 78.64 |
| 8/13/2013 12:40:02 PM | 1.66722 | 1059.22 | 78.64 |
| 8/13/2013 12:40:03 PM | 1.66750 | 1059.23 | 78.64 |
| 8/13/2013 12:40:04 PM | 1.66778 | 1059.23 | 78.64 |
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| 8/13/2013 12:40:07 PM | 1.66861 | 1059.23 | 78.64 |
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| 8/13/2013 12:40:10 PM | 1.66944 | 1059.23 | 78.64 |
| 8/13/2013 12:40:11 PM | 1.66972 | 1059.23 | 78.64 |
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| 8/13/2013 12:40:13 PM | 1.67028 | 1059.23 | 78.63 |
| 8/13/2013 12:40:14 PM | 1.67056 | 1059.24 | 78.63 |
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| 8/13/2013 12:40:16 PM | 1.67111 | 1059.24 | 78.63 |
| 8/13/2013 12:40:17 PM | 1.67139 | 1059.24 | 78.63 |
| 8/13/2013 12:40:18 PM | 1.67167 | 1059.24 | 78.63 |
| 8/13/2013 12:40:19 PM | 1.67194 | 1059.25 | 78.63 |
| 8/13/2013 12:40:20 PM | 1.67222 | 1059.25 | 78.63 |
| 8/13/2013 12:40:21 PM | 1.67250 | 1059.26 | 78.63 |
| 8/13/2013 12:40:22 PM | 1.67278 | 1059.26 | 78.63 |
| 8/13/2013 12:40:23 PM | 1.67306 | 1059.26 | 78.63 |
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| 8/13/2013 12:40:25 PM | 1.67361 | 1059.27 | 78.63 |
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| 8/13/2013 12:40:28 PM | 1.67444 | 1059.28 | 78.63 |
| 8/13/2013 12:40:29 PM | 1.67472 | 1059.28 | 78.63 |
| 8/13/2013 12:40:30 PM | 1.67500 | 1059.29 | 78.63 |
| 8/13/2013 12:40:31 PM | 1.67528 | 1059.29 | 78.63 |
| 8/13/2013 12:40:32 PM | 1.67556 | 1059.29 | 78.63 |
| 8/13/2013 12:40:33 PM | 1.67583 | 1059.29 | 78.63 |
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| 8/13/2013 12:40:36 PM | 1.67667 | 1059.29 | 78.63 |
| 8/13/2013 12:40:37 PM | 1.67694 | 1059.29 | 78.63 |
| 8/13/2013 12:40:38 PM | 1.67722 | 1059.29 | 78.63 |
| 8/13/2013 12:40:39 PM | 1.67750 | 1059.29 | 78.62 |
| 8/13/2013 12:40:40 PM | 1.67778 | 1059.30 | 78.62 |
| 8/13/2013 12:40:41 PM | 1.67806 | 1059.30 | 78.62 |
| 8/13/2013 12:40:42 PM | 1.67833 | 1059.30 | 78.62 |
| 8/13/2013 12:40:43 PM | 1.67861 | 1059.30 | 78.62 |
| 8/13/2013 12:40:44 PM | 1.67889 | 1059.30 | 78.62 |
| 8/13/2013 12:40:45 PM | 1.67917 | 1059.30 | 78.62 |
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| 8/13/2013 12:40:47 PM | 1.67972 | 1059.30 | 78.62 |
| 8/13/2013 12:40:48 PM | 1.68000 | 1059.31 | 78.62 |
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| 8/13/2013 12:40:50 PM | 1.68056 | 1059.31 | 78.62 |
| 8/13/2013 12:40:51 PM | 1.68083 | 1059.31 | 78.62 |
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| 8/13/2013 12:40:53 PM | 1.68139 | 1059.32 | 78.62 |
| 8/13/2013 12:40:54 PM | 1.68167 | 1059.32 | 78.62 |
| 8/13/2013 12:40:55 PM | 1.68194 | 1059.32 | 78.62 |
| 8/13/2013 12:40:56 PM | 1.68222 | 1059.32 | 78.62 |
| 8/13/2013 12:40:57 PM | 1.68250 | 1059.32 | 78.62 |
| 8/13/2013 12:40:58 PM | 1.68278 | 1059.32 | 78.62 |
| 8/13/2013 12:40:59 PM | 1.68306 | 1059.32 | 78.62 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:41:00 PM | 1.68333 | 1059.33 | 78.62 |
| 8/13/2013 12:41:01 PM | 1.68361 | 1059.33 | 78.62 |
| 8/13/2013 12:41:02 PM | 1.68389 | 1059.33 | 78.61 |
| 8/13/2013 12:41:03 PM | 1.68417 | 1059.33 | 78.61 |
| 8/13/2013 12:41:04 PM | 1.68444 | 1059.34 | 78.61 |
| 8/13/2013 12:41:05 PM | 1.68472 | 1059.34 | 78.61 |
| 8/13/2013 12:41:06 PM | 1.68500 | 1059.34 | 78.61 |
| 8/13/2013 12:41:07 PM | 1.68528 | 1059.34 | 78.61 |
| 8/13/2013 12:41:08 PM | 1.68556 | 1059.34 | 78.61 |
| 8/13/2013 12:41:09 PM | 1.68583 | 1059.35 | 78.61 |
| 8/13/2013 12:41:10 PM | 1.68611 | 1059.35 | 78.61 |
| 8/13/2013 12:41:11 PM | 1.68639 | 1059.35 | 78.61 |
| 8/13/2013 12:41:12 PM | 1.68667 | 1059.35 | 78.61 |
| 8/13/2013 12:41:13 PM | 1.68694 | 1059.35 | 78.61 |
| 8/13/2013 12:41:14 PM | 1.68722 | 1059.35 | 78.61 |
| 8/13/2013 12:41:15 PM | 1.68750 | 1059.35 | 78.61 |
| 8/13/2013 12:41:16 PM | 1.68778 | 1059.35 | 78.61 |
| 8/13/2013 12:41:17 PM | 1.68806 | 1059.35 | 78.61 |
| 8/13/2013 12:41:18 PM | 1.68833 | 1059.35 | 78.61 |
| 8/13/2013 12:41:19 PM | 1.68861 | 1059.35 | 78.61 |
| 8/13/2013 12:41:20 PM | 1.68889 | 1059.35 | 78.61 |
| 8/13/2013 12:41:21 PM | 1.68917 | 1059.36 | 78.61 |
| 8/13/2013 12:41:22 PM | 1.68944 | 1059.36 | 78.61 |
| 8/13/2013 12:41:23 PM | 1.68972 | 1059.36 | 78.61 |
| 8/13/2013 12:41:24 PM | 1.69000 | 1059.37 | 78.61 |
| 8/13/2013 12:41:25 PM | 1.69028 | 1059.37 | 78.61 |
| 8/13/2013 12:41:26 PM | 1.69056 | 1059.37 | 78.61 |
| 8/13/2013 12:41:27 PM | 1.69083 | 1059.37 | 78.61 |
| 8/13/2013 12:41:28 PM | 1.69111 | 1059.37 | 78.60 |
| 8/13/2013 12:41:29 PM | 1.69139 | 1059.37 | 78.60 |
| 8/13/2013 12:41:30 PM | 1.69167 | 1059.37 | 78.60 |
| 8/13/2013 12:41:31 PM | 1.69194 | 1059.37 | 78.60 |
| 8/13/2013 12:41:32 PM | 1.69222 | 1059.37 | 78.60 |
| 8/13/2013 12:41:33 PM | 1.69250 | 1059.37 | 78.60 |
| 8/13/2013 12:41:34 PM | 1.69278 | 1059.37 | 78.60 |
| 8/13/2013 12:41:35 PM | 1.69306 | 1059.37 | 78.60 |
| 8/13/2013 12:41:36 PM | 1.69333 | 1059.38 | 78.60 |
| 8/13/2013 12:41:37 PM | 1.69361 | 1059.38 | 78.60 |
| 8/13/2013 12:41:38 PM | 1.69389 | 1059.38 | 78.60 |
| 8/13/2013 12:41:39 PM | 1.69417 | 1059.38 | 78.60 |
| 8/13/2013 12:41:40 PM | 1.69444 | 1059.38 | 78.60 |
| 8/13/2013 12:41:41 PM | 1.69472 | 1059.38 | 78.60 |
| 8/13/2013 12:41:42 PM | 1.69500 | 1059.38 | 78.60 |
| 8/13/2013 12:41:43 PM | 1.69528 | 1059.38 | 78.60 |
| 8/13/2013 12:41:44 PM | 1.69556 | 1059.38 | 78.60 |
| 8/13/2013 12:41:45 PM | 1.69583 | 1059.38 | 78.60 |
| 8/13/2013 12:41:46 PM | 1.69611 | 1059.39 | 78.60 |
| 8/13/2013 12:41:47 PM | 1.69639 | 1059.39 | 78.60 |
| 8/13/2013 12:41:48 PM | 1.69667 | 1059.39 | 78.60 |
| 8/13/2013 12:41:49 PM | 1.69694 | 1059.39 | 78.60 |
| 8/13/2013 12:41:50 PM | 1.69722 | 1059.39 | 78.60 |
| 8/13/2013 12:41:51 PM | 1.69750 | 1059.39 | 78.60 |
| 8/13/2013 12:41:52 PM | 1.69778 | 1059.39 | 78.60 |
| 8/13/2013 12:41:53 PM | 1.69806 | 1059.40 | 78.60 |
| 8/13/2013 12:41:54 PM | 1.69833 | 1059.40 | 78.59 |
| 8/13/2013 12:41:55 PM | 1.69861 | 1059.40 | 78.59 |
| 8/13/2013 12:41:56 PM | 1.69889 | 1059.40 | 78.59 |
| 8/13/2013 12:41:57 PM | 1.69917 | 1059.40 | 78.59 |
| 8/13/2013 12:41:58 PM | 1.69944 | 1059.41 | 78.59 |
| 8/13/2013 12:41:59 PM | 1.69972 | 1059.41 | 78.59 |
| 8/13/2013 12:42:00 PM | 1.70000 | 1059.41 | 78.59 |
| 8/13/2013 12:42:01 PM | 1.70028 | 1059.41 | 78.59 |
| 8/13/2013 12:42:02 PM | 1.70056 | 1059.42 | 78.59 |
| 8/13/2013 12:42:03 PM | 1.70083 | 1059.42 | 78.59 |
| 8/13/2013 12:42:04 PM | 1.70111 | 1059.42 | 78.59 |
| 8/13/2013 12:42:05 PM | 1.70139 | 1059.42 | 78.59 |
| 8/13/2013 12:42:06 PM | 1.70167 | 1059.42 | 78.59 |
| 8/13/2013 12:42:07 PM | 1.70194 | 1059.42 | 78.59 |
| 8/13/2013 12:42:08 PM | 1.70222 | 1059.42 | 78.59 |
| 8/13/2013 12:42:09 PM | 1.70250 | 1059.43 | 78.59 |
| 8/13/2013 12:42:10 PM | 1.70278 | 1059.43 | 78.59 |
| 8/13/2013 12:42:11 PM | 1.70306 | 1059.43 | 78.59 |
| 8/13/2013 12:42:12 PM | 1.70333 | 1059.43 | 78.59 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:42:13 PM | 1.70361 | 1059.43 | 78.59 |
| 8/13/2013 12:42:14 PM | 1.70389 | 1059.43 | 78.59 |
| 8/13/2013 12:42:15 PM | 1.70417 | 1059.44 | 78.59 |
| 8/13/2013 12:42:16 PM | 1.70444 | 1059.44 | 78.59 |
| 8/13/2013 12:42:17 PM | 1.70472 | 1059.44 | 78.59 |
| 8/13/2013 12:42:18 PM | 1.70500 | 1059.44 | 78.59 |
| 8/13/2013 12:42:19 PM | 1.70528 | 1059.44 | 78.59 |
| 8/13/2013 12:42:20 PM | 1.70556 | 1059.45 | 78.59 |
| 8/13/2013 12:42:21 PM | 1.70583 | 1059.45 | 78.59 |
| 8/13/2013 12:42:22 PM | 1.70611 | 1059.45 | 78.59 |
| 8/13/2013 12:42:23 PM | 1.70639 | 1059.45 | 78.59 |
| 8/13/2013 12:42:24 PM | 1.70667 | 1059.45 | 78.59 |
| 8/13/2013 12:42:25 PM | 1.70694 | 1059.46 | 78.59 |
| 8/13/2013 12:42:26 PM | 1.70722 | 1059.46 | 78.59 |
| 8/13/2013 12:42:27 PM | 1.70750 | 1059.46 | 78.58 |
| 8/13/2013 12:42:28 PM | 1.70778 | 1059.46 | 78.58 |
| 8/13/2013 12:42:29 PM | 1.70806 | 1059.46 | 78.58 |
| 8/13/2013 12:42:30 PM | 1.70833 | 1059.46 | 78.58 |
| 8/13/2013 12:42:31 PM | 1.70861 | 1059.46 | 78.58 |
| 8/13/2013 12:42:32 PM | 1.70889 | 1059.46 | 78.58 |
| 8/13/2013 12:42:33 PM | 1.70917 | 1059.46 | 78.58 |
| 8/13/2013 12:42:34 PM | 1.70944 | 1059.47 | 78.58 |
| 8/13/2013 12:42:35 PM | 1.70972 | 1059.47 | 78.58 |
| 8/13/2013 12:42:36 PM | 1.71000 | 1059.47 | 78.58 |
| 8/13/2013 12:42:37 PM | 1.71028 | 1059.47 | 78.58 |
| 8/13/2013 12:42:38 PM | 1.71056 | 1059.47 | 78.58 |
| 8/13/2013 12:42:39 PM | 1.71083 | 1059.47 | 78.58 |
| 8/13/2013 12:42:40 PM | 1.71111 | 1059.47 | 78.58 |
| 8/13/2013 12:42:41 PM | 1.71139 | 1059.47 | 78.58 |
| 8/13/2013 12:42:42 PM | 1.71167 | 1059.47 | 78.58 |
| 8/13/2013 12:42:43 PM | 1.71194 | 1059.47 | 78.58 |
| 8/13/2013 12:42:44 PM | 1.71222 | 1059.48 | 78.58 |
| 8/13/2013 12:42:45 PM | 1.71250 | 1059.48 | 78.58 |
| 8/13/2013 12:42:46 PM | 1.71278 | 1059.48 | 78.58 |
| 8/13/2013 12:42:47 PM | 1.71306 | 1059.48 | 78.58 |
| 8/13/2013 12:42:48 PM | 1.71333 | 1059.48 | 78.58 |
| 8/13/2013 12:42:49 PM | 1.71361 | 1059.49 | 78.58 |
| 8/13/2013 12:42:50 PM | 1.71389 | 1059.49 | 78.58 |
| 8/13/2013 12:42:51 PM | 1.71417 | 1059.49 | 78.58 |
| 8/13/2013 12:42:52 PM | 1.71444 | 1059.49 | 78.58 |
| 8/13/2013 12:42:53 PM | 1.71472 | 1059.49 | 78.58 |
| 8/13/2013 12:42:54 PM | 1.71500 | 1059.49 | 78.58 |
| 8/13/2013 12:42:55 PM | 1.71528 | 1059.49 | 78.58 |
| 8/13/2013 12:42:56 PM | 1.71556 | 1059.49 | 78.58 |
| 8/13/2013 12:42:57 PM | 1.71583 | 1059.49 | 78.57 |
| 8/13/2013 12:42:58 PM | 1.71611 | 1059.49 | 78.57 |
| 8/13/2013 12:42:59 PM | 1.71639 | 1059.49 | 78.57 |
| 8/13/2013 12:43:00 PM | 1.71667 | 1059.49 | 78.57 |
| 8/13/2013 12:43:01 PM | 1.71694 | 1059.49 | 78.57 |
| 8/13/2013 12:43:02 PM | 1.71722 | 1059.49 | 78.57 |
| 8/13/2013 12:43:03 PM | 1.71750 | 1059.50 | 78.57 |
| 8/13/2013 12:43:04 PM | 1.71778 | 1059.50 | 78.57 |
| 8/13/2013 12:43:05 PM | 1.71806 | 1059.50 | 78.57 |
| 8/13/2013 12:43:06 PM | 1.71833 | 1059.50 | 78.57 |
| 8/13/2013 12:43:07 PM | 1.71861 | 1059.50 | 78.57 |
| 8/13/2013 12:43:08 PM | 1.71889 | 1059.51 | 78.57 |
| 8/13/2013 12:43:09 PM | 1.71917 | 1059.51 | 78.57 |
| 8/13/2013 12:43:10 PM | 1.71944 | 1059.51 | 78.57 |
| 8/13/2013 12:43:11 PM | 1.71972 | 1059.51 | 78.57 |
| 8/13/2013 12:43:12 PM | 1.72000 | 1059.51 | 78.57 |
| 8/13/2013 12:43:13 PM | 1.72028 | 1059.51 | 78.57 |
| 8/13/2013 12:43:14 PM | 1.72056 | 1059.52 | 78.57 |
| 8/13/2013 12:43:15 PM | 1.72083 | 1059.52 | 78.57 |
| 8/13/2013 12:43:16 PM | 1.72111 | 1059.52 | 78.57 |
| 8/13/2013 12:43:17 PM | 1.72139 | 1059.52 | 78.57 |
| 8/13/2013 12:43:18 PM | 1.72167 | 1059.52 | 78.57 |
| 8/13/2013 12:43:19 PM | 1.72194 | 1059.52 | 78.57 |
| 8/13/2013 12:43:20 PM | 1.72222 | 1059.52 | 78.57 |
| 8/13/2013 12:43:21 PM | 1.72250 | 1059.52 | 78.57 |
| 8/13/2013 12:43:22 PM | 1.72278 | 1059.52 | 78.57 |
| 8/13/2013 12:43:23 PM | 1.72306 | 1059.53 | 78.56 |
| 8/13/2013 12:43:24 PM | 1.72333 | 1059.53 | 78.56 |
| 8/13/2013 12:43:25 PM | 1.72361 | 1059.53 | 78.56 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:43:26 PM | 1.72389 | 1059.53 | 78.56 |
| 8/13/2013 12:43:27 PM | 1.72417 | 1059.53 | 78.56 |
| 8/13/2013 12:43:28 PM | 1.72444 | 1059.54 | 78.56 |
| 8/13/2013 12:43:29 PM | 1.72472 | 1059.54 | 78.56 |
| 8/13/2013 12:43:30 PM | 1.72500 | 1059.54 | 78.56 |
| 8/13/2013 12:43:31 PM | 1.72528 | 1059.54 | 78.56 |
| 8/13/2013 12:43:32 PM | 1.72556 | 1059.55 | 78.56 |
| 8/13/2013 12:43:33 PM | 1.72583 | 1059.55 | 78.56 |
| 8/13/2013 12:43:34 PM | 1.72611 | 1059.55 | 78.56 |
| 8/13/2013 12:43:35 PM | 1.72639 | 1059.56 | 78.56 |
| 8/13/2013 12:43:36 PM | 1.72667 | 1059.56 | 78.56 |
| 8/13/2013 12:43:37 PM | 1.72694 | 1059.56 | 78.56 |
| 8/13/2013 12:43:38 PM | 1.72722 | 1059.56 | 78.56 |
| 8/13/2013 12:43:39 PM | 1.72750 | 1059.56 | 78.56 |
| 8/13/2013 12:43:40 PM | 1.72778 | 1059.56 | 78.56 |
| 8/13/2013 12:43:41 PM | 1.72806 | 1059.56 | 78.56 |
| 8/13/2013 12:43:42 PM | 1.72833 | 1059.56 | 78.56 |
| 8/13/2013 12:43:43 PM | 1.72861 | 1059.56 | 78.56 |
| 8/13/2013 12:43:44 PM | 1.72889 | 1059.56 | 78.56 |
| 8/13/2013 12:43:45 PM | 1.72917 | 1059.56 | 78.56 |
| 8/13/2013 12:43:46 PM | 1.72944 | 1059.56 | 78.56 |
| 8/13/2013 12:43:47 PM | 1.72972 | 1059.56 | 78.56 |
| 8/13/2013 12:43:48 PM | 1.73000 | 1059.57 | 78.56 |
| 8/13/2013 12:43:49 PM | 1.73028 | 1059.57 | 78.56 |
| 8/13/2013 12:43:50 PM | 1.73056 | 1059.57 | 78.56 |
| 8/13/2013 12:43:51 PM | 1.73083 | 1059.57 | 78.56 |
| 8/13/2013 12:43:52 PM | 1.73111 | 1059.58 | 78.56 |
| 8/13/2013 12:43:53 PM | 1.73139 | 1059.58 | 78.56 |
| 8/13/2013 12:43:54 PM | 1.73167 | 1059.58 | 78.56 |
| 8/13/2013 12:43:55 PM | 1.73194 | 1059.58 | 78.56 |
| 8/13/2013 12:43:56 PM | 1.73222 | 1059.59 | 78.56 |
| 8/13/2013 12:43:57 PM | 1.73250 | 1059.59 | 78.56 |
| 8/13/2013 12:43:58 PM | 1.73278 | 1059.59 | 78.56 |
| 8/13/2013 12:43:59 PM | 1.73306 | 1059.59 | 78.56 |
| 8/13/2013 12:44:00 PM | 1.73333 | 1059.59 | 78.55 |
| 8/13/2013 12:44:01 PM | 1.73361 | 1059.60 | 78.55 |
| 8/13/2013 12:44:02 PM | 1.73389 | 1059.60 | 78.55 |
| 8/13/2013 12:44:03 PM | 1.73417 | 1059.60 | 78.55 |
| 8/13/2013 12:44:04 PM | 1.73444 | 1059.60 | 78.55 |
| 8/13/2013 12:44:05 PM | 1.73472 | 1059.60 | 78.55 |
| 8/13/2013 12:44:06 PM | 1.73500 | 1059.60 | 78.55 |
| 8/13/2013 12:44:07 PM | 1.73528 | 1059.60 | 78.55 |
| 8/13/2013 12:44:08 PM | 1.73556 | 1059.60 | 78.55 |
| 8/13/2013 12:44:09 PM | 1.73583 | 1059.60 | 78.55 |
| 8/13/2013 12:44:10 PM | 1.73611 | 1059.60 | 78.55 |
| 8/13/2013 12:44:11 PM | 1.73639 | 1059.60 | 78.55 |
| 8/13/2013 12:44:12 PM | 1.73667 | 1059.61 | 78.55 |
| 8/13/2013 12:44:13 PM | 1.73694 | 1059.61 | 78.55 |
| 8/13/2013 12:44:14 PM | 1.73722 | 1059.61 | 78.55 |
| 8/13/2013 12:44:15 PM | 1.73750 | 1059.62 | 78.55 |
| 8/13/2013 12:44:16 PM | 1.73778 | 1059.62 | 78.55 |
| 8/13/2013 12:44:17 PM | 1.73806 | 1059.62 | 78.55 |
| 8/13/2013 12:44:18 PM | 1.73833 | 1059.62 | 78.55 |
| 8/13/2013 12:44:19 PM | 1.73861 | 1059.63 | 78.55 |
| 8/13/2013 12:44:20 PM | 1.73889 | 1059.63 | 78.55 |
| 8/13/2013 12:44:21 PM | 1.73917 | 1059.63 | 78.55 |
| 8/13/2013 12:44:22 PM | 1.73944 | 1059.63 | 78.55 |
| 8/13/2013 12:44:23 PM | 1.73972 | 1059.63 | 78.55 |
| 8/13/2013 12:44:24 PM | 1.74000 | 1059.63 | 78.55 |
| 8/13/2013 12:44:25 PM | 1.74028 | 1059.64 | 78.55 |
| 8/13/2013 12:44:26 PM | 1.74056 | 1059.64 | 78.55 |
| 8/13/2013 12:44:27 PM | 1.74083 | 1059.64 | 78.55 |
| 8/13/2013 12:44:28 PM | 1.74111 | 1059.64 | 78.55 |
| 8/13/2013 12:44:29 PM | 1.74139 | 1059.64 | 78.55 |
| 8/13/2013 12:44:30 PM | 1.74167 | 1059.64 | 78.55 |
| 8/13/2013 12:44:31 PM | 1.74194 | 1059.65 | 78.55 |
| 8/13/2013 12:44:32 PM | 1.74222 | 1059.65 | 78.55 |
| 8/13/2013 12:44:33 PM | 1.74250 | 1059.65 | 78.55 |
| 8/13/2013 12:44:34 PM | 1.74278 | 1059.65 | 78.55 |
| 8/13/2013 12:44:35 PM | 1.74306 | 1059.65 | 78.55 |
| 8/13/2013 12:44:36 PM | 1.74333 | 1059.65 | 78.55 |
| 8/13/2013 12:44:37 PM | 1.74361 | 1059.65 | 78.55 |
| 8/13/2013 12:44:38 PM | 1.74389 | 1059.66 | 78.54 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:44:39 PM | 1.74417 | 1059.66 | 78.54 |
| 8/13/2013 12:44:40 PM | 1.74444 | 1059.66 | 78.54 |
| 8/13/2013 12:44:41 PM | 1.74472 | 1059.66 | 78.54 |
| 8/13/2013 12:44:42 PM | 1.74500 | 1059.67 | 78.54 |
| 8/13/2013 12:44:43 PM | 1.74528 | 1059.67 | 78.54 |
| 8/13/2013 12:44:44 PM | 1.74556 | 1059.67 | 78.54 |
| 8/13/2013 12:44:45 PM | 1.74583 | 1059.67 | 78.54 |
| 8/13/2013 12:44:46 PM | 1.74611 | 1059.68 | 78.54 |
| 8/13/2013 12:44:47 PM | 1.74639 | 1059.68 | 78.54 |
| 8/13/2013 12:44:48 PM | 1.74667 | 1059.68 | 78.54 |
| 8/13/2013 12:44:49 PM | 1.74694 | 1059.68 | 78.54 |
| 8/13/2013 12:44:50 PM | 1.74722 | 1059.68 | 78.54 |
| 8/13/2013 12:44:51 PM | 1.74750 | 1059.68 | 78.54 |
| 8/13/2013 12:44:52 PM | 1.74778 | 1059.68 | 78.54 |
| 8/13/2013 12:44:53 PM | 1.74806 | 1059.68 | 78.54 |
| 8/13/2013 12:44:54 PM | 1.74833 | 1059.69 | 78.54 |
| 8/13/2013 12:44:55 PM | 1.74861 | 1059.69 | 78.54 |
| 8/13/2013 12:44:56 PM | 1.74889 | 1059.69 | 78.54 |
| 8/13/2013 12:44:57 PM | 1.74917 | 1059.69 | 78.54 |
| 8/13/2013 12:44:58 PM | 1.74944 | 1059.69 | 78.54 |
| 8/13/2013 12:44:59 PM | 1.74972 | 1059.69 | 78.54 |
| 8/13/2013 12:45:00 PM | 1.75000 | 1059.69 | 78.54 |
| 8/13/2013 12:45:01 PM | 1.75028 | 1059.70 | 78.54 |
| 8/13/2013 12:45:02 PM | 1.75056 | 1059.70 | 78.54 |
| 8/13/2013 12:45:03 PM | 1.75083 | 1059.70 | 78.54 |
| 8/13/2013 12:45:04 PM | 1.75111 | 1059.70 | 78.54 |
| 8/13/2013 12:45:05 PM | 1.75139 | 1059.71 | 78.53 |
| 8/13/2013 12:45:06 PM | 1.75167 | 1059.71 | 78.53 |
| 8/13/2013 12:45:07 PM | 1.75194 | 1059.71 | 78.53 |
| 8/13/2013 12:45:08 PM | 1.75222 | 1059.71 | 78.53 |
| 8/13/2013 12:45:09 PM | 1.75250 | 1059.72 | 78.53 |
| 8/13/2013 12:45:10 PM | 1.75278 | 1059.72 | 78.53 |
| 8/13/2013 12:45:11 PM | 1.75306 | 1059.73 | 78.53 |
| 8/13/2013 12:45:12 PM | 1.75333 | 1059.73 | 78.53 |
| 8/13/2013 12:45:13 PM | 1.75361 | 1059.73 | 78.53 |
| 8/13/2013 12:45:14 PM | 1.75389 | 1059.73 | 78.53 |
| 8/13/2013 12:45:15 PM | 1.75417 | 1059.74 | 78.53 |
| 8/13/2013 12:45:16 PM | 1.75444 | 1059.74 | 78.53 |
| 8/13/2013 12:45:17 PM | 1.75472 | 1059.74 | 78.53 |
| 8/13/2013 12:45:18 PM | 1.75500 | 1059.75 | 78.53 |
| 8/13/2013 12:45:19 PM | 1.75528 | 1059.75 | 78.53 |
| 8/13/2013 12:45:20 PM | 1.75556 | 1059.75 | 78.53 |
| 8/13/2013 12:45:21 PM | 1.75583 | 1059.75 | 78.53 |
| 8/13/2013 12:45:22 PM | 1.75611 | 1059.75 | 78.53 |
| 8/13/2013 12:45:23 PM | 1.75639 | 1059.75 | 78.53 |
| 8/13/2013 12:45:24 PM | 1.75667 | 1059.75 | 78.53 |
| 8/13/2013 12:45:25 PM | 1.75694 | 1059.76 | 78.53 |
| 8/13/2013 12:45:26 PM | 1.75722 | 1059.76 | 78.53 |
| 8/13/2013 12:45:27 PM | 1.75750 | 1059.76 | 78.53 |
| 8/13/2013 12:45:28 PM | 1.75778 | 1059.76 | 78.53 |
| 8/13/2013 12:45:29 PM | 1.75806 | 1059.76 | 78.53 |
| 8/13/2013 12:45:30 PM | 1.75833 | 1059.76 | 78.53 |
| 8/13/2013 12:45:31 PM | 1.75861 | 1059.76 | 78.53 |
| 8/13/2013 12:45:32 PM | 1.75889 | 1059.76 | 78.53 |
| 8/13/2013 12:45:33 PM | 1.75917 | 1059.76 | 78.53 |
| 8/13/2013 12:45:34 PM | 1.75944 | 1059.76 | 78.53 |
| 8/13/2013 12:45:35 PM | 1.75972 | 1059.76 | 78.53 |
| 8/13/2013 12:45:36 PM | 1.76000 | 1059.76 | 78.53 |
| 8/13/2013 12:45:37 PM | 1.76028 | 1059.76 | 78.53 |
| 8/13/2013 12:45:38 PM | 1.76056 | 1059.77 | 78.53 |
| 8/13/2013 12:45:39 PM | 1.76083 | 1059.77 | 78.53 |
| 8/13/2013 12:45:40 PM | 1.76111 | 1059.77 | 78.53 |
| 8/13/2013 12:45:41 PM | 1.76139 | 1059.77 | 78.53 |
| 8/13/2013 12:45:42 PM | 1.76167 | 1059.78 | 78.53 |
| 8/13/2013 12:45:43 PM | 1.76194 | 1059.78 | 78.53 |
| 8/13/2013 12:45:44 PM | 1.76222 | 1059.78 | 78.53 |
| 8/13/2013 12:45:45 PM | 1.76250 | 1059.78 | 78.53 |
| 8/13/2013 12:45:46 PM | 1.76278 | 1059.79 | 78.52 |
| 8/13/2013 12:45:47 PM | 1.76306 | 1059.79 | 78.52 |
| 8/13/2013 12:45:48 PM | 1.76333 | 1059.80 | 78.52 |
| 8/13/2013 12:45:49 PM | 1.76361 | 1059.80 | 78.52 |
| 8/13/2013 12:45:50 PM | 1.76389 | 1059.80 | 78.52 |
| 8/13/2013 12:45:51 PM | 1.76417 | 1059.81 | 78.52 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:45:52 PM | 1.76444 | 1059.81 | 78.52 |
| 8/13/2013 12:45:53 PM | 1.76472 | 1059.81 | 78.52 |
| 8/13/2013 12:45:54 PM | 1.76500 | 1059.81 | 78.52 |
| 8/13/2013 12:45:55 PM | 1.76528 | 1059.82 | 78.52 |
| 8/13/2013 12:45:56 PM | 1.76556 | 1059.82 | 78.52 |
| 8/13/2013 12:45:57 PM | 1.76583 | 1059.82 | 78.52 |
| 8/13/2013 12:45:58 PM | 1.76611 | 1059.82 | 78.52 |
| 8/13/2013 12:45:59 PM | 1.76639 | 1059.82 | 78.52 |
| 8/13/2013 12:46:00 PM | 1.76667 | 1059.82 | 78.52 |
| 8/13/2013 12:46:01 PM | 1.76694 | 1059.82 | 78.52 |
| 8/13/2013 12:46:02 PM | 1.76722 | 1059.83 | 78.52 |
| 8/13/2013 12:46:03 PM | 1.76750 | 1059.83 | 78.52 |
| 8/13/2013 12:46:04 PM | 1.76778 | 1059.83 | 78.52 |
| 8/13/2013 12:46:05 PM | 1.76806 | 1059.83 | 78.52 |
| 8/13/2013 12:46:06 PM | 1.76833 | 1059.83 | 78.52 |
| 8/13/2013 12:46:07 PM | 1.76861 | 1059.83 | 78.52 |
| 8/13/2013 12:46:08 PM | 1.76889 | 1059.84 | 78.52 |
| 8/13/2013 12:46:09 PM | 1.76917 | 1059.84 | 78.52 |
| 8/13/2013 12:46:10 PM | 1.76944 | 1059.84 | 78.52 |
| 8/13/2013 12:46:11 PM | 1.76972 | 1059.84 | 78.52 |
| 8/13/2013 12:46:12 PM | 1.77000 | 1059.84 | 78.52 |
| 8/13/2013 12:46:13 PM | 1.77028 | 1059.84 | 78.52 |
| 8/13/2013 12:46:14 PM | 1.77056 | 1059.84 | 78.52 |
| 8/13/2013 12:46:15 PM | 1.77083 | 1059.84 | 78.52 |
| 8/13/2013 12:46:16 PM | 1.77111 | 1059.85 | 78.52 |
| 8/13/2013 12:46:17 PM | 1.77139 | 1059.85 | 78.52 |
| 8/13/2013 12:46:18 PM | 1.77167 | 1059.85 | 78.52 |
| 8/13/2013 12:46:19 PM | 1.77194 | 1059.85 | 78.52 |
| 8/13/2013 12:46:20 PM | 1.77222 | 1059.86 | 78.52 |
| 8/13/2013 12:46:21 PM | 1.77250 | 1059.86 | 78.52 |
| 8/13/2013 12:46:22 PM | 1.77278 | 1059.86 | 78.52 |
| 8/13/2013 12:46:23 PM | 1.77306 | 1059.86 | 78.52 |
| 8/13/2013 12:46:24 PM | 1.77333 | 1059.86 | 78.52 |
| 8/13/2013 12:46:25 PM | 1.77361 | 1059.86 | 78.51 |
| 8/13/2013 12:46:26 PM | 1.77389 | 1059.86 | 78.51 |
| 8/13/2013 12:46:27 PM | 1.77417 | 1059.86 | 78.51 |
| 8/13/2013 12:46:28 PM | 1.77444 | 1059.86 | 78.51 |
| 8/13/2013 12:46:29 PM | 1.77472 | 1059.86 | 78.51 |
| 8/13/2013 12:46:30 PM | 1.77500 | 1059.86 | 78.51 |
| 8/13/2013 12:46:31 PM | 1.77528 | 1059.86 | 78.51 |
| 8/13/2013 12:46:32 PM | 1.77556 | 1059.87 | 78.51 |
| 8/13/2013 12:46:33 PM | 1.77583 | 1059.87 | 78.51 |
| 8/13/2013 12:46:34 PM | 1.77611 | 1059.87 | 78.51 |
| 8/13/2013 12:46:35 PM | 1.77639 | 1059.88 | 78.51 |
| 8/13/2013 12:46:36 PM | 1.77667 | 1059.88 | 78.51 |
| 8/13/2013 12:46:37 PM | 1.77694 | 1059.88 | 78.51 |
| 8/13/2013 12:46:38 PM | 1.77722 | 1059.88 | 78.51 |
| 8/13/2013 12:46:39 PM | 1.77750 | 1059.89 | 78.51 |
| 8/13/2013 12:46:40 PM | 1.77778 | 1059.89 | 78.51 |
| 8/13/2013 12:46:41 PM | 1.77806 | 1059.89 | 78.51 |
| 8/13/2013 12:46:42 PM | 1.77833 | 1059.89 | 78.51 |
| 8/13/2013 12:46:43 PM | 1.77861 | 1059.89 | 78.51 |
| 8/13/2013 12:46:44 PM | 1.77889 | 1059.90 | 78.51 |
| 8/13/2013 12:46:45 PM | 1.77917 | 1059.90 | 78.51 |
| 8/13/2013 12:46:46 PM | 1.77944 | 1059.90 | 78.51 |
| 8/13/2013 12:46:47 PM | 1.77972 | 1059.90 | 78.51 |
| 8/13/2013 12:46:48 PM | 1.78000 | 1059.90 | 78.51 |
| 8/13/2013 12:46:49 PM | 1.78028 | 1059.91 | 78.51 |
| 8/13/2013 12:46:50 PM | 1.78056 | 1059.91 | 78.51 |
| 8/13/2013 12:46:51 PM | 1.78083 | 1059.91 | 78.51 |
| 8/13/2013 12:46:52 PM | 1.78111 | 1059.92 | 78.51 |
| 8/13/2013 12:46:53 PM | 1.78139 | 1059.92 | 78.51 |
| 8/13/2013 12:46:54 PM | 1.78167 | 1059.92 | 78.51 |
| 8/13/2013 12:46:55 PM | 1.78194 | 1059.92 | 78.51 |
| 8/13/2013 12:46:56 PM | 1.78222 | 1059.93 | 78.51 |
| 8/13/2013 12:46:57 PM | 1.78250 | 1059.93 | 78.51 |
| 8/13/2013 12:46:58 PM | 1.78278 | 1059.94 | 78.50 |
| 8/13/2013 12:46:59 PM | 1.78306 | 1059.94 | 78.50 |
| 8/13/2013 12:47:00 PM | 1.78333 | 1059.94 | 78.50 |
| 8/13/2013 12:47:01 PM | 1.78361 | 1059.94 | 78.50 |
| 8/13/2013 12:47:02 PM | 1.78389 | 1059.94 | 78.50 |
| 8/13/2013 12:47:03 PM | 1.78417 | 1059.95 | 78.50 |
| 8/13/2013 12:47:04 PM | 1.78444 | 1059.95 | 78.50 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:47:05 PM | 1.78472 | 1059.95 | 78.50 |
| 8/13/2013 12:47:06 PM | 1.78500 | 1059.95 | 78.50 |
| 8/13/2013 12:47:07 PM | 1.78528 | 1059.95 | 78.50 |
| 8/13/2013 12:47:08 PM | 1.78556 | 1059.95 | 78.50 |
| 8/13/2013 12:47:09 PM | 1.78583 | 1059.95 | 78.50 |
| 8/13/2013 12:47:10 PM | 1.78611 | 1059.95 | 78.50 |
| 8/13/2013 12:47:11 PM | 1.78639 | 1059.95 | 78.50 |
| 8/13/2013 12:47:12 PM | 1.78667 | 1059.95 | 78.50 |
| 8/13/2013 12:47:13 PM | 1.78694 | 1059.95 | 78.50 |
| 8/13/2013 12:47:14 PM | 1.78722 | 1059.95 | 78.50 |
| 8/13/2013 12:47:15 PM | 1.78750 | 1059.96 | 78.50 |
| 8/13/2013 12:47:16 PM | 1.78778 | 1059.96 | 78.50 |
| 8/13/2013 12:47:17 PM | 1.78806 | 1059.96 | 78.50 |
| 8/13/2013 12:47:18 PM | 1.78833 | 1059.96 | 78.50 |
| 8/13/2013 12:47:19 PM | 1.78861 | 1059.96 | 78.50 |
| 8/13/2013 12:47:20 PM | 1.78889 | 1059.97 | 78.50 |
| 8/13/2013 12:47:21 PM | 1.78917 | 1059.97 | 78.50 |
| 8/13/2013 12:47:22 PM | 1.78944 | 1059.97 | 78.50 |
| 8/13/2013 12:47:23 PM | 1.78972 | 1059.97 | 78.50 |
| 8/13/2013 12:47:24 PM | 1.79000 | 1059.98 | 78.50 |
| 8/13/2013 12:47:25 PM | 1.79028 | 1059.98 | 78.50 |
| 8/13/2013 12:47:26 PM | 1.79056 | 1059.98 | 78.50 |
| 8/13/2013 12:47:27 PM | 1.79083 | 1059.98 | 78.50 |
| 8/13/2013 12:47:28 PM | 1.79111 | 1059.98 | 78.50 |
| 8/13/2013 12:47:29 PM | 1.79139 | 1059.98 | 78.50 |
| 8/13/2013 12:47:30 PM | 1.79167 | 1059.99 | 78.50 |
| 8/13/2013 12:47:31 PM | 1.79194 | 1059.99 | 78.50 |
| 8/13/2013 12:47:32 PM | 1.79222 | 1059.99 | 78.50 |
| 8/13/2013 12:47:33 PM | 1.79250 | 1059.99 | 78.50 |
| 8/13/2013 12:47:34 PM | 1.79278 | 1059.99 | 78.50 |
| 8/13/2013 12:47:35 PM | 1.79306 | 1059.99 | 78.50 |
| 8/13/2013 12:47:36 PM | 1.79333 | 1059.99 | 78.50 |
| 8/13/2013 12:47:37 PM | 1.79361 | 1059.99 | 78.50 |
| 8/13/2013 12:47:38 PM | 1.79389 | 1060.00 | 78.50 |
| 8/13/2013 12:47:39 PM | 1.79417 | 1060.00 | 78.50 |
| 8/13/2013 12:47:40 PM | 1.79444 | 1060.00 | 78.50 |
| 8/13/2013 12:47:41 PM | 1.79472 | 1060.00 | 78.50 |
| 8/13/2013 12:47:42 PM | 1.79500 | 1060.01 | 78.49 |
| 8/13/2013 12:47:43 PM | 1.79528 | 1060.01 | 78.49 |
| 8/13/2013 12:47:44 PM | 1.79556 | 1060.01 | 78.49 |
| 8/13/2013 12:47:45 PM | 1.79583 | 1060.01 | 78.49 |
| 8/13/2013 12:47:46 PM | 1.79611 | 1060.01 | 78.49 |
| 8/13/2013 12:47:47 PM | 1.79639 | 1060.01 | 78.49 |
| 8/13/2013 12:47:48 PM | 1.79667 | 1060.02 | 78.49 |
| 8/13/2013 12:47:49 PM | 1.79694 | 1060.02 | 78.49 |
| 8/13/2013 12:47:50 PM | 1.79722 | 1060.02 | 78.49 |
| 8/13/2013 12:47:51 PM | 1.79750 | 1060.02 | 78.49 |
| 8/13/2013 12:47:52 PM | 1.79778 | 1060.02 | 78.49 |
| 8/13/2013 12:47:53 PM | 1.79806 | 1060.02 | 78.49 |
| 8/13/2013 12:47:54 PM | 1.79833 | 1060.02 | 78.49 |
| 8/13/2013 12:47:55 PM | 1.79861 | 1060.02 | 78.49 |
| 8/13/2013 12:47:56 PM | 1.79889 | 1060.03 | 78.49 |
| 8/13/2013 12:47:57 PM | 1.79917 | 1060.03 | 78.49 |
| 8/13/2013 12:47:58 PM | 1.79944 | 1060.03 | 78.49 |
| 8/13/2013 12:47:59 PM | 1.79972 | 1060.03 | 78.49 |
| 8/13/2013 12:48:00 PM | 1.80000 | 1060.04 | 78.49 |
| 8/13/2013 12:48:01 PM | 1.80028 | 1060.04 | 78.49 |
| 8/13/2013 12:48:02 PM | 1.80056 | 1060.04 | 78.49 |
| 8/13/2013 12:48:03 PM | 1.80083 | 1060.04 | 78.49 |
| 8/13/2013 12:48:04 PM | 1.80111 | 1060.05 | 78.49 |
| 8/13/2013 12:48:05 PM | 1.80139 | 1060.05 | 78.49 |
| 8/13/2013 12:48:06 PM | 1.80167 | 1060.05 | 78.49 |
| 8/13/2013 12:48:07 PM | 1.80194 | 1060.06 | 78.49 |
| 8/13/2013 12:48:08 PM | 1.80222 | 1060.06 | 78.49 |
| 8/13/2013 12:48:09 PM | 1.80250 | 1060.06 | 78.49 |
| 8/13/2013 12:48:10 PM | 1.80278 | 1060.06 | 78.49 |
| 8/13/2013 12:48:11 PM | 1.80306 | 1060.06 | 78.49 |
| 8/13/2013 12:48:12 PM | 1.80333 | 1060.06 | 78.49 |
| 8/13/2013 12:48:13 PM | 1.80361 | 1060.06 | 78.49 |
| 8/13/2013 12:48:14 PM | 1.80389 | 1060.06 | 78.49 |
| 8/13/2013 12:48:15 PM | 1.80417 | 1060.06 | 78.49 |
| 8/13/2013 12:48:16 PM | 1.80444 | 1060.07 | 78.49 |
| 8/13/2013 12:48:17 PM | 1.80472 | 1060.07 | 78.48 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:48:18 PM | 1.80500 | 1060.07 | 78.48 |
| 8/13/2013 12:48:19 PM | 1.80528 | 1060.07 | 78.48 |
| 8/13/2013 12:48:20 PM | 1.80556 | 1060.07 | 78.48 |
| 8/13/2013 12:48:21 PM | 1.80583 | 1060.07 | 78.48 |
| 8/13/2013 12:48:22 PM | 1.80611 | 1060.08 | 78.48 |
| 8/13/2013 12:48:23 PM | 1.80639 | 1060.08 | 78.48 |
| 8/13/2013 12:48:24 PM | 1.80667 | 1060.09 | 78.48 |
| 8/13/2013 12:48:25 PM | 1.80694 | 1060.09 | 78.48 |
| 8/13/2013 12:48:26 PM | 1.80722 | 1060.09 | 78.48 |
| 8/13/2013 12:48:27 PM | 1.80750 | 1060.10 | 78.48 |
| 8/13/2013 12:48:28 PM | 1.80778 | 1060.10 | 78.48 |
| 8/13/2013 12:48:29 PM | 1.80806 | 1060.10 | 78.48 |
| 8/13/2013 12:48:30 PM | 1.80833 | 1060.10 | 78.48 |
| 8/13/2013 12:48:31 PM | 1.80861 | 1060.10 | 78.48 |
| 8/13/2013 12:48:32 PM | 1.80889 | 1060.10 | 78.48 |
| 8/13/2013 12:48:33 PM | 1.80917 | 1060.11 | 78.48 |
| 8/13/2013 12:48:34 PM | 1.80944 | 1060.11 | 78.48 |
| 8/13/2013 12:48:35 PM | 1.80972 | 1060.11 | 78.48 |
| 8/13/2013 12:48:36 PM | 1.81000 | 1060.11 | 78.48 |
| 8/13/2013 12:48:37 PM | 1.81028 | 1060.11 | 78.48 |
| 8/13/2013 12:48:38 PM | 1.81056 | 1060.11 | 78.48 |
| 8/13/2013 12:48:39 PM | 1.81083 | 1060.12 | 78.48 |
| 8/13/2013 12:48:40 PM | 1.81111 | 1060.12 | 78.48 |
| 8/13/2013 12:48:41 PM | 1.81139 | 1060.12 | 78.48 |
| 8/13/2013 12:48:42 PM | 1.81167 | 1060.12 | 78.48 |
| 8/13/2013 12:48:43 PM | 1.81194 | 1060.13 | 78.48 |
| 8/13/2013 12:48:44 PM | 1.81222 | 1060.13 | 78.48 |
| 8/13/2013 12:48:45 PM | 1.81250 | 1060.13 | 78.48 |
| 8/13/2013 12:48:46 PM | 1.81278 | 1060.13 | 78.48 |
| 8/13/2013 12:48:47 PM | 1.81306 | 1060.13 | 78.48 |
| 8/13/2013 12:48:48 PM | 1.81333 | 1060.13 | 78.48 |
| 8/13/2013 12:48:49 PM | 1.81361 | 1060.13 | 78.48 |
| 8/13/2013 12:48:50 PM | 1.81389 | 1060.14 | 78.48 |
| 8/13/2013 12:48:51 PM | 1.81417 | 1060.14 | 78.48 |
| 8/13/2013 12:48:52 PM | 1.81444 | 1060.14 | 78.48 |
| 8/13/2013 12:48:53 PM | 1.81472 | 1060.14 | 78.48 |
| 8/13/2013 12:48:54 PM | 1.81500 | 1060.15 | 78.48 |
| 8/13/2013 12:48:55 PM | 1.81528 | 1060.15 | 78.48 |
| 8/13/2013 12:48:56 PM | 1.81556 | 1060.15 | 78.48 |
| 8/13/2013 12:48:57 PM | 1.81583 | 1060.15 | 78.48 |
| 8/13/2013 12:48:58 PM | 1.81611 | 1060.15 | 78.48 |
| 8/13/2013 12:48:59 PM | 1.81639 | 1060.15 | 78.47 |
| 8/13/2013 12:49:00 PM | 1.81667 | 1060.16 | 78.47 |
| 8/13/2013 12:49:01 PM | 1.81694 | 1060.16 | 78.47 |
| 8/13/2013 12:49:02 PM | 1.81722 | 1060.16 | 78.47 |
| 8/13/2013 12:49:03 PM | 1.81750 | 1060.16 | 78.47 |
| 8/13/2013 12:49:04 PM | 1.81778 | 1060.17 | 78.47 |
| 8/13/2013 12:49:05 PM | 1.81806 | 1060.17 | 78.47 |
| 8/13/2013 12:49:06 PM | 1.81833 | 1060.17 | 78.47 |
| 8/13/2013 12:49:07 PM | 1.81861 | 1060.18 | 78.47 |
| 8/13/2013 12:49:08 PM | 1.81889 | 1060.18 | 78.47 |
| 8/13/2013 12:49:09 PM | 1.81917 | 1060.19 | 78.47 |
| 8/13/2013 12:49:10 PM | 1.81944 | 1060.19 | 78.47 |
| 8/13/2013 12:49:11 PM | 1.81972 | 1060.19 | 78.47 |
| 8/13/2013 12:49:12 PM | 1.82000 | 1060.19 | 78.47 |
| 8/13/2013 12:49:13 PM | 1.82028 | 1060.19 | 78.47 |
| 8/13/2013 12:49:14 PM | 1.82056 | 1060.19 | 78.47 |
| 8/13/2013 12:49:15 PM | 1.82083 | 1060.19 | 78.47 |
| 8/13/2013 12:49:16 PM | 1.82111 | 1060.19 | 78.47 |
| 8/13/2013 12:49:17 PM | 1.82139 | 1060.19 | 78.47 |
| 8/13/2013 12:49:18 PM | 1.82167 | 1060.19 | 78.47 |
| 8/13/2013 12:49:19 PM | 1.82194 | 1060.19 | 78.47 |
| 8/13/2013 12:49:20 PM | 1.82222 | 1060.19 | 78.47 |
| 8/13/2013 12:49:21 PM | 1.82250 | 1060.19 | 78.47 |
| 8/13/2013 12:49:22 PM | 1.82278 | 1060.19 | 78.47 |
| 8/13/2013 12:49:23 PM | 1.82306 | 1060.20 | 78.47 |
| 8/13/2013 12:49:24 PM | 1.82333 | 1060.20 | 78.47 |
| 8/13/2013 12:49:25 PM | 1.82361 | 1060.20 | 78.47 |
| 8/13/2013 12:49:26 PM | 1.82389 | 1060.21 | 78.47 |
| 8/13/2013 12:49:27 PM | 1.82417 | 1060.21 | 78.47 |
| 8/13/2013 12:49:28 PM | 1.82444 | 1060.21 | 78.47 |
| 8/13/2013 12:49:29 PM | 1.82472 | 1060.22 | 78.47 |
| 8/13/2013 12:49:30 PM | 1.82500 | 1060.22 | 78.47 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:49:31 PM | 1.82528 | 1060.22 | 78.47 |
| 8/13/2013 12:49:32 PM | 1.82556 | 1060.23 | 78.47 |
| 8/13/2013 12:49:33 PM | 1.82583 | 1060.23 | 78.47 |
| 8/13/2013 12:49:34 PM | 1.82611 | 1060.23 | 78.47 |
| 8/13/2013 12:49:35 PM | 1.82639 | 1060.23 | 78.47 |
| 8/13/2013 12:49:36 PM | 1.82667 | 1060.23 | 78.47 |
| 8/13/2013 12:49:37 PM | 1.82694 | 1060.23 | 78.47 |
| 8/13/2013 12:49:38 PM | 1.82722 | 1060.24 | 78.47 |
| 8/13/2013 12:49:39 PM | 1.82750 | 1060.24 | 78.47 |
| 8/13/2013 12:49:40 PM | 1.82778 | 1060.24 | 78.47 |
| 8/13/2013 12:49:41 PM | 1.82806 | 1060.24 | 78.47 |
| 8/13/2013 12:49:42 PM | 1.82833 | 1060.24 | 78.47 |
| 8/13/2013 12:49:43 PM | 1.82861 | 1060.24 | 78.47 |
| 8/13/2013 12:49:44 PM | 1.82889 | 1060.24 | 78.47 |
| 8/13/2013 12:49:45 PM | 1.82917 | 1060.25 | 78.47 |
| 8/13/2013 12:49:46 PM | 1.82944 | 1060.25 | 78.47 |
| 8/13/2013 12:49:47 PM | 1.82972 | 1060.25 | 78.47 |
| 8/13/2013 12:49:48 PM | 1.83000 | 1060.25 | 78.47 |
| 8/13/2013 12:49:49 PM | 1.83028 | 1060.26 | 78.47 |
| 8/13/2013 12:49:50 PM | 1.83056 | 1060.26 | 78.47 |
| 8/13/2013 12:49:51 PM | 1.83083 | 1060.27 | 78.47 |
| 8/13/2013 12:49:52 PM | 1.83111 | 1060.27 | 78.47 |
| 8/13/2013 12:49:53 PM | 1.83139 | 1060.27 | 78.47 |
| 8/13/2013 12:49:54 PM | 1.83167 | 1060.28 | 78.47 |
| 8/13/2013 12:49:55 PM | 1.83194 | 1060.28 | 78.46 |
| 8/13/2013 12:49:56 PM | 1.83222 | 1060.28 | 78.46 |
| 8/13/2013 12:49:57 PM | 1.83250 | 1060.29 | 78.46 |
| 8/13/2013 12:49:58 PM | 1.83278 | 1060.29 | 78.46 |
| 8/13/2013 12:49:59 PM | 1.83306 | 1060.29 | 78.46 |
| 8/13/2013 12:50:00 PM | 1.83333 | 1060.29 | 78.46 |
| 8/13/2013 12:50:01 PM | 1.83361 | 1060.29 | 78.46 |
| 8/13/2013 12:50:02 PM | 1.83389 | 1060.29 | 78.46 |
| 8/13/2013 12:50:03 PM | 1.83417 | 1060.30 | 78.46 |
| 8/13/2013 12:50:04 PM | 1.83444 | 1060.30 | 78.46 |
| 8/13/2013 12:50:05 PM | 1.83472 | 1060.30 | 78.46 |
| 8/13/2013 12:50:06 PM | 1.83500 | 1060.31 | 78.46 |
| 8/13/2013 12:50:07 PM | 1.83528 | 1060.31 | 78.46 |
| 8/13/2013 12:50:08 PM | 1.83556 | 1060.31 | 78.46 |
| 8/13/2013 12:50:09 PM | 1.83583 | 1060.31 | 78.46 |
| 8/13/2013 12:50:10 PM | 1.83611 | 1060.32 | 78.46 |
| 8/13/2013 12:50:11 PM | 1.83639 | 1060.32 | 78.46 |
| 8/13/2013 12:50:12 PM | 1.83667 | 1060.32 | 78.46 |
| 8/13/2013 12:50:13 PM | 1.83694 | 1060.32 | 78.46 |
| 8/13/2013 12:50:14 PM | 1.83722 | 1060.33 | 78.46 |
| 8/13/2013 12:50:15 PM | 1.83750 | 1060.33 | 78.46 |
| 8/13/2013 12:50:16 PM | 1.83778 | 1060.33 | 78.46 |
| 8/13/2013 12:50:17 PM | 1.83806 | 1060.33 | 78.46 |
| 8/13/2013 12:50:18 PM | 1.83833 | 1060.33 | 78.46 |
| 8/13/2013 12:50:19 PM | 1.83861 | 1060.34 | 78.46 |
| 8/13/2013 12:50:20 PM | 1.83889 | 1060.34 | 78.46 |
| 8/13/2013 12:50:21 PM | 1.83917 | 1060.34 | 78.46 |
| 8/13/2013 12:50:22 PM | 1.83944 | 1060.34 | 78.46 |
| 8/13/2013 12:50:23 PM | 1.83972 | 1060.34 | 78.46 |
| 8/13/2013 12:50:24 PM | 1.84000 | 1060.34 | 78.46 |
| 8/13/2013 12:50:25 PM | 1.84028 | 1060.34 | 78.46 |
| 8/13/2013 12:50:26 PM | 1.84056 | 1060.35 | 78.46 |
| 8/13/2013 12:50:27 PM | 1.84083 | 1060.35 | 78.46 |
| 8/13/2013 12:50:28 PM | 1.84111 | 1060.35 | 78.46 |
| 8/13/2013 12:50:29 PM | 1.84139 | 1060.35 | 78.46 |
| 8/13/2013 12:50:30 PM | 1.84167 | 1060.35 | 78.46 |
| 8/13/2013 12:50:31 PM | 1.84194 | 1060.36 | 78.46 |
| 8/13/2013 12:50:32 PM | 1.84222 | 1060.36 | 78.46 |
| 8/13/2013 12:50:33 PM | 1.84250 | 1060.36 | 78.46 |
| 8/13/2013 12:50:34 PM | 1.84278 | 1060.36 | 78.46 |
| 8/13/2013 12:50:35 PM | 1.84306 | 1060.37 | 78.46 |
| 8/13/2013 12:50:36 PM | 1.84333 | 1060.37 | 78.46 |
| 8/13/2013 12:50:37 PM | 1.84361 | 1060.37 | 78.46 |
| 8/13/2013 12:50:38 PM | 1.84389 | 1060.37 | 78.46 |
| 8/13/2013 12:50:39 PM | 1.84417 | 1060.37 | 78.46 |
| 8/13/2013 12:50:40 PM | 1.84444 | 1060.38 | 78.46 |
| 8/13/2013 12:50:41 PM | 1.84472 | 1060.38 | 78.46 |
| 8/13/2013 12:50:42 PM | 1.84500 | 1060.38 | 78.46 |
| 8/13/2013 12:50:43 PM | 1.84528 | 1060.38 | 78.46 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:50:44 PM | 1.84556 | 1060.39 | 78.46 |
| 8/13/2013 12:50:45 PM | 1.84583 | 1060.39 | 78.46 |
| 8/13/2013 12:50:46 PM | 1.84611 | 1060.39 | 78.46 |
| 8/13/2013 12:50:47 PM | 1.84639 | 1060.39 | 78.46 |
| 8/13/2013 12:50:48 PM | 1.84667 | 1060.39 | 78.46 |
| 8/13/2013 12:50:49 PM | 1.84694 | 1060.40 | 78.46 |
| 8/13/2013 12:50:50 PM | 1.84722 | 1060.40 | 78.45 |
| 8/13/2013 12:50:51 PM | 1.84750 | 1060.40 | 78.45 |
| 8/13/2013 12:50:52 PM | 1.84778 | 1060.40 | 78.45 |
| 8/13/2013 12:50:53 PM | 1.84806 | 1060.40 | 78.45 |
| 8/13/2013 12:50:54 PM | 1.84833 | 1060.41 | 78.45 |
| 8/13/2013 12:50:55 PM | 1.84861 | 1060.41 | 78.45 |
| 8/13/2013 12:50:56 PM | 1.84889 | 1060.41 | 78.45 |
| 8/13/2013 12:50:57 PM | 1.84917 | 1060.41 | 78.45 |
| 8/13/2013 12:50:58 PM | 1.84944 | 1060.41 | 78.45 |
| 8/13/2013 12:50:59 PM | 1.84972 | 1060.42 | 78.45 |
| 8/13/2013 12:51:00 PM | 1.85000 | 1060.42 | 78.45 |
| 8/13/2013 12:51:01 PM | 1.85028 | 1060.42 | 78.45 |
| 8/13/2013 12:51:02 PM | 1.85056 | 1060.42 | 78.45 |
| 8/13/2013 12:51:03 PM | 1.85083 | 1060.42 | 78.45 |
| 8/13/2013 12:51:04 PM | 1.85111 | 1060.43 | 78.45 |
| 8/13/2013 12:51:05 PM | 1.85139 | 1060.43 | 78.45 |
| 8/13/2013 12:51:06 PM | 1.85167 | 1060.43 | 78.45 |
| 8/13/2013 12:51:07 PM | 1.85194 | 1060.43 | 78.45 |
| 8/13/2013 12:51:08 PM | 1.85222 | 1060.44 | 78.45 |
| 8/13/2013 12:51:09 PM | 1.85250 | 1060.44 | 78.45 |
| 8/13/2013 12:51:10 PM | 1.85278 | 1060.44 | 78.45 |
| 8/13/2013 12:51:11 PM | 1.85306 | 1060.44 | 78.45 |
| 8/13/2013 12:51:12 PM | 1.85333 | 1060.44 | 78.45 |
| 8/13/2013 12:51:13 PM | 1.85361 | 1060.45 | 78.45 |
| 8/13/2013 12:51:14 PM | 1.85389 | 1060.45 | 78.45 |
| 8/13/2013 12:51:15 PM | 1.85417 | 1060.45 | 78.45 |
| 8/13/2013 12:51:16 PM | 1.85444 | 1060.45 | 78.45 |
| 8/13/2013 12:51:17 PM | 1.85472 | 1060.45 | 78.45 |
| 8/13/2013 12:51:18 PM | 1.85500 | 1060.45 | 78.45 |
| 8/13/2013 12:51:19 PM | 1.85528 | 1060.45 | 78.45 |
| 8/13/2013 12:51:20 PM | 1.85556 | 1060.46 | 78.45 |
| 8/13/2013 12:51:21 PM | 1.85583 | 1060.46 | 78.45 |
| 8/13/2013 12:51:22 PM | 1.85611 | 1060.46 | 78.45 |
| 8/13/2013 12:51:23 PM | 1.85639 | 1060.46 | 78.45 |
| 8/13/2013 12:51:24 PM | 1.85667 | 1060.46 | 78.45 |
| 8/13/2013 12:51:25 PM | 1.85694 | 1060.47 | 78.45 |
| 8/13/2013 12:51:26 PM | 1.85722 | 1060.47 | 78.45 |
| 8/13/2013 12:51:27 PM | 1.85750 | 1060.47 | 78.45 |
| 8/13/2013 12:51:28 PM | 1.85778 | 1060.47 | 78.45 |
| 8/13/2013 12:51:29 PM | 1.85806 | 1060.47 | 78.45 |
| 8/13/2013 12:51:30 PM | 1.85833 | 1060.48 | 78.45 |
| 8/13/2013 12:51:31 PM | 1.85861 | 1060.48 | 78.45 |
| 8/13/2013 12:51:32 PM | 1.85889 | 1060.48 | 78.45 |
| 8/13/2013 12:51:33 PM | 1.85917 | 1060.49 | 78.45 |
| 8/13/2013 12:51:34 PM | 1.85944 | 1060.49 | 78.45 |
| 8/13/2013 12:51:35 PM | 1.85972 | 1060.49 | 78.45 |
| 8/13/2013 12:51:36 PM | 1.86000 | 1060.50 | 78.45 |
| 8/13/2013 12:51:37 PM | 1.86028 | 1060.50 | 78.45 |
| 8/13/2013 12:51:38 PM | 1.86056 | 1060.50 | 78.45 |
| 8/13/2013 12:51:39 PM | 1.86083 | 1060.50 | 78.45 |
| 8/13/2013 12:51:40 PM | 1.86111 | 1060.50 | 78.45 |
| 8/13/2013 12:51:41 PM | 1.86139 | 1060.51 | 78.45 |
| 8/13/2013 12:51:42 PM | 1.86167 | 1060.51 | 78.45 |
| 8/13/2013 12:51:43 PM | 1.86194 | 1060.51 | 78.45 |
| 8/13/2013 12:51:44 PM | 1.86222 | 1060.51 | 78.45 |
| 8/13/2013 12:51:45 PM | 1.86250 | 1060.51 | 78.45 |
| 8/13/2013 12:51:46 PM | 1.86278 | 1060.51 | 78.45 |
| 8/13/2013 12:51:47 PM | 1.86306 | 1060.51 | 78.45 |
| 8/13/2013 12:51:48 PM | 1.86333 | 1060.52 | 78.45 |
| 8/13/2013 12:51:49 PM | 1.86361 | 1060.52 | 78.45 |
| 8/13/2013 12:51:50 PM | 1.86389 | 1060.52 | 78.45 |
| 8/13/2013 12:51:51 PM | 1.86417 | 1060.52 | 78.44 |
| 8/13/2013 12:51:52 PM | 1.86444 | 1060.53 | 78.44 |
| 8/13/2013 12:51:53 PM | 1.86472 | 1060.53 | 78.44 |
| 8/13/2013 12:51:54 PM | 1.86500 | 1060.53 | 78.44 |
| 8/13/2013 12:51:55 PM | 1.86528 | 1060.53 | 78.44 |
| 8/13/2013 12:51:56 PM | 1.86556 | 1060.54 | 78.44 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:51:57 PM | 1.86583 | 1060.54 | 78.44 |
| 8/13/2013 12:51:58 PM | 1.86611 | 1060.54 | 78.44 |
| 8/13/2013 12:51:59 PM | 1.86639 | 1060.54 | 78.44 |
| 8/13/2013 12:52:00 PM | 1.86667 | 1060.54 | 78.44 |
| 8/13/2013 12:52:01 PM | 1.86694 | 1060.55 | 78.44 |
| 8/13/2013 12:52:02 PM | 1.86722 | 1060.55 | 78.44 |
| 8/13/2013 12:52:03 PM | 1.86750 | 1060.55 | 78.44 |
| 8/13/2013 12:52:04 PM | 1.86778 | 1060.55 | 78.44 |
| 8/13/2013 12:52:05 PM | 1.86806 | 1060.55 | 78.44 |
| 8/13/2013 12:52:06 PM | 1.86833 | 1060.56 | 78.44 |
| 8/13/2013 12:52:07 PM | 1.86861 | 1060.56 | 78.44 |
| 8/13/2013 12:52:08 PM | 1.86889 | 1060.56 | 78.44 |
| 8/13/2013 12:52:09 PM | 1.86917 | 1060.56 | 78.44 |
| 8/13/2013 12:52:10 PM | 1.86944 | 1060.56 | 78.44 |
| 8/13/2013 12:52:11 PM | 1.86972 | 1060.57 | 78.44 |
| 8/13/2013 12:52:12 PM | 1.87000 | 1060.57 | 78.44 |
| 8/13/2013 12:52:13 PM | 1.87028 | 1060.57 | 78.44 |
| 8/13/2013 12:52:14 PM | 1.87056 | 1060.57 | 78.44 |
| 8/13/2013 12:52:15 PM | 1.87083 | 1060.58 | 78.44 |
| 8/13/2013 12:52:16 PM | 1.87111 | 1060.58 | 78.44 |
| 8/13/2013 12:52:17 PM | 1.87139 | 1060.58 | 78.44 |
| 8/13/2013 12:52:18 PM | 1.87167 | 1060.58 | 78.44 |
| 8/13/2013 12:52:19 PM | 1.87194 | 1060.58 | 78.44 |
| 8/13/2013 12:52:20 PM | 1.87222 | 1060.58 | 78.44 |
| 8/13/2013 12:52:21 PM | 1.87250 | 1060.58 | 78.44 |
| 8/13/2013 12:52:22 PM | 1.87278 | 1060.58 | 78.44 |
| 8/13/2013 12:52:23 PM | 1.87306 | 1060.59 | 78.44 |
| 8/13/2013 12:52:24 PM | 1.87333 | 1060.59 | 78.44 |
| 8/13/2013 12:52:25 PM | 1.87361 | 1060.59 | 78.44 |
| 8/13/2013 12:52:26 PM | 1.87389 | 1060.59 | 78.44 |
| 8/13/2013 12:52:27 PM | 1.87417 | 1060.60 | 78.44 |
| 8/13/2013 12:52:28 PM | 1.87444 | 1060.60 | 78.44 |
| 8/13/2013 12:52:29 PM | 1.87472 | 1060.60 | 78.44 |
| 8/13/2013 12:52:30 PM | 1.87500 | 1060.60 | 78.44 |
| 8/13/2013 12:52:31 PM | 1.87528 | 1060.61 | 78.44 |
| 8/13/2013 12:52:32 PM | 1.87556 | 1060.61 | 78.44 |
| 8/13/2013 12:52:33 PM | 1.87583 | 1060.61 | 78.44 |
| 8/13/2013 12:52:34 PM | 1.87611 | 1060.61 | 78.44 |
| 8/13/2013 12:52:35 PM | 1.87639 | 1060.62 | 78.44 |
| 8/13/2013 12:52:36 PM | 1.87667 | 1060.62 | 78.44 |
| 8/13/2013 12:52:37 PM | 1.87694 | 1060.62 | 78.44 |
| 8/13/2013 12:52:38 PM | 1.87722 | 1060.63 | 78.44 |
| 8/13/2013 12:52:39 PM | 1.87750 | 1060.63 | 78.44 |
| 8/13/2013 12:52:40 PM | 1.87778 | 1060.63 | 78.44 |
| 8/13/2013 12:52:41 PM | 1.87806 | 1060.63 | 78.44 |
| 8/13/2013 12:52:42 PM | 1.87833 | 1060.64 | 78.44 |
| 8/13/2013 12:52:43 PM | 1.87861 | 1060.64 | 78.44 |
| 8/13/2013 12:52:44 PM | 1.87889 | 1060.64 | 78.44 |
| 8/13/2013 12:52:45 PM | 1.87917 | 1060.64 | 78.44 |
| 8/13/2013 12:52:46 PM | 1.87944 | 1060.64 | 78.44 |
| 8/13/2013 12:52:47 PM | 1.87972 | 1060.64 | 78.44 |
| 8/13/2013 12:52:48 PM | 1.88000 | 1060.64 | 78.44 |
| 8/13/2013 12:52:49 PM | 1.88028 | 1060.64 | 78.44 |
| 8/13/2013 12:52:50 PM | 1.88056 | 1060.63 | 78.44 |
| 8/13/2013 12:52:51 PM | 1.88083 | 1060.63 | 78.44 |
| 8/13/2013 12:52:52 PM | 1.88111 | 1060.63 | 78.44 |
| 8/13/2013 12:52:53 PM | 1.88139 | 1060.64 | 78.44 |
| 8/13/2013 12:52:54 PM | 1.88167 | 1060.64 | 78.44 |
| 8/13/2013 12:52:55 PM | 1.88194 | 1060.64 | 78.43 |
| 8/13/2013 12:52:56 PM | 1.88222 | 1060.64 | 78.43 |
| 8/13/2013 12:52:57 PM | 1.88250 | 1060.65 | 78.43 |
| 8/13/2013 12:52:58 PM | 1.88278 | 1060.65 | 78.43 |
| 8/13/2013 12:52:59 PM | 1.88306 | 1060.65 | 78.43 |
| 8/13/2013 12:53:00 PM | 1.88333 | 1060.66 | 78.43 |
| 8/13/2013 12:53:01 PM | 1.88361 | 1060.66 | 78.43 |
| 8/13/2013 12:53:02 PM | 1.88389 | 1060.66 | 78.43 |
| 8/13/2013 12:53:03 PM | 1.88417 | 1060.66 | 78.43 |
| 8/13/2013 12:53:04 PM | 1.88444 | 1060.67 | 78.43 |
| 8/13/2013 12:53:05 PM | 1.88472 | 1060.67 | 78.43 |
| 8/13/2013 12:53:06 PM | 1.88500 | 1060.67 | 78.43 |
| 8/13/2013 12:53:07 PM | 1.88528 | 1060.67 | 78.43 |
| 8/13/2013 12:53:08 PM | 1.88556 | 1060.68 | 78.43 |
| 8/13/2013 12:53:09 PM | 1.88583 | 1060.68 | 78.43 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:53:10 PM | 1.88611 | 1060.68 | 78.43 |
| 8/13/2013 12:53:11 PM | 1.88639 | 1060.68 | 78.43 |
| 8/13/2013 12:53:12 PM | 1.88667 | 1060.69 | 78.43 |
| 8/13/2013 12:53:13 PM | 1.88694 | 1060.69 | 78.43 |
| 8/13/2013 12:53:14 PM | 1.88722 | 1060.69 | 78.43 |
| 8/13/2013 12:53:15 PM | 1.88750 | 1060.69 | 78.43 |
| 8/13/2013 12:53:16 PM | 1.88778 | 1060.69 | 78.43 |
| 8/13/2013 12:53:17 PM | 1.88806 | 1060.69 | 78.43 |
| 8/13/2013 12:53:18 PM | 1.88833 | 1060.69 | 78.43 |
| 8/13/2013 12:53:19 PM | 1.88861 | 1060.69 | 78.43 |
| 8/13/2013 12:53:20 PM | 1.88889 | 1060.70 | 78.43 |
| 8/13/2013 12:53:21 PM | 1.88917 | 1060.70 | 78.43 |
| 8/13/2013 12:53:22 PM | 1.88944 | 1060.70 | 78.43 |
| 8/13/2013 12:53:23 PM | 1.88972 | 1060.70 | 78.43 |
| 8/13/2013 12:53:24 PM | 1.89000 | 1060.70 | 78.43 |
| 8/13/2013 12:53:25 PM | 1.89028 | 1060.70 | 78.43 |
| 8/13/2013 12:53:26 PM | 1.89056 | 1060.70 | 78.43 |
| 8/13/2013 12:53:27 PM | 1.89083 | 1060.70 | 78.43 |
| 8/13/2013 12:53:28 PM | 1.89111 | 1060.71 | 78.43 |
| 8/13/2013 12:53:29 PM | 1.89139 | 1060.71 | 78.43 |
| 8/13/2013 12:53:30 PM | 1.89167 | 1060.71 | 78.43 |
| 8/13/2013 12:53:31 PM | 1.89194 | 1060.71 | 78.43 |
| 8/13/2013 12:53:32 PM | 1.89222 | 1060.72 | 78.43 |
| 8/13/2013 12:53:33 PM | 1.89250 | 1060.72 | 78.43 |
| 8/13/2013 12:53:34 PM | 1.89278 | 1060.72 | 78.43 |
| 8/13/2013 12:53:35 PM | 1.89306 | 1060.73 | 78.43 |
| 8/13/2013 12:53:36 PM | 1.89333 | 1060.73 | 78.43 |
| 8/13/2013 12:53:37 PM | 1.89361 | 1060.73 | 78.43 |
| 8/13/2013 12:53:38 PM | 1.89389 | 1060.74 | 78.43 |
| 8/13/2013 12:53:39 PM | 1.89417 | 1060.74 | 78.43 |
| 8/13/2013 12:53:40 PM | 1.89444 | 1060.74 | 78.43 |
| 8/13/2013 12:53:41 PM | 1.89472 | 1060.74 | 78.43 |
| 8/13/2013 12:53:42 PM | 1.89500 | 1060.74 | 78.43 |
| 8/13/2013 12:53:43 PM | 1.89528 | 1060.74 | 78.43 |
| 8/13/2013 12:53:44 PM | 1.89556 | 1060.74 | 78.43 |
| 8/13/2013 12:53:45 PM | 1.89583 | 1060.74 | 78.43 |
| 8/13/2013 12:53:46 PM | 1.89611 | 1060.75 | 78.43 |
| 8/13/2013 12:53:47 PM | 1.89639 | 1060.75 | 78.42 |
| 8/13/2013 12:53:48 PM | 1.89667 | 1060.75 | 78.42 |
| 8/13/2013 12:53:49 PM | 1.89694 | 1060.76 | 78.42 |
| 8/13/2013 12:53:50 PM | 1.89722 | 1060.76 | 78.42 |
| 8/13/2013 12:53:51 PM | 1.89750 | 1060.76 | 78.42 |
| 8/13/2013 12:53:52 PM | 1.89778 | 1060.77 | 78.42 |
| 8/13/2013 12:53:53 PM | 1.89806 | 1060.77 | 78.42 |
| 8/13/2013 12:53:54 PM | 1.89833 | 1060.77 | 78.42 |
| 8/13/2013 12:53:55 PM | 1.89861 | 1060.78 | 78.42 |
| 8/13/2013 12:53:56 PM | 1.89889 | 1060.78 | 78.42 |
| 8/13/2013 12:53:57 PM | 1.89917 | 1060.78 | 78.42 |
| 8/13/2013 12:53:58 PM | 1.89944 | 1060.78 | 78.42 |
| 8/13/2013 12:53:59 PM | 1.89972 | 1060.79 | 78.42 |
| 8/13/2013 12:54:00 PM | 1.90000 | 1060.79 | 78.42 |
| 8/13/2013 12:54:01 PM | 1.90028 | 1060.79 | 78.42 |
| 8/13/2013 12:54:02 PM | 1.90056 | 1060.79 | 78.42 |
| 8/13/2013 12:54:03 PM | 1.90083 | 1060.79 | 78.42 |
| 8/13/2013 12:54:04 PM | 1.90111 | 1060.79 | 78.42 |
| 8/13/2013 12:54:05 PM | 1.90139 | 1060.79 | 78.42 |
| 8/13/2013 12:54:06 PM | 1.90167 | 1060.79 | 78.42 |
| 8/13/2013 12:54:07 PM | 1.90194 | 1060.79 | 78.42 |
| 8/13/2013 12:54:08 PM | 1.90222 | 1060.80 | 78.42 |
| 8/13/2013 12:54:09 PM | 1.90250 | 1060.80 | 78.42 |
| 8/13/2013 12:54:10 PM | 1.90278 | 1060.80 | 78.42 |
| 8/13/2013 12:54:11 PM | 1.90306 | 1060.81 | 78.42 |
| 8/13/2013 12:54:12 PM | 1.90333 | 1060.81 | 78.42 |
| 8/13/2013 12:54:13 PM | 1.90361 | 1060.81 | 78.42 |
| 8/13/2013 12:54:14 PM | 1.90389 | 1060.81 | 78.42 |
| 8/13/2013 12:54:15 PM | 1.90417 | 1060.82 | 78.42 |
| 8/13/2013 12:54:16 PM | 1.90444 | 1060.82 | 78.42 |
| 8/13/2013 12:54:17 PM | 1.90472 | 1060.82 | 78.42 |
| 8/13/2013 12:54:18 PM | 1.90500 | 1060.82 | 78.42 |
| 8/13/2013 12:54:19 PM | 1.90528 | 1060.82 | 78.42 |
| 8/13/2013 12:54:20 PM | 1.90556 | 1060.83 | 78.42 |
| 8/13/2013 12:54:21 PM | 1.90583 | 1060.83 | 78.42 |
| 8/13/2013 12:54:22 PM | 1.90611 | 1060.83 | 78.42 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:54:23 PM | 1.90639 | 1060.83 | 78.42 |
| 8/13/2013 12:54:24 PM | 1.90667 | 1060.83 | 78.42 |
| 8/13/2013 12:54:25 PM | 1.90694 | 1060.84 | 78.42 |
| 8/13/2013 12:54:26 PM | 1.90722 | 1060.84 | 78.42 |
| 8/13/2013 12:54:27 PM | 1.90750 | 1060.84 | 78.42 |
| 8/13/2013 12:54:28 PM | 1.90778 | 1060.84 | 78.42 |
| 8/13/2013 12:54:29 PM | 1.90806 | 1060.84 | 78.42 |
| 8/13/2013 12:54:30 PM | 1.90833 | 1060.85 | 78.42 |
| 8/13/2013 12:54:31 PM | 1.90861 | 1060.85 | 78.42 |
| 8/13/2013 12:54:32 PM | 1.90889 | 1060.85 | 78.42 |
| 8/13/2013 12:54:33 PM | 1.90917 | 1060.85 | 78.42 |
| 8/13/2013 12:54:34 PM | 1.90944 | 1060.86 | 78.42 |
| 8/13/2013 12:54:35 PM | 1.90972 | 1060.86 | 78.42 |
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| 8/13/2013 12:54:41 PM | 1.91139 | 1060.88 | 78.42 |
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| 8/13/2013 12:54:43 PM | 1.91194 | 1060.88 | 78.42 |
| 8/13/2013 12:54:44 PM | 1.91222 | 1060.89 | 78.42 |
| 8/13/2013 12:54:45 PM | 1.91250 | 1060.89 | 78.42 |
| 8/13/2013 12:54:46 PM | 1.91278 | 1060.89 | 78.42 |
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| 8/13/2013 12:54:51 PM | 1.91417 | 1060.90 | 78.41 |
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| 8/13/2013 12:54:57 PM | 1.91583 | 1060.90 | 78.41 |
| 8/13/2013 12:54:58 PM | 1.91611 | 1060.91 | 78.41 |
| 8/13/2013 12:54:59 PM | 1.91639 | 1060.91 | 78.41 |
| 8/13/2013 12:55:00 PM | 1.91667 | 1060.91 | 78.41 |
| 8/13/2013 12:55:01 PM | 1.91694 | 1060.91 | 78.41 |
| 8/13/2013 12:55:02 PM | 1.91722 | 1060.92 | 78.41 |
| 8/13/2013 12:55:03 PM | 1.91750 | 1060.92 | 78.41 |
| 8/13/2013 12:55:04 PM | 1.91778 | 1060.92 | 78.41 |
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| 8/13/2013 12:55:28 PM | 1.92444 | 1060.98 | 78.41 |
| 8/13/2013 12:55:29 PM | 1.92472 | 1060.98 | 78.41 |
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| 8/13/2013 12:55:31 PM | 1.92528 | 1060.98 | 78.41 |
| 8/13/2013 12:55:32 PM | 1.92556 | 1060.98 | 78.41 |
| 8/13/2013 12:55:33 PM | 1.92583 | 1060.98 | 78.41 |
| 8/13/2013 12:55:34 PM | 1.92611 | 1060.99 | 78.41 |
| 8/13/2013 12:55:35 PM | 1.92639 | 1060.99 | 78.41 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:55:36 PM | 1.92667 | 1060.99 | 78.41 |
| 8/13/2013 12:55:37 PM | 1.92694 | 1060.99 | 78.41 |
| 8/13/2013 12:55:38 PM | 1.92722 | 1060.99 | 78.41 |
| 8/13/2013 12:55:39 PM | 1.92750 | 1060.99 | 78.41 |
| 8/13/2013 12:55:40 PM | 1.92778 | 1061.00 | 78.40 |
| 8/13/2013 12:55:41 PM | 1.92806 | 1061.00 | 78.40 |
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| 8/13/2013 12:55:43 PM | 1.92861 | 1061.00 | 78.40 |
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| 8/13/2013 12:55:45 PM | 1.92917 | 1061.01 | 78.40 |
| 8/13/2013 12:55:46 PM | 1.92944 | 1061.01 | 78.40 |
| 8/13/2013 12:55:47 PM | 1.92972 | 1061.01 | 78.40 |
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| 8/13/2013 12:55:50 PM | 1.93056 | 1061.02 | 78.40 |
| 8/13/2013 12:55:51 PM | 1.93083 | 1061.02 | 78.40 |
| 8/13/2013 12:55:52 PM | 1.93111 | 1061.02 | 78.40 |
| 8/13/2013 12:55:53 PM | 1.93139 | 1061.02 | 78.40 |
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| 8/13/2013 12:55:57 PM | 1.93250 | 1061.03 | 78.40 |
| 8/13/2013 12:55:58 PM | 1.93278 | 1061.03 | 78.40 |
| 8/13/2013 12:55:59 PM | 1.93306 | 1061.03 | 78.40 |
| 8/13/2013 12:56:00 PM | 1.93333 | 1061.03 | 78.40 |
| 8/13/2013 12:56:01 PM | 1.93361 | 1061.03 | 78.40 |
| 8/13/2013 12:56:02 PM | 1.93389 | 1061.04 | 78.40 |
| 8/13/2013 12:56:03 PM | 1.93417 | 1061.04 | 78.40 |
| 8/13/2013 12:56:04 PM | 1.93444 | 1061.04 | 78.40 |
| 8/13/2013 12:56:05 PM | 1.93472 | 1061.05 | 78.40 |
| 8/13/2013 12:56:06 PM | 1.93500 | 1061.05 | 78.40 |
| 8/13/2013 12:56:07 PM | 1.93528 | 1061.05 | 78.40 |
| 8/13/2013 12:56:08 PM | 1.93556 | 1061.05 | 78.40 |
| 8/13/2013 12:56:09 PM | 1.93583 | 1061.06 | 78.40 |
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| 8/13/2013 12:56:12 PM | 1.93667 | 1061.06 | 78.40 |
| 8/13/2013 12:56:13 PM | 1.93694 | 1061.07 | 78.40 |
| 8/13/2013 12:56:14 PM | 1.93722 | 1061.07 | 78.40 |
| 8/13/2013 12:56:15 PM | 1.93750 | 1061.07 | 78.40 |
| 8/13/2013 12:56:16 PM | 1.93778 | 1061.08 | 78.40 |
| 8/13/2013 12:56:17 PM | 1.93806 | 1061.08 | 78.40 |
| 8/13/2013 12:56:18 PM | 1.93833 | 1061.08 | 78.40 |
| 8/13/2013 12:56:19 PM | 1.93861 | 1061.08 | 78.40 |
| 8/13/2013 12:56:20 PM | 1.93889 | 1061.08 | 78.40 |
| 8/13/2013 12:56:21 PM | 1.93917 | 1061.09 | 78.40 |
| 8/13/2013 12:56:22 PM | 1.93944 | 1061.09 | 78.40 |
| 8/13/2013 12:56:23 PM | 1.93972 | 1061.09 | 78.40 |
| 8/13/2013 12:56:24 PM | 1.94000 | 1061.09 | 78.40 |
| 8/13/2013 12:56:25 PM | 1.94028 | 1061.09 | 78.39 |
| 8/13/2013 12:56:26 PM | 1.94056 | 1061.10 | 78.39 |
| 8/13/2013 12:56:27 PM | 1.94083 | 1061.10 | 78.39 |
| 8/13/2013 12:56:28 PM | 1.94111 | 1061.10 | 78.39 |
| 8/13/2013 12:56:29 PM | 1.94139 | 1061.10 | 78.39 |
| 8/13/2013 12:56:30 PM | 1.94167 | 1061.10 | 78.39 |
| 8/13/2013 12:56:31 PM | 1.94194 | 1061.10 | 78.39 |
| 8/13/2013 12:56:32 PM | 1.94222 | 1061.10 | 78.39 |
| 8/13/2013 12:56:33 PM | 1.94250 | 1061.10 | 78.39 |
| 8/13/2013 12:56:34 PM | 1.94278 | 1061.10 | 78.39 |
| 8/13/2013 12:56:35 PM | 1.94306 | 1061.10 | 78.39 |
| 8/13/2013 12:56:36 PM | 1.94333 | 1061.10 | 78.39 |
| 8/13/2013 12:56:37 PM | 1.94361 | 1061.10 | 78.39 |
| 8/13/2013 12:56:38 PM | 1.94389 | 1061.11 | 78.39 |
| 8/13/2013 12:56:39 PM | 1.94417 | 1061.11 | 78.39 |
| 8/13/2013 12:56:40 PM | 1.94444 | 1061.11 | 78.39 |
| 8/13/2013 12:56:41 PM | 1.94472 | 1061.11 | 78.39 |
| 8/13/2013 12:56:42 PM | 1.94500 | 1061.12 | 78.39 |
| 8/13/2013 12:56:43 PM | 1.94528 | 1061.12 | 78.39 |
| 8/13/2013 12:56:44 PM | 1.94556 | 1061.12 | 78.39 |
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| 8/13/2013 12:56:46 PM | 1.94611 | 1061.12 | 78.39 |
| 8/13/2013 12:56:47 PM | 1.94639 | 1061.12 | 78.39 |
| 8/13/2013 12:56:48 PM | 1.94667 | 1061.13 | 78.39 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:56:49 PM | 1.94694 | 1061.13 | 78.39 |
| 8/13/2013 12:56:50 PM | 1.94722 | 1061.13 | 78.39 |
| 8/13/2013 12:56:51 PM | 1.94750 | 1061.13 | 78.39 |
| 8/13/2013 12:56:52 PM | 1.94778 | 1061.13 | 78.39 |
| 8/13/2013 12:56:53 PM | 1.94806 | 1061.14 | 78.39 |
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| 8/13/2013 12:56:55 PM | 1.94861 | 1061.14 | 78.39 |
| 8/13/2013 12:56:56 PM | 1.94889 | 1061.14 | 78.39 |
| 8/13/2013 12:56:57 PM | 1.94917 | 1061.14 | 78.39 |
| 8/13/2013 12:56:58 PM | 1.94944 | 1061.14 | 78.39 |
| 8/13/2013 12:56:59 PM | 1.94972 | 1061.15 | 78.39 |
| 8/13/2013 12:57:00 PM | 1.95000 | 1061.15 | 78.39 |
| 8/13/2013 12:57:01 PM | 1.95028 | 1061.15 | 78.39 |
| 8/13/2013 12:57:02 PM | 1.95056 | 1061.15 | 78.39 |
| 8/13/2013 12:57:03 PM | 1.95083 | 1061.15 | 78.39 |
| 8/13/2013 12:57:04 PM | 1.95111 | 1061.16 | 78.39 |
| 8/13/2013 12:57:05 PM | 1.95139 | 1061.16 | 78.39 |
| 8/13/2013 12:57:06 PM | 1.95167 | 1061.16 | 78.39 |
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| 8/13/2013 12:57:12 PM | 1.95333 | 1061.17 | 78.39 |
| 8/13/2013 12:57:13 PM | 1.95361 | 1061.17 | 78.39 |
| 8/13/2013 12:57:14 PM | 1.95389 | 1061.17 | 78.39 |
| 8/13/2013 12:57:15 PM | 1.95417 | 1061.18 | 78.39 |
| 8/13/2013 12:57:16 PM | 1.95444 | 1061.18 | 78.39 |
| 8/13/2013 12:57:17 PM | 1.95472 | 1061.18 | 78.39 |
| 8/13/2013 12:57:18 PM | 1.95500 | 1061.19 | 78.38 |
| 8/13/2013 12:57:19 PM | 1.95528 | 1061.19 | 78.38 |
| 8/13/2013 12:57:20 PM | 1.95556 | 1061.19 | 78.38 |
| 8/13/2013 12:57:21 PM | 1.95583 | 1061.20 | 78.38 |
| 8/13/2013 12:57:22 PM | 1.95611 | 1061.20 | 78.38 |
| 8/13/2013 12:57:23 PM | 1.95639 | 1061.20 | 78.38 |
| 8/13/2013 12:57:24 PM | 1.95667 | 1061.20 | 78.38 |
| 8/13/2013 12:57:25 PM | 1.95694 | 1061.20 | 78.38 |
| 8/13/2013 12:57:26 PM | 1.95722 | 1061.20 | 78.38 |
| 8/13/2013 12:57:27 PM | 1.95750 | 1061.20 | 78.38 |
| 8/13/2013 12:57:28 PM | 1.95778 | 1061.20 | 78.38 |
| 8/13/2013 12:57:29 PM | 1.95806 | 1061.21 | 78.38 |
| 8/13/2013 12:57:30 PM | 1.95833 | 1061.21 | 78.38 |
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| 8/13/2013 12:57:33 PM | 1.95917 | 1061.21 | 78.38 |
| 8/13/2013 12:57:34 PM | 1.95944 | 1061.21 | 78.38 |
| 8/13/2013 12:57:35 PM | 1.95972 | 1061.21 | 78.38 |
| 8/13/2013 12:57:36 PM | 1.96000 | 1061.21 | 78.38 |
| 8/13/2013 12:57:37 PM | 1.96028 | 1061.22 | 78.38 |
| 8/13/2013 12:57:38 PM | 1.96056 | 1061.22 | 78.38 |
| 8/13/2013 12:57:39 PM | 1.96083 | 1061.22 | 78.38 |
| 8/13/2013 12:57:40 PM | 1.96111 | 1061.22 | 78.38 |
| 8/13/2013 12:57:41 PM | 1.96139 | 1061.22 | 78.38 |
| 8/13/2013 12:57:42 PM | 1.96167 | 1061.23 | 78.38 |
| 8/13/2013 12:57:43 PM | 1.96194 | 1061.23 | 78.38 |
| 8/13/2013 12:57:44 PM | 1.96222 | 1061.23 | 78.38 |
| 8/13/2013 12:57:45 PM | 1.96250 | 1061.23 | 78.38 |
| 8/13/2013 12:57:46 PM | 1.96278 | 1061.24 | 78.38 |
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| 8/13/2013 12:57:50 PM | 1.96389 | 1061.24 | 78.38 |
| 8/13/2013 12:57:51 PM | 1.96417 | 1061.25 | 78.38 |
| 8/13/2013 12:57:52 PM | 1.96444 | 1061.25 | 78.38 |
| 8/13/2013 12:57:53 PM | 1.96472 | 1061.25 | 78.38 |
| 8/13/2013 12:57:54 PM | 1.96500 | 1061.26 | 78.38 |
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| 8/13/2013 12:57:58 PM | 1.96611 | 1061.27 | 78.38 |
| 8/13/2013 12:57:59 PM | 1.96639 | 1061.27 | 78.38 |
| 8/13/2013 12:58:00 PM | 1.96667 | 1061.27 | 78.38 |
| 8/13/2013 12:58:01 PM | 1.96694 | 1061.27 | 78.38 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
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| 8/13/2013 12:58:05 PM | 1.96806 | 1061.28 | 78.37 |
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| 8/13/2013 12:58:07 PM | 1.96861 | 1061.28 | 78.37 |
| 8/13/2013 12:58:08 PM | 1.96889 | 1061.28 | 78.37 |
| 8/13/2013 12:58:09 PM | 1.96917 | 1061.28 | 78.37 |
| 8/13/2013 12:58:10 PM | 1.96944 | 1061.28 | 78.37 |
| 8/13/2013 12:58:11 PM | 1.96972 | 1061.29 | 78.37 |
| 8/13/2013 12:58:12 PM | 1.97000 | 1061.29 | 78.37 |
| 8/13/2013 12:58:13 PM | 1.97028 | 1061.29 | 78.37 |
| 8/13/2013 12:58:14 PM | 1.97056 | 1061.29 | 78.37 |
| 8/13/2013 12:58:15 PM | 1.97083 | 1061.29 | 78.37 |
| 8/13/2013 12:58:16 PM | 1.97111 | 1061.30 | 78.37 |
| 8/13/2013 12:58:17 PM | 1.97139 | 1061.30 | 78.37 |
| 8/13/2013 12:58:18 PM | 1.97167 | 1061.30 | 78.37 |
| 8/13/2013 12:58:19 PM | 1.97194 | 1061.30 | 78.37 |
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| 8/13/2013 12:58:24 PM | 1.97333 | 1061.30 | 78.37 |
| 8/13/2013 12:58:25 PM | 1.97361 | 1061.30 | 78.37 |
| 8/13/2013 12:58:26 PM | 1.97389 | 1061.30 | 78.37 |
| 8/13/2013 12:58:27 PM | 1.97417 | 1061.31 | 78.37 |
| 8/13/2013 12:58:28 PM | 1.97444 | 1061.31 | 78.37 |
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| 8/13/2013 12:58:30 PM | 1.97500 | 1061.32 | 78.37 |
| 8/13/2013 12:58:31 PM | 1.97528 | 1061.32 | 78.37 |
| 8/13/2013 12:58:32 PM | 1.97556 | 1061.33 | 78.37 |
| 8/13/2013 12:58:33 PM | 1.97583 | 1061.33 | 78.37 |
| 8/13/2013 12:58:34 PM | 1.97611 | 1061.34 | 78.37 |
| 8/13/2013 12:58:35 PM | 1.97639 | 1061.34 | 78.37 |
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| 8/13/2013 12:58:53 PM | 1.98139 | 1061.39 | 78.36 |
| 8/13/2013 12:58:54 PM | 1.98167 | 1061.39 | 78.36 |
| 8/13/2013 12:58:55 PM | 1.98194 | 1061.39 | 78.36 |
| 8/13/2013 12:58:56 PM | 1.98222 | 1061.40 | 78.36 |
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| 8/13/2013 12:58:58 PM | 1.98278 | 1061.40 | 78.36 |
| 8/13/2013 12:58:59 PM | 1.98306 | 1061.40 | 78.36 |
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| 8/13/2013 12:59:03 PM | 1.98417 | 1061.41 | 78.36 |
| 8/13/2013 12:59:04 PM | 1.98444 | 1061.41 | 78.36 |
| 8/13/2013 12:59:05 PM | 1.98472 | 1061.41 | 78.36 |
| 8/13/2013 12:59:06 PM | 1.98500 | 1061.41 | 78.36 |
| 8/13/2013 12:59:07 PM | 1.98528 | 1061.42 | 78.36 |
| 8/13/2013 12:59:08 PM | 1.98556 | 1061.42 | 78.36 |
| 8/13/2013 12:59:09 PM | 1.98583 | 1061.42 | 78.36 |
| 8/13/2013 12:59:10 PM | 1.98611 | 1061.42 | 78.36 |
| 8/13/2013 12:59:11 PM | 1.98639 | 1061.43 | 78.36 |
| 8/13/2013 12:59:12 PM | 1.98667 | 1061.43 | 78.36 |
| 8/13/2013 12:59:13 PM | 1.98694 | 1061.43 | 78.36 |
| 8/13/2013 12:59:14 PM | 1.98722 | 1061.43 | 78.36 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 12:59:15 PM | 1.98750 | 1061.43 | 78.36 |
| 8/13/2013 12:59:16 PM | 1.98778 | 1061.43 | 78.36 |
| 8/13/2013 12:59:17 PM | 1.98806 | 1061.44 | 78.36 |
| 8/13/2013 12:59:18 PM | 1.98833 | 1061.44 | 78.36 |
| 8/13/2013 12:59:19 PM | 1.98861 | 1061.44 | 78.36 |
| 8/13/2013 12:59:20 PM | 1.98889 | 1061.44 | 78.36 |
| 8/13/2013 12:59:21 PM | 1.98917 | 1061.45 | 78.36 |
| 8/13/2013 12:59:22 PM | 1.98944 | 1061.45 | 78.36 |
| 8/13/2013 12:59:23 PM | 1.98972 | 1061.45 | 78.36 |
| 8/13/2013 12:59:24 PM | 1.99000 | 1061.45 | 78.36 |
| 8/13/2013 12:59:25 PM | 1.99028 | 1061.45 | 78.36 |
| 8/13/2013 12:59:26 PM | 1.99056 | 1061.46 | 78.36 |
| 8/13/2013 12:59:27 PM | 1.99083 | 1061.46 | 78.36 |
| 8/13/2013 12:59:28 PM | 1.99111 | 1061.46 | 78.36 |
| 8/13/2013 12:59:29 PM | 1.99139 | 1061.46 | 78.36 |
| 8/13/2013 12:59:30 PM | 1.99167 | 1061.47 | 78.36 |
| 8/13/2013 12:59:31 PM | 1.99194 | 1061.47 | 78.36 |
| 8/13/2013 12:59:32 PM | 1.99222 | 1061.47 | 78.36 |
| 8/13/2013 12:59:33 PM | 1.99250 | 1061.47 | 78.36 |
| 8/13/2013 12:59:34 PM | 1.99278 | 1061.48 | 78.36 |
| 8/13/2013 12:59:35 PM | 1.99306 | 1061.48 | 78.36 |
| 8/13/2013 12:59:36 PM | 1.99333 | 1061.48 | 78.36 |
| 8/13/2013 12:59:37 PM | 1.99361 | 1061.48 | 78.36 |
| 8/13/2013 12:59:38 PM | 1.99389 | 1061.49 | 78.36 |
| 8/13/2013 12:59:39 PM | 1.99417 | 1061.49 | 78.36 |
| 8/13/2013 12:59:40 PM | 1.99444 | 1061.49 | 78.36 |
| 8/13/2013 12:59:41 PM | 1.99472 | 1061.49 | 78.36 |
| 8/13/2013 12:59:42 PM | 1.99500 | 1061.50 | 78.35 |
| 8/13/2013 12:59:43 PM | 1.99528 | 1061.50 | 78.35 |
| 8/13/2013 12:59:44 PM | 1.99556 | 1061.50 | 78.35 |
| 8/13/2013 12:59:45 PM | 1.99583 | 1061.50 | 78.35 |
| 8/13/2013 12:59:46 PM | 1.99611 | 1061.50 | 78.35 |
| 8/13/2013 12:59:47 PM | 1.99639 | 1061.51 | 78.35 |
| 8/13/2013 12:59:48 PM | 1.99667 | 1061.51 | 78.35 |
| 8/13/2013 12:59:49 PM | 1.99694 | 1061.51 | 78.35 |
| 8/13/2013 12:59:50 PM | 1.99722 | 1061.51 | 78.35 |
| 8/13/2013 12:59:51 PM | 1.99750 | 1061.51 | 78.35 |
| 8/13/2013 12:59:52 PM | 1.99778 | 1061.51 | 78.35 |
| 8/13/2013 12:59:53 PM | 1.99806 | 1061.52 | 78.35 |
| 8/13/2013 12:59:54 PM | 1.99833 | 1061.52 | 78.35 |
| 8/13/2013 12:59:55 PM | 1.99861 | 1061.52 | 78.35 |
| 8/13/2013 12:59:56 PM | 1.99889 | 1061.52 | 78.35 |
| 8/13/2013 12:59:57 PM | 1.99917 | 1061.52 | 78.35 |
| 8/13/2013 12:59:58 PM | 1.99944 | 1061.53 | 78.35 |
| 8/13/2013 12:59:59 PM | 1.99972 | 1061.53 | 78.35 |
| 8/13/2013 1:00:00 PM | 2.00000 | 1061.53 | 78.35 |
| 8/13/2013 1:00:01 PM | 2.00028 | 1061.53 | 78.35 |
| 8/13/2013 1:00:02 PM | 2.00056 | 1061.53 | 78.35 |
| 8/13/2013 1:00:03 PM | 2.00083 | 1061.54 | 78.35 |
| 8/13/2013 1:00:04 PM | 2.00111 | 1061.54 | 78.35 |
| 8/13/2013 1:00:05 PM | 2.00139 | 1061.54 | 78.35 |
| 8/13/2013 1:00:06 PM | 2.00167 | 1061.54 | 78.35 |
| 8/13/2013 1:00:07 PM | 2.00194 | 1061.54 | 78.35 |
| 8/13/2013 1:00:08 PM | 2.00222 | 1061.54 | 78.35 |
| 8/13/2013 1:00:09 PM | 2.00250 | 1061.54 | 78.35 |
| 8/13/2013 1:00:10 PM | 2.00278 | 1061.55 | 78.35 |
| 8/13/2013 1:00:11 PM | 2.00306 | 1061.55 | 78.35 |
| 8/13/2013 1:00:12 PM | 2.00333 | 1061.55 | 78.35 |
| 8/13/2013 1:00:13 PM | 2.00361 | 1061.55 | 78.35 |
| 8/13/2013 1:00:14 PM | 2.00389 | 1061.56 | 78.35 |
| 8/13/2013 1:00:15 PM | 2.00417 | 1061.56 | 78.35 |
| 8/13/2013 1:00:16 PM | 2.00444 | 1061.56 | 78.35 |
| 8/13/2013 1:00:17 PM | 2.00472 | 1061.56 | 78.35 |
| 8/13/2013 1:00:18 PM | 2.00500 | 1061.57 | 78.35 |
| 8/13/2013 1:00:19 PM | 2.00528 | 1061.57 | 78.35 |
| 8/13/2013 1:00:20 PM | 2.00556 | 1061.57 | 78.35 |
| 8/13/2013 1:00:21 PM | 2.00583 | 1061.58 | 78.35 |
| 8/13/2013 1:00:22 PM | 2.00611 | 1061.58 | 78.35 |
| 8/13/2013 1:00:23 PM | 2.00639 | 1061.58 | 78.35 |
| 8/13/2013 1:00:24 PM | 2.00667 | 1061.58 | 78.35 |
| 8/13/2013 1:00:25 PM | 2.00694 | 1061.59 | 78.35 |
| 8/13/2013 1:00:26 PM | 2.00722 | 1061.59 | 78.35 |
| 8/13/2013 1:00:27 PM | 2.00750 | 1061.59 | 78.35 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:00:28 PM | 2.00778 | 1061.59 | 78.35 |
| 8/13/2013 1:00:29 PM | 2.00806 | 1061.59 | 78.35 |
| 8/13/2013 1:00:30 PM | 2.00833 | 1061.59 | 78.35 |
| 8/13/2013 1:00:31 PM | 2.00861 | 1061.59 | 78.35 |
| 8/13/2013 1:00:32 PM | 2.00889 | 1061.59 | 78.35 |
| 8/13/2013 1:00:33 PM | 2.00917 | 1061.60 | 78.35 |
| 8/13/2013 1:00:34 PM | 2.00944 | 1061.60 | 78.35 |
| 8/13/2013 1:00:35 PM | 2.00972 | 1061.60 | 78.34 |
| 8/13/2013 1:00:36 PM | 2.01000 | 1061.60 | 78.34 |
| 8/13/2013 1:00:37 PM | 2.01028 | 1061.60 | 78.34 |
| 8/13/2013 1:00:38 PM | 2.01056 | 1061.61 | 78.34 |
| 8/13/2013 1:00:39 PM | 2.01083 | 1061.61 | 78.34 |
| 8/13/2013 1:00:40 PM | 2.01111 | 1061.61 | 78.34 |
| 8/13/2013 1:00:41 PM | 2.01139 | 1061.61 | 78.34 |
| 8/13/2013 1:00:42 PM | 2.01167 | 1061.62 | 78.34 |
| 8/13/2013 1:00:43 PM | 2.01194 | 1061.62 | 78.34 |
| 8/13/2013 1:00:44 PM | 2.01222 | 1061.62 | 78.34 |
| 8/13/2013 1:00:45 PM | 2.01250 | 1061.62 | 78.34 |
| 8/13/2013 1:00:46 PM | 2.01278 | 1061.63 | 78.34 |
| 8/13/2013 1:00:47 PM | 2.01306 | 1061.63 | 78.34 |
| 8/13/2013 1:00:48 PM | 2.01333 | 1061.63 | 78.34 |
| 8/13/2013 1:00:49 PM | 2.01361 | 1061.63 | 78.34 |
| 8/13/2013 1:00:50 PM | 2.01389 | 1061.63 | 78.34 |
| 8/13/2013 1:00:51 PM | 2.01417 | 1061.63 | 78.34 |
| 8/13/2013 1:00:52 PM | 2.01444 | 1061.64 | 78.34 |
| 8/13/2013 1:00:53 PM | 2.01472 | 1061.64 | 78.34 |
| 8/13/2013 1:00:54 PM | 2.01500 | 1061.64 | 78.34 |
| 8/13/2013 1:00:55 PM | 2.01528 | 1061.64 | 78.34 |
| 8/13/2013 1:00:56 PM | 2.01556 | 1061.64 | 78.34 |
| 8/13/2013 1:00:57 PM | 2.01583 | 1061.64 | 78.34 |
| 8/13/2013 1:00:58 PM | 2.01611 | 1061.65 | 78.34 |
| 8/13/2013 1:00:59 PM | 2.01639 | 1061.65 | 78.34 |
| 8/13/2013 1:01:00 PM | 2.01667 | 1061.65 | 78.34 |
| 8/13/2013 1:01:01 PM | 2.01694 | 1061.65 | 78.34 |
| 8/13/2013 1:01:02 PM | 2.01722 | 1061.65 | 78.34 |
| 8/13/2013 1:01:03 PM | 2.01750 | 1061.65 | 78.34 |
| 8/13/2013 1:01:04 PM | 2.01778 | 1061.65 | 78.34 |
| 8/13/2013 1:01:05 PM | 2.01806 | 1061.66 | 78.34 |
| 8/13/2013 1:01:06 PM | 2.01833 | 1061.66 | 78.34 |
| 8/13/2013 1:01:07 PM | 2.01861 | 1061.66 | 78.34 |
| 8/13/2013 1:01:08 PM | 2.01889 | 1061.67 | 78.34 |
| 8/13/2013 1:01:09 PM | 2.01917 | 1061.67 | 78.34 |
| 8/13/2013 1:01:10 PM | 2.01944 | 1061.67 | 78.34 |
| 8/13/2013 1:01:11 PM | 2.01972 | 1061.68 | 78.34 |
| 8/13/2013 1:01:12 PM | 2.02000 | 1061.68 | 78.34 |
| 8/13/2013 1:01:13 PM | 2.02028 | 1061.68 | 78.34 |
| 8/13/2013 1:01:14 PM | 2.02056 | 1061.68 | 78.34 |
| 8/13/2013 1:01:15 PM | 2.02083 | 1061.68 | 78.34 |
| 8/13/2013 1:01:16 PM | 2.02111 | 1061.68 | 78.34 |
| 8/13/2013 1:01:17 PM | 2.02139 | 1061.68 | 78.34 |
| 8/13/2013 1:01:18 PM | 2.02167 | 1061.69 | 78.34 |
| 8/13/2013 1:01:19 PM | 2.02194 | 1061.69 | 78.34 |
| 8/13/2013 1:01:20 PM | 2.02222 | 1061.69 | 78.34 |
| 8/13/2013 1:01:21 PM | 2.02250 | 1061.69 | 78.34 |
| 8/13/2013 1:01:22 PM | 2.02278 | 1061.70 | 78.34 |
| 8/13/2013 1:01:23 PM | 2.02306 | 1061.70 | 78.34 |
| 8/13/2013 1:01:24 PM | 2.02333 | 1061.70 | 78.34 |
| 8/13/2013 1:01:25 PM | 2.02361 | 1061.70 | 78.34 |
| 8/13/2013 1:01:26 PM | 2.02389 | 1061.70 | 78.34 |
| 8/13/2013 1:01:27 PM | 2.02417 | 1061.70 | 78.33 |
| 8/13/2013 1:01:28 PM | 2.02444 | 1061.71 | 78.33 |
| 8/13/2013 1:01:29 PM | 2.02472 | 1061.71 | 78.33 |
| 8/13/2013 1:01:30 PM | 2.02500 | 1061.71 | 78.33 |
| 8/13/2013 1:01:31 PM | 2.02528 | 1061.71 | 78.33 |
| 8/13/2013 1:01:32 PM | 2.02556 | 1061.71 | 78.33 |
| 8/13/2013 1:01:33 PM | 2.02583 | 1061.71 | 78.33 |
| 8/13/2013 1:01:34 PM | 2.02611 | 1061.72 | 78.33 |
| 8/13/2013 1:01:35 PM | 2.02639 | 1061.72 | 78.33 |
| 8/13/2013 1:01:36 PM | 2.02667 | 1061.72 | 78.33 |
| 8/13/2013 1:01:37 PM | 2.02694 | 1061.72 | 78.33 |
| 8/13/2013 1:01:38 PM | 2.02722 | 1061.72 | 78.33 |
| 8/13/2013 1:01:39 PM | 2.02750 | 1061.72 | 78.33 |
| 8/13/2013 1:01:40 PM | 2.02778 | 1061.72 | 78.33 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:01:41 PM | 2.02806 | 1061.73 | 78.33 |
| 8/13/2013 1:01:42 PM | 2.02833 | 1061.73 | 78.33 |
| 8/13/2013 1:01:43 PM | 2.02861 | 1061.73 | 78.33 |
| 8/13/2013 1:01:44 PM | 2.02889 | 1061.73 | 78.33 |
| 8/13/2013 1:01:45 PM | 2.02917 | 1061.73 | 78.33 |
| 8/13/2013 1:01:46 PM | 2.02944 | 1061.74 | 78.33 |
| 8/13/2013 1:01:47 PM | 2.02972 | 1061.74 | 78.33 |
| 8/13/2013 1:01:48 PM | 2.03000 | 1061.74 | 78.33 |
| 8/13/2013 1:01:49 PM | 2.03028 | 1061.74 | 78.33 |
| 8/13/2013 1:01:50 PM | 2.03056 | 1061.75 | 78.33 |
| 8/13/2013 1:01:51 PM | 2.03083 | 1061.75 | 78.33 |
| 8/13/2013 1:01:52 PM | 2.03111 | 1061.75 | 78.33 |
| 8/13/2013 1:01:53 PM | 2.03139 | 1061.75 | 78.33 |
| 8/13/2013 1:01:54 PM | 2.03167 | 1061.76 | 78.33 |
| 8/13/2013 1:01:55 PM | 2.03194 | 1061.76 | 78.33 |
| 8/13/2013 1:01:56 PM | 2.03222 | 1061.76 | 78.33 |
| 8/13/2013 1:01:57 PM | 2.03250 | 1061.76 | 78.33 |
| 8/13/2013 1:01:58 PM | 2.03278 | 1061.76 | 78.33 |
| 8/13/2013 1:01:59 PM | 2.03306 | 1061.77 | 78.33 |
| 8/13/2013 1:02:00 PM | 2.03333 | 1061.77 | 78.33 |
| 8/13/2013 1:02:01 PM | 2.03361 | 1061.77 | 78.33 |
| 8/13/2013 1:02:02 PM | 2.03389 | 1061.78 | 78.33 |
| 8/13/2013 1:02:03 PM | 2.03417 | 1061.78 | 78.33 |
| 8/13/2013 1:02:04 PM | 2.03444 | 1061.78 | 78.33 |
| 8/13/2013 1:02:05 PM | 2.03472 | 1061.78 | 78.33 |
| 8/13/2013 1:02:06 PM | 2.03500 | 1061.79 | 78.33 |
| 8/13/2013 1:02:07 PM | 2.03528 | 1061.79 | 78.33 |
| 8/13/2013 1:02:08 PM | 2.03556 | 1061.79 | 78.33 |
| 8/13/2013 1:02:09 PM | 2.03583 | 1061.79 | 78.33 |
| 8/13/2013 1:02:10 PM | 2.03611 | 1061.79 | 78.33 |
| 8/13/2013 1:02:11 PM | 2.03639 | 1061.79 | 78.33 |
| 8/13/2013 1:02:12 PM | 2.03667 | 1061.79 | 78.33 |
| 8/13/2013 1:02:13 PM | 2.03694 | 1061.79 | 78.33 |
| 8/13/2013 1:02:14 PM | 2.03722 | 1061.80 | 78.33 |
| 8/13/2013 1:02:15 PM | 2.03750 | 1061.80 | 78.33 |
| 8/13/2013 1:02:16 PM | 2.03778 | 1061.80 | 78.33 |
| 8/13/2013 1:02:17 PM | 2.03806 | 1061.80 | 78.33 |
| 8/13/2013 1:02:18 PM | 2.03833 | 1061.81 | 78.33 |
| 8/13/2013 1:02:19 PM | 2.03861 | 1061.81 | 78.33 |
| 8/13/2013 1:02:20 PM | 2.03889 | 1061.81 | 78.33 |
| 8/13/2013 1:02:21 PM | 2.03917 | 1061.81 | 78.33 |
| 8/13/2013 1:02:22 PM | 2.03944 | 1061.82 | 78.33 |
| 8/13/2013 1:02:23 PM | 2.03972 | 1061.82 | 78.33 |
| 8/13/2013 1:02:24 PM | 2.04000 | 1061.82 | 78.33 |
| 8/13/2013 1:02:25 PM | 2.04028 | 1061.82 | 78.33 |
| 8/13/2013 1:02:26 PM | 2.04056 | 1061.82 | 78.33 |
| 8/13/2013 1:02:27 PM | 2.04083 | 1061.82 | 78.33 |
| 8/13/2013 1:02:28 PM | 2.04111 | 1061.83 | 78.33 |
| 8/13/2013 1:02:29 PM | 2.04139 | 1061.83 | 78.33 |
| 8/13/2013 1:02:30 PM | 2.04167 | 1061.83 | 78.33 |
| 8/13/2013 1:02:31 PM | 2.04194 | 1061.83 | 78.33 |
| 8/13/2013 1:02:32 PM | 2.04222 | 1061.83 | 78.33 |
| 8/13/2013 1:02:33 PM | 2.04250 | 1061.84 | 78.33 |
| 8/13/2013 1:02:34 PM | 2.04278 | 1061.84 | 78.33 |
| 8/13/2013 1:02:35 PM | 2.04306 | 1061.84 | 78.33 |
| 8/13/2013 1:02:36 PM | 2.04333 | 1061.84 | 78.33 |
| 8/13/2013 1:02:37 PM | 2.04361 | 1061.85 | 78.33 |
| 8/13/2013 1:02:38 PM | 2.04389 | 1061.85 | 78.33 |
| 8/13/2013 1:02:39 PM | 2.04417 | 1061.85 | 78.32 |
| 8/13/2013 1:02:40 PM | 2.04444 | 1061.86 | 78.32 |
| 8/13/2013 1:02:41 PM | 2.04472 | 1061.86 | 78.32 |
| 8/13/2013 1:02:42 PM | 2.04500 | 1061.86 | 78.32 |
| 8/13/2013 1:02:43 PM | 2.04528 | 1061.86 | 78.32 |
| 8/13/2013 1:02:44 PM | 2.04556 | 1061.86 | 78.32 |
| 8/13/2013 1:02:45 PM | 2.04583 | 1061.87 | 78.32 |
| 8/13/2013 1:02:46 PM | 2.04611 | 1061.87 | 78.32 |
| 8/13/2013 1:02:47 PM | 2.04639 | 1061.87 | 78.32 |
| 8/13/2013 1:02:48 PM | 2.04667 | 1061.87 | 78.32 |
| 8/13/2013 1:02:49 PM | 2.04694 | 1061.87 | 78.32 |
| 8/13/2013 1:02:50 PM | 2.04722 | 1061.88 | 78.32 |
| 8/13/2013 1:02:51 PM | 2.04750 | 1061.88 | 78.32 |
| 8/13/2013 1:02:52 PM | 2.04778 | 1061.88 | 78.32 |
| 8/13/2013 1:02:53 PM | 2.04806 | 1061.88 | 78.32 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:02:54 PM | 2.04833 | 1061.88 | 78.32 |
| 8/13/2013 1:02:55 PM | 2.04861 | 1061.88 | 78.32 |
| 8/13/2013 1:02:56 PM | 2.04889 | 1061.88 | 78.32 |
| 8/13/2013 1:02:57 PM | 2.04917 | 1061.88 | 78.32 |
| 8/13/2013 1:02:58 PM | 2.04944 | 1061.89 | 78.32 |
| 8/13/2013 1:02:59 PM | 2.04972 | 1061.89 | 78.32 |
| 8/13/2013 1:03:00 PM | 2.05000 | 1061.89 | 78.32 |
| 8/13/2013 1:03:01 PM | 2.05028 | 1061.89 | 78.32 |
| 8/13/2013 1:03:02 PM | 2.05056 | 1061.89 | 78.32 |
| 8/13/2013 1:03:03 PM | 2.05083 | 1061.90 | 78.32 |
| 8/13/2013 1:03:04 PM | 2.05111 | 1061.90 | 78.32 |
| 8/13/2013 1:03:05 PM | 2.05139 | 1061.90 | 78.32 |
| 8/13/2013 1:03:06 PM | 2.05167 | 1061.91 | 78.32 |
| 8/13/2013 1:03:07 PM | 2.05194 | 1061.91 | 78.32 |
| 8/13/2013 1:03:08 PM | 2.05222 | 1061.91 | 78.32 |
| 8/13/2013 1:03:09 PM | 2.05250 | 1061.91 | 78.32 |
| 8/13/2013 1:03:10 PM | 2.05278 | 1061.92 | 78.32 |
| 8/13/2013 1:03:11 PM | 2.05306 | 1061.92 | 78.32 |
| 8/13/2013 1:03:12 PM | 2.05333 | 1061.92 | 78.32 |
| 8/13/2013 1:03:13 PM | 2.05361 | 1061.93 | 78.32 |
| 8/13/2013 1:03:14 PM | 2.05389 | 1061.93 | 78.32 |
| 8/13/2013 1:03:15 PM | 2.05417 | 1061.93 | 78.32 |
| 8/13/2013 1:03:16 PM | 2.05444 | 1061.93 | 78.32 |
| 8/13/2013 1:03:17 PM | 2.05472 | 1061.94 | 78.32 |
| 8/13/2013 1:03:18 PM | 2.05500 | 1061.94 | 78.32 |
| 8/13/2013 1:03:19 PM | 2.05528 | 1061.94 | 78.32 |
| 8/13/2013 1:03:20 PM | 2.05556 | 1061.94 | 78.32 |
| 8/13/2013 1:03:21 PM | 2.05583 | 1061.94 | 78.32 |
| 8/13/2013 1:03:22 PM | 2.05611 | 1061.94 | 78.32 |
| 8/13/2013 1:03:23 PM | 2.05639 | 1061.95 | 78.32 |
| 8/13/2013 1:03:24 PM | 2.05667 | 1061.95 | 78.31 |
| 8/13/2013 1:03:25 PM | 2.05694 | 1061.95 | 78.31 |
| 8/13/2013 1:03:26 PM | 2.05722 | 1061.95 | 78.31 |
| 8/13/2013 1:03:27 PM | 2.05750 | 1061.96 | 78.31 |
| 8/13/2013 1:03:28 PM | 2.05778 | 1061.96 | 78.31 |
| 8/13/2013 1:03:29 PM | 2.05806 | 1061.96 | 78.31 |
| 8/13/2013 1:03:30 PM | 2.05833 | 1061.97 | 78.31 |
| 8/13/2013 1:03:31 PM | 2.05861 | 1061.97 | 78.31 |
| 8/13/2013 1:03:32 PM | 2.05889 | 1061.97 | 78.31 |
| 8/13/2013 1:03:33 PM | 2.05917 | 1061.98 | 78.31 |
| 8/13/2013 1:03:34 PM | 2.05944 | 1061.98 | 78.31 |
| 8/13/2013 1:03:35 PM | 2.05972 | 1061.98 | 78.31 |
| 8/13/2013 1:03:36 PM | 2.06000 | 1061.99 | 78.31 |
| 8/13/2013 1:03:37 PM | 2.06028 | 1061.99 | 78.31 |
| 8/13/2013 1:03:38 PM | 2.06056 | 1061.99 | 78.31 |
| 8/13/2013 1:03:39 PM | 2.06083 | 1062.00 | 78.31 |
| 8/13/2013 1:03:40 PM | 2.06111 | 1062.00 | 78.31 |
| 8/13/2013 1:03:41 PM | 2.06139 | 1062.00 | 78.31 |
| 8/13/2013 1:03:42 PM | 2.06167 | 1062.00 | 78.31 |
| 8/13/2013 1:03:43 PM | 2.06194 | 1062.01 | 78.31 |
| 8/13/2013 1:03:44 PM | 2.06222 | 1062.01 | 78.31 |
| 8/13/2013 1:03:45 PM | 2.06250 | 1062.01 | 78.31 |
| 8/13/2013 1:03:46 PM | 2.06278 | 1062.01 | 78.31 |
| 8/13/2013 1:03:47 PM | 2.06306 | 1062.01 | 78.31 |
| 8/13/2013 1:03:48 PM | 2.06333 | 1062.02 | 78.31 |
| 8/13/2013 1:03:49 PM | 2.06361 | 1062.02 | 78.31 |
| 8/13/2013 1:03:50 PM | 2.06389 | 1062.02 | 78.31 |
| 8/13/2013 1:03:51 PM | 2.06417 | 1062.02 | 78.31 |
| 8/13/2013 1:03:52 PM | 2.06444 | 1062.02 | 78.31 |
| 8/13/2013 1:03:53 PM | 2.06472 | 1062.02 | 78.31 |
| 8/13/2013 1:03:54 PM | 2.06500 | 1062.03 | 78.31 |
| 8/13/2013 1:03:55 PM | 2.06528 | 1062.03 | 78.31 |
| 8/13/2013 1:03:56 PM | 2.06556 | 1062.03 | 78.31 |
| 8/13/2013 1:03:57 PM | 2.06583 | 1062.03 | 78.31 |
| 8/13/2013 1:03:58 PM | 2.06611 | 1062.04 | 78.31 |
| 8/13/2013 1:03:59 PM | 2.06639 | 1062.04 | 78.31 |
| 8/13/2013 1:04:00 PM | 2.06667 | 1062.04 | 78.31 |
| 8/13/2013 1:04:01 PM | 2.06694 | 1062.05 | 78.31 |
| 8/13/2013 1:04:02 PM | 2.06722 | 1062.05 | 78.31 |
| 8/13/2013 1:04:03 PM | 2.06750 | 1062.05 | 78.31 |
| 8/13/2013 1:04:04 PM | 2.06778 | 1062.05 | 78.31 |
| 8/13/2013 1:04:05 PM | 2.06806 | 1062.06 | 78.31 |
| 8/13/2013 1:04:06 PM | 2.06833 | 1062.06 | 78.31 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:04:07 PM | 2.06861 | 1062.06 | 78.31 |
| 8/13/2013 1:04:08 PM | 2.06889 | 1062.06 | 78.31 |
| 8/13/2013 1:04:09 PM | 2.06917 | 1062.06 | 78.31 |
| 8/13/2013 1:04:10 PM | 2.06944 | 1062.06 | 78.31 |
| 8/13/2013 1:04:11 PM | 2.06972 | 1062.06 | 78.31 |
| 8/13/2013 1:04:12 PM | 2.07000 | 1062.06 | 78.31 |
| 8/13/2013 1:04:13 PM | 2.07028 | 1062.06 | 78.31 |
| 8/13/2013 1:04:14 PM | 2.07056 | 1062.06 | 78.31 |
| 8/13/2013 1:04:15 PM | 2.07083 | 1062.06 | 78.31 |
| 8/13/2013 1:04:16 PM | 2.07111 | 1062.06 | 78.31 |
| 8/13/2013 1:04:17 PM | 2.07139 | 1062.07 | 78.31 |
| 8/13/2013 1:04:18 PM | 2.07167 | 1062.07 | 78.31 |
| 8/13/2013 1:04:19 PM | 2.07194 | 1062.07 | 78.31 |
| 8/13/2013 1:04:20 PM | 2.07222 | 1062.07 | 78.31 |
| 8/13/2013 1:04:21 PM | 2.07250 | 1062.08 | 78.31 |
| 8/13/2013 1:04:22 PM | 2.07278 | 1062.08 | 78.31 |
| 8/13/2013 1:04:23 PM | 2.07306 | 1062.08 | 78.31 |
| 8/13/2013 1:04:24 PM | 2.07333 | 1062.09 | 78.31 |
| 8/13/2013 1:04:25 PM | 2.07361 | 1062.09 | 78.31 |
| 8/13/2013 1:04:26 PM | 2.07389 | 1062.09 | 78.31 |
| 8/13/2013 1:04:27 PM | 2.07417 | 1062.09 | 78.31 |
| 8/13/2013 1:04:28 PM | 2.07444 | 1062.09 | 78.31 |
| 8/13/2013 1:04:29 PM | 2.07472 | 1062.10 | 78.31 |
| 8/13/2013 1:04:30 PM | 2.07500 | 1062.10 | 78.31 |
| 8/13/2013 1:04:31 PM | 2.07528 | 1062.10 | 78.31 |
| 8/13/2013 1:04:32 PM | 2.07556 | 1062.10 | 78.31 |
| 8/13/2013 1:04:33 PM | 2.07583 | 1062.11 | 78.31 |
| 8/13/2013 1:04:34 PM | 2.07611 | 1062.11 | 78.31 |
| 8/13/2013 1:04:35 PM | 2.07639 | 1062.12 | 78.31 |
| 8/13/2013 1:04:36 PM | 2.07667 | 1062.12 | 78.31 |
| 8/13/2013 1:04:37 PM | 2.07694 | 1062.12 | 78.31 |
| 8/13/2013 1:04:38 PM | 2.07722 | 1062.12 | 78.31 |
| 8/13/2013 1:04:39 PM | 2.07750 | 1062.12 | 78.31 |
| 8/13/2013 1:04:40 PM | 2.07778 | 1062.12 | 78.30 |
| 8/13/2013 1:04:41 PM | 2.07806 | 1062.13 | 78.30 |
| 8/13/2013 1:04:42 PM | 2.07833 | 1062.13 | 78.30 |
| 8/13/2013 1:04:43 PM | 2.07861 | 1062.13 | 78.30 |
| 8/13/2013 1:04:44 PM | 2.07889 | 1062.13 | 78.30 |
| 8/13/2013 1:04:45 PM | 2.07917 | 1062.13 | 78.30 |
| 8/13/2013 1:04:46 PM | 2.07944 | 1062.13 | 78.30 |
| 8/13/2013 1:04:47 PM | 2.07972 | 1062.13 | 78.30 |
| 8/13/2013 1:04:48 PM | 2.08000 | 1062.13 | 78.30 |
| 8/13/2013 1:04:49 PM | 2.08028 | 1062.13 | 78.30 |
| 8/13/2013 1:04:50 PM | 2.08056 | 1062.13 | 78.30 |
| 8/13/2013 1:04:51 PM | 2.08083 | 1062.14 | 78.30 |
| 8/13/2013 1:04:52 PM | 2.08111 | 1062.14 | 78.30 |
| 8/13/2013 1:04:53 PM | 2.08139 | 1062.14 | 78.30 |
| 8/13/2013 1:04:54 PM | 2.08167 | 1062.14 | 78.30 |
| 8/13/2013 1:04:55 PM | 2.08194 | 1062.15 | 78.30 |
| 8/13/2013 1:04:56 PM | 2.08222 | 1062.15 | 78.30 |
| 8/13/2013 1:04:57 PM | 2.08250 | 1062.15 | 78.30 |
| 8/13/2013 1:04:58 PM | 2.08278 | 1062.15 | 78.30 |
| 8/13/2013 1:04:59 PM | 2.08306 | 1062.15 | 78.30 |
| 8/13/2013 1:05:00 PM | 2.08333 | 1062.16 | 78.30 |
| 8/13/2013 1:05:01 PM | 2.08361 | 1062.16 | 78.30 |
| 8/13/2013 1:05:02 PM | 2.08389 | 1062.16 | 78.30 |
| 8/13/2013 1:05:03 PM | 2.08417 | 1062.16 | 78.30 |
| 8/13/2013 1:05:04 PM | 2.08444 | 1062.16 | 78.30 |
| 8/13/2013 1:05:05 PM | 2.08472 | 1062.16 | 78.30 |
| 8/13/2013 1:05:06 PM | 2.08500 | 1062.17 | 78.30 |
| 8/13/2013 1:05:07 PM | 2.08528 | 1062.17 | 78.30 |
| 8/13/2013 1:05:08 PM | 2.08556 | 1062.17 | 78.30 |
| 8/13/2013 1:05:09 PM | 2.08583 | 1062.17 | 78.30 |
| 8/13/2013 1:05:10 PM | 2.08611 | 1062.17 | 78.30 |
| 8/13/2013 1:05:11 PM | 2.08639 | 1062.18 | 78.30 |
| 8/13/2013 1:05:12 PM | 2.08667 | 1062.18 | 78.30 |
| 8/13/2013 1:05:13 PM | 2.08694 | 1062.18 | 78.30 |
| 8/13/2013 1:05:14 PM | 2.08722 | 1062.18 | 78.30 |
| 8/13/2013 1:05:15 PM | 2.08750 | 1062.19 | 78.30 |
| 8/13/2013 1:05:16 PM | 2.08778 | 1062.19 | 78.30 |
| 8/13/2013 1:05:17 PM | 2.08806 | 1062.19 | 78.30 |
| 8/13/2013 1:05:18 PM | 2.08833 | 1062.19 | 78.30 |
| 8/13/2013 1:05:19 PM | 2.08861 | 1062.19 | 78.30 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:05:20 PM | 2.08889 | 1062.19 | 78.30 |
| 8/13/2013 1:05:21 PM | 2.08917 | 1062.20 | 78.30 |
| 8/13/2013 1:05:22 PM | 2.08944 | 1062.20 | 78.30 |
| 8/13/2013 1:05:23 PM | 2.08972 | 1062.20 | 78.30 |
| 8/13/2013 1:05:24 PM | 2.09000 | 1062.21 | 78.30 |
| 8/13/2013 1:05:25 PM | 2.09028 | 1062.21 | 78.30 |
| 8/13/2013 1:05:26 PM | 2.09056 | 1062.22 | 78.30 |
| 8/13/2013 1:05:27 PM | 2.09083 | 1062.22 | 78.30 |
| 8/13/2013 1:05:28 PM | 2.09111 | 1062.22 | 78.30 |
| 8/13/2013 1:05:29 PM | 2.09139 | 1062.22 | 78.30 |
| 8/13/2013 1:05:30 PM | 2.09167 | 1062.23 | 78.30 |
| 8/13/2013 1:05:31 PM | 2.09194 | 1062.23 | 78.30 |
| 8/13/2013 1:05:32 PM | 2.09222 | 1062.23 | 78.30 |
| 8/13/2013 1:05:33 PM | 2.09250 | 1062.23 | 78.30 |
| 8/13/2013 1:05:34 PM | 2.09278 | 1062.23 | 78.30 |
| 8/13/2013 1:05:35 PM | 2.09306 | 1062.23 | 78.30 |
| 8/13/2013 1:05:36 PM | 2.09333 | 1062.23 | 78.30 |
| 8/13/2013 1:05:37 PM | 2.09361 | 1062.23 | 78.30 |
| 8/13/2013 1:05:38 PM | 2.09389 | 1062.23 | 78.30 |
| 8/13/2013 1:05:39 PM | 2.09417 | 1062.23 | 78.30 |
| 8/13/2013 1:05:40 PM | 2.09444 | 1062.24 | 78.29 |
| 8/13/2013 1:05:41 PM | 2.09472 | 1062.24 | 78.29 |
| 8/13/2013 1:05:42 PM | 2.09500 | 1062.24 | 78.29 |
| 8/13/2013 1:05:43 PM | 2.09528 | 1062.24 | 78.29 |
| 8/13/2013 1:05:44 PM | 2.09556 | 1062.24 | 78.29 |
| 8/13/2013 1:05:45 PM | 2.09583 | 1062.24 | 78.29 |
| 8/13/2013 1:05:46 PM | 2.09611 | 1062.25 | 78.29 |
| 8/13/2013 1:05:47 PM | 2.09639 | 1062.25 | 78.29 |
| 8/13/2013 1:05:48 PM | 2.09667 | 1062.25 | 78.29 |
| 8/13/2013 1:05:49 PM | 2.09694 | 1062.25 | 78.29 |
| 8/13/2013 1:05:50 PM | 2.09722 | 1062.25 | 78.29 |
| 8/13/2013 1:05:51 PM | 2.09750 | 1062.26 | 78.29 |
| 8/13/2013 1:05:52 PM | 2.09778 | 1062.26 | 78.29 |
| 8/13/2013 1:05:53 PM | 2.09806 | 1062.26 | 78.29 |
| 8/13/2013 1:05:54 PM | 2.09833 | 1062.26 | 78.29 |
| 8/13/2013 1:05:55 PM | 2.09861 | 1062.26 | 78.29 |
| 8/13/2013 1:05:56 PM | 2.09889 | 1062.27 | 78.29 |
| 8/13/2013 1:05:57 PM | 2.09917 | 1062.27 | 78.29 |
| 8/13/2013 1:05:58 PM | 2.09944 | 1062.27 | 78.29 |
| 8/13/2013 1:05:59 PM | 2.09972 | 1062.27 | 78.29 |
| 8/13/2013 1:06:00 PM | 2.10000 | 1062.27 | 78.29 |
| 8/13/2013 1:06:01 PM | 2.10028 | 1062.27 | 78.29 |
| 8/13/2013 1:06:02 PM | 2.10056 | 1062.27 | 78.29 |
| 8/13/2013 1:06:03 PM | 2.10083 | 1062.27 | 78.29 |
| 8/13/2013 1:06:04 PM | 2.10111 | 1062.28 | 78.29 |
| 8/13/2013 1:06:05 PM | 2.10139 | 1062.28 | 78.29 |
| 8/13/2013 1:06:06 PM | 2.10167 | 1062.28 | 78.29 |
| 8/13/2013 1:06:07 PM | 2.10194 | 1062.28 | 78.29 |
| 8/13/2013 1:06:08 PM | 2.10222 | 1062.29 | 78.29 |
| 8/13/2013 1:06:09 PM | 2.10250 | 1062.29 | 78.29 |
| 8/13/2013 1:06:10 PM | 2.10278 | 1062.29 | 78.29 |
| 8/13/2013 1:06:11 PM | 2.10306 | 1062.29 | 78.29 |
| 8/13/2013 1:06:12 PM | 2.10333 | 1062.29 | 78.29 |
| 8/13/2013 1:06:13 PM | 2.10361 | 1062.30 | 78.29 |
| 8/13/2013 1:06:14 PM | 2.10389 | 1062.30 | 78.29 |
| 8/13/2013 1:06:15 PM | 2.10417 | 1062.30 | 78.29 |
| 8/13/2013 1:06:16 PM | 2.10444 | 1062.30 | 78.29 |
| 8/13/2013 1:06:17 PM | 2.10472 | 1062.30 | 78.29 |
| 8/13/2013 1:06:18 PM | 2.10500 | 1062.31 | 78.29 |
| 8/13/2013 1:06:19 PM | 2.10528 | 1062.31 | 78.29 |
| 8/13/2013 1:06:20 PM | 2.10556 | 1062.31 | 78.29 |
| 8/13/2013 1:06:21 PM | 2.10583 | 1062.31 | 78.29 |
| 8/13/2013 1:06:22 PM | 2.10611 | 1062.32 | 78.29 |
| 8/13/2013 1:06:23 PM | 2.10639 | 1062.32 | 78.29 |
| 8/13/2013 1:06:24 PM | 2.10667 | 1062.32 | 78.29 |
| 8/13/2013 1:06:25 PM | 2.10694 | 1062.33 | 78.29 |
| 8/13/2013 1:06:26 PM | 2.10722 | 1062.33 | 78.29 |
| 8/13/2013 1:06:27 PM | 2.10750 | 1062.33 | 78.29 |
| 8/13/2013 1:06:28 PM | 2.10778 | 1062.33 | 78.29 |
| 8/13/2013 1:06:29 PM | 2.10806 | 1062.34 | 78.29 |
| 8/13/2013 1:06:30 PM | 2.10833 | 1062.34 | 78.29 |
| 8/13/2013 1:06:31 PM | 2.10861 | 1062.34 | 78.29 |
| 8/13/2013 1:06:32 PM | 2.10889 | 1062.34 | 78.29 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:06:33 PM | 2.10917 | 1062.34 | 78.29 |
| 8/13/2013 1:06:34 PM | 2.10944 | 1062.35 | 78.29 |
| 8/13/2013 1:06:35 PM | 2.10972 | 1062.35 | 78.29 |
| 8/13/2013 1:06:36 PM | 2.11000 | 1062.35 | 78.29 |
| 8/13/2013 1:06:37 PM | 2.11028 | 1062.36 | 78.29 |
| 8/13/2013 1:06:38 PM | 2.11056 | 1062.36 | 78.29 |
| 8/13/2013 1:06:39 PM | 2.11083 | 1062.36 | 78.29 |
| 8/13/2013 1:06:40 PM | 2.11111 | 1062.36 | 78.29 |
| 8/13/2013 1:06:41 PM | 2.11139 | 1062.37 | 78.29 |
| 8/13/2013 1:06:42 PM | 2.11167 | 1062.37 | 78.29 |
| 8/13/2013 1:06:43 PM | 2.11194 | 1062.37 | 78.29 |
| 8/13/2013 1:06:44 PM | 2.11222 | 1062.37 | 78.29 |
| 8/13/2013 1:06:45 PM | 2.11250 | 1062.37 | 78.29 |
| 8/13/2013 1:06:46 PM | 2.11278 | 1062.37 | 78.29 |
| 8/13/2013 1:06:47 PM | 2.11306 | 1062.37 | 78.29 |
| 8/13/2013 1:06:48 PM | 2.11333 | 1062.38 | 78.29 |
| 8/13/2013 1:06:49 PM | 2.11361 | 1062.38 | 78.29 |
| 8/13/2013 1:06:50 PM | 2.11389 | 1062.38 | 78.29 |
| 8/13/2013 1:06:51 PM | 2.11417 | 1062.38 | 78.28 |
| 8/13/2013 1:06:52 PM | 2.11444 | 1062.38 | 78.28 |
| 8/13/2013 1:06:53 PM | 2.11472 | 1062.39 | 78.28 |
| 8/13/2013 1:06:54 PM | 2.11500 | 1062.39 | 78.28 |
| 8/13/2013 1:06:55 PM | 2.11528 | 1062.39 | 78.28 |
| 8/13/2013 1:06:56 PM | 2.11556 | 1062.39 | 78.28 |
| 8/13/2013 1:06:57 PM | 2.11583 | 1062.39 | 78.28 |
| 8/13/2013 1:06:58 PM | 2.11611 | 1062.40 | 78.28 |
| 8/13/2013 1:06:59 PM | 2.11639 | 1062.40 | 78.28 |
| 8/13/2013 1:07:00 PM | 2.11667 | 1062.40 | 78.28 |
| 8/13/2013 1:07:01 PM | 2.11694 | 1062.40 | 78.28 |
| 8/13/2013 1:07:02 PM | 2.11722 | 1062.40 | 78.28 |
| 8/13/2013 1:07:03 PM | 2.11750 | 1062.40 | 78.28 |
| 8/13/2013 1:07:04 PM | 2.11778 | 1062.40 | 78.28 |
| 8/13/2013 1:07:05 PM | 2.11806 | 1062.41 | 78.28 |
| 8/13/2013 1:07:06 PM | 2.11833 | 1062.41 | 78.28 |
| 8/13/2013 1:07:07 PM | 2.11861 | 1062.41 | 78.28 |
| 8/13/2013 1:07:08 PM | 2.11889 | 1062.41 | 78.28 |
| 8/13/2013 1:07:09 PM | 2.11917 | 1062.42 | 78.28 |
| 8/13/2013 1:07:10 PM | 2.11944 | 1062.42 | 78.28 |
| 8/13/2013 1:07:11 PM | 2.11972 | 1062.42 | 78.28 |
| 8/13/2013 1:07:12 PM | 2.12000 | 1062.42 | 78.28 |
| 8/13/2013 1:07:13 PM | 2.12028 | 1062.43 | 78.28 |
| 8/13/2013 1:07:14 PM | 2.12056 | 1062.43 | 78.28 |
| 8/13/2013 1:07:15 PM | 2.12083 | 1062.43 | 78.28 |
| 8/13/2013 1:07:16 PM | 2.12111 | 1062.44 | 78.28 |
| 8/13/2013 1:07:17 PM | 2.12139 | 1062.44 | 78.28 |
| 8/13/2013 1:07:18 PM | 2.12167 | 1062.44 | 78.28 |
| 8/13/2013 1:07:19 PM | 2.12194 | 1062.44 | 78.28 |
| 8/13/2013 1:07:20 PM | 2.12222 | 1062.45 | 78.28 |
| 8/13/2013 1:07:21 PM | 2.12250 | 1062.45 | 78.28 |
| 8/13/2013 1:07:22 PM | 2.12278 | 1062.45 | 78.28 |
| 8/13/2013 1:07:23 PM | 2.12306 | 1062.45 | 78.28 |
| 8/13/2013 1:07:24 PM | 2.12333 | 1062.45 | 78.28 |
| 8/13/2013 1:07:25 PM | 2.12361 | 1062.46 | 78.28 |
| 8/13/2013 1:07:26 PM | 2.12389 | 1062.46 | 78.28 |
| 8/13/2013 1:07:27 PM | 2.12417 | 1062.46 | 78.28 |
| 8/13/2013 1:07:28 PM | 2.12444 | 1062.46 | 78.28 |
| 8/13/2013 1:07:29 PM | 2.12472 | 1062.46 | 78.28 |
| 8/13/2013 1:07:30 PM | 2.12500 | 1062.47 | 78.28 |
| 8/13/2013 1:07:31 PM | 2.12528 | 1062.47 | 78.28 |
| 8/13/2013 1:07:32 PM | 2.12556 | 1062.47 | 78.28 |
| 8/13/2013 1:07:33 PM | 2.12583 | 1062.48 | 78.28 |
| 8/13/2013 1:07:34 PM | 2.12611 | 1062.48 | 78.28 |
| 8/13/2013 1:07:35 PM | 2.12639 | 1062.48 | 78.28 |
| 8/13/2013 1:07:36 PM | 2.12667 | 1062.48 | 78.28 |
| 8/13/2013 1:07:37 PM | 2.12694 | 1062.49 | 78.28 |
| 8/13/2013 1:07:38 PM | 2.12722 | 1062.49 | 78.28 |
| 8/13/2013 1:07:39 PM | 2.12750 | 1062.49 | 78.28 |
| 8/13/2013 1:07:40 PM | 2.12778 | 1062.49 | 78.28 |
| 8/13/2013 1:07:41 PM | 2.12806 | 1062.50 | 78.28 |
| 8/13/2013 1:07:42 PM | 2.12833 | 1062.50 | 78.28 |
| 8/13/2013 1:07:43 PM | 2.12861 | 1062.50 | 78.28 |
| 8/13/2013 1:07:44 PM | 2.12889 | 1062.50 | 78.28 |
| 8/13/2013 1:07:45 PM | 2.12917 | 1062.50 | 78.28 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:07:46 PM | 2.12944 | 1062.51 | 78.28 |
| 8/13/2013 1:07:47 PM | 2.12972 | 1062.51 | 78.28 |
| 8/13/2013 1:07:48 PM | 2.13000 | 1062.51 | 78.28 |
| 8/13/2013 1:07:49 PM | 2.13028 | 1062.51 | 78.28 |
| 8/13/2013 1:07:50 PM | 2.13056 | 1062.51 | 78.28 |
| 8/13/2013 1:07:51 PM | 2.13083 | 1062.51 | 78.28 |
| 8/13/2013 1:07:52 PM | 2.13111 | 1062.52 | 78.28 |
| 8/13/2013 1:07:53 PM | 2.13139 | 1062.52 | 78.28 |
| 8/13/2013 1:07:54 PM | 2.13167 | 1062.52 | 78.28 |
| 8/13/2013 1:07:55 PM | 2.13194 | 1062.53 | 78.28 |
| 8/13/2013 1:07:56 PM | 2.13222 | 1062.53 | 78.28 |
| 8/13/2013 1:07:57 PM | 2.13250 | 1062.53 | 78.28 |
| 8/13/2013 1:07:58 PM | 2.13278 | 1062.54 | 78.28 |
| 8/13/2013 1:07:59 PM | 2.13306 | 1062.54 | 78.28 |
| 8/13/2013 1:08:00 PM | 2.13333 | 1062.54 | 78.28 |
| 8/13/2013 1:08:01 PM | 2.13361 | 1062.54 | 78.28 |
| 8/13/2013 1:08:02 PM | 2.13389 | 1062.54 | 78.28 |
| 8/13/2013 1:08:03 PM | 2.13417 | 1062.55 | 78.28 |
| 8/13/2013 1:08:04 PM | 2.13444 | 1062.55 | 78.28 |
| 8/13/2013 1:08:05 PM | 2.13472 | 1062.55 | 78.28 |
| 8/13/2013 1:08:06 PM | 2.13500 | 1062.55 | 78.28 |
| 8/13/2013 1:08:07 PM | 2.13528 | 1062.55 | 78.28 |
| 8/13/2013 1:08:08 PM | 2.13556 | 1062.55 | 78.28 |
| 8/13/2013 1:08:09 PM | 2.13583 | 1062.56 | 78.28 |
| 8/13/2013 1:08:10 PM | 2.13611 | 1062.56 | 78.28 |
| 8/13/2013 1:08:11 PM | 2.13639 | 1062.56 | 78.28 |
| 8/13/2013 1:08:12 PM | 2.13667 | 1062.56 | 78.28 |
| 8/13/2013 1:08:13 PM | 2.13694 | 1062.57 | 78.28 |
| 8/13/2013 1:08:14 PM | 2.13722 | 1062.57 | 78.28 |
| 8/13/2013 1:08:15 PM | 2.13750 | 1062.57 | 78.28 |
| 8/13/2013 1:08:16 PM | 2.13778 | 1062.58 | 78.28 |
| 8/13/2013 1:08:17 PM | 2.13806 | 1062.58 | 78.28 |
| 8/13/2013 1:08:18 PM | 2.13833 | 1062.58 | 78.28 |
| 8/13/2013 1:08:19 PM | 2.13861 | 1062.59 | 78.28 |
| 8/13/2013 1:08:20 PM | 2.13889 | 1062.59 | 78.28 |
| 8/13/2013 1:08:21 PM | 2.13917 | 1062.59 | 78.28 |
| 8/13/2013 1:08:22 PM | 2.13944 | 1062.60 | 78.28 |
| 8/13/2013 1:08:23 PM | 2.13972 | 1062.60 | 78.28 |
| 8/13/2013 1:08:24 PM | 2.14000 | 1062.60 | 78.28 |
| 8/13/2013 1:08:25 PM | 2.14028 | 1062.60 | 78.28 |
| 8/13/2013 1:08:26 PM | 2.14056 | 1062.60 | 78.28 |
| 8/13/2013 1:08:27 PM | 2.14083 | 1062.60 | 78.28 |
| 8/13/2013 1:08:28 PM | 2.14111 | 1062.60 | 78.28 |
| 8/13/2013 1:08:29 PM | 2.14139 | 1062.60 | 78.28 |
| 8/13/2013 1:08:30 PM | 2.14167 | 1062.61 | 78.28 |
| 8/13/2013 1:08:31 PM | 2.14194 | 1062.61 | 78.28 |
| 8/13/2013 1:08:32 PM | 2.14222 | 1062.61 | 78.28 |
| 8/13/2013 1:08:33 PM | 2.14250 | 1062.61 | 78.28 |
| 8/13/2013 1:08:34 PM | 2.14278 | 1062.61 | 78.27 |
| 8/13/2013 1:08:35 PM | 2.14306 | 1062.62 | 78.27 |
| 8/13/2013 1:08:36 PM | 2.14333 | 1062.62 | 78.27 |
| 8/13/2013 1:08:37 PM | 2.14361 | 1062.62 | 78.27 |
| 8/13/2013 1:08:38 PM | 2.14389 | 1062.62 | 78.27 |
| 8/13/2013 1:08:39 PM | 2.14417 | 1062.63 | 78.27 |
| 8/13/2013 1:08:40 PM | 2.14444 | 1062.63 | 78.27 |
| 8/13/2013 1:08:41 PM | 2.14472 | 1062.63 | 78.27 |
| 8/13/2013 1:08:42 PM | 2.14500 | 1062.63 | 78.27 |
| 8/13/2013 1:08:43 PM | 2.14528 | 1062.63 | 78.27 |
| 8/13/2013 1:08:44 PM | 2.14556 | 1062.63 | 78.27 |
| 8/13/2013 1:08:45 PM | 2.14583 | 1062.63 | 78.27 |
| 8/13/2013 1:08:46 PM | 2.14611 | 1062.64 | 78.27 |
| 8/13/2013 1:08:47 PM | 2.14639 | 1062.64 | 78.27 |
| 8/13/2013 1:08:48 PM | 2.14667 | 1062.64 | 78.27 |
| 8/13/2013 1:08:49 PM | 2.14694 | 1062.64 | 78.27 |
| 8/13/2013 1:08:50 PM | 2.14722 | 1062.64 | 78.27 |
| 8/13/2013 1:08:51 PM | 2.14750 | 1062.65 | 78.27 |
| 8/13/2013 1:08:52 PM | 2.14778 | 1062.65 | 78.27 |
| 8/13/2013 1:08:53 PM | 2.14806 | 1062.65 | 78.27 |
| 8/13/2013 1:08:54 PM | 2.14833 | 1062.65 | 78.27 |
| 8/13/2013 1:08:55 PM | 2.14861 | 1062.66 | 78.27 |
| 8/13/2013 1:08:56 PM | 2.14889 | 1062.66 | 78.27 |
| 8/13/2013 1:08:57 PM | 2.14917 | 1062.66 | 78.27 |
| 8/13/2013 1:08:58 PM | 2.14944 | 1062.66 | 78.27 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:08:59 PM | 2.14972 | 1062.66 | 78.27 |
| 8/13/2013 1:09:00 PM | 2.15000 | 1062.66 | 78.27 |
| 8/13/2013 1:09:01 PM | 2.15028 | 1062.66 | 78.27 |
| 8/13/2013 1:09:02 PM | 2.15056 | 1062.66 | 78.27 |
| 8/13/2013 1:09:03 PM | 2.15083 | 1062.67 | 78.27 |
| 8/13/2013 1:09:04 PM | 2.15111 | 1062.67 | 78.27 |
| 8/13/2013 1:09:05 PM | 2.15139 | 1062.67 | 78.27 |
| 8/13/2013 1:09:06 PM | 2.15167 | 1062.68 | 78.27 |
| 8/13/2013 1:09:07 PM | 2.15194 | 1062.68 | 78.27 |
| 8/13/2013 1:09:08 PM | 2.15222 | 1062.68 | 78.27 |
| 8/13/2013 1:09:09 PM | 2.15250 | 1062.69 | 78.27 |
| 8/13/2013 1:09:10 PM | 2.15278 | 1062.69 | 78.27 |
| 8/13/2013 1:09:11 PM | 2.15306 | 1062.70 | 78.27 |
| 8/13/2013 1:09:12 PM | 2.15333 | 1062.70 | 78.27 |
| 8/13/2013 1:09:13 PM | 2.15361 | 1062.70 | 78.27 |
| 8/13/2013 1:09:14 PM | 2.15389 | 1062.71 | 78.27 |
| 8/13/2013 1:09:15 PM | 2.15417 | 1062.71 | 78.27 |
| 8/13/2013 1:09:16 PM | 2.15444 | 1062.71 | 78.27 |
| 8/13/2013 1:09:17 PM | 2.15472 | 1062.71 | 78.27 |
| 8/13/2013 1:09:18 PM | 2.15500 | 1062.71 | 78.27 |
| 8/13/2013 1:09:19 PM | 2.15528 | 1062.71 | 78.27 |
| 8/13/2013 1:09:20 PM | 2.15556 | 1062.71 | 78.27 |
| 8/13/2013 1:09:21 PM | 2.15583 | 1062.71 | 78.27 |
| 8/13/2013 1:09:22 PM | 2.15611 | 1062.71 | 78.27 |
| 8/13/2013 1:09:23 PM | 2.15639 | 1062.71 | 78.27 |
| 8/13/2013 1:09:24 PM | 2.15667 | 1062.72 | 78.27 |
| 8/13/2013 1:09:25 PM | 2.15694 | 1062.72 | 78.27 |
| 8/13/2013 1:09:26 PM | 2.15722 | 1062.72 | 78.27 |
| 8/13/2013 1:09:27 PM | 2.15750 | 1062.72 | 78.27 |
| 8/13/2013 1:09:28 PM | 2.15778 | 1062.72 | 78.27 |
| 8/13/2013 1:09:29 PM | 2.15806 | 1062.73 | 78.27 |
| 8/13/2013 1:09:30 PM | 2.15833 | 1062.73 | 78.27 |
| 8/13/2013 1:09:31 PM | 2.15861 | 1062.73 | 78.27 |
| 8/13/2013 1:09:32 PM | 2.15889 | 1062.74 | 78.27 |
| 8/13/2013 1:09:33 PM | 2.15917 | 1062.74 | 78.27 |
| 8/13/2013 1:09:34 PM | 2.15944 | 1062.74 | 78.27 |
| 8/13/2013 1:09:35 PM | 2.15972 | 1062.75 | 78.27 |
| 8/13/2013 1:09:36 PM | 2.16000 | 1062.75 | 78.27 |
| 8/13/2013 1:09:37 PM | 2.16028 | 1062.75 | 78.27 |
| 8/13/2013 1:09:38 PM | 2.16056 | 1062.76 | 78.27 |
| 8/13/2013 1:09:39 PM | 2.16083 | 1062.76 | 78.27 |
| 8/13/2013 1:09:40 PM | 2.16111 | 1062.76 | 78.27 |
| 8/13/2013 1:09:41 PM | 2.16139 | 1062.76 | 78.27 |
| 8/13/2013 1:09:42 PM | 2.16167 | 1062.76 | 78.27 |
| 8/13/2013 1:09:43 PM | 2.16194 | 1062.76 | 78.27 |
| 8/13/2013 1:09:44 PM | 2.16222 | 1062.76 | 78.26 |
| 8/13/2013 1:09:45 PM | 2.16250 | 1062.77 | 78.26 |
| 8/13/2013 1:09:46 PM | 2.16278 | 1062.77 | 78.26 |
| 8/13/2013 1:09:47 PM | 2.16306 | 1062.77 | 78.26 |
| 8/13/2013 1:09:48 PM | 2.16333 | 1062.77 | 78.26 |
| 8/13/2013 1:09:49 PM | 2.16361 | 1062.77 | 78.26 |
| 8/13/2013 1:09:50 PM | 2.16389 | 1062.77 | 78.26 |
| 8/13/2013 1:09:51 PM | 2.16417 | 1062.78 | 78.26 |
| 8/13/2013 1:09:52 PM | 2.16444 | 1062.78 | 78.26 |
| 8/13/2013 1:09:53 PM | 2.16472 | 1062.78 | 78.26 |
| 8/13/2013 1:09:54 PM | 2.16500 | 1062.78 | 78.26 |
| 8/13/2013 1:09:55 PM | 2.16528 | 1062.78 | 78.26 |
| 8/13/2013 1:09:56 PM | 2.16556 | 1062.79 | 78.26 |
| 8/13/2013 1:09:57 PM | 2.16583 | 1062.79 | 78.26 |
| 8/13/2013 1:09:58 PM | 2.16611 | 1062.79 | 78.26 |
| 8/13/2013 1:09:59 PM | 2.16639 | 1062.79 | 78.26 |
| 8/13/2013 1:10:00 PM | 2.16667 | 1062.80 | 78.26 |
| 8/13/2013 1:10:01 PM | 2.16694 | 1062.80 | 78.26 |
| 8/13/2013 1:10:02 PM | 2.16722 | 1062.80 | 78.26 |
| 8/13/2013 1:10:03 PM | 2.16750 | 1062.81 | 78.26 |
| 8/13/2013 1:10:04 PM | 2.16778 | 1062.81 | 78.26 |
| 8/13/2013 1:10:05 PM | 2.16806 | 1062.81 | 78.26 |
| 8/13/2013 1:10:06 PM | 2.16833 | 1062.81 | 78.26 |
| 8/13/2013 1:10:07 PM | 2.16861 | 1062.82 | 78.26 |
| 8/13/2013 1:10:08 PM | 2.16889 | 1062.82 | 78.26 |
| 8/13/2013 1:10:09 PM | 2.16917 | 1062.82 | 78.26 |
| 8/13/2013 1:10:10 PM | 2.16944 | 1062.82 | 78.26 |
| 8/13/2013 1:10:11 PM | 2.16972 | 1062.82 | 78.26 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:10:12 PM | 2.17000 | 1062.83 | 78.26 |
| 8/13/2013 1:10:13 PM | 2.17028 | 1062.83 | 78.26 |
| 8/13/2013 1:10:14 PM | 2.17056 | 1062.83 | 78.26 |
| 8/13/2013 1:10:15 PM | 2.17083 | 1062.83 | 78.26 |
| 8/13/2013 1:10:16 PM | 2.17111 | 1062.83 | 78.26 |
| 8/13/2013 1:10:17 PM | 2.17139 | 1062.83 | 78.26 |
| 8/13/2013 1:10:18 PM | 2.17167 | 1062.83 | 78.26 |
| 8/13/2013 1:10:19 PM | 2.17194 | 1062.83 | 78.26 |
| 8/13/2013 1:10:20 PM | 2.17222 | 1062.83 | 78.26 |
| 8/13/2013 1:10:21 PM | 2.17250 | 1062.84 | 78.26 |
| 8/13/2013 1:10:22 PM | 2.17278 | 1062.84 | 78.26 |
| 8/13/2013 1:10:23 PM | 2.17306 | 1062.84 | 78.26 |
| 8/13/2013 1:10:24 PM | 2.17333 | 1062.84 | 78.26 |
| 8/13/2013 1:10:25 PM | 2.17361 | 1062.84 | 78.26 |
| 8/13/2013 1:10:26 PM | 2.17389 | 1062.84 | 78.26 |
| 8/13/2013 1:10:27 PM | 2.17417 | 1062.84 | 78.26 |
| 8/13/2013 1:10:28 PM | 2.17444 | 1062.84 | 78.26 |
| 8/13/2013 1:10:29 PM | 2.17472 | 1062.85 | 78.26 |
| 8/13/2013 1:10:30 PM | 2.17500 | 1062.85 | 78.26 |
| 8/13/2013 1:10:31 PM | 2.17528 | 1062.85 | 78.26 |
| 8/13/2013 1:10:32 PM | 2.17556 | 1062.85 | 78.26 |
| 8/13/2013 1:10:33 PM | 2.17583 | 1062.85 | 78.26 |
| 8/13/2013 1:10:34 PM | 2.17611 | 1062.86 | 78.26 |
| 8/13/2013 1:10:35 PM | 2.17639 | 1062.86 | 78.26 |
| 8/13/2013 1:10:36 PM | 2.17667 | 1062.86 | 78.26 |
| 8/13/2013 1:10:37 PM | 2.17694 | 1062.86 | 78.26 |
| 8/13/2013 1:10:38 PM | 2.17722 | 1062.87 | 78.26 |
| 8/13/2013 1:10:39 PM | 2.17750 | 1062.87 | 78.26 |
| 8/13/2013 1:10:40 PM | 2.17778 | 1062.87 | 78.26 |
| 8/13/2013 1:10:41 PM | 2.17806 | 1062.87 | 78.26 |
| 8/13/2013 1:10:42 PM | 2.17833 | 1062.88 | 78.26 |
| 8/13/2013 1:10:43 PM | 2.17861 | 1062.88 | 78.26 |
| 8/13/2013 1:10:44 PM | 2.17889 | 1062.88 | 78.26 |
| 8/13/2013 1:10:45 PM | 2.17917 | 1062.89 | 78.26 |
| 8/13/2013 1:10:46 PM | 2.17944 | 1062.89 | 78.26 |
| 8/13/2013 1:10:47 PM | 2.17972 | 1062.90 | 78.26 |
| 8/13/2013 1:10:48 PM | 2.18000 | 1062.90 | 78.26 |
| 8/13/2013 1:10:49 PM | 2.18028 | 1062.90 | 78.26 |
| 8/13/2013 1:10:50 PM | 2.18056 | 1062.90 | 78.26 |
| 8/13/2013 1:10:51 PM | 2.18083 | 1062.91 | 78.25 |
| 8/13/2013 1:10:52 PM | 2.18111 | 1062.91 | 78.25 |
| 8/13/2013 1:10:53 PM | 2.18139 | 1062.91 | 78.25 |
| 8/13/2013 1:10:54 PM | 2.18167 | 1062.91 | 78.25 |
| 8/13/2013 1:10:55 PM | 2.18194 | 1062.91 | 78.25 |
| 8/13/2013 1:10:56 PM | 2.18222 | 1062.91 | 78.25 |
| 8/13/2013 1:10:57 PM | 2.18250 | 1062.91 | 78.25 |
| 8/13/2013 1:10:58 PM | 2.18278 | 1062.91 | 78.25 |
| 8/13/2013 1:10:59 PM | 2.18306 | 1062.92 | 78.25 |
| 8/13/2013 1:11:00 PM | 2.18333 | 1062.92 | 78.25 |
| 8/13/2013 1:11:01 PM | 2.18361 | 1062.92 | 78.25 |
| 8/13/2013 1:11:02 PM | 2.18389 | 1062.92 | 78.25 |
| 8/13/2013 1:11:03 PM | 2.18417 | 1062.92 | 78.25 |
| 8/13/2013 1:11:04 PM | 2.18444 | 1062.92 | 78.25 |
| 8/13/2013 1:11:05 PM | 2.18472 | 1062.93 | 78.25 |
| 8/13/2013 1:11:06 PM | 2.18500 | 1062.93 | 78.25 |
| 8/13/2013 1:11:07 PM | 2.18528 | 1062.93 | 78.25 |
| 8/13/2013 1:11:08 PM | 2.18556 | 1062.93 | 78.25 |
| 8/13/2013 1:11:09 PM | 2.18583 | 1062.94 | 78.25 |
| 8/13/2013 1:11:10 PM | 2.18611 | 1062.94 | 78.25 |
| 8/13/2013 1:11:11 PM | 2.18639 | 1062.94 | 78.25 |
| 8/13/2013 1:11:12 PM | 2.18667 | 1062.94 | 78.25 |
| 8/13/2013 1:11:13 PM | 2.18694 | 1062.95 | 78.25 |
| 8/13/2013 1:11:14 PM | 2.18722 | 1062.95 | 78.25 |
| 8/13/2013 1:11:15 PM | 2.18750 | 1062.95 | 78.25 |
| 8/13/2013 1:11:16 PM | 2.18778 | 1062.95 | 78.25 |
| 8/13/2013 1:11:17 PM | 2.18806 | 1062.96 | 78.25 |
| 8/13/2013 1:11:18 PM | 2.18833 | 1062.96 | 78.25 |
| 8/13/2013 1:11:19 PM | 2.18861 | 1062.96 | 78.25 |
| 8/13/2013 1:11:20 PM | 2.18889 | 1062.96 | 78.25 |
| 8/13/2013 1:11:21 PM | 2.18917 | 1062.97 | 78.25 |
| 8/13/2013 1:11:22 PM | 2.18944 | 1062.97 | 78.25 |
| 8/13/2013 1:11:23 PM | 2.18972 | 1062.97 | 78.25 |
| 8/13/2013 1:11:24 PM | 2.19000 | 1062.98 | 78.25 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:11:25 PM | 2.19028 | 1062.98 | 78.25 |
| 8/13/2013 1:11:26 PM | 2.19056 | 1062.98 | 78.25 |
| 8/13/2013 1:11:27 PM | 2.19083 | 1062.98 | 78.25 |
| 8/13/2013 1:11:28 PM | 2.19111 | 1062.98 | 78.25 |
| 8/13/2013 1:11:29 PM | 2.19139 | 1062.98 | 78.25 |
| 8/13/2013 1:11:30 PM | 2.19167 | 1062.99 | 78.25 |
| 8/13/2013 1:11:31 PM | 2.19194 | 1062.99 | 78.25 |
| 8/13/2013 1:11:32 PM | 2.19222 | 1062.99 | 78.25 |
| 8/13/2013 1:11:33 PM | 2.19250 | 1062.99 | 78.25 |
| 8/13/2013 1:11:34 PM | 2.19278 | 1062.99 | 78.25 |
| 8/13/2013 1:11:35 PM | 2.19306 | 1062.99 | 78.25 |
| 8/13/2013 1:11:36 PM | 2.19333 | 1063.00 | 78.25 |
| 8/13/2013 1:11:37 PM | 2.19361 | 1063.00 | 78.25 |
| 8/13/2013 1:11:38 PM | 2.19389 | 1063.01 | 78.25 |
| 8/13/2013 1:11:39 PM | 2.19417 | 1063.01 | 78.25 |
| 8/13/2013 1:11:40 PM | 2.19444 | 1063.02 | 78.25 |
| 8/13/2013 1:11:41 PM | 2.19472 | 1063.02 | 78.25 |
| 8/13/2013 1:11:42 PM | 2.19500 | 1063.03 | 78.25 |
| 8/13/2013 1:11:43 PM | 2.19528 | 1063.03 | 78.25 |
| 8/13/2013 1:11:44 PM | 2.19556 | 1063.03 | 78.25 |
| 8/13/2013 1:11:45 PM | 2.19583 | 1063.04 | 78.25 |
| 8/13/2013 1:11:46 PM | 2.19611 | 1063.04 | 78.25 |
| 8/13/2013 1:11:47 PM | 2.19639 | 1063.04 | 78.25 |
| 8/13/2013 1:11:48 PM | 2.19667 | 1063.04 | 78.25 |
| 8/13/2013 1:11:49 PM | 2.19694 | 1063.04 | 78.25 |
| 8/13/2013 1:11:50 PM | 2.19722 | 1063.04 | 78.25 |
| 8/13/2013 1:11:51 PM | 2.19750 | 1063.04 | 78.25 |
| 8/13/2013 1:11:52 PM | 2.19778 | 1063.04 | 78.25 |
| 8/13/2013 1:11:53 PM | 2.19806 | 1063.04 | 78.25 |
| 8/13/2013 1:11:54 PM | 2.19833 | 1063.04 | 78.25 |
| 8/13/2013 1:11:55 PM | 2.19861 | 1063.05 | 78.25 |
| 8/13/2013 1:11:56 PM | 2.19889 | 1063.05 | 78.25 |
| 8/13/2013 1:11:57 PM | 2.19917 | 1063.05 | 78.25 |
| 8/13/2013 1:11:58 PM | 2.19944 | 1063.05 | 78.25 |
| 8/13/2013 1:11:59 PM | 2.19972 | 1063.06 | 78.25 |
| 8/13/2013 1:12:00 PM | 2.20000 | 1063.06 | 78.25 |
| 8/13/2013 1:12:01 PM | 2.20028 | 1063.07 | 78.25 |
| 8/13/2013 1:12:02 PM | 2.20056 | 1063.07 | 78.25 |
| 8/13/2013 1:12:03 PM | 2.20083 | 1063.07 | 78.25 |
| 8/13/2013 1:12:04 PM | 2.20111 | 1063.07 | 78.24 |
| 8/13/2013 1:12:05 PM | 2.20139 | 1063.07 | 78.24 |
| 8/13/2013 1:12:06 PM | 2.20167 | 1063.07 | 78.24 |
| 8/13/2013 1:12:07 PM | 2.20194 | 1063.07 | 78.24 |
| 8/13/2013 1:12:08 PM | 2.20222 | 1063.07 | 78.24 |
| 8/13/2013 1:12:09 PM | 2.20250 | 1063.06 | 78.24 |
| 8/13/2013 1:12:10 PM | 2.20278 | 1063.06 | 78.24 |
| 8/13/2013 1:12:11 PM | 2.20306 | 1063.05 | 78.24 |
| 8/13/2013 1:12:12 PM | 2.20333 | 1063.04 | 78.24 |
| 8/13/2013 1:12:13 PM | 2.20361 | 1063.04 | 78.24 |
| 8/13/2013 1:12:14 PM | 2.20389 | 1063.03 | 78.24 |
| 8/13/2013 1:12:15 PM | 2.20417 | 1063.03 | 78.24 |
| 8/13/2013 1:12:16 PM | 2.20444 | 1063.02 | 78.24 |
| 8/13/2013 1:12:17 PM | 2.20472 | 1063.02 | 78.24 |
| 8/13/2013 1:12:18 PM | 2.20500 | 1063.02 | 78.24 |
| 8/13/2013 1:12:19 PM | 2.20528 | 1063.03 | 78.24 |
| 8/13/2013 1:12:20 PM | 2.20556 | 1062.88 | 78.24 |
| 8/13/2013 1:12:21 PM | 2.20583 | 1063.01 | 78.24 |
| 8/13/2013 1:12:22 PM | 2.20611 | 1062.96 | 78.24 |
| 8/13/2013 1:12:23 PM | 2.20639 | 1062.79 | 78.24 |
| 8/13/2013 1:12:24 PM | 2.20667 | 1062.89 | 78.24 |
| 8/13/2013 1:12:25 PM | 2.20694 | 1062.78 | 78.24 |
| 8/13/2013 1:12:26 PM | 2.20722 | 1062.52 | 78.24 |
| 8/13/2013 1:12:27 PM | 2.20750 | 1057.97 | 78.24 |
| 8/13/2013 1:12:28 PM | 2.20778 | 1056.98 | 78.24 |
| 8/13/2013 1:12:29 PM | 2.20806 | 1046.56 | 78.23 |
| 8/13/2013 1:12:30 PM | 2.20833 | 1039.79 | 78.22 |
| 8/13/2013 1:12:31 PM | 2.20861 | 1035.63 | 78.22 |
| 8/13/2013 1:12:32 PM | 2.20889 | 1025.76 | 78.22 |
| 8/13/2013 1:12:33 PM | 2.20917 | 1018.90 | 78.21 |
| 8/13/2013 1:12:34 PM | 2.20944 | 1012.48 | 78.21 |
| 8/13/2013 1:12:35 PM | 2.20972 | 999.50 | 78.20 |
| 8/13/2013 1:12:36 PM | 2.21000 | 992.62 | 78.20 |
| 8/13/2013 1:12:37 PM | 2.21028 | 984.15 | 78.20 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:12:38 PM | 2.21056 | 972.11 | 78.19 |
| 8/13/2013 1:12:39 PM | 2.21083 | 966.28 | 78.19 |
| 8/13/2013 1:12:40 PM | 2.21111 | 956.48 | 78.19 |
| 8/13/2013 1:12:41 PM | 2.21139 | 945.42 | 78.19 |
| 8/13/2013 1:12:42 PM | 2.21167 | 939.75 | 78.18 |
| 8/13/2013 1:12:43 PM | 2.21194 | 928.80 | 78.18 |
| 8/13/2013 1:12:44 PM | 2.21222 | 918.00 | 78.18 |
| 8/13/2013 1:12:45 PM | 2.21250 | 911.76 | 78.18 |
| 8/13/2013 1:12:46 PM | 2.21278 | 900.18 | 78.17 |
| 8/13/2013 1:12:47 PM | 2.21306 | 889.92 | 78.17 |
| 8/13/2013 1:12:48 PM | 2.21333 | 883.20 | 78.17 |
| 8/13/2013 1:12:49 PM | 2.21361 | 871.45 | 78.17 |
| 8/13/2013 1:12:50 PM | 2.21389 | 861.82 | 78.16 |
| 8/13/2013 1:12:51 PM | 2.21417 | 852.52 | 78.16 |
| 8/13/2013 1:12:52 PM | 2.21444 | 838.68 | 78.16 |
| 8/13/2013 1:12:53 PM | 2.21472 | 820.08 | 78.15 |
| 8/13/2013 1:12:54 PM | 2.21500 | 804.55 | 78.14 |
| 8/13/2013 1:12:55 PM | 2.21528 | 782.96 | 78.13 |
| 8/13/2013 1:12:56 PM | 2.21556 | 753.92 | 78.12 |
| 8/13/2013 1:12:57 PM | 2.21583 | 730.24 | 78.11 |
| 8/13/2013 1:12:58 PM | 2.21611 | 708.31 | 78.10 |
| 8/13/2013 1:12:59 PM | 2.21639 | 679.98 | 78.09 |
| 8/13/2013 1:13:00 PM | 2.21667 | 657.77 | 78.08 |
| 8/13/2013 1:13:01 PM | 2.21694 | 635.52 | 78.08 |
| 8/13/2013 1:13:02 PM | 2.21722 | 610.09 | 78.07 |
| 8/13/2013 1:13:03 PM | 2.21750 | 588.88 | 78.07 |
| 8/13/2013 1:13:04 PM | 2.21778 | 566.63 | 78.06 |
| 8/13/2013 1:13:05 PM | 2.21806 | 543.92 | 78.06 |
| 8/13/2013 1:13:06 PM | 2.21833 | 523.77 | 78.05 |
| 8/13/2013 1:13:07 PM | 2.21861 | 502.07 | 78.05 |
| 8/13/2013 1:13:08 PM | 2.21889 | 481.34 | 78.05 |
| 8/13/2013 1:13:09 PM | 2.21917 | 462.27 | 78.04 |
| 8/13/2013 1:13:10 PM | 2.21944 | 441.56 | 78.04 |
| 8/13/2013 1:13:11 PM | 2.21972 | 422.61 | 78.04 |
| 8/13/2013 1:13:12 PM | 2.22000 | 404.57 | 78.04 |
| 8/13/2013 1:13:13 PM | 2.22028 | 380.11 | 78.03 |
| 8/13/2013 1:13:14 PM | 2.22056 | 362.20 | 78.03 |
| 8/13/2013 1:13:15 PM | 2.22083 | 336.02 | 78.02 |
| 8/13/2013 1:13:16 PM | 2.22111 | 311.18 | 78.02 |
| 8/13/2013 1:13:17 PM | 2.22139 | 293.81 | 78.02 |
| 8/13/2013 1:13:18 PM | 2.22167 | 265.03 | 78.01 |
| 8/13/2013 1:13:19 PM | 2.22194 | 237.59 | 78.00 |
| 8/13/2013 1:13:20 PM | 2.22222 | 216.96 | 78.00 |
| 8/13/2013 1:13:21 PM | 2.22250 | 188.23 | 77.99 |
| 8/13/2013 1:13:22 PM | 2.22278 | 170.10 | 77.99 |
| 8/13/2013 1:13:23 PM | 2.22306 | 149.65 | 77.99 |
| 8/13/2013 1:13:24 PM | 2.22333 | 125.58 | 77.99 |
| 8/13/2013 1:13:25 PM | 2.22361 | 111.08 | 77.99 |
| 8/13/2013 1:13:26 PM | 2.22389 | 82.89 | 77.98 |
| 8/13/2013 1:13:27 PM | 2.22417 | 64.65 | 77.98 |
| 8/13/2013 1:13:28 PM | 2.22444 | 38.15 | 77.97 |
| 8/13/2013 1:13:29 PM | 2.22472 | 17.68 | 77.98 |
| 8/13/2013 1:13:30 PM | 2.22500 | 14.61 | 77.98 |
| 8/13/2013 1:13:31 PM | 2.22528 | 14.54 | 77.99 |
| 8/13/2013 1:13:32 PM | 2.22556 | 14.49 | 78.00 |
| 8/13/2013 1:13:33 PM | 2.22583 | 14.42 | 78.01 |
| 8/13/2013 1:13:34 PM | 2.22611 | 14.39 | 78.02 |
| 8/13/2013 1:13:35 PM | 2.22639 | 14.35 | 78.02 |
| 8/13/2013 1:13:36 PM | 2.22667 | 14.33 | 78.03 |
| 8/13/2013 1:13:37 PM | 2.22694 | 14.32 | 78.03 |
| 8/13/2013 1:13:38 PM | 2.22722 | 14.30 | 78.03 |
| 8/13/2013 1:13:39 PM | 2.22750 | 14.30 | 78.04 |
| 8/13/2013 1:13:40 PM | 2.22778 | 14.30 | 78.04 |
| 8/13/2013 1:13:41 PM | 2.22806 | 14.30 | 78.04 |
| 8/13/2013 1:13:42 PM | 2.22833 | 14.30 | 78.04 |
| 8/13/2013 1:13:43 PM | 2.22861 | 14.30 | 78.04 |
| 8/13/2013 1:13:44 PM | 2.22889 | 14.30 | 78.04 |
| 8/13/2013 1:13:45 PM | 2.22917 | 14.30 | 78.04 |
| 8/13/2013 1:13:46 PM | 2.22944 | 14.30 | 78.04 |
| 8/13/2013 1:13:47 PM | 2.22972 | 14.30 | 78.04 |
| 8/13/2013 1:13:48 PM | 2.23000 | 14.30 | 78.03 |
| 8/13/2013 1:13:49 PM | 2.23028 | 14.30 | 78.03 |
| 8/13/2013 1:13:50 PM | 2.23056 | 14.30 | 78.03 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:13:51 PM | 2.23083 | 14.30 | 78.02 |
| 8/13/2013 1:13:52 PM | 2.23111 | 14.30 | 78.02 |
| 8/13/2013 1:13:53 PM | 2.23139 | 14.29 | 78.01 |
| 8/13/2013 1:13:54 PM | 2.23167 | 14.29 | 78.01 |
| 8/13/2013 1:13:55 PM | 2.23194 | 14.28 | 78.00 |
| 8/13/2013 1:13:56 PM | 2.23222 | 14.26 | 78.00 |
| 8/13/2013 1:13:57 PM | 2.23250 | 14.23 | 77.99 |
| 8/13/2013 1:13:58 PM | 2.23278 | 14.17 | 77.99 |
| 8/13/2013 1:13:59 PM | 2.23306 | 14.10 | 77.98 |
| 8/13/2013 1:14:00 PM | 2.23333 | 14.00 | 77.97 |
| 8/13/2013 1:14:01 PM | 2.23361 | 13.88 | 77.97 |
| 8/13/2013 1:14:02 PM | 2.23389 | 13.76 | 77.96 |
| 8/13/2013 1:14:03 PM | 2.23417 | 13.64 | 77.96 |
| 8/13/2013 1:14:04 PM | 2.23444 | 13.54 | 77.95 |
| 8/13/2013 1:14:05 PM | 2.23472 | 13.46 | 77.94 |
| 8/13/2013 1:14:06 PM | 2.23500 | 13.42 | 77.94 |
| 8/13/2013 1:14:07 PM | 2.23528 | 13.41 | 77.93 |
| 8/13/2013 1:14:08 PM | 2.23556 | 13.44 | 77.93 |
| 8/13/2013 1:14:09 PM | 2.23583 | 13.52 | 77.92 |
| 8/13/2013 1:14:10 PM | 2.23611 | 13.64 | 77.92 |
| 8/13/2013 1:14:11 PM | 2.23639 | 13.76 | 77.91 |
| 8/13/2013 1:14:12 PM | 2.23667 | 13.88 | 77.91 |
| 8/13/2013 1:14:13 PM | 2.23694 | 13.99 | 77.90 |
| 8/13/2013 1:14:14 PM | 2.23722 | 14.09 | 77.90 |
| 8/13/2013 1:14:15 PM | 2.23750 | 14.17 | 77.89 |
| 8/13/2013 1:14:16 PM | 2.23778 | 14.24 | 77.89 |
| 8/13/2013 1:14:17 PM | 2.23806 | 14.28 | 77.88 |
| 8/13/2013 1:14:18 PM | 2.23833 | 14.30 | 77.88 |
| 8/13/2013 1:14:19 PM | 2.23861 | 14.30 | 77.88 |
| 8/13/2013 1:14:20 PM | 2.23889 | 14.30 | 77.87 |
| 8/13/2013 1:14:21 PM | 2.23917 | 14.30 | 77.87 |
| 8/13/2013 1:14:22 PM | 2.23944 | 14.30 | 77.86 |
| 8/13/2013 1:14:23 PM | 2.23972 | 14.30 | 77.86 |
| 8/13/2013 1:14:24 PM | 2.24000 | 14.30 | 77.86 |
| 8/13/2013 1:14:25 PM | 2.24028 | 14.30 | 77.86 |
| 8/13/2013 1:14:26 PM | 2.24056 | 14.30 | 77.85 |
| 8/13/2013 1:14:27 PM | 2.24083 | 14.30 | 77.85 |
| 8/13/2013 1:14:28 PM | 2.24111 | 14.30 | 77.85 |
| 8/13/2013 1:14:29 PM | 2.24139 | 14.30 | 77.85 |
| 8/13/2013 1:14:30 PM | 2.24167 | 14.30 | 77.85 |
| 8/13/2013 1:14:31 PM | 2.24194 | 14.30 | 77.84 |
| 8/13/2013 1:14:32 PM | 2.24222 | 14.30 | 77.84 |
| 8/13/2013 1:14:33 PM | 2.24250 | 14.30 | 77.84 |
| 8/13/2013 1:14:34 PM | 2.24278 | 14.30 | 77.84 |
| 8/13/2013 1:14:35 PM | 2.24306 | 14.30 | 77.84 |
| 8/13/2013 1:14:36 PM | 2.24333 | 14.30 | 77.84 |
| 8/13/2013 1:14:37 PM | 2.24361 | 14.30 | 77.84 |
| 8/13/2013 1:14:38 PM | 2.24389 | 14.30 | 77.83 |
| 8/13/2013 1:14:39 PM | 2.24417 | 14.30 | 77.83 |
| 8/13/2013 1:14:40 PM | 2.24444 | 14.30 | 77.83 |
| 8/13/2013 1:14:41 PM | 2.24472 | 14.30 | 77.83 |
| 8/13/2013 1:14:42 PM | 2.24500 | 14.30 | 77.83 |
| 8/13/2013 1:14:43 PM | 2.24528 | 14.30 | 77.83 |
| 8/13/2013 1:14:44 PM | 2.24556 | 14.30 | 77.83 |
| 8/13/2013 1:14:45 PM | 2.24583 | 14.30 | 77.83 |
| 8/13/2013 1:14:46 PM | 2.24611 | 14.30 | 77.83 |
| 8/13/2013 1:14:47 PM | 2.24639 | 14.30 | 77.83 |
| 8/13/2013 1:14:48 PM | 2.24667 | 14.30 | 77.83 |
| 8/13/2013 1:14:49 PM | 2.24694 | 14.30 | 77.83 |
| 8/13/2013 1:14:50 PM | 2.24722 | 14.30 | 77.83 |
| 8/13/2013 1:14:51 PM | 2.24750 | 14.30 | 77.82 |
| 8/13/2013 1:14:52 PM | 2.24778 | 14.30 | 77.82 |
| 8/13/2013 1:14:53 PM | 2.24806 | 14.30 | 77.82 |
| 8/13/2013 1:14:54 PM | 2.24833 | 14.30 | 77.82 |
| 8/13/2013 1:14:55 PM | 2.24861 | 14.30 | 77.82 |
| 8/13/2013 1:14:56 PM | 2.24889 | 14.30 | 77.82 |
| 8/13/2013 1:14:57 PM | 2.24917 | 14.30 | 77.82 |
| 8/13/2013 1:14:58 PM | 2.24944 | 14.30 | 77.82 |
| 8/13/2013 1:14:59 PM | 2.24972 | 14.30 | 77.82 |
| 8/13/2013 1:15:00 PM | 2.25000 | 14.30 | 77.82 |
| 8/13/2013 1:15:01 PM | 2.25028 | 14.30 | 77.82 |
| 8/13/2013 1:15:02 PM | 2.25056 | 14.30 | 77.82 |
| 8/13/2013 1:15:03 PM | 2.25083 | 14.30 | 77.82 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:15:04 PM | 2.25111 | 14.30 | 77.82 |
| 8/13/2013 1:15:05 PM | 2.25139 | 14.30 | 77.82 |
| 8/13/2013 1:15:06 PM | 2.25167 | 14.30 | 77.81 |
| 8/13/2013 1:15:07 PM | 2.25194 | 14.30 | 77.81 |
| 8/13/2013 1:15:08 PM | 2.25222 | 14.30 | 77.81 |
| 8/13/2013 1:15:09 PM | 2.25250 | 14.30 | 77.81 |
| 8/13/2013 1:15:10 PM | 2.25278 | 14.30 | 77.81 |
| 8/13/2013 1:15:11 PM | 2.25306 | 14.30 | 77.81 |
| 8/13/2013 1:15:12 PM | 2.25333 | 14.30 | 77.81 |
| 8/13/2013 1:15:13 PM | 2.25361 | 14.30 | 77.81 |
| 8/13/2013 1:15:14 PM | 2.25389 | 14.30 | 77.81 |
| 8/13/2013 1:15:15 PM | 2.25417 | 14.30 | 77.81 |
| 8/13/2013 1:15:16 PM | 2.25444 | 14.30 | 77.81 |
| 8/13/2013 1:15:17 PM | 2.25472 | 14.30 | 77.81 |
| 8/13/2013 1:15:18 PM | 2.25500 | 14.30 | 77.81 |
| 8/13/2013 1:15:19 PM | 2.25528 | 14.30 | 77.81 |
| 8/13/2013 1:15:20 PM | 2.25556 | 14.30 | 77.81 |
| 8/13/2013 1:15:21 PM | 2.25583 | 14.30 | 77.81 |
| 8/13/2013 1:15:22 PM | 2.25611 | 14.30 | 77.81 |
| 8/13/2013 1:15:23 PM | 2.25639 | 14.30 | 77.81 |
| 8/13/2013 1:15:24 PM | 2.25667 | 14.30 | 77.81 |
| 8/13/2013 1:15:25 PM | 2.25694 | 14.30 | 77.81 |
| 8/13/2013 1:15:26 PM | 2.25722 | 14.30 | 77.81 |
| 8/13/2013 1:15:27 PM | 2.25750 | 14.30 | 77.81 |
| 8/13/2013 1:15:28 PM | 2.25778 | 14.30 | 77.81 |
| 8/13/2013 1:15:29 PM | 2.25806 | 14.30 | 77.81 |
| 8/13/2013 1:15:30 PM | 2.25833 | 14.30 | 77.80 |
| 8/13/2013 1:15:31 PM | 2.25861 | 14.30 | 77.80 |
| 8/13/2013 1:15:32 PM | 2.25889 | 14.30 | 77.80 |
| 8/13/2013 1:15:33 PM | 2.25917 | 14.30 | 77.80 |
| 8/13/2013 1:15:34 PM | 2.25944 | 14.30 | 77.80 |
| 8/13/2013 1:15:35 PM | 2.25972 | 14.30 | 77.80 |
| 8/13/2013 1:15:36 PM | 2.26000 | 14.30 | 77.80 |
| 8/13/2013 1:15:37 PM | 2.26028 | 14.30 | 77.80 |
| 8/13/2013 1:15:38 PM | 2.26056 | 14.30 | 77.80 |
| 8/13/2013 1:15:39 PM | 2.26083 | 14.30 | 77.80 |
| 8/13/2013 1:15:40 PM | 2.26111 | 14.30 | 77.80 |
| 8/13/2013 1:15:41 PM | 2.26139 | 14.30 | 77.79 |
| 8/13/2013 1:15:42 PM | 2.26167 | 14.30 | 77.79 |
| 8/13/2013 1:15:43 PM | 2.26194 | 14.30 | 77.79 |
| 8/13/2013 1:15:44 PM | 2.26222 | 14.30 | 77.79 |
| 8/13/2013 1:15:45 PM | 2.26250 | 14.30 | 77.79 |
| 8/13/2013 1:15:46 PM | 2.26278 | 14.30 | 77.79 |
| 8/13/2013 1:15:47 PM | 2.26306 | 14.30 | 77.78 |
| 8/13/2013 1:15:48 PM | 2.26333 | 14.30 | 77.78 |
| 8/13/2013 1:15:49 PM | 2.26361 | 14.30 | 77.78 |
| 8/13/2013 1:15:50 PM | 2.26389 | 14.30 | 77.78 |
| 8/13/2013 1:15:51 PM | 2.26417 | 14.30 | 77.78 |
| 8/13/2013 1:15:52 PM | 2.26444 | 14.30 | 77.78 |
| 8/13/2013 1:15:53 PM | 2.26472 | 14.30 | 77.78 |
| 8/13/2013 1:15:54 PM | 2.26500 | 14.30 | 77.77 |
| 8/13/2013 1:15:55 PM | 2.26528 | 14.30 | 77.77 |
| 8/13/2013 1:15:56 PM | 2.26556 | 14.30 | 77.77 |
| 8/13/2013 1:15:57 PM | 2.26583 | 14.30 | 77.77 |
| 8/13/2013 1:15:58 PM | 2.26611 | 14.30 | 77.77 |
| 8/13/2013 1:15:59 PM | 2.26639 | 14.30 | 77.77 |
| 8/13/2013 1:16:00 PM | 2.26667 | 14.30 | 77.77 |
| 8/13/2013 1:16:01 PM | 2.26694 | 14.30 | 77.77 |
| 8/13/2013 1:16:02 PM | 2.26722 | 14.30 | 77.77 |
| 8/13/2013 1:16:03 PM | 2.26750 | 14.30 | 77.76 |
| 8/13/2013 1:16:04 PM | 2.26778 | 14.30 | 77.76 |
| 8/13/2013 1:16:05 PM | 2.26806 | 14.30 | 77.76 |
| 8/13/2013 1:16:06 PM | 2.26833 | 14.30 | 77.76 |
| 8/13/2013 1:16:07 PM | 2.26861 | 14.30 | 77.76 |
| 8/13/2013 1:16:08 PM | 2.26889 | 14.30 | 77.76 |
| 8/13/2013 1:16:09 PM | 2.26917 | 14.30 | 77.76 |
| 8/13/2013 1:16:10 PM | 2.26944 | 14.30 | 77.75 |
| 8/13/2013 1:16:11 PM | 2.26972 | 14.30 | 77.75 |
| 8/13/2013 1:16:12 PM | 2.27000 | 14.30 | 77.75 |
| 8/13/2013 1:16:13 PM | 2.27028 | 14.30 | 77.75 |
| 8/13/2013 1:16:14 PM | 2.27056 | 14.30 | 77.75 |
| 8/13/2013 1:16:15 PM | 2.27083 | 14.30 | 77.75 |
| 8/13/2013 1:16:16 PM | 2.27111 | 14.30 | 77.74 |

Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:16:17 PM | 2.27139 | 14.30 | 77.74 |
| 8/13/2013 1:16:18 PM | 2.27167 | 14.30 | 77.73 |
| 8/13/2013 1:16:19 PM | 2.27194 | 14.30 | 77.73 |
| 8/13/2013 1:16:20 PM | 2.27222 | 14.30 | 77.73 |
| 8/13/2013 1:16:21 PM | 2.27250 | 14.30 | 77.72 |
| 8/13/2013 1:16:22 PM | 2.27278 | 14.30 | 77.72 |
| 8/13/2013 1:16:23 PM | 2.27306 | 14.30 | 77.71 |
| 8/13/2013 1:16:24 PM | 2.27333 | 14.30 | 77.70 |
| 8/13/2013 1:16:25 PM | 2.27361 | 14.30 | 77.69 |
| 8/13/2013 1:16:26 PM | 2.27389 | 14.30 | 77.69 |
| 8/13/2013 1:16:27 PM | 2.27417 | 14.30 | 77.68 |
| 8/13/2013 1:16:28 PM | 2.27444 | 14.30 | 77.67 |
| 8/13/2013 1:16:29 PM | 2.27472 | 14.30 | 77.66 |
| 8/13/2013 1:16:30 PM | 2.27500 | 14.30 | 77.65 |
| 8/13/2013 1:16:31 PM | 2.27528 | 14.30 | 77.64 |
| 8/13/2013 1:16:32 PM | 2.27556 | 14.30 | 77.64 |
| 8/13/2013 1:16:33 PM | 2.27583 | 14.30 | 77.63 |
| 8/13/2013 1:16:34 PM | 2.27611 | 14.30 | 77.61 |
| 8/13/2013 1:16:35 PM | 2.27639 | 14.30 | 77.61 |
| 8/13/2013 1:16:36 PM | 2.27667 | 14.30 | 77.59 |
| 8/13/2013 1:16:37 PM | 2.27694 | 14.30 | 77.58 |
| 8/13/2013 1:16:38 PM | 2.27722 | 14.30 | 77.58 |
| 8/13/2013 1:16:39 PM | 2.27750 | 14.30 | 77.56 |
| 8/13/2013 1:16:40 PM | 2.27778 | 14.30 | 77.56 |
| 8/13/2013 1:16:41 PM | 2.27806 | 14.30 | 77.55 |
| 8/13/2013 1:16:42 PM | 2.27833 | 14.30 | 77.54 |
| 8/13/2013 1:16:43 PM | 2.27861 | 14.30 | 77.53 |
| 8/13/2013 1:16:44 PM | 2.27889 | 14.30 | 77.52 |
| 8/13/2013 1:16:45 PM | 2.27917 | 14.30 | 77.51 |
| 8/13/2013 1:16:46 PM | 2.27944 | 14.30 | 77.50 |
| 8/13/2013 1:16:47 PM | 2.27972 | 14.30 | 77.49 |
| 8/13/2013 1:16:48 PM | 2.28000 | 14.30 | 77.49 |
| 8/13/2013 1:16:49 PM | 2.28028 | 14.30 | 77.48 |
| 8/13/2013 1:16:50 PM | 2.28056 | 14.30 | 77.47 |
| 8/13/2013 1:16:51 PM | 2.28083 | 14.30 | 77.46 |
| 8/13/2013 1:16:52 PM | 2.28111 | 14.30 | 77.45 |
| 8/13/2013 1:16:53 PM | 2.28139 | 14.30 | 77.45 |
| 8/13/2013 1:16:54 PM | 2.28167 | 14.30 | 77.44 |
| 8/13/2013 1:16:55 PM | 2.28194 | 14.30 | 77.43 |
| 8/13/2013 1:16:56 PM | 2.28222 | 14.30 | 77.42 |
| 8/13/2013 1:16:57 PM | 2.28250 | 14.30 | 77.42 |
| 8/13/2013 1:16:58 PM | 2.28278 | 14.30 | 77.41 |
| 8/13/2013 1:16:59 PM | 2.28306 | 14.30 | 77.40 |
| 8/13/2013 1:17:00 PM | 2.28333 | 14.30 | 77.39 |
| 8/13/2013 1:17:01 PM | 2.28361 | 14.30 | 77.39 |
| 8/13/2013 1:17:02 PM | 2.28389 | 14.30 | 77.38 |
| 8/13/2013 1:17:03 PM | 2.28417 | 14.30 | 77.37 |
| 8/13/2013 1:17:04 PM | 2.28444 | 14.30 | 77.36 |
| 8/13/2013 1:17:05 PM | 2.28472 | 14.30 | 77.36 |
| 8/13/2013 1:17:06 PM | 2.28500 | 14.30 | 77.35 |
| 8/13/2013 1:17:07 PM | 2.28528 | 14.30 | 77.34 |
| 8/13/2013 1:17:08 PM | 2.28556 | 14.30 | 77.33 |
| 8/13/2013 1:17:09 PM | 2.28583 | 14.30 | 77.33 |
| 8/13/2013 1:17:10 PM | 2.28611 | 14.30 | 77.32 |
| 8/13/2013 1:17:11 PM | 2.28639 | 14.30 | 77.31 |
| 8/13/2013 1:17:12 PM | 2.28667 | 14.30 | 77.31 |
| 8/13/2013 1:17:13 PM | 2.28694 | 14.30 | 77.30 |
| 8/13/2013 1:17:14 PM | 2.28722 | 14.30 | 77.29 |
| 8/13/2013 1:17:15 PM | 2.28750 | 14.30 | 77.28 |
| 8/13/2013 1:17:16 PM | 2.28778 | 14.30 | 77.28 |
| 8/13/2013 1:17:17 PM | 2.28806 | 14.30 | 77.27 |
| 8/13/2013 1:17:18 PM | 2.28833 | 14.30 | 77.26 |
| 8/13/2013 1:17:19 PM | 2.28861 | 14.30 | 77.26 |
| 8/13/2013 1:17:20 PM | 2.28889 | 14.30 | 77.25 |
| 8/13/2013 1:17:21 PM | 2.28917 | 14.30 | 77.25 |
| 8/13/2013 1:17:22 PM | 2.28944 | 14.30 | 77.24 |
| 8/13/2013 1:17:23 PM | 2.28972 | 14.30 | 77.23 |
| 8/13/2013 1:17:24 PM | 2.29000 | 14.30 | 77.23 |
| 8/13/2013 1:17:25 PM | 2.29028 | 14.30 | 77.22 |
| 8/13/2013 1:17:26 PM | 2.29056 | 14.30 | 77.22 |
| 8/13/2013 1:17:27 PM | 2.29083 | 14.30 | 77.21 |
| 8/13/2013 1:17:28 PM | 2.29111 | 14.30 | 77.20 |
| 8/13/2013 1:17:29 PM | 2.29139 | 14.30 | 77.20 |

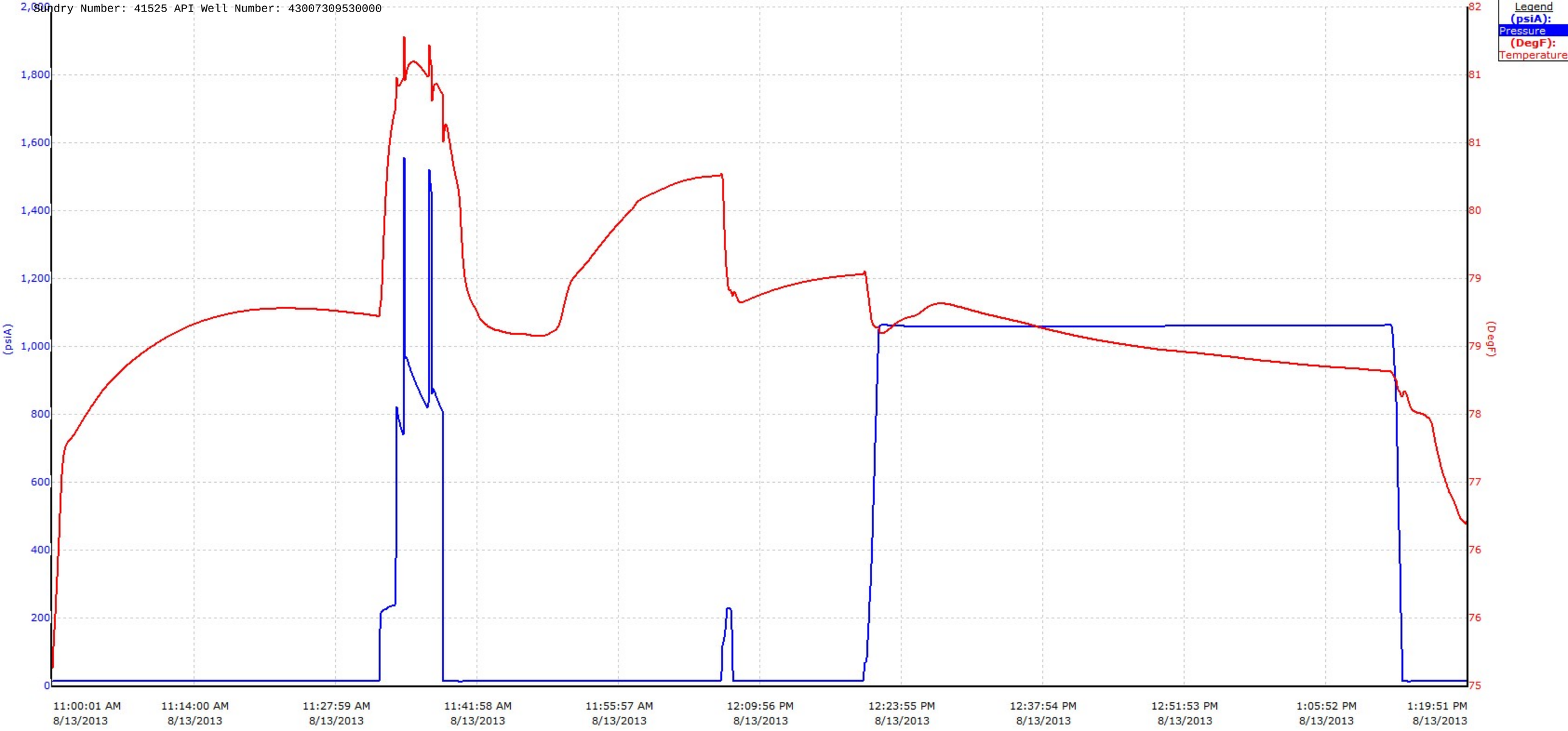
Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:17:30 PM | 2.29167 | 14.30 | 77.19 |
| 8/13/2013 1:17:31 PM | 2.29194 | 14.30 | 77.19 |
| 8/13/2013 1:17:32 PM | 2.29222 | 14.30 | 77.18 |
| 8/13/2013 1:17:33 PM | 2.29250 | 14.30 | 77.18 |
| 8/13/2013 1:17:34 PM | 2.29278 | 14.30 | 77.17 |
| 8/13/2013 1:17:35 PM | 2.29306 | 14.30 | 77.17 |
| 8/13/2013 1:17:36 PM | 2.29333 | 14.30 | 77.16 |
| 8/13/2013 1:17:37 PM | 2.29361 | 14.30 | 77.16 |
| 8/13/2013 1:17:38 PM | 2.29389 | 14.30 | 77.15 |
| 8/13/2013 1:17:39 PM | 2.29417 | 14.30 | 77.15 |
| 8/13/2013 1:17:40 PM | 2.29444 | 14.30 | 77.14 |
| 8/13/2013 1:17:41 PM | 2.29472 | 14.30 | 77.14 |
| 8/13/2013 1:17:42 PM | 2.29500 | 14.30 | 77.13 |
| 8/13/2013 1:17:43 PM | 2.29528 | 14.30 | 77.13 |
| 8/13/2013 1:17:44 PM | 2.29556 | 14.30 | 77.12 |
| 8/13/2013 1:17:45 PM | 2.29583 | 14.30 | 77.12 |
| 8/13/2013 1:17:46 PM | 2.29611 | 14.30 | 77.11 |
| 8/13/2013 1:17:47 PM | 2.29639 | 14.30 | 77.11 |
| 8/13/2013 1:17:48 PM | 2.29667 | 14.30 | 77.10 |
| 8/13/2013 1:17:49 PM | 2.29694 | 14.30 | 77.10 |
| 8/13/2013 1:17:50 PM | 2.29722 | 14.30 | 77.09 |
| 8/13/2013 1:17:51 PM | 2.29750 | 14.30 | 77.09 |
| 8/13/2013 1:17:52 PM | 2.29778 | 14.30 | 77.08 |
| 8/13/2013 1:17:53 PM | 2.29806 | 14.30 | 77.08 |
| 8/13/2013 1:17:54 PM | 2.29833 | 14.30 | 77.07 |
| 8/13/2013 1:17:55 PM | 2.29861 | 14.30 | 77.06 |
| 8/13/2013 1:17:56 PM | 2.29889 | 14.30 | 77.06 |
| 8/13/2013 1:17:57 PM | 2.29917 | 14.30 | 77.06 |
| 8/13/2013 1:17:58 PM | 2.29944 | 14.30 | 77.05 |
| 8/13/2013 1:17:59 PM | 2.29972 | 14.30 | 77.04 |
| 8/13/2013 1:18:00 PM | 2.30000 | 14.30 | 77.04 |
| 8/13/2013 1:18:01 PM | 2.30028 | 14.30 | 77.03 |
| 8/13/2013 1:18:02 PM | 2.30056 | 14.30 | 77.03 |
| 8/13/2013 1:18:03 PM | 2.30083 | 14.30 | 77.02 |
| 8/13/2013 1:18:04 PM | 2.30111 | 14.30 | 77.02 |
| 8/13/2013 1:18:05 PM | 2.30139 | 14.30 | 77.01 |
| 8/13/2013 1:18:06 PM | 2.30167 | 14.30 | 77.01 |
| 8/13/2013 1:18:07 PM | 2.30194 | 14.30 | 77.00 |
| 8/13/2013 1:18:08 PM | 2.30222 | 14.30 | 77.00 |
| 8/13/2013 1:18:09 PM | 2.30250 | 14.30 | 77.00 |
| 8/13/2013 1:18:10 PM | 2.30278 | 14.30 | 76.99 |
| 8/13/2013 1:18:11 PM | 2.30306 | 14.30 | 76.99 |
| 8/13/2013 1:18:12 PM | 2.30333 | 14.30 | 76.98 |
| 8/13/2013 1:18:13 PM | 2.30361 | 14.30 | 76.98 |
| 8/13/2013 1:18:14 PM | 2.30389 | 14.30 | 76.98 |
| 8/13/2013 1:18:15 PM | 2.30417 | 14.30 | 76.98 |
| 8/13/2013 1:18:16 PM | 2.30444 | 14.30 | 76.97 |
| 8/13/2013 1:18:17 PM | 2.30472 | 14.30 | 76.97 |
| 8/13/2013 1:18:18 PM | 2.30500 | 14.30 | 76.97 |
| 8/13/2013 1:18:19 PM | 2.30528 | 14.30 | 76.96 |
| 8/13/2013 1:18:20 PM | 2.30556 | 14.30 | 76.96 |
| 8/13/2013 1:18:21 PM | 2.30583 | 14.30 | 76.96 |
| 8/13/2013 1:18:22 PM | 2.30611 | 14.30 | 76.95 |
| 8/13/2013 1:18:23 PM | 2.30639 | 14.30 | 76.95 |
| 8/13/2013 1:18:24 PM | 2.30667 | 14.30 | 76.95 |
| 8/13/2013 1:18:25 PM | 2.30694 | 14.30 | 76.94 |
| 8/13/2013 1:18:26 PM | 2.30722 | 14.30 | 76.94 |
| 8/13/2013 1:18:27 PM | 2.30750 | 14.30 | 76.94 |
| 8/13/2013 1:18:28 PM | 2.30778 | 14.30 | 76.93 |
| 8/13/2013 1:18:29 PM | 2.30806 | 14.30 | 76.93 |
| 8/13/2013 1:18:30 PM | 2.30833 | 14.30 | 76.92 |
| 8/13/2013 1:18:31 PM | 2.30861 | 14.30 | 76.92 |
| 8/13/2013 1:18:32 PM | 2.30889 | 14.30 | 76.92 |
| 8/13/2013 1:18:33 PM | 2.30917 | 14.30 | 76.91 |
| 8/13/2013 1:18:34 PM | 2.30944 | 14.30 | 76.91 |
| 8/13/2013 1:18:35 PM | 2.30972 | 14.30 | 76.91 |
| 8/13/2013 1:18:36 PM | 2.31000 | 14.30 | 76.90 |
| 8/13/2013 1:18:37 PM | 2.31028 | 14.30 | 76.90 |
| 8/13/2013 1:18:38 PM | 2.31056 | 14.30 | 76.90 |
| 8/13/2013 1:18:39 PM | 2.31083 | 14.30 | 76.89 |
| 8/13/2013 1:18:40 PM | 2.31111 | 14.30 | 76.89 |
| 8/13/2013 1:18:41 PM | 2.31139 | 14.30 | 76.89 |
| 8/13/2013 1:18:42 PM | 2.31167 | 14.30 | 76.88 |

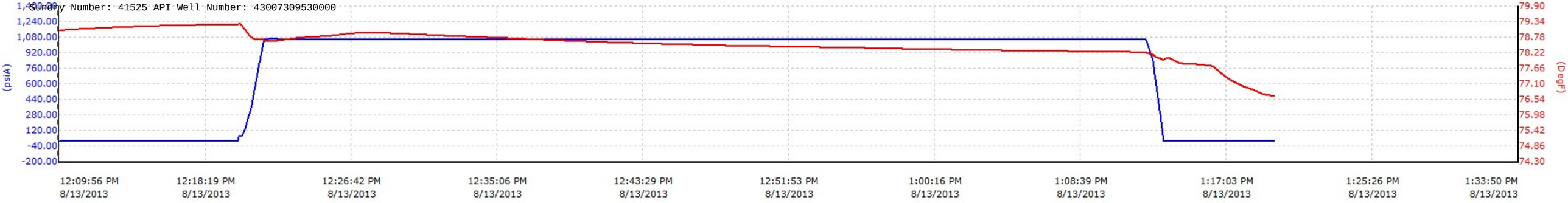
Bill Barrett Corporation

| SN: SH50472 | Elapsed | Pressure | Temperature |
|---|---|---|---|
| Date / Time | hrs | (psiA) | (DegF) |
| 8/13/2013 1:18:43 PM | 2.31194 | 14.30 | 76.88 |
| 8/13/2013 1:18:44 PM | 2.31222 | 14.30 | 76.87 |
| 8/13/2013 1:18:45 PM | 2.31250 | 14.30 | 76.87 |
| 8/13/2013 1:18:46 PM | 2.31278 | 14.30 | 76.86 |
| 8/13/2013 1:18:47 PM | 2.31306 | 14.30 | 76.86 |
| 8/13/2013 1:18:48 PM | 2.31333 | 14.30 | 76.85 |
| 8/13/2013 1:18:49 PM | 2.31361 | 14.30 | 76.85 |
| 8/13/2013 1:18:50 PM | 2.31389 | 14.30 | 76.84 |
| 8/13/2013 1:18:51 PM | 2.31417 | 14.30 | 76.84 |
| 8/13/2013 1:18:52 PM | 2.31444 | 14.30 | 76.83 |
| 8/13/2013 1:18:53 PM | 2.31472 | 14.30 | 76.83 |
| 8/13/2013 1:18:54 PM | 2.31500 | 14.30 | 76.82 |
| 8/13/2013 1:18:55 PM | 2.31528 | 14.30 | 76.81 |
| 8/13/2013 1:18:56 PM | 2.31556 | 14.30 | 76.81 |
| 8/13/2013 1:18:57 PM | 2.31583 | 14.30 | 76.80 |
| 8/13/2013 1:18:58 PM | 2.31611 | 14.30 | 76.80 |
| 8/13/2013 1:18:59 PM | 2.31639 | 14.30 | 76.79 |
| 8/13/2013 1:19:00 PM | 2.31667 | 14.30 | 76.79 |
| 8/13/2013 1:19:01 PM | 2.31694 | 14.30 | 76.78 |
| 8/13/2013 1:19:02 PM | 2.31722 | 14.30 | 76.78 |
| 8/13/2013 1:19:03 PM | 2.31750 | 14.30 | 76.77 |
| 8/13/2013 1:19:04 PM | 2.31778 | 14.30 | 76.77 |
| 8/13/2013 1:19:05 PM | 2.31806 | 14.30 | 76.76 |
| 8/13/2013 1:19:06 PM | 2.31833 | 14.30 | 76.76 |
| 8/13/2013 1:19:07 PM | 2.31861 | 14.30 | 76.75 |
| 8/13/2013 1:19:08 PM | 2.31889 | 14.30 | 76.75 |
| 8/13/2013 1:19:09 PM | 2.31917 | 14.30 | 76.75 |
| 8/13/2013 1:19:10 PM | 2.31944 | 14.30 | 76.74 |
| 8/13/2013 1:19:11 PM | 2.31972 | 14.30 | 76.74 |
| 8/13/2013 1:19:12 PM | 2.32000 | 14.30 | 76.74 |
| 8/13/2013 1:19:13 PM | 2.32028 | 14.30 | 76.73 |
| 8/13/2013 1:19:14 PM | 2.32056 | 14.30 | 76.73 |
| 8/13/2013 1:19:15 PM | 2.32083 | 14.30 | 76.73 |
| 8/13/2013 1:19:16 PM | 2.32111 | 14.30 | 76.73 |
| 8/13/2013 1:19:17 PM | 2.32139 | 14.30 | 76.72 |
| 8/13/2013 1:19:18 PM | 2.32167 | 14.30 | 76.72 |
| 8/13/2013 1:19:19 PM | 2.32194 | 14.30 | 76.72 |
| 8/13/2013 1:19:20 PM | 2.32222 | 14.30 | 76.72 |
| 8/13/2013 1:19:21 PM | 2.32250 | 14.30 | 76.72 |
| 8/13/2013 1:19:22 PM | 2.32278 | 14.30 | 76.71 |
| 8/13/2013 1:19:23 PM | 2.32306 | 14.30 | 76.71 |
| 8/13/2013 1:19:24 PM | 2.32333 | 14.30 | 76.71 |
| 8/13/2013 1:19:25 PM | 2.32361 | 14.30 | 76.71 |
| 8/13/2013 1:19:26 PM | 2.32389 | 14.30 | 76.71 |
| 8/13/2013 1:19:27 PM | 2.32417 | 14.30 | 76.70 |
| 8/13/2013 1:19:28 PM | 2.32444 | 14.30 | 76.70 |
| 8/13/2013 1:19:29 PM | 2.32472 | 14.30 | 76.70 |
| 8/13/2013 1:19:30 PM | 2.32500 | 14.30 | 76.70 |
| 8/13/2013 1:19:31 PM | 2.32528 | 14.30 | 76.70 |
| 8/13/2013 1:19:32 PM | 2.32556 | 14.30 | 76.70 |
| 8/13/2013 1:19:33 PM | 2.32583 | 14.30 | 76.69 |
| 8/13/2013 1:19:34 PM | 2.32611 | 14.30 | 76.69 |
| 8/13/2013 1:19:35 PM | 2.32639 | 14.30 | 76.69 |
| 8/13/2013 1:19:36 PM | 2.32667 | 14.30 | 76.69 |
| 8/13/2013 1:19:37 PM | 2.32694 | 14.30 | 76.69 |
| 8/13/2013 1:19:38 PM | 2.32722 | 14.30 | 76.69 |
| 8/13/2013 1:19:39 PM | 2.32750 | 14.30 | 76.69 |
| 8/13/2013 1:19:40 PM | 2.32778 | 14.30 | 76.68 |
| 8/13/2013 1:19:41 PM | 2.32806 | 14.30 | 76.68 |
| 8/13/2013 1:19:42 PM | 2.32833 | 14.30 | 76.68 |
| 8/13/2013 1:19:43 PM | 2.32861 | 14.30 | 76.68 |
| 8/13/2013 1:19:44 PM | 2.32889 | 14.30 | 76.68 |
| 8/13/2013 1:19:45 PM | 2.32917 | 14.30 | 76.68 |
| 8/13/2013 1:19:46 PM | 2.32944 | 14.30 | 76.68 |
| 8/13/2013 1:19:47 PM | 2.32972 | 14.30 | 76.67 |
| 8/13/2013 1:19:48 PM | 2.33000 | 14.30 | 76.68 |
| 8/13/2013 1:19:49 PM | 2.33028 | 14.30 | 76.68 |
| 8/13/2013 1:19:50 PM | 2.33056 | 14.30 | 76.69 |
| 8/13/2013 1:19:51 PM | 2.33083 | 14.29 | 76.70 |

Sundry Number: 41525 API Well Number: 43007309530000



Sundry Number: 41525 API Well Number: 43007309530000



# United States Department of the Interior

BUREAU OF LAND MANAGEMENT
Utah State Office
440 West 200 South, Suite 500
Salt Lake City, UT 84101
http://www.blm.gov/ut/st/en.html

IN REPLY REFER TO:
3180 (UTU79487X)
UT-922000

AUG 2 8 2013



Mr. Matt Mulverhill
Bill Barrett Corporation
1099 18th Street, Suite 2300
Denver, Colorado 80202

Re: Automatic Contraction
Prickly Pear Unit
Carbon County, Utah

Dear Mr. Mulverhill:

Your letter of August 2, 2013, describes the lands automatically eliminated effective December 31, 2012, from the Prickly Pear Unit Area, located in Carbon County, Utah, pursuant to Section 2(e) of the unit agreement and requests our concurrence. The lands you have described contain 18,487.90 acres more or less, and constitute all legal subdivisions, no parts of which are included in the Prickly Pear Wasatch Mesaverde Participating Area "A-E" and the Prickly Pear Wasatch Mesaverde Participating Area "F". As a result of the automatic contraction, the unit is reduced to 7,139.77 acres.

The following Federal Leases are entirely eliminated from the unit area:

| | | |
|---|---|---|
| UTU01519B | UTU73671 | UTU89234 |
| UTU013064 | UTU74388 | |
| UTU15254 | UTU75035 | |
| UTU65776 | UTU76713* | |
| UTU69095 | UTU77059 | |
| UTU69096 | UTU77060 | |
| UTU72054 | UTU77513 | |
| UTU73666 | UTU79004 | |

*Indicates non-committed lease

The following Federal Leases are partially eliminated from the unit area:

| | | | |
|---|---|---|---|
| UTU0137844 | UTU73006 | UTU73669 | UTU74386 |
| UTU11604 | UTU73665 | UTU73670 | |
| UTU65773 | UTU73668 | UTU73896 | |

You have complied with the requirements of Section 2(e), provided you promptly notify all interested parties. If you have any questions, please contact Judy Nordstrom of this office at (801) 539-4108.

Sincerely,

Roger L. Bankert
Chief, Branch of Minerals

Enclosure

cc: UDOGM
SITLA
ONRR w/Exhibit "B" (Attn: Nancy McCarthy)
BLM FOM – Price (UTG02) w/enclosure

Wells Removed from PPU per BLM 8/28/2013 Letter

| API | Well Name | TWP | RNG | SEC | QTR/QTR |
|---|---|---|---|---|---|
| 4300730823 | PRICKLY PEAR U FED 10-4 | 120S | 140E | 10 | SESE |
| 4300730014 | STONE CABIN FED 1-11 | 120S | 140E | 11 | SWSE |
| 4300716542 | STONE CABIN UNIT 1 | 120S | 140E | 13 | SWNE |
| 4300730825 | PRICKLY PEAR UNIT 13-4 | 120S | 140E | 13 | C-SE |
| 4300731008 | PRICKLY PEAR U FED 5-13-12-14 | 120S | 140E | 13 | SWNW |
| 4300730953 | PRICKLY PEAR U FED 12-24 | 120S | 140E | 24 | SWSW |
| 4300716045 | SHARPLES 1 GOVT PICKRELL | 120S | 150E | 11 | SENW |
| 4300730860 | PRICKLY PEAR U FASSELIN 5-19-12-15 | 120S | 150E | 19 | SWNW |
| 4300715016 | CLAYBANK SPRINGS 33-1A | 120S | 150E | 33 | SWNW |
| 4300730985 | PRICKLY PEAR U FED 7-33D-12-15 | 120S | 150E | 33 | SWNE |
| 4300731226 | PRICKLY PEAR U ST 2-36-12-15 | 120S | 150E | 36 | NWNE |

**Division of Oil, Gas and Mining**

# OPERATOR CHANGE WORKSHEET (for state use only)

**ROUTING**
CDW

**X - Change of Operator (Well Sold)** Operator Name Change/Merger

The operator of the well(s) listed below has changed, effective: **1/1/2014**

| **FROM:** (Old Operator): | **TO:** ( New Operator): |
|---|---|
| N2165-Bill Barrett Corporation | N4040-EnerVest Operating, LLC |
| 1099 18th Street, Suite 230 | 1001 Fannin Street, Suite 800 |
| Denver, CO 80202 | Houston, TX 77002 |
| Phone: 1 (303) 312-8134 | Phone: 1 (713) 659-3500 |

**CA No.** **Unit:** N/A

| WELL NAME | SEC | TWN | RNG | API NO | ENTITY NO | LEASE TYPE | WELL TYPE | WELL STATUS |
|---|---|---|---|---|---|---|---|---|
| See Attached List | | | | | | | | |

## OPERATOR CHANGES DOCUMENTATION

**Enter date after each listed item is completed**

1. (R649-8-10) Sundry or legal documentation was received from the **FORMER** operator on: 1/7/2014
2. (R649-8-10) Sundry or legal documentation was received from the **NEW** operator on: 1/7/2014
3. The new company was checked on the **Department of Commerce, Division of Corporations Database on:** 1/28/2014
4a. Is the new operator registered in the State of Utah: ____ Business Number: 8850806-0161
5a. (R649-9-2)Waste Management Plan has been received on: Not Yet
5b. Inspections of LA PA state/fee well sites complete on: Yes
5c. Reports current for Production/Disposition & Sundries on: 1/24/2014
6. **Federal and Indian Lease Wells:** The BLM and or the BIA has approved the merger, name change, or operator change for all wells listed on Federal or Indian leases on: BLM Not Yet BIA N/A
7. **Federal and Indian Units:**
   The BLM or BIA has approved the successor of unit operator for wells listed on: N/A
8. **Federal and Indian Communization Agreements ("CA"):**
   The BLM or BIA has approved the operator for all wells listed within a CA on: N/A
9. **Underground Injection Control ("UIC")** Division has approved UIC Form 5 Transfer of Authority to **Inject,** for the enhanced/secondary recovery unit/project for the water disposal well(s) listed on: Yes

## DATA ENTRY:

1. Changes entered in the **Oil and Gas Database on:** 1/28/2014
2. Changes have been entered on the **Monthly Operator Change Spread Sheet on:** 1/28/2014
3. Bond information entered in RBDMS on: 1/28/2014
4. Fee/State wells attached to bond in RBDMS on: 1/28/2014
5. Injection Projects to new operator in RBDMS on: 1/28/2014
6. Receipt of Acceptance of Drilling Procedures for APD/New on: 1/7/2014
7. Surface Agreement Sundry from **NEW** operator on Fee Surface wells received on: 1/7/2014

## BOND VERIFICATION:

1. Federal well(s) covered by Bond Number: RLB7886
2. Indian well(s) covered by Bond Number: RLB7886
3a. (R649-3-1) The **NEW** operator of any state/fee well(s) listed covered by Bond Number B008371
3b. The **FORMER** operator has requested a release of liability from their bond on: N/A

## LEASE INTEREST OWNER NOTIFICATION:

4. (R649-2-10) The **NEW** operator of the fee wells has been contacted and informed by a letter from the Division of their responsibility to notify all interest owners of this change on: 1/28/2014

**COMMENTS:**

Bill Barrett Corporation (N2165) to EnerVest Operating, LLC (N4040)
Effective 1/1/2014

| Well Name | Sec | TWN | RNG | API Number | Entity | Mineral Lease | Surface Lease | Well Type | Well Status |
|---|---|---|---|---|---|---|---|---|---|
| JACK CANYON UNIT 8-32 | 32 | 120S | 160E | 4300730460 | 15167 | State | State | WI | A |
| PRICKLY PEAR U FED 10-4 | 10 | 120S | 140E | 4300730823 | 14462 | Federal | Federal | WI | A |
| JACK CYN U ST 14-32 | 32 | 120S | 160E | 4300730913 | 15166 | State | State | WD | A |
| PRICKLY PEAR U FED 12-24 | 24 | 120S | 140E | 4300730953 | 14467 | Federal | Federal | WD | A |
| HORSE BENCH FED 4-27D-12-16 | 27 | 120S | 160E | 4300750092 | | Federal | Federal | GW | APD |
| HORSE BENCH FED 5-27D-12-16 | 27 | 120S | 160E | 4300750093 | | Federal | Federal | GW | APD |
| HORSE BENCH FED 4-20D-12-17 | 19 | 120S | 170E | 4300750350 | | Federal | Federal | GW | APD |
| Horse Bench Federal 16-18D-12-17 | 19 | 120S | 170E | 4300750351 | | Federal | Federal | GW | APD |
| SHARPLES 1 GOVT PICKRELL | 11 | 120S | 150E | 4300716045 | 7030 | Federal | Federal | GW | P |
| STONE CABIN UNIT 1 | 13 | 120S | 140E | 4300716542 | 12052 | Federal | Federal | GW | P |
| STONE CABIN FED 1-11 | 11 | 120S | 140E | 4300730014 | 6046 | Federal | Federal | GW | P |
| JACK CANYON 101-A | 33 | 120S | 160E | 4300730049 | 2455 | Federal | Federal | GW | P |
| PETERS POINT ST 2-2-13-16 | 2 | 130S | 160E | 4300730521 | 14387 | State | State | GW | P |
| HUNT RANCH 3-4 | 3 | 120S | 150E | 4300730775 | 13158 | State | Fee | GW | P |
| PRICKLY PEAR UNIT 13-4 | 13 | 120S | 140E | 4300730825 | 14353 | Federal | Federal | GW | P |
| PETERS POINT ST 4-2-13-16 | 2 | 130S | 160E | 4300730866 | 14386 | State | State | GW | P |
| PRICKLY PEAR U FED 5-13-12-14 | 13 | 120S | 140E | 4300731008 | 14897 | Federal | Federal | GW | P |
| PETERS POINT ST 5-2D-13-16 DEEP | 2 | 130S | 160E | 4300731056 | 15909 | State | State | GW | P |
| PRICKLY PEAR U ST 2-36-12-15 | 36 | 120S | 150E | 4300731226 | 15719 | State | State | GW | P |
| PP ST 8-2D-13-16 (DEEP) | 2 | 130S | 160E | 4300731280 | 16069 | State | State | GW | P |
| PETERS POINT U FED 14-27D-12-16 | 27 | 120S | 160E | 4300750068 | 18204 | Federal | Federal | GW | P |
| PRICKLY PEAR U FASSELIN 5-19-12-15 | 19 | 120S | 150E | 4300730860 | 14853 | Fee | Fee | GW | PA |
| PETERS POINT ST 6-2D-13-16 | 2 | 130S | 160E | 4300731017 | 14472 | State | State | D | PA |
| PRICKLY PEAR U FED 7-33D-12-15 | 33 | 120S | 150E | 4300730985 | 14771 | Federal | Federal | GW | S |
| PETERS POINT ST 8-2D-13-16 | 2 | 130S | 160E | 4300731016 | 14471 | State | State | GW | S |

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

UIC FORM 5

# TRANSFER OF AUTHORITY TO INJECT

| | |
|---|---|
| Well Name and Number: PRICKLY PEAR U FED | API Number: 12-24 43-607-30953 |
| Location of Well: Footage : 1271 FSL 0483 FWL; QQ, Section, Township, Range: SWSW 24 12S 14E; County : CARBON; State : UTAH | Field or Unit Name: NINE MILE CANYON/PRICKLY PEA; Lease Designation and Number: UTU-77513 |

**EFFECTIVE DATE OF TRANSFER:** 1/1/2014

**CURRENT OPERATOR**

Company: BILL BARRETT CORP
Address: 1099 18th Street Ste 2300
city DENVER state CO zip 80202
Phone: (303) 293-9100
Comments:

Name: DUANE ZAVADIL
Signature: [signature]
Title: Senior Vice President - EH&S, Government and Regulatory Affairs
Date: 12/10/2013

**NEW OPERATOR**

Company: EnerVest Operating, L.L.C.
Address: 1001 Fannin, Suite 800
city Houston state TX zip 77002
Phone: (713) 659-3500
Comments:

Name: RONNIE YOUNG
Signature: [signature]
Title: DIRECTOR - REGULATORY
Date: 12/10/2013

(This space for State use only)

Transfer approved by: [signature]
Title: UIC Manager

Approval Date: 1/22/14

RECEIVED
JAN 07 2014
DIV. OF OIL, GAS & MINING

Comments:

(5/2000)

COPY

FORM 9

**STATE OF UTAH**
DEPARTMENT OF NATURAL RESOURCES
DIVISION OF OIL, GAS AND MINING

5. LEASE DESIGNATION AND SERIAL NUMBER: (see attached well list)

## SUNDRY NOTICES AND REPORTS ON WELLS

6. IF INDIAN, ALLOTTEE OR TRIBE NAME: N/A

7. UNIT or CA AGREEMENT NAME:

Do not use this form for proposals to drill new wells, significantly deepen existing wells below current bottom-hole depth, reenter plugged wells, or to drill horizontal laterals. Use APPLICATION FOR PERMIT TO DRILL form for such proposals.

1. TYPE OF WELL: OIL WELL ☐ GAS WELL ☐ OTHER _____

8. WELL NAME and NUMBER: (see attached well list)

2. NAME OF OPERATOR: ENERVEST OPERATING, LLC

9. API NUMBER:

3. ADDRESS OF OPERATOR: 1001 FANNIN, ST. STE 800 CITY HOUSTON STATE TX ZIP 77002

PHONE NUMBER: (713) 659-3500

10. FIELD AND POOL, OR WILDCAT:

4. LOCATION OF WELL

FOOTAGES AT SURFACE: (see attached well list)

COUNTY:

QTR/QTR, SECTION, TOWNSHIP, RANGE, MERIDIAN:

STATE: UTAH

11. CHECK APPROPRIATE BOXES TO INDICATE NATURE OF NOTICE, REPORT, OR OTHER DATA

| TYPE OF SUBMISSION | TYPE OF ACTION | | |
|---|---|---|---|
| ☑ NOTICE OF INTENT (Submit in Duplicate) | ☐ ACIDIZE | ☐ DEEPEN | ☐ REPERFORATE CURRENT FORMATION |
| Approximate date work will start: 1/1/2014 | ☐ ALTER CASING | ☐ FRACTURE TREAT | ☐ SIDETRACK TO REPAIR WELL |
| | ☐ CASING REPAIR | ☐ NEW CONSTRUCTION | ☐ TEMPORARILY ABANDON |
| | ☐ CHANGE TO PREVIOUS PLANS | ☑ OPERATOR CHANGE | ☐ TUBING REPAIR |
| | ☐ CHANGE TUBING | ☐ PLUG AND ABANDON | ☐ VENT OR FLARE |
| ☐ SUBSEQUENT REPORT (Submit Original Form Only) | ☐ CHANGE WELL NAME | ☐ PLUG BACK | ☐ WATER DISPOSAL |
| Date of work completion: | ☐ CHANGE WELL STATUS | ☐ PRODUCTION (START/RESUME) | ☐ WATER SHUT-OFF |
| | ☐ COMMINGLE PRODUCING FORMATIONS | ☐ RECLAMATION OF WELL SITE | ☐ OTHER: _____ |
| | ☐ CONVERT WELL TYPE | ☐ RECOMPLETE - DIFFERENT FORMATION | |

12. DESCRIBE PROPOSED OR COMPLETED OPERATIONS. Clearly show all pertinent details including dates, depths, volumes, etc.

ENERVEST OPERATING, LLC IS SUBMITTING THIS SUNDRY AS NOTIFICATION THAT THE WELLS LISTED ON THE ATTACHED LIST HAVE BEEN SOLD TO ENERVEST OPERATING, LLC BY BILL BILL BARRETT CORPORATION EFFECTIVE 1/1/2014. PLEASE REFER ALL FUTURE CORRESPONDENCE TO THE ADDRESS BELOW.

EnerVest Operating, L.L.C.
1001 Fannin, Suite 800
Houston, Texas 77002
713-659-3500
(BLM BOND # RLB 7886, STATE/FEE BOND # B008371)

BILL BARRETT CORPORATION

Duane Zavadil NAME (PLEASE PRINT)

SIGNATURE

Senior Vice President -
EH&S, Government and Regulatory Affairs N2165

ENERVEST OPERATING, LLC

Ronnie L Young NAME (PLEASE PRINT)

Ronnie L Young SIGNATURE

DIRECTOR - REGULATORY
N4040

NAME (PLEASE PRINT) RONNIE YOUNG TITLE DIRECTOR - REGULATORY

SIGNATURE Ronnie L Young DATE 12/10/2013

(This space for State use only)

APPROVED

JAN 28 2014

DIV. OIL, GAS & MINING

BY: Rachel Medina

RECEIVED

JAN 07 2014

DIV. OF OIL, GAS & MINING

(5/2000) (See Instructions on Reverse Side)

UDOGM CHANGE OF OPERATOR WELL LIST

| Well Name | Sec | TWN | RNG | API Number | Entity | Lease | Well Type | Well Status | Unit |
|---|---|---|---|---|---|---|---|---|---|
| JACK CANYON UNIT 8-32 | 32 | 120S | 160E | 4300730460 | 15167 | State | WI | A | |
| JACK CYN U ST 14-32 | 32 | 120S | 160E | 4300730913 | 15166 | State | WD | A | |
| PRICKLY PEAR U FED 12-24 | 24 | 120S | 140E | 4300730953 | 14467 | Federal | WD | A | |
| PPU FED 11-23D-12-15 | 23 | 120S | 150E | 4300731440 | | Federal | GW | APD | PRICKLY PEAR |
| PPU FED 4-26D-12-15 | 23 | 120S | 150E | 4300731441 | | Federal | GW | APD | PRICKLY PEAR |
| PPU FED 14-23D-12-15 | 23 | 120S | 150E | 4300731442 | | Federal | GW | APD | PRICKLY PEAR |
| PPU FED 12-23D-12-15 | 23 | 120S | 150E | 4300731443 | | Federal | GW | APD | PRICKLY PEAR |
| PPU FED 11-34D-12-16 | 34 | 120S | 160E | 4300731465 | | Federal | GW | APD | PETERS POINT |
| PPU FED 10-34D-12-16 | 34 | 120S | 160E | 4300731469 | | Federal | GW | APD | PETERS POINT |
| HORSE BENCH FED 4-27D-12-16 | 27 | 120S | 160E | 4300750092 | | Federal | GW | APD | |
| HORSE BENCH FED 5-27D-12-16 | 27 | 120S | 160E | 4300750093 | | Federal | GW | APD | |
| PRICKLY PEAR U FED 12-7D-12-15 | 07 | 120S | 150E | 4300750094 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR U FED 11-7D-12-15 | 07 | 120S | 150E | 4300750095 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR U FED 13-7D-12-15 | 07 | 120S | 150E | 4300750096 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR U FED 14-7D-12-15 | 07 | 120S | 150E | 4300750097 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11-8D-12-15 | 08 | 120S | 150E | 4300750124 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 12-8D-12-15 | 08 | 120S | 150E | 4300750125 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 13-8D-12-15 | 08 | 120S | 150E | 4300750126 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 14-8D-12-15 | 08 | 120S | 150E | 4300750127 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9-21D-12-15 | 21 | 120S | 150E | 4300750128 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-21D-12-15 | 21 | 120S | 150E | 4300750129 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10-21D-12-15 | 21 | 120S | 150E | 4300750130 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10A-21D-12-15 | 21 | 120S | 150E | 4300750131 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-21D-12-15 | 21 | 120S | 150E | 4300750132 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15X-21D-12-15 | 21 | 120S | 150E | 4300750133 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16-21D-12-15 | 21 | 120S | 150E | 4300750134 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-21D-12-15 | 21 | 120S | 150E | 4300750135 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 13A-22D-12-15 | 21 | 120S | 150E | 4300750148 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 1A-27D-12-15 | 22 | 120S | 150E | 4300750161 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 2A-27D-12-15 | 22 | 120S | 150E | 4300750162 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 3A-27D-12-15 | 22 | 120S | 150E | 4300750163 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-22D-12-15 | 22 | 120S | 150E | 4300750164 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10A-22D-12-15 | 22 | 120S | 150E | 4300750165 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11A-22D-12-15 | 22 | 120S | 150E | 4300750166 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 12A-22D-12-15 | 22 | 120S | 150E | 4300750167 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 14A-22D-12-15 | 22 | 120S | 150E | 4300750168 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-22D-12-15 | 22 | 120S | 150E | 4300750169 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-22D-12-15 | 22 | 120S | 150E | 4300750170 | | Federal | GW | APD | PRICKLY PEAR |
| PETERS POINT UF 15X-36D-12-16 | 36 | 120S | 160E | 4300750178 | | Federal | GW | APD | PETERS POINT |
| PRICKLY PEAR UF 15A-15D-12-15 | 15 | 120S | 150E | 4300750180 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11B-15D-12-15 | 15 | 120S | 150E | 4300750181 | | Federal | GW | APD | PRICKLY PEAR |
| PETERS POINT UF 10-1D-13-16 | 36 | 120S | 160E | 4300750182 | | Federal | GW | APD | PETERS POINT |
| PETERS POINT UF 9-1D-13-16 | 36 | 120S | 160E | 4300750183 | | Federal | GW | APD | PETERS POINT |
| PRICKLY PEAR UF 16A-15D-12-15 | 15 | 120S | 150E | 4300750184 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 3A-18D-12-15 | 07 | 120S | 150E | 4300750185 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 4A-18D-12-15 | 07 | 120S | 150E | 4300750186 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11A-7D-12-15 | 07 | 120S | 150E | 4300750187 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 2-18D-12-15 | 07 | 120S | 150E | 4300750188 | | Federal | GW | APD | PRICKLY PEAR |

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|---|---|---|---|---|---|---|---|---|
| PRICKLY PEAR UF 12A-7D-12-15 | 07 | 120S | 150E | 4300750189 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 13A-7D-12-15 | 07 | 120S | 150E | 4300750190 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 14A-7D-12-15 | 07 | 120S | 150E | 4300750191 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR FEDERAL 1-12D-12-14 | 12 | 120S | 140E | 4300750205 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 2-12D-12-14 | 12 | 120S | 140E | 4300750206 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7-12D-12-14 | 12 | 120S | 140E | 4300750207 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7A-12D-12-14 | 12 | 120S | 140E | 4300750208 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8-12D-12-14 | 12 | 120S | 140E | 4300750209 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 4-7D-12-15 | 12 | 120S | 140E | 4300750210 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 5-7D-12-15 | 12 | 120S | 140E | 4300750211 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8A-12D-12-14 | 12 | 120S | 140E | 4300750212 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 5A-7D-12-15 | 12 | 120S | 140E | 4300750213 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7-14D-12-15 | 14 | 120S | 150E | 4300750214 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7A-14D-12-15 | 14 | 120S | 150E | 4300750215 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9-14D-12-15 | 14 | 120S | 150E | 4300750217 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-14D-12-15 | 14 | 120S | 150E | 4300750218 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10-14D-12-15 | 14 | 120S | 150E | 4300750219 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10A-14D-12-15 | 14 | 120S | 150E | 4300750220 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-14D-12-15 | 14 | 120S | 150E | 4300750222 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16-14D-12-15 | 14 | 120S | 150E | 4300750223 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-14D-12-15 | 14 | 120S | 150E | 4300750224 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 1A-18D-12-15 | 07 | 120S | 150E | 4300750225 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 2A-18D-12-15 | 07 | 120S | 150E | 4300750226 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-7D-12-15 | 07 | 120S | 150E | 4300750227 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10A-7D-12-15 | 07 | 120S | 150E | 4300750228 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-7D-12-15 | 07 | 120S | 150E | 4300750229 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-7D-12-15 | 07 | 120S | 150E | 4300750230 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-12D-12-14 | 12 | 120S | 140E | 4300750233 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10A-12D-12-14 | 12 | 120S | 140E | 4300750234 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-12D-12-14 | 12 | 120S | 140E | 4300750235 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 12A-8D-12-15 | 08 | 120S | 150E | 4300750236 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-12D-12-14 | 12 | 120S | 140E | 4300750237 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11A-8D-12-15 | 08 | 120S | 150E | 4300750238 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 13A-8D-12-15 | 08 | 120S | 150E | 4300750239 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 14A-8D-12-15 | 08 | 120S | 150E | 4300750240 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 5A-8D-12-15 | 08 | 120S | 150E | 4300750260 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6A-8D-12-15 | 08 | 120S | 150E | 4300750261 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 4-8D-12-15 | 08 | 120S | 150E | 4300750262 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 3-8D-12-15 | 08 | 120S | 150E | 4300750263 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 2-8D-12-15 | 08 | 120S | 150E | 4300750264 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7A-8D-12-15 | 08 | 120S | 150E | 4300750265 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7-8D-12-15 | 08 | 120S | 150E | 4300750266 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 5-8D-12-15 | 08 | 120S | 150E | 4300750267 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6-8D-12-15 | 08 | 120S | 150E | 4300750268 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10A-8D-12-15 | 08 | 120S | 150E | 4300750269 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-8D-12-15 | 08 | 120S | 150E | 4300750270 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8-8D-12-15 | 08 | 120S | 150E | 4300750271 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 1-8D-12-15 | 08 | 120S | 150E | 4300750272 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8A-8D-12-15 | 08 | 120S | 150E | 4300750273 | Federal | GW | APD | PRICKLY PEAR |

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|---|---|---|---|---|---|---|---|
| PRICKLY PEAR UF 5-9D-12-15 | 09 | 120S | 150E | 4300750274 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 5A-9D-12-15 | 09 | 120S | 150E | 4300750275 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 4-9D-12-15 | 09 | 120S | 150E | 4300750276 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 3-9D-12-15 | 09 | 120S | 150E | 4300750277 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6A-9D-12-15 | 09 | 120S | 150E | 4300750278 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11-9D-12-15 | 09 | 120S | 150E | 4300750279 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 12A-9D-12-15 | 09 | 120S | 150E | 4300750280 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6-9D-12-15 | 09 | 120S | 150E | 4300750281 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11A-9D-12-15 | 09 | 120S | 150E | 4300750282 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR US 1X-16D-12-15 | 10 | 120S | 150E | 4300750283 | State | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 5A-15D-12-15 | 10 | 120S | 150E | 4300750284 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6A-15D-12-15 | 10 | 120S | 150E | 4300750285 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 3-15D-13-15 | 10 | 120S | 150E | 4300750286 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-10D-12-15 | 15 | 120S | 150E | 4300750287 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 13-10D-12-15 | 10 | 120S | 150E | 4300750288 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15-10D-12-15 | 15 | 120S | 150E | 4300750289 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-10D-12-15 | 15 | 120S | 150E | 4300750290 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9-10D-12-15 | 15 | 120S | 150E | 4300750291 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 14A-10D-12-15 | 10 | 120S | 150E | 4300750292 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10-10D-12-15 | 15 | 120S | 150E | 4300750293 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16-10D-12-15 | 15 | 120S | 150E | 4300750294 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 13-11D-12-15 | 15 | 120S | 150E | 4300750295 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 13A-11D-12-15 | 15 | 120S | 150E | 4300750296 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 12-11D-12-15 | 15 | 120S | 150E | 4300750297 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 13A-10D-12-15 | 10 | 120S | 150E | 4300750298 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 12-10D-12-15 | 10 | 120S | 150E | 4300750299 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11-10D-12-15 | 10 | 120S | 150E | 4300750300 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 3A-15D-12-15 | 10 | 120S | 150E | 4300750301 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 12-14D-12-15 | 14 | 120S | 150E | 4300750302 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 4-15D-12-15 | 10 | 120S | 150E | 4300750303 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 4A-15D-12-15 | 10 | 120S | 150E | 4300750304 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 14-10D-12-15 | 10 | 120S | 150E | 4300750305 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-17D-12-15 | 17 | 120S | 150E | 4300750306 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8A-17D-12-15 | 17 | 120S | 150E | 4300750307 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10A-17D-12-15 | 17 | 120S | 150E | 4300750308 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 3-7D-12-15 | 07 | 120S | 150E | 4300750309 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-17D-12-15 | 17 | 120S | 150E | 4300750310 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6-7D-12-15 | 07 | 120S | 150E | 4300750311 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-17D-12-15 | 17 | 120S | 150E | 4300750312 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6A-7D-12-15 | 07 | 120S | 150E | 4300750313 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7A-7D-12-15 | 07 | 120S | 150E | 4300750314 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8A-7D-12-15 | 07 | 120S | 150E | 4300750315 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6X-17D-12-15 | 17 | 120S | 150E | 4300750316 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11A-17D-12-15 | 17 | 120S | 150E | 4300750317 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15B-17D-12-15 | 17 | 120S | 150E | 4300750318 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8A-20D-12-15 | 20 | 120S | 150E | 4300750319 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 1-7D-12-15 | 07 | 120S | 150E | 4300750320 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7A-20D-12-15 | 20 | 120S | 150E | 4300750321 | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-20D-12-15 | 20 | 120S | 150E | 4300750322 | Federal | GW | APD | PRICKLY PEAR |

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|---|---|---|---|---|---|---|---|---|
| PRICKLY PEAR UF 10A-20D-12-15 | 20 | 120S | 150E | 4300750323 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 10-20D-12-15 | 20 | 120S | 150E | 4300750324 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 2-7D-12-15 | 07 | 120S | 150E | 4300750325 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 14A-20D-12-15 | 20 | 120S | 150E | 4300750326 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-20D-12-15 | 20 | 120S | 150E | 4300750327 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-20D-12-15 | 20 | 120S | 150E | 4300750328 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8-7D-12-15 | 07 | 120S | 150E | 4300750329 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 15-20D-12-15 | 20 | 120S | 150E | 4300750330 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7-7D-12-15 | 07 | 120S | 150E | 4300750331 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6-10D-12-15 | 09 | 120S | 150E | 4300750332 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 5A-10D-12-15 | 09 | 120S | 150E | 4300750333 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 11A-10D-12-15 | 09 | 120S | 150E | 4300750334 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 6A-10D-12-15 | 09 | 120S | 150E | 4300750335 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 5-10D-12-15 | 09 | 120S | 150E | 4300750336 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 12A-10D-12-15 | 09 | 120S | 150E | 4300750338 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 3-10D-12-15 | 09 | 120S | 150E | 4300750339 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 4-10D-12-15 | 09 | 120S | 150E | 4300750340 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8-9D-12-15 | 09 | 120S | 150E | 4300750341 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 8A-9D-12-15 | 09 | 120S | 150E | 4300750342 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7A-9D-12-15 | 09 | 120S | 150E | 4300750343 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 7-9D-12-15 | 09 | 120S | 150E | 4300750344 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 1-9D-12-15 | 09 | 120S | 150E | 4300750345 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 2-9D-12-15 | 09 | 120S | 150E | 4300750346 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 1-24D-12-1 | 24 | 120S | 150E | 4300750348 | | Federal | GW | APD | PRICKLY PEAR |
| PRICKLY PEAR UF 9-13D-12-15 | 13 | 120S | 150E | 4300750349 | | Federal | GW | APD | PRICKLY PEAR |
| HORSE BENCH FED 4-20D-12-17 | 19 | 120S | 170E | 4300750350 | | Federal | GW | APD | |
| Horse Bench Federal 16-18D-12-17 | 19 | 120S | 170E | 4300750351 | | Federal | GW | APD | |
| PPU FED 9-34D-12-16 | 34 | 120S | 160E | 4300731430 | 17225 | Federal | GW | OPS | PETERS POINT |
| PPU FED 15-35D-12-16 | 35 | 120S | 160E | 4300731475 | 2470 | Federal | GW | OPS | PETERS POINT |
| PETERS POINT U FED 12A-6D-13-17 | 31 | 120S | 170E | 4300750034 | 2470 | Federal | GW | OPS | PETERS POINT |
| PETERS POINT U FED 11A-31D-12-17 | 31 | 120S | 170E | 4300750036 | 2470 | Federal | GW | OPS | PETERS POINT |
| PRICKLY PEAR U FED 7-21D-12-15 | 21 | 120S | 150E | 4300750055 | 14794 | Federal | GW | OPS | PRICKLY PEAR |
| PETERS POINT U FED 9-6D-13-17 | 06 | 130S | 170E | 4300750120 | 2470 | Federal | GW | OPS | PETERS POINT |
| PETERS POINT U FED 14-6D-13-17 | 06 | 130S | 170E | 4300750121 | 2470 | Federal | GW | OPS | PETERS POINT |
| PETERS POINT U FED 15-6D-13-17 | 06 | 130S | 170E | 4300750122 | 2470 | Federal | GW | OPS | PETERS POINT |
| PETERS POINT UF 2-7D-13-17 | 06 | 130S | 170E | 4300750149 | 2470 | Federal | GW | OPS | PETERS POINT |
| PETERS POINT UF 1-7D-13-17 | 06 | 130S | 170E | 4300750150 | 2470 | Federal | GW | OPS | PETERS POINT |
| PRICKLY PEAR US 1A-16D-12-15 | 09 | 120S | 150E | 4300750192 | 14794 | State | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR US 2A-16D-12-15 | 09 | 120S | 150E | 4300750193 | 14794 | State | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR US 2-16D-12-15 | 09 | 120S | 150E | 4300750194 | 14794 | State | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-9D-12-15 | 09 | 120S | 150E | 4300750196 | 14794 | Federal | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR UF 10-9D-12-15 | 09 | 120S | 150E | 4300750197 | 14794 | Federal | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR UF 10A-9D-12-15 | 09 | 120S | 150E | 4300750198 | 14794 | Federal | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR UF 14-9D-12-15 | 09 | 120S | 150E | 4300750199 | 14794 | Federal | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR UF 14A-9D-12-15 | 09 | 120S | 150E | 4300750200 | 14794 | Federal | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR UF 15-9D-12-15 | 09 | 120S | 150E | 4300750201 | 14794 | Federal | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-9D-12-15 | 09 | 120S | 150E | 4300750203 | 14794 | Federal | GW | OPS | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-9D-12-15 | 09 | 120S | 150E | 4300750204 | 14794 | Federal | GW | OPS | PRICKLY PEAR |
| SHARPLES 1 GOVT PICKRELL | 11 | 120S | 150E | 4300716045 | 7030 | Federal | GW | P | |

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| STONE CABIN UNIT 1 | 13 | 120S | 140E | 4300716542 | 12052 | Federal | GW | P | |
| STONE CABIN FED 1-11 | 11 | 120S | 140E | 4300730014 | 6046 | Federal | GW | P | |
| STONE CABIN FED 2-B-27 | 27 | 120S | 150E | 4300730018 | 14794 | Federal | GW | P | PRICKLY PEAR |
| JACK CANYON 101-A | 33 | 120S | 160E | 4300730049 | 2455 | Federal | GW | P | |
| PETERS POINT ST 2-2-13-16 | 02 | 130S | 160E | 4300730521 | 14387 | State | GW | P | |
| PRICKLY PEAR ST 16-15 | 16 | 120S | 150E | 4300730522 | 14794 | State | GW | P | PRICKLY PEAR |
| PETERS POINT U FED 36-2 | 36 | 120S | 160E | 4300730761 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 36-3 | 36 | 120S | 160E | 4300730762 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 36-4 | 36 | 120S | 160E | 4300730763 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 14-25D-12-16 | 36 | 120S | 160E | 4300730764 | 2470 | Federal | GW | P | PETERS POINT |
| HUNT RANCH 3-4 | 03 | 120S | 150E | 4300730775 | 13158 | State | GW | P | |
| PETERS POINT U FED 4-31D-12-17 | 36 | 120S | 160E | 4300730810 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 16-26D-12-16 | 36 | 120S | 160E | 4300730812 | 2470 | Federal | GW | P | PETERS POINT |
| PRICKLY PEAR UNIT 13-4 | 13 | 120S | 140E | 4300730825 | 14353 | Federal | GW | P | |
| PRICKLY PEAR UNIT 21-2 | 21 | 120S | 150E | 4300730828 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PETERS POINT U FED 6-7D-13-17 | 06 | 130S | 170E | 4300730859 | 14692 | Federal | GW | P | PETERS POINT |
| PETERS POINT ST 4-2-13-16 | 02 | 130S | 160E | 4300730866 | 14386 | State | GW | P | |
| PRICKLY PEAR U ST 13-16 | 16 | 120S | 150E | 4300730933 | 14794 | State | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U ST 11-16 | 16 | 120S | 150E | 4300730944 | 14794 | State | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U ST 7-16 | 16 | 120S | 150E | 4300730945 | 14794 | State | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 7-25 | 25 | 120S | 150E | 4300730954 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PETERS POINT U FED 16-35 | 35 | 120S | 160E | 4300730965 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 11-6-13-17 | 06 | 130S | 170E | 4300730982 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 16-6D-13-17 | 06 | 130S | 170E | 4300731004 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 16-31D-12-17 | 06 | 130S | 170E | 4300731005 | 2470 | Federal | GW | P | PETERS POINT |
| PRICKLY PEAR U FED 5-13-12-14 | 13 | 120S | 140E | 4300731008 | 14897 | Federal | GW | P | |
| PETERS POINT U FED 12-31D-12-17 | 36 | 120S | 160E | 4300731009 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 2-36D-12-16 | 36 | 120S | 160E | 4300731010 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 9-36-12-16 | 36 | 120S | 160E | 4300731011 | 2470 | Federal | GW | P | PETERS POINT |
| PRICKLY PEAR U ST 36-06 | 36 | 120S | 150E | 4300731018 | 14794 | State | GW | P | PRICKLY PEAR |
| PETERS POINT U FED 8-35D-12-16 | 36 | 120S | 160E | 4300731024 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 4-12D-13-16 | 02 | 130S | 160E | 4300731049 | 14692 | Federal | GW | P | PETERS POINT |
| PETERS POINT ST 5-2D-13-16 DEEP | 02 | 130S | 160E | 4300731056 | 15909 | State | GW | P | |
| PRICKLY PEAR U FED 13-23-12-15 | 23 | 120S | 150E | 4300731073 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 1-27D-12-15 | 23 | 120S | 150E | 4300731074 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 3-26D-12-15 | 23 | 120S | 150E | 4300731075 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 15-22D-12-15 | 23 | 120S | 150E | 4300731076 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 3-28D-12-15 | 21 | 120S | 150E | 4300731121 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PETERS POINT U FED 2-12D-13-16 | 06 | 130S | 170E | 4300731158 | 14692 | Federal | GW | P | PETERS POINT |
| PRICKLY PEAR U FED 15-21-12-15 | 21 | 120S | 150E | 4300731164 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 7-28D-12-15 | 21 | 120S | 150E | 4300731165 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 13-21D-12-15 | 21 | 120S | 150E | 4300731166 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PETERS POINT U FED 10-36D-12-16 | 36 | 120S | 160E | 4300731174 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 12-36D-12-16 | 36 | 120S | 160E | 4300731175 | 2470 | Federal | GW | P | PETERS POINT |
| PRICKLY PEAR U FED 15-17-12-15 | 17 | 120S | 150E | 4300731183 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 11-17D-12-15 | 17 | 120S | 150E | 4300731184 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 7-22D-12-15 | 22 | 120S | 150E | 4300731186 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 3-22-12-15 | 22 | 120S | 150E | 4300731187 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 5-22D-12-15 | 22 | 120S | 150E | 4300731188 | 14794 | Federal | GW | P | PRICKLY PEAR |

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| PRICKLY PEAR 11-15D-12-15 | 22 | 120S | 150E | 4300731189 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 9-18D-12-15 | 18 | 120S | 150E | 4300731192 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 15-18-12-15 | 18 | 120S | 150E | 4300731193 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 16-27D-12-15 | 27 | 120S | 150E | 4300731194 | 15569 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 12-27D-12-15 | 27 | 120S | 150E | 4300731195 | 15568 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 10-27-12-15 | 27 | 120S | 150E | 4300731196 | 15570 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 9-20D-12-15 | 20 | 120S | 150E | 4300731197 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 7-20-12-15 | 20 | 120S | 150E | 4300731198 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 1-20-12-15 | 20 | 120S | 150E | 4300731206 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U ST 2-36-12-15 | 36 | 120S | 150E | 4300731226 | 15719 | State | GW | P | |
| PRICKLY PEAR U ST 4-36-12-15 | 36 | 120S | 150E | 4300731227 | 14794 | State | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 4-27D-12-15 | 22 | 120S | 150E | 4300731237 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 13-22-12-15 | 22 | 120S | 150E | 4300731238 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 3-27D-12-15 | 22 | 120S | 150E | 4300731239 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U ST 9-16-12-15 | 16 | 120S | 150E | 4300731240 | 14794 | State | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 9-28D-12-15 | 28 | 120S | 150E | 4300731241 | 16028 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 5-27D-12-15 | 28 | 120S | 150E | 4300731242 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 1-28-12-15 | 28 | 120S | 150E | 4300731243 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 8-28D-12-15 | 28 | 120S | 150E | 4300731244 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U ST 1-16-12-15 | 16 | 120S | 150E | 4300731245 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU FED 11-18D-12-15 | 18 | 120S | 150E | 4300731257 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 11-20D-12-15 | 20 | 120S | 150E | 4300731258 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 4-25D-12-15 | 25 | 120S | 150E | 4300731259 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 12-25D-12-15 | 25 | 120S | 150E | 4300731260 | 16068 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 15-6D-13-17 | 06 | 130S | 170E | 4300731261 | 16103 | Federal | GW | P | PETERS POINT |
| PP UF 3-36-12-16 | 36 | 120S | 160E | 4300731271 | 2470 | Federal | GW | P | PETERS POINT |
| PP UF 6-36-12-16 | 36 | 120S | 160E | 4300731272 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 6-35D-12-16 | 35 | 120S | 160E | 4300731275 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 14-26D-12-16 | 26 | 120S | 160E | 4300731277 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 8-34-12-16 | 34 | 120S | 160E | 4300731279 | 2470 | Federal | GW | P | PETERS POINT |
| PP ST 8-2D-13-16 (DEEP) | 02 | 130S | 160E | 4300731280 | 16069 | State | GW | P | |
| PPU FED 6-34D-12-16 | 34 | 120S | 160E | 4300731281 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 14-26D-12-15 | 35 | 120S | 150E | 4300731282 | 16224 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 2-35-12-15 | 35 | 120S | 150E | 4300731283 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 10-26D-12-15 | 35 | 120S | 150E | 4300731284 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 9-17-12-15 | 17 | 120S | 150E | 4300731287 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 1-17D-12-15 | 17 | 120S | 150E | 4300731288 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 7-17D-12-15 | 17 | 120S | 150E | 4300731289 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 7-1D-13-16 ULTRA DEEP | 06 | 130S | 170E | 4300731293 | 14692 | Federal | GW | P | PETERS POINT |
| PPU FED 1-18D-12-15 | 18 | 120S | 150E | 4300731294 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 7-18D-12-15 | 18 | 120S | 150E | 4300731295 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 5-17D-12-15 | 18 | 120S | 150E | 4300731296 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 10-17D-12-15 | 17 | 120S | 150E | 4300731307 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 8-17D-12-15 | 17 | 120S | 150E | 4300731308 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 12-17D-12-15 | 17 | 120S | 150E | 4300731309 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 13-17D-12-15 | 17 | 120S | 150E | 4300731310 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 14-17D-12-15 | 17 | 120S | 150E | 4300731311 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 16-18D-12-15 | 17 | 120S | 150E | 4300731312 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 8-18D-12-15 | 18 | 120S | 150E | 4300731313 | 14794 | Federal | GW | P | PRICKLY PEAR |

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| PPU FED 3-18D-12-15 | 18 | 120S | 150E | 4300731314 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 4-18-12-15 | 18 | 120S | 150E | 4300731315 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 5-18D-12-15 | 18 | 120S | 150E | 4300731316 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 6-18D-12-15 | 18 | 120S | 150E | 4300731317 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 16-27-12-16 | 27 | 120S | 160E | 4300731318 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 10-27D-12-16 | 27 | 120S | 160E | 4300731319 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 2-34D-12-16 | 34 | 120S | 160E | 4300731320 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 16-17D-12-15 | 17 | 120S | 150E | 4300731321 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU ST 15-16D-12-15 | 16 | 120S | 150E | 4300731322 | 14794 State | GW | P | PRICKLY PEAR |
| PPU ST 16-16D-12-15 | 16 | 120S | 150E | 4300731323 | 14794 State | GW | P | PRICKLY PEAR |
| PPU ST 14-16D-12-15 | 16 | 120S | 150E | 4300731324 | 14794 State | GW | P | PRICKLY PEAR |
| PPU FED 2-7D-13-17 DEEP | 06 | 130S | 170E | 4300731326 | 14692 Federal | GW | P | PETERS POINT |
| PPU FED 3-21D-12-15 | 21 | 120S | 150E | 4300731328 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 4-21D-12-15 | 21 | 120S | 150E | 4300731329 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 2-35D-12-16 | 35 | 120S | 160E | 4300731345 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 7-35D-12-16 | 35 | 120S | 160E | 4300731346 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 4-35D-12-16 | 35 | 120S | 160E | 4300731347 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 7-36D-12-16 | 36 | 120S | 160E | 4300731348 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 11-36D-12-16 | 36 | 120S | 160E | 4300731349 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 15-25D-12-16 | 36 | 120S | 160E | 4300731351 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 13-25D-12-16 | 36 | 120S | 160E | 4300731352 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 4-36D-12-16 | 36 | 120S | 160E | 4300731353 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 13-15D-12-15 | 22 | 120S | 150E | 4300731358 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 14-15D-12-15 | 22 | 120S | 150E | 4300731359 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 4-22D-12-15 | 22 | 120S | 150E | 4300731360 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 6-22D-12-15 | 22 | 120S | 150E | 4300731361 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 2-28D-12-15 | 28 | 120S | 150E | 4300731362 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 16X-21D-12-15 | 28 | 120S | 150E | 4300731363 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 5A-27D-12-15 | 28 | 120S | 150E | 4300731364 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 1-35D-12-16 | 35 | 120S | 160E | 4300731365 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 1A-28D-12-15 | 28 | 120S | 150E | 4300731368 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 14A-18D-12-15 | 18 | 120S | 150E | 4300731393 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 10-18D-12-15 | 18 | 120S | 150E | 4300731394 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 15A-18D-12-15 | 18 | 120S | 150E | 4300731395 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 16A-18D-12-15 | 18 | 120S | 150E | 4300731396 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 12-22D-12-15 | 22 | 120S | 150E | 4300731398 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 11-22D-12-15 | 22 | 120S | 150E | 4300731399 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 14-22D-12-15 | 22 | 120S | 150E | 4300731400 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 4A-27D-12-15 | 22 | 120S | 150E | 4300731401 | 14794 Federal | GW | P | PRICKLY PEAR |
| PPU FED 13-26D-12-16 | 26 | 120S | 160E | 4300731403 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 15-26D-12-16 | 26 | 120S | 160E | 4300731404 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 3-35D-12-16 | 26 | 120S | 160E | 4300731405 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 10-26D-12-16 | 26 | 120S | 160E | 4300731406 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 11-26D-12-16 | 26 | 120S | 160E | 4300731407 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 12-26D-12-16 | 26 | 120S | 160E | 4300731408 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 11-27D-12-16 | 27 | 120S | 160E | 4300731409 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 15-27D-12-16 | 27 | 120S | 160E | 4300731410 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 9-27D-12-16 | 27 | 120S | 160E | 4300731411 | 2470 Federal | GW | P | PETERS POINT |
| PPU FED 11-21D-12-15 | 21 | 120S | 150E | 4300731412 | 14794 Federal | GW | P | PRICKLY PEAR |

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|---|---|---|---|---|---|---|---|---|
| PPU FED 6-21D-12-15 | 21 | 120S | 150E | 4300731413 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 12-21D-12-15 | 21 | 120S | 150E | 4300731414 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 8-20D-12-15 | 20 | 120S | 150E | 4300731419 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 1A-20D-12-15 | 20 | 120S | 150E | 4300731420 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 2-20D-12-15 | 20 | 120S | 150E | 4300731421 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU ST 7A-16D-12-15 | 16 | 120S | 150E | 4300731422 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 6-16D-12-15 | 16 | 120S | 150E | 4300731423 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 10A-16D-12-15 | 16 | 120S | 150E | 4300731424 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 3-16D-12-15 | 16 | 120S | 150E | 4300731425 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU FED 1-34D-12-16 | 34 | 120S | 160E | 4300731427 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 7-34D-12-16 | 34 | 120S | 160E | 4300731428 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 5-35D-12-16 | 34 | 120S | 160E | 4300731429 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 5-21D-12-15 | 21 | 120S | 150E | 4300731451 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU ST 8-16D-12-15 | 16 | 120S | 150E | 4300731455 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 12-16D-12-15 | 16 | 120S | 150E | 4300731456 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 12A-16D-12-15 | 16 | 120S | 150E | 4300731457 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 15A-16D-12-15 | 16 | 120S | 150E | 4300731458 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 10-16D-12-15 | 16 | 120S | 150E | 4300731459 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 11A-16D-12-15 | 16 | 120S | 150E | 4300731460 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 13A-16D-12-15 | 16 | 120S | 150E | 4300731461 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU FED 3-34D-12-16 | 34 | 120S | 160E | 4300731466 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 5-34D-12-16 | 34 | 120S | 160E | 4300731467 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 4-34D-12-16 | 34 | 120S | 160E | 4300731468 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 10-7D-12-15 | 07 | 120S | 150E | 4300731470 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 15-7D-12-15 | 07 | 120S | 150E | 4300731471 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 9-7D-12-15 | 07 | 120S | 150E | 4300731472 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 16-7D-12-15 | 07 | 120S | 150E | 4300731473 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PPU FED 10-35D-12-16 | 35 | 120S | 160E | 4300731474 | 2470 | Federal | GW | P | PETERS POINT |
| PPU FED 9-35D-12-16 | 35 | 120S | 160E | 4300731476 | 2470 | Federal | GW | P | PETERS POINT |
| PPU ST 6A-16D-12-15 | 16 | 120S | 150E | 4300731477 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 4-16D-12-15 | 16 | 120S | 150E | 4300731478 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 4A-16D-12-15 | 16 | 120S | 150E | 4300731479 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 5A-16D-12-15 | 16 | 120S | 150E | 4300731480 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 3A-16D-12-15 | 16 | 120S | 150E | 4300731481 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 16A-16D-12-15 | 16 | 120S | 150E | 4300731484 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 9A-16D-12-15 | 16 | 120S | 150E | 4300731485 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 16B-16D-12-15 | 16 | 120S | 150E | 4300731514 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 14B-16D-12-15 | 16 | 120S | 150E | 4300731515 | 14794 | State | GW | P | PRICKLY PEAR |
| PPU ST 13B-16D-12-15 | 16 | 120S | 150E | 4300731516 | 14794 | State | GW | P | PRICKLY PEAR |
| PETERS POINT U FED 9-26D-12-16 | 25 | 120S | 160E | 4300750021 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 11-25D-12-16 | 25 | 120S | 160E | 4300750022 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 10-31D-12-17 | 31 | 120S | 170E | 4300750023 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 11-31D-12-17 | 31 | 120S | 170E | 4300750024 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 13A-31D-12-17 | 31 | 120S | 170E | 4300750025 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 13-31D-12-17 | 31 | 120S | 170E | 4300750026 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 14-31D-12-17 | 31 | 120S | 170E | 4300750027 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 14A-31D-12-17 | 31 | 120S | 170E | 4300750028 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 12-25D-12-16 | 25 | 120S | 160E | 4300750029 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 12-6D-13-17 | 31 | 120S | 170E | 4300750033 | 2470 | Federal | GW | P | PETERS POINT |

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|---|---|---|---|---|---|---|---|---|
| PETERS POINT U FED 10-25D-12-16 | 25 | 120S | 160E | 4300750035 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 13-36D-12-16 | 36 | 120S | 160E | 4300750037 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 15-36D-12-16 | 36 | 120S | 160E | 4300750038 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 11-1D-13-16 | 36 | 120S | 160E | 4300750039 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 12-1D-13-16 | 36 | 120S | 160E | 4300750040 | 2470 | Federal | GW | P | PETERS POINT |
| PRICKLY PEAR U FED 9-22D-12-15 | 22 | 120S | 150E | 4300750041 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 10-22D-12-15 | 22 | 120S | 150E | 4300750042 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 16-22D-12-15 | 22 | 120S | 150E | 4300750043 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 2-27D-12-15 | 22 | 120S | 150E | 4300750044 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 16-15D-12-15 | 15 | 120S | 150E | 4300750045 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 15-15D-12-15 | 15 | 120S | 150E | 4300750046 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 10-15D-12-15 | 15 | 120S | 150E | 4300750047 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 9-15D-12-15 | 15 | 120S | 150E | 4300750048 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 11A-15D-12-15 | 15 | 120S | 150E | 4300750049 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 1-21D-12-15 | 21 | 120S | 150E | 4300750050 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 2-21D-12-15 | 21 | 120S | 150E | 4300750051 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 2A-21D-12-15 | 21 | 120S | 150E | 4300750052 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 4A-22D-12-15 | 21 | 120S | 150E | 4300750053 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 5A-22D-12-15 | 21 | 120S | 150E | 4300750054 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 7A-21D-12-15 | 21 | 120S | 150E | 4300750056 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 8-21D-12-15 | 21 | 120S | 150E | 4300750057 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 8A-21D-12-15 | 21 | 120S | 150E | 4300750058 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 16-8D-12-15 | 08 | 120S | 150E | 4300750059 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 15-8D-12-15 | 08 | 120S | 150E | 4300750060 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 2-17D-12-15 | 08 | 120S | 150E | 4300750061 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 1A-17D-12-15 | 08 | 120S | 150E | 4300750062 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PETERS POINT U FED 3A-34D-12-16 | 27 | 120S | 160E | 4300750063 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 4A-34D-12-16 | 27 | 120S | 160E | 4300750064 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 12-27D-12-16 | 27 | 120S | 160E | 4300750065 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 13-27D-12-16 | 27 | 120S | 160E | 4300750066 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 13A-27D-12-16 | 27 | 120S | 160E | 4300750067 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 14-27D-12-16 | 27 | 120S | 160E | 4300750068 | 18204 | Federal | GW | P | |
| PETERS POINT U FED 14A-27D-12-16 | 27 | 120S | 160E | 4300750069 | 2470 | Federal | GW | P | PETERS POINT |
| PRICKLY PEAR U FED 1-22D-12-15 | 22 | 120S | 150E | 4300750076 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 2-22D-12-15 | 22 | 120S | 150E | 4300750077 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 8-22D-12-15 | 22 | 120S | 150E | 4300750078 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 3-17D-12-15 | 17 | 120S | 150E | 4300750079 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 3A-17D-12-15 | 17 | 120S | 150E | 4300750080 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 4-17D-12-15 | 17 | 120S | 150E | 4300750081 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 4A-17D-12-15 | 17 | 120S | 150E | 4300750082 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 5A-17D-12-15 | 17 | 120S | 150E | 4300750083 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 6-17D-12-15 | 17 | 120S | 150E | 4300750084 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 6A-17D-12-15 | 17 | 120S | 150E | 4300750085 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 7A-17D-12-15 | 17 | 120S | 150E | 4300750086 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 12A-17D-12-15 | 17 | 120S | 150E | 4300750087 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 9-12D-12-14 | 12 | 120S | 140E | 4300750088 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 10-12D-12-14 | 12 | 120S | 140E | 4300750089 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 15-12D-12-14 | 12 | 120S | 140E | 4300750090 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 16-12D-12-14 | 12 | 120S | 140E | 4300750091 | 14794 | Federal | GW | P | PRICKLY PEAR |

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| PRICKLY PEAR U FED 3-20D-12-15 | 20 | 120S | 150E | 4300750098 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 3A-20D-12-15 | 20 | 120S | 150E | 4300750099 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 4-20D-12-15 | 20 | 120S | 150E | 4300750100 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 4A-20D-12-15 | 20 | 120S | 150E | 4300750101 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 5-20D-12-15 | 20 | 120S | 150E | 4300750102 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 6-20D-12-15 | 20 | 120S | 150E | 4300750104 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 6A-20D-12-15 | 20 | 120S | 150E | 4300750105 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 11A-20D-12-15 | 20 | 120S | 150E | 4300750106 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR U FED 12A-20D-12-15 | 20 | 120S | 150E | 4300750107 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PETERS POINT U FED 5-31D-12-17 | 36 | 120S | 160E | 4300750109 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 6-31D-12-17 | 36 | 120S | 160E | 4300750116 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 9X-36D-12-16 | 36 | 120S | 160E | 4300750117 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 1-36D-12-16 | 36 | 120S | 160E | 4300750118 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 10-6D-13-17 | 06 | 130S | 170E | 4300750119 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT U FED 15-31D-12-17 | 06 | 130S | 170E | 4300750123 | 2470 | Federal | GW | P | PETERS POINT |
| PRICKLY PEAR UF 7A-18D-12-15 | 17 | 120S | 150E | 4300750136 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 8A-18D-12-15 | 17 | 120S | 150E | 4300750137 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 9A-18D-12-15 | 17 | 120S | 150E | 4300750138 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 12-20D-12-15 | 20 | 120S | 150E | 4300750139 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 16A-8D-12-15 | 08 | 120S | 150E | 4300750140 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 15A-8D-12-15 | 08 | 120S | 150E | 4300750141 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 13A-9D-12-15 | 08 | 120S | 150E | 4300750142 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 13-9D-12-15 | 08 | 120S | 150E | 4300750143 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 12-9D-12-15 | 08 | 120S | 150E | 4300750144 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 10-8D-12-15 | 08 | 120S | 150E | 4300750145 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 9-8D-12-15 | 08 | 120S | 150E | 4300750146 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 2A-17D-12-15 | 08 | 120S | 150E | 4300750147 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PETERS POINT UF 12-5D-13-17 | 06 | 130S | 170E | 4300750151 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 13-5D-13-17 | 06 | 130S | 170E | 4300750152 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 13-30D-12-17 | 30 | 120S | 170E | 4300750153 | 18347 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 14-30D-12-17 | 30 | 120S | 170E | 4300750154 | 18350 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 12-30D-12-17 | 30 | 120S | 170E | 4300750155 | 18346 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 11-30D-12-17 | 30 | 120S | 170E | 4300750156 | 18348 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 3-31D-12-17 | 30 | 120S | 170E | 4300750157 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 2-31D-12-17 | 30 | 120S | 170E | 4300750158 | 18349 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 16-25D-12-16 | 30 | 120S | 170E | 4300750159 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 9-25D-12-16 | 30 | 120S | 170E | 4300750160 | 2470 | Federal | GW | P | PETERS POINT |
| PRICKLY PEAR UF 1A-22D-12-15 | 22 | 120S | 150E | 4300750171 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 6A-22D-12-15 | 22 | 120S | 150E | 4300750173 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 7A-22D-12-15 | 22 | 120S | 150E | 4300750174 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 8A-22D-12-15 | 22 | 120S | 150E | 4300750175 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 14B-15D-12-15 | 22 | 120S | 150E | 4300750176 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 9-9D-12-15 | 09 | 120S | 150E | 4300750195 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 16-9D-12-15 | 09 | 120S | 150E | 4300750202 | 14794 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 8-14D-12-15 | 14 | 120S | 150E | 4300750216 | 18289 | Federal | GW | P | PRICKLY PEAR |
| PRICKLY PEAR UF 15-14D-12-15 | 14 | 120S | 150E | 4300750221 | 18290 | Federal | GW | P | PRICKLY PEAR |
| PETERS POINT UF 7X-36D-12-16 | 36 | 120S | 160E | 4300750231 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT UF 8-36D-12-16 | 36 | 120S | 160E | 4300750232 | 2470 | Federal | GW | P | PETERS POINT |
| PETERS POINT ST 6-2D-13-16 | 02 | 130S | 160E | 4300731017 | 14472 | State | D | PA | |

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| PTS 33-36 STATE | 36 | 110S | 140E | 4301330486 | 6190 | State | GW | PA | ARGYLE |
| PRICKLY PEAR U FED 10-4 | 10 | 120S | 140E | 4300730823 | 14462 | Federal | GW | S | |
| PRICKLY PEAR U FASSELIN 5-19-12-15 | 19 | 120S | 150E | 4300730860 | 14853 | Fee | GW | S | |
| PRICKLY PEAR U ST 5-16 | 16 | 120S | 150E | 4300730943 | 14794 | State | GW | S | PRICKLY PEAR |
| PRICKLY PEAR U FED 7-33D-12-15 | 33 | 120S | 150E | 4300730985 | 14771 | Federal | GW | S | |
| PETERS POINT ST 8-2D-13-16 | 02 | 130S | 160E | 4300731016 | 14471 | State | GW | S | |
| PPU FED 4-35D-12-15 | 35 | 120S | 150E | 4300731285 | 16223 | Federal | GW | S | PRICKLY PEAR |
| PPU FED 5-36D-12-16 | 36 | 120S | 160E | 4300731350 | 2470 | Federal | GW | S | PETERS POINT |
| PRICKLY PEAR U FED 5A-20D-12-15 | 20 | 120S | 150E | 4300750103 | 14794 | Federal | GW | S | PRICKLY PEAR |
| PRICKLY PEAR U FED 13A-17D-12-15 | 20 | 120S | 150E | 4300750108 | 14794 | Federal | GW | S | PRICKLY PEAR |
| PRICKLY PEAR UF 2A-22D-12-15 | 22 | 120S | 150E | 4300750172 | 14794 | Federal | GW | S | PRICKLY PEAR |

Lisha Cordova <lishacordova@utah.gov>

# Re: Enervest Operating - Prickly Pear U Fed 12-24/43-007-30953

1 message 43 007 30953 24 12S 14E

**Jim Davis** <jimdavis1@utah.gov> Tue, Aug 26, 2014 at 8:44 AM
To: Lisha Cordova <lishacordova@utah.gov>

Lisha,
Here's In-Lieu List 116. The lands you're interested in appear about 2/3 of the way down on the fourth page of the scan. Thanks for keeping up on this.
-Jim

On Wed, Aug 20, 2014 at 11:20 AM, Lisha Cordova <lishacordova@utah.gov> wrote:
2nd attempt...

---------- Forwarded message ----------
From: **Lisha Cordova** <lishacordova@utah.gov>
Date: Wed, Aug 20, 2014 at 11:16 AM
Subject: Enervest Operating - Prickly Pear U Fed 12-24/43-007-30953
To: "Jim Davis (SITLA)" <jimdavis@utah.gov>

Hi Jim,

In July you sent me an email confirming that SITLA is the surface owner of the above referenced well eff. 11/2/1923 by the actions of In-Lieu Selection List #116; please send me a copy so that DOGM can officially change the surface owner from Fed to State. Also, see attached inspections & recent insp pics. If you have any questions or concerns please call. Still waiting on updated info from Enervest regarding cleanup, will notify you when I get it ok.

Thanks,
Lisha

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*Lisha Cordova, Env. Scientist*
*Division of Oil, Gas and Mining*
*1594 W. North Temple, Suite 1210*
*Salt Lake City, Utah 84116*
*T: 801-538-5296*
*C: 801-396-3902*
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*Lisha Cordova, Env. Scientist*
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*T: 801-538-5296*

4—309A.

# APPROVED LIST NO. 116 OF

*EXHIBITING the tracts selected by the State of* UTAH *in the school lands, or losses to its grant for the support of Common Schools, assigned as bases for the* (25 Stat., 107) and February 25, 1891 (26 Stat., 796), amending Sections 2275 and 2276, R. S.

6—1307

| CAUSE OF LOSS. | DESCRIPTION OF BASES. | SECTION. | TOWNSHIP. | RANGE. | MERIDIAN. | AREA OF TRACTS. ACRES. | TOTAL AREA OF BASES. ACRES. |
|---|---|---|---|---|---|---|---|
| National Forest | S½ SW¼ | 2 | 33 S | 1 W | S.Lake | 80 | |
| " " | W½ NE¼ | 16 | 33 S | 1 W | " | 80 | |
| Fractional Township | Deficiency | | 9 N | 8 E | " | 28 44 | 188 44 |
| National Forest | SE¼ SE¼ | 16 | 1 N | 20 E | " | | 40 |
| " " | SE¼ NW¼ | 2 | 1 N | 18 E | " | | 40 |
| Patented Entry | NW¼ NE¼ | 32 | 4 S | 21 E | " | 40 | |
| " " | NE¼ NE¼ | 32 | 4 S | 22 E | " | 40 | 80 |
| Uintah Indian Reservation | NW¼, SW¼ NE¼ & NE¼ SE¼ | 32 | 6 S | 9 W | Uinta | 240 | |
| " " " | Part of NW¼ SE¼ | 32 | 6 S | 9 W | " | 26 56 | 266 56 |
| National Forest | Part of frl,uns'd protrac'd | 2 | 18 S | 5 E | S.Lake | 10 | |
| " " | " " " " " | 2 | 20 S | 4 E | " | 26 90 | |
| " " | " " " " " | 2 | 20 S | 5 E | " | 309 79 | 346 69 |
| " " | SW¼ SW¼ | 32 | 25 S | 6 W | " | 40 | |
| " " | NE¼ NE¼ | 16 | 25 S | 6 W | " | 40 | 80 |
| " " | NW¼ SE¼,S½ SE¼ & SW¼ | 2 | 20 S | 3 W | " | 280 | |
| " " | NE¼ NE¼ | 36 | 30 S | 6 W | " | 40 | 320 |
| " " | Part of frl,uns'd protrac'd | 2 | 20 S | 5 E | " | 80 | |
| " " | " " " " " | 2 | 31 S | 2 E | " | 240 | |
| " " | " " " " " | 2 | 31 S | 3 E | " | 240 | |
| " " | " " " " " | 2 | 31 S | 4 E | " | 40 | 600 |
| " " | SW¼ SE¼ & SW¼ | 16 | 30 S | 5 W | " | | 200 |
| Patented Mineral Entry | NW¼ NW¼ & SE¼ NW¼ | 32 | 1 S | 18 W | " | | 80 |
| National Forest | Lot 4 | 16 | 30 S | 4 W | " | 35 48 | |
| Patented Mineral Entry | Lot 1 | 2 | 1 S | 18 W | " | 39 41 | |
| " " " | Part of Lot 2 | 2 | 1 S | 18 W | " | 3 84 | |
| " " " | SW¼ NW¼ & S½ | 32 | 1 S | 18 W | " | 360 | |
| " " " | N½ NE¼, | 36 | 1 S | 18 W | " | 80 | 518 73 |
| National Forest | NW¼NE¼,S½NE¼,N½NW¼,N½SW¼ | 32 | 11 N | 3 E | " | | 280 |
| " " | Part of Lot 3 | 32 | 32 S | 7 W | " | 10007 | |
| " " | Part of Lot 4 | 32 | 32 S | 7 W | " | 32 01 | |
| " " | W½ NE¼, NW¼, NW¼ SE¼,NW¼SW¼ | 36 | 33 S | 7 W | " | 320 | |
| " " | Part of Lot 1 | 36 | 32 S | 7 W | " | 35 75 | |
| " " | Part of Lot 3 | 36 | 32 S | 7 W | " | 28 22 | |
| " " | Part of Lot 4 | 36 | 32 S | 7 W | " | 32 04 | |
| " " | NE¼ NE¼ | 32 | 35 S | 8 W | " | 40 | 498 09 |
| " " | NE¼ SW¼ | 2 | 32 S | 1 W | " | 40 | |
| " " | NE¼ SE¼ & N½ | 2 | 38 S | 4 W | " | 360 | 400 |
| " " | SW¼ NW¼ | 2 | 38 S | 4½W | " | 40 | |
| " " | SW¼ NE¼ b | 2 | 8 N | 4 E | " | 40 | 80 |
| " " | NW¼NW¼,S½NW¼,N½SE¼,NE¼SW¼ | 32 | 8 N | 4 E | " | | 240 |
| " " | Lots 5,6,7,8, 9 & 10 | 2 | 22 S | 2½W | " | 240 | |
| " " | Lots 11, 12 & N½ SE¼ | 2 | 22 S | 2½W | " | 160 | |
| " " | Part of Lot 4 | 2 | 8 N | 4 E | " | 27 44 | |
| " " | Part of Lot 4 | 36 | 8 N | 4 E | " | 16 84 | 444 28 |
| " " | S½NW¼,NW¼SE¼,S½SE¼, & SW¼ | 16 | 26 S | 6 W | " | 360 | |
| " " | Lot 21 | 36 | 22 S | 3 W | " | 22 80 | |
| " " | Part of Lot 22 | 36 | 22 S | 3 W | " | 14 70 | 397 50 |
| " " | S½ SW¼ | 36 | 27 S | 6 W | " | 80 | |
| " " | NE¼ & N½ NW¼ | 16 | 28 S | 5 W | " | 240 | 320 |
| | | | | | Carried forward | | 5420 29 |

# SCHOOL INDEMNITY LANDS.

SALT LAKE CITY Land District, in lieu of, or as indemnity for, the corresponding selections, which were made under the provisions of the Acts of Congress approved July 16, 1894 Revised Statutes, as made applicable to said State by the Act of Congress approved May 3, 1902 (32 Stat. 188)

9—1207

| DATE OF SELECTION. | NUMBER OF LIST. | DESCRIPTION OF TRACTS SELECTED. | SECTION. | TOWNSHIP. | RANGE. | MERIDIAN. | AREA OF TRACTS. ACRES. | TOTAL AREA OF SELECTION. ACRES. |
|---|---|---|---|---|---|---|---|---|
| Coal reserved to the United States under the act of June 22, 1910 (36 Stat., 583), as supplemented by the Act of April 30, 1912 (37 Stat., 105). | | | | | | | | |
| October 29, 1915 | 016236 | Lots 1, 2 & 4. 8875 | 1 | 11 S | 7 E | S. Lake | 148 44 | Utah 188 44 |
| " " " | " | SE¼ SE¼ 8877 | 13 | 11 S | 7 E | " | 40 | " |
| November 29, 1915 | 016440 | SE¼ SW¼ 8892 | 13 | 11 S | 7 E | " | | " 40 |
| September 29, 1916 | 018266 | NE¼ SE¼ 8969 | 10 | 13 S | 7 E | " | | Garfield 40 |
| February 23, 1917 | 020134 | W½ SE¼ 9039 | 27 | 17 S | 16 E | " | | Emery 80 |
| August 6, 1918 | 023355 | SW¼ SE¼ | 25 | 11 S | 7 E | " | 40 | Utah |
| " " " | " | Lots 2,6,7,8,NW¼SE¼,SE¼SE¼ 9348 | 31 | 11 S | 8 E | " | 226 56 | " 266 56 |
| February 20,1920 | 025403 | Lot 1 9287 | 7 | 13 S | 9 E | " | 36 90 | Garfield |
| " " " | " | Lots 7,8,12,13,14 & 18 9111 | 30 | 39 S | 4 W | " | 240 | Kane |
| " " " | " | Lots 3 & 5 " | 31 | 39 S | 4 W | " | 69 79 | " 346 69 |
| April 7, 1920 | 026003 | E½ SW¼ 9266 9234 | 33 | 20 S | 2 E | " | | Sevier 80 |
| May 18, 1920 | 026297 | NE¼ SE¼ | 6 | 12 S | 9 E | " | 40 | Carbon |
| " " " | " | SW¼ NE¼, W½ SE¼ & SE¼ SW¼ 9234 | 7 | 12 S | 9 E | " | 160 | " |
| " " " | " | SE¼ NW¼ " | 8 | 12 S | 9 E | " | 40 | " |
| " " " | " | S½ NE¼ " | 18 | 12 S | 9 E | " | 80 | " 320 |
| June 18, 1920 | 026537 | W½ NE¼ & W½ SE¼ 9511 | 24 | 11 S | 7 E | " | 160 | Utah |
| " " " | " | SW¼ NW¼, W½ SW¼ & SW¼ SW¼ " | 24 | 11 S | 7 E | " | 160 | " |
| " " " | " | NW¼ & SW¼ NE¼ " | 25 | 11 S | 7 E | " | 200 | " |
| " " " | " | NE¼ SE¼ & SW¼ SE¼ " | 25 | 11 S | 7 E | " | 80 | " 600 |
| June 30, 1920 | 026607 | SE¼SW¼, W½SE¼, NE¼SE¼, SE¼NE¼ 9545 | 17 | 11 S | 8 E | " | | " 200 |
| July 6, 1920 | 026689 | NE¼ SW¼ & NW¼ NE¼ | 14 | 39 S | 9 W | " | | Kane 80 |
| " " " | 026680 | W½ SW¼, 9529 | 29 | 12 S | 13 E | " | 80 | Carbon |
| " " " | " | E½ NE¼, NE¼ SE¼ & Lot 6 " | 31 | 12 S | 13 E | " | 152 47 | " |
| " " " | " | SE¼, E½ NE¼ & Lot 1 " | 30 | 12 S | 13 E | " | 286 26 | " 518 73 |
| July 9, 1920 | 026707 | W½NE¼, NE¼NW¼, NE¼SW¼, NW¼ SE¼ 9494 | 28 | 38 S | 10 W | " | 200 | Washington |
| " " " | " | W½ SW¼ 9441 | 33 | 20 S | 2 E | " | 80 | Sevier 280 |
| July 23, 1920 | 026787 | Lot 2, SE¼NW¼, NE¼SW¼, W½NE¼ 9214 | 19 | 12 S | 7 E | " | 194 65 | Carbon |
| " " " | " | Lots 1,2,NE¼NW¼,E½NE¼, " | 30 | 12 S | 7 E | " | 191 40 | " |
| " " " | " | SE¼ SW¼ 9501 | 30 | 11 S | 10 E | " | 40 | Sucrepe |
| " " " | " | NE¼ SW¼ & Lot 5 " | 31 | 11 S | 10 E | " | 72 04 | " 498 09 |
| July 26, 1920 | 026803 | NW¼NE¼, SE¼SE¼, NW¼SE¼, NE¼SW¼ 9420 | 9 | 13 S | 8 E | " | 160 | Carbon |
| " " " | " | E½ NW¼ & SW¼ " | 10 | 13 S | 8 E | " | 240 | " 400 |
| " " " | 026805 | SW¼ SE¼ 9491 | 25 | 11 S | 10 E | " | 40 | Sucrepe |
| " " " | " | NW¼ NE¼ 9511 | 18 | 22 S | 4 E | " | 40 | Sevier 80 |
| August 10, 1920 | 026881 | NW¼ SW¼ 8910 | 14 | 39 S | 9 W | " | 40 | Kane |
| " " " | " | NW¼ NE¼ 8911 | 18 | 39 S | 9 W | " | 40 | " |
| " " " | " | SW¼ NE¼, N½ SE¼ & SE¼ SE¼ 9516 | 20 | 38 S | 10 W | " | 160 | Washington 240 |
| August 28, 1920 | 027019 | SE¼ NE¼ 9197 | 24 | 12 S | 12 E | " | 40 | Carbon |
| " " " | " | Lot 10,NE¼SW¼,N½SE¼,SE¼NE¼ " | 19 | 12S | 13 E | " | 204 28 | " |
| " " " | " | S½ NW¼, NE¼ SW¼ & SW¼ SW¼ " | 20 | 12 S | 13 E | " | 160 | " |
| " " " | " | NW¼ NW¼ " | 29 | 12 S | 13 E | " | 40 | " 444 28 |
| September 16,1920 | 027149 | SW¼ NW¼ & SW¼ SW¼ | 26 | 11 S | 10 E | " | 80 | Sanpete |
| " " " | " | E½ SE¼,NW¼ SE¼ & SE¼ SW¼ " | 27 | 11 S | 10 E | " | 160 | " |
| " " " | " | NE¼ NW¼,NE¼ NE¼ & SW¼ NE¼ " | 34 | 11 S | 10 E | " | 120 | " |
| " " " | " | Lot 3 " | 35 | 11 S | 10 E | " | 37 50 | " 397 50 |
| October 14, 1920 | 027383 | E½ NE¼ & E½ SW¼ 9524 | 11 | 40 S | 9 W | " | 160 | Kane |
| " " " | " | W½ SW¼, NE¼ SW¼ & NW¼ SE¼ " | 1 | 40 S | 9 W | " | 160 | " 320 |
| | | | | | | Carried forward | | 5480 89 |

4—309A.

# APPROVED LIST NO. 116 OF

*EXHIBITING the tracts selected by the State of* UTAH *in the school lands, or losses to its grant for the support of Common Schools, assigned as bases for the*

4—1307

| CAUSE OF LOSS. | DESCRIPTION OF BASES. | SECTION. | TOWNSHIP. | RANGE. | MERIDIAN. | AREA OF TRACTS. ACRES. | TOTAL AREA OF BASES. ACRES. |
|---|---|---|---|---|---|---|---|
| | | | | | Brought Forward | | 5420 29 |
| National Forest | Lot 1 | 2 | 28 S | 4 W | S. Lake | 30 32 | |
| " " | Part of Lot 2 | 2 | 28 S | 4 W | " | 4 16 | |
| " " | S½ NW¼ & S½ | 16 | 28 S | 5 W | " | 400 | |
| " " | NE¼ & NE¼ NW¼ | 36 | 25 S | 3 W | " | 200 | 634 48 |
| Zion National Park. | N½ SW¼ & SE¼ SW¼ | 16 | 40 S | 10 W | " | 120 | |
| " " " | Part of SW¼ SW¼ | 16 | 40 S | 10 W | " | 35 02 | 155 02 |
| National Forest | S½ NE¼ | 32 | 3 S | 9 E | " | | 80 |
| Uintah Indian Reservation | Lot 8 | 2 | 3 S | 4 W | Uinta | 40 62 | |
| " " " | Part of Lot 2 | 2 | 5 S | 10 W | " | 40 68 | |
| " " " | Part of Lot 4 | 2 | 6 S | 8 W | " | 40 72 | |
| " " " | Part of Lot 6 | 2 | 4 S | 3 W | " | 40 78 | |
| " " " | N½ NE¼ | 36 | 5 S | 9 W | " | 80 | 242 80 |
| " " " | S½ SE¼ & SW¼ | 32 | 6 S | 5 W | " | 240 | |
| " " " | N½ NE¼ & SE¼ NE¼ | 36 | 6 S | 5 W | " | 120 | 360 |
| National Forest | S½ NE¼, S½ NW¼, S½ &Lot 20 | 2 | 24 S | 5 W | S.Lake | 520 | |
| " " | N½ NE¼ & SE¼ NE¼ | 32 | 23 S | 3 W | " | 120 | 640 |
| " " | NW¼NE¼, S½NE¼, NW¼ & S½ | 16 | 5 S | 7 W | " | 600 | |
| " " | NE¼ NE¼ | 36 | 31 S | 4 W | " | 40 | 640 |
| Patented Mineral Entry | W½ of NW¼ of SE¼ | 36 | 1 S | 18 W | S.Lake | 20 | |
| " " " | Part of Lot 1 | 2 | 2 S | 18 W | " | 10 20 | |
| " " " | Lot 2 | 2 | 2 S | 18 W | " | 40 08 | |
| " " " | W½ of SW¼ of SE¼ | 36 | 1 N | 18 W | " | 20 | |
| " " " | E½ of SW¼ of SW¼ | 36 | 1 N | 18 W | " | 20 | |
| " " " | Lots 3, 4, & N½ SE¼ | 2 | 2 S | 18 W | " | 160 16 | |
| " " " | Part of SE¼ SE¼ | 2 | 2 S | 18 W | " | 17 84 | |
| " " " | SW¼SE¼, S½SW¼ & SE¼ SW¼ | 2 | 2 S | 18 W | " | 160 | |
| National Forest | Part of Lot 3 | 2 | 11 N | 3 E | " | 22 81 | 471 09 |
| | | | | | TOTAL | | 8,643 68 |

# SCHOOL INDEMNITY LANDS.

SALT LAKE CITY *Land District, in lieu of, or as indemnity for, the corresponding selections, which were made under the provisions of the Acts of Congress approved*

| DATE OF SELECTION. | NUMBER OF LIST. | DESCRIPTION OF TRACTS SELECTED. | SECTION. | TOWNSHIP. | RANGE. | MERIDIAN. | AREA OF TRACTS. ACRES. | TOTAL AREA OF SELECTION. ACRES. |
|---|---|---|---|---|---|---|---|---|
| | | **Coal reserved to the United States under the Act of June 22, 1910 (36 Stat., 583), as supplemented by the Act of April 30, 1912 (37 Stat., 105).** | | | | | Brought forward | 5420 29 |
| October 14, 1920 | 027384 | SW¼ NW¼ | 5 | 39 S | 9 W | S. Lake | 40 | Kane |
| " " " | " | Lot 1 | 6 | 39 S | 9 W | " | 34 48 | " |
| " " " | " | W½ SW¼ | 8 | 39 S | 9 W | " | 80 | " |
| " " " | " | W½ SW¼ | 11 | 39 S | 9 W | " | 80 | " |
| " " " | " | SW¼ SW¼ | 14 | 39 S | 9 W | " | 40 | " |
| " " " | " | NW¼ NW¼ | 17 | 39 S | 9 W | " | 40 | " |
| " " " | " | NE¼ NE¼ & NW¼ SE¼ | 18 | 39 S | 9 W | " | 80 | " |
| " " " | " | S½ NE¼ & SE¼ NW¼ | 19 | 39 S | 9 W | " | 120 | " |
| " " " | " | NE¼ NE¼ | 22 | 39 S | 9 W | " | 40 | " |
| " " " | " | NE¼ SE¼ & SE¼ SW¼ | 23 | 39 S | 9 W | " | 80 | 634 48 |
| January 19, 1921 | 027903 | W½ NE¼, SE¼ NW¼ & Lot 1 | 25 | 11 S | 8 E | " | Utah | 155 02 |
| April 14, 1921 | 029504 | SW¼ SW¼ | 21 | 12 S | 10 E | " | 40 | Carbon |
| " " " | " | NE¼ NE¼ | 29 | 12 S | 10 E | " | 40 | " 80 |
| | | **Phosphate reserved to the United States under the Act of July 17, 1914 (38 Stat., 509).** | | | | | | |
| July 29, 1917 | 021546 | Lots 1, 2, 3, 4, SE¼NE¼, SW¼NW¼ | 1 | 7 E | 3 E | S. Lake | | 248 80 |
| " " " | 021547 | E½ SE¼, SE¼ NE¼, & W½ NE¼ | 10 | 7 E | 3 E | " | 200 | " |
| " " " | " | E½ SW¼, SW¼ SW¼ & SW¼ NW¼ | 10 | 7 E | 3 E | " | 160 | " 360 |
| | | **Oil and gas reserved to the United States under the act of July 17, 1914 (38 Stat., 509).** | | | | | | |
| April 24, 1920 | 026120 | E½ SE¼ | 19 | 13 S | 15 E | S. Lake | 80 | Carbon |
| " " " | " | S½ | 20 | 13 S | 15 E | " | 320 | " |
| " " " | " | W½ SE¼ & SW¼ | 21 | 13 S | 15 E | " | 240 | " 640 |
| July 9, 1920 | 026710 | E½ | 23 | 12 S | 14 E | " | 320 | " |
| " " " | " | SW¼NE¼, SW¼, NW¼SE¼, & S½NW¼ | 24 | 12 S | 14 E | " | 320 | " 640 |
| | | **Coal reserved to the United States under the act of June 22, 1910 (36 Stat., 583), as supplemented by the act of April 30, 1912 (37 Stat., 105), and oil and gas reserved to the United States under the act of July 17, 1914 (38 Stat., 509).** | | | | | | |
| July 6, 1920 | 026682 | Lots 1, 2, 3 & 4 | 6 | 14 S | 16 E | S. Lake | 150 70 | Carbon |
| " " " | " | SE¼SW¼, Lots 2, 3, 4, NE¼NW¼ | 31 | 13 S | 16 E | " | 200 39 | " |
| " " " | " | E½ SW¼ & SE¼ NW¼ | 30 | 13 S | 16 E | " | 120 | " 471 09 |
| | | | | | | | TOTAL | 8,683.68 |

Enervest Oper.
Prickly Pear U
Fed 12-24
43-007-30953

DEPARTMENT OF THE INTERIOR

GENERAL LAND OFFICE

Washington, D. C., October 19, 1923.

This certifies that the tracts of land described in the foregoing list have been carefully examined and compared with the township plats and tract books in this office and the same have been found to inure to the State of Utah under its grant for the purpose stated, being free from conflicts or other adverse claims of record. All of the selected lands are embraced in coal, oil and gas, or phosphate withdrawals or reserves, as shown on the face of the list. Some of the lands which are withdrawn for coal have been classified as coal lands at a stated price. All of the withdrawals and reserves were made prior to date of selection of the lands. The State has consented in writing to take title to all of such selected lands with reservation to the United States of all of the mineral deposits therein for which they have been withdrawn, classified, or reserved, in accord with the acts of June 22, 1910 (36 Stat., 583) as supplemented by the act of April 30, 1912 (37 Stat., 105), and July 17, 1914 (38 Stat., 509), as the case may be. The selected lands are not embraced in any other withdrawal or reservation in so far as the records of this office show. The records here do not indicate that any of the selected lands are valuable for minerals other than those above specified. The Geological Survey has reported that the records of that office indicate that the selected lands contain no valuable deposits of mineral other than that for which they have been withdrawn or reserved.

(Signed) Frost Scuffle
Examiner

APPROVED:

(Signed) J. H. Priesbook
Chief, Division "D".

DEPARTMENT OF THE INTERIOR

GENERAL LAND OFFICE

Washington, D. C., November 1, 1923.

It is hereby certified that the tracts of land described in this list, No. 136, are embraced in the original lists on file in this office of lands selected by the State of Utah, pursuant to the laws of that State, in the Salt Lake City land district, as indemnity for losses in the sections and townships named, which school land indemnity selections are authorized by the acts of Congress cited.

It is further certified that the lands reported lost or deficient in said list and those selected in lieu thereof have been examined and compared with the township plats and tract books in this office; that the indemnity lands claimed have been found to be properly due the townships for which they were selected and the selected lands are shown to be subject to such selection being public lands within the limits of said State, free from adverse claims of record. It is disclosed by the records of this office, as indicated on the face of this list, that all of the selected lands have been withdrawn, classified or reserved as coal lands or as valuable for oil, gas or phosphate. All of the lands are still so withdrawn, classified or reserved. The State has filed written waivers of all its claim or right to the coal, oil, gas or phosphate in the lands and has consented to take title to such lands in accord with the acts of June 22, 1910 (36 Stat., 583) and July 17, 1914 (38 Stat., 509), as the case may be.

It is, therefore, recommended that the selections in this list, embracing 8,643.68 acres, be approved subject to any valid interfering rights existing at date of selection, but, as shown on the face of the list, excepting and reserving to the United States all the coal, oil, gas and phosphate in the selected lands, and to the United States or persons authorized by the United States the right to prospect for, mine and remove the coal, oil, gas or phosphate from the same, upon compliance with the conditions and subject to the provisions, and limitations of the act of Congress approved June 22, 1910 (as to coal) and July 17, 1914 (as to oil, gas and phosphate), supra, and excepting and reserving to the United States rights of way over and across the said selected lands for ditches or canals constructed by authority of the United States, all as directed and required by the act of Congress approved August 30, 1890 (26 Stat., 391).

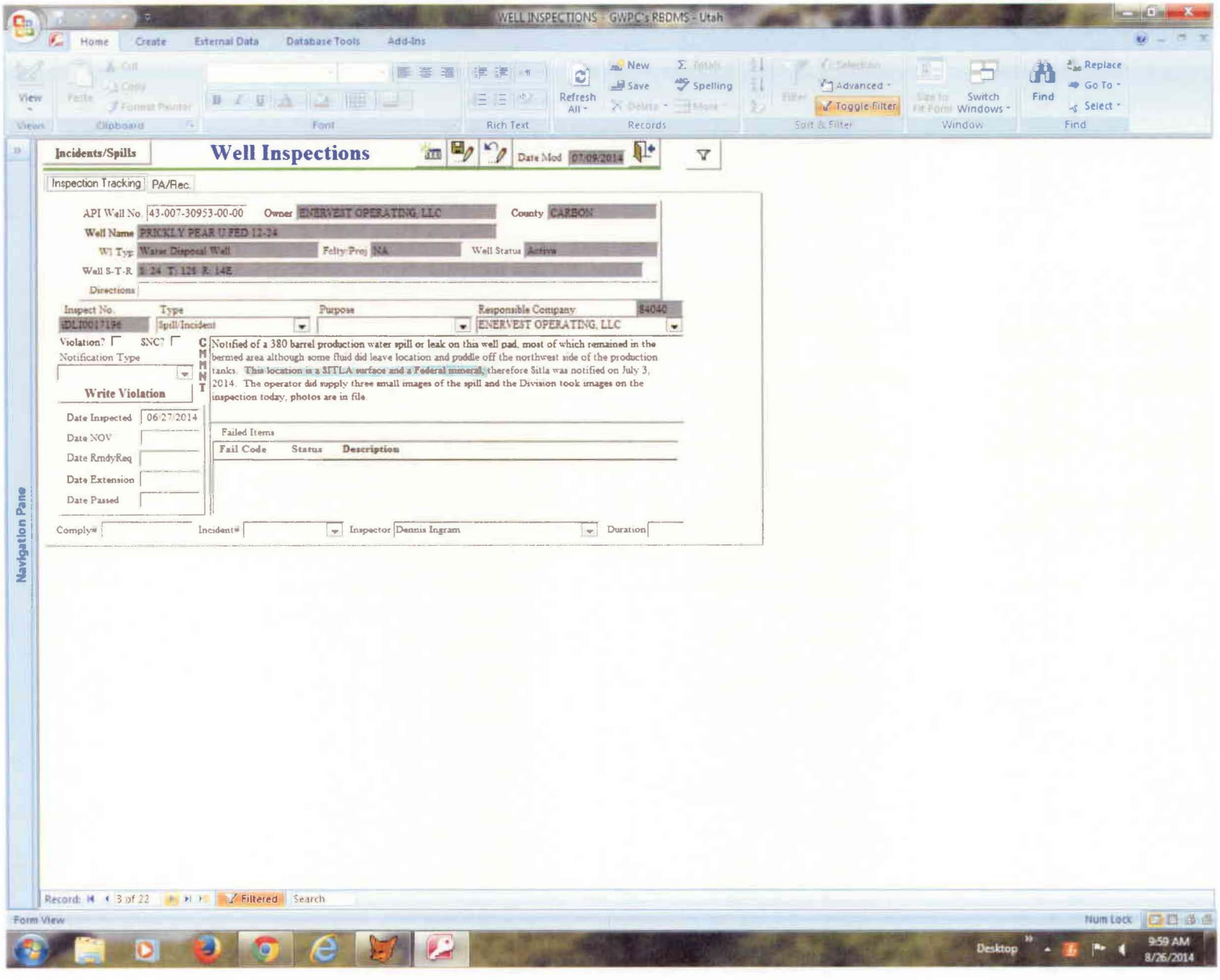
(Signed) William Spry
Commissioner

DEPARTMENT OF THE INTERIOR
OFFICE OF THE SECRETARY

Washington, D. C., November 2, 1923

The foregoing selections embracing 8,643.68 acres, are hereby approved subject to any valid interfering rights existing at date of selection, but, as shown on the face of the list, excepting and reserving to the United States all the coal, oil, gas or phosphate in the selected lands and to the United States or persons authorized by the United States, the right to prospect for, mine and remove from such lands, the deposits of mineral for which they have been withdrawn, classified or reserved, upon compliance with the conditions and subject to the provisions and limitations of the acts of Congress approved June 22, 1910 (36 Stat., 583) and July 17, 1914 (38 Stat., 509), and excepting and reserving to the United States rights of way over and across said selected lands for ditches or canals constructed by authority of the United States, all as directed and required by the act of Congress approved August 30, 1890 (26 Stat., 391).

(Signed) E. C. Finney
First Assistant Secretary


WELL INSPECTIONS : GWPC's RBDMS - Utah
Home
Create
External Data
Database Tools
Add-Ins
Refresh All
New
Save
Spelling
Delete
Advanced
Toggle Filter
Find
Replace
Go To
Select
Switch Windows
Incidents/Spills
Well Inspections
Date Mod 07/09/2014
Inspection Tracking
PA/Rec
API Well No 43-007-30953-00-00
Owner ENERVEST OPERATING, LLC
County CARBON
Well Name PRICKLY PEAR U FED 12-24
Wl Typ Water Disposal Well
Fclty/Proj NA
Well Status Active
Well S-T-R 12 24 T. 12S R. 14E
Directions
Inspect No
DLI0017196
Type
Spill/Incident
Purpose
Responsible Company
84040
ENERVEST OPERATING, LLC
Violation?
SNC?
Notification Type
Write Violation
Notified of a 380 barrel production water spill or leak on this well pad, most of which remained in the bermed area although some fluid did leave location and puddle off the northwest side of the production tanks. This location is a SITLA surface and a Federal mineral, therefore Sitla was notified on July 3, 2014. The operator did supply three small images of the spill and the Division took images on the inspection today, photos are in file.
Date Inspected 06/27/2014
Date NOV
Date RmdyReq
Date Extension
Date Passed
Failed Items
Fail Code
Status
Description
Comply#
Incident#
Inspector Dennis Ingram
Duration
Navigation Pane
Record: 3 of 22
Filtered
Search
Form View
Num Lock
Desktop
9:59 AM
8/26/2014